

# SPRAGUE <br> the mark of reliability 

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## INTEGRATED CIRCUITS DATA BOOK

INTERFACE CIRCUITS<br>- High Voltage<br>- High Current<br>- BiMOS and Complex Arrays

## LINEAR CIRCUITS

- Radio
- Television
- Audio


## HALL EFFECT DEVICES

TRANSISTOR ARRAYS

## SPRAGUE ELECTRIC COMPANY

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| :--- | :--- |

BiMOS AND COMPLEX ARRAY INTERFACE DRIVERS

INDUSTRIAL, MILITARY, AND AEROSPACE DEVICES

| RADIO INTEGRATED CIRCUITS |  |
| :--- | :--- |
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AUDIO INTEGRATED CIRCUITS

HALL EFFECT DEVICES

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UGN-3013T/U
UGN/UGS-3019T/U
UGN/UGS-3020T/U
UGN/UGS-3030T/U
UGN-3040T/U
UGN/UGS-3075T/U
UGN/UGS-3076T/U
UGN-3201M and 3203M
UGN-3220S
ULN-3304M
ULN-3305M
ULN-3306M
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## Sprague Part Numbering Systems


$N=$ COMMERCIAL/INDUSTRIAL, SEE DETAIL SPECIFICATIONS
$Q=$ EXTENDED $\left(-40^{\circ} \mathrm{C} T 0+85^{\circ} \mathrm{C}\right)$
$S=$ FULL MILITARY $\left(-55^{\circ} \mathrm{C} T 0+125^{\circ} \mathrm{C}\right)$
$X=$ SPECIAL SIGNIFIER FOR PRE-PRODUCTION DEVICES
FAMILY (UC, UD, UG, UL, OR UT).

## Sprague Part Numbering Systems

$]^{\mathrm{UH}}{ }^{\mathrm{D}}-\frac{400}{1}$<br>1 = SELECTED VERSION, SEE DETALL SPECIFICATIONS<br>MIL = MLLITARY GRADE WITH SCREENING TO MIL-STD-883, CLASS B (PACKAGES C AND D ONLY)<br>DEVICE TYPE (THREE DIGITS).<br>PACKAGE DESIGNATION.<br>C = GLASS/METAL HERMETIC, 14-PIN FLAT PACK<br>D = GLASS/METAL HERMETIC, 14 OR 16-PIN DUAL IN-LINE<br>$K=$ UNPACKAGED CHIP OR PROBED WAFER<br>P = PLASTIC, 14-, 16-, OR 18-PIN DUAL IN-LINE

FAMILY (UH ONLY)


## CROSS-REFERENCE in Numerical Order

The suggested Sprague replacement devices are based on similarity as shown in currently published data. Exact replacement in all applications is not guaranteed and the user should compare the specifications of the competitive and recommended Sprague replacement.

| Mfr. Abbreviations: |  |
| :--- | :--- |
| CS | Cherry Semiconductor |
| DI | Dionics, Inc. |
| EXR | Exar Integrated Systems |
| FER | Ferranti Limited |
| FSC | Fairchild Semiconductor |
| GE | General Electric* |
| HIT | Hitachi Ltd. |
| ITT | ITT Semiconductors |
| MIT | Mitsubishi Electric Corp. |
| MOT | Motorola Semiconductor |
| NEC | Nippon Electric Co. |
| NS | National Semiconductor |
| OKI | Oki Semiconductor |
| PE | Pro-Electron $\ddagger$ |
| PLS | Plessey Semiconductor |
| RCA | RCA |
| RFA | Rifa |
| SANY | Sanyo |
| SG | Silicon General Inc. |
| SIG | Signetics Corp. |
| SGS | SGS/ATES |
| SPC | Sprague Products Co.* |
| SPR | Sprague Electric Co. |
| TI | Texas Instruments |
| TLF | AEG-Telefunken |
| TOKO | RCL Toko |
| TOS | Toshiba Corp. |


| Competitive |  | Suggested <br> Part |
| :--- | :--- | :--- |
| Number |  | Sprague <br> Replacement |
| CA758E | Mfr. | ULX-3811A§ |
| CA1190E | RCA | ULN-2290B |
| CA1190Q | RCA | ULN-22900 |
| CA1310E | RCA | ULN-3810A |
| CA1391E | RCA | ULN-2291M* |
| CA1394E | RCA | ULN-2294M* |
| CA1398E | RCA | ULN-2298A* |
| CA2002 | RCA | ULN-3701Z |
| CA2002M | RCA | ULN-3701ZH |
| CA2004 | RCA | ULN-37022 |
| CA2004M | RCA | ULN-3702ZH |
| CA2111AE | RCA | ULN-2111A |
| CA2136AE | RCA | ULN-2136A |
| CA3045 | RCA | ULS-2045H |
| CA3045F | RCA | ULS-2045H |
| CA3046 | RCA | ULN-2046A |
| CA3054 | RCA | ULN-2054A |
| CA3064E | RCA | ULN-2264A* |
| CA3065 | RCA | ULN-2165A* |
| CA3066 | RCA | ULN-2266A* |
| CA3067 | RCA | ULN-2267A* |
| CA3070 | RCA | ULN-2124A* |
| CA3071 | RCA | ULN-2127A* |
| CA3072 | RCA | ULN-2228A* |
| CA3075 | RCA | ULN-2129A* |

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[^1]| Competitive Part Number | Mfr. | Suggested <br> Sprague <br> Replacement | Competitive Part <br> Number | Mfr. | Suggested Sprague Replacement |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LA3089 | SANY | ULN-2289A* | LM3070N | NS | ULN-2124A* |
| LA3301 | SANY | ULN-3810A-1 | LM30712 | NS | ULN-2127A* |
| LA3350 | SANY | ULN-3810A | LM3072N | NS | ULN-2228A* |
| LM377N | NS | ULN-2274B* | LM3075N | NS | ULN-2129A* |
| LM378N | NS | ULN-2278B-1* | LM3086N | NS | ULN-2086A |
| LM380N | NS | ULN-2280B | LM3089N | NS | ULN-2289A* |
| LM383AT | NS | ULN-3702Z | LM3611N | NS | UDN-3611M |
| LM383T | NS | ULN-37012 | LM3612N | NS | UDN-3612M |
| LM384N | NS | ULN-2281B* | LM3613N | NS | UDN-3613M |
| LM746N | NS | ULN-2228A* | LM3614N | NS | UDN-3614M |
| LM1304 | NS | ULN-2120A* | M54523 | MIT | ULN-2003A |
| LM1305 | NS | ULN-2122A* | M54524P | MIT | ULN-2001A |
| LM1307N | NS | ULN-2128A* | M54525P | MIT | ULN-2002A |
| LM1310N | NS | ULN-3810A-1 | M54526P | MIT | ULN-2004A |
| LM1391N | NS | ULN-2291M* | M54532P | MIT | ULN-2064B |
| LM1394N | NS | ULN-2294M* | M54562P | MIT | UDN-2982A |
| LM1800N | NS | ULX-3811A§ | M54563P | MIT | UDN-2981A |
| LM1820N | NS | ULN-2137A* | MC1304 | MOT | ULN-2120A* |
| LM1827N | NS | ULN-2224A | MC1305 | MOT | ULN-2122A* |
| LM1828N | NS | ULN-2228A* | MC1307P | MOT | ULN-2128A* |
| LM1829N | NS | ULX-2262A* | MC1309 | MOT | ULN-3809A |
| LM1841N | NS | ULN-2136A | MC1310P | MOT | ULN-3810A |
| LM1848N | NS | ULN-2229A* | MC1310EP | MOT | ULN-3810A |
| LM1877N | NS | ULN-2274B* | MC1311P | MOT | ULX-3811A§ |
| LM2002T | NS | ULN-37012 | MC1320P | MOT | ULN-2137A* |
| LM2002AT | NS | ULN-37022 | MC1324P | MOT | ULN-2224A |
| LM2111N | NS | ULN-2111A | MC1326P | MOT | ULN-2226A* |
| LM2113N | NS | ULN-2111A | MC1327P | MOT | ULN-2217A* |
| LM3045D | NS | ULS-2045H | MC1328P | MOT | ULN-2228A* |
| LM3046N | NS | ULN-2046A | MC1329P | MOT | ULN-2229A* |
| LM3053N | NS | ULN-2209M* | MC1339P | MOT | ULN-2126A* |
| LM3054N | NS | ULN-2054A | MC1344P | MOT | ULX-3811A§ |
| LM3064N | NS | ULN-2264A* | MC1356P | MOT | ULN-2136A |
| LM3065N | NS | ULN-2165A* | MC1357P | MOT | ULN-2111A |
| LM3066N | NS | ULN-2266A* | MC1358P | MOT | ULN-2165A* |
| LM3067N | NS | ULN-2267A* | MC1364P | MOT | ULN-2264A* |

[^2]| Competitive <br> Part Number | Mfr. | Suggested <br> Sprague <br> Replacement | Competitive <br> Part <br> Number | Mfr. | Suggested <br> Sprague <br> Replacement |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| MC1370P | MOT | ULN-2124A* | NE5501N | SIG | ULN-2021A |
| MC1371P | MOT | ULN-2127A* | NE5502N | SIG | ULN-2022A |
| MC1375P | MOT | ULN-2129A* | NE5503N | SIG | ULN-2023A |
| MC1389P | MOT | ULN-2289A* | NE5504N | SIG | ULN-2024A |
| MC1391P | MOT | ULN-2291M* | NE5560F | SIG | ULN-8160R |
| MC1394P | MOT | ULN-2294M* | NE5560N | SIG | ULN-8160A |
| MC1398P | MOT | ULN-2298A* | NE5561N | SIG | ULX-8161M |
| MC1411L | MOT | ULN-2001R§ | NE5601N | SIG | ULN-2001A |
| MC1411P | MOT | ULN-2001A | NE5602N | SIG | ULN-2002A |
| MC1412L | MOT | ULN-2002R§ | NE5603N | SIG | ULN-2003A |
| MC1412P | MOT | ULN-2002A | NE5604N | SIG | ULN-2004A |
| MC1413L | MOT | ULN-2003R§ | PA239 | GE | ULN-2126A* |
| MC1413P | MOT | ULN-2003A | PBD352301J | RFA | ULN-2001R§ |
| MC1413TP | MOT | ULQ-2003A§ | PBD352301N | RFA | ULN-2001A |
| MC1416L | MOT | ULN-2004R§ | PBD352302J | RFA | ULN-2004R§ |
| MC1416P | MOT | ULN-2004A | PBD352302N | RFA | ULN-2004A |
| MC1417P | MOT | UDN-2580A | PBD352303J | RFA | ULN-2003R§ |
| MC1471P1 | MOT | UDN-5711M | PBD352303N | RFA | ULN-2003A |
| MC1472P1 | MOT | UDN-5712M | PBD352304J | RFA | ULN-2002R§ |
| MC1473P1 | MOT | UDN-5713M | PBD352304N | RFA | ULN-2002A |
| MC1474P1 | MOT | UDN-5714M | PBD352311N | RFA | ULN-2021A |
| MC3346 | MOT | ULN-2046A | PBD352312N | RFA | ULN-2024A |
| MC3386P | MOT | ULN-2086A | PBD352313N | RFA | ULN-2023A |
| MFC4050 | MOT | ULN-2135E* | PBD352314N | RFA | ULN-2022A |
| ML3045 |  | ULS-2045H | PBD353801J | RFA | ULN-2801R§ |
| ML3046 |  | ULN-2046A | PBD353802J | RFA | ULN-2804R§ |
| ML3086 |  | ULN-2086A | PBD353803J | RFA | ULN-2803R§ |
| MSL912R | OKI | UDN-6118A-2 | PBD353804J | RFA | ULN-2802R§ |
| N2211A | SIG | ULN-2211B | SA594 |  | UDN-6118A |
| N2212A | SIG | ULN-2212B* | SE5560F | SIG | ULS-8160R |
| N5065A | SIG | ULN-2165A* | SFC2046E |  | ULN-2046A |
| N5070B | SIG | ULN-2124A* | SFC2054EC |  | ULN-2054A |
| N5071A | SIG | ULN-2127A* | SFC2086E |  | ULN-2086A |
| N5072A | SIG | ULN-2228A* | SG1526J | SG | ULS-8126R |
| N5111A | SIG | ULN-2111A | SG2001J | SG | ULQ-2001R |
| NA3086 |  | ULN-2086A | SG2001N | SG | ULN-2001A |

[^3]| Competitive Part Number | Mfr. | Suggested <br> Sprague <br> Replacement | Competitive <br> Part <br> Number | Mfr. | Suggested <br> Sprague <br> Replacement |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SG2002J | SG | ULQ-2002R | SL3183E | PLS | ULN-2083A-1 |
| SG2002N | SG | ULN-2002A | SN75064NE | TI | ULN-2064B |
| SG2003J | SG | ULQ-2003R | SN75065NE | TI | ULN-2065B |
| SG2003N | SG | ULN-2003A | SN75066NE | T | ULN-2066B |
| SG2004 | SG | ULQ-2004R | SN75067NE | T | ULN-2067B |
| SG2004N | SG | ULN-2004A | SN75068NE | TI | ULN-2068B |
| SG2526J | SG | ULQ-8126R | SN75069NE | II | ULN-2069B |
| SG2841N | SG | UDN-2841B | SN75074NE | TI | ULN-2074B |
| SG3045J | SG | ULS-2045H | SN75075NE | II | ULN-2075B |
| SG3081N | SG | ULN-2081A | SN75437ND | II | UDN-2541BS |
| SG3082N | SG | ULN-2082A | SN75466J | It | ULN-2021R§ |
| SG3086N | SG | ULN-2086A | SN75466N | It | ULN-2021A |
| SG3146N | SG | ULN-2046A-1 | SN75467J | II | ULN-2022R§ |
| SG3183N | SG | ULN-2083A-1 | SN75467N | II | ULN-2022A |
| SG3526J | SG | ULN-8126R | SN75468J | II | ULN-2023R§ |
| SG3821J | SG | ULS-2045H | SN75468N | TI | ULN-2023A |
| SG3821N | SG | ULN-2046A | SN75469J | TI | ULN-2024R§ |
| SG3822N | SG | ULN-2054A | SN75469N | TI | ULN-2024A |
| SG3851J | SG | ULQ-2011R | SN75471P | TI | UDN-3611M $\dagger$ |
| SG3851N | SG | ULN-2021A | SN75472P | TI | UDN-3612M $\dagger$ |
| SG3852 | SG | ULQ-2012R | SN75473P | $\pi$ | UDN-3613M $\dagger$ |
| SG3852N | SG | ULN-2022A | SN75474P | $\pi$ | UDN-3614M $\dagger$ |
| SG3853J | SG | ULQ-2013R | SN75476P | TI | UDN-5711M $\dagger$ |
| SG3853N | SG | ULN-2023A | SN75477P | II | UDN-5712M $\dagger$ |
| SG3854N | SG | ULN-2024A | SN75478P | II | UDN-5713M $\dagger$ |
| SG3886N | SG | ULN-2086A | SN75479P | II | UDN-5714M $\dagger$ |
| SG6118N | SG | UDN-6118A | SN76104N | $\pi$ | ULN-2120A* |
| SL3045C | PLS | ULS-2045H | SN76105N | T | ULN-2122A* |
| SL3046C | PLS | ULN-2046A | SN76110N | TI | ULN-2128A* |
| SL3054 | PLS | ULN-2054A | SN76111N | II | ULN-2121A* |
| SL3081C | PLS | ULN-2081A | SN76113N | It | ULN-2128A* |
| SL3082C | PLS | ULN-2082A | SN76115N | II | ULN-3810A |
| SL3083E | PLS | ULN-2083A | SN76116N | It | ULX-3811A§ |
| SL3086 | PLS | ULN-2086A | SN76130N | II | ULN-2126A* |
| SL3145E | PLS | ULS-2045H | SN76177ND | TI | ULN-2278B* |
| SL3146E | PLS | ULN-2046A-1 | SN76226N | TI | ULN-2216A* |

[^4]| Competitive |  | Suggested | Competitive |  | Suggested |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Part |  | Sprague | Part |  | Sprague |
| Number | Mfr． | Replacement | Number | Mfr． | Replacement |
| SN76227N | TI | ULN－2217A＊ | TD62074P | TOS | ULN－2074B |
| SN76228N | TI | ULN－2218A＊ | TD62101P | TOS | ULN－2001A |
| SN76242N | TI | ULN－2124A＊ | TD62103P | TOS | ULN－2003A |
| SN76243AN | TI | ULN－2127A＊ | TD62104P | TOS | ULN－2004A |
| SN76246N | TI | ULN－2228A＊ | TD62705P | TOS | UHP－491 |
| SN76266N | TI | ULN－2266A＊ | TDA1060 | PE $\ddagger$ | ULN－8160A |
| SN76267N | TI | ULN－2267A＊ | TDA1083 | PE $\ddagger$ | ULN－2204A |
| SN76298N | TI | ULN－2298A＊ | TDA1090 | PE $\ddagger$ | ULN－2242A |
| SN76564N | TI | ULN－2264A＊ | TDA1170 | PE $\ddagger$ | ULN－22700 |
| SN76565N | TI | ULN－2264A＊ | TDA1190 | PEも | ULX－3908Q＊ |
| SN76591P | TI | ULN－2291M＊ | TDA1190P | PEも | ULN－2290B |
| SN76594P | TI | ULN－2294M＊ | TDA11902 | PE $\ddagger$ | ULN－22900 |
| SN76635N | It | ULN－2137A＊ | TDA1200 | PE $\ddagger$ | ULN－2289A＊ |
| SN76642N | T | ULN－2111A | TDA1230 | PEも | ULX－3801Q＊ |
| SN76643N | TI | ULN－2111A | TDA1327 | PE\＃ | ULN－2217A＊ |
| SN76665N | II | ULN－2165A＊ | TDA2002 | PE $\ddagger$ | ULN－37012 |
| SN76669N | TI | ULN－2136A | TDA2002A | PE $\ddagger$ | ULN－37022 |
| SN76675N | TI | ULN－2129A＊ | TDA2002H | PE才 | ULN－37012H |
| SN76678P | TI | ULN－2209M＊ | tdA2002V | PE才 | ULN－37012V |
| SN76688ND | It | ULN－2211B | TDA2003H | PE $\ddagger$ | ULN－3703Z |
| SN76689N | II | ULN－2289A＊ | TDA2003V | PE\＃ | ULN－3703ZV |
| SN76883N | Ti | ULX－2230A＊ | TDA3189 | PE才 | ULN－3889A |
| TA7070P | TOS | ULN－2264A＊ | TDA3190 | PEま | ULN－2290B |
| TA7103P | TOS | ULN－2224A | TDA3190P | PEま | ULN－2290B |
| TA7141AP | TOS | ULN－2217A＊ | TDA3950A | PEま | ULN－2220A＊ |
| TA7157P | TOS | ULN－3810A | TVCM－1 | SPC | ULN－2114W＊ |
| TA7613P | TOS | ULN－2204A | TVCM－2 | SPC | ULN－2114A＊ |
| TAA930 |  | ULN－2111A | TVCM－3 | SPC | ULN－2114K＊ |
| TBA395 |  | ULN－2218A＊ | TVCM－4 | SPC | ULN－2111A |
| TBA396 |  | ULN－2219A＊ | TVCM－5 | SPC | ULN－2111A |
| TCA3089 | PE $\ddagger$ | ULN－2289A＊ | TVCM－6 | SPC | ULN－2120A＊ |
| TCA3189 | PE $\ddagger$ | ULN－3889A | TVCM－7 | SPC | ULN－2122A＊ |
| TD62001P | TOS | ULN－2001A | TVCM－8 | SPC | ULN－2124A＊ |
| TD62002P | TOS | ULN－2002A | TVCM－9 | SPC | ULN－2127A＊ |
| TD62003P | TOS | ULN－2003A | TVCM－10 | SPC | ULN－2128A＊ |
| TD62004P | TOS | ULN－2004A | TVCM－11 | SPC | ULN－2165A＊ |
| TD62064P | TOS | ULN－2064B | TVCM－12 | SPC | ULN－2121A＊ |

[^5]| Competitive <br> Part <br> Number | Mfr. | Suggested <br> Sprague <br> Replacement | Competitive <br> Part <br> Number | Mfr. | Suggested <br> Sprague <br> Replacement |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TVCM-13 | SPC | ULN-2126A* | UA746PC | FSC | ULN-2228A* |
| TVCM-14 | SPC | ULN-2131M* | UA753TC | FSC | ULN-2209M* |
| TVCM-15 | SPC | ULN-2125A* | UA758PC | FSC | ULX-3811A§ |
| TVCM-16 | SPC | ULN-2129A* | UA767PC | FSC | ULN-2128A* |
| TVCM-17 | SPC | ULN-2135E* | UA780PC | FSC | ULN-2124A* |
| TVCM-18 | SPC | ULN-2136A | UA781PC | FSC | ULN-2127A* |
| TVCM-19 | SPC | ULN-2137A* | UA787PC | FSC | ULN-2262A* |
| TVCM-20 | SPC | ULN-2209M* | UA1391TC | FSC | ULN-2291M* |
| TVCM-21 | SPC | ULN-2224A | UA1394TC | FSC | ULN-2294M* |
| TVCM-22 | SPC | ULN-2228A* | UA2136PC | FSC | ULN-2136A |
| TVCM-23 | SPC | ULN-2274B** | UA3045DM | FSC | ULS-2045H |
| TVCM-24 | SPC | ULN-2276P* | UA3046PC | FSC | ULN-2046A |
| TVCM-25 | SPC | ULN-2278B* | UA3054PC | FSC | ULN-2054A |
| TVCM-26 | SPC | ULN-2278B* | UA3064PC | FSC | ULN-2264A* |
| TVCM-27 | SPC | ULN-2298A* | UA3065PC | FSC | ULN-2165A* |
| TVCM-28 | SPC | ULN-2211B | UA3075PC | FSC | ULN-2129A* |
| TVCM-29 | SPC | ULX-3811A§ | UA3066PC | FSC | ULN-2266A* |
| TVCM-30 | SPC | ULN-2264A* | UA3067PC | FSC | ULN-2267A* |
| TVCM-33 | SPC | ULN-2267A* | UA3086PC | FSC | ULN-2086A |
| TVCM-34 | SPC | ULN-2269A* | UA3089PC | FSC | ULN-2289A* |
| TVCM-35 | SPC | ULN-2280B | UA7327 | FSC | ULN-2270B |
| TVCM-36 | SPC | ULN-2281B* | UCN4810N | TI | UCN-4810A |
| TVCM-37 | SPC | ULN-2285A* | UDN2841NE | TI | UDN-2841B |
| TVCM-38 | SPC | ULN-2285P* | UDN2845NE | TI | UDN-2845B |
| TVCM-39 | SPC | ULN-2289A* | UDN5711N | TI | UDN-5711M |
| TVCM-40 | SPC | ULN-2298A* | UDN5712N | TI | UDN-5712M |
| TVCM-62 | SPC | ULX-3811A§ | UDN5713N | TI | UDN-5713M |
| TVCM-65 | SPC | ULN-2278B* | UDN5714N | TI | UDN-5714M |
| TVCM-66 | SPC | ULN-2046A | UDN-6164A | SPR | UDN-6116A-1 |
| TVCM-67 | SPC | ULN-2054A | UDN-6184A | SPR | UDN-6118A-1 |
| TVCM-68 | SPC | ULN-2208M* | UGN-3600M | SPR | UGN-3604M |
| TVCM-73 | SPC | ULN-3810A | UGN-3601M | SPR | UGN-3605M |
| U417B | TLF | ULN-2289A* | ULN2001AJ | TI | ULN-2001R§ |
| UA704PC | FSC | ULN-2211B | ULN2001AN | TI | ULN-2001A |
| UA705PC | FSC | ULX-3811A§ | ULN2002AJ | TI | ULN-2002R§ |
| UA720PC | FSC | ULN-2137A* | ULN2002AN | TI | ULN-2002A |
| UA729PC | FSC | ULN-2122A* | ULN2003AJ | TI | ULN-2003R§ |
| UA732PC | FSC | ULN-2120A* | ULN2003AN | Tl | ULN-2003A |
| UA737EC | FSC | ULN-2114K* | ULN2004AJ | Tl | ULN-2004R§ |
| UA739PC | FSC | ULN-2126A* | ULN2004AN | Tl | ULN-2004A |

[^6]| Competitive Part |  | Suggested <br> Sprague | Competitive Part |  | Suggested Sprague |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Number | Mfr. | Replacement | Number | Mfr. | Replacement |
| ULN2005AJ | TI | ULN-2005R§ | XR2001CN | EXR | ULN-2001R§ |
| ULN2005AN | Tl | ULN-2005A | XR2001P | EXR | ULQ-2001A§ |
| ULN2064NE | TI | ULN-2064B | XR2002CN | EXR | ULN-2002R§ |
| ULN2065NE | T | ULN-2065B | XR2002P | EXR | ULQ-2002A§ |
| ULN2066NE | $\pi$ | ULN-2066B | XR2003CN | EXR | ULN-2003R§ |
| ULN2067NE | $\pi$ | ULN-2067B | XR2003P | EXR | ULQ-2003A§ |
| ULN2068 | MOT | ULN-2068B | XR2004CN | EXR | ULN-2004R§ |
| ULN2068NE | II | ULN-2068B | XR2004P | EXR | ULQ-2004A§ |
| ULN2069NE | T | ULN-2069B | XR2011CN | EXR | ULN-2011R§ |
| ULIN2074NE | $\pi$ | ULN-2074B | XR2011CP | EXR | ULN-2011A |
| ULN2075NE | TI | ULN-2075B | XR2012CN | EXR | ULN-2012R§ |
| ULN-2110A | SPR | ULN-3810A | XR2012CP | EXT | ULN-2012A |
| ULN-2113A | SPR | ULN-2111A | XR2013CN | EXR | ULN-2013R§ |
| ULN-2114A | SPR | ULN-2228A* | XR2013CP | EXR | ULN-2013A |
| ULN-2209V |  | ULN-2209M* | XR2014CN | EXR | ULN-2014R§ |
| ULN-2210A | SPR | ULN-3810A | XR2014CP | EXR | ULN-2014A |
| ULN-2225P | SPR | ULN-2211B | XR2201CP | EXR | ULN-2001A |
| ULN-2226A | SPR | ULN-2224A | XR2202CP | EXR | ULN-2002A |
| ULN-2244A | SPR | ULX-3811A§ | XR2203CP | EXR | ULN-2003A |
| ULN-2275P | SPR | ULN-2274B* | XR2204CP | EXR | ULN-2004A |
| ULN-2277P | SPR | ULN-2278B* | XR2205CP | EXR | ULN-2005A |
| ULN-2287A | SPR | ULN-2289A* | XR6118P | EXR | UDN-6118A |
| ULN-2301M | SPR | ULN-2300M* | XR6128P | EXR | UDN-6128A |
| ULN-3006M | SPR | UGN-3201M | 2N1060 | FER | ULN-8160A |
| ULN-3006T | SPR | UGN-3019T | 512 | $1 T$ | UHP-491 |
| ULN-3007M | SPR | UGN-3203M | 552 | $1 \pi$ | ULN-2001A |
| ULN-3008M | SPR | UGN-3501M | 554 | $1 \pi$ | ULN-2002A |
| ULN-3008T | SPR | UGN-3501T | 556 | 17 | ULN-2003A |
| ULN-3100M | SPR | UGN-3604M | 652 | 17 | ULN-2001A |
| ULN-3101M | SPR | UGN-3605M | 654 | 17 | ULN-2002A |
| ULN-3330Y-2 | SPR | ULN-3330Y | 656 | $1 T$ | ULN-2003A |
| ULN-3905A | SPR | ULN-3914A | 96650 C | FSC | ULN-2001R§ |
| ULS-3006T | SPR | UGS-3019T | 9665PC | FSC | ULN-2001A |
| UPA2001C | NEC | ULN-2001A | 96660C | FSC | ULN-2002R§ |
| UPA2002C | NEC | ULN-2002A | 9666PC | FSC | ULN-2002A |
| UPA2003C | NEC | ULN-2003A | 9667DC | FSC | ULN-2003R§ |
| UPA2004C | NEC | ULN-2004A | 9667PC | FSC | ULN-2003A |
| XR1310CP | EXR | ULN-3810A | 9668DC | FSC | ULN-2004R§ |
| XR1800P | EXR | ULX-3811A§ | 9668PC | FSC | ULN-2004A |

[^7]
## HOW TO ORDER

TO PLACE AN ORDER, obtain price and delivery, or request additional technical literature, call or write your local sales office (see inside back cover) or:

From U.S.A. Sprague Electric Co.
Marshall Street
North Adams, MA 01247
413-664-4411
From Asia Sprague World Trade Corp.
G.P.O. Box 4289

Eastern Branch, Hong Kong 5-626231-4
From Europe Sprague World Trade Corp.
Case Postale 436
1215 Geneva Airport 15
Geneva, Switzerland 022-98-4021
$\mathbf{R}^{\text {EQUESTS FOR additional technical information }}$ on standard or custom devices (also see Section 6) may be sent to the appropriate manufacturing facility:

For all monolithic integrated circuits except Hall effect devices,

Sprague Electric Co.
115 Northeast Cutoff
Worcester, MA 01606
617-853-5000
For discrete semiconductors and Hall effect devices,

Sprague Electric Co.
70 Pembroke Road
Concord, NH 03301
603-224-1961

## SPRAGUE FACILITIES

Sprague Electric Company manufactures active and passive components in 17 locations in the United States and in five countries in Europe and the Far East. Headquarters of the Semiconductor Division is located in Worcester, Mass. All semiconductor wafer fabrication is done in the Worcester plant, as
are all services integral to its support. Volume assembly operations are located both in Worcester and in Manila, Philippines. Marketing and sales offices and sales representatives are located throughout the United States and Canada, Latin America, Europe, Japan, Africa, and the Far East.


INTEGRATED CIRCUIT OPERATIONS, Worcester, Massachusetts

## Semiconductor Operations

The integrated circuits operation of the Sprague Electric Semiconductor Division is located in a modern 115,000-square-foot plant in Worcester, Mass. Discrete components, such as transistors and diodes, and Hall effect integrated circuits are manufactured at the division's Concord, N.H., plant, which occupies some 30,000 square feet of floor space.

Sprague Electric is a leading manufacturer of volume integrated circuits serving the consumer, industrial controls, and peripherals markets. Production process technologies include complementary metal-gate MOS, high-voltage and high-current bipolar, and high-performance bipolar linear. This breadth of process technology makes it possible for Sprague Electric to manufacture optimal costperformance integrated circuits.


TRANSISTOR OPERATIONS, Concord, New Hampshire

## How Integrated Circuits are Shipped

Integrated circuits are shipped in one of these carriers:

## A-Channel Anti-Static Plastic Tubing

 TO-220 Plastic MagazineIndividual Plastic Box

Integrated circuit chips are shipped in either unscribed wafer form or individually partitioned in a plastic box.

## Quality Control and Reliability

All critical points in the manufacturing processes of Sprague Electric integrated circuits are carefully
monitored for compliance to engineering specifications. Electrical tests are made on $100 \%$ of the parts by automatic test systems. Lot sampling assures meeting customer A.Q.L. requirements. Calibration of test standards and equipment is performed at periodic intervals in order to maintain test accuracy.

Sprague Electric Company conducts a continuing reliability assurance program to detect deviations in device characteristics. Test samples are taken at random from each lot and are subjected to testing for performance evaluation and specification compliance. Routinely, finished samples are subjected to all electrical performance tests. A copy of the quality control inspection plan used for specific integrated circuits is available on request.

## GENERAL INFORMATION (Continued)

## ENGINEERING BULLETINS

The information in this data book is equivalent to the Sprague Engineering Bulletins listed below. If an individual bulletin and this data book are compared, the latest revision takes precedence. For example, the ULQ2801R, described on page 5-26 (Bulletin 29304.4A), supersedes Bulletin 29304.4, which is presently in print. If that bulletin is revised identical to this data book, it will receive the ' $A$ ' revision letter. If additional revisions beyond what appear here are incorporated, the bulletin would then receive a ' $B$ ' revision letter.

| Part Number | Bulletin Number |  | Part Number | Bulletin Number |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| UHC/UHD-400 through 433-1 | 29300.1 | 3 P | ULN-2224A | 27103.12B |  |
| UHP-400 through 433-1 | 29300 B | 2 P | ULN-2231A | 27115.20 |  |
| UHP-480 through 482 | 29301 C | 2 P | ULN-2240A | 27121.62 |  |
| UHD/UHP-490 and 491 | 29302 | 2 P | ULN-2241A | 27121.61 |  |
| UHP-495 | 29303A |  | ULN-2242A | 27121.60A |  |
| UHC/UHD-500 through 533 | 29300.1 | 3 P | ULN-2243A | 27105.1 |  |
| UHP-500 through 533 | 29300B | 2 P | ULN-2245A | 27109.101 |  |
| TPP-1000 and 2000 | 29714 |  | ULN-2249A | 27121.10 |  |
| ULN-2001A through 2015A | 29304B | 2 P | ULN-2260A | 27119.2 |  |
| ULS-2001H through 2015 | 29304.1B |  | ULN-2261A | 27104.10 |  |
| ULQ-2001R through 2015R | 29304.1 B |  | ULN-2270B and 22700 | 27124.10 |  |
| ULN-2021A through 2025A | 29304B | 2P | ULN-2280B | 27117.11A |  |
| ULS-2021H through 2025 | 29304.1B |  | ULN-2283B and 2283B-1 | 27117.21 | 2P |
| ULN-2031A through 2033A | 29710A | 2P | ULN-2290B and 22900 | 27110.32 | 2 P |
| ULS-2045H | 29707 | 2 P | ULN-2350C and 2351C | 27405 |  |
| ULN-2046A | 29707 | 2 P | ULN-2401A | 27460 |  |
| ULN-2046A-1 | - |  | ULN-2429A | 27461 |  |
| ULN-2047A | 29712 | 2P | ULN-2430M | 27462 |  |
| ULN-2054A | 29708A | 2P | TPQ-2483 and 2484 | 29711 |  |
| ULN-2061M and 2062M | 29305B | 2 P | UDN-2540B | - |  |
| ULN-2064B through 2077B | 29305B | 2P | UDN-2580A through 2588A | 29316 |  |
| ULS-2064H through 2077 | 29305.1 |  | UDN-2595A | 29320 |  |
| ULN-2081A and 2082A | 29709 |  | ULN-2801A through 2815A | 29304.3A | 2P |
| ULN-2083A | 29713 | 2P | ULS-2801H through 2815H | 29304.4A |  |
| ULN-2083A-1 | - |  | ULQ-2801R through 2815R | 29304.4A |  |
| ULS-2083H | 29713 | 2P | ULN-2821A through 2825A | 29304.3A | 2P |
| ULN-2086A | - |  | ULS-2821H through 2825H | 29304.4A |  |
| ULN-2111A | 27102 E | 2 P | UDN-2841B through 2846B | 29314 | 2P |
| ULN-2136A | 27102.40B | 2P | UTN-2886B and 2888A | 29401 | 2P |
| ULN-2140A | 29015.210A | 2P | TPQ-2906 and 2907 | 29711 |  |
| ULS-2140H | 29015.210 A | 2 P | UDN-2949Z | 29318 | 2P |
| ULN-2204A | 27121.50A |  | UDN-2952B and 2952W | 29319 |  |
| ULN-2211B | 27110.30B |  | UDN-2956A and 2957A | 29309A | 2P |
| TPQ-2221 and 2222 | 29711 |  | UDQ-2956R and 2957R | 29309.1A |  |

NOTE: 2P (2nd printing) indicates minor changes and/or corrections not normally affecting device performance.

## ENGINEERING BULLETINS <br> (Continued)

| Part Number | Bulletin Number |  |
| :--- | :--- | :--- |
| UDN-2981A through 2984A | 29310 A |  |
| UDS-2981H through 2984H | 29310.1 | 2P |
| TPP-3000 | 29714 |  |
| UGH-3013T | $27603 A$ |  |
| UGN/UGS-3019T | $27601 A$ |  |
| UGN/UGS-3020T | $27602 A$ |  |
| UGN/UGS-3030T | 27606 |  |
|  |  |  |
| UGN-3201M and 3203M | 27604 |  |
| UGN-3220S | 27605 |  |
| ULN-3304M | 27450.01 | 2P |
| ULN-3305M | 27450.10 | $2 P$ |
| ULN-3306M | 27450.12 | $2 P$ |
| ULN-3330Y | $27480 A$ |  |
| UGN-3501M | 27500.1 |  |
| UGN-3501T | 27500 |  |
| UGN-3604M and 3605M | $27120 C$ |  |
| UDN-3611M through 3614M | 29308 | $2 P$ |
| UDS-3611H through 3614H | 29308.1 |  |
| ULN-3701Z | 27117.31 |  |
| ULN-3702Z | 27117.33 |  |
| ULN-3703Z | 27117.34 |  |
| TPQ-3724 through 3725A | 29711 |  |
| ULX-3777W | 27117.60 |  |
| ULX-3788W | 27117.61 |  |
| TPQ-3798 and 3799 | 29711 |  |
| ULX-3804A | 27121.52 |  |
| ULN-3809A | 27109.112 |  |
| ULN-3810A | 27109.113 |  |
| ULX-3840A | 27121.64 |  |
| ULN-3859A | 27105.10 |  |
| ULN-3889A | 27102.62 |  |
| TPQ-3904 | 29711 |  |
|  |  |  |
|  |  |  |


| Part Number | Bulletin |  |
| :--- | :--- | :--- |
| TPQ-3906 | 29711 |  |
| ULN-3914A | 27125 |  |
| TPP-4000 | 29714 |  |
| UCN-4202A | 26184 | $2 P$ |
| UCN-4401A | $26180 A$ |  |
| UCS-4401H | 26180.1 |  |
| UCN-4801A | $26180 A$ |  |
| UCS-4801H | 26180.1 |  |
| UCN-4805A and 4806A | 26181 | $2 P$ |
| UCN-4810A | 26182 | $2 P$ |
| UCN-4815A | 26183 | $2 P$ |
| UCN-4821A through 4823A | 26185 |  |
| UDN-5703A through 5707A | 29306 | $2 P$ |
| UDS-5703H through 5707H | 29306.1 | $2 P$ |
| UDN-5711M through 5714M | $29307 A$ | $2 P$ |
| UDS-5711H through 5714H | 29307.1 |  |
| UDN-5733M | 29306 | $2 P$ |
| UDS-5733H | 29306.1 | $2 P$ |
| UDS-5790H and 5791H | 29315.1 | $2 P$ |
| TPQ-6001 through 6100A | 29711 |  |
| UDN-6116A through 6128A-2 |  |  |
| UDN-6116A through 6128R-2 | $29313 B$ | $2 P$ |
| UDN-6138A through 6148A-2 | $29313 B$ | $2 P$ |
| UDN-6164A and 6184A | $29313 B$ | $2 P$ |
| TPQ-6501 through 6700 | $29312 B$ |  |
| UDN-7180A through 7186A | 29711 |  |
| ULN-8126A and 8126R | $29311 A$ | $2 P$ |
| ULQ-8126A and 8126R | 27466.10 |  |
| ULS-8126R | 27466.10 |  |
| ULN-8160A and 8160R | 27466.10 |  |
| ULS-8160R | 27466 |  |
| ULX-8161M | 27466 |  |
|  | 27466.1 |  |
|  |  |  |

[^8]

GENERAL INFORMATION

HIGH-VOLTAGE INTERFACE DRIVERS

HIGH-CURRENT INTERFACE DRIVERS

BiMOS AND COMPLEX ARRAY INTERFACE DRIVERS

INDUSTRIAL, MILITARY, AND AEROSPACE DEVICES

## RADIO INTEGRATED CIRCUITS

TELEVISION INTEGRATED CIRCUITS

## AUDIO INTEGRATED CIRCUITS

HALL EFFECT DEVICES

TRANSISTOR ARRAYS AND MISCELLANEOUS DEVICES

CUSTOM DEVICES

PACKAGE INFORMATION
$\qquad$

## SECTION 2 - HIGH-VOLTAGE INTERFACE DRIVERS

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UHD/UHP-490 and -491 Gas-Discharge Display Digit Drivers ..... 2-5
UHP-495 Gas-Discharge Display Digit Driver ..... 2-8
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UDN-6116R through 6128R-2 Hermetic Fluorescent Display Drivers ..... 2-10
UDN-6138A through 6148A-2 Fluorescent Display Drivers ..... 2-10
UDN-6164A and 6184A Gas-Discharge Display Digit Drivers ..... 2-14
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Trends in IC Interface for Electronic Displays ..... 2-28

SELECTION GUIDE TO HIGH-VOLTAGE INTERFACE DRIVERS

| Device Type | Absolute Maximum Ratings |  |  |
| :---: | :---: | :---: | :---: |
|  | $\mathrm{I}_{\text {Out }}$ | $\mathrm{V}_{\text {Out }}$ | Outputs |
| UHP-480 | 15 mA | 130 V | Sink 5 |
| UHP-481 | 15 mA | 130 V | Sink 7 |
| UHP-482 | 15 mA | 130 V | Sink 8 |
| UHD/UHP-490 | $-30 \mathrm{~mA}$ | -80 V | Source 5 |
| UHD/UHP-491 | $-30 \mathrm{~mA}$ | $-80 \mathrm{~V}$ | Source 6 |
| UHP-495 | - 30 mA | -80 V | Source 6 |
| UDN-6116A/R | -40 mA | 85 V | Source 6 |
| UDN-6116A-1 | -40 mA | 115 V | Source 6 |
| UDN-6116A/R-2 | -40 mA | 65 V | Source 6 |
| UDN-6118A/R | -40 mA | 85 V | Source 8 |
| UDN-6118A-1 | -40 mA | 115 V | Source 8 |
| UDN-6118A/R-2 | -40 mA | 65 V | Source 8 |
| UDN-6126A/R | -40 mA | 85 V | Source 6 |
| UDN-6126A-1 | -40 mA | 115 V | Source 6 |
| UDN-6126A/R-2 | -40 mA | 65 V | Source 6 |
| UDN-6128A/R | -40 mA | 85 V | Source 8 |
| UDN-6128A-1 | -40 mA | 115 V | Source 8 |
| UDN-6128A/R-2 | -40 mA | 65 V | Source 8 |
| UDN-6138A | -40 mA | $\pm 40 \mathrm{~V}$ | Source 8 |
| UDN-6138A-2 | -40 mA | $\pm 30 \mathrm{~V}$ | Source 8 |
| UDN-6148A | -40 mA | $\pm 40 \mathrm{~V}$ | Source 8 |
| UDN-6148A-2 | -40 mA | $\pm 30 \mathrm{~V}$ | Source 8 |
| UDN-6164A | -40 mA | 115 V | Source 6 |
| UDN-6184A | -40 mA | 115 V | Source 8 |
| UDN-7180A | 20 mA | $-115 \mathrm{~V}$ | Sink 8 |
| UDN-7183A | 3.25 mA | $-115 \mathrm{~V}$ | Sink 8 |
| UDN-7184A | 2.0 mA | -115V | Sink 8 |
| UDN-7186A | 1.0 mA | -115V | Sink 8 |

## SERIES UHP-480 HIGH-VOLTAGE DISPLAY DRIVERS

## Features:

- Reliable Monolithic Integrated Construction
- Low-Output Leakage Current
- High-Voltage Output Capability
- Small Size
- 130 Volt Breakdown


## Description

SERIES UHP-480 display drivers are bipolar monolithic integrated circuits - high-voltage switches designed for interface applications between MOS or open-collector TTL logic and gas discharge displays. They are packaged in industry standard dual-in-line plastic packages and are available with 5 (UHP-480), 7 (UHP-481), or 8 (UHP-482) switches per package.

## Applications

Sprague Series UHP-480 drivers may be used with gas discharge displays, such as Burroughs Panaplex ${ }^{\circ}$, Cherry Plasma-Lux ${ }^{\oplus}$ and Beckman SP Series devices, intended for use in the cathode portion of the displays. Applications include calculators, DVM's, DMM's, DPM's, mini-computers, clocks, etc. These drivers replace the major portion of discrete components typically required to interface between a MOS calculator or counter/decoder circuit and a gas discharge display. Their high reliability and small size make them an excellent choice for applications where space is at a premium.

[^9]

UHP-480
14-Lead Dual In-Line


UHP-481
16-Lead Dual In-Line


UHP-482
18-Lead Dual In-Line


UHP-480, 481 and 482 (1 Driver)

## ELECTRICAL CHARACTERISTICS @ $\mathbf{T}_{\mathrm{A}}=\mathbf{2 5}{ }^{\circ} \mathrm{C}$ unless otherwise specified

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Output Sink Current | Iout | $V_{\text {IV }}=4 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=5 \mathrm{~V}$ | 2.0 | 5.5 | - | mA |
|  |  | $\mathrm{V}_{\text {II }}=5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=5 \mathrm{~V}$ | 3.0 | 7.0 | - | mA |
|  |  | $V_{\text {II }}=6 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=5 \mathrm{~V}$ | 4.0 | 8.0 | - | mA |
|  |  | $V_{\text {II }}=7 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=5 \mathrm{~V}$ | 5.0 | 9.0 | - | mA |
| Output Leakage Current | ICEX | $\mathrm{V}_{\text {IN }}=0 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=130 \mathrm{~V}$ | - | 0.2 | 1.5 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {IN }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CE}}=130 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 1.5 | 15 | $\mu \mathrm{A}$ |
| Tnput Current | IN | $V_{\text {IN }}=7 \mathrm{~V}$ | - | 200 | 350 | $\mu \mathrm{A}$ |
|  |  | $V_{\text {IN }}=15 \mathrm{~V}$ | - | 490 | 700 | $\mu \mathrm{A}$ |
| Output Saturation Voltage | $V_{\text {CESSAD }}$ | $\mathrm{I}_{\text {OUT }}=5.5 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=9 \mathrm{~V}$ | - | 1.3 | 2.5 | V |
| Turn-on Delay Time | $\mathrm{t}_{\mathrm{ON}}$ | $\mathrm{R}_{\mathrm{L}}=56 \mathrm{k} \Omega, \mathrm{V}_{\text {CC }}=130 \mathrm{~V}$ | - | 2 | 5 | $\mu \mathrm{s}$ |
| Turn-off Delay Time | $\mathrm{t}_{\text {OFF }}$ | $\mathrm{R}_{\mathrm{L}}=56 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{CC}}=130 \mathrm{~V}$ | - | 2 | 5 | $\mu \mathrm{s}$ |

## TYPICAL CLOCK APPLICATION



Type 206C and 216C are single in-line networks

Because of the high input impedance of these devices, they are susceptable to static discharge damage sometimes associated with handling and testing. Therefore, techniques similar to those used for handling MOS devices should be employed.

## SERIES 490 and 491 <br> HIGH-VOLTAGE DISPLAY DRIVERS

## FEATURES

- Reliable Monolithic Integrated Construction
- Low Output Leakage Currents
- High Output Breakdown Voltages
- Small Size


## Description

The Series 490 and 491 high-voltage display drivers are bipolar monolithic integrated circuits designed for interfacing MOS or other low-voltage circuitry with high-voltage gas discharge displays or loads. These drivers replace most of the discrete components normally required to drive multiplexed gas discharge displays from MOS calculator or clock circuits. The Series 490 and 491 high-voltage display drivers are intended for use in the anode portion of the display and are available with either 5 (Series 490) or 6 (Series 491) drivers per dual in-line package.

## Applications

The Series 490 and 491 may be used in a variety of low-voltage to highvoltage interfacing applications such as are found in MOS calculators, digital clocks, etc. Their high reliability and small size make them an excellent choice for those applications where space is at a premium.

## Packages

| Package | Part <br> Number | Drivers/ <br> Package |
| :--- | :---: | :---: |
| 14-Lead Hermetic <br> Dual In-line | UHD-490 | 5 |
| 14-Lead Plastic <br> Dual In-line | UHP-490 | 5 |
| 16-Lead Hermetic <br> Dual In-line | UHD-491 | 6 |
| 16-Lead Plastic <br> Dual In-line | UHP-491 | 6 |

## ABSOLUTE MAXIMUM RATINGS

 (referenced to $\mathrm{V}_{\mathrm{ss}}$ )Output Voltage. ..... $-80 \mathrm{~V}$
Output Source Current. ..... 30 mA
$V_{D D}$ Supply Voltage ..... $-30 \mathrm{~V}$
Input Voltage ..... $-30 \mathrm{~V}$
Input Diode Forward Current. ..... 20 mA
Operating Temperature Range:
UHP-490, UHP-491

$$
-20^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C}
$$

UHD-490, UHD-491 ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Storage Temperature Range. $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS @ $T_{A}=25^{\circ} \mathrm{C} \mathrm{V}_{S S}=O V$ (unless otherwise specified)

| Characteristic | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Max. | Units |
| "1" Input Voltage | \% | - | $V_{\text {DD }}+2.5$ | V |
| "0" Input Voltage |  | $V_{D D}+6$ | - | $V$ |
| Output Leakage Current | $\mathrm{V}_{\mathbb{W}}=\mathrm{V}_{\text {DD }}+2.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}$ | - | 1.5 | $\mu \mathrm{A}$ |
|  | $\mathrm{V}_{\mathbb{N}}=\mathrm{V}_{\text {DD }}+2.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 15 | $\mu \mathrm{A}$ |
| Output Saturation Voltage | $\mathrm{V}_{\mathbb{W}}=\mathrm{V}_{\text {DD }}+6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=5 \mathrm{~mA}$ | - | 2 | V |
|  | $V_{\mathbb{N}}=V_{\text {DD }}+6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=15 \mathrm{~mA}$ | - | 5 | V |
| Input Current | $\mathrm{V}_{\mathbb{N}}=\mathrm{V}_{\text {SS }}, \mathrm{I}_{\text {OUT }}=15 \mathrm{~mA}, \mathrm{~V}_{\text {DO }}=-15 \mathrm{~V}$ | - | 400 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {DD }}$ Supply Current | $\mathrm{V}_{\mathbb{N}}=\mathrm{V}_{\text {SS }}, \mathrm{I}_{\text {OUT }}=15 \mathrm{~mA}, \mathrm{~V}_{\text {DO }}=-15 \mathrm{~V}$ | - | 2 | mA |
| Input Diode Forward Voltage | $\mathrm{I}_{\mathrm{D}}=20 \mathrm{~mA}$ | - | 2 | V |
| Turn-on Delay Time | $\mathrm{R}_{\mathrm{L}}=4 \mathrm{k} \Omega$ | - | 3 | $\mu \mathrm{s}$ |
| Turn-off Delay Time | $\mathrm{R}_{\mathrm{L}}=4 \mathrm{k} \Omega$ | - | 5 | $\mu \mathrm{s}$ |



UHD-491
UHP-491


UHD-490
UHP-490


Series 490 and 491 (1 Driver)

TYPICAL SMALL CALCULATOR APPLICATION


## UHP-495 <br> HIGH-VOLTAGE DISPLAY DRIVER

## FEATURES

- Reliable Monolithic Integrated Construction
- Low Output-Leakage Currents
- High Output-Breakdown Voltages
- 14-Pin Dual In-Line Plastic Package

THIS MONOLITHIC integrated circuit is designed for use as an interface between MOS or other low-voltage circuitry and high-voltage gas-discharge displays or similar loads.

Type UHP-495 replaces most of the discrete components normally required to drive multiplexed gas-discharge displays with MOS calculator or clock circuits. The high-voltage bipolar interface is designed for use in the anode portion of a display. It has six drivers per package.


## ABSOLUTE MAXIMUM RATINGS (Referenced to $\mathbf{V}_{5 s}$ )

Output Voltage ..... $-80 \mathrm{~V}$
Output Source Current ..... - 30 mA
Input Voltage ..... $-30 \mathrm{~V}$
input Diode Forward Current ..... 20 mA
Operating Temperature Range ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range ..... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
NOTE: Positive (negative) current is defined as current going into (coming out of) the specified device pin.


ELECTRICAL CHARACTERISTICS of $T_{A}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\text {SS }}=0 \mathrm{~V}, \mathrm{~V}_{\text {SUB }}=-80 \mathrm{~V}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Input Voltage | $V_{\text {IN }}$ | $\mathrm{I}_{\text {OUT }}=-15 \mathrm{~mA}, \mathrm{~V}_{\text {OUT }} \leq-5 \mathrm{~V}$ | - | -3.5 | -6.0 | $V$ |
| Input Current | $1{ }_{\text {IN }}$ | $V_{\text {IN }}=-12 \mathrm{~V}$ | 400 | 600 | 850 | $\mu \mathrm{A}$ |
| Output Saturation Voltage | $\mathrm{V}_{\text {CESAD }}$ | $V_{\text {IN }}=-6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-15 \mathrm{~mA}$ | - | 2.0 | 5.0 | V |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | $\mathrm{V}_{\text {OUI }}=-80 \mathrm{~V}$ | - | - | -1.5 | $\mu \mathrm{A}$ |
| Substrate Current | $\mathrm{I}_{\text {SUB }}$ | $\mathrm{V}_{\text {IN }}=-6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-1 \mathrm{~mA}$ | - | - | -1.5 | mA |
| Substrate Leakage Current |  | $\mathrm{V}_{\text {OUT }}=0 \mathrm{~V}, \mathrm{~V}_{\text {SS }}=$ open | - | -0.4 | -1.5 | $\mu \mathrm{A}$ |
| Diode Forward Voltage | $V_{F}$ | $\mathrm{I}_{\mathrm{F}}=20 \mathrm{~mA}$ | - | 1.6 | 2.0 | V |
| Diode Breakdown Voltage | $\mathrm{BV}_{\mathrm{B}}$ |  | 30 | 50 | - | V |
| Turn-on Delay Time | $\mathrm{t}_{\text {PHL }}$ | $\mathrm{R}_{\mathrm{L}}=6.8 \mathrm{k} \Omega$ | - | 3.0 | 7.0 | $\mu \mathrm{S}$ |
| Turnoff Delay Time | $\mathrm{t}_{\text {PLH }}$ | $\mathrm{R}_{\mathrm{L}}=6.8 \mathrm{k} \Omega$ | - | 3.0 | 7.0 | $\mu \mathrm{s}$ |

## SERIES UDN-6100A and UDN-6100R FLUORESCENT DISPLAY DRIVERS

## FEATURES

- Digit or Segment Drivers
- Low Input Current
- Integral Output Pull-Down Resistors
- High Output Breakdown Voltage
- Single or Split Supply Operation


UDN-6116*
UDN-6126*


UDN-6118*
UDN-6128*


DWG. NO. A-11,222
UDN-6138*
UDN-6148*

## DEVICE TYPE NUMBER DESIGNATION

| Input Compatibility | No. of Drivers | $V_{\text {OUT }}$ | No. of Pins | Type Number |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Plastic DIP | Ceramic DIP |
| 5 V TLL, CMOS | 6 | 60 V | 16 | UDN-6116A-2 | UDN-6116R-2 |
|  |  | 80 V | 16 | UDN-6116A | UDN-6116R |
|  |  | 110 V | 16 | UDN-6116A-1 | - |
|  | 8 | 60 V | 18 | UDN-6118A-2 | UDN-6118R-2 |
|  |  | 80 V | 18 | UDN-6118A | UDN-6118R |
|  |  | 110 V | 18 | UDN=6118A-1 | - |
|  |  | $\pm 30 \mathrm{~V}$ | 20 | UDN-6138A-2 | - |
|  |  | $\pm 40 \mathrm{~V}$ | 20 | UDN-6138A | - |
| 6-15V CMOS, PMOS | 6 | 60 V | 16 | UDN-6126A-2 | UDN-6126R-2 |
|  |  | 80 V | 16 | UDN-6126A | UDN-6126R |
|  |  | 110 V | 16 | UDN-6126A-1 | - |
|  | 8 | 60 V | 18 | UDN-6128A-2 | UDN-6128R-2 |
|  |  | 80 V | 18 | UDN-6128A | UDN-6128R |
|  |  | 110 V | 18 | UDN-6128A-1 | - |
|  |  | $\pm 30 \mathrm{~V}$ | 20 | UDN-6148A-2 | - |
|  |  | $\pm 40 \mathrm{~V}$ | 20 | UDN-6148A | - |

ABSOLUTE MAXIMUM RATINGS at $\mathrm{T}_{\mathrm{A}}=+\mathbf{2 5}{ }^{\circ} \mathrm{C}$(Voltages are with reference to ground unless otherwise shown)
Supply Voltage, $V_{B B}$ (all devices, suffix $A$ or $R$ ) ..... 85 V
(UDN-6138/48A or R, ref. $\mathrm{V}_{\mathrm{EE}}$ ) ..... 85 V
(all devices, suffix $A-1$ ) ..... 115 V
(all devices, suffix A-2 or R-2) ..... 65 V
(UDN-6138/48A-2 or R-2, ref. VEE) ..... 65 V
Supply Voltage, $\mathrm{V}_{\mathrm{EE}}$ (UDN-6138/48 all suffixes) ..... $-40 \mathrm{~V}$
Input Voltage, $\mathrm{V}_{\mathrm{IN}}$ (all devices) ..... 20 V
(UDN-6138/48 all suffixes, ref. $\mathrm{V}_{\mathrm{EE}}$ ) ..... 55 V
Output Current, IOUT . . . . . ............. ..... -40 mA
Operating Temperature Range, $T_{A}$
$-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{I}_{S}$ ..... $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$


DWG. 10. A-11,224

## ELECTRICAL CHARACTERISTICS (over operating temperature range)

Note: All Values Specified At -

| Suffixes | $A$ | $R$ | $A-1$ | $A-2$ | $R-2$ |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{B E}=$ | 80 | 80 | 110 | 60 | 60 | Volts |
| ${ }^{V_{F I}}=$ | 0 | 0 | NA | 0 | 0 | Volts |

*UDN-6138 and UDN-6148

| Characteristic | Symbol | Applicable Devices |  | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Basic Part No. | Suffix |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | Iout | All | All | $\mathrm{V}_{\text {IN }}=0.4 \mathrm{~V}$ | - | - | 15 | $\mu \mathrm{A}$ |
| Output OFF Voltage | $V_{\text {Out }}$ | All | All | $\mathrm{V}_{1 \text { IN }}=0.4 \mathrm{~V}$ | - | - | 1.0 | V |
| Output Pull-Down Current | I ${ }_{\text {OUT }}$ | All | A or R | Input Open,$V_{\text {OUT }}=V_{\text {BB }}$ | 450 | 650 | 1100 | $\mu \mathrm{A}$ |
|  |  |  | A-1 |  | 600 | 900 | 1500 | $\mu \mathrm{A}$ |
|  |  |  | A-2 or R-2 |  | 350 | 500 | 715 | $\mu \mathrm{A}$ |
| Output ON Voltage | $\mathrm{V}_{\text {OUT }}$ | UDN-6116/18/38 | $A$ or R | $\begin{aligned} & \mathrm{V}_{\text {IV }}=2.4 \mathrm{~V}, \\ & \mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA} \end{aligned}$ | 77 | 78 | - | V |
|  |  |  | A-1 |  | 107 | 108 | - | V |
|  |  |  | A-2 or R-2 |  | 57 | 58 | - | V |
|  |  | UDN-6126/28/48 | A or R | $\begin{aligned} & V_{\text {IN }}=4.0 \mathrm{~V}, \\ & \mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA} \end{aligned}$ | 77 | 78 | - | V |
|  |  |  | A-1 |  | 107 | 108 | - | V |
|  |  |  | A-2 or R-2 |  | 57 | 58 | - | V |
| Input ON Current | $\mathrm{I}_{\mathrm{N}}$ | UDN-6116/18/38 | All | $\mathrm{V}_{\text {IV }}=2.4 \mathrm{~V}$ | - | 120 | 225 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$ | - | 375 | 650 | $\mu \mathrm{A}$ |
|  |  | UDN-6126/28/48 | All | $V_{\text {IN }}=4.0 \mathrm{~V}$ | - | 130 | 250 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {IN }}=15 \mathrm{~V}$ | - | 675 | 1150 | $\mu \mathrm{A}$ |
| Supply Current | $\mathrm{I}_{\text {BB }}$ | $\frac{\text { All }}{\text { UDN-6116 }}$ | All | All Inputs Open | - | 10 | 100 | $\mu \mathrm{A}$ |
|  |  |  | A or R | All Inputs $=2.4 \mathrm{~V}$ | - | 5.0 | 7.5 | mA |
|  |  |  | A-1 | Two Inputs $=2.4 \mathrm{~V}$ | - | 2.5 | 4.5 | mA |
|  |  |  | A-2 or R-2 | All Inputs $=2.4 \mathrm{~V}$ | - | 4.0 | 6.0 | mA |
|  |  | UDN-6118/38 | A or R | All Inputs $=2.4 \mathrm{~V}$ | - | 6.0 | 9.0 | mA |
|  |  |  | A-1 | Two Inputs $=2.4 \mathrm{~V}$ | - | 2.5 | 4.5 | mA |
|  |  |  | A-2 or R-2 | All Inputs $=2.4 \mathrm{~V}$ | - | 5.5 | 8.0 | mA |
|  |  | UDN-6126 | $A$ or R | All Inputs $=4.0 \mathrm{~V}$ | - | 5.0 | 7.5 | mA |
|  |  |  | A-1 | Two !nputs $=4.0 \mathrm{~V}$ | - | 2.5 | 4.5 | mA |
|  |  |  | A-2 or R-2 | All Inputs $=4.0 \mathrm{~V}$ | - | 4.0 | 6.0 | mA |
|  |  | UDN-6128/48 | $A$ or R | All Inputs $=4.0 \mathrm{~V}$ | - | 6.0 | 9.0 | mA |
|  |  |  | A-1 | Two Inputs $=4.0 \mathrm{~V}$ | - | 2.5 | 4.5 | mA |
|  |  |  | A-2 or R-2 | All Inputs $=4.0 \mathrm{~V}$ | - | 5.5 | 8.0 | mA |

## RECOMMENDED OPERATING CONDITIONS

| Supply Voltage | $V_{B B}$ | $\begin{gathered} \text { UDN-6116/18/ } \\ 26 / 28 \end{gathered}$ | $A$ or $R$ | 5.0 | - | 70 | $V$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | A-1 | 5.0 | - | 100 | V |
|  |  |  | A-2 or R-2 | 5.0 | - | 50 | V |
|  |  | UDN-6138/48 | A | 5.0 | - | 40 | V |
|  |  |  | A-2 | 5.0 | - | 30 | V |
|  | $V_{\text {EE }}$ | UDN-6138/48 | A | 0 | - | -40 | V |
|  |  |  | A-2 | 0 | - | -30 | V |
| Input ON Voltage | $V_{\text {IN }}$ | UDN-6116/18/38 | All | 2.4 | - | 15 | V |
|  |  | UDN-6126/28/48 | All | 4.0 | - | 15 | V |
| Output ON Current | $\mathrm{I}_{\text {OUT }}$ | All | All | - | - | -25 | mA |

[^10]
## PARTIAL SCHEMATIC

| Type (All Suffixes) | $R_{\text {IN }}$ | $R_{B}$ |
| :---: | :---: | :---: |
| UDN-6116/18/38 | $10 \mathrm{k} \Omega$ | $30 \mathrm{k} \Omega$ |
| UDN-6126/28/48 | $20 \mathrm{k} \Omega$ | $20 \mathrm{k} \Omega$ |



OWG.NO. A-10,592C

TYPICAL MULTIPLEXED FLUORESCENT DISPLAY


# UDN-6164A AND UDN-6184A GAS-DISCHARGE DISPLAY DRIVERS 

## FEATURES

- TTL/MOS Compatible Inputs
- High Output Breakdown Voltage
- High Output Current Capability
- Low Power
- Reliable Monolithic Construction

THESE monolithic high-voltage bipolar integrated circuits dramatically reduce the number of discrete components required to link MOS, or other low-voltage circuitry, with the anodes of gas-discharge display panels.

Types UDN-6164A and UDN-6184A are used with multiplexed gasdischarge display panels, such as the Burroughs Panaplex ${ }^{\circledR}$, the Cherry Plasma-Lux ${ }^{\circledR}$, and the Beckman SP series, in calculator, clock, or instrumentation applications.

Each driver has appropriate level shifting, signal amplification, output off-state voltage bias, and 40 mA output current sourcing for sequential addressing of display panel anodes. The inputs include pull-down resistors for direct connection to open-drain PMOS logic.

Type UDN-6164A contains six drivers; Type UDN-6184A contains eight drivers. Applications with a greater number of digits may use any combination of units for minimum package count.

The devices can be used in a wide variety of low- to high-voltage applications. High reliability, small size, ease of installation, and low cost make them an ideal choice for many applications.

[^11]
## ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ Free-Air Temperature

| Supply Voltage, $\mathrm{V}_{\text {BB }}$ | +115V |
| :---: | :---: |
| Input Voltage, $\mathrm{V}_{\text {W }}$ | $+20 \mathrm{~V}$ |
| Output Current, $\mathrm{I}_{\text {out }}$ | -40 mA |
| Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ |  |
| UDN-6164A | 2.1 W* |
| UDN-6184A | 2.3 W** |
| Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature Range, $\mathrm{T}_{S}$ | $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

[^12]

UDN-6164A
(SIX DRIVERS)


UDN-6184A (EIGHT DRIVERS)

## PARTIAL SCHEMATIC

ONE OF SIX DRIVERS (UDN-6164A)
ONE OF EIGHT DRIVERS (UDN-6184A)


The high input impedance of these devices makes them susceptible to static discharge damage associated with handling and testing. Techniques similar to those used for handling MOS devices should be employed.

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{BB}}=110 \mathrm{~V}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | Iout | $\mathrm{V}_{\mathrm{IN}}=0.4 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 15 | $\mu \mathrm{A}$ |
| Output OFF Voltage | $V_{\text {OUT }}$ | $\mathrm{V}_{\mathbb{I N}}=0.4 \mathrm{~V}$ | - | - | 1.0 | V |
| Output Pull-Down Current | $\mathrm{I}_{\text {OUT }}$ | Input Open, $\mathrm{V}_{\text {OUT }}=\mathrm{V}_{\text {BB }}$ | 600 | 900 | 1500 | $\mu \mathrm{A}$ |
| Output ON Voltage | $V_{\text {out }}$ | $\mathrm{V}_{\text {IN }}=2.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$ | 107 | 108 | - | V |
| Input ON Current | $\mathrm{I}_{\text {w }}$ | $V_{\mathbb{N}}=2.4 \mathrm{~V}$ | - | 120 | 225 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\mathrm{IN}}=5.0 \mathrm{~V}$ | - | 375 | 650 | $\mu \mathrm{A}$ |
| Supply Current | $I_{B B}$ | All Inputs Open | - | 10 | 100 | $\mu A$ |
|  |  | Two Inputs $=2.4 \mathrm{~V}$ | - | 2.5 | 4.5 | mA |

## RECOMMENDED OPERATING CONDITIONS

| Supply Voltage | $V_{B B}$ |  | - | - | 100 |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Input ON Voltage | $V_{\mathbb{I N}}$ |  | - | 15 | V |
| Output ON Current | $\mathrm{I}_{\mathbb{N}}$ |  | - | - | -25 |

[^13]
## SERIES UDN-7180A <br> GAS DISCHARGE DISPLAY SEGMENT DRIVERS

## FEATURES

- Reliable Monolithic Construction
- High Output Breakdown Voltage
- Low Power
- TIL/MOS Compatible Inputs



## Description

Series UDN-7180A segment drivers are monolithic high-voltage bipolar integrated circuits for interfacing between MOS or other low-voltage circuits and the cathode of gas-discharge display panels.

These drivers reduce substantially the number of discrete components required with panels (Beckman, Burroughs, Dale, Matsushita, NEC, Pantek, etc) in calculator, clock and instrumentation applications.

The UDN-7183A, UDN-7184A, and UDN-7186A drivers contain appropriate level shifting, signal amplification, current limiting, and output OFF-state voltage bias. The UDN-7180A driver requires external current limiting and is intended for higher-current applications or where individual outputs are operated at different current levels (i.e. with alpha-numeric displays). All inputs have pull-down resistors for direct connection to open-drain PMOS logic.

These devices provide output currents suitable for display segments in a wide variety of display sizes and number of display digits. Either a fixed split supply operation or a feedback-controlled scheme is allowed.

## Applications

The Series UDN-7180A drivers can be used in a wide variety of lowlevel to high-voltage applications utilizing gas discharge displays such as those found in calculators, clocks, point-of-sale terminals, and instruments. Their high reliability combined with minimum size, ease of installation, and the cost advantages of a complete monolithic interface make them the ideal choice in many applications. A typical application showing the use of these devices, and their counterpart anode drivers, is shown.

## ABSOLUTE MAXIMUM RATINGS AT $25^{\circ} \mathrm{C}$

Suppiy Voltage, $\mathrm{V}_{\text {kK }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . -115 V
Input Voltage, $\mathrm{V}_{\mathbb{N}}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . +20 V
Output Current, I Iout: UDN-7180A . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20 mA

UDN-7184A . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 2.0 mA
UDN-7186A . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1.0 mA
Power Dissipation, $P_{0}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1.13 W*

Storage Temperature Range, $T_{S} \ldots . . . . . . . . . . . . . . . . . . . . . . . .{ }^{\circ} 5^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $9.1 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$

Due to the high input impedance of these devices, they are susceptible to static discharge damage sometimes associated with handling and testing. Therefore, techniques similar to those used for handling MOS devices should be employed.

ELECTRICAL CHARACTERISTICS: $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{Kx}}=-110 \mathrm{~V}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | $\begin{aligned} & \text { Test } \\ & \text { Fig. } \end{aligned}$ | UDN-7180/83A |  |  | UDN-7184A |  |  | UDN-7186A |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Min. | Typ. | Max. | Min. | Typ. | Max. |  |
| $\begin{aligned} & \hline \text { Output ON Voltage } \\ & \text { UDN-7183/84/86A } \\ & \hline \end{aligned}$ | $V_{\text {ON }}$ | All inputs at 4.5 V | 1 | -100 | -104 | - | -98 | -102 | - | -97 | -100 | - | V |
|  |  | All inputs at 4.5 $\mathrm{V}, \mathrm{V}_{\mathrm{KK}}=-70 \mathrm{~V}$ | 1 | - | -66 | - | - | -65 | - | - | -63 | - | V |
| $\begin{aligned} & \text { Output ON Voltage } \\ & \text { UDN-7180A } \end{aligned}$ | $V_{\text {ON }}$ | $\begin{aligned} & \text { All inputs at } 4.5 \mathrm{~V} \text {, } \end{aligned}$ |  | -105 | -108 | - | - | - | - | - | - | - | V |
| Output OFF Voltage | $V_{\text {OfF }}$ | All inputs at 0.4 V , Reference $V_{\mathrm{KK}}$ | 2 | 76 | 84 | - | 76 | 84 | - | 76 | 84 | - | V |
| $\begin{gathered} \hline \begin{array}{c} \text { Output Current } \\ (\text { (Imiring }) \end{array} \\ \hline \end{gathered}$ | $\mathrm{T}_{\mathrm{N}}$ | All inputs at $15 \mathrm{~V}, \mathrm{~V}_{\mathrm{KK}}=-110 \mathrm{~V}$, <br> Test output held at -60 V | 3 A | UDN-7183A only$1475 \quad 1850 \quad 2450$ |  |  | 910 | 1140 | 1520 | 440 | 550 | 725 | $\mu \mathrm{A}$ |
| $\begin{aligned} & \text { Output Current } \\ & (\text { I SESNSE } \text { ) } \end{aligned}$ | $\mathrm{T}_{\text {ON }}$ | All inputs at $0.4 \mathrm{~V}, \mathrm{~V}_{\mathrm{KK}}=-110 \mathrm{~V}$, <br> Test output held at -66 V | 3 B | -95 | -120 | -155 | -65 | -85 | -115 | -50 | -65 | -90 | $\mu \mathrm{A}$ |
| Tnput High Current | $I_{1 H}$ | Test input at 15 V , Other inputs at 0 V | 4 | - | 200 | 275 | - | 200 | 275 | - | 200 | 275 | $\mu \mathrm{A}$ |
| Tnput Low Current | $I_{1 L}$ | Test input at 0.4 V , One input at 4.5 V , Other inputs at 0.4 V | 6 | - |  | 10 | - |  | 10 | - |  | 10 | $\mu \mathrm{A}$ |
| Supply Current | $\mathrm{T}_{\mathrm{KK}}$ | All inputs at OV | 6 |  | -125 | -175 | - | -125 | -175 |  | -125 | -175 | $\mu \mathrm{A}$ |

NOTES:

1. All voltage measurements are referenced to pin 9 unless otherwise specified.
2. All voltage measurements made with $10 \mathrm{M} \Omega$, DVM or VTVM.
3. Recommended $\mathrm{V}_{\mathrm{KK}}$ operating range: -85 to -110 V .
4. Positive (negative) current is defined as going into (coming out of) the specified device pin.

## TEST CIRCUITS



FIGURE 1


DWG. NO. A-9738B

FIGURE 2


DWG. NO. A-9739B
FIGURE 3A


DWG. NO. A-9740B

FIGURE 3B

FIGURE 4


FIGURE 5


DWG: No. A-9743

FIGURE 6

## PARTIAL SCHEMATIC




TYPICAL SIX-DIGIT CLOCK



## ANODE AND CATHODE WAVEFORMS



# A Monolithic IC Series for Gas-Discharge Display Interface 

## Introduction

The switching of the high voltages necessary for display panels such as the Burroughs Panaplex ${ }^{(3)}$ has long presented difficulties to the semiconductor industry - particularly to IC manufacturers. It is difficult to fabricate devices capable of sustaining 200 volts or greater with standard IC processes of today. Solutions to the high voltage gas discharge display interface also must be inexpensive as well as functional; this cost/ simplicity factor prohibits most unusual or exotic circuit designs and/or IC processes.

The earliest (and a great many recent) gas discharge interface schemes used discrete components, but that has been an increasingly cumbersome and expensive solution. Competition at the system level has largely come from LEDs, and a great many standard ICs are available for the smaller LEDs. In most instances, the small displays have gone to LEDs. However, the larger display applications are still an opportunity for gas discharge since character size and cost are not directly related. The cost impact upon the potential for gas discharge displays in many systems is a function of interface complexity and cost, and it was to this end that a joint Sprague/Burroughs effort was launched.

Early Sprague/Burroughs meetings were held to define the relevant factors involved in such a program and provide the necessary insight for both parties into
the capabilities of diode isolated ICs, the voltage and current requirements of the Panaplex displays, the need for minimization of power (battery systems), packaging of the circuits, component count and cost, etc. Add to this the potential for use with feedback controlled supplied, poorly regulated d-c supplies, the wide variety of numbers of display digits, the range of digit sizes (in use or contemplated), etc., and our task was not to be an easy one.

Our direction was determined by two factors: a history of fabricating $130-140$ volt PN diode isolated display circuits, and a more recent effort to utilize compatible thin-film resistor technology. These factors, coupled with considerable expertise in designing and processing high voltage ICs, dictated an approach utilizing a split ( $\pm 100 \mathrm{~V}$ ) supply. The split supply would provide the 200 volts needed to ionize the display and the resistor capability would greatly aid the incorporation of functions previously done by discrete components - including both input and output (segment) current limiting, pulldown (open drain PMOS), pullup and pulldown reference for IC outputs, and a high impedance voltage divider for the output OFF bias. All level shifting is accomplished via use of PNP or NPN transistors, and the capacitors previously required were negated.

Figure 1


## Basic Scheme

Replacing discrete components through incorporating their function into this IC series results in the block diagram of Figure 1 with its basic requirement for a single digit and single segment driver; a scheme capable of driving as many as eight digits and the eight segments. Additional digits or segments beyond the eight provided in an 18 -lead DIP may be driven by combinations of packages beyond the minimum two necessary. Example: three ICs - two digit and one segment - will fulfill the needs of a 12 to 16 digit calculator.

Included in this series of high voltage interface are two digit driver packages: UDN-6164 (6-digit), and UDN-6184 (8-digit). Segment drivers include the UDN-7180, UDN-7183, UDN-7184, and UDN-7186, and the four offer current ranges compatible with display sizes from $0.250^{\prime \prime}$ to $1^{\prime \prime}$ panels, and others will be made available as needs are defined.

## Digit Interface

The digit driver is the more complex of the two and its schematic is shown in Figure 2. Input address polarity is positive (active high in TTL parlance) and the circuit is designed to interface from TTL ( 4.5 volts from open collector - or using pull-up to $\mathrm{V}_{\mathrm{Cc}}$ ), CMOS, PMOS, etc. Input currentlimiting and one-half of the pull-down for open drain PMOS is the function of $\mathrm{R}_{5} ; \mathrm{R}_{6}$ adds the second half of the pull-down to the ground bus. The protective value of $R_{4}$ and $R_{5}$ must be noted; a junction failure in $\mathrm{Q}_{1}$ has the two resistors as a current limiter to the MOS (or TTL) output and will minimize the likelihood of destroying the low level logic outputs.

Input transistor $\mathrm{Q}_{4}$ is a high voltage inverter and sinks the base current of PNP $\mathrm{Q}_{3}$. A positive input ( 4.5 to 20 V ) will turn on $\mathrm{Q}_{4}$ and this base current ( $65 \mu \mathrm{~A}$ typ.) for $\mathrm{PNP}_{3}$ will turn on the output Darlington $\left(\mathrm{Q}_{1}\right.$ and $\left.\mathrm{Q}_{2}\right)$ and source digit current.

## ELECTRICAL CHARACTERISTICS: $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{KK}}=-110 \mathrm{~V}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Test Fig. | UDN-7180/83A | UDN-7184A |  |  | UDN-7186A |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. Typ. Max. | Min. | Typ. | Max. | Min. | Typ. Max. |  |
| Output ON Voltage UDN-7183/84/86A | VON | All inputs at $6 \mathrm{~V}^{*}$ | 1 | -100-104- | -98 | -102 |  | -97 | -100- | V |
|  |  | All inputs at $6 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{KK}}=-70 \mathrm{~V}$ | 1 | -66 | - | -65 | - | - | -63 | V |
| Output ON Voltage UDN F 7180A | VON | All inputs at $6 \mathrm{~V}^{*}$, $\mathrm{ION}_{\mathrm{N}}=14 \mathrm{~mA}$ |  | $-105-108-$ | - | - | - | - | - - | V |
| Output OFF Voltage | Voff | All inputs at 0.5 V , Reterence $V_{K K}$ | 2 | $76.84-$ | 76 | 84 | - | 76 | 84 | V |
| Output Current (limiting) | Ion | All inputs at $15 \mathrm{~V}, \mathrm{~V}_{\mathrm{KK}}=-110 \mathrm{~V}$, Test output held at -60 V | 3A | $\begin{array}{\|ccc\|} \hline \text { UDN- } 7183 \mathrm{~A} \text { only } \\ 1475 & 1850 & 2450 \\ \hline \end{array}$ | 910 | 1140 | 1520 | 440 | $550 \quad 725$ | $\mu \mathrm{A}$ |
| Output Current (ISENSE) | ION | All inputs at $0.5 \mathrm{~V}, \mathrm{~V}_{K K}=-110 \mathrm{~V}$, Test output held at -66 V | 3B | $-95-120-155$ | -65 | -85 | -115 | -50 | -65-90 | $\mu \mathrm{A}$ |
| Input High Current | $I \mathrm{IH}$ | Test input at 15 V , Other inputs at 0 V | 4 | $200 \quad 275$ | - | 200 | 275 |  | $200 \quad 275$ | $\mu \mathrm{A}$ |
| Input Low Current | 111 | Test input at $0.5 \mathrm{~V}, 0$ one input at $6 \mathrm{~V}^{*}, 0$ ther inputs at 0.5 V | 5 | 110 | - | 1 | 10 | - | 110 | $\mu \mathrm{A}$ |
| Supply Current | IKK | All inputs at 0 V | 6 | - $125 \quad 175$ |  | 125 | 175 |  | $125 \quad 175$ | $\mu \mathrm{A}$ |

[^14]
## PARTIAL SCHEMATIC



DWG.NO. A-11,364

Figure 2

Consistent ionization and extinguishing of the display panel is the result of the $60-75$ volt swings available from both digit and segment ICs. The conditions that previously created problems for the direct MOS drive with minimal swings at the output have been very adequately handled with the increased output swings of the $6100 / 7100$ series. Problems from leading zero blanking, low temperature, low ambient light, etc. which previously gave difficulty are well taken care of with this series of ICs.

## Segment Inferface

The segment driver circuit is shown in Figure 3 and the value of $R_{2}$ (segment limiting) is determined via masking for the appropriate display current. Its
counterpart pull-up resistor $R_{1}$ is also changed to some known ratio of $R_{2}$. The ground terminal (\#9) is referenced near, or connected directly to ground, and the $\mathrm{V}_{\mathrm{KK}}$ line is typically a -90 to -100 volts.
The input PNP $\left(Q_{1}\right)$ serves as a level translator and provides $\mathrm{d}-\mathrm{c}$ level shifting to the output Darlington $\left(Q_{2}\right.$ and $\left.Q_{3}\right)$. Emitter resistor ( $R_{3}$ ) both limits the input current and furnished pull-down for open drain PMOS. An added intent is the measure of protection furnished the MOS by the very high impedance of $\mathrm{R}_{3}$.
The basic switching function is the combination of PNP $Q_{1}$, Darlington $Q_{2}$ and $Q_{3}$, and the associated resistors $R_{1}, R_{2}$, and $R_{3}$. Address polarity is again active high. The input may be raised a maximum of 20 volts above ground and will function with input levels obtained from CMOS and open collector TTL (4.5 V).

## PARTIAL SCHEMATIC



Figure 3

## TYPICAL APPLICATION



Figure 4

## HIGH-VOLTAGE INTERFACE DRIVERS (Continued)

The OFF output biasing network is common to all the individual drivers with the level of bias determined by the ratio of $R_{7}$ to the total of $R_{7}$ and $R_{8}$. As in the digit driver, the value of output bias is $\approx 2 / 3$ the voltage across $\mathrm{V}_{\mathrm{KK}}$ and ground - thus insuring sufficient 'on to off' swings to properly fire, and effectively extinguish unaddressed segments during a scan. Emitter follower $Q_{4}$ and $Q_{5}$ sources current to the pull-up bus connected to the various outputs as they are turned on during the display scan.

## Minimum Component Interface

The impact of this new product family may be seen in the typical digital clock of Figure 5. This a-c powered clock uses a Mostek 50250 clock IC, a UDN-6164 digit driver, and a UDN-7183 segment driver. Total component count is approximately 30
pieces, and the board layout is straightforward and uses single-sided board.

Many calculator interface schemes use considerable numbers of components (70 to 100 typically) to drive gas discharge panels. As one example: a twelve digit/eight segment machine uses 85-90 discretes while the new IC version uses only three packages, and results in less space along with considerable simplification. Other applications will benefit similarly with this series of circuits.

## Summary

Display technology and usage has emerged at a mind boggling rate in the past several years - largely due to the fantastic growth rate of calculators. The planar gas panels have been an integral portion of this burgeoning market, but like all the other displays


Figure 5
available does not meet the requirements for an ideal display.

Gas discharge panels are a fine combination of aesthetics, reliability, low cost, large character size, multiplexing capability, etc., but have been impacted to some degree by the lack of an available and inexpensive, totally monolithic interface. The move toward IC interface for displays has stifled some potential - largely in favor of LEDs; although many applications requiring large characters and/or in high ambient light turn toward gas panels. The planar gas discharge display is a long way from obscurity, and the availability of this family of ICs should open up new areas as well as satisfying existing systems.

The intent from the inception of this program has been to produce and provide a standard, inexpensive and easy to use interface for gas discharge displays. A great many potential applications exist for these circuits in consumer and commercial products. From the calculator and digital clock areas this product also will find use in automotive dashboards, point-of-sale systems, electronic cash registers and scales, and instrumentation. The market for displays is still very elastic, and many applications for gas discharge panels are continuing to appear. The Sprague contribution to this market is this series of state-of-theart interface ICs.

## TRENDS IN IC INTERFACE FOR ELECTRONIC DISPLAYS

## Introduction

Display technology was truly set into high gear by the explosion of the electronic calculator business. Expansion at a phenomenal pace continues, encompassing a multitude of products, particularly high-volume consumer products (calculators, clocks, games, and watches). Recently, further stimulated by the "microprocessor revolution," with its far-reaching effects, and the resulting changeover to solid state design from electromechanical, mechanical, fluidic, or electrical systems, the vistas for displays have expanded well beyond the horizon. Products have been and are being developed, using microprocessors and displays, that never previously existed.

To augment this microprocessor revolution, semiconductor manufacturers are developing many new interface circuits useful with displays, although some of these will not be exclusively for display systems. To accomplish this, the present boundaries of device design, process, packaging, and electrical parameters will require continual extension and expansion.

## Display Buffers

A continuing evolution of standard interface ICs is needed to buffer low-level logic from high-voltage and/or high-current loads. Some of this buffer development will serve display systems. Since there already is a broad assortment of buffers (particularly for low- to medium-current LED applications), the ongoing development in simple or low-order interface will mainly concentrate upon further reduction in discrete component count, package improvement (particularly for high-current/high-power devices), improvements in device current, voltage, switching speed, and greater reliability.

Figures 1, 2, and 3 show some Sprague interface ICs that represent buffer circuits; other vendors supply similar, or identical, high-current or high-voltage buffers to allow operation of displays from low-level logic. Two basic changes have occurred relatively recently:

1. Greater use of 18 -pin DIPs for eight driver channels (Source Driver, Figure 2).
2. Creation of sourcing functions (Figures 2 and 3 ; useful for LED, gas-discharge, vacuum fluorescent, incandescent, and electromagnetic displays, depending upon device ratings). While further buffer designs are needed (particularly in high-current (>2 A) and high-voltage ( $>100 \mathrm{~V}$ ) circuits), the main emphasis will be toward the incorporation of logic and control circuitry with output buffers.

## Complex Interface

Paralleling (though lagging) the microprocessor LSI revolution is the area of greatest future for IC display circuits: The need for complex, smart or high-order interface. This will be MSI to LSI logic (with perhaps some linear functions) combined with suitable output buffers.


DVG. No. A-9236A
Figure 1A


DWG. No. A-9248 A

Figure 1B

UHP-480 GAS DISCHARGE DRIVER


Figure 2A


Figure 28

## SERIES UDN-2980 SOURCE DRIVER

Display interface ICs (similar to the MOS I/O control chips), both custom and standard product, are becoming available in this category. High-volume applications may justify custom ICs, but the more general trend will be toward standard, off-the-shelf designs chiefly due to the high costs of developing custom ICs.

The higher voltage displays (gas-discharge, vacuum fluorescent, a-c plasma, and d-c electroluminescent) may share some circuits (if appropriately planned and designed), particularly in the area of matrix displays. It is difficult to imagine, however, much commonality between high-current LEDs, high-voltage gas-discharge or a-c plasma, and low-power LCDs,


Figure 3
8-DIGIT/8-SEGMENT HIGH-CURRENT LED INTERFACE
although they should share considerably the development of cellular CAD circuit designs. Basic shift registers, latches and decoders do have considerable commonality.

In Figure 4 is a pinout and logic diagram of the first BiMOS Sprague IC combining logic and output drive. Although not expressly intended for display applications, this BiMOS (CMOS logic and bipolar outputs) IC has a great deal of utility to engineers working with lower voltages and high currents (LEDs, incandescent and electromagnetic displays). Type UCN4801A is a parallel-in/parallel-out unit composed of eight ' $D$ ' latches and eight $350 \mathrm{~mA} / 50 \mathrm{~V}$ bipolar Darlington outputs.


Figure 4A


Figure 4B
UCN-4801A BIMOS LATCH/DRIVER

More recently, Sprague has designed a serial-in/parallel-out BiMOS interface IC expressly for use with vacuum fluorescent displays. Figure 5 shows the UCN-4810A 10-bit serial-in/ parallel-out interface for use with VF displays; the use of serial data allows 10 output lines, data in and data out in a standard 18-lead DIP. It makes possible both fewer IC packages and simpler PC board wiring, although it is slower than a parallel data approach. It uses only a single pin of the I/O ports.


Figure 5A UCN-4810A PINOUT


Figure 5B
UCN-4810A VF DRIVER BLOCK DIAGRAM

A slightly more recent design for vacuum fluorescent displays is the Sprague UCN-4815A. This is a 22 -lead, 8 -bit parallel-in/parallel-out BiMOS unit. The unit may have data inputs and a strobe bus (see Figure 6). The chip enable/blanking pin provides control of VF buffers. A power-on-clear is internally incorporated.


Figure 6
UCN-4815A PARALLEL 8-BIT VF INTERFACE

## Device Technologies

With the exception of LCD displays (which at least until recently have been largely, if not entirely, driven by MOS) the display and interface technologies in high-volume use are mainly associated with bipolar semiconductors. Early display interface ICs (particularly devices such as the 7447 and 7448 ) were aimed at LED technology and represent MSI with modest output capability. The increasing use of higher voltage displays, multiplexed high-current applications, and the need for greater circuit complexity and low pin count will dictate other technologies, such as $I^{2} L$, BiMOS, CMOS /DMOS, and possibly DMOS.

## Standard Bipolar

Standard bipolar technology, long associated with TTL or linears (early op amps), appears very limited in scope for the future. Circuit density and supply power requirements will dictate other processes for functions beyond the simple MSI level. The advantages of standard bipolar ICs appear to be in the areas of simple high-current, high-power or high-voltage interface. In particular, applications requiring the combination of high voltages ( $\geq 100 \mathrm{~V}$ ) or multiple high-current outputs ( $\geq 2 \mathrm{~A}$ ) will restrict the logic /control circuitry to a low level. Cost, chip size and package power dissipation will restrict this circuitry largely to versatile, simple buffers.

## $I^{2} L$

Anticipated to increase significantly is the use of $I^{2} L$ for systems of low to modest voltages (LEDs through VF). The present limits of $I^{2} L$ appear to be limited to applications below the 50to 60 -volt level. $I^{2} L$, with its combination of circuit density, low power and reasonable switching speeds should make a fine match for LEDs or other low-voltage display applications. For higher voltages ( $>25$ or 30 V ), prospects the penalty of reduced circuit density may diminish its cost effectiveness. Some increase in standoff voltage may be afforded by the uses of cascaded output transistors or process improvements, thus reducing the need to sacrifice logic density. Without a standard $\mathrm{I}^{2} \mathrm{~L}$ logic family, the main market penetration would appear to be custom designs although there is a definite opportunity for standard interface for lower voltage applications, particularly LEDs and vacuum fluorescent.

## BiMOS

BiMOS, a combination of CMOS and bipolar for interface ICs, seems to fit a technology niche of higher breakdown voltages than $I^{2} L$, especially where logic power and supply voltage range ( 5 to 15 V ) is important. BiMOS or BiFET ICs, which are presently on the market, are largely related to operational amplifiers, although other uses, such as the Sprague application of BiMOS to interface, are emerging.

Currently, it is feasible to design and manufacture BiMOS interface with breakdown voltages in the 80 to 100 V range. With additional time and greater concentration on increasing BV, it appears that higher voltages ( $\geq 150 \mathrm{~V}$ ) for output buffers could be obtained. By obtaining breakdowns in the 120 V to 160 V range, BiMOS then becomes a viable IC technology for interface for the higher voltage displays: d-c gas-discharge with $\pm 100$ to $\pm 130 \mathrm{~V}$; a-c plasma with 160 to 170 V , and glow transfer or d-c electroluminescent (DCEL) opportunities with a range of $120-150$ volts.

Switching speeds and output configurations (active pull-down or resistive) are critical to matrix displays (particularly a-c plasma) with large numbers of drive lines. Adding active pull-down or pull-up will tend to increase chip size (and cost), thus adding to the potential overall difficulty of BiMOS with its greater process complexity and slightly longer manufacturing cycle. This does appear to be a very key technology for the near future. Its product niche will include for applications requiring 60 to 100 V (or more) breakdowns, low-power logic, wide supply range, modest speeds, and MSI to small LSI.

## CMOS/DMOS

Chiefly being carried on by Texas Instruments, CMOS /DMOS display interface appears to be intended for much of the same display market as BiMOS. Product information now available indicates 60 to 100 V breakdown (DMOS outputs), CMOS logic, low to modest output currents ( $\leq 25 \mathrm{~mA}$ ), and logic speeds to 4 MHz . Designs now being promoted are targeted toward a-c plasma and vacuum fluorescent panels.

Two apparent disadvantages now appear to exist:

1. Logic operates from $12 \mathrm{~V} \pm 10 \%$ (may be done to provide maximum speed).
2. Output drive current is insufficient for high-current displays (without 100 mA , or more, the larger matrix panels will use discretes or another technology).
These shortcomings may be modified with time, although it is doubtful if 500 mA to 1 A DMOS outputs are practical.

## Dielectric Isolation

Affording the highest breakdown voltage capability of present technologies is dielectric isolation. Since there is no collector-to-substrate PN junction, nor a collector-to-isolation wall PN junction, considerable improvement in collector-to-base and collector-to-emitter voltage is possible. Additionally, transistor sizes are considerably smaller than their PN-isolated counterparts. The dielectrically isolated devices offered by Dionics span a spectrum of approximately 100 volts to 280 volts (a-c plasma driver). DI affords the maximum breakdown voltage capability currently available.

Opposing this great advantage in breakdown voltage, however, is the increased process complexity of dielectrically isolated ICs. Definite improvements are needed in the area of process simplification, cost reduction, and alternate sources. Large-volume use of DI circuits will be restrained until these problems (particularly alternate sources) can be overcome. DI interface, with its potential for 300 V transistors, has a great promise if the barriers can be overcome.

## Packaging

Semiconductor design and process have greatly outstripped packaging currently in use, particularly in the area of power-handling capability. Greater concentration and resources are required to solve some of the following display interface related problems:

1. DIP power dissipation.
2. Greater number of leads (and smaller package sizes).
3. Improved plastic DIP resistance to moisture and corrosive environments.
4. Lower package manufacturing costs.
5. Smaller module or display subassemblies.

Power dissipation difficulties (strobed high currents) are most associated with LEDs. Use of very low duty-cycle and bright LEDs (particularly alphanumeric and matrix) dictates a need for multiplexing with peak currents as high as 3 A . Nothing currently on the market exceeds 1.75 A per output, and DIP ratings preclude d-c operation at such currents. However, many of the high-current applications are within the capability of standard bipolar ICs now offered.

For LSI ICs containing many I/O lines, the $24-, 28-$, and 40 -lead DIPs are standard. Since package size and cost increase together, it may be desirable to constrain many newer ICs to 18 -, 20-, or 22-lead DIPs (with $0.300^{\prime \prime}$ spacing, 22 also in use with $0.450^{\prime \prime}$ width). Printed wiring board real estate is increasingly dictating smaller size. Solutions such as the quad in-line (Rockwell) or less than $0.100^{\prime \prime}$ centers are possible. There are problems associated with a non-standard configuration (lack of sockets and higher prices) and the smaller physical size will not aid the quest for higher power (LEDs).

Improvements in plastic DIP moisture resistance and reliability are already underway; uses of tri-metal schemes (such as RCA's), silicon nitride or quartz passivation will continue to improve resistance to moisture and corrosive fumes. For display applications, these reliability improvements are of greatest concern in high-voltage devices.

Lower package costs are necessary to further increase the use of ICs in areas such as flat panel matrix displays. Currently, much of the cost of such a system is related to drive electronics, and much of the cost of the interface is the assembly cost of the DIPs (or hybrids). Increased use of automated assembly, film-carrier techniques and solder bumps will enhance the choice of ICs over discretes, and flat panel over CRT.

Also of concern is the possible mating of IC chips, solder-bump chips, or film-strip chips into the display assembly. Candidates for such a treatment would include d-c and a-c plasma, LEDs (already being done to a degree), DCEL, ACEL, LCD, and VF. Panel technologies using thick or thin-film techniques could benefit from such an approach. The biggest barrier to such an integrated assembly is the market data needed to justify tooling and lead time. It will only require one manufacturer willing to be a pioneer to further swing display technology into integrated systems. Prospects for purchasing a display complete with all drive electronics, such as a flat panel a-c plasma matrix (chips mounted via hybrid techniques on the rear of the glass envelope), are improving with time.

## Summary

A bright future exists for IC interface in display systems; the combination of logic (from MSI to small LSI) with suitable output buffers will further assist display designs. The following IC Technology-Display Interface matrix lists the key characteristics and primary display applications of various semiconductor technologies. Since many of these characteristics are changing, the table lists the device characteristics either now available or for the near future.

The most dynamic technologies for the immediate future appear to be BiMOS, $I^{2} L$, CMOS /DMOS, and, perhaps soon, DMOS. Sprague, Dionics, RCA, Texas Instruments, National Semiconductor, and others are using these device technologies to carve market niches where suitable. The dynamics of the IC market make for an uncertain future for any supplier of display circuitry unable or unwilling to continue the technological advancement necessary to meet the changing demands of the display market.

IC TECHNOLOGY - DISPLAY INTERFACE

| Technology | Breakdown V | Output 1 | Speed | LOGIC |  |  | Primary Display Suitability |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Supply |  |  |
|  |  |  |  | $\frac{\text { Complexity }}{(\max )}$ | Range | Power |  |
| Linear Process Bipolar | 10 to $\simeq 170 \mathrm{~V}$ | $<10 \mathrm{~mA}$ to 2 A | $<1 \mathrm{MHz}$ | MSI | 5 V | High | $\begin{aligned} & \text { LEDs, GD, VF, ACP, } \\ & \text { DCEL, EM } \end{aligned}$ |
| $I^{2} \mathrm{~L}$ | 20 to $\simeq 60 \mathrm{~V}$ | $<10 \mathrm{~mA}$ to 2 A | $3-6 \mathrm{MHz}$ | LSI | 5 V | Low-Modest | LED, VF, EM |
| BiMOS | 50 to $\simeq 150 \mathrm{~V}$ | $<10 \mathrm{MA}$ to 500 mA | 2-5 MHz | LSI | 5 to 15 V | Low | $\begin{aligned} & \text { LED, GD, VF, ACP, } \\ & \text { DCEL, EM } \end{aligned}$ |
| CMOS/DMOS | 60 to $\simeq 100 \mathrm{~V}$ | $\simeq 25 \mathrm{~mA}$ | 2-4 MHz | LSI | 12 V | Low | GD, VF, ACP, LCD |
| DI | $\simeq 200$ to $\simeq 300 \mathrm{~V}$ | $<10 \mathrm{~mA}$ to 100 mA (est) | 1 MHz (est) | MSI | 5 V | High | GD, VF, ACP, DCEL |

[^15]DCEL $=$ D-C Electroluminescent
$\mathrm{EM}=$ Electromagnetic

| GENERAL INFORMATION |  |
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## SELECTION GUIDE TO HIGH-CURRENT INTERFACE DRIVERS

| Device Type | Absolute Maximum Ratings |  | Outputs |
| :---: | :---: | :---: | :---: |
|  | $\mathrm{I}_{\text {OUT }}$ | $V_{\text {Out }}$ |  |
| UHP-400 through 433 | 500 mA | 40 V | Sink 4 |
| UHP-400 through 433-1 | 500 mA | 70 V | Sink 4 |
| UHP-500 through 533 | 500 mA | 100 V | Sink 4 |
| ULN-2001 through 2005A | 500 mA | 50 V | Sink 7 |
| ULN-2011 through 2015A | 600 mA | 50 V | Sink 7 |
| ULN-2021 through 2025A | 500 mA | 95 V | Sink 7 |
| ULN-2061M | 1.75 A | 50 V | Source/Sink 2 |
| ULN-2062M | 1.75 A | 80 V | Source/Sink 2 |
| ULN-2064/66/68/70B | 1.75 A | 50 V | Sink 4 |
| ULN-2065/67/69/71B | 1.75 A | 80 V | Sink 4 |
| ULN-2074/76B | 1.75 A | 50 V | Source/Sink 4 |
| ULN-2075/77B | 1.75 A | 80 V | Source/Sink 4 |
| UDN-2540B | 1.5 A | 60 V | Sink 4 |
| UDN-2580A | - 500 mA | 50 V | Source 8 |
| UDN-2580A-1 | - 500 mA | 80 V | Source 8 |
| UDN-2585A | -250 mA | 20 V | Source 8 |
| UDN-2588A | - 500 mA | 50 V | Source 8 |
| UDN-2588A-1 | - 500 mA | 80 V | Source 8 |
| UDN-2595A | 200 mA | 20 V | Sink 8 |
| ULN-2801 through 2805A | 500 mA | 50 V | Sink 8 |
| ULN-2811 through 2815A | 600 mA | 50 V | Sink 8 |
| ULN-2821 through 2825A | 500 mA | 95 V | Sink 8 |
| UDN-2841/42B | 1.75 A | $-50 \mathrm{~V}$ | Sink 4 |
| UDN-2843/44B | -1.75 A | -50 V | Source 4 |
| UDN-2845/46B | $\pm 1.75 \mathrm{~A}$ | -50 V | Source/Sink 4 |
| UTN-2886B | 800/1600 mA | 35 V | Sink 4/2 |
| UTN-2888A | 800 mA | 35 V | Sink 8 |
| UDN-2949Z | $\pm 2.0 \mathrm{~A}$ | 30 V | Half-Bridge |
| UDN-2952B | $\pm 1.0 \mathrm{~A}$ | 36 V | Full-Bridge |
| UDN-2952W | $\pm 2.0 \mathrm{~A}$ | 36 V | Full-Bridge |
| UDN-2956/57A | $-500 \mathrm{~mA}$ | -80 V | Source 5 |
| UDN-2981/82A | - 500 mA | 50 V | Source 8 |
| UDN-2983/84A | - 500 mA | 80 V | Source 8 |
| UDN-3611 through 3614M | 600 mA | 80 V | Sink 2 |
| UDN-5703 through 5707A | 600 mA | 80 V | Sink 4 |
| UDN-5711 through 5714M | 600 mA | 80 V | Sink 2 |
| UDN-5733A | 600 mA | 80 V | Sink 4 |

## SERIES UHP-400, UHP-400-1 and UHP-500 POWER and RELAY DRIVERS

## FEATURES

- Inputs Compatible with DTL/TTL
- 500 mA Output Sink Current Capability
- Pinning Compatible with 54/74 Logic Series
- Transient Protected Outputs on Relay Drivers
- High Voltage Output - 100 V Series UHP-500, 70 V Series

UHP-400-1, 40V Series UHP-400

## Description

These power and relay drivers are bi-polar monolithic circuits and incorporate logic gates and high-current switching transistors on the same chip. Each output transistor is capable of sinking 500 mA in the ON state. In the OFF state, Series UHP-400 devices will sustain 40V, Series UHP-400-1 devices will sustain 70V, and Series UHP-500 devices will sustain 100 V .

## Applications

The UHP-400, UḤP-400-1, and UHP-500 Series Power Drivers are ideally suited for driving incandescent lamps, relays, solenoids, and other interface devices with up to 1 A output current per package.

| $\begin{aligned} & \text { UHP-400/400-1/500 } \\ & \text { Quad } 2 \text { AND } \end{aligned}$ | UHP-402/402-1/502 Quad 2 OR | UHP-403/403-1/503 Quad OR | UHP-406/406-1/506 Quad AND |
| :---: | :---: | :---: | :---: |
| UHP-407/407-1/507 Quad NAND | UHP-408/408-1/508 Quad 2 NAND | UHP-432/432-1/532 Quad 2 NOR | UHP-433/433-1/533 Quad NOR |

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $V_{c c}$ ..... $7 V$
Input Voltage, $\mathrm{V}_{\text {in }}$ ..... 5.5VOutput Off-state Voltage, $\mathrm{V}_{\text {off }}$
40 V
Series UHP-400
70 V
Series UHP-400-1
100 V
Series UHP-500
500 mA
Output On-State Sink Current, I Ion
40 V
Suppression Diode Off-State Voltage, $\mathrm{V}_{\text {off }}$ Series UHP-400
70V
Series UHP-400-1
100 V
Series UHP-500
500 mA
Suppression Diode On-State Current, Ion .....
$-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ .....
$-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ..... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Free-Air Temperature Range, $\mathrm{T}_{\mathrm{A}}$
Operating Free-Air Temperature Range, $\mathrm{T}_{\mathrm{A}}$

## RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :--- | :--- | :--- | :--- | :---: |
| Supply Voltage (VCC) | 4.75 | 5.0 | 5.25 | V |
| Operating Temperature Range | 0 | +25 | $+85^{\circ}$ | ${ }^{\circ} \mathrm{C}$ |
| Current into any output (ON state) |  |  | 250 | mA |

Series UHP-14-pin plastic dual in-line; copper lead frame and epoxy encapsulation standard for high power handling capability.*
Thermal Resistance:



* $\phi_{i a}$ of $60^{\circ} \mathrm{C} / \mathrm{W}$ permits operation of four outputs continuously and simultaneously at 250 mA with a junction temperature which will not exceed $+150^{\circ} \mathrm{C}\left(\phi_{i}\right)$ at a $+85^{\circ} \mathrm{C}$ ambient.

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | VCC | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Input Voltage | $V_{\text {in }}(1)$ | MIN |  |  |  |  | 2.0 |  |  | V |  |
| " 0 " Input Voltage | $V_{\text {in }}(0)$ | MIN |  |  |  |  | 0.8 V |  |  |  |  |
| " 0 " Input Current at all Inputs except Strobe | Iin(0) | MAX |  | 0.4 V | 4.5 V |  | $-0.55$ |  | -0.8 | mA | 2 |
| "0" Input Current at Strobe | $\mathrm{I}_{\text {in }(0)}$ |  | MAX | 0.4 V | 4.5 V |  |  | -1.1 | -1.6 | mA |  |
| "1" Input Current at all Inputs | $\operatorname{lin}(1)$ |  | MAX | 2.4 V | OV |  |  |  | 40 | $\mu \mathrm{A}$ | 2 |
| except Strobe |  |  | MAX | 5.5V | OV |  |  |  | 1 | mA |  |
| "1" Input Current at Strobe | $\operatorname{lin}(1)$ |  | MAX | 2.4 V | OV |  |  |  | 100 | $\mu \mathrm{A}$ | 2 |
|  |  |  | MAX | 5.5V | OV |  |  |  | 1 | mA |  |

SWITCHING CHARACTERISTICS at $\mathrm{V}_{C C}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |  |
| Turn-on Delay Time | $\mathrm{t}_{\mathrm{pd} 0}$ | $\mathrm{V}_{\mathrm{S}}=40 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=265 \Omega$ (6 Watts) |  |  |  |  |  |
| Series UHP-400 |  | $\mathrm{V}_{\mathrm{S}}=70 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=465 \Omega$ (10 Watts) |  |  |  |  |  |
| Series UHP-400-1 |  | $V_{S}=100 \mathrm{~V}, R_{L}=670 \Omega$ (15 Watts) |  | 200 | 500 | ns | 3 |
| Series UHP-500 |  | $\mathrm{C}_{\mathrm{L}}=15 \mathrm{pF}$ |  |  |  |  |  |
| Turn-off Delay Time | $t_{\text {pdI }}$ | $\mathrm{V}_{\mathrm{S}}=40 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=265 \Omega$ (6 Watts) |  |  |  |  |  |
| Series UHP-400 |  | $V_{S}=70 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=465 \Omega$ (10 Watts) |  |  |  |  |  |
| Series UHP-400-1 |  | $\mathrm{V}_{\mathrm{S}}=100 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=670 \Omega$ (15 Watts) |  | 3.00 | 750 | ns | 3 |

NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each input tested separately.
3. Voltage values shown in the test circuit waveforms are with respect to network ground terminal.
4. Capacitance values specified include probe and test fixture capacitance.

INPUT PULSE CHARACTERISTICS

| $V_{\text {in }(0)}=0 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{f}}=7 \mathrm{~ns}$ | $\mathrm{t}_{\mathrm{p}}=1 \mu \mathrm{~S}$ |
| :--- | :--- | ---: |
| $V_{\text {in }(1)}=3.5 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{r}}=14 \mathrm{~ns}$ | PRR $=500 \mathrm{kHz}$ |

## Type UHP-400, UHP-400-1, and UHP-500

## Quad 2-Input AND Power Drivers



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. Typ. | Max. | Units |  |
| " 1 " Output Reverse Current Type UHP-400 | loff |  | MIN | 2.0 V | 2.0 V | 40 V |  | 50 | $\mu \mathrm{A}$ |  |
| "1" Output Reverse Current Type UHP-400-1 | Ioff |  | MIN | 2.0 V | 2.0 V | 70 V |  | 50 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current Type UHP-500 | loff |  | MIN | 2.0 V | 2.0 V | 100 V |  | 50 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | $V_{\text {on }}$ |  | MIN | 0.8 V | $\mathrm{V}_{\mathrm{cc}}$ | 150 mA |  | 0.5 | V | 12 |
|  |  |  | MIN | 0.8 V | $\mathrm{V}_{\mathrm{cc}}$ | 250 mA |  | 0.7 | V |  |
| "1" Level Supply Current | $\operatorname{ICC}(1)$ | NOM | MAX | 5.0 V | 5.0 V |  | 4 | 6 | mA |  |
| "0" Level Supply Current | $\operatorname{ICc}(0)$ | NOM | MAX | OV | OV |  | 17.5 | 24.5 | mA | 1,2 |

## NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each gate.
3. Capacitance values specified include probe and test fixture capacitance.


## Type UHP-402, UHP-402-1, and UHP-502

## Quad 2-Input OR Power Drivers



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {cc }}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| " 1 " Output Reverse Current Type UHP-402 | loff |  | MIN | 2.0 V | OV | 40 V |  |  | 50 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current Type UHP-402-1 | loff |  | MIN | 2.0 V | OV | 70 V |  |  | 50 | $\mu \mathrm{A}$ |  |
| "1" Output Reverse Current Type UHP-502 | loff |  | MIN | 2.0 V | OV | 100 V |  |  | 50 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 0.8 V | 0.8 V | 150 mA |  |  | 0.5 | V | 1,2 |
|  |  |  | MIN | 0.8 V | 0.8 V | 250 mA |  |  | 0.7 | V |  |
| "1" Level Supply Current | $\operatorname{Icc}(1)$ | NOM | MAX | 5.0V | 5.0V |  |  | 4.1 | 6.3 | mA |  |
| "0" Level Supply Current | $\operatorname{Icc}(0)$ | NOM | MAX | OV | OV |  |  | 18 | 25 | mA | 1,2 |

NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each gate.
3. Capacitance values specified include probe and test fixture capacitance.


## Type UHP-403, UHP-403-1, and UHP-503 Quad OR Relay Drivers



## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)



NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each gate.
3. Diode leakage current measured at $\mathrm{V}_{\mathrm{R}}=\mathrm{V}_{\text {off(min) }}$.
4. Diode forward voltage drop measured at $I_{f}=200 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.


## Type UHP-406, UHP-406-1, and UHP-506 Quad AND Relay Drivers



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {cc }}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| " 1 " Output Reverse Current Type UHP-406 | loff |  | MIN | 2.0 V | 2.0 V | 40 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current Type UHP-406-1 | Iotf |  | MIN | 2.0 V | 2.0 V | 70 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current <br> Type UHP-506 | loff |  | MIN | 2.0 V | 2.0 V | 100 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 0 " Output Voltage | Von |  | MIN | 0.8 V | VCC | 150 mA |  |  | 0.5 | V |  |
|  |  |  | MIN | 0.8 V | VCc | 250 mA |  |  | 0.7 | V |  |
| Diode Leakage Current | lıK | NOM | NOM | OV | OV | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | $V_{D}$ | NOM | NOM | VCC | VCc |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | ICC(1) | NOM | MAX | 5.0 V | 5.0V |  |  | 4 | 6 | mA | 1,2 |
| "0" Level Supply Current | Icc(0) | NOM | MAX | OV | OV |  |  | 17.5 | 24.5 | mA | 1,2 |

## NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each gate.
3. Diode leakage current measured at $\mathrm{V}_{\mathrm{R}}=\mathrm{V}_{\mathrm{off}(\mathrm{min})}$.
4. Diode forward voltage drop measured at $I_{f}=200 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.


# Type UHP-407, UHP-407-1, and UHP-507 Quad NAND Relay Drivers 



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vce | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| " 1 " Output Reverse Current Type UHP-407 | loff |  | MIN | 0.8 V | Vcc | 40 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "1" Output Reverse Current; Type UHP-407-1 | lofi |  | MIN | 0.8 V | Vcc | 70 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current Type UHP-507 | loft |  | MIN | 0.8 V | Vcc | 100 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | 2.0 V | 150 mA |  |  | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | 2.0 V | 250 mA |  |  | 0.7 | V |  |
| Diode Leakage Current | lik | NOM | NOM | V CC | $\mathrm{V}_{\mathrm{Cc}}$ | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 4 |
| Diode Forward Voltage Drop | V | NOM | NOM | OV | OV |  |  | 1.5 | 1.75 | $V$ | 5 |
| "1" Level Supply Current | ICC(1) | NOM | MAX | OV | OV |  |  | 6 | 7.5 | mA | 1,2 |
| " 0 " Level Supply Current | ICC(0) | NOM | MAX | 5 V | 5 V |  |  | 20 | 26.5 | mA | 1,2 |

## NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each gate.
3. Capacitance values specified include probe and test fixture capacitance.
4. Diode leakage current measured at $V_{R}=V_{\text {off(min) }}$.
5. Diode forward voltage drop measured at $I_{f}=200 \mathrm{~mA}$.


## Type UHP-408, UHP-408-1, and UHP-508 Quad 2-Input NAND Power Drivers



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | VCC | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| " 1 " Output Reverse Current Type UHP-408 | $\mathrm{l}_{\text {off }}$ |  | MIN | 0.8 V | VCC | 40 V |  |  | 50 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current Type UHP-408-1 | loff |  | MIN | 0.8 V | $V_{C C}$ | 70 V |  |  | 50 | $\mu \mathrm{A}$. |  |
| " 1 " Output Reverse Current Type UHP-508 | loff |  | MIN | 0.8 V | $V_{\text {cc }}$ | 100 V |  |  | 50 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | 2.0 V | 150 mA |  |  | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | 2.0 V | 250 mA |  |  | 0.7 | V |  |
| "1" Level Supply Current | $\mathrm{ICC}(1)$ | NOM | MAX | OV | OV |  |  | 6 | 7.5 | mA | 1,2 |
| "0" Level Supply Current | Icc(0) | NOM | MAX | 5.0 V | 5.0 V |  |  | 20 | 26.5 | mA | 1,2 | NOTES:

1. Typical values are at $\mathrm{V}_{C C}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each gate.
3. Capacitance values specified include probe and test fixture capacitance.
4. Diode leakage current measured at $V_{R}=V_{\text {off(min) }}$.
5. Diode forward voltage drop measured at $I_{f}=200 \mathrm{~mA}$.


## Type UHP-432, UHP-432-1, and UHP-532 <br> Quad 2-Input NOR Power Drivers



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| " 1 " Output Reverse Current Type UHP-432 | loff |  | MIN | 0.8 V | 0.8 V | 40 V |  |  | 50 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current Type UHP-432-1 | loff |  | MIN | 0.8 V | 0.8 V | 70 V |  |  | 50 | $\mu \mathrm{A}$ |  |
| "1" Output Reverse Current Type UHP-532 | loff |  | MIN | 0.8 V | 0.8 V | 100 V |  |  | 50 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | OV | 150 mA |  |  | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | OV | 250 mA |  |  | 0.7 | V |  |
| "0" Level Supply Current | ICC(0) | NOM | MAX | 5.0 V | 5.0 V |  |  | 20 | 25 | mA | 1,2 |
| "1" Level Supply Current | $\mathrm{ICC}(1)$ | NOM | MAX | OV | OV |  |  | 6 | 7.5 | mA | 1,2 |

NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each gate.
3. Diode leakage current measured at $V_{R}=V_{\text {off(min) }}$.
4. Diode forward voltage drop measured at $\mathrm{I}_{\mathrm{f}}=200 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.


DWG. No. A-7900A

## Type UHP-433, UHP-433-1, and UHP-533 Quad NOR Relay Drivers



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | $\begin{aligned} & \text { Other } \\ & \text { Input } \end{aligned}$ | Output | Min. | Typ. | Max. | Units |  |
| " 1 " Output Reverse Current Type UHP-433 | Ioff |  | MIN | 0.8 V | 0.8 V | 40 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current Type UHP-433-1 | loff |  | MIN | 0.8 V | 0.8 V | 70V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 1 " Output Reverse Current Type UHP-533 | loff |  | MIN | 0.8 V | 0.8 V | 100 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | OV | 150 mA |  |  | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | OV | 250 mA |  |  | 0.7 | V |  |
| Diode Leakage Current | ILK | NOM | NOM | V CC | VCC | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | $V_{D}$ | NOM | NOM | OV | OV |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | ICC(1) | NOM | MAX | OV | OV |  |  | 6 | 7.5 | mA | 1,2 |
| "0" Level Supply Current | $\mathrm{K} \mathrm{Cc}(0)$ | NOM | MAX | 5 V | 5 V |  |  | 20 | 25 | mA | 1,2 |

## NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each gate.
3. Diode leakage current measured at $V_{R}=V_{\text {off }}(m i n)$.
4. Diode forward voltage drop measured at $I_{f}=200 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.


## SERIES ULN-2000A HIGH-VOLTAGE, HIGH-CURRENT DARLINGTON TRANSISTOR ARRAYS

THESE high-voltage, high-current Darlington arrays are comprised of seven silicon NPN Darlington pairs on a common monolithic substrate. All units feature open collector outputs and integral diodes for inductive load transient suppression. Peak inrush currents to 600 mA (Series ULN-2000A and ULN-2020A) or 750 mA (Series ULN-2010A) are permissable, making them ideal for driving tungsten filament lamp loads.

The Series ULN-2001A devices are general purpose arrays which may be used with standard bipolar digital logic using external current limiting, or with most PMOS or CMOS directly. All are pinned with outputs opposite inputs to facilitate ease of circuit board layout and are priced to compete directly with discrete transistor alternatives.

The Series ULN-2002A was specifically designed for use with 14 to 25 V PMOS devices. Each input has a Zener diode and resistor in series to limit the input current to a safe value in that application. The Zener diode also means excellent noise immunity for these devices.

The Series ULN-2003A has a $2.7 \mathrm{k} \Omega$ series base resistor to each Darlington pair, and thus allows operation directly with TTL or CMOS operating at a supply voltage of 5 V . These devices will handle numerous interface needs - particularly those beyond the capabilities of standard logic buffers.

The Series ULN-2004A features a $10.5 \mathrm{k} \Omega$ series input resistor to permit their operation directly from CMOS or PMOS outputs utilizing supply voltages of 6 to 15 V . The required input current is below that of the Series ULN-2003A while the required input voltage is less than that required by the Series ULN-2002A.

The Series ULN-2005A is especially designed for use with standard and Schottky TTL where higher output currents are required and loading of the logic output is not a concern. These devices will sink a minimum of 350 mA when driven from a "totem

pole" logic output. Typical voltage and current levels for both the Series ULN-2003A and ULN2005A are shown in the graphs.

The Series ULN-2000A is the original high-voltage, high-current Darlington array. The output transistors are capable of sinking 500 mA and will sustain at least 50 V in the off state. Outputs may be paralleled for higher load current capability. The Series ULN-2010A devices are similar except that they will sink 600 mA . The Series ULN-2020A will sustain 95 V in the off state.

All Series ULN-2000A Darlington arrays are furnished in a 16 -pin dual in-line plastic package.

Device Type Number Designation

| $V_{\text {CEIMAX }}=$ <br> $I_{\text {C(MAX) }}=$ | 50 V <br> 500 mA | 50 V <br> 600 mA | 95 V <br> 500 mA |
| :---: | :---: | :---: | :---: |
|  | Type Number |  |  |
| General Purpose <br> PMOS, CMOS | ULN-2001A | ULN-2011A | ULN-2021A |
| $14-25 \mathrm{~V}$ <br> PMOS | ULN-2002A | ULN-2012A | ULN-2022A |
| 5 V <br> TTL, CMOS | ULN-2003A | ULN-2013A | ULN-2023A |
| 6-15 V <br> CMOS, PMOS | ULN-2004A | ULN-2014A | ULN-2024A |
| High Output <br> TTL | ULN-2005A | ULN-2015A | ULN-2025A |

## ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ Free-Air Temperature <br> for any one Darlington pair (unless otherwise noted)

Output Voltage, $\mathrm{V}_{\text {CE }}$ (Series ULN-2000, 2010A) ..... 50 V
(Series ULN-2020A) ..... 95 V
Input Voltage, $\mathrm{V}_{\text {IN }}$ (Series ULN-2002, 2003, 2004A) ..... 30 V
(Series ULN-2005A) ..... 15 V
Continuous Collector Current, IC (Series ULN-2000, 2020A) ..... 500 mA
(Series ULN-2010A) ..... 600 mA
Continuous Input Current, $\mathrm{I}_{\mathrm{I}}$ ..... 25 mA
Power Dissipation, $P_{D}$ (one Darlington pair) ..... 1.0 W
(total package) ..... 2.0 W*
Operating Ambient Temperature Range, $\mathrm{T}_{\mathrm{A}}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$$-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $16.67 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$.
Under normal operating conditions, these devices will sustain 350 mA per output with $V_{\text {CE(SAT) }}=1.6 \mathrm{~V}$ at $70^{\circ} \mathrm{C}$ with a pulse width of 20 ms and a duty cycle of $34 \%$.

## PARTIAL SCHEMATICS



DWi. no: A-9595
Series ULN-2001A (each driver)


DWG. No. A-9650

Series ULN-2002A
(each driver)


DWG. Ko. A-9651

Series ULN-2003A (each driver)


DwG. No. A-9898A

Series ULN-2004A
(each driver)


Series ULN-2005A
(each driver)

## SERIES ULN-2000A

ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {CEX }}$ | 1 A | All | $\mathrm{V}_{C E}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{C E}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 1B | ULN-2002A | $\mathrm{V}_{\mathrm{CE}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=6.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2004A | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=1.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CEISAT }}$ | 2 | All | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=250 \mu \mathrm{~A}$ | - | 0.9 | 1.1 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | - | 1.1 | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | - | 1.3 | 1.6 | V |
| Input Current | $\mathrm{I}_{\text {IN(ON) }}$ | 3 | ULN-2002A | $\mathrm{V}_{\mathrm{IN}}=17 \mathrm{~V}$ | - | 0.82 | 1.25 | mA |
|  |  |  | ULN-2003A | $\mathrm{V}_{\mathrm{IN}}=3.85 \mathrm{~V}$ | - | 0.93 | 1.35 | mA |
|  |  |  | ULN-2004A | $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$ | - | 0.35 | 0.5 | mA |
|  |  |  |  | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ | - | 1.0 | 1.45 | mA |
|  |  |  | ULN-2005A | $\mathrm{V}_{\text {IN }}=3.0 \mathrm{~V}$ | - | 1.5 | 2.4 | mA |
|  | $\mathrm{I}_{\text {IN(OFF) }}$ | 4 | All | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | 50 | 65 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {IN(ON }}$ | 5 | ULN-2002A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 13 | V |
|  |  |  | ULN-2003A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | - | 2.4 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | - | - | 2.7 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 3.0 | V |
|  |  |  | ULN-2004A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=125 \mathrm{~mA}$ | - | - | 5.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | - | 6.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | - | - | 7.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | - | - | 8.0 | V |
|  |  |  | ULN-2005A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | - | - | 2.4 | V |
| D-C Forward Current Transfer Ratio | $\mathrm{hfe}_{\text {fe }}$ | 2 | ULN-2001A | $\mathrm{V}_{C E}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 1000 | - | - |  |
| Input Capacitance | $\mathrm{C}_{\text {IN }}$ | - | All |  | - | 15 | 25 | pF |
| Turn-On Delay | $\mathrm{t}_{\text {PLH }}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PHL }}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Clamp Diode Leakage Current | $I_{R}$ | 6 | All | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | 7 | All | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 1.7 | 2.0 | V |

## SERIES ULN-2010A

## ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {CEX }}$ | 1A | All | $\mathrm{V}_{\mathrm{CE}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 1B | ULN-2012A | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=6.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2014A | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=1.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CEISAT }}$ | 2 | All | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | - | 1.1 | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | - | 1.3 | 1.6 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=600 \mu \mathrm{~A}$ | - | 1.7 | 1.9 | V |
| Input Current | $\mathrm{I}_{\text {INON }}$ | 3 | ULN-2012A | $\mathrm{V}_{\mathbb{I N}}=17 \mathrm{~V}$ | - | 0.82 | 1.25 | mA |
|  |  |  | ULN-2013A | $\mathrm{V}_{\text {IN }}=3.85 \mathrm{~V}$ | - | 0.93 | 1.35 | mA |
|  |  |  | ULN-2014A | $\mathrm{V}_{\mathbb{N}}=5.0 \mathrm{~V}$ | - | 0.35 | 0.5 | mA |
|  |  |  |  | $\mathrm{V}_{\mathbb{I N}}=12 \mathrm{~V}$ | - | 1.0 | 1.45 | mA |
|  |  |  | ULN-2015A | $\mathrm{V}_{\text {IN }}=3.0 \mathrm{~V}$ | - | 1.5 | 2.4 | mA |
|  | $\mathrm{I}_{\text {IN(OFF) }}$ | 4 | All | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | 50 | 65 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {IN(ON }}$ | 5 | ULN-2012A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | - | - | 17 | V |
|  |  |  | ULN-2013A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | - | - | 2.7 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 3.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | - | - | 3.5 | V |
|  |  |  | ULN-2014A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | - | - | 7.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | - | - | 8.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | - | - | 9.5 | V |
|  |  |  | ULN-2015A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | - | - | 2.6 | V |
| D-C Forward Current Transfer Ratio | $\mathrm{h}_{\text {FE }}$ | 2 | ULN-2011A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 1000 | - | - |  |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 900 | - | - |  |
| Input Capacitance | $\mathrm{C}_{1 \times}$ | - | All |  | - | 15 | 25 | pF |
| Turn-On Delay | $\mathrm{t}_{\text {PLH }}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PHL }}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Clamp Diode Leakage Current | $\mathrm{I}_{\mathrm{R}}$ | 6 | All | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode | $V_{F}$ | 7 | All | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 1.7 | 2.0 | V |
| Forward Voltage |  |  |  | $\mathrm{I}_{\mathrm{F}}=500 \mathrm{~mA}$ | - | 2.1 | 2.5 | V |

## SERIES ULN-2020A

ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | 1A | All | $\mathrm{V}_{\mathrm{CE}}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 1B | ULN-2022A | $\mathrm{V}_{\text {CE }}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IV }}=6.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2024A | $\mathrm{V}_{\mathrm{CE}}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=1.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CEISAT }}$ | 2 | All | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=250 \mu \mathrm{~A}$ | - | 0.9 | 1.1 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | - | 1.1 | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | - | 1.3 | 1.6 | V |
| Input Current | $1 \mathrm{I}_{\text {(ION) }}$ | 3 | ULN-2022A | $\mathrm{V}_{\mathbb{I N}}=17 \mathrm{~V}$ | - | 0.82 | 1.25 | mA |
|  |  |  | ULN-2023A | $\mathrm{V}_{\text {IV }}=3.85 \mathrm{~V}$ | - | 0.93 | 1.35 | mA |
|  |  |  | ULN-2024A | $\mathrm{V}_{1 \mathrm{~N}}=5.0 \mathrm{~V}$ | - | 0.35 | 0.5 | mA |
|  |  |  |  | $\mathrm{V}_{\text {IN }}=12 \mathrm{~V}$ | - | 1.0 | 1.45 | mA |
|  |  |  | ULN-2025A | $\mathrm{V}_{1 \mathbb{N}}=3.0 \mathrm{~V}$ | - | 1.5 | 2.4 | mA |
|  | $1{ }_{1 \text { IN(OFF) }}$ | 4 | All | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | 50 | 65 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {INION }}$ | 5 | ULN-2022A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 13 | V |
|  |  |  | ULN-2023A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | - | 2.4 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | - | - | 2.7 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 3.0 | V |
|  |  |  | ULN-2024A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=125 \mathrm{~mA}$ | - | - | 5.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | - | 6.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | - | - | 7.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=350 \mathrm{~mA}$ | - | - | 8.0 | V |
|  |  |  | ULN-2025A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | - | - | 2.4 | V |
| D-C Forward Current Transfer Ratio | $\mathrm{h}_{\mathrm{FE}}$ | 2 | ULN-2021A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 1000 | - | - |  |
| Input Capacitance | $\mathrm{C}_{\text {IN }}$ | - | All |  | - | 15 | 25 | pF |
| Turn-On Delay | $\mathrm{t}_{\mathrm{PLH}}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | $t_{\text {PHL }}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Clamp Diode | $\mathrm{I}_{\mathrm{R}}$ | 6 | All | $\mathrm{V}_{\mathrm{R}}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
| Leakage Current |  |  |  | $\mathrm{V}_{\mathrm{R}}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $\mathrm{V}_{\mathrm{F}}$ | 7 | All | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 1.7 | 2.0 | V |

## TEST FIGURES



FIGURE IA


FIGURE 2


FIGURE 4


FIGURE 6


FIGURE IB

FIGURE 3


FIGURE 5


FIGURE 7

COLLECTOR CURRENT
AS A FUNCTION OF SATURATION VOLTAGE


PEAK COLLECTOR CURRENT
AS A FUNCTION OF DUTY CYCLE


COLLECTOR CURRENT AS A FUNCTION OF INPUT CURRENT


ALLOWABLE AVERAGE POWER DISSIPATION AS A FUNCTION OF AMBIENT TEMPERATURE


DWG.NO. A-9753B

## INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE



Ow. No. A-9757A

SERIES ULN-2002A


SERIES ULN-2003A


SERIES ULN-2004A


SERIES ULN-2005A

## TYPICAL APPLICATIONS



PMOS TO LOAD


OUTPUT

TTL TO LOAD


USE OF PULL-UP RESISTORS
TO INCREASE DRIVE CURRENT

## TYPICAL PRINTER INTERFACE



## ULN-2061M through ULN-2077B 1.5 A DARLINGTON SWITCHES

## FEATURES

-TTL, DTL, PMOS, CMOS Compatible Inputs

- Transient Protected Outputs
- Handle Loads to 480 Watts
-Plastic Dual In-Line Packages
With Heat Sink Contact Tabs (Quad Arrays)

HIGH-VOLTAGE, HIGH-CURRENT Darlington Arrays ULN-2061M through ULN-2077B are designed to interface low-level logic to a variety of peripheral loads such as relays, solenoids, d-c and stepper motors, multiplexed LED and incandescent displays, heaters, and similar loads to 480 watts ( 1.5 A per output, $80 \mathrm{~V}, 26 \%$ duty cycle).
The devices are specified with a minimum output breakdown of 50 volts and $\mathrm{V}_{\mathrm{CE} \text { (SUS) }}$ minimum of 35 volts measured at 100 mA , or, a minimum output breakdown of 80 volts, $\mathrm{V}_{\text {CE(SUS) }}$ minimum of 50 volts; and an output current specification of 1.5 A (saturated).
Dual driver Type ULN-2061M and ULN-2062M arrays are used for common-emitter (externally connected), or emitter-follower applications. Both devices are supplied in miniature 8 -pin dual in-line plastic packages.

Quad driver Types ULN-2064B, ULN-2065B, ULN-2068B and ULN2069B are intended for use with TTL, low-speed TTL, and 5 V MOS logic. The ULN-2065B and ULN-2069B are selected for the 80 V minimum output breakdown specification. The ULN-2068B and ULN-2069B incorporate predriver stages and are most suitable for applications requiring high gain (low input current loading).
Types ULN-2066B, ULN-2067B, ULN-2070B and ULN-2071B are similar to the preceding quad drivers except that they are designed for use with PMOS and 12 V CMOS logic. The ULN-2070B and ULN-2071B both use a predriver stage and are best suited for use where current is restricted by MOS output ratings.

Isolated Darlington arrays Types ULN-2074B through ULN-2077B are identical to Types ULN-2064B through ULN-2067B except for the isolated Darlington pin-out and the deletion of suppression diodes. These switches are for emitter-follower or similar isolated Darlington applications.

All of the quad Darlington arrays (suffix "B" devices) are supplied in a 16-pin plastic dual in-line package with heat-sink contact tabs. A copperalloy lead frame provides maximum power dissipation using standard cooling methods. This lead configuration facilitates easy attachment of external heat sinks for increased power dissipation with standard IC sockets and printed wiring boards.


ULN-2061M ULN-2062M


## ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ Free-Air Temperature for any one driver (unless otherwise noted)



| Type Number | $\mathrm{V}_{\text {CEX(MAX) }}$ | $V_{\text {CES(SUSXMIN }}$ | $V_{\text {IN(MAX }}$ | Application |
| :---: | :---: | :---: | :---: | :---: |
| ULN-2061M | 50 V | 35 V | 30 V | TTL, DTL, Schottky TTL, |
| ULN-2062M | 80 V | 50 V | 60 V | and 5 V CMOS |
| ULN-2064B | 50 V | 35 V | 15 V | TTL, DTL, Schottky TTL |
| ULN-2065B | 80 V | 50 V | 15 V | and 5 V CMOS |
| ULN-2066B | 50 V | 35 V | 30 V | 6 to 15 V CMOS |
| ULN-2067B | 80 V | 50 V | 30 V | and PMOS |
| ULN-2068B | 50 V | 35 V | 15 V | TL, DTL, Schottky TLL, |
| ULN-2069B | 80 V | 50 V | 15 V | and 5 V CMOS |
| ULN-2070B | 50 V | 35 V | 30 V | 6 to 15 V CMOS |
| ULN-2071B | 80 V | 50 V | 30 V | and PMOS |
| ULN-2074B | 50 V | 35 V | 30 V | General Purpose |
| ULN-2075B | 80 V | 50 V | 60 V |  |
| ULN-2076B | 50 V | 35 V | 30 V | 6 to 15 V CMOS |
| ULN-2077B | 80 V | 50 V | 60 V | and PMOS |

[^16]
## ULN-2061M and ULN-2062M

## PARTIAL SCHEMATIC



ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Max. | Units |
| Output Leakage Current | $I_{\text {cex }}$ | 1 | ULN-2061M | $V_{C E}=50 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2062M | $V_{C E}=80 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {CES }}$ SUS) | 2 | ULN-2061M | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{IN}}=0.4 \mathrm{~V}$ | 35 | - | $V$ |
|  |  |  | ULN-2062M | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=0.4 \mathrm{~V}$ | 50 | - | V |
| Collector-Emitter Saturation Voltage | $V_{\text {CE(SAT }}$ | 3 | Both | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=625 \mu \mathrm{~A}$ | - | 1.1 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=935 \mu \mathrm{~A}$ | - | 1.2 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=1.25 \mathrm{~mA}$ | - | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}^{*}, I_{B}=2.0 \mathrm{~mA}$ | - | 1.4 | V |
|  |  |  | ULN-2062M | $\mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}^{*}, \mathrm{I}_{\mathrm{B}} 2.25 \mathrm{~mA}$ | - | 1.5 | V |
| Input Current | IIN(ON) | 4 | Both | $\mathrm{V}_{\text {IN }}=2.4 \mathrm{~V}$ | 1.4 | 4.3 | mA |
|  |  |  |  | $V_{\text {IN }}=3.75 \mathrm{~V}$ | 3.3 | 9.6 | mA |
| Input Voltage | $V_{\text {IN(ON })}$ | 5 | Both | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | - | 2.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=1.5 \mathrm{~A}$ | - | 2.5 | V |
| Turn-On Delay | ${ }_{\text {tplH }}$ | - | Both | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 1.0 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PHL }}$ | - | Both | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 1.5 | $\mu \mathrm{s}$ |
| Clamp Diode Leakage Current | $\mathrm{I}_{\mathrm{R}}$ | 6 | ULN-2061M | $V_{R}=50 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{A}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \bar{A}$ |
|  |  |  | ULN-2062M | $V_{R}=80 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}, \mathrm{~T}_{A}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | 7 | Both | $\mathrm{I}_{\mathrm{F}}=1.0 \mathrm{~A}$ | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{F}}=1.5 \mathrm{~A}$ | - | 2.0 | V |

[^17]
## ULN-2064B through ULN-2067B

## PARTIAL SCHEMATIC


(SIMILAR TO ULN-2074B through ULN-2077B)

## ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Max. | Units |
| Output Leakage Current | ICEX | 1 | ULN-2064/66B | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  |  | $V_{C E}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2065/67B | $V_{\text {CE }}=80 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $V_{\text {CE(SUS })}$ | 2 | ULN-2064/66B | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{1 \mathrm{~N}}=0.4 \mathrm{~V}$ | 35 | - | V |
|  |  |  | ULN-2065/67B | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=0.4 \mathrm{~V}$ | 50 | - | V |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CE(SAD }}$ | 3 | All | $\mathrm{I}_{C}=500 \mathrm{~mA}, I_{B}=625 \mu \mathrm{~A}$ | - | 1.1 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, I_{B}=935 \mu \mathrm{~A}$ | - | 1.2 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=1.25 \mathrm{~mA}$ | - | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.0 \mathrm{~mA}$ | - | 1.4 | V |
|  |  |  | ULN-2065/67B | $\mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.25 \mathrm{~mA}$ | - | 1.5 | V |
| Input Current | IIN(ON) | 4 | ULN-2064/65B | $\mathrm{V}_{\text {IN }}=2.4 \mathrm{~V}$ | 1.4 | 4.3 | mA |
|  |  |  |  | $V_{\text {IN }}=3.75 \mathrm{~V}$ | 3.3 | 9.6 | mA |
|  |  |  | ULN-2066/67B | $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$ | 0.6 | 1.8 | mA |
|  |  |  |  | $V_{\text {IN }}=12 \mathrm{~V}$ | 1.7 | 5.2 | mA |
| Input Voltage | $V_{\text {IN(ON }}$ | 5 | ULN-2064/65B | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | - | 2.0 | V |
|  |  |  |  | $V_{C E}=2.0 \mathrm{~V}, I_{C}=1.5 \mathrm{~A}$ | - | 2.5 | V |
|  |  |  | ULN-2066/67B | $V_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | - | 6.5 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}$ | - | 10 | V |
| Turn-On Delay | tPLH | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 1.0 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PHL }}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 1.5 | $\mu \mathrm{S}$ |
| Clamp Diode Leakage Current | $I_{R}$ | 6 | ULN-2064/66B | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $V_{R}=50 \mathrm{~V}, \mathrm{~T}_{A}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2065/67B | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}, \mathrm{~T}_{A}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | 7 | All | $\mathrm{I}_{\mathrm{F}}=1.0 \mathrm{~A}$ | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{F}}=1.5 \mathrm{~A}$ | - | 2.0 | V |

## ULN-2068B through ULN-2071B

## PARTIAL SCHEMATIC



DWG.NO. A-10,354B


ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)
$V_{S}=5.0 \mathrm{~V}$ (ULN-2068/69B) OR $\mathrm{V}_{\mathrm{S}}=12 \mathrm{~V}$ (ULN-2070/71B)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Max. | Units |
| Output Leakage Current | $I_{\text {cex }}$ | 1 | ULN-2068/70B | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 500 | $\mu$ A |
|  |  |  | ULN-2069/71B | $\mathrm{V}_{\text {CE }}=80 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $V_{\text {CESUS }}$ | 2 | ULN-2068/70B | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{IN}}=0.4 \mathrm{~V}$ | 35 | - | V |
|  |  |  | ULN-2069/71B | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=0.4 \mathrm{~V}$ | 50 | - | V |
| Collector-Emitter Saturation Voltage | $V_{\text {CE(SAT }}$ | 2 | ULN-2068/69B | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=2.75 \mathrm{~V}$ | - | 1.1 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=2.75 \mathrm{~V}$ | - | 1.2 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{~V}_{\text {IN }}=2.75 \mathrm{~V}$ | - | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{~V}_{\mathrm{IN}}=2.75 \mathrm{~V}$ | - | 1.4 | V |
|  |  |  | $\frac{\text { ULN-2069B }}{\text { ULN-2070/71B }}$ | $\mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}, \mathrm{~V}_{\text {IN }}=2.75 \mathrm{~V}$ | - | 1.5 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=5.0 \mathrm{~V}$ | - | 1.1 | V |
|  |  |  |  | $T_{C}=750 \mathrm{~mA}, V_{\text {IN }}=5.0 \mathrm{~V}$ | - | 1.2 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{~V}$ IN $=5.0 \mathrm{~V}$ | - | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{~V}_{\text {IN }}=5.0 \mathrm{~V}$ | - | 1.4 | V |
|  |  |  | ULN-2071B | $\mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}, \mathrm{~V}_{\text {IN }}=5.0 \mathrm{~V}$ | - | 1.5 | V |
| Input Current | IIN(ON) | 4 | ULN-2068/69B | $\mathrm{V}_{\text {IN }}=2.75 \mathrm{~V}$ | - | 550 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {IN }}=3.75 \mathrm{~V}$ | - | 1000 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2070/71B | $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$ | - | 400 | $\mu \mathrm{A}$ |
|  |  |  |  | $V_{\text {IN }}=12 \mathrm{~V}$ | - | 1250 | $\mu \mathrm{A}$ |
| Input Voltage | $V_{\text {INON }}(\mathrm{O})$ | 5 | ULN-2068/69B | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}$ | - | 2.75 | V |
|  |  |  | ULN-2070/71B | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}$ | - | 5.0 | V |
| Supply Current | Is | 8 | ULN-2068/69B | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=2.75 \mathrm{~V}$ | - | 6.0 | mA |
|  |  |  | ULN-2070/71B | $\mathrm{T}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=5.0 \mathrm{~V}$ | - | 4.5 | mA |
| Turn-On Delay | tpLH | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 1.0 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PHL }}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out, }}, 1 \mathrm{l}=1.25 \mathrm{~A}$ | - | 1.5 | $\mu \mathrm{s}$ |
| Clamp Diode Leakage Current | $I_{R}$ | 6 | ULN-2068/70B | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2069/71B | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | 7 | All | $\mathrm{I}_{\mathrm{F}}=1.0 \mathrm{~A}$ | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{F}}=1.5 \mathrm{~A}$ | - | 2.0 | V |

## ULN-2074B through ULN-2077B

## PARTIAL SCHEMATIC



$$
\begin{aligned}
& \left.\begin{array}{l}
\text { ULN-2074B } \\
\text { ULN-2075B }
\end{array}\right\} R_{I N}=350 \Omega \\
& \left.\begin{array}{l}
\text { ULN-2076B } \\
\text { ULN-2077B }
\end{array}\right\} R_{I N}=3 \mathrm{k} \Omega
\end{aligned}
$$

(SIMILAR TO ULN-2064B through ULN-2067B)


3

## ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Max. | Units |
| Output Leakage Current | $I_{\text {cex }}$ | 1 | ULN-2074/76B | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2075/77B | $V_{\text {CE }}=80 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {CE(SUS }}$ | 2 | ULN-2074/76B | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=0.4 \mathrm{~V}$ | 35 | - | V |
|  |  |  | ULN-2075/77B | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\text {IN }}=0.4 \mathrm{~V}$ | 50 | - | $V$ |
| Collector-Emitter Saturation Voltage | $V_{\text {CES (SA) }}$ | 3 | All | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=625 \mu \mathrm{~A}$ | - | 1.1 | $V$ |
|  |  |  |  | $I_{C}=750 \mathrm{~mA}, I_{B}=935 \mu \mathrm{~A}$ | - | 1.2 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=1.25 \mathrm{~mA}$ | - | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.0 \mathrm{~mA}$ | - | 1.4 | V |
|  |  |  | ULN-2075/77B | $\mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.25 \mathrm{~mA}$ | - | 1.5 | V |
| Input Current | İINON) | 4 | ULN-2074/75B | $\mathrm{V}_{\mathrm{IN}}=2.4 \mathrm{~V}$ | 1.4 | 4.3 | mA |
|  |  |  |  | $V_{\text {IN }}=3.75 \mathrm{~V}$ | 3.3 | 9.6 | mA |
|  |  |  | ULN-2076/77B | $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$ | 0.6 | 1.8 | mA |
|  |  |  |  | $V_{\text {IN }}=12 \mathrm{~V}$ | 1.7 | 5.2 | mA |
| Input Voltage | VIN(ON) | 5 | ULN-2074/75B | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | - | 2.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}$ | - | 2.5 | V |
|  |  |  | ULN-2076/77B | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | - | 6.5 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.5 \mathrm{~A}$ | - | 10 | V |
| Turn-On Delay | tpLH | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 1.0 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PHL }}$ | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 1.5 | $\mu \mathrm{S}$ |

## TEST FIGURES



Figure 1


Figure 2


Figure 3


Figure 6

Figure 5


Figure 7


Figure 8

## INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE AT $\mathbf{2 5}^{\circ} \mathrm{C}$





PEAK COLLECTOR CURRENT
AS A FUNCTION OF DUTY CYCLE





## TYPICAL APPLICATION



BIDIRECTIONAL MOTOR CONTROL
(The Series ULN-2000A, Series UDN-2980A, and the other devices in this series are recommended for use with multiple-winding stepping motors)

## PEAK COLLECTOR CURRENT

AS A FUNCTION OF DUTY CYCLE


## TYPICAL APPLICATIONS



COMMON-ANODE LED DRIVERS
(The Series UDN-2980A devices can also be used in similar applications for currents to $\mathbf{5 0 0} \mathbf{~ m A}$ )

(Types ULN-2068/70B are also applicable)

## UDN-2540B <br> QUAD NAND POWER DRIVER

## Replaced by UDN-2541B

DESIGNED for use in extremely harsh electrical environments, Type UDN-2540B quad NAND driver links low-level signal processing circuits and medium-power inductive loads.

The inputs are compatible with most TTL, DTL, LS TTL, 5 V to 15 V CMOS, and PMOS logic. The outputs include transient suppression diodes for inductive loads such as relays, solenoids, d-c and stepping motors. This device can also be used to drive incandescent or heater loads.


Dwg. No. A-11,561

## ABSOLUTE MAXIMUM RATINGS <br> at $25^{\circ} \mathrm{C}$ Free-Air Temperature

Output Voltage, $\mathrm{V}_{\text {our }}$ ..... 60 V
Output Sustaining Voltage, $\mathrm{V}_{\text {CESSUS }}$ ..... 35 V
Output Current, I Iout ..... 1.5 A
Logic Supply Voltage, V Cc ..... 18 V
Input Voltage, $\mathrm{V}_{\mathbb{I}}$ ..... 30 V
Power Dissipation, $P_{D}$ (each driver) ..... 2.5 W
(total package) ..... 2.77W*
Operating Temperature Range, $T_{A}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{S}$ ..... $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

[^18]
## RECOMMENDED OPERATING CONDITIONS

| Supply Voltage Range, $\mathrm{V}_{\text {cc }}$ | +10.5V to +17 V |
| :---: | :---: |
| Collector Current, It | < 500 mA |
| High-Level Input Voltage, $V_{\text {V(I) }}$ | $>2.0 \mathrm{~V}$ |
| Low-Level Input Voltage, $\mathrm{V}_{\mathbb{M}(1)}$ | $<0.4 \mathrm{~V}$ |
| Output Diode Reverse Voltage, Vs. | < 65 V |

ELECTRICAL CHARACTERISTICS at $\mathbf{V}_{\text {cc }}=10 \mathrm{~V}$ to 15 V , over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Max. | Units |
| "1" Output Reverse Current | $\mathrm{I}_{\text {OFF }}$ | $\mathrm{V}_{\text {OUT }}=50 \mathrm{~V}, \mathrm{~V}_{\mathbb{N}}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {EMabli }}=2.0 \mathrm{~V}$ | - | 500 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {OUT }}=50 \mathrm{~V}, \mathrm{~V}_{\text {W }}=2.0 \mathrm{~V}, \mathrm{~V}_{\text {EMable }}=0.4 \mathrm{~V}$ | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {cefisis) }}$ | $\mathrm{I}_{\text {Ouf }}=50 \mathrm{~mA}, \mathrm{~V}_{\text {W }}=\mathrm{V}_{\text {Emabie }}=0.4 \mathrm{~V}$ | 35 | - | V |
| "0" Output Voltage | $V_{\text {on }}$ | $\mathrm{I}_{\text {OUT }}=500 \mathrm{~mA}, \mathrm{~V}_{\mathbb{N}}=\mathrm{V}_{\text {EMMBIE }}=2.0 \mathrm{~V}$ | - | 1.1 | V |
|  |  | $\mathrm{I}_{\text {off }}=750 \mathrm{~mA}, \mathrm{~V}_{\text {W }}=\mathrm{V}_{\text {Emale }}=2.0 \mathrm{~V}$ | - | 1.25 | V |
|  |  | $\mathrm{I}_{\text {OUI }}=1.0 \mathrm{~A}, \mathrm{~V}_{\mathbb{W}}=\mathrm{V}_{\text {Eatale }}=2.0 \mathrm{~V}$ | - | 1.4 | V |
|  |  | $\mathrm{I}_{\text {OUT }}=1.25 \mathrm{~A}, \mathrm{~V}_{\mathbb{W}}=\mathrm{V}_{\text {EMable }}=2.0 \mathrm{~V}, \mathrm{~V}_{\text {CC }}=12 \mathrm{~V}$ | - | 1.6 | V |
| "1" Input Voltage | $V_{\text {W(1) }}$ |  | 2.0 | - | V |
| "0" Input Voltage | $V_{\text {M(0) }}$ |  | - | 0.5 | V |
| "1" Input Current | $\mathrm{I}_{\text {(1) }}$ | $\mathrm{V}_{\mathrm{N}}=15 \mathrm{~V}$ | - | 20 | $\mu \mathrm{A}$ |
| "0" Input Current | $\mathrm{I}_{\text {mio) }}$ | $V_{\text {W }}=0.4 \mathrm{~V}$ | - | -200 | $\mu \mathrm{A}$ |
| Input Clamp Voltage | $V_{1 k}$ | $\mathrm{I}_{\mathbb{N}}=-10 \mathrm{~mA}$ | - | -1.5 | V |
| Supply Current | $I_{\text {cc }}$ | $\mathrm{I}_{\text {OUT }}=500 \mathrm{~mA}, \mathrm{~V}_{\text {WV }}=\mathrm{V}_{\text {Exale }}=2.0 \mathrm{~V}, \mathrm{~V}_{\text {cC }}=15 \mathrm{~V}$ | - | 33 | mA |
|  |  | $V_{\text {OUT }}=50 \mathrm{~V}, \mathrm{~V}_{\text {IV }}=V_{\text {EMable }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {cC }}=15 \mathrm{~V}$ | - | 7.0 | ma |
| Clamp Diode Forward Voltage | $V_{F}$ | $\mathrm{I}_{\mathrm{F}}=1.0 \mathrm{~A}$ | - | 2.1 | V |
|  |  | $\mathrm{I}_{\mathrm{F}}=1.25 \mathrm{~A}$ | - | 2.5 | V |
| Clamp Diode Leakage Current | $I_{R}$ | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~V}_{\mathrm{W}}=\mathrm{V}_{\text {Exale }}=2.0 \mathrm{~V}, \mathrm{D}_{1}+\mathrm{D}_{2}$ or $\mathrm{D}_{3}+\mathrm{D}_{4}$ | - | 1.0 | mA |

# SERIES UDN-2580A 8-CHANNEL SOURCE DRIVERS 

## FEATURES

- TLL, CMOS, PMOS, NMOS Compatible
- High Output Current Ratings
- Internal Transient Suppression
- Efficient Input/Output Pin Structure

THIS versatile family of integrated circuits, originally designed to link NMOS logic with high-current inductive loads, will work with many combinations of logic- and load-voltage levels, meeting interface requirements beyond the capabilities of standard logic buffers.
Series UDN-2580A source drivers can drive incandescent, LED, or vacuum fluorescent displays. Internal transient-suppression diodes permit the drivers to be used with inductive loads.
Type UDN-2580A is a high-current source driver used to switch the ground ends of loads that are directly connected to a negative supply. Typical loads are telephone relays, PIN diodes, and LEDs.

Type UDN-2585A is a driver designed for applications requiring low output saturation voltages. Typical loads are low-voltage LEDs and incandescent displays. The eight non-Darlington outputs will simultaneously sustain continuous load currents of -120 mA at ambient temperatures to $+70^{\circ} \mathrm{C}$.
Type UDN-2588A, a high-current source driver similar to Type UDN-2580A, has separate logic and driver supply lines. Its eight drivers can serve as an interface between positive logic (TTL, CMOS, PMOS) or negative logic (NMOS) and either negative or split-load supplies.

Types UDN-2580A and UDN-2588A are rated for operation with output voltages of up to 50 V . Selected devices, carrying the suffix " -1 " on the Sprague part number, have maximum ratings of 80 V .

Types UDN-2580A and UDN-2585A are furnished in 18-pin dual in-line plastic packages; Type UDN-2588A is supplied in a 20 -pin dual in-line plastic package. All input connections are on one side of the packages, output pins on the other, to simplify printed wiring board layout.



UDN-2588A

Output Voltage, $\mathrm{V}_{\mathrm{CE}}$
Supply Voltage, $V_{S}$ (ref. sub.)
Supply Voltage, $\mathrm{V}_{\mathrm{cc}}$ (ref. sub.)
Input Voltage, $\mathrm{V}_{\mathbb{N}}$ (ref. $\mathrm{V}_{S}$ )
Total Current, $I_{C C}+I_{S}$
Substrate Current, $I_{\text {SUB }}$

## ABSOLUTE MAXIMUM RATINGS <br> at $25^{\circ} \mathrm{C}$ Free-Air Temperature <br> for Any One Driver <br> (unless otherwise noted)

Allowable Power Dissipation, $P_{D}$ (single output)
(total package) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 2.2 W*

Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $18 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$
For simplification, these devices are characterized on the following pages with specific voltages for inputs, logic supply ( $\mathrm{V}_{\mathrm{s}}$ ), load supply $\left(\mathrm{V}_{\mathrm{EE}}\right)$, and collector supply ( $\mathrm{V}_{\mathrm{CC}}$ ). Typical use of the UDN-2580A and UDN-2580A-1 is with negative referenced logic. The more common application of the UDN-2585A, UDN-2588A, and UDN-2588A-1 is with positive referenced logic supplies. In application, the devices are capable of operation over a wide range of logic and supply voltage levels:

TYPICAL OPERATING VOLTAGES

| $\mathrm{V}_{\text {s }}$ | $V_{\text {Mrow }}$ | $V_{\text {moff }}$ | $\mathrm{V}_{\text {cc }}$ | $V_{\text {EEmax }}$ | Device Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OV | -15 V to -3.6 V | -0.5 V to 0 V | NA | -25V | UDN-2585A |
|  |  |  |  | $-50 \mathrm{~V}$ | UDN-2580A |
|  |  |  |  | -80 V | UDN-2580A-1 |
| $+5 \mathrm{~V}$ | OV to +1.4V | +4.5 V to +5 V | NA | -20 V | UDN-2585A |
|  |  |  |  | -45V | UDN-2580A |
|  |  |  |  | -75V | UDN-2580A-1 |
|  |  |  | $\leq 5 \mathrm{~V}$ | -45 V | UDN-2588A |
|  |  |  |  | -75V | UDN-2588A-1 |
| +12 V | 0 V to +8.4 V | +11.5 V to +12. V | NA | -13V | UDN-2585A |
|  |  |  |  | -38V | UDN-2580A |
|  |  |  |  | -68V | UDN-2580A-1 |
|  |  |  | $\leq 12 \mathrm{~V}$ | -38 V | UDN-2588A |
|  |  |  |  | -68V | UDN-2588A-1 |
| +15V | OV to +11.4 V | +14.5V to +15V | NA | -10 V | UDN-2585A |
|  |  |  |  | -35 V | UDN-2580A |
|  |  |  |  | -65 V | UDN-2580A-1 |
|  |  |  | $\leq 15 \mathrm{~V}$ | -35 V | UDN2588A |
|  |  |  |  | -65 V | UDN-2588A-1 |

NOTE: The substrate must be tied to the most negative point in the external circuit to maintain isolation between drivers and to provide for normal circuit operation.

## UDN-2580A <br> UDN-2580A-1

## PARTIAL SCHEMATIC



DWG.NO. A-11,358


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$,
$V_{S}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-45 \mathrm{~V}$ (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | UDN-2580A | $\mathrm{V}_{\mathbb{N}}=-0.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-50 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\mathrm{N}}=-0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | UDN-2580A-1 | $\mathrm{V}_{\text {IV }}=-0.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-80 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=-0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {CEISUS }}$ | UDN-2580A | $\mathrm{V}_{\mathbb{N}}=-0.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$, Note 1 | 35 | - | V |
|  |  | UDN-2580A-1 | $\mathrm{V}_{\mathrm{W}}=-0.4 \mathrm{~V}, \mathrm{~V}_{\text {EE }}=-75 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$, Note 1 | 50 | - | V |
| Output Saturation Voltage | $\mathrm{V}_{\text {CESSAT }}$ | Both | $\mathrm{V}_{\mathrm{IN}}=-2.4 \mathrm{~V}, \mathrm{I}_{\text {OUI }}=-100 \mathrm{~mA}$ | - | 1.8 | $V$ |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=-3.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-225 \mathrm{~mA}$ | - | 1.9 | V |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=-3.6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | - | 2.0 | V |
| Input Current | $\mathrm{I}_{\text {(NON) }}$ | Both | $\mathrm{V}_{\text {IN }}=-3.6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | - | -500 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\mathrm{IV}}=-15 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | - | -2.1 | mA |
|  | $I_{\text {INOFF) }}$ | Both | $\mathrm{I}_{\text {OUT }}=-500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$, Note 3 | -50 | - | $\mu^{\prime \prime}{ }^{\text {A }}$ |
| Input Voltage | $\mathrm{V}_{\text {IN(ON }}$ | Both | $\mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}, \mathrm{~V}_{\text {CE }} \leq 1.8 \mathrm{~V}$, Note 4 | - | -2.4 | V |
|  |  |  | $\mathrm{I}_{\text {OUI }}=-225 \mathrm{~mA}, \mathrm{~V}_{\text {CE }} \leq 1.9 \mathrm{~V}$, Note 4 | - | -3.0 | V |
|  |  |  | $\mathrm{I}_{\text {Out }}=-350 \mathrm{~mA}, \mathrm{~V}_{\text {CE }} \leq 2.0 \mathrm{~V}$, Note 4 | - | -3.6 | V |
|  | $V_{\text {IV (VFF) }}$ | Both | $\mathrm{I}_{\text {OUT }}=-500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | -0.2 | - | V |
| Clamp Diode Leakage Current | $\mathrm{I}_{\mathrm{R}}$ | UDN-2580A | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  | UDN-2580A-1 | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $\overline{V_{F}}$ | Both | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 2.0 | $\stackrel{\text { V }}{ }$ |
| Input Capacitance | $\mathrm{C}_{\text {IV }}$ | Both |  | - | 25 | pF |
| Turn-On Delay | $t_{\text {PriL }}$ | Both | $0.5 \mathrm{E}_{\text {IN }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 5.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PLH }}$ | Both | $0.5 \mathrm{E}_{\text {IN }}$ to $0.5 \mathrm{E}_{\text {Out }}$ | - | 5.0 | $\mu \mathrm{s}$ |

NOTES: 1. Pulsed test, $t_{p} \leq 300 \mu \mathrm{~s}$, duty cycle $\leq 2 \%$.
2. Negative current is defined as coming out of the specified device pin.
3. The $I_{\text {INOFF }}$ current limit guarantees against partial turn-on of the output.
4. The $V_{\text {INON }}$ voltage limit guarantees a minimum oufput source current per the specified conditions.
5. The substrate must always be tied to the most negative point and must be at least 4.0 V below $\mathrm{V}_{\mathrm{s}}$.

## UDN-2585A

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$,
$\mathbf{V}_{\mathrm{S}}=\mathbf{O V}, \mathrm{V}_{\mathrm{EE}}=-20 \mathrm{~V}$ (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | $\mathrm{V}_{\mathbb{I V}}=-0.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-25 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\mathbb{N}}=-0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-25 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {ce(SUS) }}$ | $\mathrm{V}_{\mathbb{N}}=-0.4 \mathrm{~V}, \mathrm{I}_{\text {Out }}=-25 \mathrm{~mA}$, Note 1 | 15 | - | V |
| Output Saturation Voltage | $V_{\text {CEESAT }}$ | $\mathrm{V}_{\mathbb{N}}=-4.6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-60 \mathrm{~mA}$ | - | 1.1 | V |
|  |  | $\mathrm{V}_{\mathbb{W}}=-4.6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-120 \mathrm{~mA}$ | - | 1.2 | V |
| Input Current | $\mathrm{I}_{\text {Inow }}$ | $\mathrm{V}_{\text {IN }}=-4.6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-120 \mathrm{~mA}$ | - | -1.6 | mA |
|  |  | $\mathrm{V}_{\text {IN }}=-14.6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-120 \mathrm{~mA}$ | - | -5.0 | mA |
| Input Voltage | $V_{\text {INON }}$ | $\mathrm{I}_{\text {OUT }}=-120 \mathrm{~mA}, \mathrm{~V}_{\text {CE }} \leq 1.2 \mathrm{~V}$, Note 3 | - | -4.6 | V |
|  | $V_{\text {IV(OFF) }}$ | $\mathrm{I}_{\text {OUT }}=-100 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | -0.4 | - | V |
| Clamp Diode Leakage Current | $I_{R}$ | $\mathrm{V}_{\mathrm{R}}=25 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{\text {F }}$ | $\mathrm{I}_{\mathrm{F}}=120 \mathrm{~mA}$ | - | 2.0 | V |
| Input Capacitance | $\mathrm{C}_{\text {IN }}$ |  | - | 25 | pF |
| Turn-On Delay | $\mathrm{t}_{\text {PHL }}$ | $0.5 \mathrm{E}_{\text {IN }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 5.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PLH }}$ | $0.5 \mathrm{E}_{\text {IN }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 5.0 | $\mu \mathrm{S}$ |

NOTES: 1. Pulsed test, $\mathrm{t}_{\mathrm{p}} \leq 300 \mu \mathrm{~s}$, duty cycle $\leq 2 \%$.
2. Negative current is defined as coming out of the specified device pin.
3. The $V_{\text {inow }}$ voltage limit guarantees a minimum output source current per the specified conditions.
4. The substrate must always be tied to the most negative point and must be at least 4.0 V below $V_{s}$.

PARTIAL SCHEMATIC


DWG.NO. A-11,360


## UDN-2588A-1

PARTIAL SCHEMATIC


DwG.No. A-11, 361


DWG.NO. A-11, 357

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$,
$V_{S}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-40 \mathrm{~V}$ (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | UDN-2588A | $\mathrm{V}_{\text {IN }} \geq 4.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-45 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\text {IN }} \geq 4.6 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-45 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | UDN-2588A-1 | $\mathrm{V}_{\text {IN }} \geq 4.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-75 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\mathbb{N}} \geq 4.6 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {EE }}=-75 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {CEISUS }}$ | UDN-2588A | $\mathrm{V}_{\text {IN }} \geq 4.6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$, Note 1 | 35 | - | V |
|  |  | UDN-2588A-1 | $\mathrm{V}_{\mathbb{N}} \geq 4.6 \mathrm{~V}, \mathrm{~V}_{\text {EE }}=-70 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$, Note 1 | 50 | - | V |
| Output Saturation Voltage | $V_{\text {celsat }}$ | Both | $\mathrm{V}_{\mathbb{I}}=2.6 \mathrm{~V}, \mathrm{I}_{\text {out }}=-100 \mathrm{~mA}$, Ref. $\mathrm{V}_{\text {cc }}$ | - | 1.8 | V |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=2.0 \mathrm{~V}$, $\mathrm{I}_{\text {OUT }}=-225 \mathrm{~mA}$, Ref. $\mathrm{V}_{\text {cc }}$ | - | 1.9 | V |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=1.4 \mathrm{~V}, \mathrm{I}_{\text {out }}=-350 \mathrm{~mA}$, Ref. $\mathrm{V}_{\text {cc }}$ | - | 2.0 | V |
| Input Current | $\mathrm{I}_{\text {INON }}$ | Both | $\mathrm{V}_{\mathbb{N}}=1.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | - | -500 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\mathrm{S}}=15 \mathrm{~V}, \mathrm{~V}_{\text {EE }}=-30 \mathrm{~V}, \mathrm{~V}_{\text {IV }}=0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | - | -2.1 | mA |
|  | $\mathrm{I}_{\text {in(off }}$ | Both | $\mathrm{I}_{\text {Out }}=-500 \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$, Note 3 | -50 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {IVON }}$ | Both | $\mathrm{T}_{\text {OUT }}=-100 \mathrm{~mA}, \mathrm{~V}_{\text {CE }} \leq 1.8 \mathrm{~V}$, Note 4 | - | 2.6 | V |
|  |  |  | $\mathrm{I}_{\text {OUT }}=-225 \mathrm{~mA}, \mathrm{~V}_{\text {CE }} \leq 1.9 \mathrm{~V}$, Note 4 | - | 2.0 | V |
|  |  |  | $\mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}, \mathrm{~V}_{\text {CE }} \leq 2.0 \mathrm{~V}$, Note 4 | - | 1.4 | V |
|  | $V_{\text {IN(OFF }}$ | Both | $\mathrm{I}_{\text {Out }}=-500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | 4.8 | - | V |
| Clamp Diode Leakage Current | $I_{R}$ | UDN-2588A | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  | UDN-2588A-1 | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{\text {F }}$ | Both | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 2.0 | V |
| Input Capacitance | $\mathrm{C}_{\text {IN }}$ | Both |  | - | 25 | pF |
| Turn-On Delay | $\mathrm{t}_{\text {PHL }}$ | Both | $0.5 \mathrm{E}_{\text {IN }}$ to $0.5 \mathrm{E}_{\text {Out }}$ | - | 5.0 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {PLH }}$ | Both | $0.5 \mathrm{E}_{\text {IN }}$ to $0.5 \mathrm{E}_{\text {OUT }}$ | - | 5.0 | $\mu \mathrm{s}$ |

NOTES: 1. Pulsed test, $\mathrm{t}_{\mathrm{p}} \leq 300 \mu \mathrm{~s}$, duty cycle $\leq 2 \%$.
2. Negative current is defined as coming out of the specified device pin.
3. The $I_{\text {INoff }}$ current limit guarantees against partial turn-on of the output.
4. The $V_{\mathbb{N ( O N})}$ voltage limit guarantees a minimum output source current per the specified conditions.
5. The substrate must always be tied to the most negative point and must be at least 4.0 V below $\mathrm{V}_{\mathrm{s}}$.
6. $V_{C C}$ must never be more positive than $V_{S}$.


Allowable peak collector current AT $7 \mathbf{7 0}^{\circ} \mathrm{C}$ AS A FUNCTION OF DUTY CYCLE


## TYPICAL APPLICATIONS



COMMON-CATHODE LED DRIVER


TELECOMMUNICATIONS
RELAY DRIVER
(Negative Logic)


TELECOMMUNICATIONS RELAY DRIVER
(Positive Logic)


OWG.NO. A-11,363

VACUUM FLUORESCENT DISPLAY DRIVER
(Split Supply)

## UDN-2595A 8-CHANNEL CURRENT-SINK DRIVER

## FEATURES

- 200 mA Current Rating
- Low Saturation Voltage
- TLL, CMOS, NMOS Compatible
- Efficient Input/Output Pin Format
- 18-Pin Dual In-Line Plastic Package

DEVELOPED for use with low-voltage LED and incandescent displays requiring low output saturation voltage, Type UDN-2595A meets many other interface needs, including those exceeding the capabilities of standard logic buffers.

The eight non-Darlington outputs of this driver can simultaneously sink load currents of 200 mA at ambient temperatures of up to $+85^{\circ} \mathrm{C}$.

The eight-channel driver's active low inputs can be linked directly to TTL, Schottky TTL, DTL, 5 to 16 V CMOS, and NMOS logic. All input connections are on one side of the package, output connections on the other, for simplified layout of printed wiring boards.

Type UDN-2595A is supplied in an 18-pin dual-in-line plastic package with a copper lead frame that maximizes the driver's power-handling capabilities. A hermetically sealed version of Type UDN-2595A, with reduced package power dissipation ratings, is available on special order.

This device complements Sprague Type UDN2585 A , an eight-channel source driver.


## ABSOLUTE MAXIMUM RATINGS

 at $25^{\circ} \mathrm{C}$ Free-Air Temperature for any one driver (unless otherwise noted)Output Voltage, $\mathrm{V}_{\mathrm{CE}}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20 V
Supply Voltage, $\mathrm{V}_{5}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20 V
Input Voltage, $\mathrm{V}_{\mathbb{N}}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20 V
Output Collector Current, $I_{C}$. . . . . . . . . . . . . . . . . . . 200 mA
Ground Terminal Current, $\mathrm{I}_{\text {GND }}$. . . . . . . . . . . . . . . . . . . . . 1.6 A
Allowable Power Dissipation, $P_{0}$
(single output) . . . . . . . . . . . . . . . . . . . . . . . . 1.0 W
(total package) . . . . . . . . . . . . . . . . . . . . . . . . . 2.2 W*
Operating Temperature Range, $T_{A} \ldots \ldots .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . . .-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $18 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+25^{\circ} \mathrm{C}$.

ELECTRICAL CHARACTERISTICS at $T_{A}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}=5.0 \mathrm{~V}$ (unless otherwise noted).

| Characteristic | Symbol | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | $\mathrm{V}_{\mathbb{N}} \geq 4.5 \mathrm{~V}, \mathrm{~V}_{\text {out }}=20 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {IN }} \geq 4.6 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=20 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
| Output Saturation Voltage | $V_{\text {CEESAT }}$ | $\mathrm{V}_{\text {is }}=0.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=50 \mathrm{~mA}$ | - | 0.5 | V |
|  |  | $\mathrm{V}_{\text {IV }}=0.4 \mathrm{~V}, \mathrm{I}_{\text {out }}=100 \mathrm{~mA}$ | - | 0.6 | V |
| Tnput Current | INON) | $\mathrm{V}_{\text {IV }}=0.4 \mathrm{~V}, \mathrm{I}_{\text {out }}=100 \mathrm{~mA}$ | - | -1.6 | mA |
|  |  | $\mathrm{V}_{\mathbb{N}}=0.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{S}}=15 \mathrm{~V}$ | - | -5.0 | mA |
| Input Voltage |  | $\mathrm{I}_{\text {OUT }}=100 \mathrm{~mA}, \mathrm{~V}_{\text {out }} \leq 0.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}=5 \mathrm{~V}$ | - | 0.4 | V |
|  | $V_{\text {(V)OFF) }}$ | $\mathrm{I}_{\text {OUT }}=100 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | 4.6 | - | V |
| Input Capacitance | $\mathrm{C}_{\text {N }}$ |  | - | 25 | pF |
| Supply Current | $\mathrm{l}_{\text {ss }}$ | $\mathrm{V}_{\text {IV }}=0.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=100 \mathrm{~mA}$ | - | 6.0 | mA |
|  |  | $\mathrm{V}_{\text {IV }}=0.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=100 \mathrm{~mA}, \mathrm{~V}_{\text {S }}=15 \mathrm{~V}$ | - | 20 | mA |

## NOTES:

1. Negative current is defined as coming out of the specified device pin.
2. The $V_{\mathbb{N}(O N)}$ voltage limit guarantees a minimum output sink current per the specified conditions.
3. $I_{S S}$ is measured with any one of eight drivers turned $O N$.


# SERIES ULN-2800A HIGH-VOLTAGE, HIGH-CURRENT DARLINGTON TRANSISTOR ARRAYS 

$I^{\mathrm{D}}$DEALLY SUITED for interfacing between lowlevel digital logic circuitry and high-power peripheral loads, the Series ULN-2800A high-voltage, highcurrent Darlington transistor arrays feature peak load current ratings of 600 mA (Series ULN-2800A and ULN-2820A) or 750 mA (Series ULN-2810A) for each of the eight drivers in each device. Under the proper conditions, high-power loads of up to 4 A at 50 V ( 200 W at $23 \%$ duty cycle) or 3.2 A at 95 V ( 304 W at $33 \%$ duty cycle) can be controlled. Typical loads include relays, solenoids, stepping motors, multiplexed LED and incandescent displays, and heaters. All devices feature open collector outputs and integral diodes for inductive load transient suppression.

The Series ULN-2801A devices are general purpose arrays which may be used with standard bipolar digital logic using external current limiting, or with most PMOS or CMOS directly. All are pinned with outputs opposite inputs to facilitate ease of circuit board layout and are priced to compete directly with discrete transistor alternatives.

The Series ULN-2802A was specifically designed for use with 14 to 25 V PMOS devices. Each input has a Zener diode and resistor in series to limit the input current to a safe value in that application. The Zener diode also means excellent noise immunity for these devices.

The Series ULN-2803A has a $2.7 \mathrm{k} \Omega$ series base resistor to each Darlington pair, and thus allows operation directly with TTL or CMOS operating at a supply voltage of 5 V . These devices will handle numerous interface needs - particularly those beyond the capabilities of standard logic buffers.

The Series ULN-2804A features a $10.5 \mathrm{k} \Omega$ series input resistor to permit their operation directly from CMOS or PMOS outputs utilizing supply voltages of 6 to 15 V . The required input current is below that of the Series ULN-2803A while the required input voltage is less than that required by the Series ULN-2802A.

The Series ULN-2805A is especially designed for use with standard and Schottky TTL where higher output currents are required and loading of the logic

output is not a concern. These devices will sink a minimum of 350 mA when driven from a "totem pole" logic output.

The Series ULN-2800A is the standard highvoltage, high-current Darlington array. The output transistors are capable of sinking 500 mA and will withstand at least 50 V in the OFF state. Outputs may be paralleled for higher load current capability. The Series ULN-2810A devices are similar except that they will sink 600 mA . The Series ULN-2820A will withstand 95 V in the OFF state.

All Series ULN-2800A Darlington arrays are furnished in an 18-pin dual in-line plastic package.

Device Type Number Designation

| $\begin{aligned} V_{C E(M A X)} & = \\ I_{C(M A X)} & = \end{aligned}$ | $\begin{gathered} 50 \mathrm{~V} \\ 500 \mathrm{~mA} \end{gathered}$ | $\begin{gathered} 50 \mathrm{~V} \\ 600 \mathrm{~mA} \end{gathered}$ | $\begin{gathered} 95 \mathrm{~V} \\ 500 \mathrm{~mA} \end{gathered}$ |
| :---: | :---: | :---: | :---: |
|  | Type Number |  |  |
| General Purpose PMOS, CMOS | ULN-2801A | ULN-2811A | ULN-2821A |
| $\begin{gathered} 14-25 \mathrm{~V} \\ \text { PMOS } \end{gathered}$ | ULN-2802A | ULN-2812A | ULN-2822A |
| $\begin{gathered} 5 \mathrm{~V} \\ \mathrm{TTL}, \mathrm{CMOS} \end{gathered}$ | ULN-2803A | ULN-2813A | ULN-2823A |
| $\begin{gathered} 6-15 \mathrm{~V} \\ \text { CMOS, PMOS } \end{gathered}$ | ULN-2804A | ULN-2814A | ULN-2824A |
| $\begin{aligned} & \text { High Output } \\ & \text { TTL } \end{aligned}$ | ULN-2805A | ULN-2815A | ULN-2825A. |

## ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ Free-Air Temperature for any one Darlington pair (unless otherwise noted)

| Output Voltage, V CE $^{\text {(Series ULN-2800, 2810A) }}$ | 50 V |
| :---: | :---: |
| (Series ULN-2820A) | 95 V |
| Input Voltage, $\mathrm{V}_{\text {IN }}$ (Series ULN-2802, 2803, 2804A) | 30 V |
| (Series ULN-2805A) | 15 V |
| Continuous Collector Current, $\mathrm{I}_{C}$ (Series ULN-2800, 2820A) | . 500 mA |
| (Series ULN-2810A) | .600 mA |
| Continuous Base Current, $I_{B}$ | 25 mA |
| Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ (one Darlington pair) | 1.0 W |
| (total package). | 2.25 W* |
| Operating Ambient Temperature Range, $\mathrm{T}_{\mathrm{A}}$ | $+85^{\circ} \mathrm{C}$ |
| Storage Temperature Range, $\mathrm{T}_{\mathbf{s}}$ | $+150^{\circ} \mathrm{C}$ |

*Derate at the rate of $18.18 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$.
Under normal operating conditions, these devices will sustain 350 mA per output with $\mathrm{V}_{\text {CESAA }}=1.6 \mathrm{~V}$ at $50^{\circ} \mathrm{C}$ with a pulse width of 20 ms and a duty cycle of $40 \%$.

## PARTIAL SCHEMATICS


owi. no. A-9595
Series ULN-2801A
(each driver)


OWG. No. A-9650

## Series ULN-2802A <br> (each driver)



DwG. No. A-965I

Series ULN-2803A
(each driver)


DWG. NO. A-9898 A:

Series ULN-2804A
(each driver)


Series ULN-2805A
(each driver)

## SERIES ULN-2800A

ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | 1 A | All | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 18 | ULN-2802A | $V_{C E}=50 \mathrm{~V}, T_{A}=70^{\circ} \mathrm{C}, V_{\text {IN }}=6.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2804A | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IV }}=1.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CESSAT }}$ | 2 | All | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=250 \mu \mathrm{~A}$ | - | 0.9 | 1.1 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | - | 1.1 | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | - | 1.3 | 1.6 | V |
| Input Current | $\mathrm{I}_{\text {INON }}$ | 3 | ULN-2802A | $\mathrm{V}_{\mathrm{IN}}=17 \mathrm{~V}$ | - | 0.82 | 1.25 | mA |
|  |  |  | ULN-2803A | $\mathrm{V}_{\text {IN }}=3.85 \mathrm{~V}$ | - | 0.93 | 1.35 | mA |
|  |  |  | ULN-2804A | $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$ | - | 0.35 | 0.5 | mA |
|  |  |  |  | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ | - | 1.0 | 1.45 | mA |
|  |  |  | ULN-2805A | $\mathrm{V}_{1 \mathrm{~V}}=3.0 \mathrm{~V}$ | - | 1.5 | 2.4 | mA |
|  | 1 Inioff | 4 | All | $\mathrm{I}_{\mathrm{C}}=500 \mu{\mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}}$ | 50 | 65 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {INON }}$ | 5 | ULN-2802A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 13 | V |
|  |  |  | ULN-2803A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | - | 2.4 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | - | - | 2.7 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 3.0 | V |
|  |  |  | ULN-2804A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=125 \mathrm{~mA}$ | - | - | 5.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | - | 6.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | - | - | 7.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=350 \mathrm{~mA}$ | - | - | 8.0 | V |
|  |  |  | ULN-2805A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | - | - | 2.4 | V |
| D-C Forward Current Transfer Ratio | $\mathrm{h}_{\mathrm{FE}}$ | 2 | ULN-2801A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 1000 | - | - |  |
| Input Capacitance | $\mathrm{C}_{\text {IN }}$ | - | All |  | - | 15 | 25 | pF |
| Turn-On Delay | ton | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | toff | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Clamp Diode Leakage Current | $\mathrm{I}_{\mathrm{R}}$ | 6 | All | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $\mathrm{V}_{\mathrm{F}}$ | 7 | All | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 1.7 | 2.0 | V |

[^19]
## SERIES ULN-2810A

## ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $I_{\text {cex }}$ | 1A | All | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 1B | ULN-2812A | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=6.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2814A | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=1.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CEISAT) }}$ | 2 | All | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | - | 1.1 | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | - | 1.3 | 1.6 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=600 \mu \mathrm{~A}$ | - | 1.7 | 1.9 | V |
| Input Current | $\mathrm{I}_{\text {IN(ON }}$ | 3 | ULN-2812A | $\mathrm{V}_{\text {IN }}=17 \mathrm{~V}$ | - | 0.82 | 1.25 | mA |
|  |  |  | ULN-2813A | $\mathrm{V}_{\mathbb{I}}=3.85 \mathrm{~V}$ | - | 0.93 | 1.35 | mA |
|  |  |  | ULN-2814A | $\mathrm{V}_{\mathbb{I N}}=5.0 \mathrm{~V}$ | - | 0.35 | 0.5 | mA |
|  |  |  |  | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ | - | 1.0 | 1.45 | mA |
|  |  |  | ULN-2815A | $\mathrm{V}_{\mathrm{N}}=3.0 \mathrm{~V}$ | - | 1.5 | 2.4 | mA |
|  | $\mathrm{I}_{\text {IN(OFF) }}$ | 4 | All | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | 50 | 65 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {IN(ON) }}$ | 5 | ULN-2812A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | - | - | 17 | V |
|  |  |  | ULN-2813A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | - | - | 2.7 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 3.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | - | - | 3.5 | V |
|  |  |  | ULN-2814A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | - | - | 7.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | - | - | 8.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | - | - | 9.5 | V |
|  |  |  | ULN-2815A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | - | - | 2.6 | V |
| D-C Forward Current Transfer Ratio | $\mathrm{h}_{\mathrm{FE}}$ | 2 | ULN-2811A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 1000 | - | - |  |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 900 | - | - |  |
| Input Capacitance | $\mathrm{Clin}^{\text {IN }}$ | - | All |  | - | 15 | 25 | pF |
| Turn-On Delay | ton | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | toff | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Clamp Diode Leakage Current | $I_{R}$ | 6 | All | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode | $V_{F}$ | 7 | All | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 1.7 | 2.0 | V |
| Forward Voltage |  |  |  | $\mathrm{I}_{F}=500 \mathrm{~mA}$ |  | 2.1 | 2.5 | V |

Series ULN-2800A and ULN-2810A devices are also available (with reduced package power capability) in industrial-grade hermetic packages. To order, change the last letter of the part number from ' $A$ ' to ' $R$ '. Note that the high-voltage devices ( $B V_{C E} \geq 95 \mathrm{~V}$ ) are not presently available with this packaging option.

## SERIES ULN-2820A

ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ (unless otherwise noted)

| Characteristic | Symbol | Test Fig. | Applicable Devices | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $I_{\text {cex }}$ | 1 A | All | $V_{C E}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{C E}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 1B | ULN-2822A | $\mathrm{V}_{\text {CE }}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=6.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
|  |  |  | ULN-2824A | $\mathrm{V}_{\text {CE }}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=1.0 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $V_{\text {CEISAT }}$ | 2 | All | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=250 \mu \mathrm{~A}$ | - | 0.9 | 1.1 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | - | 1.1 | 1.3 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | - | 1.3 | 1.6 | V |
| Input Current | IIN(ON) | 3 | ULN-2822A | $\mathrm{V}_{\mathrm{IN}}=17 \mathrm{~V}$ | - | 0.82 | 1.25 | mA |
|  |  |  | ULN-2823A | $\mathrm{V}_{\text {IN }}=3.85 \mathrm{~V}$ | -- | 0.93 | 1.35 | mA |
|  |  |  | ULN-2824A | $\mathrm{V}_{\mathbb{N}}=5.0 \mathrm{~V}$ | - | 0.35 | 0.5 | mA |
|  |  |  |  | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ | - | 1.0 | 1.45 | mA |
|  |  |  | ULN-2825A | $\mathrm{V}_{\mathbb{I N}}=3.0 \mathrm{~V}$ | - | 1.5 | 2.4 | mA |
|  | $\mathrm{I}_{\text {IN(OFF) }}$ | 4 | All | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | 50 | 65 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {IN(ON }}$ | 5 | ULN-2822A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 13 | V |
|  |  |  | ULN-2823A | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | - | 2.4 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | - | - | 2.7 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | - | - | 3.0 | V |
|  |  |  | ULN-2824A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=125 \mathrm{~mA}$ | - | - | 5.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | - | 6.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | - | - | 7.0 | $V$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | - | - | 8.0 | V |
|  |  |  | ULN-2825A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | - | - | 2.4 | V |
| D-C Forward Current Transfer Ratio | $\mathrm{h}_{\mathrm{FE}}$ | 2 | ULN-2821A | $\mathrm{V}_{\mathrm{CE}}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 1000 | - | - |  |
| Input Capacitance | $\mathrm{C}_{\text {IN }}$ | - | All |  | - | 15 | 25 | pF |
| Turn-On Delay | ton | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | toff | - | All | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 0.25 | 1.0 | $\mu \mathrm{S}$ |
| Clamp DiodeLeakage Current | $I_{\text {R }}$ | 6 | All | $V_{R}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{R}}=95 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$. | - | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | 7 | All | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 1.7 | 2.0 | V |

## TEST FIGURES



FIGURE 1A


FIGURE 2


FIGURE 4


FIGURE 6


FIGURE IB


FIGURE 3


FIGURE 5


FIGURE 7

COLLECTOR CURRENT
AS A FUNCTION OF SATURATION VOLTAGE


COLLECTOR CURRENT
AS A FUNCTION OF INPUT CURRENT


ALLOWABLE AVERAGE POWER DISSIPATION AS A FUNCTION OF AMBIENT TEMPERATURE


PEAK COLLECTOR CURRENT AS A FUNCTION OF DUTY CYCLE




DW. No. A-9757A


SERIES ULN-2804A


SERIES ULN-2805A


OFF VOLTAGE BIAS FOR HIGH-VOLTAGE LOADS


TTL TO LOAD


BUFFER FOR HIGHER CURRENT LOADS

USE OF PULL-UP RESISTORS TO INCREASE DRIVE CURRENT

## TYPICAL DISPLAY INTERFACE



## TYPE UDN-284 1B through UDN-2846B* QUAD 1.5 AMPERE DRIVERS

## FEATURES

- Inputs Compatible with DTL/TTL/LS TTL/CMOS/PMOS
- High Voltage Output: -50 V
- High Current Gain
- Sink from Negative Supply: UDN-2841B and UDN-2842B
- Source to Negative Supply: UDN-2843B and UDN-2844B
- Sink \& Source Combination: UDN-2845B and UDN-2846B

THIS SERIES of quad Darlington switches is especially designed for high-current, high-voltage peripheral driver applications. It is intended to provide solutions to interface problems involving electronic discharge printers, d-c motor drive (bipolar or unipolar), telephone relays, PIN diodes, LEDs, and other high-current loads operating from negative supplies.

Types UDN-2841B and UDN-2842B are intended for sinking applications in which the load is connected to ground and the IC output switches the negative supply. The input PNP transistor in each driver serves as a level translator and the first NPN stage provides sufficient current gain to drive the output Darlingtons.

Type UDN-2843B and UDN-2844B quad drivers are primarily intended for switching the ground end of loads which utilize negative supply voltages. The NPN Darlington outputs are operated as emitter followers in this application.

Type UDN-2845B and UDN-2846B devices are sink-and-source combinations in a single dual in-line package. Either device can be used for bipolar switching applications in which both ends of the load are floating.

The UDN-2841B, UDN-2843B, and UDN-2845B I.C.s are intended for use with 5 V TTL, Schottky TTL, DTL, and CMOS logic. The UDN-2842B,


UDN-2841B, UDN-2842B, ${ }^{*}$ UDN-2845B, UDN-2846B *


UDN-2843B, UDN-2844B*

UDN2844B, and UDN-2846B feature a higher input impedance and are intended for use with 8 V to 15 V PMOS and CMOS logic.

All types reduce component count, lower system cost, reduce circuit and board complexity, and provide solutions for many interface requirements.
> *UDN-2842B, UDN-2843B, UDN-2844B, and UDN-2846B Available Until Current Stock Depleted

SCHEMATIC (each driver)


| Type Number | Resistor Values in $\mathrm{k} \Omega$ |  |  |  |
| :---: | ---: | ---: | ---: | ---: |
|  | Amplifier 1 \& 3 |  | Amplifier 2 \& 4 |  |
|  | $\mathrm{R}_{\text {IN }}$ | $\mathrm{R}_{\mathrm{S}}$ | $\mathrm{R}_{\text {IN }}$ | $\mathrm{R}_{\mathrm{S}}$ |
|  | 10.5 | 15 | 3.3 | 15 |
| UDN-2843B | 3.3 | 15 | 10.5 | 15 |
| UDN-2844B | 10.5 | 1 | 3.3 | 1 |
| UDN-2845B | 3.3 | 1 | 15 | 3.5 |
| UDN-2846B | 10.5 | 15 | 10.5 | 1 |

NOTE: The substrate terminals must be tied to the most negative point in the external circuit to maintain isolation between transistors and to provide for normal device operation.

ABSOLUTE MAXIMUM RATINGS at $+25^{\circ} \mathrm{C}$
Free-Air Temperature for any one Darlington
Output (unless otherwise noted)
Output Volțage, $\mathrm{V}_{\text {CEIOFF) }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . 50 V

Substrate Voltage, V'sub . . . .............................. 50 V
Continuous Output Current, Iour......................... 1.75 A

Input Voltage, $\mathrm{V}_{\text {, }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . See Table
Power Dissipation, $P_{D}$ (one output)................... . 2.25 W*
(total package) . . . . . . . . . . . . . 2.77 W*
Operating Temperature Range, $T_{A} \ldots \ldots . .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{5} \ldots \ldots . . .-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate linearly to 0 W at $+150^{\circ} \mathrm{C}$.

| Type Number | $\mathrm{V}_{\text {S(MAX) }}$ | $\mathrm{V}_{\text {IMMAX) }}$ | Application |
| :---: | :---: | :---: | :--- |
| UDN-2841B | 10 V | 10 V | TTL, DTL, 5 V CMOS; current sink |
| UDN-2842B | 15 V | 15 V | $8-15 \mathrm{~V}$ PMOS \& CMOS; current sink |
| UDN-2843B | 10 V | 10 V | TLL, DTL, 5 V CMOS; current source |
| UDN-2844B | 15 V | 15 V | $8-15 \mathrm{~V}$ PMOS \& CMOS; current source |
| UDN-2845B | 10 V | 10 V | TTL, DTL, 5 V CMOS; source \& sink |
| UDN-2846B | 10 V | 15 V | $8-15 \mathrm{~V}$ PMOS \& CMOS; source \& sink |



Current Sink


Current Source

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ (unless otherwise noted),
See Applicable Test Figure for Conditions not Specified

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | ${ }^{-1} \mathrm{lexx}$ | $\mathrm{V}_{\text {EE }}=-50 \mathrm{~V}, \mathrm{~V}_{\mathrm{N}}=0.4 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {EE }}=-50 \mathrm{~V}, \mathrm{~V}_{\mathbb{W}}=0.4 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {cesus) }}$ | $\mathrm{V}_{\mathrm{EE}}=-50 \mathrm{~V}, \mathrm{~V}_{\mathrm{WN}}=0.4 \mathrm{~V}, \mathrm{l}_{\text {OUI }}=100 \mathrm{~mA}$ | 35 | 50 | - | V |
| Output Saturation Voltage | $\mathrm{V}_{\text {cesati) }}$ | $\mathrm{I}_{\text {OUT }}=500 \mathrm{~mA}$ | - | - | 1.1 | V |
|  |  | $\mathrm{I}_{\text {Ouf }}=1.0 \mathrm{~A}$ (Note 1) | - | - | 1.4 | V |
|  |  | $\mathrm{I}_{\text {Oif }}=1.5 \mathrm{~A}$ (Note 1) | - | - | 1.7 | V |
| Input Current | $\mathrm{I}_{\text {M(OW) }}$ | $\mathrm{I}_{\text {OUT }}=500 \mathrm{~mA}, \mathrm{UDN}-2841 / 43 / 45 \mathrm{~B}, \mathrm{~V}_{\mathrm{W}}=2.4 \mathrm{~V}$ | - | 300 | 625 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{I}_{\text {OUf }}=500 \mathrm{~mA}, \mathrm{UDN}-2842 / 44 / 46 \mathrm{~B}, \mathrm{~V}_{\mathrm{W}}=5.0 \mathrm{~V}$ | - | 350 | 660 | $\mu \mathrm{A}$ |
| Input Voltage (Note 1) | $\mathrm{v}_{\text {mow }}$ | $\mathrm{I}_{\text {Out }}=1.5 \mathrm{~A}$, UDN-2841/43/45B | - | - | 2.4 | V |
|  |  | $\mathrm{I}_{\text {ouf }}=1.5 \mathrm{~A}, \mathrm{UDN}-2842 / 44 / 46 \mathrm{~B}$ | - | - | 5.0 | V |
| Supply Current <br> (Note 1) | $\mathrm{I}_{\mathrm{s}}$ | $\mathrm{I}_{\text {OUT }}=500 \mathrm{~mA}, \mathrm{UDN}-2841 / 42 \mathrm{~B}, \mathrm{UDN}$-2845/46B (Note 2) | - | 2.5 | 5.0 | mA |
|  |  | $\mathrm{I}_{\text {OUT }}=500 \mathrm{~mA}, \mathrm{UDN}-2843 / 44 \mathrm{~B}, \mathrm{UDN}$-2845/46B (Note 3) | - | 3.3 | 10 | mA |
| Turn-On Delay | $\mathrm{t}_{\text {putan) }}$ | $\mathrm{R}_{\mathrm{L}}=39 \Omega, 0.5 \mathrm{~V}_{\mathbb{N}}$ to $0.5 \mathrm{~V}_{\text {out }}$ | - | - | 2.0 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {putaff }}$ | $\mathrm{R}_{\mathrm{L}}=39 \Omega, 0.5 \mathrm{~V}_{\mathrm{W}}$ to $0.5 \mathrm{~V}_{\text {our }}$ | - | - | 5.0 | $\mu \mathrm{s}$ |

## NOTES:

1. Each driver tested separately.
2. Drivers $1 \& 3$ (sink drivers) only, $\mathrm{V}_{S}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-40 \mathrm{~V}$.
3. Drivers 2 \& 4 (source drivers) only, $\mathrm{V}_{\mathrm{S}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-40 \mathrm{~V}$.



TYPE UDN-2841B and UDN-2842B TEST CIRCUIT

$V_{\text {IN }}=+2.4 V$ (UDN-2843B) or $+5.0 V$ (UDN-2844B)
DWG. No A-10,486A
TYPE UDN-2843B and UDN-2844B TEST CIRCUIT


TYPE UDN-2845B and UDN-2846B TEST CIRCUIT

ALLOWABLE OUTPUT CURRENT
AS A FUNCTION OF DUTY CYCLE



## TYPICAL BIPOLAR MOTOR DRIVE APPLICATION



TYPICAL ELECTROSENSITIVE PRINTER APPLICATION


## UTN-2886B and UTN-2888A MONOLITHIC SCR ARRAYS

## FEATURES

- Low Input Current
- TTL, LSTTL and CMOS Compatible
- Momentary Inrush Current Capability to 2 A
- Minimum Forward Blocking Voltage 35 V
- Use with Full-Wave or Half-Wave Sources

INTENDED FOR USE with microprocessors that are strobing power loads, these monolithic SCR arrays will interface to high-current loads including lamps, relays, and solenoids. The use of multiple SCRs in a single package reduces component count, insertion costs, assembly time, and circuit space, while improving overall circuit reliability.

Each array contains multiple SCRs with integral current limiting and gate-to-cathode resistors. In all cases, the maximum allowable SCR current rating at $+25^{\circ} \mathrm{C}$ is 800 mA continuous or 2 amperes nonrecurring peak. Outputs may be paralleled for higher load current capability within the limits of the allowable package power dissipation rating.

The UTN-2886B array contains four individual SCRs and two pairs of paralleled SCRs (pins 8-9 and 1-16). Each SCR is capable of continuous and simultaneous operation at $250 \mathrm{~mA}(500 \mathrm{~mA}$ at pins 9 and 16) at an ambient temperature of $+50^{\circ} \mathrm{C}$. The $16-$ lead package with heat-sink contact tabs allows maximum power dissipation with standard cooling methods. Further increases in power dissipation can be obtained by attaching an external heat sink to the webbed leads.

The UTN-2888A SCR array contains eight isolated devices, each capable of continuous and simultaneous operation at 200 mA at an ambient temperature of $+50^{\circ} \mathrm{C}$.

These SCR arrays operate from an unfiltered half-wave ( 50 or 60 Hz ) or full-wave ( 100 or $120 \mathrm{~Hz})$ rectified source. They are not intended for use with a-c sources, and will not sustain commercial a-c line voltages ( 115 VAC ).


UTN-2886B


UTN-2888A

## ABSOLUTE MAXIMUM RATINGS

ALLOWABLE AVERAGE POWER DISSIPATION
Forward Blocking Voltage (Input Open), $\mathrm{V}_{\mathrm{AK}}$35 V
Reverse Blocking Voltage, V ..... 300 mV
Continuous Forward Current, ..... 800 mA
Peak Forward Surge Current, I ..... 2.0 A
Gate Input Power, $\mathrm{P}_{\text {IN }}$ ..... 10 mW
Peak Gate Input Power, $\mathrm{P}_{\mathrm{IN}}$ ..... 50 mW
Gate Input Current, $\mathrm{I}_{\mathrm{N}}$ ..... 50 mA
Reverse Gate Input Voltage, $\mathrm{V}_{\text {IN }}$ ..... 5.0 V
Total Package Power Dissipation, P ..... See Graph
Operating Temperature Range, $T_{A}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{S}$ ..... $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## AS A FUNCTION OF AMBIENT TEMPERATURE



## ELECTRICAL CHARACTERISTICS for any one individual SCR*

| Characteristic | Symbol | Test Temp. | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Max. | Units |
| Forward Blocking Current | $\mathrm{I}_{\text {A }}$ | $+70^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathrm{AK}}=35 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=100 \mathrm{mV}$ | - | 50 | $\mu \mathrm{A}$ |
| Gate-to-Anode Leakage Current | $I_{\text {IN }}$ | $+70^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {AK }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=5.0 \mathrm{~V}$ | - | 250 | $\mu \mathrm{A}$ |
| Forward ON Voltage | $V_{\text {AK(ON) }}$ | $+25^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{A}}=275 \mathrm{~mA}, \mathrm{~V}_{\mathbb{N}}=2.5 \mathrm{~V}$ | - | 1.2 | V |
|  |  | $+55^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{A}}=275 \mathrm{~mA}, \mathrm{~V}_{\mathbb{N}}=2.5 \mathrm{~V}$ | - | 1.15 | V |
| Gate Trigger Current | $1_{\text {INOON }}$ | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {AK }}=7.0 \mathrm{~V}, \mathrm{~V}_{\mathbb{N}}=2.5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=50 \Omega$ | - | 300 | $\mu \mathrm{A}$ |
| Gate Trigger Voltage | $V_{\text {IVON) }}$ | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {AK }}=1.7 \mathrm{~V}, \mathrm{t}_{\mathrm{gt}}=20 \mu \mathrm{~s}, \mathrm{R}_{\mathrm{L}}=50 \Omega$ | - | 2.5 | V |
| Gate OFF Voltage | $V_{1 \text { IVOFF) }}$ | $+70^{\circ} \mathrm{C}$ | $V_{\text {AK }}=35 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=50 \Omega$ | 100 | - | mV |
| Gate OFF Current | $1_{1 \text { (1 Off) }}$ | $+70^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {AK }}=35 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=50 \Omega$ | - | 10 | $\mu \mathrm{A}$ |
| Holding Current | $\mathrm{T}_{\mathrm{H}}$ | $0^{\circ} \mathrm{C}$ | $\mathrm{T}_{\text {IN(NTIT })}=20 \mathrm{~mA}$ | - | 10 | mA |
|  |  | $+55^{\circ} \mathrm{C}$ | $\mathrm{l}_{\text {In(mint }}=20 \mathrm{~mA}$ | - | 5.0 | mA |
| Anode OFF Voltage | $\mathrm{V}_{\text {AK( }}$ (f) | $+55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathrm{IN}}=5.0 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=50 \Omega$ | 400 | - | mV |

[^20]

TYPICAL LAMP APPLICATION


Dwg. No. A-11,089
TYPICAL WAVEFORMS

## APPLICATION NOTES

1. These devices normally operate from an unfiltered half-wave or full-wave rectified source. They cannot be operated with a bidirectional (unrectified) a-c source.
2. During operation, the SCR is turned ON by application of a positive voltage to the input. The SCR will remain ON, even though the input voltage is removed or made slightly negative, until the anode-to-cathode voltage is reduced to below the anode OFF voltage.
3. When using multiple SCRs and a common suplly, gate-to-anode leakage currents can hold the
supply voltage above the anode OFF voltage and prevent proper turn-OFF. To insure proper operation, resistor $R$ should be used as shown in the typical application. The maximum resistor value is determined from:

$$
R=\frac{V_{\text {AKIOFF }}}{(n-1) I_{G A}}=\frac{400 \mathrm{mV}}{(\mathrm{n}-1) 250 \mu \mathrm{~A}}
$$

where $n$ is the number of SCRs being used in the system. Note that $\mathrm{n}=2$ for pin 8-9 and pin 1-16 of the UTN-2886B .
4. Various combinations of number of outputs conducting, duty cycle, and ambient temperature must be held within the allowable package power dissipation limits shown.

# UDN-2949Z HIGH-CURRENT BIPOLAR HALF-BRIDGE MOTOR DRIVER 

## FEATURES

- 3.5 A Peak Output
- $32 . V$ Output Breakdown
- Output Transient Suppression
- TTL, CMOS, PMOS, NMOS Compatible Inputs
- High-Speed Chopper (to 100 kHz )
- Low Standby Current ( 10 mA )
- T0-220 Style Package

THE UDN-2949Z is a monolithic half-bridge motor driver supplied in a power-tab TO-220 style package. The circuit combines sink and source drivers with diode protection, gain and level shifting systems, and a voltage regulator for single-supply operation. The unit is specifically designed for servomotor drive applications using pulse-width modulation (chopping).

The chopper drive mode is characterized by a minimum power dissipation requirement, low saturation voltages, and low chopper storage times for the NPN sink driver. Predriver stages reduce input drive requirements while allowing the output to switch currents of 2 amperes. Output d-c current accuracies of better than $10 \%$ at 100 kHz can be obtained.

The PNP sourcing driver is turned ON by an active high input while the NPN sinking driver is activated with a low input. These inputs are completely compatible with TTL, low-voltage CMOS, PMOS, and NMOS.

The UDN-2949Z may be used in pairs (fullbridge) for d-c stepper motor or brushless a-c motor drive applications. Such applications may require an external ground clamp diode ( 1 N 4000 ) connected at the output of each device in order to minimize package power dissipation.


Single-chip construction and the power-tab TO-220 style package provide improved cost effectiveness and reliability over discrete component motor drive systems with excellent power dissipation capability, minimum size, ease of installation, and heat sinking.

The package heat tab is at ground potential. Multiple devices may share a common heat sink without insulating hardware.

The UDN-2949Z power driver may be used in stepper-motor bipolar bridge-driver circuits, for example, with the Sprague UCN-4202A Stepper Motor Translator/Driver.

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage Range, $V_{S}$ ..... 15 V to 30 V
Input Voltage Range, $V_{\text {IN }}$ ..... -0.3 V to +7.0 V
Peak Output Current, ( $100 \mathrm{~ms}, 10 \%$ d.c.), $\mathrm{I}_{0 \mathrm{p}}$ ..... $\pm 3.5 \mathrm{~A}$
Continuous Output Current, I Iout ..... $\pm 2.0 \mathrm{~A}$
Package Power Dissipation, $P_{D}$ ..... See Graph
Operating Temperature Range, $T_{A}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## LOGIC TRUTH TABLE

| Source Driver | Sink Driver | Output, |
| :---: | :---: | :---: |
| Input, $V_{2}$ | Input, $V_{5}$ | $V_{4}$ |
| Low | Low | Low |
| Low | High | Open |
| High | High | High |
| High | Low | Disallowed |

ELECTRICAL CHARACTERISTICS at $T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}=24 \mathrm{~V}$ (unless otherwise noted).

| Characteristic | Test Conditions |  |  |  | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Source Driver Input, Pin 2 | Sink Driver Input, Pin 5 | Output Pin 4 | Other |  |  |  |
|  |  |  |  |  | Min. | Max. | Units |
| Output Leakage Current | 0.8 V | 2.4 V | OV | $V_{S}=28 \mathrm{~V}$ | - | -500 | $\mu \mathrm{A}$ |
|  | 0.8 V | 2.4 V | 28 V | $V_{S}=28 \mathrm{~V}$ | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | 0.8 V | 0.8 to 2.4 V | 2.0A | Test Fig. 1 | 30 | - | $V$ |
| Output Saturation Voltage | 2.4 V | 2.4 V | -2.0 A |  | 22 | - | V |
|  | 0.8 V | 0.8 V | 2.0 A |  | - | 2.0 | V |
| Output Source Current | 2.4 V | 2.4 V | - |  | -2.0 | - | A |
| Output Sink Current | 0.8 V | 0.8 V | - |  | 2.0 | - | A |
| Input Open-Circuit Voltage | $-250 \mu \mathrm{~A}$ | $-250 \mu \mathrm{~A}$ | - |  | - | 7.5 | $V$ |
| Input Current | 2.4 V | 2.4 V | NC |  | - | -700 | U |
|  | 0.8 V | 0.8 V | NC |  | - | -5.0 | mA |
| Propagation Delay | 0.8 V | 0.8 to 2.4 V | NC |  | - | 750 | ns |
|  | 0.8 to 2.4 V | 2.4 V | NC |  | - | 5.0 | us |
| Clamp Diode Forward Voltage | NC | NC | 2.0 A | Test Fig. 2 | - | 2.2 | $V$ |
| Supply Current | NC | NC | NC |  | - | 35 | mA |

Note: Positive (negative) current is defined as going into (coming out of) the specified device pin.


## APPLICATION NOTES

1. The source and sink outputs should not be ON simultaneously ( $\mathrm{V}_{2}$ High, $\mathrm{V}_{5}$ Low). High "crossover" currents could degrade or destroy the device.
2. Do not assume from the Logic Truth Table that both inputs can be connected ( $\mathrm{V}_{4}$ High or Low only). The sink driver is considerably faster than the source driver. An input shift from high-to-low levels could produce a condition where both drivers are ON, and that condition could occur for as long as $5 \mu$.
3. It is recommended that the inputs be driven separately, and that the sink driver input
not be pulled low (turned ON) for at least $5 \mu \mathrm{~s}$ (max. source $t_{P D}$ ) after the source driver input is pulled low (turned OFF). The sink driver should be allowed to go high (turned OFF) at least 750 ns (max. sink tpD) before the source driver goes high (turned ON).



PACKAGE POWER DISSIPATION
AS A FUNCTION OF TEMPERATURE


DWG. NO. A-11,183

SINGLE-WINDING D-C OR STEPPER MOTOR
FULL-BRIDGE D-C SERVO MOTOR APPLICATION


## UDN-2952B AND UDN-2952W FULL-BRIDGE MOTOR DRIVERS

## FEATURES

- High Output Current
- Adjustable Short-Circuit Protection
- Thermal Shutdown
- Internal Clamp Diodes
- TTL, DTL, PMOS, CMOS Compatible
- DIP or SIP Packaging

FULL-BRIDGE motor driver IC Types UDN-2952B and UDN-2952W have both the logic circuitry and Darlington-pair power drivers for bidirectional control of d-c motors operating at currents of up to 2 A .

The integrated circuits carry extensive circuit protection. Output current-limiting is determined by the user's selection of sensing resistors. Both drivers have thermal shutdown networks that disable motor drive if the circuits' power dissipation ratings are exceeded. Internal transient suppression is built into both.
Type UDN-2952B is in a 16 -pin dual in-line package with heat-sink contact tabs. The lead configuration enables easy attachment of a heat sink while fitting a standard integrated circuit socket or printed wiring board layout. Type UDN-2952W, for higher power requirements, is in a 12 -pin single in-line power tab package.
Both drivers have tab temperature ratings of $+70^{\circ} \mathrm{C}$ and require external heat sinks.


UDN-2952B


UDN-2952W

$$
\begin{aligned}
& \text { ABSOLUTE MAXIMUM RATINGS } \\
& \text { of } \mathrm{T}_{\mathrm{TAB}}=+70^{\circ} \mathrm{C}
\end{aligned}
$$


Logic Supply Voltage, $\mathrm{V}_{\text {od }}$........................... 7.0 V

Input Voltage, $\mathrm{V}_{\text {IN }}$ or $\mathrm{V}_{\text {emabie }} \ldots \ldots . . . . . . . . . . . . .30 \mathrm{~V}$
Output Current, Iour (UDN-2952B) Continuous ...... $\pm 1.0 \mathrm{~A}$
$100 \mathrm{~ms}, 10 \%$ duty cycle . . $\pm 3.5 \mathrm{~A}$
(UDN-2952W) Continuous ...... $\pm 2.0 \mathrm{~A}$
$100 \mathrm{~ms}, 10 \%$ duty cycle . $\pm 5.0 \mathrm{~A}$
Package Power Dissipation, $P_{0}$ (UDN-2952B) .........6.7 W*
(UDN-2952W) ..... 27 W**
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{s}} \ldots \ldots \ldots-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $83.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\text {TAB }}=+70^{\circ} \mathrm{C}$.
**Derate at the rate of $333 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\text {TAB }}=+70^{\circ} \mathrm{C}$.

## UDN-2952W



UDN-2952B


Dwg. No. A-11,368B

## FUNCTIONAL BLOCK DIAGRAM



# UDN-2956A and UDN-2957A HIGH-VOLTAGE, HIGH-CURRENT SOURCE DRIVERS 

$\mathrm{C}^{\mathrm{C}}$OMPRISED of five common collector NPN Darlington output stages, the associated common base PNP input stages, and a common "enable" stage, the UDN-2956A and UDN-2957A high-voltage, high-current source drivers are used to switch the ground end of loads which are directly connected to a negative supply. Typical loads include telephone relays, PIN diodes, and LEDs. Both devices will sustain output OFF voltages of -80 V and will source currents to -500 mA per driver. Under normal operating conditions, these units will sustain load currents of -200 mA on each of the five drivers simultaneously at ambient temperatures up to $+70^{\circ} \mathrm{C}$.

The UDN-2956A driver is intended for use with MOS (PMOS or CMOS) logic input levels operating with supply voltages from 6 V to 16 V . The UDN2957A driver has appropriate input current limiting resistors for operation from TTL, Schottky TTL, DTL, and 5 V CMOS. With either device, the input and enable levels must both be biased towards the positive supply to activate the output load.

Integral transient suppression diodes allow these devices to be used with inductive loads without the need for discrete diodes. In order to maintain isolation between drivers, the substrate should be connected to the most negative supply applied.

Input connections are on one side of the dual in-line package, output connections on the other side to simplify printed wiring board layout.

The UDN-2956A and UDN-2957A high-voltage, high-current drivers are supplied in 14 -lead dual in-line packages conforming to JEDEC outline


TO-116 (MO-001AA). Hermetically-sealed versions of these devices (with reduced package power dissipation capability) are available.

## ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ Free-Air Temperature (reference pin 7)


Input Voltage, $\mathrm{V}_{\mathbb{N}}$ (UDN-2956A) $\ldots . . . . . . . . . . . . .+20 \mathrm{~V}$
(UDN-2957A) ................... +10 V
Output Current, $\mathrm{I}_{\text {our }}$........................... . -500 mA
Power Dissipation, $P_{0}$ (any one driver) ................ 1.0 W
(total package) ............. 2.0 W* $^{*}$
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots .-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $16.67 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$.

ELECTRICAL CHARACTERISTICS at $T_{A}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\text {Emale }}=\mathrm{V}_{\text {II }}$ (unless otherwise specified)

| Characteristic | Symbol | Applicable Devices | Test Conditions | Limit |
| :---: | :---: | :---: | :---: | :---: |
| Output Leakage Current | $\mathrm{I}_{\text {CEX }}$ | UDN-2956A | $\mathrm{V}_{\mathbb{N}}=\mathrm{V}_{\text {EVable }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | $-200 \mu \mathrm{~A} \mathrm{Max}$. |
|  |  |  | $V_{\text {IN }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {Enabie }}=15 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | $-200 \mu \mathrm{~A}$ Max. |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=15 \mathrm{~V}, \mathrm{~V}_{\text {ENabIE }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | $-200 \mu \mathrm{~A}$ Max. |
|  |  | UDN-2957A | $\mathrm{V}_{\mathbb{I}}=\mathrm{V}_{\text {ENABLE }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | $-200 \mu \mathrm{~A}$ Max. |
|  |  |  | $\mathrm{V}_{\text {IN }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {EAABLE }}=3.85 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | $-200 \mu \mathrm{~A}$ Max. |
|  |  |  | $\mathrm{V}_{\mathbb{W}}=3.85 \mathrm{~V}, \mathrm{~V}_{\text {EMABLE }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | $-200 \mu \mathrm{~A}$ Max. |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CeISAT }}$ | UDN-2956A | $\mathrm{V}_{\mathrm{W}}=6.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=100 \mathrm{~mA}$ | -1.20 V Max. |
|  |  |  | $\mathrm{V}_{\text {IN }}=7.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=175 \mathrm{~mA}$ | -1.35 V Max. |
|  |  |  | $\mathrm{V}_{\mathbb{W}}=10 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | -1.70 V Max. |
|  |  | UDN-2957A | $\mathrm{V}_{\mathrm{W}}=2.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}$ | -1.20 V Max. |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=2.7 \mathrm{~V}, \mathrm{I}_{\text {out }}=-175 \mathrm{~mA}$ | -1.35 V Max. |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=3.9 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | -1.70 V Max. |
| Input Current | $I_{\text {m(ON) }}$ | UDN-2956A | $\mathrm{V}_{\mathbb{N}}=6.0 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | $650 \mu \mathrm{~A}$ Max. |
|  |  |  | $\mathrm{V}_{\mathbb{W}}=15 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | 1.85 mA Max. |
|  |  | UDN-2957A | $\mathrm{V}_{\mathbb{N}}=2.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | $675 \mu \mathrm{~A}$ Max. |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=3.85 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | 1.40 mA Max . |
|  | $I_{\text {MNOFF }}$ | ALL | $\mathrm{I}_{\text {out }}=-500 \mu \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | $50 \mu \mathrm{~A}$ Min. |
| Output Source Current | $\mathrm{I}_{\text {OUT }}$ | UDN-2956A | $\mathrm{V}_{\mathbb{W}}=5.0 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | -125 mA Min . |
|  |  |  | $\mathrm{V}_{\mathrm{W}}=6.0 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | -200 mA Min. |
|  |  |  | $\mathrm{V}_{\text {IN }}=7.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -250 mA Min. |
|  |  |  | $\mathrm{V}_{\text {W }}=8.0 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | -300 mA Min. |
|  |  |  | $\mathrm{V}_{\text {WN }}=9.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -350 mA Min. |
|  |  | UDN-2957A | $\mathrm{V}_{\mathbb{N}}=2.4 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -125 mA Min. |
|  |  |  | $\mathrm{V}_{\text {IN }}=2.7 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | - $200 \mathrm{~mA} \mathrm{Min}$. |
|  |  |  | $V_{\text {IN }}=3.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -250 mA Min. |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -300 mA Min . |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -350 mA Min. |
| Output Sustaining Voltage | $\mathrm{V}_{\text {ceISUS) }}$ | UDN-2956A | $\mathrm{V}_{\mathbb{W}}=0.4 \mathrm{~V}, \mathrm{I}_{\text {Out }}=-25 \mathrm{~mA}$ | 50 V Min. |
|  |  | UDN-2957A | $\mathrm{V}_{\text {IN }}=0.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$ | 50 V Min. |
| Clamp Diode Leakage Current | $I_{R}$ | ALL | $V_{R}=80 \mathrm{~V}$ | $50 \mu \mathrm{~A}$ Max. |
| Clamp Diode Forward Voltage | $V_{F}$ | ALL | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | 2.0 V Max. |
| Turn-On Delay | $\mathrm{t}_{\mathrm{ON}}$ | ALL | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}, \mathrm{R}_{\mathrm{L}}=400 \Omega \mathrm{C}_{\mathrm{I}}=25 \mathrm{pF}$ | $4.0 \mu \mathrm{~s}$ Max. |
| Turn-Off Delay | $\mathrm{t}_{\text {Off }}$ | ALL | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }} \mathrm{R}_{\mathrm{L}}=400 \Omega \mathrm{C}_{\mathrm{T}}=25 \mathrm{pF}$ | $10 \mu s$ Max. |

## INPUT CURRENT

## AS A FUNCTION OF INPUT VOLTAGE




## ALLOWABLE PEAK OUTPUT CURRENT AS A FUNCTION OF DUTY CYCLE




## SERIES UDN-2980A HIGH-VOLTAGE, HIGH-CURRENT SOURCE DRIVERS

## FEATURES

- TTL, DTL, PMOS, or CMOS Compatible Inputs
- 500 mA Output Source Current Capability
- Transient-Protected Outputs
- Output Breakdown Voltage to 80 V

RECOMMENDED for applications requiring separate logic and load grounds, load supply voltage to +80 V , and load currents to 500 mA , Series UDN-2980A source drivers are used as interfaces between standard low-power digital logic and relays, solenoids, stepping motors, and LEDs.

Under normal operating conditions, these devices will sustain 120 mA continuously for each of the eight outputs at an ambient temperature of $+50^{\circ} \mathrm{C}$ and a supply of +15 V . All devices in this series incorporate input current limiting resistors and output transient suppression diodes.

Type UDN-2981A and UDN-2983A drivers are for use with +5 V logic systems - TTL, Schottky TTL, DTL, and 5 V CMOS. Type UDN-2982A and UDN-2984A drivers are intended for MOS interface (PMOS and CMOS) operating from supply voltages

of 6 to 16 V . Types UDN-2981A and UDN-2982A will sustain a maximum output OFF voltage of +50 V , while Types UDN-2983A and UDN-2984A will sustain an output voltage of +80 V . In all cases, the output is switched on by an active high input level.

Series UDN-2980A high-voltage, high-current source drivers are supplied in 18-lead dual in-line packages. On special order, hermetically-sealed versions of these devices (with reduced package power dissipation capability) can also be furnished.

## ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ Free-Air Temperature

| Output Voltage, Range $\mathrm{V}_{\text {CE }}$ (UDN-2981A \& UDN-2982A) <br> (UDN-2983A \& UDN-2984A) | $\begin{aligned} & +5 \mathrm{~V} \text { to }+50 \mathrm{~V} \\ & +35 \mathrm{~V} \text { to }+80 \mathrm{~V} \end{aligned}$ |
| :---: | :---: |
| Input Voltage, $\mathrm{V}_{\text {IN }}$ (UDN-2981A \& UDN-2983A) <br> (UDN-2982A \& UDN-2984A) | $\begin{aligned} & +15 \mathrm{~V} \\ & +30 \mathrm{~V} \end{aligned}$ |
| Output Current, $\mathrm{I}_{\text {our }}$ | - 500 mA |
| Power Dissipation, $P_{D}$ (any one driver) (total package) | $\begin{aligned} & 1.1 \mathrm{~W} \\ & 2.2 \mathrm{~W}^{*} \end{aligned}$ |
| Operating Temperature Range, $\mathrm{T}_{A}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ | $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

ONE OF EIGHT DRIVERS


POWER DISSIPATION
AS A FUNCTION OF AMBIENT TEMPERATURE


AMBIENT TEMPERATURE IN ${ }^{\circ} \mathrm{C}$

## ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ (unless otherwise specified)

| Characteristic | Symbol | Applicable Devices | Test Conditions | Test Fig. | Limit |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | UDN-2981/82A | $\mathrm{V}_{\mathbb{I} \mathrm{N}}=0.4 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{S}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | 1 | - | - | 200 | $\mu \mathrm{A}$ |
|  |  | UDN-2983/84A | $\mathrm{V}_{\mathbb{N}}=0.4 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{S}}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | 1 | - | - | 200 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $V_{\text {celsat }}$ | All | $\mathrm{V}_{\text {IN }}=2.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}$ | 2 | - | 1.6 | 1.8 | V |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=2.4 \mathrm{~V}, \mathrm{I}_{\text {Out }}=-225 \mathrm{~mA}$ | 2 | - | 1.7 | 1.9 | V |
|  |  |  | $\mathrm{V}_{\mathbb{N}}=2.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | 2 | - | 1.8 | 2.0 | $V$ |
| Input Current | $\mathrm{I}_{\text {(NON }}$ | UDN-2981/83A | $\mathrm{V}_{\mathbb{N}}=2.4 \mathrm{~V}$ | 3 | - | 140 | 200 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\text {IV }}=3.85 \mathrm{~V}$ | 3 | - | 310 | 450 | $\mu \mathrm{A}$ |
|  |  | UDN-2982/84A | $\mathrm{V}_{\text {W }}=2.4 \mathrm{~V}$ | 3 | - | 140 | 200 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ | 3 | - | 1.25 | 1.93 | mA |
| Output Source Current | $\mathrm{I}_{\text {OUT }}$ | UDN-2981/83A | $\mathrm{V}_{\mathbb{1}}=2.4 \mathrm{~V}, \mathrm{~V}_{\mathrm{CE}}=2.0 \mathrm{~V}$ | 2 | -350 | - | - | mA |
|  |  | UDN-2982/84A | $\mathrm{V}_{\text {IN }}=2.4 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=2.0 \mathrm{~V}$ | 2 | -350 | - | - | mA |
| Supply Current (Outputs Open) | $\mathrm{I}_{5}$ | UDN-2981/82A | $\mathrm{V}_{\text {iN }}=2.4 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{S}}=50 \mathrm{~V}$ | 4 | - | - | 10 | mA |
|  |  | UDN-2983/84A | $\mathrm{V}_{\mathbb{N}}=2.4 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{S}}=80 \mathrm{~V}$ | 4 | - | - | 10 | mA |
| Clamp Diode Leakage Current | $I_{R}$ | UDN-2981/82A | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=0.4 \mathrm{~V}^{*}$ | 5 | - | - | 50 | $\mu \mathrm{A}$ |
|  |  | UDN-2983/84A | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}, \mathrm{~V}_{\mathbb{N}}=0.4 \mathrm{~V}^{*}$ | 5 | - | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{\text {F }}$ | All | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | 6 | - | 1.5 | 2.0 | V |
| Turn-On Delay | $\mathrm{t}_{\text {ON }}$ | All | $\begin{aligned} 0.5 \mathrm{E}_{\text {IN }} \text { to } 0.5 \mathrm{E}_{\text {out },} \mathrm{R}_{\mathrm{L}} & =100 \Omega, \\ \mathrm{~V}_{\mathrm{S}} & =35 \mathrm{~V} \end{aligned}$ | - | - | 1.0 | 2.0 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {off }}$ | All | $\begin{aligned} 0.5 \mathrm{E}_{\mathbb{N}} \text { to } 0.5 \mathrm{E}_{\text {out }}, \mathrm{R}_{\mathrm{L}} & =100 \Omega, \\ V_{S} & =35 \mathrm{~V} \end{aligned}$ | - | - | 5.0 | 10 | $\mu \mathrm{S}$ |

[^21]
## TEST FIGURES



Figure 1

Figure 3


Figure 5


Figure 2


Figure 4

Figure 6

## ALLOWABLE PEAK COLLECTOR CURRENT <br> AS A FUNCTION OF DUTY CYCLE TYPE UDN-2981A/82A




## allowable peak collector current AS A FUNCTION OF DUTY CYCLE

 SERIES UDN-2980A


## ALLOWABLE PEAK COLLECTOR CURRENT

 AS A FUNCTION OF DUTY CYCLETYPES UDN-2983A84A



INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE FOR TYPES UDN-2981/83A

INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE FOR TYPES UDN-2982/84A


## TYPICAL ELECTROSENSITIVE PRINTER APPLICATION



TYPICAL VALUES: $\mathrm{V}_{\mathrm{s}}=50 \mathrm{~V}$

$$
\mathrm{I}_{\text {OUT }}=200-300 \mathrm{~mA}
$$

# SERIES UDN-3600M <br> DUAL 2-INPUT PERIPHERAL and POWER DRIVERS 

## FEATURES

- Four Logic Types
- DTL/TTL/PMOS/CMOS Compatible Inputs
- Low Input Current
- 300 mA Continuous Output Current
- Sustaining Voltage of 80 V
- Pin-for-Pin Replacement for Series LM3600N
- Pin-for-Pin Replacement for SN75451BP thru SN75454BP and 75461 thru 75464


## Description

These "mini-DIP" dual 2 -input peripheral and power drivers are bi-polar monolithic integrated circuits incorporating AND, NAND, OR, or NOR logic gates, and high-current switching transistors on the same chip. The two output transistors are capable of simultaneously sinking 300 mA continuously at ambient temperatures of up to $+70^{\circ} \mathrm{C}$. In the OFF state, these drivers will sustain at least 80 V .

## Applications

The Series UDN-3600M dual drivers are ideally suited for interface between low-level or high-level logic and high-current/high-voltage loads. Typical applications include driving peripheral loads such as incandescent lamps, light-emitting diodes, memories, heaters, and other non-inductive loads of up to 600 mA (both drivers in parallel).

With appropriate external diode transient suppression, the Series UDN3600M drivers can also be used with inductive loads such as relays, solenoids, and stepping motors.

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\mathrm{cc}}$ ..... 7.0 V
Input Voltage, $\mathrm{V}_{\mathbb{N}}$ ..... 30 V
Output Off-State Voltage, $\mathrm{V}_{\text {off }}$ ..... 80 V
Output On-State Sink Current, $\mathrm{I}_{\mathrm{ON}}$ ..... 600 mA
Power Dissipation, $P_{D}$ ..... 1.5 W
Each Driver ..... 0.8 W
Derating Factor Above $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ $12.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ or $80^{\circ} \mathrm{C} / \mathrm{W}$
Operating Free-Air Temperature Range, $\mathrm{T}_{\mathrm{A}}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :--- | :---: | :---: | :---: | :---: |
| Supply Voltage $\left(V_{c c}\right)$ | 4.75 | 5.0 | 5.25 | V |
| Operating Temperature Range | 0 | +25 | +85 | ${ }^{\circ} \mathrm{C}$ |
| Current into any output (ON state) |  |  | 300 | mA |

INPUT PULSE CHARACTERISTICS

| $V_{\text {in }(0)}=0 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{f}}=7 \mathrm{~ns}$ | $\mathrm{t}_{\mathrm{p}}=1 \mu \mathrm{~s}$ |
| :--- | ---: | ---: |
| $\mathrm{~V}_{\text {in }(1)}=3.5 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{r}}=14 \mathrm{~ns}$ | PRR $=500 \mathrm{kHz}$ |

## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  | Units | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. |  |  |
| "1" Input Voltage | $V_{\text {in(1) }}$ |  | MIN |  |  |  | 2.0 |  |  | V |  |
| "0" Input Voltage | $V_{\text {in(0) }}$ |  | MIN |  |  |  |  |  | 0.8 | V |  |
| "0" Input Current | $\operatorname{lin}(0)$ |  | MAX | 0.4 V | 30 V |  |  | 50 | 100 | $\mu \mathrm{A}$ | 2 |
| "1" Input Current | $\operatorname{lin}(1)$ |  | MAX | 30 V | 0 V |  |  |  | 10 | $\mu \mathrm{A}$ | 2 |
| Input Clamp Voltage | $V_{1}$ |  | MIN | $-12 \mathrm{~mA}$ |  |  |  |  | -1.5 | V |  |

SWITCHING CHARACTERISTICS at $V_{C C}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |  |
| Turn-on Delay Time | $\mathrm{t}_{\text {pdo }}$ | $\begin{aligned} & V_{\mathrm{S}}=70 \mathrm{~V}, R_{\mathrm{L}}=465!(10 \text { Watts }) \\ & C_{\mathrm{L}}=15 \mathrm{pF} \end{aligned}$ |  | 200 | 500 | ns | 3 |
| Turn-off Delay Time | $t_{\text {pd }}$ | $\begin{aligned} & \left.\mathrm{V}_{\mathrm{S}}=70 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=465 \mathrm{(10} \text { Watts }\right) \\ & \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF} \end{aligned}$ |  | 300 | 750 | ns | 3 |

NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each input tested separately.
3. Voltage values shown in the test circuit waveforms are with respect to network ground terminal.
4. Capacitance values specified include probe and test fixture capacitance.

## Type UDN-3611M Dual AND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | VCC | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | loff |  | MIN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 0.8 V | $V_{\text {cc }}$ | 100 mA |  | 0.25 | 0.4 | V |  |
|  |  |  | MIN | 0.8 V | VCC | 300 mA |  | 0.5 | 0.7 | V |  |
| "1" Level Supply Current | $\operatorname{Icc}(1)$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 8.0 | 12 | mA | 1,2 |
| "0" Level Supply Current | ICC(0) | NOM | MAX | OV | OV |  |  | 35 | 49 | mA | 1,2 |

## Type UDN-3612M Dual NAND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {cc }}$ | Driven Input | Other Input | Output | Min. | Гур. | Max. | Units |  |
| "1" Output Reverse Current | Ioff |  | MIN | 0.8 V | $V_{\text {cc }}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 0.8 V | $V_{\text {cc }}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | 2.0 V | 100 mA |  | 0.25 | 0.4 | V |  |
|  |  |  | MIN | 2.0 V | 2.0 V | 300 mA |  | 0.5 | 0.7 | V |  |
| "1" Level Supply Current | $\operatorname{lcc}(1)$ | NOM | MAX | 0 V | 0 V |  |  |  | 14 | mA | 1,2 |
| "0" Level Supply Current | ICC(0) | NOM | MAX | 5.0 V | 5.0 V |  |  |  | 53 | mA | 1,2 |



## Type UDN-3613M Dual OR Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)



## Type UDN-3614M Dual NOR Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {cc }}$ | Driven Input . | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | $\mathrm{l}_{\text {off }}$ |  | MIN | 0.8 V | 0.8 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 0.8 V | 0.8 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | 0 V | 100 mA |  | 0.25 | 0.4 | V |  |
|  |  |  | MIN | 2.0 V | OV | 300 mA |  | 0.5 | 0.7 | V |  |
| "1" Level Supply Current | $\operatorname{lcc}(1)$ | NOM | MAX | OV | OV | - |  | 12 | 15 | mA | 1,2 |
| "0" Level Supply Current | $\operatorname{ICC}(0)$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 40 | 50 | mA | 1,2 |



## NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Capacitance values specified include probe and test fixture capacitance.

## SERIES UDN-5700A <br> QUAD 2-INPUT PERIPHERAL and POWER DRIVERS

— TRANSIENT PROTECTED OUTPUTS

## FEATURES:

- Four Logic Types
- DTL/TTL/PMOS/CMOS Compatible Inputs
- Low Input Current
- 300 mA Continuous Output Current
- Sustaining Voltage of 80 V


## Description

These 16 -lead quad 2 -input peripheral and power drivers are bi-polar monolithic integrated circuits incorporating AND, NAND, OR, and NOR logic gates, high-current switching transistors, and transient suppression diodes on the same chip. The four output transistors are capable of simultaneously sinking 300 mA continuously at ambient temperatures of up to $+70^{\circ} \mathrm{C}$. In the OFF state, these drivers will sustain at least 80 V .

## Applications

The Series UDN-5700A quad drivers are ideally suited for interface between low-level or high-level logic and high-current/high-voltage loads. Typical applications include driving peripheral loads such as incandescent lamps, light-emitting diodes, memories, and heaters.
The integral transient suppression diodes allow their use with inductive loads such as relays, solenoids, or stepping motors without the need for discrete diodes. For non-inductive loads, the diode common bus can be used as a convenient lamp test.

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\text {cc }}$ ..... 7.0 V
Input Voltage, $V_{I N}$ ..... 30 V
Output Off-State Voltage, $\mathrm{V}_{\text {off }}$ ..... 80 V
Output On-State Sink Current, $I_{O N}$ ..... 600 mA
Suppression Diode Off-State Voltage, $\mathrm{V}_{\text {off }}$ ..... 80 V
Suppression Diode On-State Current, $\mathrm{I}_{\mathrm{oN}}$. ..... 600 mA
Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ ..... 2.0 W
Each Driver ..... 0.8 W
Derating Factor Above $25^{\circ} \mathrm{C}$ $16.7 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ or $60^{\circ} \mathrm{C} / \mathrm{W}$
Operating Free-Air Temperature Range, $\mathrm{T}_{\mathrm{A}}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :--- | :---: | :---: | :---: | :---: |
| Supply Voltage $\left(V_{\text {cc }}\right):$ | 4.75 | 5.0 | 5.25 | V |
| Operating Temperature Range | 0 | +25 | +85 | ${ }^{\circ} \mathrm{C}$ |
| Current into any output (ON state) |  |  | 300 | mA |

INPUT PULSE CHARACTERISTICS

| $V_{\text {in }(0)}=0 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{f}}=7 \mathrm{~ns}$ | $\mathrm{t}_{\mathrm{p}}=1 \mu \mathrm{~s}$ |
| ---: | :--- | ---: |
| $\mathrm{~V}_{\text {in }(1)}=3.5 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{r}}=14 \mathrm{~ns}$ | PRR $=500 \mathrm{kHz}$ |

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  | Units | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{C C}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. |  |  |
| "1" Input Voltage | $V_{\text {in }}(1)$ |  | MIN |  |  |  | 2.0 |  |  | V |  |
| "0" Input Voltage | $\mathrm{V}_{\text {in }(0)}$ |  | MIN |  |  |  |  |  | 0.8 | V |  |
| "0" Input Current | $\mathrm{I}_{\text {in }(0)}$ |  | MAX | 0.4 V | 30 V |  |  | 50 | 100 | $\mu \mathrm{A}$ | 2 |
| "1" Input Current | $\mathrm{I}_{\text {in( }(1)}$ |  | MAX | 30 V | 0 V |  |  |  | 10 | $\mu \mathrm{A}$ | 2 |
| Input Clamp Voltage | $V_{1}$ |  | MIN | $-12 \mathrm{~mA}$ |  |  |  |  | -1.5 | V |  |

SWITCHING CHARACTERISTICS at $V_{c c}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |  |
| Turn-on Delay Time | $t_{\text {pdo }}$ | $\begin{aligned} & V_{S}=70 \mathrm{~V}, R_{L}=465 \Omega(10 \text { Watts }) \\ & C_{L}=15 \mathrm{pF} \end{aligned}$ |  | 200 | 500 | ns | 3 |
| Turn-off Delay Time | $t_{\text {pd }}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{S}}=70 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=465 \Omega(10 \text { Watts }) \\ & \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF} \end{aligned}$ |  | 300 | 750 | ns | 3 |

NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each input tested separately.
3. Voltage values shown in the test circuit waveforms are with. respect to network ground terminal.
4. Capacitance values specified include probe and test fixture capacitance.

## Type UDN-5703A Quad OR Driver

## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {cc }}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | loff |  | MIN | 2.0 V | 0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | 0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0' Output Voltage | Von |  | MIN | 0.8 V | 0.8 V | 150 mA |  | 0.35 | 0.5 | $V$ |  |
|  |  |  | MIN | 0.8 V | 0.8 V | 300 mA |  | 0.5 | 0.7 | $V$ |  |
| Diode Leakage Current | ILK | NOM | NOM | 0 V | 0 V | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | $V_{C C}$ | VCC |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | $I_{\text {cc(1) }}$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 16 | 25 | mA | 1,2 |
| "0" Level Supply Current | $\operatorname{ICC}(0)$ | NOM | MAX | 0 V | 0 V |  |  | 72 | 100 | mA | 1,2 |



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $\mathrm{V}_{\mathrm{Cc}}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | loff |  | MIN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 0.8 V | Vcc | 150 mA |  | 0.35 | 0.5 | V |  |
|  |  |  | MIN | 0.8 V | $V_{\text {cc }}$ | 300 mA |  | 0.5 | 0.7 | V |  |
| Diode Leakage Current | ILK | NOM | NOM | 0 V | OV | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | VCc | VCC |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | $I_{C C(1)}$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 16 | 24 | mA | 1,2 |
| "0" Level Supply Current | ICC(0) | NOM | MAX | 0 V | 0 V |  |  | 70 | 98 | mA | 1, 2 |


2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off }}$ min).
4. Diode forward voltage drop measured at $\mathrm{I}_{\mathrm{f}}=300 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.

## Type UDN-5707A Quad NAND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | Ioff |  | MIN | 0.8 V | $V_{\text {CC }}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 0.8 V | $V_{C C}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | 2.0 V | 150 mA |  | 0.35 | 0.5 | $V$ |  |
|  |  |  | MIN | 2.0 V | 2.0 V | 300 mA |  | 0.5 | 0.7 | V |  |
| Diode Leakage Current | ILK | NOM | NOM | VCC | Vcc | OPEN |  |  | 200 | ${ }_{\mu} \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | OV | OV |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | ICC(1) | NOM | MAX | 0 V | 0 V |  |  | 24 | 30 | mA | 1,2 |
| "0" Level Supply Current | $\mathrm{ICC}(0)$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 80 | 106 | mA | 1,2 |



DWG. NO. A-7839A


DWG. HO. A-T900A

## Type UDN-5733A Quad NOR Driver



## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | VCc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | Ioff | * | MIN | 0.8 V | 0.8 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 0.8 V | 0.8 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | 0 V | 150 mA |  | 0.35 | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | 0 V | 300 mA |  | 0.5 | 0.7 | V |  |
| Diode Leakage Current | ILK | NOM | NOM | VCC | $V_{C C}$ | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | 0 V | 0 V |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | ICC(1) | NOM | MAX | 0 V | 0 V |  |  | 24 | 30 | mA | 1,2 |
| "0" Level Supply Current | I cc(0) | NOM | MAX | 5.0 V | 5.0 V |  |  | 80 | 100 | mA | 1,2 |



1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off(min). }}$.
4. Diode forward voltage drop measured at $\mathrm{I}_{\mathrm{f}}=300 \mathrm{~mA}$
5. Capacitance values specified include probe and test fixture capacitance.

## SERIES UDN-5700M DUAL PERIPHERAL and POWER DRIVERS

## — TRANSIENT PROTECTED OUTPUTS

## FEATURES

- Four Logic Types
- DTL/TTL/PMOS/CMOS Compatible Inputs
- Low Input Current
- 300 mA Continuous Output Current
- Sustaining Voltage of 80 V


## Description

These "mini-DIP" dual peripheral and power drivers are bi-polar monolithic integrated circuits incorporating AND, NAND, OR, or NOR logic gates, high-current switching transistors, and transient suppression diodes on the same chip. The two output transistors are capable of simultaneously sinking 300 mA continuously at ambient temperatures of up to $+70^{\circ} \mathrm{C}$. In the OFF state, these drivers will sustain at least 80 V .

## Applications

The Series UDN-5700M dual drivers are ideally suited for interface between low-level or high-level logic and high-current/high-voltage loads. Typical applications include driving peripheral loads such as incandescent lamps, light-emitting diodes, memories, and heaters with a load current of up to 600 mA .

The integral transient suppression diodes allow the use of these drivers with inductive loads such as relays, solenoids, or stepping motors without the need for discrete diodes. When not required for transient suppression, the diode common bus can be used to perform the "lamp test" function.

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\mathrm{CC}}$ ..... 7.0 V
Input Voltage, $\mathrm{V}_{\text {in }}$. ..... 30 V
Output Off-State Voltage, $\mathrm{V}_{\text {off }}$ ..... 80 V
Output On-State Sink Current, I ..... 600 mA
Suppression Diode Off-State Voltage, $\mathrm{V}_{\text {off }}$ ..... 80 V
Suppression Diode On-State Current, $\mathrm{I}_{\text {on }}$ ..... 600 mA
Power Dissipation at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{D}}$. ..... 1.5 W
Each Driver. ..... 0.8 W
Derating Factor. $12.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ or $80^{\circ} \mathrm{C} / \mathrm{W}$
Operating Free-Air Temperature Range, $\mathrm{T}_{\mathrm{A}}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$. $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :--- | :--- | :--- | :--- | :--- |
| Supply Voltage $\left(\mathrm{V}_{\mathrm{CC}}\right)$ : | 4.75 | 5.0 | 5.25 | V |
| Operating Temperature Range | 0 | +25 | +85 | ${ }^{\circ} \mathrm{C}$ |
| Current into any output (ON state) |  |  | 300 | mA |

## INPUT PULSE CHARACTERISTICS

| $V_{\text {in }(0)}=0 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{f}}=7 \mathrm{~ns}$ | $\mathrm{t}_{\mathrm{p}}=1 \mu \mathrm{~s}$ |
| :--- | :--- | :---: |
| $\mathrm{~V}_{\text {in }(1)}=3.5 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{r}}=14 \mathrm{~ns}$ | PRR $=500 \mathrm{kHz}$ |

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {cc }}$ | Driven Input | Other Input Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Input Voltage | $V_{\text {in( }}$ (1) |  | MIN |  | . |  | 2.0 |  |  | V |  |
| "0" Input Voltage | $V_{\text {in }(0)}$ |  | MIN |  |  |  |  |  | 0.8 | V |  |
| " 0 " Input Current at all Inputs except Strobe | $\mathrm{I}_{\text {in(0) }}$ |  | MAX | 0.4 V | 30 V |  |  | 50 | 100 | $\mu \mathrm{A}$ | 2 |
| " 0 " Input Current at Strobe | 1 in(0) |  | MAX | 0.4 V | 30 V |  |  | 100 | 200 | $\mu \mathrm{A}$ |  |
| "1" Input Current at all Inputs except Strobe | $\mathrm{I}_{\text {in(1) }}$ |  | MAX | 30 V | 0 V |  |  |  | 10 | $\mu \mathrm{A}$ | 2 |
| "1" Input Current at Strobe | $\mathrm{In}(1)$ |  | MAX | 30 V | OV |  |  |  | 20 | $\mu \mathrm{A}$ | 2 |
| Input Clamp Voltage | V |  | MIN | -12 mA |  |  |  |  | -1.5 | V |  |

## SWITCHING CHARACTERISTICS at $V_{\text {cc }}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

|  | Symbol | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Characteristic |  |  | Min. | Typ. | Max. | Units |  |
| Turn-on Delay Time | $\mathrm{t}_{\mathrm{pd} 0}$ | $\begin{aligned} & V_{S}=70 \mathrm{~V}, R_{\mathrm{L}}=465!2 \text { (10 Watts) } \\ & C_{\mathrm{L}}=15 \mathrm{pF} \end{aligned}$ |  | 200 | 500 | ns | 3 |
| Turn-off Delay Time | $t_{p d 1}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{S}}=70 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=465 \mathrm{~s} \text { ( } 10 \mathrm{Watts} \text { ) } \\ & \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF} \end{aligned}$ |  | 300 | 750 | ns | 3 |

## NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each input tested separately.
3. Voltage values shown in the test circuit waveforms are with respect to network ground terminal.
4. Capacitance values specified include probe and test fixture capacitance.

## Type UDN-57IIM Dual AND Driver

## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| " 1 " Output Reverse Current | loff |  | MIN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 0.8 V | $V_{\text {cc }}$ | 150 mA |  | 0.35 | 0.5 | V |  |
|  |  |  | MIN | 0.8 V | $V_{C C}$ | 300 mA |  | 0.5 | 0.7 | V |  |
| Diode Leakage Current | lıK | NOM | NOM | OV | OV | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | VCC | $V_{C C}$ |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | $\mathrm{ICC}(1)$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 8.0 | 12 | mA | 1,2 |
| "0" Level Supply Current | $\operatorname{lcc}(0)$ | NOM | MAX | 0 V | 0 V |  |  | 35 | 49 | mA | 1,2 |



## Type UDN-5712M Dual NAND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)



NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off }}(\min )$.
4. Diode forward voltage drop measured at $I_{f}=300 \mathrm{~mA}$
5. Capacitance values specified include probe and test fixture capacitance.

## Type UDN-5713M Dual OR Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)



## Type UDN-5714M Dual NOR Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)



# Series ULN-2000A Darlington Transistor Arrays* - Description and Application 

## Introduction

The increased use of electronic circuits in systems formerly built with mechanical, electro-mechanical, or hydraulic components has resulted in systems becoming more precise, more reliable, generally less expensive, smaller, more efficient, and faster. Although the drive capabilities of monolithic integrated logic circuits are adequate for most information processing applications, there now exists a large and rapidly growing number of system applications where the currentcarrying and/or voltage-sustaining capability of the integrated circuit logic is inadequate. Typically, these deficiencies arise when the logic must control such peripheral components as relays, solenoids, punches, stepping motors, and a variety of indicators (incandescent, LED, or gas discharge lamps and displays).

A very common solution to this output interface inadequacy has been the addition of discrete power transistors (or SCRs) and associated passive components to the logic output in order to obtain the necessary current and/or voltage capability. Although this provides a very satisfactory electrical solution, the large number of discrete components often required, high assembly labor costs, and space (packaging) limitations often mean additional problems and cost. A simple, and less expensive solution is the use of monolithic integrated circuits.

The Series ULN-2000A is comprised of four different high-voltage/high-current interface circuits. They are capable of controlling resistive, inductive, or tungsten filament loads of up to 125 watts and are compatible with all standard digital logic families (DTL, TTL, PMOS, and CMOS) without the need for additional discrete components.

High-Voltage and High-Current Capability
A large number of interface problems have been simplified by the Series ULN-2000A high-voltage, high-current Darlington transistor arrays. These devices are suitable for voltage, current, and gain levels beyond the limits of other monolithic buffers and arrays.

The four devices in the ULN-2000A series are all comprised of seven silicon NPN Darlington pairs on a common monolithic substrate. All units feature open collector outputs and integral suppression diodes for use with inductive loads.

All devices have an output sink current capability of 500 mA although peak inrush currents to 600 mA are permissible, making them ideal for use with tungsten filament lamps. All of the outputs will sustain "OFF" voltages of at least 50 volts. Each individual Darlington circuit may therefore switch up to 25 watts ( 50 V at 500 mA ).
A definite asset of monolithic device technology is the very fine match between adjacent outputs when used in parallel. Applications requiring a sink current beyond the capability of a single output can be accommodated by parallel outputs. Continuous operation of all outputs at the maximum rated current is not allowed because of power dissipation limitations imposed by the package. However, as illustrated in Figure 1, under certain conditions, the Series ULN-2000A Darlington arrays are capable of switching loads totaling more than 125 watts at an ambient temperature of $+70^{\circ} \mathrm{C}$.

[^22]Figure 1

## COLLECTOR CURRENT AS A FUNCTION OF dUTY CYCLE AND NUMBER OF OUTPUTS




Figure 2
ALLOWABLE AVERAGE PACKAGE POWER DISSIPATION AS A FUNCTION OF AMBIENT TEMPERATURE

## The Basic Darlington Array

The first, and basic array, in this series, is the Type ULN-2001A. This is a general-purpose version with input current limiting normally accomplished via the use of an appropriate discrete resistor connected in series with each input. It is also possible to utilize the intrinsic current limiting of many MOS outputs as shown in Figure 4; a typical P-channel characteristic.

The use of TTL in such a manner is not recommended due to the higher currents and resultant high level of package power dissipation. Outputs of most PMOS and CMOS circuits will not normally source currents of any significance due to their high source impedance.


DWU. NO. A-9595
(each driver)
Figure 3
TYPE ULN-2001A SCHEMATIC

## 14 to 25 Volts PMOS Applications

The Type ULN-2002A Darlington array was specifically designed for use with 14 to 25 volt PMOS devices. Each input has a 7 V Zener diode and a 10,500 ohm resistor (nominal values) to limit the input current to within the capability of most PMOS of the type specified. The basic circuit diagram is shown in Figure 5 with a typical application. Note that there are no pull-down resistors or other external discrete components necessary. The incorporation of the Zener diode also results in excellent noise immunity for this array.

## TTL and CMOS INTERFACE

The ULN-2001A and ULN-2002A allow only a limited number of input options. Shown in Figure 6 is the basic circuit diagram of the Type ULN-2003A. This device has a series base input resistor to each Darlington pair, and thus allows operation directly with TTL or CMOS logic operating at a supply voltage of 5 V (or 12 V CMOS using FET characteristics).

A guarantee of 200 mA output sink current capability (saturated) is provided with the worse case TTL logic 1 level of 2.4 volts. Low-power Schottky-clamped TTL logic is generally specified to have a minimum Vout of 2.7 volts. The ULN-2003A is guaranteed to sink 250 mA under this input condition. With the more typical input of 3 volts, the ULN-2003A Darl ington pair will sink at least 300 mA in the "ON" state.


Figure 4
TYPICAL P-CHANNEL DRAIN CHARACTERISTIC


Figure 5
TYPE ULN-2002A SCHEMATIC AND APPLICATION

TTL totem pole outputs are not specified between the $400 \mu \mathrm{~A}$ logic 1 fanout condition and the maximum output short-circuit current ( 20 to 55 mA for the 7400 series). Between these rather wide limits lies the required ULN-2003A input current. The maximum Type ULN-2003A input current level is specified at 1.35 mA at the extrapolated TTL maximum logic 1 level of 3.85 V .

The ULN-2003A Darlington array will handle a great many interface needs - particularly those beyond the capabilities of TTL buffers. Also shown in Figure 6, is a typical application of the ULN-2003A Darlington array. Of particular interest in this application is an unusual use of the transient-suppression diodes for a non-inductive load. The lamp test feature can of course be used with any of the devices in this series.


Figure 6
TYPE ULN-2003A SCHEMATIC AND APPLICATION

The diodes are designed to handle the same current and voltage as the output transistors. Switching can be accomplished through an ordinary switch or an appropriate power transistor. With the standard $+70^{\circ} \mathrm{C}$ ambient and the most widely used lamps ( 2 No. 327 or 2 No. 387 lamps per output) there is no problem with continuous operation.

## 6 to $\mathbf{1 5}$ Volt CMOS or PMOS Applications

The Type ULN-2004A Darlington array has an appropriate series input resistor (nominally $10.5 \mathrm{k} \Omega$ ) to allow its operation directly from CMOS or PMOS logic outputs utilizing supply voltages of between 6 and 15 V .

Shown in Figure 7 is a typical application of this array. Although the discrete output buffer could be used to increase the output capability of any of the devices in this series, this is most often done by paralleling outputs as was described earlier.


Figure 7
Type ULN-2004A SCHEMATIC AND APPLICATION

## Input Current

The Darlington collector current (output in saturation) at an ambient temperature of $+25^{\circ} \mathrm{C}$, for any input current is the same for all four devices in this series and is shown in the graph of Figure 8. More accurately, the maximum input current for any collector current is described by the equation:

$$
I_{\mathbb{N}(\mu \mathrm{A})}=I_{C(\operatorname{mA})}+140 \mu \mathrm{~A}
$$

where $I_{i n}$ is the input current in microamperes, $I_{C}$ is the collector current in milliamperes, and the figure 140 represents the maximum shunt current through the emitter-base resistors. The typical input current can be described as:

$$
I_{1 N(\mu A)}=0.58 I_{\mathrm{CmmA}^{2}}+110 \mu \mathrm{~A}
$$

where the figure 0.58 is an adjustment for the typical Darlington current gain and the figure 110 represents the typical shunt current.


Figure 8
COLLECTOR CURRENT as a function of input current

The input current as a function of input voltage is shown in Figure 9 for the ULN-2002A, ULN-2003A, and the ULN-2004A. The Type ULN-2001A Darlington array is not shown since input current is more a function of the external circuitry. Systems utilizing either CMOS or PMOS logic should be evaluated for intrinsic current limiting as was shown in Figure 4.


Figure 9
INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE

## Low Available Drive Current Operation

Occasionally, applications featuring minimum available input drive current and a high output load current have shown the Type ULN-2003A and ULN-2004A Darlington arrays to be inadequate for the particular requirement under worst case conditions. This usually results from the restricted drive current available from a TTL or CMOS gate operating from a nominal supply of 5 volts.

Under worst case conditions with a low logic 1 voltage ( 2.4 V ), and a high input resistor value ( $3.51 \mathrm{k} \Omega$ ), the available load current is reduced to only 145 mA . Compounding this problem would be the effect that a high drive current requirement would have on the logic output voltage since that is normally specified at only $400 \mu \mathrm{~A}$. If the gate output is connected to additional logic elements, a minimum logic 1 voltage of 2.0 V must be maintained and at that level the worst case Darlington load current would be reduced to only 31 mA !

A simple solution to this problem is through the use of inexpensive pull-up resistors as shown in Figure 10. The minimum resistor value is determined by the maximum allowable sink current ( 16 mA for TTL, $360 \mu$ A for CMOS), the minimum logic 0 output voltage, and the maximum supply voltage as per the following equation:

$$
R_{p} \geq \frac{V_{s}-V_{\text {out(0) }}}{\text { lout }}
$$

For standard TTL, the minimum value for $R_{p}$ is about $316 \Omega$ with values between $3000 \Omega$ and $5000 \Omega$ being used customarily. Multiple pull-up resistors in a single in-line package are shown in Sprague Engineering Bulletin No. 7041 ; resistors in a dual in-line package are shown in Bulletin No. 7042.

## Conclusion

Since the Series ULN-2000A high-voltage, highcurrent Darlington transistor arrays are quite conservatively designed, the basic product is fully capable of being ordered to higher voltages and/or higher currents than the standard specifications. Presently, parts are available to withstand up to 95 volts on the output. Parts with this higher voltage rating would create a potential for switching loads far in excess of 125 watts! Aside from the higher power handling capability, the higher voltage rating is required for driving plasma or gas-discharge displays.

Although not intended for high power applications, there is also available a Series ULS-2000H with hermetic sealing and an operating temperature range to $+125^{\circ} \mathrm{C}$. These parts are recommended for military and aerospace applications as well as commercial and industrial control applications where severe environments may be encountered.

Cer-DIP, industrial-grade hermetic devices, Se ries ULQ-2000R, are rated for use over the temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, permitting their use in commercial and industrial applications requiring a moderate package power dissipation ( 1 W at $\mathrm{T}_{\mathrm{A}}=$ $+85^{\circ} \mathrm{C}$ ).

All of these Darlington transistor arrays offer a common solution to a great many interface needs. The minimal component count and straightforward printed wiring board layout offer benefits in cost reduction, simplicity of board layout, and savings in space. Other benefits are a reduction in insertion costs, and lower handling and inventory costs than other alternatives. Cost benefits from some of these factors are not very tangible. However, fewer components, less complex boards, etc. usually result in lower system manufacturing costs.


Figure 10
USE OF PULL-UP RESISTORS TO INCREASE DRIVE CURRENT

# INTERFACE IC MOTOR DRIVE APPLICATIONS 

THE INCORPORATION OF LOGIC systems and power drivers into a monolithic integrated circuit requires special skill and experience. Sprague Electric Company has developed such skill, and has long been a leader in solid-state interface technology and devices.
Improved systems reliability and performance, lower component counts, space savings
and cost economy are some of the benefits to be derived from the use of Sprague Interface ICs. An increasing number of these Sprague devices are especially designed for or are easily adapted to motor drive applications. The availability of these devices is especially significant in view of the increasing use of microprocessor-based controls for servo and stepper motors.

## UCN-4202A STEPPER MOTOR TRANSLATOR/DRIVER

THE UCN-4202A will drive permanent magnet (PM) stepper motors rated to 500 mA and 15 V with a minimum of external components required, or, the device may be used as a logic translator to drive discrete high-power transistors or the Sprague UDN-2949Z HalfBridge Motor Driver.
With the MONOSTABLE RC timing pin (Pin 11) tied to $\mathrm{V}_{\mathrm{CC}}(\operatorname{Pin} 16)$ the circuit performs a full-step function. States B and D are stationary states and a separate input pulse is required to move through each of four output states.
The UCN-4202A internal step logic activates one of four output sink drivers to step the load from one position to the next. The logic is activated when the STEP INPUT (Pin 10) is pulled low for at least $1 \mu \mathrm{~s}$ and then allowed to return high. The sequence of states is determined by the DIRECTION CONTROL (Pin 12), either A-B-C-D, or A-D-C-B.

In the double-step mode states B and D are transition states with durations determined by the MONOSTABLE RC timing (Pin 11). Improved motor torque is obtained at double the nominal motor step angle, and motor stability is improved for high step rates.

## RECOMMENDED MAX. OPERATING CONDITIONS


Output Current, lout . . . . . . . . . . . . . . . . . . . . . . . . . . 500 mA
Supply Voltage, $\mathrm{V}_{\mathrm{cc}} \ldots . . . . . . . . . . . . . . . . . . . . . . . .5 .5 \mathrm{~V}$



Timing Conditions - Double-Step Mode


D! MG. NO. A-11,186
NOTE: State B and State D Output pulse duration is typically 11.5 ms, with $R=510 \mathrm{k} \Omega$, and $\mathrm{C}=0.02 \mu \mathrm{~F}$.


L/R DRIVE CIRCUIT
Used to Drive A 12-Volt
500 mA Unipolar Stepper Motor (Double-Step Mode)

Dwg. No. A-11, 187

TYPICAL A-C MOTOR APPLICATION


## UDN-2949Z HIGH-CURRENT BIPOLAR HALF-BRIDGE MOTOR DRIVER

THE UDN-2949Z is a monolithic half-bridge motor driver supplied in a power tab T0-220 style package. The circuit combines sink and source drivers with diode protection, gain and level shifting systems, and a voltage regulator for single-supply operation. The unit is specifically designed for servo motor drive applications using pulse width modulation (chopping).
The chopper drive mode is characterized by a minimum power dissipation requirement while allowing the output to switch currents of 2 amperes. Output d-c current accuracies of better than $10 \%$ at 100 kHz can be obtained.

The UDN-2949Z may be used in pairs (fullbridge) for d-c stepper motor or brushless d-c motor drive applications. High load currents or step rates will usually require an external ground clamp diode ( 1 N 4000 ) connected at the output of each device.

The UDN-2949Z power driver may be also be used in stepper motor bipolar bridge drive circuits for example, with the Sprague UCN-4202A Stepper Motor Translator/Driver, as shown.

## RECOMMENDED MAX. OPERATING CONDITIONS



Continuous Output Current, Iout $\ldots \ldots . . \ldots \ldots . . . \pm 2.0 \mathrm{~A}$


FULL-BRIDGE D.C SERVO MOTOR APPLICATION


SINGLE-WINDING D-C OR STEPPER MOTOR

## TYPICAL 3-PHASE BRUSHLESS D.C MOTOR DRIVE



## ULN-3701Z and ULN-3702Z HIGH-CURRENT DRIVERS

THESE HIGH-CURRENT drivers are suitable for driving d-c motors rated to $\pm 2.5 \mathrm{~A}$ and 18 $\mathbf{V}$ with minimum external components. Internal voltage, current, and temperature shut-down circuitry protect these devices under the most severe operating conditions. The ULN-3702Z does not include the high-voltage shutdown, allowing operation with supply voltages up to 28 V . The high-gain, high-impedance operational amplifier configuration allows many specialized input, output, and feedback arrangements.


# SERIES ULN-2800A DARLINGTON ARRAYS and SERIES UDN-2980A HIGH-CURRENT SOURCE DRIVERS 

TTHE COMBINATION of separate 8-channel source and sink driver ICs provides a single or twin motor drive interface solution for "crossover" currents which may occur during switching transitions. No timing provisions are necessary provided the external resistance limits "crossover" currents to the maximum specified for the ICs $( \pm 500 \mathrm{~mA})$.

Flyback voltage should not exceed the recommended $\mathrm{V}_{\mathrm{S}}$ level $(+35 \mathrm{~V}$ or +50 V ). With a UDN-2982A/ULN-2803A combination and a +24 V supply the flyback voltage should not exceed $+35 \mathrm{~V}\left[\mathrm{~V}_{\mathrm{S}}(\max )+\mathrm{V}_{\text {Zener }}(\max )+\right.$ $\left.\mathrm{V}_{\text {clamp }}(\mathrm{max}) \leq 35 \mathrm{~V}\right]$.

Single motor drives may be accomodated by paralleling both inputs and outputs of each IC
$\left(\max \mathrm{I}_{\mathrm{OUT}}= \pm 1.0 \mathrm{~A} ;\right.$ DIP rating allows $\approx 350$ mA max).

Stepper motor bridge driver circuits using techniques such as that illustrated below should achieve greater reliability and space economy, cost reduction and improved performance.

RECOMMENDED MAX. OPERATING CONDITIONS
Supply Voltage, VS UDN-2982A and ULN-2803A . . . . . . . . . . . . . . . . . . . 35 V
UDN-2982A and ULN-2823A . . . . . . . . . . . . . . . . . . . . 50 V
Peak Output ( 100 ms ), I Iop . . . . . . . . . . . . . . . . $\pm 350 \mathrm{~mA}$
Continuous Output Current, Iout
Single Motor . ............................... $\mathbf{\pm} 300 \mathrm{~mA}$
Independent Operation Twin Motors . . . . . . . . . $\pm 300 \mathrm{~mA}$
Simultaneous Operation Twin Motors . . . . . . . . . $\pm 150 \mathrm{~mA}$

UDN-2982A and ULN-2803A Twin Motor Combination


## UDN-2580A SOURCE DRIVER

THE UDN-2580A SOURCE DRIVER serves as a direct interface from the Cybernetic Micro Systems CY500 Motor Controller, utilizing paralleled inputs and outputs. This IC is most useful with supplies of up to -35 V . A selected version (UDN-2580A-1) is available for operation to -50 V .

RECOMMENDED MAX. OPERATING CONDITIONS
Output Voltage, $\mathrm{V}_{\mathrm{CE}}$ $35 \mathrm{~V}^{*}$
Output Current, I IOUT $-350 \mathrm{~mA}$
*Referenced to -V (+5 V and -30 V shown)

## UDN-2845B and UDN-2846B QUAD DRIVERS

THESE QUAD DRIVERS are designed to handle high current loads operating from negative supplies. The d-c motor interface shown uses external diodes for clamping and commutation. A $10 \mu \mathrm{~s}$ interval between input transistions is recommended to prevent "crossover'' current damage to the IC.

RECOMMENDED MAX. OPERATING CONDITIONS

Output Current, I I
Supply Voltage, $\mathrm{V}_{S}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . 5.0 V
Input Voltage, $\mathrm{V}_{\text {IN }}$
UDN-2845B 5.0 V

UDN-2846B . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 12 V


## UCN-4401A and UCN-4801A BiMOS LATCH/DRIVERS

THESE HIGH-VOLTAGE, high-current latch/drivers are comprised of four or eight CMOS data latches, a Darlington transistor driver for each latch, and CMOS control circuitry for the common CLEAR, STROBE, and DUTY CYCLE CONTROL functions. Data bits can be sent to the latch/drivers at rates from 500 $\mathrm{kHz}\left(\mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}\right)$ to $1 \mathrm{MHz}\left(\mathrm{V}_{\mathrm{DD}}=12 \mathrm{~V}\right)$.

Microprocessor power can be utilized more effectively in motor drive systems incorporating UCN-4401A or UCN-4801A latch/drivers. The appropriate motor windings can be activated (usually at millisecond rates) while the microprocessor spends nearly $100 \%$ of its time performing other functions.

A full-step drive scheme implemented with the 4-latch UCN-4401A provides 350 mA for each output. The 8 -latch UCN-4801A may be used for systems operating more than one motor, with 300 mA available for each output.
recommended max. operating conditions

Output Current, lout ............................. 350 mA
Supply Voltage, $V_{D D} \ldots \ldots \ldots \ldots \ldots \ldots \ldots . . . .15 \mathrm{~V}$
Input Voltage, $\mathrm{V}_{\mathrm{IN}} \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots . . . \mathrm{V}_{\mathrm{DD}}$



# EXPANDING THE FRONTIERS OF IC INTERFACE FOR ELECTRONIC DISPLAYS 

## INTRODUCTION

The original monolithic high-voltage/high-current power drivers from Sprague were capable of sustaining 100 V and sinking load currents of 250 mA on each of four outputs. That 1970 peripheral driver capability has since been expanded and improved on to solve many of the most difficult display interfaces. Our newest devices are rated for operation to 130 V , sourcing or sinking to 1.5 A , and as many as eight drivers per package (not all together) with inputs for TTL, Schottky TTL, DTL, CMOS, and PMOS.

## LAMP (INCANDESCENT) INTERFACE

Utilizing marketing inputs that related to existing hybrid interface circuits, a group at Sprague designed and manufactured monolithic ICs which initially were largely used for aircraft indicator lamp interface. Although not widely known, these quad driver units were developed quite independently (and simultaneously) to the ubiquitous TI 75451 series of high-speed, low-voltage peripheral drivers. A concentration upon circuit design factors, improvements in DIP packaging (copper alloy lead frames), and tighter, tougher control of diffusion-related
parameters has allowed the manufacture of quad power drivers rather than the dual mini-DIPs offered by TI.

An increased awareness for improvements in reliability and space and power reductions provided a rather successful military market for Sprague lamp and relay interface; early success was evident in military aircraft indicator lamp interface, a tough application for TTL type ICs due to severe inrush currents resulting in secondary breakdown during "turn on". The increased current sinking capability of the Sprague ICs offers a solution to lamp interface that usually obviates the need for "warming" resistors (across the output) which slightly warm the lamp filament and thus minimize problems associated with cold lamp filaments.

The relay driver types of Sprague IC drivers (and other similar transient-protected ICs) are somewhat more useful than the so-called general purpose types, since the diode common terminal may be switched for a system lamp test. As shown in Figure 1, only a single connection to each DIP is required.


Figure 1

The high current-sinking capability of the Sprague ICs allows such loads as the \#327 or \#387 lamps (usually two in parallel - 28 V at 40 mA each) to be driven without difficulty of secondary breakdown. The device beta will usually not allow sinking of the 10 to 13 times (nominal value) inrush current of cold lamps; but the lamp rapidly reaches a current level within the device output limitations (Figure 2 shows current as a function of time for a single \#327 lamp). Sustaining this instantaneous inrush current and its peak power has been a key element in the success of many lamp interface circuits.

## GAS DISCHARGE DISPLAY ICs

Early in 1972, Sprague successfully produced its first high-voltage IC designed for gas discharge displays - a five channel, 130 V unit for cathode (segment) interface. Subsequently, other circuits, both cathode and anode drivers, were produced; most of which were used in calculator applications with the Burroughs Panaplex ${ }^{\circledR}$ II. In Figure 3 is shown a display interface system utilizing the UHP481 and UHP-491 display drivers, associated thickfilm networks, and discretes. This was a step forward, but still required external discrete components.

Through a collaborative effort begun late in 1973 between Sprague Electric and Burroughs Corp. a newer, more efficient interface scheme evolved. Featured in "Electronic Displays '75", this series of monolithic IC interface devices for the high-voltage gas discharge panels has been one of the trailblazers in the world of display interface ICs. Intended for use in multiplexed display systems, these ICs present one of the easiest and least expensive solutions to a


Figure 2
difficult interface problem. A combination of highvoltage bipolar techniques with thin-film resistor technology (circuit resistors sputtered over the IC dielectric) has provided both digit (anode) and segment (cathode) interface.

To facilitate a minimum component interface, a split supply ( $\pm 100 \mathrm{~V}$ ) is employed to allow d-c levelshifting (rather than capacitors or> $\mathbf{2 0 0} \mathrm{V}$ transistors) and both digit and segment drivers incorporate all pull-up, pull-down, current limiting, off-bias reference, etc. which were formerly required in discrete and/or hybrid systems. With the combination of the digit and segment drivers (each capable of withstanding 120 V ), the split power supply approach affords PN diode IC technology suitable for driving a display usually requiring a 180 V minimum ionization voltage (equivalent to $\pm 90 \mathrm{~V}$ in the split system).

The use of the Series UDN-6100/7100A gas discharge display drivers shows the need for only two monolithic ICs for displays of up to eight digits and eight segments as shown in Figure 4. Systems requiring digit or segment counts greater than eight employ additional driver ICs, and with the exception of the Type UDN-7180A segment driver, the segment ICs all have outputs with internal current-limiting resistors for the display segments. The UDN-7180A device, for reasons of package power dissipation and/or dissimilar segment currents (certain 14 or 16 segment alphanumeric panels) can also be used, but must have external, discrete current-limiting resistors.


Figure 3


Figure 4

Higher current applications are difficult for both programmable current and switching type display drivers. Segment currents beyond 2.5 or 3 mA present package power dissipation limitations to most dual in-line packages. By using external resistors, the Type UDN-7180A driver allows segment currents of up to 14 mA .

The transistor switch with current-limiting resistor scheme used in Sprague gas discharge display drivers
also minimizes problems associated with gas panel arcing which can destroy programmable current circuits. Some of the gas display manufacturers recommend the use of series resistors in each segment line to prevent destruction to the semiconductor interface circuit should such a panel arc occur. Without these series resistors (internal thin-film resistors in Sprague devices) the IC can be destroyed by the high voltage and resulting high current should the panel voltage drop to a very-low level during an arc.

## LED INTERFACE

With the obvious abundance and variety of LED interface integrated circuits it would seem unlikely that there are still systems in search of an IC hardware solution to further minimize cost, component count, space, etc.; but this is definitely the case. The deficiencies are chiefly related to the limited number of current-sourcing circuits and/or highcurrent drivers.

The efficiency of LED displays has improved, but with the larger digits (up to $1^{\prime \prime}$ presently) most of the IC drivers are unable to switch the higher currents required in multiplexed systems. The rule-of-thumb generally applied uses the suggested d-c current multiplied by the number of digits in the display. For example, a multiplexed display of 160 mA peak current will give approximately the same light intensity output as a steady 20 mA in each of eight digits. Of particular difficulty is the switching of currents associated with the lower efficiency yellow and green LEDs. Sprague has provided monolithic integrated circuit solutions to applications requiring segment currents of 350 mA and digit currents of up to 1.5 amperes!

Many of the Sprague ICs used in high-current LED applications were originally designed for use with electro-mechanical loads (relays, solenoids, motors, etc.) although the high-voltage ratings of the drivers are obviously not a concern. A combination of highcurrent, high-voltage Darlington drivers is shown in Figure 5.

The ULN-2074B source driver is utilized as a modified emitter-follower. Through the use of discrete diodes in the common collector line, allowing the base to be switched to a potential higher than the collector, it is then possible to obtain a saturated output. This prevents the usual emitterfollower problems associated with gain, the MOS output impedance, and power. It is also possible to now better define the voltage at the emitter output and to then provide suitable segment current-limiting resistors for the LEDs.

The ULN-2002A sink driver is a high-current Darlington array with the capability of switching multiplexed LEDs with an available limit of 155 mA for each of the seven drivers when used at a $100 \%$ duty cycle. Even the more inefficient yellow or green LEDs can be driven with higher output currents at lower duty cycles ( 400 mA at a $28 \%$ duty cycle).


Figure 5


Figure 6

A new eight-channel source driver is shown as a digit switch for common anode LEDs in Figure 6. The Series UDN-2980A drivers will handle output currents to a maximum of 500 mA . Two basic versions of the driver will allow interface from TTL, Schottky TTL, DTL, PMOS, and CMOS levels. Other versions of the ULN-2003A driver are also available for use with the various logic levels.

Of the three sink drivers shown, the ULN-2003A is probably the better choice from a standpoint of both pinout and component count. It also has straightforward in-out pinning. The ULN-2031A and ULN2081A devices offer lower cost. They are also interchangeable from a pinning aspect although the output ON voltage will be dissimilar.

A common-cathode LED configuration is shown in Figure 7 for currents of up to 1.5 A per digit! A series UDN-2980A source driver is used to switch the segment side, the ULN-2064B or ULN-2074B to switch the digit side. As has been shown with Figure 5, the IC package power dissipation must be considered with high-current applications.

The three examples that have been shown for LED interface represent only a very-small portion of the total applications area. The high-current capabilities and high gain of the Sprague drivers represent potential solutions to many difficult LED display systems alphanumeric, seven-segment, or matrix; commoncathode or common-anode; continuous or multiplexed.

## A-C PLASMA DISPLAY INTERFACE

Plasma displays, such as those manufactured by National Electronics/NCR (USA) and NEC or Fujitsu (Japan), all have one common element with their gas discharge cousin - both types use a neon gas mixture. The plasma panels emit an orange glow when switched at rather high frequencies, and light output intensity is a function of frequency. The a-c term for the plasma display is something of a misnomer since these panels actually operate from a toggled d-c supply (usually in the area of 20 kHz ).

The panel is basically a neon-filled capacitor, and has plates (electrodes) which are covered with the dielectric - between which is the neon mixture. Switching this capacitive load presents a problem
with high peak currents in addition to the older problem of the high voltages which are associated with gas displays. Drive circuits use supply voltages of 150 to 260 V (depending on unipolar or bipolar drive), and the semiconductors used must switch instantaneous currents in the order of several hundred milliamperes for the larger displays.

Several high-voltage, high-current arrays made at Sprague Electric can provide an answer to one side of the a-c plasma display interface. The Series ULN2020A Darlingtons are rated at 95 V while the Series UHP-500 power drivers are rated at 100 V . They are both able to handle the application shown in Figure 8 (a basic d-c, non-multiplexed clock interface rather than a more complex multiplexed system). The ULN-2022A is specifically designed for 14 to 25 V PMOS logic levels while the UHP-506 is intended for
use with TTL.
The high-current diodes that are internal to the Sprague arrays are utilized in the unipolar drive scheme connected to a suitable OFF reference. In one POS application, a set of 14 ULN-2023A Darlington drivers replaced more than 400 discrete components. The cost and space savings in such a machine are considerable, and a very complex printed wiring board was greatly simplified.

Further improvements in interface and plasma displays will no doubt evolve, and thus benefit all concerned - display and interface vendor along with the end user. Plasma displays are well-suited to custom panels (particularly those with various sizes of characters) and with improvements in IC breakdown voltages some further simplification of interface should evolve.


Figure 7


Figure 8

## FLUORESCENT DISPLAY INTERFACE

Although the vast majority of fluorescent displays are directly driven from MOS logic (handheld and low-cost desk calculators), there is an emerging need for interface integrated circuits for use with the larger characters (higher currents) and the higher voltages coming into use. These blue-green display panels originated in Japan, and the manufacturers are quite aggressively pursuing markets such as POS systems, clocks, cash registers, appliances, automotive displays, etc. Larger and/or more complex styles are being made, including displays with alphanumeric capability (a starburst 14 or 16 -segment pattern).

Modest voltage capability ( 60 or 70 volts) is all that is required of a semiconductor device to drive these panels, and the currents are in 20 to 30 mA region. These electrical requirements are well within the capability of many gas discharge digit drivers. In Figure 9, the UHP-491 is shown used with pulldown resistors connected to each output. When both the segment (equivalent to a vacuum tube anode) and the digit (controlled by the grid) are switched sufficiently positive with respect to the cathode (filament), the appropriate display digit/segment are energized.

Another multiplexed configuration is shown in Figure 10; the difference being that a push-pull type of MOS output is in use, and the pull-down rail does not allow the UHP-491 substrate, $\mathrm{V}_{\mathrm{DD}}$, and output potentials to be the same. The substrate and output are tied to the most-negative rail, while the VDD terminal connects to the -12 V line for the MOS.

Since these solutions using the older gas discharge digit driver circuits require the use of appropriate pull-down resistors, either in discrete or thick-film network form, a more suitable solution employs the circuit shown in Figure 11. The UDN-6118/28A devices are designed specifically for use with fluorescent displays and include internal pull-down resistors so that up to eight segments and eight digits will require only two packages and a greatly simplified power supply. The Type UDN-6118A driver is compatible with TTL, Schottky TTL, DTL, and 5 volt CMOS. The Type UDN-6128A driver is for use with 6 to 15 volt PMOS or CMOS logic.

The future of fluorescent displays looks rather strong, particularly if competition further reduces prices. For the moment at least, these displays will not seriously tax the capability of IC interface except, perhaps, from a price/cost standpoint.


Figure 9


Figure 10

## HOT WIRE READOUTS

Although hot wire readouts could easily be placed in the incandescent category, their application in multidigit, multiplexed display systems more closely resembles LED circuit operation. Since hot wire displays will conduct current in either direction, isolation diodes are required to prevent sneak paths
from partially turning ON unaddressed segments. Compare the typical hot wire display of Figure 12 with the LED display of Figure 6. The availability of a suitable, inexpensive diode array would be of considerable asset in multiplexed hot wire systems.


Figure 11


Figure 12

The hot wire readouts are available in both sevensegment and alphanumeric (16-segment) versions and are quite well-suited to high ambient light applications. They do not wash out in sunlight, although their reliability diminishes with the higher
currents required in brightly lighted applications. As described, multiplexed schemes can be cumbersome because of the great number of discrete diodes required. One avionics system using a 16 -character, 16-segment alphanumeric panel required 256 discrete diodes.


Figure 13

## GLOW TRANSFER - BAR GRAPH \& MATRIX PANELS

Neon-based display technology has shifted into many new market areas. The Burroughs Self-Scan ${ }^{\circledR}$ is a solution to many alphanumeric applications; the newer bar graph is a solid state replacement for analog instrumentation. Both use the glow transfer principle of the dot matrix Self-Scan display.

The nominal voltage for this type of panel is 250 V . High-voltage gas discharge drivers (Series UHP-480) or Darlington arrays (Series ULN-2020A) afford a cathode interface to the glow transfer panel. With a typical display current of 3 to 5 mA , the gas discharge drivers are perfectly adequate. For higher current applications, the Darlington arrays are a solution.

As illustrated in Figure 13, the bar graph cathode is easily driven with a Series UHP-480 driver. Signal level shifting is inexpensively accomplished with capacitors; the OFF reference, pull-up, and pulldown is done with a few discretes. The anodes are driven with two discrete transistors ( $\mathrm{BV}_{\mathrm{CES}} \geq 120 \mathrm{~V}$ ). By utilizing a negative supply, the level shifting is easily done in the cathode side. If a positive supply were used, relatively complex d-c level shifting would be required in the anode side. The few discretes necessary in the circuit shown are generally a viable solution when faced with cost and space parameters for the system.

## SUMMARY

The phenomenal growth in display technology has largely come as a result of the electronic calculator, and electronic displays will pervade all our lives in an ever-increasing number of products. The use of digital displays in appliances, gasoline pumps, electronic games (even pinball machines), etc., etc., etc., will also require that a continuing evolution of interface integrated circuits meet the challenges of higher brightness, increased currents, improved reliability, and lower system costs.

Both the display and semiconductor industries have demonstrated that they will meet the challenges of today, and these challenges then become routine with tomorrow.

## SPRAGUE HIGH-POWER INTERFACE ICs

## Introduction

Spurred on by the tremendous impact of the microprocessor, solid state electronics is well into its ' 3 rd' revolution. Increasingly the hardware solutions of past circuit designs have become 'software' ( $\mu \mathrm{P}$ ) resolutions; and with increasing necessity for newer, superior, lower cost components to complete the system. To be effective, the $\mu \mathrm{P}$ and other custom LSI counterparts must rely on interface from their low level logic to high-voltage/high-power loads.

To further augment this ' 3 rd' revolution, Sprague continues to introduce new, high performance interface; ICs which are designed to overcome the large numbers of discretes very often required in such systems. New functions are becoming available along with increased power handling capability, high voltages, etc. The units covered in this paper are:

## Series UDN-2840B Quad 1.5 A Switches UDS-5790H/5791H Quad PIN Diode Interface UDN-2580A NMOS Compatible 8-Channel Source Driver

## Series UDN-2840B QUAD 1.5 A SWITCHES

This series originated from a requirement to provide a monolithic interface for electronic discharge printers; subsequently other functions have been provided from the basic chip design. Three basic products make up the series, but by providing both 5 V logic compatibility and $12-15 \mathrm{~V}$ MOS compatibility, the series contains a total of six types (see Table 1).

Types UDN-2841B and UDN-2842B are intended for sinking current to a negative supply rail; an example of this is the electronic discharge or electrosensitive printer. Both devices are capable of sinking 1.5 A in each output and standing off -50 volts. A typical electrosensitive printer from Japan


Figure 1
will require -35 to -40 volts and peak currents of approximately 1 A (usually at a very low duty cycle).

Type UDN-2843B and UDN-2844B are sourcing circuits capable of switching the ground side of a load which may be connected to a negative supply of up to -50 volts. These types are for general purpose applications such as motors, solenoids, relays, filaments, etc. to the maximum output current of 1.5 A each.

Types UDN-2845B and UDN-2846B are combination sourcing/sinking devices. The four outputs are broken into source (2) and sink (2) for possible uses as a bidirectional or bridge type driver. Primary applications are $\mathrm{d}-\mathrm{c}$ and stepping motor drive. The UDN-2845B has two sink outputs from the UDN2841 B and two source outputs from the UDN-2843B, and the UDN-2846B combines the UDN-2842B and UDN-2844B types for MOS compatibility.

All devices (basic schematic Figure 1) are specified to have a minimum collector-emitter sustaining voltage of 35 volts; this is specified at 100 MA and until recently has not been a specification for monolithic circuits. Sprague Electric ICs are increasingly being characterized in a manner to provide the maximum useful information for the designer, but without getting bogged down in superfluous device specifications.

# Table 1 SERIES UDN-2840B 1.5 A QUAD 

| Type | Iout | Vout (OFF) | Outputs |  | Compatibility |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | TTL, DTL |  |
|  |  |  | Sink | Source | 5 V MOS | 10-15 V MOS |
| UDN-2841B | 1.5 A | -50 V | 4 |  | x |  |
| UDN-2842B | 1.5 A | -50 V | 4 |  |  | x |
| UDN-2843B | 1.5 A | -50 V |  | 4 | x |  |
| UDN-2844B | 1.5 A | -50 V |  | 4 |  | x |
| UDN-2845B | 1.5 A | -50 V | 2 | 2 | x |  |
| UDN-2846B | 1.5 A | -50 V | 2 | 2 |  | x |

## APPLICATIONS

UDN-2841 Electrosensitive Printers, Motor Drives, General Purpose High-Current UDN-2842 Electrosensitive Printers, Motor Drives, General Purpose High-Current UDN-2843 Motor Drive, Solenoids, other General Purpose High-Current Loads UDN-2844 Motor Drive, Solenoids, other General Purpose High-Current Loads UDN-2845 Bidirectional D-C and Stepping Motors, Other High-Current Loads UDN-2846 Bidirectional D-C and Stepping Motors, Other High-Current Loads


When switching inductive loads, the output transistor should be protected by a suitable clamping technique. The simplest approach is to use diode clamps to the supply; in Figure 2A the UDN$2841 / 42 \mathrm{~B}$ uses a discrete diode on each output. Also in Figure 3A and Figure 4, a straight diode clamp is shown for the UDN-2843/44B (Figure 3A) and for the UDN-2845/46B (Figure 4).

For improved turn-off, it may be possible to use a combination diode/Zener diode scheme; in Figures 2 B and 3B the Zener diode will allow the flyback voltage to rise above the supply voltage, thus speeding up the turn-off of the load. An appropriate


Figure 2A


Figure 3A
resistor value might be also substituted; a 1.A load operating with a $15 \Omega$ resistor will produce similar results to a 15 V Zener diode. In Figure 5, the combination Zener/clamp diode is shown for a 'bridge' configuration such as Figure 4.

The allowable output current and duty cycle as a function of the number of drivers activated is shown in Figure 6A. This graph is for a $+70^{\circ} \mathrm{C}$ ambient and will insure that the device junction temperature will not exceed a $+150^{\circ} \mathrm{C}$ level. Figure 6 A is for the ' $B$ ' package without any heat sinking; package rating is $45^{\circ} \mathrm{C} / \mathrm{W}$ or a derating of $22.2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ for this copper alloy plastic DIP.


Figure 2B


Figure 3B

Figure 4


Figure 5


UDN 284I-2846B


Figure 6A

UDN 2841-46B


Figure 6B

Through the use of a Staver V-7 heat sink, the package rating may be improved nearly twice that of Figure 6 A ; the rating of this package with the V-7 heat sink drops to a maximum of $27.5^{\circ} \mathrm{C} / \mathrm{W}$ or a derating of $36.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$. In figure 6 B the allowable output current and duty cycle at $+70^{\circ} \mathrm{C}$ with the addition of the Staver V-7 heat sink is shown. Both Figures 6A and 6B assume worst case limits of $\mathrm{V}_{\mathrm{ON}}$, IS, DIP rating, etc.

No doubt other applications will arise in the future, but these figures are representative of power interface applications which may be simplified through the use of these Sprague power integrated circuits to replace discrete components. Additionally, cost and space reductions should be achieved with the Series UDN-2840B quad 1.5 A switches.

## UDS-5790H and UDS-5791H Quad Peripheral Drivers for PIN Diodes

These monolithic, high-voltage ICs are a natural evolution from the several years of Sprague expertise with high-voltage and high-current power and display ICs. Designed for driving PIN diode phase shifters for radar antenna systems, this quad 300 mA
offers a new high in breakdown voltage ( 120 V ) for monolithic power/peripheral drivers.

Supplied in a fully hermetic 16-lead, side-brazed ceramic DIP, the PIN diode drivers are subjected to the screening procedures specified in MIL-STD-883 method 5004, class B, paragraphs 3.1.1 through 3.1.6. Also made available is a 168 hour burn-in per method 1015, condition $A$ if so required and specified.

In Table 2, the Absolute Maximum Ratings and the Recommended Operating Conditions are specified. The 5.0 V (nom) supply allows the use of the UDS- $5790 / 91 \mathrm{H}$ with TTL, LS TTL, DTL, and 5 V CMOS. The UDS-5790H is a non-inverting type while the UDS-5791H is an inverting type which more frequently corresponds to the discrete or hybrid circuits in use.

Figures 7A and 7B indicate the device pinouts; the in/out configuration tends to simplify PCB layouts and the outputs are separated (isolated) from the inputs. All pins labelled $\mathrm{R}_{\mathrm{X}}$ require a discrete resistor to determine base current for the output NPN; suitable external resistors should be based upon the minimum output transistor gain of 30 (across the full operating temperature range).

## Table 2

## ABSOLUTE MAXIMUM RATINGS over free-air operating temperature range

| Supply Voltage, $\mathrm{V}_{\mathrm{Cc}}$ | 6.0 V |
| :---: | :---: |
| Supply Voltage, $\mathrm{V}_{\mathrm{EE}}$ | -6.0 V |
| Input Voltage, $\mathrm{V}_{\text {IN }}$ | $\mathrm{V}_{\mathrm{cc}}$ |
| Output OFF-State Voltage, $\mathrm{V}_{\text {OFF }}$ (ref. $\mathrm{V}_{\mathrm{EE}}$ ) | $+120 \mathrm{~V}$ |
| Output ON-State Current, $\mathrm{I}_{\text {ON }}$ | 500 mA |
| Operating Ambient Temperature Range, $\mathrm{T}_{\mathrm{A}}$ | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Storage Temperature Range, $\mathrm{T}_{5}$ | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

## RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :---: | :---: | :---: | :---: | :---: |
| Supply Voltage, $\mathrm{V}_{\text {cc }}$ | 4.0 | 5.0 | 5.5 | V |
| Supply Voltage, $\mathrm{V}_{\mathrm{EE}}$ | -1.5 | -3.0 | $-5.5$ | $V$ |
| Output ON-State Current, ION |  |  | 300 | mA |
| Operating Ambient Temperature Range, $\mathrm{T}_{\mathrm{A}}$ | -55 | $+85$ | +125 | ${ }^{\circ} \mathrm{C}$ |



Figure 7A

Use of the external resistors minimizes system and package dissipation and junction temperature, while allowing greater output current and/or duty cycles under any ambient temperature. Control of the base drive is enhanced; and the device $\mathrm{V}_{\mathrm{ON}}$ specifications are guaranteed over the entire $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ temperature range - with only an overdrive of $25 \%$. A PIN diode current of 300 mA requires a resistor value calculated to provide an output NPN base current of 12.5 mA to adequately insure saturation, even at $-55^{\circ} \mathrm{C}$.


Figure 8


Figure 7B

In Figure 8 the circuit diagram for the UDS-5790H non-inverting type is shown; use of a grounded-base input stage is employed. For the UDS-5791H (inverting) type in Figure 9, a common emitter input is utilized. Both types specify the maximum pre-driver collector voltage so that an appropriate resistor ( $\mathrm{RX}_{\mathrm{X}}$ ) may be chosen for the combination of required output load current and supply voltages in use.


Figure 9

For a calculation of the necessary maximum resistor value, it is necessary to use the following information:

1. Output load current, IOUT
2. Minimum positive supply voltage, VCC
3. Minimum negative supply voltage, $\mathrm{V}_{\mathrm{EE}}$
4. Minimum output NPN gain, hFE
5. Maximum predriver collector voltage, $\mathrm{V}_{\mathrm{X}}$

To make an actual calculation, the nominal supply voltages will be used; but the output current, gain, and predriver voltage will be in accordance with the specifications.
$R_{X}=\frac{\left(V_{C C}-V_{E E}\right)-V_{X}}{\frac{I_{O U T}}{h_{F E}} \times 1.25}$
$R_{X}=\frac{(5.0 \mathrm{~V}+3.0 \mathrm{~V})-1.5 \mathrm{~V}}{300 \mathrm{~mA} \div 30) \times 1.25} \leq 510$ (Std value)

For an output current of 150 mA , the solution is:
$R_{X}=\frac{(5.0 \mathrm{~V}+3.0 \mathrm{~V})-1.5 \mathrm{~V}}{(150 \mathrm{~mA} \div 30) \times 1.25} \leq 1000(\mathrm{Std}$ value)
The hermetic dual in-line package is rated at $90^{\circ} \mathrm{C} / \mathrm{W}$ or a derating factor ( GOja ) of $11.1 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$; the allowable power dissipation for this device is shown in Figure 10. The maximum junction temperature should not exceed $+150^{\circ} \mathrm{C}$ (the zero power level of Figure 10).

The maximum power dissipation is a combination of $\mathrm{V}_{\mathrm{CE}}-I_{O U T}, I_{C C} \times\left(\mathrm{V}_{\mathrm{CC}}-\mathrm{V}_{E E}\right)$, and $\mathrm{V}_{\mathrm{X}} \times$ IX . For a 300 mA load at $+85^{\circ} \mathrm{C}$, the power is:
(1) $0.7 \vee \times 300 \mathrm{~mA} \leq 210 \mathrm{~mW}$
(2) $4.1 \mathrm{~mA} \times 11.0 \mathrm{~V} \leq 45.1 \mathrm{~mW}$
(3) $1.5 \vee \times 12.5 \mathrm{~mA} \leq 18.75 \mathrm{~mW}$ or $\leq 273.9 \mathrm{~mW}$

For an OFF output, the power is:
(4) $115 \vee \times 100 \mu \mathrm{~A} \leq 11.5 \mathrm{~mW}$
(5) $3.4 \mathrm{~mA} \times 11.0 \mathrm{~V} \leq 37.4 \mathrm{~mW}$

Partitioning the PIN phase shifter loads is an effective technique of minimizing the power in any single device. The quad might be used in the manner shown in Figure 11. The appropriate choice will allow all four outputs to be ON continuously without


Figure 10
excceding the package power dissipation rating. The conditions of Figure $11(75 \mathrm{~mA}, 150 \mathrm{~mA}, 225 \mathrm{~mA}$, and 300 mA ) will allow operation at an ambient temperature of $+85^{\circ} \mathrm{C}$ and the chip junction temperature will be below the $+150^{\circ} \mathrm{C}$ upper limit.


Figure 11

The Sprague PIN diode interface drivers are designed to provide a cost saving monolithic solution to phased array radar. Although primarily intended for MII-STD-883 high reliability military and aerospace programs, the units are also available in a commercial package and temperature range (plastic DIP and $0^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ) if required.

## UDN-2580A 8-Channel High-Voltage, High-Current

 Source Driver.This 8-Channel IC design originates from a need to provide an interface from NMOS to high current inductive loads. The device functions like a PNP; but an NPN Darlington has been added to provide suitable current gain. By switching the input low the output is turned ON and the load current is sourced from the compound PNP/NPN/NPN output. Maximum ratings are shown in Table 3.

In Figure 12, the basic circuit diagram is shown; a typical NMOS interface might involve -5 V , GND, and solenoid loads of -20 to -30 V . The UDN2580A affords an interface to these higher voltages and offers high current outputs of -500 mA (max).

As is usually done with devices of this type, the pinout is the in-opposite-out version shown in Figure 13. The unit is packaged in an 18 -lead plastic DIP utilizing Sprague copper alloy lead frame technology


Figure 12
for improved thermal capacity and device electrical performance.

With NMOS logic operating from negative supplies, the interface to high current inductive loads (solenoids, relays, etc.) is depicted in Figure 14. Most NMOS includes depletion load and is capable of pulling the input of the UDN-2580A sufficiently high to turn off the device. For those few instances where either open drain NMOS is to be used, or the depletion load is excessively high, external pull-up resistors may be employed.

Table 3
ABSOLUTE MAXIMUM RATINGS
at $25^{\circ} \mathrm{C}$ Free-Air Temperature for Any One Driver (unless otherwise noted)

|  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | UDN-2580A | UDN-2580A-1 | UDN-2585A | UDN-2588A | UDN-2588A-1 |
| Output Voltage, $V_{\text {CE }}$ | 50 V | 80 V | 25 V | 50 V | 80 V |
| Supply Voltage, $V_{S}$ (ref. sub.) | 50 V | 80 V | 25 V | 50 V | 80 V |
| Supply Voltage, $V_{\text {CC }}$ (ref. sub.) | - | - | 50 V | 80 V |  |
| Input Voltage, $V_{\mathbb{N}}$ (ref. $V_{S}$ ) | -30 V | -30 V | -20 V | -30 V | -30 V |
| Total Current, $I_{\text {CC }}+I_{S}$ | -500 mA | -500 mA | -250 mA | -500 mA | -500 mA |
| Substrate Current, $I_{\text {SUB }}$ | 3.0 A | 3.0 A | 2.0 A | 3.0 A | 3.0 A |

Allowable Power Dissipation, $P_{D}$ (single output) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1.0 W
(total package) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 2.2 w*


*Derate at the rate of $18 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$


Figure 13

Although the UDN-2580A is chiefly intended for high voltage inductive loads, it will help solve highcurrent, low-voltage designs as well. In Figure 15, the UDN-2580A is used as a source driver for

Figure 14

multiplexed common-cathode LEDs; the UDN2580A is a high current segment driver, while the ULN-2068B quad is the high current (1.5 A max) digit driver.

Figure 15



Figure 16

Alternatively, the UDN-2580A may be employed as a digit driver for common-anode LEDs; shown in Figure 16 is the UDN-2580A sourcing current for an cight digit application. Combined with this is the ULN-2804 Darlington array for a segment switch. This pair of units affords an eight digit cight segment solution to high-current MUXed LED or incandescent displays. For most of the IED ap-
plications, it would be necessary to use a supply of 7 to 8 volts to effectively switch the LEDs; thus it makes the UDN-2580A and other high current interface attractive for CMOS applications. The combination of $V_{f}($ LED $)$ and source and sink driver VON preclude the use of such ICs much below the 7 volt level, since some portion of the supply must be across the segment limiting resistor $\left(\mathrm{R}_{\mathrm{L}}\right)$.

It is also possible to employ the UDN-2580A as a predriver for power semiconductors for very highcurrent loads, thus considerably reducing the need for discretes in many MOS-based systems. Shown in Figure 17 A is the UDN-2580A source driver providing base current for a power NPN; with its -350 mA output capability (NPN base drive) a load current of 3 to 5 amps is quite readily available. For higher currents, the use of a power Darlington may be the solution.

For a-c loads, it is possible to use the UDN-2580A source driver for providing gate current for power thyristors. Shown in Figure 17B is an interface to a high current Triac; this is a scheme using a pulse transformer for isolation and some current limiting should be provided.

For allowable duty cycle, output currents, and number of outputs activated, the $+70^{\circ} \mathrm{C}$ limits are shown in Figure 18. This graph assumes worst case


Figure 17A
output voltage, package rating, and $+70^{\circ} \mathrm{C}$ ambient; under these conditions the chip junction temperature will be less than $+150^{\circ} \mathrm{C}$.

## Conclusion

Three new, high performance Sprague interface integrated circuits have recently been developed. They lend to simplify certain system designs while offering size and cost reductions. The UDN-2841B and UDN2842B will greatly simplify an emerging printer technology; the UDS-5790/91H will replace hybrids and discretes for PIN phase shifter arrays; and the UDN-2580A will further augment the use of NMOS LSI in a variety of systems. All of this is the result of customer and sales inquiries along with an understanding of the industry needs for improved power interface ICs. Custom interface designs are also becoming a greater factor, and Sprague Electric will also help to lead the way in solving these problems.


Figure 17B


Figure 18

?

## SECTION 4 - BiMOS AND COMPLEX ARRAY INTERFACE DRIVERS

UCN-4202A Stepper Motor Translator/Driver ..... 4-2
UCN-4401A and 4801A BiMOS Latch/Drivers ..... 4-9
UCN-4805A and 4806A BiMOS Latched Decoder/Drivers ..... 4-12
UCN-4810A 10-Bit Serial-In, Latched Driver ..... 4-16
UCN-4815A BiMOS Latch/Source Driver ..... 4-19
UCN-4821A through 4823A 8-Bit Serial-In, Latched Drivers ..... 4-22
Application Note:
Sprague BiMOS - Muscle for the Microprocessor ..... 4-26

## UCN-4202A STEPPER MOTOR TRANSLATOR/DRIVER

## features

-600 mA Power Drivers
-15 V Sustaining Voltage
-20 V Output Breakdown
-Full-Step or Double-Step Operation

- Single-Input Direction Control
-Power-On Reset
- Transient Suppression Diodes
- Schmitt Trigger Inputs

THE UCN-4202A Translator/Driver is specifically designed for driving small-tomedium permanent magnet (PM) stepper motors rated to 500 mA and 15 V . This monolithic integrated circuit employs a full-step, double pulse drive scheme that produces up to $90 \%$ utilization of the available PM stepper motor torque.

The UCN-4202A is a unique bipolar $\mathrm{I}^{2} \mathrm{~L}$ design containing approximately 100 logic gates, suitable input/output circuitry for TTL compatibility, and 600 mA outputs with internal inductive load suppression. The circuit operates with a minimum of external components, and provides an additional uncommitted driver.

The PM stepper motor is controlled by the integral step logic. To step the load from one position to the next, the STEP INPUT is pulled down to a logic low for at least $1 \mu \mathrm{~s}$, then allowed to return to a logic high. The step logic is activated on the positive-going edge, which in turn activates one of four output sink drivers. The DIRECTION CONTROL determines the sequence of states (A-B-C-D, or A-D-C-B).


DWG. NO. A-11,184

In the full-step mode the MONOSTABLE RC timing pin is tied to $\mathrm{V}_{\mathrm{CC}}$, making states B and D stationary states. A separate input pulse is required to move through each of the four output states.

The UCN-4202A will also perform a doublestep function. In the double-step mode, states B and $D$ are transition states with duration determined by the MONOSTABLE RC timing. Improved motor torque is obtained at double the nominal motor step angle, and motor stability is improved for high step rates.

Higher current ratings, or bipolar operation can be obtained by using the UCN-4202A as a logic translator to drive discrete high-power transistors or the Sprague UDN-2949Z HalfBridge Motor Driver.

## ABSOLUTE MAXIMUM RATINGS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Supply Voltage, $\mathrm{V}_{\text {cC }}$ | 7.0 V | Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ (One Driver) | 0.8 W |
| :---: | :---: | :---: | :---: |
| $V_{K}(\operatorname{Pin} 7)$ | 20V | (Total Package) | 2.0 W* |
| Output Voltage, $\mathrm{V}_{\text {CE }}$ | 20 V | Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Input Voltage, VIN | 7.0 V | Storage Temperature Range, $\mathrm{T}_{5}$ | $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Output Sink Current, Iout | . 600 mA | *Derate $16.6 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+25^{\circ} \mathrm{C}$. |  |

## ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=\boldsymbol{+ 5 . 0} \mathrm{V}$ unless otherwise noted

|  |  | Limits |  |  |  |
| :--- | :---: | :--- | :---: | :---: | :---: |
| Characteristic | Symbol | Test Conditions | Min. | Max. | Units |
| Supply Current | ICC | 2 Drivers ON | - | 85 | mA |

TTL Inputs (pins 1, 9, and 15), TTL Outputs (pins 13 and 14)

| High-Level Input Voltage | $V_{\text {IN(1) }}$ | $V_{C C}=4.5 \mathrm{~V}$ | 2.0 | - | V |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Low-Level Input Voltage | $V_{\text {IN(0) }}$ | $V_{C C}=5.5 \mathrm{~V}$ | - | 0.8 | V |
| High-Level Input Current | $\operatorname{lin(1)}$ | $\mathrm{V}_{\text {CC }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=2.4 \mathrm{~V}$ | - | 40 | $\mu \mathrm{A}$ |
| Low-Level Input Current | $1 \mathrm{IN}(0)$ | $\mathrm{V}_{\text {CC }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=0.4 \mathrm{~V}$ | - | -1.6 | mA |
| Input Clamp Voltage | IIN(CLMP) | $\mathrm{I}_{\mathrm{N}}=-12 \mathrm{~mA}$ | - | -1.5 | V |
| High-Level Output Voltage | $\mathrm{V}_{\text {OUT(1) }}$ | $\mathrm{V}_{\text {CC }}=4.5 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=80 \mu \mathrm{~A}$ | 2.4 | - | V |
| Low-Level Output Voltage | $V_{\text {OUT(0) }}$ | $\mathrm{V}_{\text {CC }}=4.5 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=3.2 \mathrm{~mA}$ | - | 0.4 | V |
| Short-Circuit Output Current | Iout(SC) | $V_{C C}=5.5 \mathrm{~V}$ | - | 38 | mA |

## Second Step Monostable RC Input (pin 11)

| Time Constant | $\mathrm{t}_{\mathrm{RC}}$ |  | 0.95 | 1.3 | $\mathrm{~s} / \mathrm{RC}$ |
| :--- | :---: | :--- | :---: | :---: | :---: |
| Reset Voltage | $\mathrm{V}_{\mathrm{MR}}$ | $\mathrm{R}=200 \mathrm{k} \Omega, \mathrm{I}_{\mathrm{IN}}=25 \mu \mathrm{~A}$ | - | 50 | mV |
| Reset Current | $\mathrm{I}_{\mathrm{MR}}$ | $\mathrm{V}_{\mathbb{I N}}=2.0 \mathrm{~V}$ | 40 | - | $\mu \mathrm{A}$ |

## Schmitt Trigger Inputs (pins 10 and 12)

| Threshold Voltage | $\mathrm{V}_{\text {T }}$ |  | 1.3 | 2.1 | V |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $V_{\text {T- }}$ |  | 0.6 | 1.1 | V |
| Hysteresis | $\Delta V_{T}$ |  | 0.2 | - | V |
| High-Level Input Current | $\underline{I N(1)}$ | $\mathrm{V}_{C C}=4.5 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=2.4 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 5.0 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {CC }}=4.5 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=2.4 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | 40 | $\mu \mathrm{A}$ |
| Low-Level Input Current | IIN(0) | $\mathrm{V}_{\text {CC }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=0.4 \mathrm{~V}$ | - | -1.6 | mA |
| Input Clamp Voltage | ViN(CLMP) | $\mathrm{I}_{\mathrm{IN}}=-12 \mathrm{~mA}$ | - | -1.5 | V |

## Open Collector Outputs (pins 2, 3, 4, 5, and 6)

| Output Leakage Current | $I_{\text {cex }}$ | $\mathrm{V}_{\text {CC }}=5.5 \mathrm{~V}, \mathrm{~K}=0$ pen, $\mathrm{V}_{\text {OUT }}=20 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | - | 500 | $\mu \mathrm{A}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{V}_{\text {CC }}=5.5 \mathrm{~V}, \mathrm{~K}=0$ pen, $\mathrm{V}_{\text {OUT }}=20 \mathrm{~V}, \mathrm{TA}=70^{\circ} \mathrm{C}$ | - | 1.0 | mA |
| Output Saturation Voltage | $V_{\text {CEISAT }}$ | $V_{\text {CC }}=4.5 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=300 \mathrm{~mA}$ | - | 500 | mV |
|  |  | $\mathrm{V}_{\text {CC }}=4.5 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=400 \mathrm{~mA}$ | - | 750 | mV |
|  |  | $\mathrm{V}_{\text {CC }}=4.5 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=500 \mathrm{~mA}$ | - | 900 | mV |
| Output Sustaining Voltage | $V_{\text {CES (SUS) }}$ | $\mathrm{I}_{\text {Out }}=30 \mathrm{~mA}, \mathrm{t}_{\mathrm{p}} \leq 300 \mu \mathrm{~s}$, Duty Cycle $\leq 2 \%$ | 15 | - | V |
| Turn-On Delay | $\mathrm{t}_{\mathrm{pd} 0}$ | $0.5 \mathrm{E}_{\text {in }}$ (pin 10) to $0.5 \mathrm{E}_{\text {out }}$ | - | 10 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $t_{\text {pd } 1}$ | $0.5 \mathrm{E}_{\text {in }}(\mathrm{pin} 10)$ to $0.5 \mathrm{E}_{\text {out }}$ | - | 10 | $\mu \mathrm{s}$ |
| Clamp Diode Leakage Current | $\mathrm{I}_{\mathrm{R}}$ | $\mathrm{V}_{\mathrm{R}}=20 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | $\mathrm{I}_{\mathrm{F}}=500 \mathrm{~mA}$ | - | 3.0 | V |

## RECOMMENDED OPERATING CONDITIONS

| Characteristic | Min. | Typ. | Max. | Units |
| :--- | :---: | :---: | :---: | :---: |
| Supply Voltage, $\mathrm{V}_{\mathrm{CC}}$ | 4.5 | 5.0 | 5.5 | V |
| $\mathrm{~V}_{\mathrm{K}}$ | - | 12 | 13.5 | V |
| Output Voltage, $\mathrm{V}_{\mathrm{CE}}$ | - | - | 13.5 | V |
| Output Sink Current, $\mathrm{I}_{\text {OUT }}$ | - | - | 500 | mA |
| Operating Temperature, $\mathrm{T}_{\mathrm{A}}$ | 10 | 25 | 55 | ${ }^{\circ} \mathrm{C}$ |



IN ms
DWG. NO. A-11,185

## MAXIMUM COLLECTOR CURRENT AS A FUNCTION OF MOTOR TIME CONSTANT AND STEP RATE

Notes: 1. Values shown take into account static d-c losses (VSATIOUT and VCClCC) as well as switching losses induced by inductive flyback through the clamp diodes with $\mathrm{V}_{\mathrm{K}}=12$ volts. Maximum package power dissipation is assumed to be 1.33 watts at $+70^{\circ} \mathrm{C}$. Higher package power dissipation may be obtained at lower operating temperatures.
2. Use of external discrete flyback diodes will eliminate power dissipation resulting from switching losses and will allow the full 500 mA output capability (Output A, B, C, or D and the Driver Output) under all conditions.

## FUNCTIONAL DESCRIPTION

## Power-On Resef

An internal RS flip-flop sets the Output A "ON" with the initial application of power. This state occurs approximately $30 \mu$ s after the logic supply voltage reaches 4 volts with supply rise times of up to $10 \mathrm{~ms} / \mathrm{V}$. Once reset, the circuit functions according to the logic input conditions.

## Step Enable

Pin 9 (Step Enable) must be held high to enable the step pulses for advancing the motor to reach the translator logic clock circuits. Pulling this pin low inhibits the translator logic.

## Step Input

Pin 10 (Step Input) is normally high. The logic will advance one position on the positive transition after the input has been pulled low for at least $1 \mu \mathrm{~s}$. The Step Input current specification is compatible with NMOS and CMOS.

## Direction Control

The direction of output rotation is determined by the logic level at pin 12. If the input is held high the rotation is A-D-C-B; if pulled low the rotation is A-B-C-D. This input is also NMOS and CMOS compatible.

## Output Enable

Outputs A through D are inhibited (all outputs 'OFF') when pin 1(Output Enable) is at high level. This condition creates a potential for wire-ORing of device outputs, or other potential control functions such as chopping or bi-level drive.

## Transient Suppression

All five power outputs are diode protected against inductive transients. However, Zener diode or resistor "flyback" voltage techniques are not allowed.

## Full-Step/Double-Step

Full-Step operation is the most commonly used drive technique. The UCN-4202A is capable of unipolar drive without external active devices, either in a full-step mode (pin 11 Monostable RC tied high), or in a double-step mode (pin 11 connected to RC timing). The double-step mode provides improved torque characteristics, while the specified angular increment is doubled.


Note: State B and State D output pulse duration is typically 11.5 ms when $R=510 \mathrm{k} \Omega$ and $C=0.02 \mu \mathrm{~F}$.

TYPICAL STEPPER MOTORS

| Manufacturer | Model | L/R | Typical <br> Ratings | Step <br> Angle |
| :---: | :---: | :---: | :---: | :---: |
| Eastern Air Devices | LA23ACK-2 | 1.4 ms | $440 \mathrm{~mA} / 12 \mathrm{~V}$ | $1.8^{\circ}$ |
|  | LA23ACY-1 | 1.2 ms | $440 \mathrm{~mA} / 12 \mathrm{~V}$ | $7.5^{\circ}$ |
|  | LA34ADK-6 | 2.6 ms | $530 \mathrm{~mA} / 14 \mathrm{~V}$ | $1.8^{\circ}$ |
| Sigma <br> Instruments | 18-2013D24-F32 | 1.5 ms | $340 \mathrm{~mA} / 12 \mathrm{~V}$ | $15^{\circ}$ |
|  | 18-2013D48-F32 | 1.5 ms | $340 \mathrm{~mA} / 12 \mathrm{~V}$ | $7.5^{\circ}$ |
|  | 20-22200200-F23 | 1.5 ms | $500 \mathrm{~mA} / 12 \mathrm{~V}$ | $1.8{ }^{\circ}$ |
| North American | K82701-P2 | 1.5 ms | $330 \mathrm{~mA} / 12 \mathrm{~V}$ | $7.5^{\circ}$ |
| Phillips | K83701-P2 | 1.5 ms | $330 \mathrm{~mA} / 12 \mathrm{~V}$ | $15^{\circ}$ |
| Superior Electric | M061-FD-301 | 0.8 ms | $440 \mathrm{~mA} / 12 \mathrm{~V}$ | $1.8{ }^{\circ}$ |

## TYPICAL APPLICATIONS



DWG. NO. A-11,187

L/R DRIVE CIRCUIT
Used to Drive A 12 -Volt 500 mA
Unipolar Stepper Motor (Double-Step Mode)

## TYPICAL APPLICATIONS



## TYPICAL APPLICATIONS



Dwg. No. 8-1447
A-C MOTOR DRIVE CIRCUIT

## UCN-4401A and UCN-4801A BiMOS LATCH/DRIVERS

## FEATURES

- High-Voltage, High-Current Outputs
- Output Transient Protection
- CMOS, PMOS, NMOS, TTL Compatible Inputs
- Internal Pull-Down Resistors
- Low-Power CMOS Latches

THESE high-voltage, high-current latch/drivers are comprised of four or eight CMOS data latches, a bipolar Darlington transistor driver for each latch, and CMOS control circuitry for the common CLEAR, STROBE, and OUTPUT ENABLE functions. The bipolar/MOS combination provides an extremely low-power latch with maximum interface flexibility. The UCN-4401A contains four latch/drivers while the UCN-4801A contains eight latch/drivers.

The CMOS inputs are compatible with standard CMOS, PMOS, and NMOS circuits. TTL or DTL circuits may require the use of appropriate pull-up resistors. The bipolar outputs are suitable for use with relays, solenoids, stepping motors, LED or incandescent displays, and other high-power loads.

Both units feature open-collector outputs and integral diodes for inductive load transient suppression. The output transistors are capable of sinking 500 mA and will sustain at least 50 V in the OFF state. Because of limitations on package power dissipation, the simultaneous operation of all drivers at maximum rated current can only be accomplished by a reduction in duty cycle. Outputs may be paralleled for higher load current capability.

The UCN-4401A 4-latch device is furnished in a standard 14-pin dual in-line plastic package. The UCN-4801A 8-latch device is furnished in a 22-pin dual in-line plastic package with lead centers on $0.400^{\prime \prime}(10.16 \mathrm{~mm})$ spacing. All outputs are pinned opposite their respective inputs to simplify circuit board layout.


TYPE UCN-4401A


TYPE UCN-4801A


## ABSOLUTE MAXIMUM RATINGS


Supply Voltage, $V_{D D}$................................................................................................... 18 V


Package Power Dissipation, $P_{D}$ (UCN-4401A)......................................................................1.67 W*
$\qquad$


*Derate at the rate of $16.7 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
${ }^{* *}$ Derate at the rate of $20 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

ELECTRICAL CHARACTERISTICS at $T_{A}=+25^{\circ} C, V_{D D}=5 \mathrm{~V}, V_{S S}=O V$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\mathrm{CE}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {celSAT) }}$ | $\mathrm{I}_{\mathrm{c}}=100 \mathrm{~mA}$ | - | 0.9 | 1.1 | V |
|  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | - | 1.1 | 1.3 | V |
|  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{~V}_{D D}=7.0 \mathrm{~V}$ | - | 1.3 | 1.6 | V |
| Input Voltage | $\frac{V_{\mathbb{I N}_{1(0)}}}{V_{\mathbb{I N}(1)}}$ |  | - | - | 1.0 | V |
|  |  | $V_{\text {DD }}=15 \mathrm{~V}$ | 13.5 | - | - | V |
|  |  | $V_{D D}=10 \mathrm{~V}$ | 8.5 | - | - | V |
|  |  | $\mathrm{V}_{\text {DD }}=5.0 \mathrm{~V}$ (See note) | 3.5 | - | - | V |
| Input Resistance | $\mathrm{R}_{\text {IN }}$ | $V_{D D}=15 \mathrm{~V}$ | 50 | 200 | - | k $\Omega$ |
|  |  | $V_{\text {DD }}=10 \mathrm{~V}$ | 50 | 300 | - | $\mathrm{k} \Omega$ |
|  |  | $\mathrm{V}_{\mathrm{DD}}=5.0 \mathrm{~V}$ | 50 | 600 | - | k $\Omega$ |
| Supply Current | $\begin{aligned} & \text { IDD(ON) } \\ & \text { (Each stage) } \end{aligned}$ | $V_{\text {DD }}=15 \mathrm{~V}$ | - | 1.0 | 2.0 | mA |
|  |  | $V_{D D}=10 \mathrm{~V}$ | - | 0.9 | 1.7 | mA |
|  |  | $\mathrm{V}_{\mathrm{DD}}=5.0 \mathrm{~V}$ | - | 0.7 | 1.0 | mA |
|  | $\mathrm{l}_{\text {D }}$ (off) | All Drivers OFF, All Inputs $=0 \mathrm{~V}$ | - | 50 | 100 | $\mu \mathrm{A}$ |
| Clamp Diode | $\mathrm{I}_{\mathrm{R}}$ | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | - | 50 | $\mu \mathrm{A}$ |
| Leakage Current |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 1.7 | 2.0 | V |

*Note: Operation of these devices with standard TTL or DTL may require the use of appropriate pull-up resistors to insure the minimum logic " l ".

TRUTH TABLE

| $1 \mathrm{~N}_{\mathrm{N}}$ | STROBE | CLEAR | OUTPUT <br> ENABLE | $\mathrm{OUT}_{\mathrm{N}}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | t-1 | t |
| 0 | 1 | 0 | 0 | X | OFF |
| 1 | 1 | 0 | 0 | X | ON |
| X | X | 1 | X | X | OFF |
| X | X | X | 1 | X | OFF |
| X | 0 | 0 | 0 | ON | ON |
| X | 0 | 0 | 0 | OFF | OFF |

$X=$ irrelevant
$\mathrm{t}-1=$ previous output state
$t=$ present output state

Information present at an input is transferred to its latch when the STROBE is high. A high CLEAR input will set all latches to the output OFF condition regardless of the data or STROBE input levels. A high OUTPUT ENABLE will set all outputs to the OFF condition regardless of any other input conditions. When the OUTPUT ENABLE is low, the outputs depend on the state of their respective latches.

## TIMING CONDITIONS

(Logic Levels are $V_{D D}$ and $V_{S S}$ )


DWG.NO. A-10,895A
A. Minimum data active time before strobe enabled (data set-up time) . . . . . . . . . . . . . . . . . . 100 ns
B. Minimum data active time after strobe disabled (data hold time) . . . . . . . . . . . . . . . . . . . 100 ns
C. Minimum strobe pulse width . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 300 ns
D. Typical time between strobe activation and output on to off transition ................. 500 ns
E. Typical time between strobe activation and output off to on transition ................. 500 ns
F. Minimum clear pulse width . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 300 ns
G. Minimum data pulse width . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 500 ns



CAUTION: Sprague CMOS devices feature input static protection but are still susceptible to damage when exposed to extremely high static electrical charges.

# UCN-4805A and UCN-4806A BiMOS LATCHED DECODER/DRIVERS 

FEATURES<br>- High-Voltage Source Outputs<br>- CMOS, PMOS, NMOS, TTL Compatible Inputs<br>- Low-Power CMOS Latches<br>- Hexadecimal Decoding<br>- Internal Pull-Up/Pull-Down Resistors<br>- Wide Supply Voltage Range

DESIGNED for use in high-voltage vacuum fluorescent display driver applications, the UCN-4805A and UCN-4806A latched decoder/ drivers combine CMOS logic with bipolar source outputs. Both devices consist of eight high-voltage bipolar sourcing outputs with internal pull-down resistors and CMOS input latches, hexadecimal decoder, and control circuitry (strobe and blanking).

The UCN-4805A BiMOS latched decoder/driver is intended to serve as the segment driver with standard 7 -segment displays incorporating a colon or decimal point. The UCN-4806A modification is designed for use with centered " 1 " ( 9 -segment) displays. It has an I/O input to permit interrogating the input latches for error-checking purposes. Both ICs use hexadecimal decoding to display $0-9, A, b, C, d$, E , and F .
Both BiMOS latched decoder/drivers have sufficient speed to permit operation with most microprocessor/LSI-based systems. The CMOS input latches provide operation over the supply voltage range of 5 to 15 volts with minimum logic loading. Internal output pull-down resistors eliminate the need for external components usually required for fluorescent display applications. When used with standard TTL or low-speed TTL logic, both devices may require employment of input pull-up resistors to insure a proper input logic high.


UCN-4805A


UCN-4806A
ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ FreeAir Temperature and $\mathbf{V}_{\text {ss }}=\mathbf{O V}$

Output Voltage, $\mathrm{V}_{\text {out }} \ldots . . . . . . . . . . . . . . . . . . . . . . . . . . . .60 \mathrm{~V}$
Logic Supply Voltage Range, $\mathrm{V}_{D 0} \ldots \ldots . . . .$.
Driver Supply Voltage Range, $\mathrm{V}_{B B} \ldots \ldots . \ldots . \mathrm{I}_{5} .0 \mathrm{~V}$ to 60 V
Input Voltage Range, $\mathrm{V}_{\mathrm{IN}} \ldots \ldots . . .$.
Continuous Output Current, $\mathrm{I}_{\text {out }} \ldots . . . . . . . . . . . .$.

Operating Temperature Range, $T_{A} \ldots \ldots .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . . .-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
*Derate at the rate of $18.18 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

| Number of | Max. Allowable Duty Cycle |  |  |
| :---: | :---: | :---: | :---: |
| Outputs ON | at Ambient Temperature of |  |  |
| $\left(\mathrm{I}_{\text {Out }}=-25 \mathrm{~mA}\right)$ | $50^{\circ} \mathrm{C}$ | $60^{\circ} \mathrm{C}$ | $70^{\circ} \mathrm{C}$ |
| 8 | $100 \%$ | $92 \%$ | $78 \%$ |
| 7 |  | $100 \%$ | $89 \%$ |
| 6 |  | 1 | $100 \%$ |
| 1 | $100 \%$ | $100 \%$ | $100 \%$ |

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{BB}}=60 \mathrm{~V}, \mathrm{~V}_{\mathrm{DO}}=4.75 \mathrm{~V}$ to $15.75 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=0 \mathrm{~V}$ (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Max. | Units |
| Output OFF Voltage | $V_{\text {OUT }}$ |  | - | 1.0 | V |
| Output ON Voltage |  | $\mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$ | 57.5 | - | V |
| Output Pull-Down Current | $\mathrm{I}_{\text {OUT }}$ | $V_{\text {OUT }}=V_{\text {BB }}$ | 400 | 850 | $\mu \mathrm{A}$ |
| Output Leakage Current |  | $\mathrm{T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | -15 | $\mu A$ |
| Input Voltage | $V_{\text {W(1) }}$ | $\mathrm{V}_{\text {DO }}=5.0 \mathrm{~V}$ | 3.5 | 5.3 | V |
|  |  | $V_{D D}=15 \mathrm{~V}$ | 13.5 | 15.3 | V |
|  | $V_{1 \times 10}$ |  | -0.3 | +0.8 | V |
| Input Current | $\mathrm{I}_{\text {(1) }}$ | $V_{D D}=5.0 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | $V_{D D}=15 \mathrm{~V}$ | - | 300 | $\mu \mathrm{A}$ |
| Input Impedance | $Z_{\text {IN }}$ | $V_{D D}=5.0 \mathrm{~V}$ | 50 | - | $k \Omega$ |
| Supply Current | $\mathrm{I}_{\text {BB }}$ | Display "8" | - | 9.1 | mA |
|  |  | All outputs OFF | -. | 100 | $\mu A$ |
|  | 100 | $\mathrm{V}_{\text {DD }}=1 / 0=$ STROBE $=5.0 \mathrm{~V}$, All other inputs $=0 \mathrm{~V}$ | - | 200 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {DD }}=1 / 0=$ STROBE $=15 \mathrm{~V}$, All other inputs $=0 \mathrm{~V}$ | - | 500 | $\mu \mathrm{A}$ |
|  |  | $V_{D D}=$ STROBE $=$ BLANK $=5.0 \mathrm{~V}$, Data latched, Display "8" | - | 7.0 | mA |
|  |  | $V_{D D}=$ STROBE $=$ BLANK $=15 \mathrm{~V}$, Data latched, Display " 8 " | - | 21 | mA |

NOTE: Positive (negative) current is defined as going into (coming out of) the specified device pin.
Caution: Sprague CMOS devices feature input static protection but are still
susceptible to damage when exposed to extremely high static electrical charges.

UCN-4805A TRUTH TABLE

| Inputs |  |  |  |  |  |  | Character | Outputs |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D | C | B | A | dp | BL | ST |  | a | b | c | d | e | $f$ | g | dp |
| 0 | 0 | 0 | 0 | 0 | 1 | 0 | Zero | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 |
| 0 | 0 | 0 | 1 | 0 | 1 | 0 | One | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 1 | 0 | 0 | 1 | 0 | Two | 1 | 1 | 0 | 1 | 1 | 0 | 1 | 0 |
| 0 | 0 | 1 | 1 | 0 | 1 | 0 | Three | 1 | 1 | 1 | 1 | 0 | 0 | 1 | 0 |
| 0 | 1 | 0 | 0 | 0 | 1 | 0 | Four | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 |
| 0 | 1 | 0 | 1 | 0 | 1 | 0 | Five | 1 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| 0 | 1 | 1 | 0 | 0 | 1 | 0 | Six | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 |
| 0 | 1 | 1 | 1 | 0 | 1 | 0 | Seven | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 1 | 0 | 0 | 0 | 0 | 1 | 0 | Eight | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| 1 | 0 | 0 | 1 | 0 | 1 | 0 | Nine | 1 | 1 | 1 | 0 | 0 | 1 | 1 | 0 |
| 1 | 0 | 1 | 0 | 0 | 1 | 0 | A | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 |
| 1 | 0 | 1 | 1 | 0 | 1 | 0 | b | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 0 |
| 1 | 1 | 0 | 0 | 0 | 1 | 0 | C | 1 | 0 | 0 | 1 | 1 | 1 | 0 | 0 |
| 1 | 1 | 0 | 1 | 0 | 1 | 0 | d | 0 | 1 | 1 | 1 | 1 | 0 | 1 | 0 |
| 1 | 1 | 1 | 0 | 0 | 1 | 0 | E | 1 | 0 | 0 | 1 | 1 | 1 | 1 | 0 |
| 1 | 1 | 1 | 1 | 0 | 1 | 0 | F | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 |
| X | X | X | X | 1 | 1 | 0 | dp | X | X | $X$ | X | X | $X$ | X | 1 |
| X | X | X | X | X | 0 | X | blank | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

$X=$ irrelevant


UCN-4806A TRUTH TABLE

| Inputs |  |  |  |  |  |  | Character | Outputs |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D | C | B | A | BL | ST | 1/0 |  | a | b | c | d | e | $f$ | g | h |
| 0 | 0 | 0 | 0 | 1 | 0 | 1 | Zero | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 |
| 0 | 0 | 0 | 1 | 1 | 0 | 1 | One | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 0 | 0 | 1 | 0 | 1 | 0 | 1 | Two | 1 | 1 | 0 | 1 | 1 | 0 | 1 | 0 |
| 0 | 0 | 1 | 1 | 1 | 0 | 1 | Three | 1 | 1 | 1 | 1 | 0 | 0 | 1 | 0 |
| 0 | 1 | 0 | 0 | 1 | 0 | 1 | Four | 0 | 1 | 1 | 0 | 0 | 1 | 1 | 0 |
| 0 | 1 | 0 | 1 | 1 | 0 | 1 | Five | 1 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| 0 | 1 | 1 | 0 | 1 | 0 | 1 | Six | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 |
| 0 | 1 | 1 | 1 | 1 | 0 | 1 | Seven | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 1 | 0 | 0 | 0 | 1 | 0 | 1 | Eight | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| 1 | 0 | 0 | 1 | 1 | 0 | 1 | Nine | 1 | 1 | 1 | 0 | 0 | 1 | 1 | 0 |
| 1 | 0 | 1 | 0 | 1 | 0 | 1 | A | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 |
| 1 | 0 | 1 | 1 | 1 | 0 | 1 | b | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 0 |
| 1 | 1 | 0 | 0 | 1 | 0 | 1 | C | 1 | 0 | 0 | 1 | 1 | 1 | 0 | 0 |
| 1 | 1 | 0 | 1 | 1 | 0 | 1 | d | 0 | 1 | 1 | 1 | 1 | 0 | 1 | 0 |
| 1 | 1 | 1 | 0 | 1 | 0 | 1 | E | 1 | 0 | 0 | 1 | 1 | 1 | 1 | 0 |
| 1 | 1 | 1 | 1 | 1 | 0 | 1 | F | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 |
| X | X | $X$ | $X$ | 0 | X | X | blank | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| X | X | X | X | X | 1 | 0 | interrogate latches | X | X | X | $x$ | X | X | X | X |

$X=$ irrelevant


## TIMING CONDITIONS

(Logic Levels are $V_{D D}$ and $V_{S S}$ )

A. Minimum Data Active Time Before Strobe Enabled (Data Set-Up Time) . . . . . . . . . . . . . . . . . . . . . . . 100 ns
B. Minimum Data Active Time After Strobe Disabled (Data Hold Time) . . . . . . . . . . . . . . . . . . . . . . . . . 100 ns
C. Minimum Strobe Pulse Width . . . . . . . . . . . . . . . . 300 ns
D. Typical Time Between Strobe Activation and Output On to Off Transition ............................ $1.0 \mu \mathrm{~s}$
E. Typical Time Between Strobe Activation and Output Off to On Transition ............................. . . 1.0 $\mathrm{\mu s}$
F. Minimum Data Pulse Width . . . . . . . . . ......... 500 ns

Information present at an input is transferred to its latch when the STROBE (ST) is low. The latches will continue to accept new data as long as the STROBE is held low. Applications where the latches are bypassed (STROBE tied low) ordinarily require that the BLANKING input be low between digit selection because of possible non-synchronous decoding.

When the BLANKING (BL) input is low, all of the output buffers are disabled (OFF) without affect-
ing the information stored in the latches. With the

TYPICAL INPUT CIRCUITS


INPUT CIRCUITS

Dwg. No. A-10,980

BLANKING input high, the outputs are controlled by the latch/decoder circuitry.

With the I/O input control (UCN-4806A only) held high, the BCD data terminals function as inputs and allow information to be transferred to the latches. With the I/O input control held low, the BCD data terminals function as high-impedance latch outputs and allow the latches to be interrogated for error-checking purposes. While I/O is low, the STROBE line must be held high.


# UCN-4810A BiMOS 10-BIT SERIAL-INPUT, LATCHED DRIVER 

## FEATURES

- High-Voltage Source Outputs
- CMOS, PMOS, NMOS, TL Compatible Inputs
- Low-Power CMOS Logic \& Latches
- Internal Pull-Down Resistors
- Wide Supply Voltage Range

COMBINING low-power CMOS logic with bipolar source drivers, the UCN-4810A BiMOS 10-bit serial-input, latched driver will simplify many display systems. Primarily designed for use with vacuum fluorescent displays, it can also be used with LED and incandescent displays within its output limitations of 60 V and 40 mA per driver.

The CMOS 10-bit shift register and associated latches are designed for operation over a supply voltage range of 5 V to 15 V . They also provide for minimum loading and are compatible with standard CMOS, PMOS, and NMOS logic. When used with standard TTL or low speed TTL logic the use of appropriate pull-up resistors may be required to insure a proper input logic high. A CMOS serial data output allows cascading these devices for interface requiring many drive lines (dot matrix, alphanumeric, bargraph, etc.).

The ten bipolar outputs are used as segment or digit drivers in vacuum fluorescent displays. Under normal operating conditions, these devices will sustain 25 mA per output at $50^{\circ} \mathrm{C}$ and a duty cycle of $85 \%$. Other combinations of number of outputs conducting and duty cycle are shown in the specifications.

The UCN-4810A driver, combined with the UCN-4805A or UCN-4806A latched hexadecimal decoder/drivers or the UCN-4815A 8-bit latched source driver, comprises a minimum component display subsystem, requiring few, if any, discrete components.


## ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ Free-Air Temperature and $\mathrm{V}_{\mathrm{ss}}=\mathbf{0} \mathbf{V}$

Output Voltage, $\mathrm{V}_{\text {out }} \ldots \ldots . .$.

Driver Supply Voltage Range, $\mathrm{V}_{B B} \ldots \ldots . \ldots . \mathrm{I}_{5} .0 \mathrm{~V}$ to 60 V
Input Voltage Range, $\mathrm{V}_{\mathbb{I}} \ldots \ldots \ldots . .-0.3 \mathrm{~V}$ to $\mathrm{V}_{D D}+0.3 \mathrm{~V}$
Continuous Output Current, $\mathrm{I}_{\text {out }} \ldots . . . . . . . . . . . . . . .-40 \mathrm{~mA}$
Package Power Dissipation, $\mathrm{P}_{0} \ldots . .$. . . . . . . . . . . . 1.82 W* $^{*}$
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots . .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots . . . .-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
*Derate at the rate of $18.18 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.

| Number of Outputs ON | Max. Allowable Duty Cycle at Ambient Temperature of |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\left(1_{\text {OUT }}=-25 \mathrm{~mA}\right)$ | $25^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $60^{\circ} \mathrm{C}$ | $70^{\circ} \mathrm{C}$ |
| 10 | 100\% | 97\% | 85\% | 73\% | 62\% |
| 9 | 4 | 100\% | 94\% | 82\% | 69\% |
| 8 |  | 4 | 100\% | 92\% | 78\% |
| 7 |  |  |  | 100\% | 89\% |
| 6 |  |  |  |  | 100\% |
| 1 | 100\% | 100\% | 100\% | 100\% | 100\% |

[^23] susceptible to damage when exposed to extremely high static electrical charges.

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{BB}}=60 \mathrm{~V}, \mathrm{~V}_{\mathrm{DO}}=4.75 \mathrm{~V}$ to $15.75 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=0 \mathrm{~V}$ (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Max. | Units |
| Output OFF Voltage | $\mathrm{V}_{\text {out }}$ |  | - | 1.0 | V |
| Output ON Voltage |  | $\mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$ | 57.5 | - | V |
| Output Pull-Down Current | Iour | $\mathrm{V}_{\text {OUI }}=\mathrm{V}_{\text {BB }}$ | 400 | 850 | $\mu \mathrm{A}$ |
| Output Leakage Current |  | $\mathrm{T}_{\mathrm{A}}=70^{\circ} \mathrm{C}$ | - | -15 | $\mu \mathrm{A}$ |
| Input Voltage | $V_{\text {W(1) }}$ | $\mathrm{V}_{\mathrm{DD}}=5.0 \mathrm{~V}$ | 3.5 | 5.3 | V |
|  |  | $\mathrm{V}_{00}=15 \mathrm{~V}$ | 13.5 | 15.3 | V |
|  | $V_{\text {M(0) }}$ |  | -0.3 | +0.8 | V |
| Input Current | $1_{\text {(1) }}$ | $\mathrm{V}_{\text {O0 }}=\mathrm{V}_{\text {W }}=5.0 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {OD }}=\mathrm{V}_{\text {W }}=15 \mathrm{~V}$ | - | 300 | $\mu \mathrm{A}$ |
| Input Impedance | $\mathrm{Z}_{\text {W }}$ | $\mathrm{V}_{00}=5.0 \mathrm{~V}$ | 50 | - | $\mathrm{k} \Omega$ |
| Serial Data Output Resistance | $\mathrm{R}_{\text {OUT }}$ | $\mathrm{V}_{\text {D0 }}=5.0 \mathrm{~V}$ | - | 20 | k $\Omega$ |
|  |  | $\mathrm{V}_{00}=15 \mathrm{~V}$ | - | 6.0 | $\mathrm{k} \Omega$ |
| Supply Current | $1_{8 B}$ | All outputs ON, All outputs open | - | 13 | mA |
|  |  | All outputs OFF | - | 200 | $\mu \mathrm{A}$ |
|  | 100 | $\mathrm{V}_{00}=5.0 \mathrm{~V}$, All outputs OFF, All inputs $=0 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {Do }}=15 \mathrm{~V}$, All outputs OFF, All inputs $=0 \mathrm{~V}$ | - | 200 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {OO }}=5.0 \mathrm{~V}$, One output ON, All inputs $=0 \mathrm{~V}$ | - | 1.0 | mA |
|  |  | $\mathrm{V}_{\text {Do }}=15 \mathrm{~V}$, One output ON, All inputs $=0 \mathrm{~V}$ | - | 3.0 | mA |

NOTE: Positive (negative) current is defined as going into (coming out of) the specified device pin.


Dwg. No. A-10.931
TYPICAL OUTPUT DRIVER


FUNCTIONAL BLOCK DIAGRAM


TIMING CONDITIONS
(Logic Levels are $V_{D D}$ and $V_{S S}$ )

| $V_{D D}=5$ | $V_{D 0}=15 \mathrm{~V}$ |
| :---: | :---: |
| 250 ns | 150 ns |
| 500 ns | 300 ns |
| $1.0 \mu \mathrm{~s}$ | 250 ns |
| $1.0 \mu \mathrm{~s}$ | 400 ns |
| 500 ns | 300 ns |
| $1.0 \mu \mathrm{~s}$ | $1.0 \mu \mathrm{~s}$ |

SERIAL DATA present at the input is transferred to the shift register on the logic ' 0 '" to logic ' 1 ", transition of the CLOCK input pulse. On succeeding CLOCK pulses, the registers shift data information towards the SERIAL DATA OUTPUT. The SERIAL DATA must appear at the input prior to the rising edge of the CLOCK input waveform.

Information present at any register is transferred to its respective latch when the STROBE is high (serial-to-parallel conversion). The latches will con-
tinue to accept new data as long as the STROBE is held high. Applications where the latches are bypassed (STROBE tied high) will require that the BLANKING input be high during serial data entry.

When the BLANKING input is high, all of the output buffers are disabled (OFF) without affecting the information stored in the latches or shift register. With the BLANKING input low, the outputs are controlled by the state of the latches.

## UCN-4810A TRUTH TABLES

| Serial Data Input | Clock Input | Shift Register Contents | Serial <br> Data <br> Output | Strobe Input | Latch Contents | Blanking Input | Output Contents |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $I_{1} I_{2} I_{3} \ldots \ldots I_{8} I_{9} I_{10}$ |  |  | $I_{1} I_{2} I_{3} \ldots \ldots I_{8} I_{9} I_{10}$ |  | $I_{1} I_{2} I_{3} \ldots \ldots I_{8} I_{9} I_{10}$ |
| H | 5 | $\mathrm{HR}_{1} \mathrm{R}_{2} \ldots \mathrm{R}_{7} \mathrm{R}_{8} \mathrm{R}_{9}$ | Rg |  |  |  |  |
| L | 5 | $L R_{1} R_{2} \ldots R_{7} R_{8} R_{9}$ | $\mathrm{R}_{9}$ |  |  |  |  |
| X | L | $\mathrm{R}_{1} \mathrm{R}_{2} \mathrm{R}_{3} \ldots \mathrm{R}_{8} \mathrm{R}_{9} \mathrm{R}_{10}$ | $\mathrm{R}_{10}$ |  |  |  |  |
|  |  | XXX $\ldots \ldots \mathrm{XXX}$ | X | L | $\mathrm{R}_{1} \mathrm{R}_{2} \mathrm{R}_{3} \ldots \mathrm{R}_{8} \mathrm{R}_{9} \mathrm{R}_{10}$ |  |  |
|  |  | $\mathrm{P}_{1} \mathrm{P}_{2} \mathrm{P}_{3} \ldots \mathrm{P}_{8} \mathrm{P}_{9} \mathrm{P}_{10}$ | $\mathrm{P}_{10}$ | H | $\mathrm{P}_{1} \mathrm{P}_{2} \mathrm{P}_{3} \ldots \mathrm{P}_{8} \mathrm{P}_{9} \mathrm{P}_{10}$ | L | $\mathrm{P}_{1} \mathrm{P}_{2} \mathrm{P}_{3} \ldots \mathrm{P}_{8} \mathrm{P}_{4} \mathrm{P}_{10}$ |
|  |  |  |  |  | XXX..... $\mathrm{XXX}^{\text {X }}$ | H | $L L L \ldots \ldots . L L L$ |

[^24]
## UCN-4815A

## BiMOS LATCH/SOURCE DRIVER

## FEATURES

- High-Voltage Source Outputs
- CMOS, PMOS, NMOS, TTL Compatible Inputs
- Low-Power CMOS Latches
- Internal Pull-Down Resistors
- Wide Supply Voltage Range

DESIGNED primarily for use with high-voltage vacuum fluorescent displays, the UCN-4815A BiMOS latch/source driver consists of eight NPN Darlington source drivers with pull-down resistors, a CMOS latch for each driver, and common strobe, blanking, and enable functions.

The CMOS inputs provide for minimum loading and are compatible with standard CMOS, PMOS, and NMOS logic commonly found in microprocessor designs. The use of CMOS latches also allows operation over a supply voltage range of 5 V to 15 V . When employed with either standard TTL or low speed TTL logic, the UCN-4815A may require the use of appropriate pull-up resistors.

The bipolar outputs may be used as segment, dot (matrix), bar, or digit drivers in vacuum fluorescent displays. All eight outputs can be activated simultaneously at ambient temperatures up to $60^{\circ} \mathrm{C}$. To simplify circuit board layout, all outputs are pinned opposite their respective inputs.

A minimum component display subsystem, requiring few or no discrete components, may be realized by using the UCN-4815A BiMOS Latch/ Source Driver with either a UCN-4805A or UCN4806A latched hexadecimal decoder/drivers or a UCN-4810A serial-to-parallel latch/driver.


Output Voltage, $\mathrm{V}_{\text {out }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . 60 V
Logic Supply Voltage Range, $V_{D 0} \ldots . . . . . . . . .4 .5 \mathrm{~V}$ to 18 V
Driver Supply Voltage Range, $\mathrm{V}_{B B} \ldots \ldots . . . \mathrm{I}^{2} .0 \mathrm{~V}$ to 60 V
Input Voltage Range, $V_{\mathbb{N}} \ldots . . . . .$.
Continuous Output Current, $\mathrm{I}_{\text {out }}$. . . . . . . . . . . . . . . -40 mA
Package Power Dissipation, $P_{D} \ldots . . . . . . . . . . . . . . . .2 .0 W^{*}$
Operating Temperature Range, $\mathrm{T}_{A} \ldots \ldots . .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . .,-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
${ }^{*}$ Derate at the rate of $20 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{A}=25^{\circ} \mathrm{C}$.

| Number of <br> Outputs 0 N | Max. Allowable Duty Cycle <br> at Ambient Temperature of |  |  |
| :---: | :---: | :---: | :---: |
| $\left(l_{\text {out }}=-25 \mathrm{~mA}\right)$ | $50^{\circ} \mathrm{C}$ | $60^{\circ} \mathrm{C}$ | $70^{\circ} \mathrm{C}$ |
| 8 | $100 \%$ | $100 \%$ | $86 \%$ |
| 7 |  |  | $98 \%$ |
| 6 |  |  | $100 \%$ |
| 1 | $100 \%$ | $100 \%$ | $100 \%$ |

Caution: Sprague CMOS devices feature input static protection but are still susceptible to damage when exposed to extremely high static electrical charges.

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{BB}}=60 \mathrm{~V}, \mathrm{~V}_{\mathrm{DO}}=4.75 \mathrm{~V}$ to $15.75 \mathrm{~V}, \mathrm{~V}_{S S}=0 \mathrm{~V}$
(unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Max. | Units |
| Output OFF Voltage | $V_{\text {OUT }}$ |  | - | 1.0 | V |
| Output ON Voltage |  | $\mathrm{I}_{\text {OUT }}=-25 \mathrm{~mA}$ | 57.5 | - | V |
| Output Pull-Down Current | $\mathrm{I}_{\text {OUT }}$ | $V_{\text {OUT }}=V_{\text {BB }}$ | 400 | 850 | $\mu \mathrm{A}$ |
| Output Leakage Current |  | $\mathrm{T}_{A^{\prime}}=70^{\circ} \mathrm{C}$ | - | -15 | $\mu \mathrm{A}$ |
| Input Voltage | $V_{\mathbb{W}(1)}$ | $\mathrm{V}_{D D}=5.0 \mathrm{~V}$ | 3.5 | 5.3 | V |
|  |  | $\mathrm{V}_{\text {DD }}=15 \mathrm{~V}$ | 13.5 | 15.3 | V |
|  | $V_{\text {IN(0) }}$ |  | -0.3 | +0.8 | V |
| Input Current | $\mathrm{I}_{\text {IN(I) }}$ | $V_{D D}=V_{\mathbb{N}}=5.0 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {DO }}=\mathrm{V}_{\mathbb{N}}=15 \mathrm{~V}$ | - | 300 | $\mu \mathrm{A}$ |
| Input Impedance | $Z_{\text {IN }}$ | $\mathrm{V}_{D 0}=5.0 \mathrm{~V}$ | 50 | - | k $\Omega$ |
| Supply Current | $I_{B B}$ | All outputs ON, All outputs open | - | 10.5 | mA |
|  |  | All outputs OFF | - | 100 | $\mu \mathrm{A}$ |
|  | $I_{D O}$ | $\mathrm{V}_{\text {DD }}=5.0 \mathrm{~V}$, All outputs OFF, All inputs $=0 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | $V_{\text {DD }}=15 \mathrm{~V}$, All outputs OFF, All inputs $=0 \mathrm{~V}$ | - | 200 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {OD }}=5.0 \mathrm{~V}$, One output 0 N, All inputs $=0 \mathrm{~V}$ | - | 1.0 | mA |
|  |  | $\mathrm{V}_{\text {DD }}=15 \mathrm{~V}$, One output 0 N , All inputs $=0 \mathrm{~V}$ | - | 3.0 | mA |

NOTE: Positive (negative) current is defined as going into (coming out of) the specified device pin.

UCN-4815A TRUTH TABLE

| Inputs |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | OUT $_{N}$ |  |  |  |  |
| $\mathbf{N}_{N}$ | STROBE | ENABLE | BLANK | T-1 | T |
| 0 | 1 | 1 | 0 | $X$ | 0 |
| 1 | 1 | 1 | 0 | $X$ | 1 |
| $X$ | $X$ | $X$ | 1 | $X$ | 0 |
| $X$ | 0 | $X$ | 0 | 1 | 1 |
| $X$ | 0 | $X$ | 0 | 0 | 0 |
| $X$ | $X$ | 0 | 0 | 1 | 1 |
| $X$ | $X$ | 0 | 0 | 0 | 0 |

[^25]

Dwg. No. A-10,980
TYPICAL INPUT CIRCUIT


TYPICAL OUTPUT DRIVER

## TIMING CONDITIONS

(Logic Levels are $V_{D D}$ and $V_{S S}$ )

A. Minimum Data Active Time Before Strobe Enabled (Data Set-Up Time) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 100 ns
B. Minimum Data Active Time After Strobe Disabled (Data Hold Time) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 100 ns
C. Typical Strobe Pulse Width For Power-Up Clear Disable . . . . . . . . . . . . . . . ....................................... . 500 ns

Minimum Strobe Pulse Width After Power-Up Clear Disabled . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 300 ns
D. Typical Time Between Strobe Activation and Output On to Off Transition ........................................... 1.0 . s
E. Typical Time Between Strobe Activation and Output Off to On Transition ............................................ 1.0 us
F. Minimum Data Pulse Width . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 500 ns

Information present at an input is transferred to its latch when the STROBE and ENABLE are high. The latches will continue to accept new data as long as both STROBE and ENABLE are held high. With either STROBE or ENABLE in the low state, no information can be loaded into the latches.

When the BLANKING input is high, all of the output buffers are disabled (OFF) without affecting the information stored in the latches. With the

BLANKING input low, the outputs are controlled by the state of the latches.

On first applying $V_{D D}$ to the device, all latch outputs assume a low state (Power-Up Clear) resulting in all outputs being OFF. The latches will remain in the low condition until the Clear is disabled by a STROBE high input. Data may be entered into the latches during Power-Up Clear disable if the ENABLE input is also high.

## SERIES UCN-4820A BiMOS 8-BIT SERIAL-INPUT, LATCHED DRIVERS

## FEATURES

- High-Voltage Current-Sink Outputs
- CMOS, PMOS, NMOS, IL Compatible
- Low-Power CMOS Logic and Latches
- Internal Pull-Up/Pull-Down Resistors
- 16-Pin Dual In-Line Plastic Packages

ACOMBINATION of bipolar and MOS technology gives Sprague's Series UCN-4820A an interface flexibility beyond the reach of standard logic buffers and power driver arrays.

The three devices in this series each have eight bipolar current-sink Darlington drivers, a CMOS data latch for each of the eight open-collector outputs, an eight-bit CMOS shift register and CMOS control circuitry. Except for maximum driver voltage ratings, Types UCN-4821A, UCN-4822A and UCN-4823A are identical.

The bipolar outputs can drive multiplexed LED displays, incandescent lamps, thermal print heads, and (with appropriate clamping techniques) relays, solenoids and other high-power inductive loads.

The CMOS shift register and latches, which operate over a 5 - to 15 -volt supply range, minimize loading and are compatible with CMOS, PMOS and NMOS logic. Use of the drivers with TTL and DTL may require a pull-up resistor to ensure an input logic high. By using the serial data output, the drivers can be cascaded for interface applications requiring additional drive lines.

These devices are also available in industrialgrade ceramic packages (Series UCQ-4820R) and in military side-brazed, hermetically sealed packages (Series UCS-4820H).


## ABSOLUTE MAXIMUM RATINGS <br> at $25^{\circ} \mathrm{C}$ Free-Air Temperature and $\mathrm{V}_{\text {ss }}=\mathrm{OV}$

Output Voltage, $V_{\text {ouI }}$ (UCN-4821A ..... 50 V
(UCN-4822A) ..... 80 V
(UCN-4823A) ..... 100 V
Logic Supply Voltage, $V_{D D}$ ..... 18 V
Input Voltage Range, $V_{\mathbb{N}}$ ..... -0.3 V to $\mathrm{V}_{D 0}+0.3 \mathrm{~V}$
Continuous Output Current, I out ..... 500 mA
Package Power Dissipation, $P_{0}$ ..... 1.67 W* $^{*}$
Operating Temperature Range, $T_{A}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{S}$ ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$

[^26]ELECTRICAL CHARACTERISTICS at $T_{A}=+25^{\circ} \mathrm{C}, \mathrm{V}_{D D}=5 \mathrm{~V}, \mathrm{~V}_{S S}=\mathrm{OV}$ (unless otherwise specified)

| Characteristic | Symbol | Applicable Devices | Test Conditions | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | UCN-4821A | $\mathrm{V}_{\text {OUf }}=50 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\text {out }}=50 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | UCN-4822A | $\mathrm{V}_{\text {OUI }}=80 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\text {out }}=80 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
|  |  | UCN-4823A | $\mathrm{V}_{\text {out }}=100 \mathrm{~V}$ | - | 50 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\text {out }}=100 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ | - | 100 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $V_{\text {CESSAT }}$ | ALL | $\mathrm{I}_{\text {OUT }}=100 \mathrm{~mA}$ | - | 1.1 | V |
|  |  |  | $\mathrm{I}_{\text {Out }}=200 \mathrm{~mA}$ | - | 1.3 | V |
|  |  |  | $\mathrm{I}_{\text {OUT }}=350 \mathrm{~mA}, \mathrm{~V}_{\text {DD }}=7.0 \mathrm{~V}$ | - | 1.6 | V |
| Tnput Voltage | $V_{\text {IN(0) }}$ | ALL |  | - | 0.8 | V |
|  | $V_{\text {IN(1) }}$ | ALL | $V_{\text {DD }}=15 \mathrm{~V}$ | 13.5 | - | V |
|  |  |  | $\mathrm{V}_{\text {D }}=10 \mathrm{~V}$ | 8.5 | - | V |
|  |  |  | $V_{D D}=5.0 \mathrm{~V}$ | 3.5 | - | V |
| Tnput Resistance | $\mathrm{R}_{\text {IN }}$ | ALL | $\mathrm{V}_{\text {D }}=15 \mathrm{~V}$ | 50 | - | $\mathrm{k} \Omega$ |
|  |  |  | $V_{D D}=10 \mathrm{~V}$ | 50 | - | $\mathrm{k} \Omega$ |
|  |  |  | $V_{D D}=5.0 \mathrm{~V}$ | 50 | - | $k \Omega$ |
| Supply Current | $\mathrm{I}_{\text {dion) }}$ | ALL | One Driver $0 \mathrm{~N}, \mathrm{~V}_{\mathrm{DD}}=15 \mathrm{~V}$ | - | 2.0 | mA |
|  |  |  | One Driver ON, $\mathrm{V}_{\text {D }}=10 \mathrm{~V}$ | - | 1.7 | mA |
|  |  |  | One Driver ON, $\mathrm{V}_{\text {D }}=5.0 \mathrm{~V}$ | - | 1.0 | mA |
|  | $\mathrm{I}_{\text {Do(0FF) }}$ | ALL | All Drivers OFF, $\mathrm{V}_{\mathbb{N}}=0 \mathrm{~V}$ | - | 100 | $\mu \mathrm{A}$ |


| Number of Outputs ON | Max. Allowable Duty Cycle at Ambient Temperature of |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\left(1_{\text {Out }}=200 \mathrm{~mA}\right)$ | $25^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $60^{\circ} \mathrm{C}$ | $70^{\circ} \mathrm{C}$ |
| 8 | 67\% | 56\% | 50\% | 43\% | 36\% |
| 7 | 76\% | 64\% | 57\% | 49\% | 41\% |
| 6 | 89\% | 74\% | 66\% | 57\% | 48\% |
| 5 | 100\% | 89\% | 80\% | 69\% | 58\% |
| 4 | $\uparrow$ | 100\% | 100\% | 75\% | 72\% |
| 3 |  |  |  | 100\% | 95\% |
| 2 | $\downarrow$ |  |  |  | 100\% |
| 1 | 100\% | 100\% | 100\% | 100\% | 100\% |

[^27]

| TIMING CONDITIONS (Logic Levels are $V_{D D}$ and $V_{S S}$ ) | $V_{D 0}=5.0$ | $\mathrm{VOD}_{\text {O }}=15 \mathrm{~V}$ |
| :---: | :---: | :---: |
| A. Minimum Data Active Time Before Clock Pulse (Data Set-Up Time) | 250 ns | 150 ns |
| B. Minimum Data Pulse Width | 500 ns | 300 ns |
| C. Minimum Clock Pulse Width | $1.0 \mu \mathrm{~s}$ | 250 ns |
| D. Minimum Time Between Clock Activation and Strobe | $1.0 \mu \mathrm{~s}$ | 400 ns |
| E. Minimum Strobe Pulse Width | 500 ns | 300 ns |
| F. Typical Time Between Strobe Activation and Output Transition | $1.0 \mu \mathrm{~s}$ | 1.0 ¢ |

SERIAL DATA present at the input is transferred to the shift register on the logic " 0 '" to logic " 1 '" transition of the CLOCK input pulse. On succeeding CLOCK pulses, the registers shift data information towards the SERIAL DATA OUTPUT. The SERIAL DATA must appear at the input prior to the rising edge of the CLOCK input waveform.

Information present at any register is transferred to its respective latch when the STROBE is high (serial-to-parallel conversion). The latches will con-
tinue to accept new data as long as the STROBE is held high. Applications where the latches are bypassed (STROBE tied high) will require that the ENABLE input be high during serial data entry.

When the $\overline{\text { ENABLE }}$ input is high, all of the output buffers are disabled (OFF) without affecting the information stored in the latches or shift register. With the ENABLE input low, the outputs are controlled by the state of the latches.

## SERIES UCN-4820A TRUTH TABLE

| Serial |  | Shift Register Contents | Serial |  | Latch Contents |  | Output Contents |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Data Input | Clock <br> Input | $\mathrm{I}_{1} \mathrm{I}_{2} \mathrm{I}_{3} \ldots \ldots \ldots . \mathrm{I}_{8}$ | Data Output | Strobe Input | $\mathrm{I}_{1} \mathrm{I}_{2} \mathrm{I}_{3} \ldots \ldots \ldots . \mathrm{I}_{8}$ | $\frac{\text { Output }}{\text { Enable }}$ | $I_{1} I_{2} I_{3} \ldots \ldots \ldots I_{8}$ |
| L | 5 | $\mathrm{HR}_{1} \mathrm{R}_{2} \ldots \ldots . . . \mathrm{R}_{7}$. | $\mathrm{R}_{7}$ |  |  |  |  |
| H | ك | $L R_{1} \mathrm{R}_{2} \ldots \ldots . . . R_{7}$ | $\mathrm{R}_{7}$ |  |  |  |  |
| X | $L$ | $\mathrm{R}_{1} \mathrm{R}_{2} \mathrm{R}_{3} \ldots \ldots . . . R_{8}$ | $\mathrm{R}_{8}$ |  |  |  |  |
|  |  | $\mathrm{XXX} \ldots \ldots \ldots \mathrm{X}$ | X | L | $\mathrm{R}_{1} \mathrm{R}_{2} \mathrm{R}_{3} \ldots \ldots . . R_{8}$ |  |  |
|  |  | $\mathrm{P}_{1} \mathrm{P}_{2} \mathrm{P}_{3} \ldots \ldots . \mathrm{P}_{8}$ | $\mathrm{P}_{8}$ | H | $\mathrm{P}_{1} \mathrm{P}_{2} \mathrm{P}_{3} \ldots \ldots . \mathrm{P}_{8}$ | L | $\mathrm{P}_{1} \mathrm{P}_{2} \mathrm{P}_{3} \ldots \ldots . \mathrm{P}_{8}$ |
|  |  |  |  |  | $\mathrm{XXX} \ldots \ldots \ldots . \mathrm{X}$ | H | HHH $\ldots \ldots \ldots$. ${ }^{\text {a }}$ |

L = Low Logic Level
$H=$ High Logic Level
$X=$ Irrelevant
$\mathrm{P}=$ Present State
$R=$ Previous State

FUNCTIONAL BLOCK DIAGRAM


TYPICAL INPUT CIRCUITS


TYPICAL OUTPUT DRIVER


Dwg. No. A-11,390

Dwg. No. A-11,389

# SPRAGUE BiMOS MUSCLE FOR THE MICROPROCESSOR 

Sprague Electric offers solutions to users' interface problems through a fusion of bipolar and CMOS technologies in BiMOS to create innovative interface devices.

The company's ability to shape technology to meet the specific needs of users is based on a commitment to provide versatile and practical interface products for systems design.

Sprague BiMOS devices are available with:

- Output breakdown voltage ratings of up to 100 V;
- Output current ratings as high as 600 mA ;
- A logic voltage-supply range of 5 V to 15 V ( $\pm 5 \%$ );
- Logic switching speeds of up to 1 MHz at 5 V and up to 2 MHz at 12 V ;
- And up to 10 channels per dual in-line package.
Among advantages of BiMOS technology are microprocessor compatibility, low-power logic, a wide logic-supply range, component-count reduction, bipolar output capability, CMOS noise immunity, and space-saving integration.


## APPLICATIONS

The following pages make up a sampler of applications for Sprague BiMOS interface devices. Performance specifications, truth tables and timing charts for these integrated circuits appear on previous pages. Additional applications are described in the Sprague brochure WR-185, 'Interface ICs for Motor Drive Applications,' and in Sprague engineering bulletins covering these BiMOS devices.

## UCN-4401A and UCN-4801A

These four- and eight-bit BiMOS latch/drivers are the first Sprague IC's to incorporate CMOS logic (data latches) and bipolar drivers (NPN Darlingtonpair outputs). Functionally, the eight-bit device is the equivalent of an octal latch and an octal NPN Darlington array.

Figure 1 depicts the use of the eight-bit latch/ driver as an interface between a microprocessor and incandescent lamps. The device can also link a microprocessor with LEDs, high-power discrete semiconductors, relays or small stepper motors. Applications with inductive loads require connection of the internal transient-suppression diodes to the load's voltage supply, or use of discrete diodes. Inductive load applications should be limited to output voltages of +35 V .

Figure 2 shows use of Type UCN-4401A as an interface between a microprocessor and a stepper motor. Input signals to the four-bit device, for both unipolar wave drive and unipolar two-phase drive, are shown in Figures 3 and 4.

Type UCN-4401A can also be used to control discrete PNP transistors providing a high-power motor interface (Figure 5). Use of either singleended or split supplies is possible with this approach.

The four-bit device can be paired with a quad PNP DIP to implement full-bridge drive for a stepper motor (Figure 6).


DWG. NO. A-11,444
Figure 1


Figure 2

## Sprague BiMOS (Continued)



Figure 3


Figure 4


Figure 5


Figure 6

## UCN-4810A

This integrated circuit functionally replaces a 10-bit serial-in, parallel-out shift register, a 10 -bit data latch, and 10 high-voltage buffers (including output pull-down resistors). It is designed for use with vacuum fluorescent displays, but has been put to many other uses, including control of thermal print heads.

Connecting a data-out line from one device to a data-in pin of a second device minimizes the number of input/output lines required for a system. A 20character $5 \times 7$ vacuum fluorescent dot matrix display, for instance, requires only six Type UCN4810 s (two as grid drivers and four as dot drivers). An example of cascaded data control is given in Figure 7. The arrangement cascades two devices for grid selection and four as dot drivers.

Data sent to the four dot drivers can be loaded in less than $80 \mu \mathrm{~s}$ using this configuration. The shiftrate limit of the dot drivers is 500 kHz at $\mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}$.

The two units that function as grid drivers are loaded with a single ' 1 "' during each scan cycle. The minimum recommended scan frequency is 100 Hz per character (a clock frequency of 2 kHz for a 20 -character display).

Since blanking ( $20 \mu \mathrm{~s}$ minimum) is required between characters, and since the minimum ON time for each digit or character is $100 \mu \mathrm{~s}$, the maximum number of characters in a display is $80(8 \mathrm{kHz}$ clock, $125 \mu_{\mathrm{S}} \mathrm{ON}$ and blanking time per character).
The typical ON time for vacuum fluorescent characters is $200 \mu \mathrm{~s}$ (40-character panel) to $500 \mu \mathrm{~s}$ ( 20 -character display). Failure to provide proper blanking time can cause ghosting or flicker.

A faster method of loading matrix data, shown in Figure 8, requires more I/O lines. This technique loads shift registers during a blanking period (greater than $20 \mu \mathrm{~s}$ ). Each dot driver has a separate data-input line, but uses common clock, strobe and blanking lines. A second clock is used with the grid drivers.

A typical data-input timing chart for this configuration is shown in Figure 9. With a 20 -character vacuum fluorescent display having a 2 kHz scan frequency, 10 bits of data are loaded during the first blanking period; succeeding 10 -bit data blocks are loaded during blanking periods at $400 \mu$ s intervals.
A more unusual application of Type UCN-4810A is shown in Figure 10: The device is used with a thermal printer. In production, the drivers (in chip form) were built into a hybrid assembly.


Figure 7


Figure 8


Figure 9


Figure 10


Figure 11


Figure 12

## UCN-4815

Type UCN-4815A provides an eight-bit parallelin, parallel-out interface for vacuum fluorescent displays. A typical application appears in Figure 11. A pair of Type UCN-4810As are used for grid control. The two Type UCN-4815As drive a 16 -segment alphanumeric display.

## UCN-4805A and UCN-4806A

Each of these devices has eight high-voltage source outputs, latched inputs, and both the hexadecimal decoding and speed capabilities for microprocessor-based designs.

Type UCN-4805A is used to decode and drive seven-segment displays. Its eighth source output is used to generate a colon or decimal point.

Type UCN-4806A is used with nine-segment (centered ' 1 '') displays. It has an I /O input that can be used to check for errors by interrogating input data latches.

A typical application with a 20-character vacuum fluorescent display is shown in Figure 12. Type

UCN-4805A is used as a seven-segment decoder/ driver. A pair of Type UCN-4810As is used for grid-select.

## SERIES UCN-4820A

The drivers in this series were designed for use in printers. Each integrated circuit has an eight-bit serial-input shift register, an eight-bit data latch, and eight NPN Darlington-pair outputs. The data entry rate for this series is 500 kHz (minimum) at $\mathrm{V}_{\mathrm{DD}}=$ 5 V .

A typical application appears in Figure 13; although the drawing depicts use with an electrosensitive printer, the device can also control inductive loads such as print hammers and solenoids, or thermal print heads.

Use of Types UCN-4823A and UCN-4810A-1 is combined in the planar gas-discharge display application shown in Figure 14. Type UCN-4810A-1 signal inputs are level-shifted (floated to the $V_{\text {вв }}$ supply level). The application requires external segment limiting and pull-up resistors and use of Zener diodes.


Figure 13


Figure 14

> GENERAL INFORMATION

HIGH-VOLTAGE INTERFACE DRIVERS

HIGH-CURRENT INTERFACE DRIVERS

BiMOS AND COMPLEX ARRAY INTERFACE DRIVERS

INDUSTRIAL, MILITARY, AND AEROSPACE DEVICES

## RADIO INTEGRATED CIRCUITS

## TELEVISION INTEGRATED CIRCUITS

## AUDIO INTEGRATED CIRCUITS

HALL EFFECT DEVICES

TRANSISTOR ARRAYS AND MISCELLANEOUS DEVICES

## CUSTOM DEVICES

## SECTION 5 - INDUSTRIAL, MILITARY, and AEROSPACE DEVICES

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NOTE: Most devices described in Sections 2, 3, and 4 can also be supplied in extended-temperature hermetic packages. Contact the local sales office or factory for additional information.

## SERIES 400, 400-1 and 500 HERMETICALLY SEALED POWER and RELAY DRIVERS

## FEATURES

- 500 mA Output Sink Current Capability
- DTL/TTL Compatible Inputs
- Transient Protected Outputs on Relay Drivers
- High Voltage Output - 100 V Series 500, 70 V Series $400-1$, and 40 V Series 400
- Hermetically Sealed Packages to MIL-M-38510
- High-Reliability Screening to MIL-STD-883, Class B


## Description

These Series $400,400-1$, and 500 hermetically sealed power and relay drivers are bipolar monolithic circuits incorporating both logic gates and high-current switching transistors on the same chip. Each device contains four drivers capable of sinking 500 mA in the ON state. In the OFF state, Series 400 devices will sustain 40V, Series 400-1 devices will sustain 70V, and Series 500 devices will sustain 100V.
All devices are available in either a 14 -pin hermetic flat-pack package (Types UHC-) or a 14 -pin hermetic dual in-line package (Types UHD-). These packages conform to the dimensional requirements of Military Specification MIL-M-38510 and meet all of the processing and environmental requirements of Military Standard MIL-STD-883, Method 5004 and 5005. These devices are also furnished in a plastic 14-pin dual in-line package (Types UHP-) for operation over a limited temperature range.

## Applications

The UHC- and UHD- Series 400, 400-1, and 500 power and relay drivers are ideally suited for driving incandescent lamps, relays, solenoids, and other interface devices with up to 1A output current per package. Hermetic sealing and an operating temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ recommend them for military and aerospace applications as well as commercial and industrial control applications where severe environments may be encountered.

## RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :--- | ---: | ---: | ---: | :---: |
| Supply Voltage $\left(V_{\text {cc }}\right)$ | 4.5 | 5.0 | 5.5 | V |
| Operating Temperature Range | -55 | +25 | +125 | ${ }^{\circ} \mathrm{C}$ |
| Current into any output (ON state) |  |  | 250 | mA |

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\mathrm{cc}}$ ..... 7 V
Input Voltage, $V_{\text {in }}$ : ..... 5.5V
Output Off-state Voltage, $\mathrm{V}_{\text {off }}$ :
Series UHC-400 and UHD-400. ..... 40V
Series UHC-400-1 and UHD-400-1 ..... 70V
Series UHC-500 and UHD-500 ..... 100 V
Output On-State Sink Current, Ion. ..... 500 mA
Suppression Diode Off-State Voltage, $\mathrm{V}_{\text {off }}$.
Series UHC-400 and UHD-400.40 V
Series UHC-400-1 and UHD-400-1 .....  70 V
Series UHC-500 and UHD-500. ..... 100 V
Suppression Diode On-State Current, ..... 500 mA
Operating Free-Air Temperature Range, $\mathrm{T}_{\mathrm{A}}$ ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{s}$ $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  | Units | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. |  |  |
| "1" Input Voltage | $V_{\text {in }(1)}$ |  | MIN |  |  |  | 2.0 |  |  | V |  |
| "0" Input Voltage | $V_{\text {in }(0)}$ |  | MIN |  |  |  |  |  | 0.8 | V |  |
| " 0 " Input Current at all Inputs except Strobe | $\mathrm{I}_{\text {in( }}(0)$ |  | MAX | 0.4 V | 4.5 V |  |  | $-0.55$ | -0.8 | mA | 1,2 |
| " 0 " Input Current at Strobe | In(0) |  | MAX | 0.4 V | 4.5 V |  |  | -1.1 | -1.6 | mA | 2 |
| " 1 " Input Current at all Inputs except Strobe | $\mathrm{I}_{\text {in( } 1)}$ |  | MAX | 2.4 V | OV |  |  |  | 40 | $\mu \mathrm{A}$ | 1 |
|  |  |  | MAX | 5.5 V | OV |  |  |  | 1 | mA | 1 |
| "1" Input Current at Strobe | I in(1) |  | MAX | 2.4 V | OV |  |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | MAX | 5.5 V | 0 V |  |  |  | 1 | mA |  |
| " 1 " Output Reverse Current <br> Series 400 <br> Series 400-1 <br> Series 500 | loff |  | MIN |  |  | 40 V |  |  | 100 | $\mu \mathrm{A}$ | 6 |
|  |  |  | MIN |  |  | 70 V |  |  | 100 | $\mu \mathrm{A}$ | 6 |
|  |  |  | MIN |  |  | 100 V |  |  | 100 | $\mu \mathrm{A}$ | 6 |
| "0" Output Voltage | Von | NOM | MIN |  |  | 150 mA |  |  | 0.5 | V | 6 |
|  |  | NOM | MIN |  |  | 250 mA |  |  | 0.7 | V | 6 |
|  |  | MAX | MIN |  |  | 150 mA |  |  | 0.6 | V | 6 |
|  |  | MAX | MIN |  |  | 250 mA |  |  | 0.8 | V | 6 |
| Diode Leakage Current | ILK | NOM | NOM |  |  | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM |  |  |  |  | 1.5 | 1.75 | V | 2, 4 |
| "1" Level Supply Current | $\mathrm{ICC}_{\text {(1) }}$ | NOM | MAX |  |  |  |  |  | 7.5 | mA | 5,6 |
| "0". Level Supply Current | ICC(0) | NOM | MAX |  |  |  |  |  | 26.5 | mA | 5,6 |

## NOTES:

1. Each input.
2. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
3. Measured at $V_{R}=V_{\text {off(min }}$.
4. Measured at $I_{f}=200 \mathrm{~mA}$.
5. Each gate.
6. Input test conditions are listed in Table IV.

Table IV
INPUT CONDITIONS FOR OUTPUT CHARACTERISTIC MEASUREMENTS

| Type UHC- or UHD- | " 1 " Output Reverse Current ( $I_{\text {off }}$ ) |  | "0" Output Voltage$\left(V_{\text {on }}\right)$ |  | " 1 " Level Supply Current (Icc(11) |  | "0" Level Supply Current ( $l_{c c .,}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Driven Input | Other Input | Driven Input | Other Input | Driven Input | Other Input | Driven Input | Other Input |
| 400, 400-1, 500 | 2.0 V | 2.0 V | 0.8 V | $V_{c c}$ | 5.0 V | 5.0 V | OV | OV |
| 402, 402-1, 502 | 2.0 V | 2.0 V | 0.8 V | 0.8 V | 5.0 V | 5.0 V | OV | OV |
| 403, 403-1, 503 | 2.0 V | OV | 0.8 V | 0.8 V | 5.0 V | 5.0 V | OV | OV |
| 406, 406-1, 506 | 2.0 V | 2.0 V | 0.8 V | $\mathrm{V}_{\mathrm{cc}}$ | 5.0 V | 5.0 V | OV | OV |
| 407, 407-1, 507 | 0.8 V | $V_{\text {cc }}$ | 2.0 V | 2.0 V | OV | OV | 5.0 V | 5.0 V |
| 408, 408-1, 508 | 0.8 V | $\mathrm{V}_{\text {cc }}$ | 2.0 V | 2.0 V | OV | OV | 5.0 V | 5.0 V |
| 432, 432-1, 532 | 0.8 V | 0.8 V | 2.0 V | OV | OV | OV | 5.0 V | 5.0 V |
| 433, 433-1, 533 | 0.8 V | 0.8 V | 2.0 V | OV | OV | OV | 5.0 V | 5.0V |

SWITCHING CHARACTERISTICS at $V_{C C}=5.0 V, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Turn-on Delay Time | $\mathrm{t}_{\mathrm{pd0}}$ |  |  |  |  |  |
| Series 400 |  | $\mathrm{V}_{S}=40 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=265^{\circ} \Omega$ (6 Watts) |  |  | 750 | ns |
| Series 400-1 |  | $\mathrm{V}_{S}=70 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=465 \Omega$ (10 Watts) |  |  | 750 | ns |
| Series 500 |  | $V_{S}=100 \mathrm{~V}, \mathrm{R}_{L}=670 \Omega$ (15 Watts) |  |  | 750 | ns |
| Turn-off Delay Time | $\mathrm{t}_{\mathrm{pd} 1}$ |  |  |  |  |  |
| Series 400 |  | $V_{S}=40 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=265 \Omega$ (6 Watts) |  |  | 500 | ns |
| Series 400-1 |  | $V_{S}=70 \mathrm{~V}, \mathrm{R}_{L}=465 \Omega$ (10 Watts) |  |  | 500 | ns |
| Series 500 |  | $V_{S}=100 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=670 \Omega$ (15 Watts) |  |  | 500 | ns |

## Typical Switching Test Circuit



Device Pinning


UHC-403
UHC-403-1
UHC-503


UHC-408
UHC-408-1
UHC-508


UHC-406
UHC-406-1
UHC-506


UHC-432
UHC-432-1
UHC-532


UHC-402 UHC-402-1 UHC-502


UHC-407
UHC-407-1 UHC-507


UHC-433
UHC-433-1
UHC-533

## Device Pinning <br> (Continued)



UHD-403
UHD-403-1
UHD-503


UHD-400
UHD-400-1
UHD-500


UHD-406 UHD-406-1
UHD-506


UHD-432
UHD-432-1
UHD-532


UHD-402
UHD-402-1
UHD-502


UHD-407
UHD-407-1
UHD-507


UHD-433
UHD-433-1
UHD-533

## SERIES ULS-2000H and ULQ-2000R HIGH-VOLTAGE, HIGH-CURRENT DARLINGTON TRANSISTOR ARRAYS

## FEATURES

- TIL, DTL, PMOS, or CMOS Compatible Inputs
- Peak Output Current to 600 mA
- Transient Protected Outputs
- Side-Brazed Hermetic Package, or
- Cer-DIP Package
- High-Reliability Screening Available
- Wide Operating Temperature Ranges

CCOMPRISED of seven silicon NPN Darlington power drivers on a common monolithic substrate, the Series ULS-2000H and ULQ-2000R arrays are ideally suited for driving relays, solenoids, lamps, and other devices with up to 3.0 A output current per package. The side-brazed, hermetically sealed Series ULS-2000H devices are rated for operation over the temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$, recommending them for military and aerospace applications. The Cer-DIP, industrial-grade hermetic Series ULQ-2000R devices are rated for use over the operating temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, allowing their use in commercial and industrial applications where severe environments may be encountered.

The twenty-five integrated circuits permit the circuit designer to select the optimum device for his application. There are two packages, five input characteristics, two output voltages, and two output currents covered by the listings. The appropriate part for use in specific applications can be determined from the Device Type Number Designation chart. Note that the high-voltage devices $\left(\mathrm{BV}_{\mathrm{CE}} \geq 95 \mathrm{~V}\right)$ are available in the Series ULS-2000H only. All units feature open collector outputs and integral diodes for inductive load transient suppression.

All Series ULS-2000H arrays are furnished in a 16-pin side-brazed dual in-line hermetic package

that conforms to the dimensional requirements of Military Specification MIL-M-38510 and meets the processing and environmental requirements of Military Standard MIL-STD-883, Methods 5004 and 5005.

Device Type Number Designation

| $V_{\text {cemax }}=$ | 50 V | 50 V | 95 V |
| :---: | :---: | :---: | :---: |
| $\mathrm{I}_{\text {C(MAx) }}=$ | 500 mA | 600 mA | 500 mA |
|  |  | Type Number |  |
| General Purpose | ULQ-2001R | ULQ-2011R |  |
| PMOS, CMOS | ULS-2001H | ULS-2011H | ULS-2021H |
| $14-25 \mathrm{~V}$ | ULQ-2002R | ULQ-2012R |  |
| PMOS | ULS-2002H | ULS-2012H | ULS-2022H |
| 5 V | ULQ-2003R | ULQ-2013R |  |
| TL, CMOS | ULS-2003H | ULS-2013H | ULS-2023H |
| $6-15 \mathrm{~V}$ | ULQ-2004R | ULQ-2014R |  |
| CMOS, PMOS | ULS-2004H | ULS-2014H | ULS-2024H |
| High Output | ULQ-2005R | ULQ-2015R |  |
| TTL | ULS-2005H | ULS-2015H | ULS-2025H |

# ABSOLUTE MAXIMUM RATINGS <br> Output Voltage, $\mathrm{V}_{\text {CE }}$ (Series 2000*, 2010*) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 50 V <br> (Series ULS-2020H) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 95 V <br> Input Voltage, $V_{\mathbb{I}}($ Series 2002*, 2003*, 2004*) . . . . . . . . . . . . . . . . . . . . . . . . . . 30 V <br> (Series 2005*) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 15 V <br> Peak Output Current, I Iout (Series 2000*, ULS-2020H) . . . . . . . . . . . . . . . . . . . . . 500 mA <br> (Series 2010*) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 600 mA <br> Ground Terminal Current, $\mathrm{I}_{\text {GND }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 3.0 A <br> Continuous Input Current, $\mathbb{I}_{\mathbb{N}}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 25 mA <br> Power Dissipation, $P_{D}$ (one Darlington pair) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1.0 W <br> (total package) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . See Graphs <br> Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ (Series ULS-2000H) $\ldots . . . . . . . .-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ <br> (Series ULQ-2000R) . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ <br> Storage Temperature Range, $\mathrm{T}_{\mathrm{s}} \ldots . . . . . . . . . . . . . . . . . . . . . . . . . . ~ . ~ . ~ 65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ 

## PARTIAL SCHEMATICS

Series 2001*
(each driver)


## Series 2002* <br> (each driver)



DWG. Ho. A-9650

Series 2003*
(each driver)

Series 2004*
(each driver)

Series 2005*
(each driver)


DwG. no. A-98984


DWG. No. A-9651

D4.5. 14. A. A-9535

(3. No. $1 \cdot 10.22 \mathrm{~m}$

[^28]
## SERIES ULS-2000H and ULQ-2000R

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices | Test Conditions |  |  | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Temp. |  | Fig. | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | All |  | $\mathrm{V}_{\mathrm{CE}}=50 \mathrm{~V}$ | 1 A | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 2002* |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~V}_{\mathbb{N}}=6 \mathrm{~V}$ | 1B | - | - | 500 | $\mu \mathrm{A}$ |
|  |  | 2004* |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=1 \mathrm{~V}$ | 1B | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CEISAT) }}$ | All | Min. | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=850 \mu \mathrm{~A}$ | 2 | - | 1.6 | 1.8 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=550 \mu \mathrm{~A}$ | 2 | - | 1.3 | 1.5 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.1 | 1.3 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | 2 | - | 1.25 | 1.6 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.1 | 1.3 | V |
|  |  |  |  | $\mathrm{T}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=250 \mu \mathrm{~A}$ | 2 | - | 0.9 | 1.1 | V |
|  |  |  | Max. | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | 2 | - | 1.6 | 1.8 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.3 | 1.5 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=250 \mu \mathrm{~A}$ | 2 | - | 1.1 | 1.3 | V |
| Input Current | $I_{\text {M }}^{\text {MON }}$ ) | 2002* |  | $V_{\text {WV }}=17 \mathrm{~V}$ | 3 | 480 | 850 | 1300 | $\mu \mathrm{A}$ |
|  |  | 2003* |  | $\mathrm{V}_{\mathrm{W}}=3.85 \mathrm{~V}$ | 3 | 650 | 930 | 1350 | $\mu \mathrm{A}$ |
|  |  | 2004* |  | $\mathrm{V}_{\text {W }}=5 \mathrm{~V}$ | 3 | 240 | 350 | 500 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathbb{W}}=12 \mathrm{~V}$ | 3 | 650 | 1000 | 1450 | $\mu \mathrm{A}$ |
|  |  | 2005* |  | $V_{1 N}=3 \mathrm{~V}$ | 3 | 1180 | 1500 | 2400 | $\mu \mathrm{A}$ |
|  | $1_{\text {Iroff }}$ | All | Max. | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}$ | 4 | 25 | 50 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {IV(O) }}$ | 2002* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 18 | V |
|  |  |  | Max. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 13 | V |
|  |  | 2003* | Min. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | 5 | - | - | 3.3 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | 5 | - | - | 3.6 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 3.9 | $V$ |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | 5 | - | - | 2.4 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | 5 | - | - | 2.7 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 3.0 | V |
|  |  | 2004* | Min. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=125 \mathrm{~mA}$ | 5 | - | - | 6.0 | V |
|  |  |  |  | $V_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | 5 | - | - | 8.0 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | 5 | - | - | 10 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 12 | V |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=125 \mathrm{~mA}$ | 5 | - | - | 5.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | 5 | - | - | 6.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | 5 | - | - | 7.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {ce }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 8.0 | V |
|  |  | 2005* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 3.0 | V |
|  |  |  | Max. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 2.4 | V |
| $\begin{aligned} & \text { D-C Forward Current } \\ & \text { Transfer Ratio } \end{aligned}$ | $\mathrm{hfE}^{\text {fe }}$ | 2001* | Min. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 2 | 500 | - | - | - |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 2 | 1000 | - | - | - |
| Input Capacitance | $\mathrm{C}_{\text {N }}$ | All | $+25^{\circ} \mathrm{C}$ |  | - | - | 15 | 25 | pF |
| Turn-On Delay | $t_{\text {PH }}$ | All | $+25^{\circ} \mathrm{C}$ | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 250 | 1000 | ns |
| Turn-Off Delay | $t_{\text {PHI }}$ | All | $+25^{\circ} \mathrm{C}$ | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 250 | 1000 | ns |
| Clamp Diode Leakage Current | $\mathrm{I}_{\text {R }}$ | All |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | 6 | - | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | All |  | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | 7 | - | 1.7 | 2.0 | V |

*Complete part number includes a prefix to indicate temperature range and a suffix to indicate package style. See following part number description.

Note 1: All limits stated apply to the complete Darlington series except as specified for a single device type.
Note 2: The $I_{\text {IN(OFF) }}$ current limit guarantees against partial turn-on of the output.
Note 3: The $\mathrm{V}_{\mathbb{I N O N})}$ voltage limit guarantees a minimum output sink current per the specified test conditions.

## SERIES ULS-2010H and ULQ-2010R

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices | Test Conditions |  |  | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Temp. |  | Fig. | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | All |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}$ | 1A | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 2012* |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~V}_{\mathbb{N}}=6 \mathrm{~V}$ | 1B | - | - | 500 | $\mu \mathrm{A}$ |
|  |  | 2014* |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~V}_{\text {IV }}=1 \mathrm{~V}$ | 1B | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {ces(Sat) }}$ | All | Min. | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=1100 \mu \mathrm{~A}$ | 2 | - | 1.8 | 2.1 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=850 \mu \mathrm{~A}$ | 2 | - | 1.6 | 1.8 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=550 \mu \mathrm{~A}$ | 2 | - | 1.3 | 1.5 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=600 \mu \mathrm{~A}$ | 2 | - | 1.7 | 1.9 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, I_{B}=500 \mu \mathrm{~A}$ | 2 | - | 1.25 | 1.6 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.1 | 1.3 | V |
|  |  |  | Max. | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=600 \mu \mathrm{~A}$ | 2 | - | 1.8 | 2.1 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | 2 | - | 1.6 | 1.8 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.3 | 1.5 | V |
| Input Current | $\mathrm{I}_{\text {M }}$ ( ${ }^{\text {a }}$ | 2012* |  | $\mathrm{V}_{\mathbb{N}}=17 \mathrm{~V}$ | 3 | 480 | 850 | 1300 | $\mu \mathrm{A}$ |
|  |  | 2013* |  | $\mathrm{V}_{\mathrm{N}}=3.85 \mathrm{~V}$ | 3 | 650 | 930 | 1350 | $\mu \mathrm{A}$ |
|  |  | 2014* |  | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}$ | 3 | 240 | 350 | 500 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathbb{N}}=12 \mathrm{~V}$ | 3 | 650 | 1000 | 1450 | $\mu \mathrm{A}$ |
|  |  | 2015* |  | $\mathrm{V}_{\mathbb{N}}=3 \mathrm{~V}$ | 3 | 1180 | 1500 | 2400 | $\mu \mathrm{A}$ |
|  | $1_{1 \times 0 F s}$ | All | Max. | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}$ | 4 | 25 | 50 | - | $\mu \mathrm{A}$ |
| Input Voltage | $V_{\text {INOM }}$ | 2012* | Min. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 23.5 | V |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 17 | V |
|  |  | 2013* | Min. | $V_{C E}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | 5 | - | - | 3.6 | $V$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 3.9 | $V$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 6.0 | $V$ |
|  |  |  | Max. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | 5 | - | - | 2.7 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 3.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 3.5 | V |
|  |  | 2014* | Min. | $V_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | 5 | - | - | 10 | V |
|  |  |  |  | $V_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 12 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 17 | V |
|  |  |  | Max. | $V_{C E}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | 5 | - | - | 7.0 | $V$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 8.0 | $V$ |
|  |  |  |  | $V_{C E}=2 V_{1} I_{C}=500 \mathrm{~mA}$ | 5 | - | - | 9.5 | $V$ |
|  |  | 2015* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 3.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 3.5 | V |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 2.4 | V |
|  |  |  |  | $V_{C f}=2 V_{,} T_{C}=500 \mathrm{~mA}$ | 5 | - | - | 2.6 | V |
| D-C Forward Current Transfer Ratio | $h_{\text {fe }}$ | 2011* | Min. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}$ | 2 | 450 | - | - | - |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{C E}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 2 | 900 | - | - | - |
| Input Capacitance | $\mathrm{C}_{11}$ | All | $+25^{\circ} \mathrm{C}$ |  | - | - | 15 | 25 | pF |
| Turn-On Delay | $\mathrm{taH}_{\text {PH }}$ | All | $+25^{\circ} \mathrm{C}$ | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {eut }}$ | - | - | 250 | 1000 | ns |
| Turn-Off Delay | $t_{\text {PHIL }}$ | All | $+25^{\circ} \mathrm{C}$ | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 250 | 1000 | ns |
| Clamp Diode Leakage Current | $I_{R}$ | All |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | 6 | - | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | All |  | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | 7 | - | 1.7 | 2.0 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{F}}=500 \mathrm{~mA}$ | 7 | - | - | 2.5 | V |

[^29]Note 1: All limits stated apply to the complete Darlington series except as specified for a single device type.
Note 2: The $\mathrm{I}_{\mathbb{N}(\mathbf{O F F})}$ current limit guarantees against partial turn-on of the output.
Note 3: The $\mathrm{V}_{\mathbb{N}(\mathbb{O})}$ voltage limit guarantees a minimum output sink current per the specified test conditions.

## SERIES ULS-2020H

## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)



Note 1: All limits stated apply to the complete Darlington series except as specified for a single device type.
Note 2: The $1_{\text {IN(OFF) }}$ current limit guarantees against partial turn-on of the output.
Note 3: The $V_{\mathbb{I N}(O N)}$ voltage limit guarantees a minimum output sink current per the specified test conditions.

## TEST FIGURES



FIGURE IA


FIGURE 4

FIGURE 2



FIGURE 1B


FIGURE 3


FIGURE 5

FIGURE 6


FIGURE 7

## SERIES ULS-2000H

## PEAK COLLECTOR CURRENT

## AS A FUNCTION OF DUTY CYCLE

AT $+50^{\circ} \mathrm{C}$


AT $+100^{\circ} \mathrm{C}$


NG. ко. $4-10.200 \mathrm{~A}$


AT $+\mathbf{1 2 5}^{\circ} \mathrm{C}$


## SERIES ULQ-2000R

PEAK COLLECTOR CURRENT
AS A FUNCTION OF DUTY CYCLE


ALLOWABLE PACKAGE POWER DISSIPATION SERIES ULS-2000H and ULQ-2000R


COLLECTOR CURRENT AS A FUNCTION OF INPUT CURRENT

## COLLECTOR CURRENT

 AS A FUNCTION OF SATURATION VOLTAGE


## SERIES ULS-2000H and ULQ-2000R PART NUMBERING SYSTEM



MIL = MILITARY GRADE WITH SCREENING TO MIL-STD-883, CLASS B

PACKAGE DESIGNATION.
C = UNPACKAGED CHIP
H = GLASS/METAL HERMETIC, DUAL IN-LINE
A = PLASTIC, DUAL IN-LINE
R $=$ CERAMIC/GLASS HERMETIC, DUAL IN-LINE
DEVICE INPUT CHARACTERISTICS
$1=$ GENERAL PURPOSE PMOS/CMOS
$2=14-25 \mathrm{~V}$ PMOS
$3=5 \mathrm{~V}$ TTL/CMOS
$4=6-15 \mathrm{~V}$ CMOS/PMOS
$5=$ HIGH-OUTPUT TTL
DEVICE OUTPUT CHARACTERISTICS
$0=50 \mathrm{~V}$ AND 500 mA MAXIMUM
$1=50 \mathrm{~V}$ AND 600 mA MAXIMUM
$2=95 \mathrm{~V}$ AND 500 mA MAXIMUM (PACKAGE H OR A ONLY)
DEVICE TYPE NUMBER (4 DIGITS IN 2000 SERIES)
OPERATING AMBIENT TEMPERATURE RANGE.
$\mathrm{N}=$ COMMERCIAL $\left(-20^{\circ} \mathrm{C} T 0+85^{\circ} \mathrm{C}\right)$
$Q=\operatorname{EXTENDED}\left(-40^{\circ} \mathrm{C} T 0+85^{\circ} \mathrm{C}\right)$
$S=$ FULL MILITARY $\left(-55^{\circ} \mathrm{C} \mathrm{TO}+125^{\circ} \mathrm{C}\right)$
FAMILY.

## INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE




SERIES 2005*

## SERIES 2004*


*Complete part number includes a prefix to indicate temperature range and a suffix to indicate package style. See previous part number description.

# ULS-2064 H through ULS-2077H 1.25 A QUAD DARLINGTON SWITCHES 

## FEATURES

- TTL, DTL, PMOS, or CMOS Compatible Inputs
- Transient-Protected Outputs
- Hermetically Sealed Package to MIL-M-38510
- High-Reliability Screening to MIL-STD-883, Class B

TNTENDED FOR MILITARY, aerospace, and related applications, ULS-2064H through ULS-2077H high-voltage high-current integrated circuit switches will interface from low-level logic to a variety of peripheral loads such as relays, solenoids, d-c and stepping motors, multiplexed LED and incandescent displays, heaters, and similar loads up to $400 \mathrm{~W}(1.25 \mathrm{~A}$ per output, $80 \mathrm{~V}, 12.5 \%$ duty cycle, $+50^{\circ} \mathrm{C}$ ).

The devices are specified with a minimum output breakdown of 50 volts, and $V_{C E(S U S)}$ minimum of 35 volts measured at 100 mA , or a minimum output breakdown of 80 volts, $\mathrm{V}_{\text {CE(SUS) }}$ minimum of 50 volts, and an output current specification of 1.25 A (saturated).

Types ULS-2064H, ULS-2065H, ULS-2068H and ULS-2069H are designed for use with TTL, DTL, Schottky TTL, and 5 V CMOS logic.

Types ULS-2066H, ULS-2067H, ULS-2070H and ULS-2071H are intended for use with 6 V to 15 V CMOS and PMOS input circuits.

All eight of these devices include integral transient suppression diodes for use with inductive loads.

Types ULS-2068H and ULS-2069H incorporate a pre-driver stage requiring a 5 V supply rail. Types ULS-2070H and ULS-2071H include an added gain stage requiring a 12 V (nominal) supply rail. The input drive requirements for these devices are reduced, while the output can switch currents up to 1.5 A .

Types ULS-2074H through ULS-2077H are intended for use in emitterfollower or similar isolated Darlington applications where common-emitter versions cannot be used. These circuits are identical with the ULS-2064H through ULS-2067H types except for the isolated Darlington pin-out and the omission of the suppression diodes.

All twelve Quad Darlington Switches are supplied in 16-pin hermetic dual-in-line packages. They meet the processing and environmental requirements of MIL-STD-883 Methods 5004 and 5005, and the dimensional requirements of MIL-M-38510.


ULS-2064H
through ULS-2067H


ULS-2068H through ULS-2071H


ULS-2074H
through ULS-2077H

## ABSOLUTE MAXIMUM RATINGS

## at $25^{\circ} \mathrm{C}$ Free-Air Temperature

for any one driver
(unless otherwise noted)


PACKAGE POWER DISSIPATION AS A FUNCTION OF TEMPERATURE


| Type Number | $V_{\text {cEX }}$ (max.) | $V_{\text {CESSUS) }}$ (min.) | $V_{\text {W }}$ (max.) | Application |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { ULS-2064H } \\ & \text { ULS-2065H } \end{aligned}$ | $\begin{aligned} & 50 \mathrm{~V} \\ & 80 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 35 \mathrm{~V} \\ & 50 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 15 \mathrm{~V} \\ & 15 \mathrm{~V} \end{aligned}$ | TLL, DTL, Schottky TTL, and 5 V CMOS |
| $\begin{aligned} & \text { ULS-2066H } \\ & \text { ULS-2067H } \end{aligned}$ | $\begin{aligned} & 50 \mathrm{~V} \\ & 80 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 35 \mathrm{~V} \\ & 50 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 30 \mathrm{~V} \\ & 30 \mathrm{~V} \end{aligned}$ | 6 to 15 V CMOS and PMOS |
| $\begin{aligned} & \text { ULS-2068H } \\ & \text { ULS-2069H } \end{aligned}$ | $\begin{aligned} & 50 \mathrm{~V} \\ & 80 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 35 \mathrm{~V} \\ & 50 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 15 \mathrm{~V} \\ & 15 \mathrm{~V} \end{aligned}$ | TLL, DTL, Schottky TL, and 5 V CMOS |
| $\begin{aligned} & \text { ULS-2070H } \\ & \text { ULS-2071H } \end{aligned}$ | $\begin{aligned} & 50 \mathrm{~V} \\ & 80 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 35 \mathrm{~V} \\ & 50 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 30 \mathrm{~V} \\ & 30 \mathrm{~V} \end{aligned}$ | 6 to 15 V CMOS and PMOS |
| $\begin{aligned} & \text { ULS-2074H } \\ & \text { ULS-2075H } \end{aligned}$ | $\begin{aligned} & 50 \mathrm{~V} \\ & 80 \mathrm{v} \end{aligned}$ | $\begin{aligned} & 35 \mathrm{~V} \\ & 50 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 30 \mathrm{~V} \\ & 60 \mathrm{~V} \end{aligned}$ | General Purpose |
| $\begin{aligned} & \text { ULS-2076H } \\ & \text { ULS-2077H } \\ & \hline \end{aligned}$ | $\begin{aligned} & 50 \mathrm{~V} \\ & 80 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 35 \mathrm{~V} \\ & 50 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 30 \mathrm{~V} \\ & 60 \mathrm{~V} \\ & \hline \end{aligned}$ | 6 to 15 V CMOS and PMOS |

Notes:

1. For allowable combinations of output current, number of outputs conducting, and duty cycle, see graphs following.
2. Input voltage is with reference to the substrate (no connection to any other pins) for the ULS-2074/75/76/77H, reference is ground for all other types.
3. Input current may be limited by maximum allowable input voltage.

## ULS-2064H through ULS-2067H

PARTIAL SCHEMATIC


$$
\begin{array}{ll}
\text { ULS-2064H } & R_{\mathbb{N}}=350 \Omega \\
\text { ULS-2065H } & \\
\text { ULS-2066H } & R_{\mathbb{I N}}=3 \mathrm{k} \Omega \\
\text { ULS-2067H }
\end{array}
$$



ULS-2068H through ULS-2071H

## PARTIAL SCHEMATIC

$$
\begin{aligned}
& \text { ULS-2068H } \quad R_{\text {IN }}=2.5 \mathrm{k} \Omega, R_{S}=900 \Omega \\
& \text { ULS-2069H } \\
& \text { ULS-2070H } \\
& \text { ULS-2071H }
\end{aligned} R_{\text {IN }}=11.6 \mathrm{k} \Omega, R_{S}=3.4 \mathrm{k} \Omega
$$



## ULS-2074H through ULS-2077H

PARTIAL SCHEMATIC


$$
\begin{array}{ll}
\text { ULS-2074H } & R_{I N}=350 \Omega \\
\text { ULS-2075H } & \\
\text { ULS-2076H } & R_{\mathbb{N}}=3 \mathrm{k} \Omega \\
\text { ULS-2077H }
\end{array}
$$



## ULS-2064H through ULS-2067H

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices |  | Test Conditions |  | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Temp. |  | Fig. | Min. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | ULS-2064/66H |  | $\mathrm{V}_{\text {cE }}=50 \mathrm{~V}$ | 1 | - | 500 | $\mu \mathrm{A}$ |
|  |  | ULS-2065/67H |  | $\mathrm{V}_{\text {CE }}=80 \mathrm{~V}$ | 1 | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {ces(Sus) }}$ | ULS-2064/66H |  | $\mathrm{T}_{\mathrm{c}}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{W}}=0.4 \mathrm{~V}$ | 2 | 35 | - | V |
|  |  | ULS-2065/67H |  | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{W}}=0.4 \mathrm{~V}$ | 2 | 50 | - | V |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {GEISAI) }}$ | All | $-55^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=1.1 \mathrm{~mA}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=1.7 \mathrm{~mA}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.25 \mathrm{~mA}$ | 3 | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=3.75 \mathrm{~mA}$ | 3 | - | 1.95 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=625 \mu \mathrm{~A}$ | 3 | - | 1.20 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{I}_{8}=935 \mu \mathrm{~A}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=1.25 \mathrm{~mA}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.0 \mathrm{~mA}$ | 3 | - | 1.75 | V |
|  |  |  | $+125^{\circ}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=625 \mu \mathrm{~A}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=935 \mu \mathrm{~A}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=1.25 \mathrm{~mA}$ | 3 | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.0 \mathrm{~mA}$ | 3 | - | 1.95 | V |
| Input Current | $T_{\text {m(OOM }}$ |  |  | $\mathrm{V}_{\mathrm{m}}=2.4 \mathrm{~V}$ | 4 | - | 4.3 | mA |
|  |  |  |  | $V_{1 W}=3.75 \mathrm{~V}$ | 4 | - | 9.6 | mA |
|  |  | ULS-2066/67H |  | $\mathrm{V}_{\text {IW }}=5.0 \mathrm{~V}$ | 4 | - | 1.8 | mA |
|  |  |  |  | $\mathrm{V}_{\text {W }}=12 \mathrm{~V}$ | 4 | - | 5.2 | mA |
| Input Voltage | $V_{\text {Mr(ow) }}$ | $\frac{\text { ULS-2064/65H }}{\text { ULS-2066/67H }}$ | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {ce }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | 5 | - | 3.1 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | 5 | - | 2.0 | V |
|  |  |  | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | 5 | - | 11.5 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {ct }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}$ | 5 | - | 6.5 | V |
| Turn-On Delay | $\mathrm{t}_{\mathrm{ON}}$ | All |  | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 1.0 | $\mu \mathrm{S}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {ff }}$ | All |  | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 1.5 | $\mu \mathrm{S}$ |
| Clamp Diode Leakage Current | $\mathrm{I}_{\mathrm{R}}$ | ULS-2064/66H |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | 6 | - | 100 | $\mu \mathrm{A}$ |
|  |  | ULS-2065/67H |  | $\mathrm{V}_{\mathrm{R}}=80 \mathrm{~V}$ | 6 | - | 100 | $\mu A$ |
| Clamp Diode Forward Voltage | $V_{F}$ | All |  | $\mathrm{I}_{\mathrm{F}}=1.25 \mathrm{~A}$ | 7 | - | 2.1 | V |

## ULS-2068H through ULS-2071H

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted),
$V_{S}=5.0 \mathrm{~V}$ (ULS-2068/69H) or $\mathrm{V}_{\mathrm{S}}=12 \mathrm{~V}$ (ULS-2070/71H)

| Characteristic | Symbol | Applicable Devices |  | Test Conditions | Fig. | Limits |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Temp. |  |  | Min. | Max. |  |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | ULS-2068/70H |  | $\mathrm{V}_{\mathrm{cE}}=50 \mathrm{~V}$ | 1 | - | 500 | $\mu \mathrm{A}$ |
|  |  | ULS-2069/71H |  | $\mathrm{V}_{\text {ce }}=80 \mathrm{~V}$ | 1 | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {ctisus) }}$ | ULS-2068/70H |  | $\mathrm{I}_{\mathrm{c}}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{W}}=0.4 \mathrm{~V}$ | 2 | 35 | - | V |
|  |  | ULS-2069/71H |  | $\mathrm{T}_{\mathrm{c}}=100 \mathrm{~mA}, \mathrm{~V}_{\text {W }}=0.4 \mathrm{~V}$ | 2 | 50 | - | $V$ |
| Collector-Emitter Saturation Voltage | $V_{\text {celsin) }}$ | ULS-2068/69H | $-55^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{~V}_{\mathbb{W}}=3.2 \mathrm{~V}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=750 \mathrm{~mA}, \mathrm{~V}_{\mathrm{W}}=3.2 \mathrm{~V}$ | 3 | - | 1.55 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}, \mathrm{~V}_{\mathrm{W}}=3.2 \mathrm{~V}$ | 3 | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{~V}_{\mathrm{N}}=3.2 \mathrm{~V}$ | 3 | - | 1.95 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}, \mathrm{~V}_{\mathbb{W}}=2.9 \mathrm{~V}$ | 3 | - | 1.20 | V |
|  |  |  |  | $\mathrm{T}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{~V}_{\text {W1 }}=2.9 \mathrm{~V}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}, \mathrm{~V}_{\mathrm{W}}=2.9 \mathrm{~V}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{~V}_{\mathrm{m}}=2.9 \mathrm{~V}$ | 3 | - | 1.75 | V |
|  |  |  | $+125^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{~V}_{\text {IV }}=2.8 \mathrm{~V}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{~V}_{\mathbb{W}}=2.8 \mathrm{~V}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}, \mathrm{~V}_{\mathrm{N}}=2.8 \mathrm{~V}$ | 3 | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.25 \mathrm{~A}, \mathrm{~V}_{\mathrm{m}}=2.8 \mathrm{~V}$ | 3 | - | 1.95 | V |
|  |  | ULS-2070/71H | $-55^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{~V}_{\mathrm{W}}=5.5 \mathrm{~V}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{~V}_{\text {W }}=5.5 \mathrm{~V}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}, \mathrm{~V}_{\mathrm{W}}=5.5 \mathrm{~V}$ | 3 | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.25 \mathrm{~A}, \mathrm{~V}_{\text {IV }}=5.5 \mathrm{~V}$ | 3 | - | 1.95 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{~V}_{\text {IV }}=5.1 \mathrm{l}$ | 3 | - | 1.20 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{~V}_{\mathrm{WH}}=5.1 \mathrm{~V}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{~V}_{\mathrm{IW}}=5.1 \mathrm{~V}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{~V} \mathrm{~V}_{\mathrm{W}}=5.1 \mathrm{~V}$ | 3 | - | 1.75 | V |
|  |  |  | $+125^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}, \mathrm{~V}_{\text {IW }}=5.0 \mathrm{~V}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{~V}_{\text {IV }}=5.0 \mathrm{~V}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{~V}_{\mathrm{W}}=5.0 \mathrm{~V}$ | 3 | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{~V}_{\mathbb{1}}=5.0 \mathrm{~V}$ | 3 | - | 1.95 | V |
| Input Current | 1 Imow) | ULS-2068/69H | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathrm{N}}=3.2 \mathrm{~V}$ | 4 | - | 600 | $\mu \mathrm{A}$ |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathrm{N}}=2.75 \mathrm{~V}$ | 4 | - | 550 | $\mu \mathrm{A}$ |
|  |  |  | $+125^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {W }}=2.75 \mathrm{~V}$ | 4 | - | 850 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{IV}}=3.75 \mathrm{~V}$ | 4 | - | 1000 | $\mu \mathrm{A}$ |
|  |  | ULS-2070/71H |  | $V_{\text {IV }}=5.0 \mathrm{~V}$ | 4 | - | 400 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{10}=12 \mathrm{~V}$ | 4 | - | 1250 | $\mu \mathrm{A}$ |
| Input Voltage | $V_{\text {w(ow) }}$ | ULS-2068/69H | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {cE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}$ | 5 | - | 3.2 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {cE }}=2.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=1.0 \mathrm{~A}$ | 5 | - | 2.75 | $V$ |
|  |  | ULS-2070/71H | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | 5 | - | 5.0 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {CE }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}$ | 5 | - | 5.0 | $\checkmark$ |
| Supply Current | $\mathrm{I}_{5}$ | ULS-2068/69H |  | $\mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}, \mathrm{~V}_{11}=3.2 \mathrm{~V}$ | 8 | - | 6.0 | mA |
|  |  | ULS-2070/71H |  | $\mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}, \mathrm{~V}_{\mathrm{WH}}=5.0 \mathrm{~V}$ | 8 | - | 4.5 | mA |
| Turn-On Delay | $\mathrm{t}_{01}$ | All |  | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {eit }}$ | - | - | 1.0 | $\mu \mathrm{S}$ |
| Iurn-Off Delay | $\mathrm{t}_{\text {ofr }}$ | All |  | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {wit }}$ | - | - | 1.5 | $\mu \mathrm{s}$ |
| Clamp Diode Leakage Current | $I_{\text {R }}$ | ULS-2068/70H |  | $\mathrm{V}_{8}=50 \mathrm{~V}$ | 6 | - | 100 | $\mu \mathrm{A}$ |
|  |  | ULS-2069/71H |  | $\mathrm{V}_{\mathrm{B}}=80 \mathrm{~V}$ | 6 | - | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Fonward Voltage | $\mathrm{V}_{\mathrm{F}}$ | All |  | $\mathrm{I}_{\mathrm{f}}=1.25 \mathrm{~A}$ | 7 | - | 2.1 | V |

## ULS-2074H through ULS-2077H

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices |  | Test Conditions |  | Limits |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Temp. |  | Fig. | Min. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | ULS-2074/76H |  | $\mathrm{V}_{\text {cE }}=50 \mathrm{~V}$ | 1 | - | 500 | $\mu \mathrm{A}$ |
|  |  | ULS-2075/77 |  | $\mathrm{V}_{\text {cE }}=80 \mathrm{~V}$ | 1 | - | 500 | $\mu \mathrm{A}$ |
| Output Sustaining Voltage | $\mathrm{V}_{\text {cessus) }}$ | ULS-2074/76 H |  | $\mathrm{I}_{\mathrm{c}}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{N}}=0.4 \mathrm{~V}$ | 2 | 35 | - | $V$ |
|  |  | ULS-2075/77H |  | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{~V}_{\mathrm{W}}=0.4 \mathrm{~V}$ | 2 | 50 | - | V |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CEISAD }}$ | All | $-55^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=1.1 \mathrm{~mA}$ | 3 | - | 1.35 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=1.7 \mathrm{~mA}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.25 \mathrm{~mA}$ | 3 | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.25 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=3.75 \mathrm{~mA}$ | 3 | - | 1.95 | $V$ |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=625 \mu \mathrm{~A}$ | 3 | - | 1.20 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=935 \mu \mathrm{~A}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=1.25 \mathrm{~mA}$ | 3 | - | 1.55 | $V$ |
|  |  |  |  | $\mathrm{I}_{6}=1.25 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.0 \mathrm{~mA}$ | 3 | - | 1.75 | V |
|  |  |  | $+125^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=625 \mu \mathrm{~A}$ | 3 | - | 1.35 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=750 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=935 \mu \mathrm{~A}$ | 3 | - | 1.55 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{g}}=1.25 \mathrm{~mA}$ | 3 | - | 1.75 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{c}}=1.25 \mathrm{~A}, \mathrm{I}_{\mathrm{B}}=2.0 \mathrm{~mA}$ | 3 | - | 1.95 | V |
| Input Current | $1_{\text {m(OM) }}$ | ULS-2074/75 |  | $\mathrm{V}_{\mathrm{VW}}=2.4 \mathrm{~V}$ | 4 | - | 4.3 | mA |
|  |  |  |  | $\mathrm{V}_{\mathrm{W}}=3.75 \mathrm{~V}$ | 4 | - | 9.6 | mA |
|  |  | ULS-2076/77H |  | $\mathrm{V}_{1 \mathrm{~V}}=5.0 \mathrm{~V}$ | 4 | - | 1.8 | mA |
|  |  |  |  | $\mathrm{V}_{\mathrm{k}}=12 \mathrm{~V}$ | 4 | - | 5.2 | mA |
| Input Voltage | $V_{\text {(maow }}$ | ULS-2074/75H | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {cF }}=2.0 \mathrm{~V}, \mathrm{I}_{6}=1.0 \mathrm{~A}$ | 5 | - | 3.1 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {CF }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | 5 | - | 2.0 | V |
|  |  | ULS-2076/77H | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {cf }}=2.0 \mathrm{~V} \mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}$ | 5 | - | 1.5 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {cf }}=2.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}$ | 5 | - | 6.5 | $V$ |
| Turn-On Delay | $\mathrm{t}_{01}$ | All |  | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {vel }}$ | - | - | 1.0 | $\mu \mathrm{s}$ |
| Turn-Off Delay | $\mathrm{t}_{\text {esf }}$ | All |  | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {aul }}$ | - | - | 1.5 | $\mu \mathrm{s}$ |

## TEST FIGURES




Figure 7


Figure 8

NOTE: Diodes not applicable to Type ULS-2074H through ULS-2077H.

## input Current as a function of input voltage




## COLLECTOR CURRENT AS A FUNCTION OF INPUT CURRENT



ALLOWABLE PEAK COLLECTOR CURRENT AS A FUNCTION OF DUTY CYCLE

AT $+50^{\circ} \mathrm{C}$


AT $+75^{\circ} \mathrm{C}$



# SERIES ULS-2800H and ULQ-2800R HIGH-VOLTAGE, HIGH-CURRENT DARLINGTON TRANSISTOR ARRAYS 

## FEATURES

- TTL, DTL, PMOS, or CMOS Compatible Inputs
- Peak Output Current to 600 mA
- Transient Protected Outputs
- Side-Brazed Hermetic Package, or
- Cer-DIP Package
- High-Reliability Screening Available
- Wide Operating Temperature Ranges

DESIGNED for interfacing between low-level logic circuitry and high-power loads, the Series ULS-2800H and ULQ-2800R arrays consist of eight silicon NPN Darlington power drivers on a common monolithic substrate. The choice of five input characteristics, two output voltage ratings ( 50 or 95 V ), two output current ratings ( 500 or 600 mA ), and two package styles (suffix 'H' or 'R') allow the circuit designer to select the optimum device for any specific application.

The side-brazed, hermetically sealed Series ULS-2800H devices are rated for operation over the temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$, recommending them for military and aerospace applications. The cer-DIP, industrial grade hermetic Series ULQ-2800R devices are rated for use over the operating temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, permitting their use in commercial and industrial applications where severe environmental conditions may be encountered.

The appropriate specific part number for use in standard logic applications can be determined from the Device Type Number Designation chart. Note that the high-voltage devices $\left(\mathrm{BV}_{\mathrm{CE}} \geq 95 \mathrm{~V}\right)$ are available in the Series ULS-2800H only. All units feature open collector outputs and integral diodes for inductive load transient suppression.

All Series ULS-2800H Darlington power drivers are furnished in an 18-pin side-brazed dual in-line

hermetic package that meets the processing and environmental requirements of Military Standard MIL-STD-883, Methods 5004 and 5005.

Device Type Number Designation

| $\begin{aligned} & V_{\text {CE(MAX) }}= \\ & \mathrm{I}_{\mathrm{C}(\text { MAX })}= \end{aligned}$ | $\begin{gathered} 50 \mathrm{~V} \\ 500 \mathrm{~mA} \end{gathered}$ | $\begin{gathered} 50 \mathrm{~V} \\ 600 \mathrm{~mA} \end{gathered}$ | $\begin{gathered} 95 \mathrm{~V} \\ 500 \mathrm{~mA} \end{gathered}$ |
| :---: | :---: | :---: | :---: |
|  | Type Number |  |  |
| General Purpose PMOS, CMOS | $\begin{aligned} & \text { ULQ-2801R } \\ & \text { ULS-2801H } \end{aligned}$ | $\begin{aligned} & \text { ULQ-2811R } \\ & \text { ULS-2811H } \end{aligned}$ | ULS-2821H |
| $\begin{gathered} 14-25 \mathrm{~V} \\ \text { PMOS } \end{gathered}$ | $\begin{aligned} & \text { ULQ-2802R } \\ & \text { ULS-2802H } \end{aligned}$ | $\begin{aligned} & \text { ULQ-2812R } \\ & \text { ULS-2812H } \end{aligned}$ | ULS-2822H |
| $\stackrel{5 \mathrm{~V}}{\mathrm{ML}, \mathrm{CMOS}}$ | $\begin{aligned} & \text { ULQ-2803R } \\ & \text { ULS-2803H } \end{aligned}$ | ULQ-2813R ULS-2813H | ULS-2823H |
| $6-15 \mathrm{~V}$ <br> CMOS, PMOS | $\begin{aligned} & \text { ULQ-2804R } \\ & \text { ULS-2804H } \end{aligned}$ | $\begin{aligned} & \text { ULQ-2814R } \\ & \text { ULS-2814H } \end{aligned}$ | ULS-2824H |
| High Output TTL | $\begin{aligned} & \text { ULQ-2805R } \\ & \text { ULS-2805H } \end{aligned}$ | $\begin{aligned} & \text { ULQ-2815R } \\ & \text { ULS-2815H } \end{aligned}$ | ULS-2825H |

## ABSOLUTE MAXIMUM RATINGS

Output Voltage, $\mathrm{V}_{\text {CE }}$ (Series 2800*, 2810*) ..... 50 V
(Series ULS-2820H) ..... 95 V
Input Voltage, $\mathrm{V}_{\mathbb{W}}$ (Series 2802*, 2803*, 2804*) ..... 30 V
(Series 2805*) ..... 15 V
Peak Output Current, I Iout (Series 2800*, ULS-2820H) ..... 500 mA
(Series 2810*) ..... 600 mA
Ground Terminal Current, I IGND ..... 3.0 A
Continuous Input Current, $\mathrm{I}_{\mathbb{N}}$ ..... 25 mA
Power Dissipation, $P_{D}$ (one Darlington pair) ..... 1.0 W(total package) . . . . . . . . . . . . . . . . . . . . . . . . . . . . See Graphs
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ (Series ULS-2800H) ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$(Series ULQ-2800R) . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## PARTIAL SCHEMATICS

## Series 2801* <br> (each driver)



Owi. No. A-9650

## Series 2803*

(each driver)


Dw. No. A-9651


Series 2805*
(each driver)


[^30]
## SERIES ULS-2800H and ULQ-2800R

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices | Test Conditions |  |  | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Temp |  | Fig. | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | All |  | $\mathrm{V}_{\text {cf }}=50 \mathrm{~V}$ | 1A | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 2802* |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~V}_{\text {W }}=6 \mathrm{~V}$ | 1 B | - | - | 500 | $\mu \mathrm{A}$ |
|  |  | 2804* |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=1 \mathrm{~V}$ | 1B | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CESSAT) }}$ | All | Min. | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=850 \mu \mathrm{~A}$ | 2 | - | 1.6 | 1.8 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=550 \mu \mathrm{~A}$ | 2 | - | 1.3 | 1.5 | $V$ |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.1 | 1.3 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | 2 | - | 1.25 | 1.6 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.1 | 1.3 | V |
|  |  |  |  | $\mathrm{T}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=250 \mu \mathrm{~A}$ | 2 | - | 0.9 | 1.1 | V |
|  |  |  | Max. | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | 2 | - | 1.6 | 1.8 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.3 | 1.5 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=250 \mu \mathrm{~A}$ | 2 | - | 1.1 | 1.3 | V |
| Input Current | $\mathrm{I}_{\text {INON) }}$ | 2802* |  | $\mathrm{V}_{\mathbb{I} \mathrm{V}}=17 \mathrm{~V}$ | 3 | 480 | 850 | 1300 | $\mu \mathrm{A}$ |
|  |  | 2803* |  | $\mathrm{V}_{\mathbb{N}}=3.85 \mathrm{~V}$ | 3 | 650 | 930 | 1350 | $\mu \mathrm{A}$ |
|  |  | 2804* |  | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}$ | 3 | 240 | 350 | 500 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=12 \mathrm{~V}$ | 3 | 650 | 1000 | 1450 | $\mu \mathrm{A}$ |
|  |  | 2805* |  | $V_{N}=3 \mathrm{~V}$ | 3 | 1180 | 1500 | 2400 | $\mu \mathrm{A}$ |
|  | $I_{\text {INOFF) }}$ | All | Max. | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}$ | 4 | 25 | 50 | - | $\mu \mathrm{A}$ |
| Input Voltage | $\mathrm{V}_{\text {INON }}$ |  | Min. | $V_{C E}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 18 | $V$ |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=300 \mathrm{~mA}$ | 5 | - | - | 13 | V |
|  |  | 2803* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | 5 | - | - | 3.3 | V |
|  |  |  |  | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | 5 | - | - | 3.6 | $V$ |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 3.9 | V |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | 5 | - | - | 2.4 | V |
|  |  |  |  | $V_{\text {Cf }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=250 \mathrm{~mA}$ | 5 | - | - | 2.7 | V |
|  |  |  |  | $V_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 3.0 | V |
|  |  | 2804* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=125 \mathrm{~mA}$ | 5 | - | - | 6.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | 5 | - | - | 8.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{~T}_{\mathrm{c}}=275 \mathrm{~mA}$ | 5 | - | - | 10 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 12 | V |
|  |  |  | Max. | $V_{\text {CF }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=125 \mathrm{~mA}$ | 5 | - | - | 5.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}$ | 5 | - | - | 6.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CF }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | 5 | - | - | 7.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 8.0 | V |
|  |  | 2805* | Min. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=350 \mathrm{~mA}$ | 5 | - | - | 3.0 | V |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 2.4 | V |
| D-C Forward Current Transfer Ratio | $\mathrm{h}_{\mathrm{fE}}$ | 2801* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=350 \mathrm{~mA}$ | 2 | 500 | - | - | - |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 2 | 1000 | - | - | - |
| Input Capacitance | $\mathrm{C}_{\text {IN }}$ | All | $+25^{\circ} \mathrm{C}$ |  | - | - | 15 | 25 | pF |
| Turn-On Delay | $t_{\text {PH }}$ | All | $+25^{\circ} \mathrm{C}$ | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 250 | 1000 | ns |
| Turn-Off Delay | $\mathrm{t}_{\text {PHL }}$ | All | $+25^{\circ} \mathrm{C}$ | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 250 | 1000 | ns |
| Clamp Diode Leakage Current | $I_{\text {R }}$ | All |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | 6 | - | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $\mathrm{V}_{\mathrm{F}}$ | All |  | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | 7 | - | 1.7 | 2.0 | V |

[^31]Note 1: All limits stated apply to the complete Darlington series except as specified for a single device type.
Note 2: The $I_{\text {INOFF) }}$ current limit guarantees against partial turn-on of the output.
Note 3: The $V_{\mathbb{N}(O N)}$ voltage limit guarantees a minimum output sink current per the specified test conditions.

## SERIES ULS-28 $10 H$ and ULQ-28 $10 R$

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices |  | Test Conditions | Limits |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Temp |  | Fig. | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | All |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}$ | 1 A | - | - | 100 | $\mu \mathrm{A}$ |
|  |  | 2812* |  | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}, \mathrm{~V}_{\text {IV }}=6 \mathrm{~V}$ | 1B | - | - | 500 | $\mu \mathrm{A}$ |
|  |  | 2814* |  | $\mathrm{V}_{\text {cf }}=50 \mathrm{~V}, \mathrm{~V}_{\text {IV }}=1 \mathrm{~V}$ | 1B | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {Gefsat }}$ | All | Min. | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=1100 \mu \mathrm{~A}$ | 2 | - | 1.8 | 2.1 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=850 \mu \mathrm{~A}$ | 2 | - | 1.6 | 1.8 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=550 \mu \mathrm{~A}$ | 2 | - | 1.3 | 1.5 | V |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=600 \mu \mathrm{~A}$ | 2 | - | 1.7 | 1.9 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | 2 | - | 1.25 | 1.6 | V |
|  |  |  |  | $I_{C}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.1 | 1.3 | V |
|  |  |  | Max. | $\mathrm{I}_{6}=500 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=600 \mu \mathrm{~A}$ | 2 | - | 1.8 | 2.1 | V |
|  |  |  |  | $\mathrm{I}_{C}=350 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ | 2 | - | 1.6 | 1.8 | V |
|  |  |  |  | $\mathrm{I}_{6}=200 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=350 \mu \mathrm{~A}$ | 2 | - | 1.3 | 1.5 | V |
| Input Current | $\mathrm{I}_{\text {INOW }}$ | 2812* |  | $\mathrm{V}_{\mathbb{N}}=17 \mathrm{~V}$ | 3 | 480 | 850 | 1300 | $\mu \mathrm{A}$ |
|  |  | 2813* |  | $\mathrm{V}_{\mathrm{N}}=3.85 \mathrm{~V}$ | 3 | 650 | 930 | 1350 | $\mu \mathrm{A}$ |
|  |  | 2814* |  | $\mathrm{V}_{\mathbb{1}}=5 \mathrm{~V}$ | 3 | 240 | 350 | 500 | $\mu \mathrm{A}$ |
|  |  |  |  | $\mathrm{V}_{\mathrm{W}}=12 \mathrm{~V}$ | 3 | 650 | 1000 | 1450 | $\mu \mathrm{A}$ |
|  |  | 2815* |  | $V_{\text {W }}=3 \mathrm{~V}$ | 3 | 1180 | 1500 | 2400 | $\mu \mathrm{A}$ |
|  | $\mathrm{I}_{\text {woff }}$ | All | Max. | $\mathrm{I}_{\mathrm{c}}=500 \mu \mathrm{~A}$ | 4 | 25 | 50 | - | $\mu \mathrm{A}$ |
| Input Voltage | $V_{\text {INON }}$ | 2812* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}$ | 5 | - | - | 23.5 | V |
|  |  |  | Max. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 17 | V |
|  |  | 2813* | Min. | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | 5 | - | - | 3.6 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 3.9 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}$ | 5 | - | - | 6.0 | V |
|  |  |  | Max. | $\mathrm{V}_{C E}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=250 \mathrm{~mA}$ | 5 | - | - | 2.7 | V |
|  |  |  |  | $V_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=300 \mathrm{~mA}$ | 5 | - | - | 3.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 3.5 | V |
|  |  | 2814* | Min. | $V_{C E}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | 5 | - | - | 10 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 12 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 17 | V |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=275 \mathrm{~mA}$ | 5 | - | - | 7.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 8.0 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}$ | 5 | - | - | 9.5 | V |
|  |  | 2815* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 3.0 | V |
|  |  |  |  | $V_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 5 | - | - | 3.5 | V |
|  |  |  | Max. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}$ | 5 | - | - | 2.4 | V |
|  |  |  |  | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}$ | 5 | - | - | 2.6 | V |
| D-C Forward Current Transfer Ratio | $\mathrm{h}_{\mathrm{fE}}$ | 2811* | Min. | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=500 \mathrm{~mA}$ | 2 | 450 | - | - | - |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {CE }}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}$ | 2 | 900 | - | - | - |
| Input Capacitance | $\mathrm{C}_{\text {IV }}$ | All | $+25^{\circ} \mathrm{C}$ |  | - | - | 15 | 25 | pF |
| Turn-On Delay | $t_{\text {PH }}$ | All | $+25^{\circ} \mathrm{C}$ | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 250 | 1000 | ns |
| Turn-Off Delay | $t_{\text {Pr1 }}$ | All | $+25^{\circ} \mathrm{C}$ | $0.5 \mathrm{E}_{\text {in }}$ to $0.5 \mathrm{E}_{\text {out }}$ | - | - | 250 | 1000 | ns |
| Clamp Diode Leakage Current | $I_{R}$ | All |  | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | 6 | - | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward <br> Voltage | $V_{F}$ | All |  | $I_{\text {f }}=350 \mathrm{~mA}$ | 7 | - | 1.7 | 2.0 | V |
|  |  |  |  | $\mathrm{I}_{\mathrm{F}}=500 \mathrm{~mA}$ | 7 | - | - | 2.5 | V |

*Complete part number includes a prefix to indicate temperature range and a suffix to indicate package style. See following part number description.
Note 1: All limits stated apply to the complete Darlington series except as specified for a single device type.
Note 2: The $I_{\text {N(OFF) }}$ current limit guarantees against partial turn-on of the output.
Note 3: The $V_{\mathbb{N}(\mathcal{O N})}$ voltage limit guarantees a minimum output sink current per the specified test conditions.

## SERIES ULS-2820H

## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)



Note 1: All limits stated apply to the complete Darlington series except as specified for a single device type.
Note 2: The $\mathrm{I}_{\text {IN(Off) }}$ current limit guarantees against partial turn-on of the output.
Note 3: The $V_{\mathbb{I N O}(\mathbb{N}}$ voitage limit guarantees a minimum output sink current per the specified test conditions.

## TEST FIGURES



FIGURE 1A

FIGURE 2

FIGURE 4

FIGURE 6



FIGURE IB


FIGURE 7

## SERIES ULS-2800H

PEAK COLLECTOR CURRENT AS A FUNCTION OF DUTY CYCLE

AT $+50^{\circ} \mathrm{C}$


AT $+100^{\circ} \mathrm{C}$


$$
\text { AT }+75^{\circ} \mathrm{C}
$$




## SERIES ULQ-2800R

PEAK COLLECTOR CURRENT AS A FUNCTION OF DUTY CYCLE


AT $+75^{\circ} \mathrm{C}$


## ALLOWABLE PACKAGE POWER DISSIPATION

SERIES ULS-2800H and ULQ-2800R


N5. M0. A-10.479

## COLLECTOR CURRENT

 AS A FUNCTION OF INPUT CURRENTCOLLECTOR CURRENT
AS A FUNCTION OF SATURATION VOLTAGE


OWG. NO. A-9754B

## SERIES ULS-2800H and ULQ-2800R PART NUMBERING SYSTEM



MIL $=$ MILITARY GRADE WITH SCREENING TO MIL-STD-883, CLASS B

PACKAGE DESIGNATION.
$\mathrm{C}=$ UNPACKAGED CHIP
H = GLASS/METAL HERMETIC, DUAL IN-LINE
A = PLASTIC, DUAL IN-LINE
R $=$ CERAMIC/GLASS HERMETIC, DUAL IN-LINE
DEVICE INPUT CHARACTERISTICS
$1=$ GENERAL PURPOSE PMOS/CMOS
$2=14-25 \mathrm{~V}$ PMOS
$3=5 \mathrm{~V} \mathrm{TTL} / \mathrm{CMOS}$
$4=6-15 \mathrm{~V}$ CMOS/PMOS
$5=$ HIGH-OUTPUT TTL
DEVICE OUTPUT CHARACTERISTICS
$0=50 \mathrm{~V}$ AND 500 mA MAXIMUM
$1=50 \mathrm{~V}$ AND 600 mA MAXIMUM
$2=95 \mathrm{~V}$ AND 500 mA MAXIMUM (PACKAGE H OR A ONLY)
DEVICE TYPE NUMBER (4 DIGITS IN 2800 SERIES)
OPERATING AMBIENT TEMPERATURE RANGE.
$N=$ COMMERCIAL $\left(-20^{\circ} \mathrm{C} T 0+85^{\circ} \mathrm{C}\right)$
$Q=$ EXTENDED $\left(-40^{\circ} \mathrm{C} T 0+85^{\circ} \mathrm{C}\right)$
$S=$ FULL MILITARY $\left(-55^{\circ} \mathrm{C} T 0+125^{\circ} \mathrm{C}\right)$
faMILY.

## INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE

SERIES 2803*

## SERIES 2802*




SERIES 2804*


*Complete part number includes a prefix to indicate temperature range and a suffix to indicate package
style. See previous part number description.

## UDQ-2956R and UDQ-2957R HIGH-VOLTAGE, HIGH-CURRENT SOURCE DRIVERS

## EACH OF THESE SOURCE-DRIVER

 arrays has five NPN Darlington-pair outputs and five PNP common-base inputs controlled by a single ENABLE stage.Types UDQ-2956R and UDQ-2957R are typically used to switch the ground ends of loads such as telephone relays, PIN diodes, LEDs and similar devices directly connected to negative supplies. Internal transient-suppression diodes allow use of the drivers with inductive loads.

Each output stage of both integrated circuits will withstand output OFF voltages of -80 V and load currents as high as -500 mA . Under normal operating conditions, the five drivers will simultaneously handle load currents of -170 mA at ambient temperatures of up to $+70^{\circ} \mathrm{C}$.

Type UDQ-2956R is designed for use with PMOS or CMOS logic input levels operating with supply voltages of 6 V to 16 V . Type UDQ2957R has input current-limiting resistors that permit its operation with TTL, Schottky TTL, DTL and 5 V CMOS.

Both devices are supplied in industrial-grade, hermetically sealed 14 -pin dual in-line ceramic packages rated for use over the temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Input connections are on one side of the packages, output connections on the other, to simplify applications designs.

The substrate of Type UDQ-2956R and Type UDQ-2957R should be tied to the most negative supply available in order to maintain isolation between drivers.


## ABSOLUTE MAXIMUM RATINGS at $25^{\circ} \mathrm{C}$ Free-Air Temperature (reference pin 7)

Supply Voltage, $\mathrm{V}_{\mathrm{EE}}$. ............................... . . -80 V
Input Voltage, $\mathrm{V}_{\mathbb{N}}$ (UDQ-2956R) . . . . . . . . . . . . . . . . . +20 V
(UDQ-2957R) . . . . . . . . . . . . . . . . . +10 V
Output Current, $\mathrm{I}_{\text {out }}$. . . . . . . . . . . . . . . . . . . . . . . -500 mA
Power Dissipation, $P_{D}$ (any one driver) . . . . . . . . . . . . . 1.0 W
(total package) . . . . . . . . . . . $1.67 \mathrm{~W}^{*}$
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots . .-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{s} \ldots . . . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

[^32]
## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Applicable Devices | Temp. | Test Conditions | Limit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | UDQ-2956R |  | $\mathrm{V}_{\text {IW }}=\mathrm{V}_{\text {EMBEE }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}$ | -200 $\mu \mathrm{A}$ Max. |
|  |  |  |  | $V_{\text {IN }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {EMBBIE }}=15 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}$ | $-200 \mu$ A Max. |
|  |  |  |  | $\mathrm{V}_{\text {W }}=15 \mathrm{~V}, \mathrm{~V}_{\text {EMBBIE }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUI }}=-80 \mathrm{~V}$ | $-200 \mu \mathrm{~A}$ Max. |
|  |  | UDQ-2957R |  | $V_{\text {IT }}=\mathrm{V}_{\text {EMBEL }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}$ | $-200 \mu \mathrm{~A}$ Max. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {EMBEE }}=3.85 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}$ | -200 $\mu \mathrm{A}$ Max. |
|  |  |  |  | $\mathrm{V}_{\mathrm{W}}=3.85 \mathrm{~V}, \mathrm{~V}_{\text {EMBEE }}=0.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-80 \mathrm{~V}$ | $-200 \mu \mathrm{~A}$ Max. |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CESSAT }}$ | UDQ-2956R | $-40^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {W }}=6.0 \mathrm{~V}, \mathrm{I}_{\text {out }}=-100 \mathrm{~mA}$ | -1.40 V Max. |
|  |  |  |  | $\mathrm{V}_{\mathbb{W}}=7.0 \mathrm{~V}, \mathrm{~T}_{\text {out }}=-175 \mathrm{~mA}$ | -1.55 V Max. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=10 \mathrm{~V}, \mathrm{I}_{\text {out }}=-350 \mathrm{~mA}$ | -1.90 V Max. |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathrm{W}}=6.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}$ | -1.20 V Max. |
|  |  |  |  | $\mathrm{V}_{\mathbb{W}}=7.0 \mathrm{~V}, \mathrm{I}_{\text {out }}=-175 \mathrm{~mA}$ | -1.35 V Max . |
|  |  |  |  | $\mathrm{V}_{\mathrm{N}}=10 \mathrm{~V}, \mathrm{I}_{\text {OUI }}=-350 \mathrm{~mA}$ | -1.70 V Max. |
|  |  |  | $+85^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathbb{N}}=6.0 \mathrm{~V}, \mathrm{l}_{\text {Out }}=-100 \mathrm{~mA}$ | -1.40 V Max. |
|  |  |  |  | $\mathrm{V}_{\mathbb{W}}=7.0 \mathrm{~V}, \mathrm{I}_{\text {out }}=-175 \mathrm{~mA}$ | -1.55 V Max. |
|  |  |  |  | $\mathrm{V}_{\text {WN }}=10 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | -1.90 V Max. |
|  |  | UDQ-2957R | $-40^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathbb{N}}=2.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}$ | -1.40 V Max. |
|  |  |  |  | $\mathrm{V}_{\text {WW }}=2.7 \mathrm{~V}, \mathrm{I}_{\text {out }}=-175 \mathrm{~mA}$ | -1.55 V Max. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=3.9 \mathrm{~V}, \mathrm{I}_{\text {OUI }}=-350 \mathrm{~mA}$ | -1.90 V Max. |
|  |  |  | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {IN }}=2.4 \mathrm{~V}, \mathrm{I}_{\text {OUI }}=-100 \mathrm{~mA}$ | -1.20 V Max . |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=2.7 \mathrm{~V}, \mathrm{I}_{\text {oui }}=-175 \mathrm{~mA}$ | -1.35 V Max. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=3.9 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | -1.70 V Max. |
|  |  |  | $+85^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {IN }}=2.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}$ | -1.40 V Max. |
|  |  |  |  | $\mathrm{V}_{\mathbb{N}}=2.7 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-175 \mathrm{~mA}$ | -1.55 V Max. |
|  |  |  |  | $\mathrm{V}_{\mathrm{W}}=3.9 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-350 \mathrm{~mA}$ | -1.90 V Max. |
| Input Current | $1_{\text {m(OW) }}$ | UDQ-2956R |  | $\mathrm{V}_{\text {IV }}=6.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | 0.8 mA Max . |
|  |  |  |  | $\mathrm{V}_{\text {If }}=15 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | 2.25 mA Max. |
|  |  | UDQ-2957R |  | $\mathrm{V}_{\mathbb{N}}=2.4 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | 1.0 mA Max. |
|  |  |  |  | $\mathrm{V}_{\text {WI }}=3.85 \mathrm{~V}, \mathrm{~V}_{\text {OVI }}=-2.0 \mathrm{~V}$ | 2.0 mA Max. |
|  | $1_{\text {IMOFA }}$ | ALL |  | $\mathrm{I}_{\text {OUF }}=-500 \mu \mathrm{~A}$ | $50 \mu \mathrm{~A}$ Min. |
| Output Source Current | $\mathrm{I}_{\text {Out }}$ | UDQ-2956R | $-40^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathbb{N}}=5.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | - 75 mA Min. |
|  |  |  |  | $\mathrm{V}_{\mathbb{N}}=6.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -125 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {W }}=7.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -175 mA Min. |
|  |  |  |  | $\mathrm{V}_{\mathbb{N}}=8.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -250 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=9.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -300 mA Min. |
|  |  |  | $+85^{\circ} \mathrm{C}$ | $\mathrm{V}_{\mathrm{W}}=5.0 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | - 125 mA Min . |
|  |  |  |  | $\mathrm{V}_{\mathrm{W}}=6.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -200 mA Min. |
|  |  |  |  | $\mathrm{V}_{\mathbb{W}}=7.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -250 mA Min. |
|  |  |  |  | $\mathrm{V}_{\mathbb{W}}=8.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | - 300 mA Min. |
|  |  |  |  | $\mathrm{V}_{\mathbb{W}}=9.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -350 mA Min. |
|  |  | UDQ-2957R | $-40^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {IN }}=2.4 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | - 50 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {IW }}=2.7 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | -125 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=3.0 \mathrm{~V} \mathrm{~V}_{\text {Out }}=-2.0 \mathrm{~V}$ | -200 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {IN }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -250 mA Min. |
|  |  |  |  | $\mathrm{V}_{\mathbb{W}}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=-2.0 \mathrm{~V}$ | -300 mA Min. |
|  |  |  | $+85^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {IV }}=2.4 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=-2.0 \mathrm{~V}$ | -125 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {IT }}=2.7 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -200 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=3.0 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -250 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {W }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {out }}=-2.0 \mathrm{~V}$ | -300 mA Min. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {Out }}=-2.0 \mathrm{~V}$ | -350 mA Min. |
| Clamp Diode Leakage Current | $T_{R}$ | ALL |  | $V_{R}=80 \mathrm{~V}$ | $50 \mu \mathrm{~A}$ Max. |
| Clamp Diode Forward Voltage | $V_{F}$ | ALL |  | $\mathrm{I}_{\mathrm{F}}=350 \mathrm{~mA}$ | 2.0 V Max. |
| Turn-On Delay | $\mathrm{t}_{\text {O }}$ | ALL |  | $0.5 \mathrm{E}_{\text {IN }}$ to $0.5 \mathrm{E}_{\text {out, }} \mathrm{R}_{\mathrm{L}}=400 \Omega \mathrm{C}_{\mathrm{T}}=25 \mathrm{pF}$ | $4.0 \mu \mathrm{~s}$ Max. |
| Turn-Off Delay | $\mathrm{t}_{\text {Off }}$ | ALL |  | $0.5 \mathrm{E}_{\text {IW }}$ to $0.5 \mathrm{E}_{\text {out. }} \mathrm{R}_{\mathrm{L}}=400 \Omega \mathrm{C}_{\mathrm{T}}=25 \mathrm{pF}$ | $10 \mu s$ Max. |



ALLOWABLE PEAK OUTPUT CURRENT AS A FUNCTION OF DUTY CYCLE


INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE at $T_{A}=+25^{\circ} \mathrm{C}$



## SERIES UDS-2980H HERMETICALLY SEALED HIGH-VOLTAGE, HIGH-CURRENT SOURCE DRIVERS

## FEATURES:

- TTL, DTL, PMOS or CMOS Compatible Inputs
- -500 mA Output Source Current Capability
- Transient-Protected Outputs
- High-Reliability Screening to MIL-STD-883, Class B
- Operating Temperature $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$

SERIES UDS-2980H HERMETICALLY SEALED source drivers interface between standard low-power digital logic, and relays, solenoids, stepping motors, LEDs, lamps, etc., in applications requiring separate logic and load grounds, load supply voltages to +80 V , and /or load currents to 500 mA .

Under normal operating conditions these devices will sustain 50 mA continuously on each of the eight outputs, at an ambient temperature of $+85^{\circ} \mathrm{C}$, with a supply of +15 V . All four devices incorporate input current limiting resistors and output suppression diodes.

UDS-2981H and UDS-2983H drivers are intended for use with +5 V logic systems (TTL, Schottky TTL, DTL and 5 V CMOS). UDS-2982H and UDS-2984H drivers are intended for MOS interface (PMOS and CMOS) operating from supply voltages of from +6 to +16 V .

UDS-2981H and UDS-2982H drivers will sustain a maximum output OFF voltage of +50 V ; UDS2983 H and UDS-2984H drivers a maximum output OFF voltage of +80 V .

In all cases the output is switched ON by an active high input level.

Note that the maximum current rating may not be obtained at $-55^{\circ} \mathrm{C}$ because of beta fall-off, or at $+125^{\circ} \mathrm{C}$ because of package power limitations.


Series UDS-2980H drivers are furnished in 18-pin hermetic dual-in-line packages, and are processed to the requirements of MIL-STD-883, Methods 5004 and 5005.

at $T_{A}=+25^{\circ} \mathrm{C}$
Output Voltage Range, $\mathrm{V}_{\mathrm{CE}}$
(UDS-2981H \& UDS-2982H) . . . . . . . . . . . . . +5 to +50 V
(UDS-2983H \& UDS-2984H) . ............. +35 to +80 V
Input Voltage, $\mathrm{V}_{\text {W }}$ (UDS-2981H \& UDS-2983H) $\ldots . . .$.
(UDS-2982H \& UDS-2984H) $\ldots . . .$. . +30 V
Output Current, I Iour ........................ 500 mA
(total package) ............... 1.67W*
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots .-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
*Derate at $13.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$.


ELECTRICAL CHARACTERISTICS from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ (unless otherwise specified)

| Characteristic | Symbol | Applicable Devices | Temp. | Test Conditions | Fig. | Limit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Output Leakage Current | $\mathrm{l}_{\text {cex }}$ | UDS-2981/82 ${ }^{\text {H }}$ |  | $\mathrm{V}_{\mathrm{W}}=0.25 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{S}}=50 \mathrm{~V}$ | 1 | $200 \mu \mathrm{~A}$ Max. |
|  |  | UDS-2983/84H |  | $\mathrm{V}_{\mathrm{W}}=0.25 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{S}}=80 \mathrm{~V}$ | 1 | $200 \mu \mathrm{~A}$ Max. |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CEESAT }}$ | UDS-2981/83H | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {WV }}=2.4 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}$ | 2 | 2.0 V Max. |
|  |  |  |  | $V_{\text {W }}=2.4 \mathrm{~V}, \mathrm{~T}_{\text {OUT }}=-200 \mathrm{~mA}$ | 2 | 2.IV Max. |
|  |  |  | $\frac{+25^{\circ} \mathrm{C}}{+125^{\circ} \mathrm{C}}$ | $\mathrm{V}_{\text {IV }}=2.4 \mathrm{~V}, \mathrm{l}_{\text {OuT }}=-350 \mathrm{~mA}$ | 2 | 2.0 V Max. |
|  |  |  |  | $V_{\text {iV }}=2.4 \mathrm{~V}, \mathrm{~T}_{\text {OUT }}=-100 \mathrm{~mA}$ | 2 | 1.8 V Max. |
|  |  |  |  | $\mathrm{V}_{\text {IV }}=2.4 \mathrm{~V}$, $\mathrm{I}_{\text {or }}=-200 \mathrm{~mA} * *$ | 2 | 1.9 V Max. |
|  |  | UDS-2982/84H | $-55^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {IV }}=5.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}$ | 2 | 2.00V Max. |
|  |  |  |  | $V_{\text {IW }}=5.0 \mathrm{~V}, \mathrm{I}_{\text {OIT }}=-200 \mathrm{~mA}$ | 2 | 2.1 V Max. |
|  |  |  | $\frac{+25^{\circ} \mathrm{C}}{+125^{\circ} \mathrm{C}}$ | $\mathrm{V}_{\text {IV }}=5.0 \mathrm{~V}, \mathrm{l}_{\text {OUT }}=-350 \mathrm{~mA}$ | 2 | 2.0 V Max. |
|  |  |  |  | $\mathrm{V}_{\text {WI }}=5.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-100 \mathrm{~mA}$ | 2 | 1.8 V Max. |
|  |  |  |  | $\mathrm{V}_{\text {WIV }}=5.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=-200 \mathrm{~mA} *$ | 2 | 1.9 V Max. |
| Input Current | $1_{\text {maon }}$ | UDS-2981/83H |  | $V_{\text {W }}=2.4 \mathrm{~V}$ |  | $575 \mu \mathrm{~A}$ Max. |
|  |  |  |  | $V_{\text {VIV }}=3.85 \mathrm{~V}$ | 3 | 1.26 mA Max. |
|  |  | UDS-2982/84H |  | $V_{1 / 2}=5.0 \mathrm{~V}$ | 3 | $640 \mu$ A Max. |
|  |  |  |  | $\mathrm{V}_{\mathrm{m}}=12 \mathrm{~V}$ | , | 1.8 mA Max. |
|  | ${ }_{1 \text { moff }}$ | UDS-2981/82 |  | $\mathrm{V}_{\mathrm{W}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}=50 \mathrm{~V}$ | 3 | $10 \mu \mathrm{~A}$ Max. |
|  |  | UDS-2983/84H |  | $\mathrm{V}_{\text {IW }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{S}}=80 \mathrm{~V}$ | 3 | $10 \mu \mathrm{~A}$ Max. |
| Output Source Current | $\mathrm{I}_{\text {OU }}$ | UDS-2981/83H |  | $\mathrm{V}_{\mathrm{W}}=2.4 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=2.2 \mathrm{~V}$ | 2 | -200 mA Min. |
|  |  | UDS-2982/84H |  | $\mathrm{V}_{\mathrm{W}}=5.0 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=2.2 \mathrm{~V}$ | 2 | -200 mA Min. |
| Supply Current (Outputs Open) | $\mathrm{I}_{\mathrm{s}}$ | UDS-2981H | $+25^{\circ} \mathrm{C}$ | $\mathrm{V}_{\text {IV }}=2.4 \hat{\mathrm{~V}}^{*}, \mathrm{~V}_{\mathrm{S}}=50 \mathrm{~V}$ | 4 | 10 mA Max. |
|  |  | UDS-2982 |  | $\mathrm{V}_{\text {IV }}=5.0 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{S}}=50 \mathrm{~V}$ | 4 | 10 mA Max. |
|  |  | UDS-2983H |  | $\mathrm{V}_{\text {IV }}=2.4 \mathrm{~V}^{*}, \mathrm{~V}_{\text {S }}=80 \mathrm{~V}$ | 4 | 10 mA Max. |
|  |  | UDS-2984H |  | $\mathrm{V}_{\text {IV }}=5.0 \mathrm{~V}^{*}, \mathrm{~V}_{\mathrm{S}}=80 \mathrm{~V}$ | 4 | 10 mA Max. |
| Clamp Diode Leakage Current | $I_{\text {R }}$ | UDS-2981/82 |  | $\mathrm{V}_{\text {S }}=50 \mathrm{~V}$ (All Inputs $\mathrm{V}_{\text {IV }}=0.25 \mathrm{~V}$ ) | 5 | $50 \mu \mathrm{~A} \mathrm{Max}$. |
|  |  | UDS-2983/84H |  | $\mathrm{V}_{\mathrm{s}}=80 \mathrm{~V}\left(\right.$ All Inputs $\left.\mathrm{V}_{\mathrm{W}}=0.25 \mathrm{~V}\right)$ | 5 | $50 \mu \mathrm{~A}$ Max. |
| Clamp Diode Forward Voltage | $\mathrm{V}_{\mathrm{F}}$ | ALL |  | $\mathrm{I}_{\mathrm{f}}=200 \mathrm{~mA}$ | 6 | 1.75 V Max. |

[^33]
## TEST FIGURES



Figure 1


Figure 3


Figure 2


DWG. NO. A-11,086
Figure 4


Figure 6

## allowable peak collector current AS A FUNCTION OF DUTY CYCLE

UDS-2981/82H


ALL DEVICES


UDS-2983/84H


UDS-2981/82H


ALL DEVICES


DWG. NO. A-11,080

UDS-2983/84H


INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE FOR TYPE UDS-2981/83H


OWG. NO. A-11,074

INPUT CURRENT AS A FUNCTION OF INPUT VOLTAGE FOR TYPE UDS-2982/84H


DISSIPATION AS A FUNCTION OF AMBIENT TEMPERATURE


## SERIES UDS-3600H DUAL 2-INPUT PERIPHERAL and POWER DRIVERS Hermetically Sealed

## FEATURES

- Four Logic Types
- DTL/TL/PMOS/CMOS Compatible Inputs
- Low Input Current
- Sustaining Voltage of 80 V
- Hermetically Sealed Package
- High-Reliability Screening to MIL-STD-883, Class B


## Description

These 'mini-DIP'" dual 2-input peripheral and power drivers are bi-polar monolithic integrated circuits incorporating AND, NAND, OR, or NOR logic gates, and high-current switching transistors on the same chip. The two output transistors are capable of simultaneously sinking 250 mA continuously at an ambient temperature of $+75^{\circ} \mathrm{C}$. In the OFF state, these drivers will sustain at least 80 V .

## Applications

The Series UDS-3600H dual drivers are ideally suited for interface between low-level or high-level logic and high-current/high-voltage loads. Typical applications include driving peripheral loads such as incandescent lamps, light-emitting diodes, memories, and heaters.

With appropriate external diode transient suppression, the Series UDS-3600H drivers can also be used with inductive loads such as relays, solenoids, and stepping motors.


UDS-3613H

## ABSOLUTE MAXIMUM RATINGS

$\qquad$
Supply Voltage, $\mathrm{V}_{\text {cc }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 7.0 V
Input Voltage, $V_{\text {in }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 30 V
Output Off-State Voltage, $\mathrm{V}_{\text {off }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 80 V
Output On-State Sink Current, $\mathrm{I}_{\text {on }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 600 mA
Power Dissipation, $P_{D}$ (one output) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1.0 W (total package) . . . . . . . . . . . . . . . . . . . . . . . . . . . . See Graph
Ambient Temperature Range (operating), $\mathrm{T}_{\mathrm{A}} \ldots \ldots . . . . . . . . . .{ }^{\circ} .5^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$



UDS-3611H


UDS-3612H


UDS-3614H

## PACKAGE POWER DISSIPATION

 AS A FUNCTION OF TEMPERATURE

## RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :--- | :--- | :--- | :--- | :---: |
| Supply Voltage $\left(V_{c c}\right)$ | 4.5 | 5.0 | 5.5 | V |
| Operating Temperature Range | -55 | +25 | +125 | ${ }^{\circ} \mathrm{C}$ |
| Current into any output (ON state) | - | - | 300 | mA |

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {cc }}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Input Voltage | $V_{\text {in(1) }}$ |  | MIN |  |  |  | 2.0 |  |  | V |  |
| "0" Input Voltage | $V_{\text {in(0) }}$ |  | MIN |  |  |  |  |  | 0.7 | V |  |
| "0" Input Current | $\mathrm{I}_{\text {in(0) }}$ |  | MAX | 0.4 V | 30 V |  |  | 50 | 100 | $\mu \mathrm{A}$ | 2 |
| "1" Input Current | $\mathrm{I}_{\text {in(1) }}$ |  | MAX | 30 V | 0 V |  |  |  | 10 | $\mu \mathrm{A}$ | 2 |
| Input Clamp Voltage | $V_{1}$ |  | MIN | -12 mA |  |  |  |  | -1.5 | V |  |

## SWITCHING CHARACTERISTICS at $V_{\text {cC }}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |  |
| Turn-on Delay Time | $\mathrm{t}_{\mathrm{pd} 0}$ | $\begin{aligned} & V_{S}=70 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=465 \Omega \text { (10 Watts) } \\ & C_{\mathrm{L}}=15 \mathrm{pF} \end{aligned}$ | - | 200 | 500 | ns | 3 |
| Turn-off Delay Time | $\mathrm{t}_{\mathrm{pd} 1}$ | $\begin{aligned} & V_{S}=70 V_{,} R_{L}=465 \Omega \text { (10 Watts) } \\ & C_{L}=15 \mathrm{pF} \end{aligned}$ | - | 300 | 750 | ns | 3 |

NOTES:

1. Typical values are at $V_{C C}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each input tested separately.
3. Voltage values shown in the test circuit waveforms are with respect to network ground terminal.
4. Capacitance values specified include probe and test fixture capacitance.

| INPUT PULSE CHARACTERISTICS |  |  |
| :--- | :---: | ---: |
| $V_{\text {in }(0)}=0 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{f}}=7 \mathrm{~ns}$ | $\mathrm{t}_{\mathrm{p}}=1 \mu \mathrm{~s}$ |
| $V_{\mathrm{in}(1)}=3.5 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{r}}=14 \mathrm{~ns}$ | PRR $=500 \mathrm{kHz}$ |

## Type UDS-3611H Dual AND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {CC }}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | $\mathrm{I}_{\text {off }}$ |  | MIN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 0 " Output Voltage | $V_{\text {on }}$ |  | MIN | 0.8 V | $V_{\text {cc }}$ | 150 mA |  | 0.4 | 0.5 | V |  |
|  |  |  | MIN | 0.8 V | $V_{C C}$ | 300 mA |  | 0.6 | 0.8 | V |  |
| "1" Level Supply Current | $\mathrm{I}_{\mathrm{CC}(1)}$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 8.0 | 12 | mA | 1,2 |
| "0" Level Supply Current | $I_{\text {cc(0) }}$ | NOM | MAX | OV | OV |  |  | 35 | 49 | mA | 1,2 |



## Type UDS-3612H Dual NAND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{c c}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | $\mathrm{I}_{\text {off }}$ |  | MIN | 0.8 V | $\mathrm{V}_{\text {c }}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$. |  |
|  |  |  | OPEN | 0.8 V | $V_{c c}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | $V_{\text {on }}$ |  | MIN | 2.0 V | -2.0 V | 150 mA |  | 0.4 | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | 2.0 V | 300 mA |  | 0.6 | 0.8 | V |  |
| "1" Level Supply Current | $\mathrm{I}_{\mathrm{CC}(1)}$ | NOM | MAX | 0 V | 0 V |  |  | 12 | 15 | mA | 1,2 |
| "0" Level Supply Current | $\mathrm{I}_{\text {ç(0) }}$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 40 | 53 | mA | 1,2 |



NOTES
2. Per package.

## Type UDS-3613H Dual OR Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{c c}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | $\mathrm{I}_{\text {off }}$ |  | MIN | 2.0 V | OV | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | OV | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | $\mathrm{V}_{\text {on }}$ |  | MIN | 0.8 V | 0.8 V | 150 mA |  | 0.4 | 0.5 | V |  |
|  |  |  | MIN | 0.8 V | 0.8 V | 300 mA |  | 0.6 | 0.8 | V |  |
| "1" Level Supply Current | $\mathrm{I}_{\text {c(1) }}$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 8.0 | 13 | mA | 1,2 |
| "0" Level Supply Current | $\mathrm{I}_{\text {c(0) }}$ | NOM | MAX | 0 V | OV |  |  | 36 | 50 | mA | 1,2 |



## Type UDS-3614H Dual NOR Driver

## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)



NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Capacitance values specified include probe and test fixture capacitance.

## UCS-4401H and UCS-4801H BiMOS LATCHED DRIVERS - Hermetically Sealed

## FEATURES

- High-Voltage, High-Current Outputs
- Output Transient Protection
- CMOS, PMOS, NMOS, TTL Compatible
- Internal Pull-Down Resistors
- Low-Power CMOS Latches

HIGH-VOLTAGE, HIGH-CURRENT interface for military, aerospace and related applications is supplied by these latched drivers. Type UCS4401 H contains four pairs of latches and drivers; Type UCS-4801H has eight pairs of latches and drivers.

The integrated circuits' CMOS inputs work with standard CMOS, PMOS and NMOS logic levels and (with appropriate pull-up resistors) with TTL or DTL circuits. The bipolar open-collector outputs can be used with relays, solenoids, motors, LED or incandescent displays, and other high-power loads.

The output transistors can sink 500 mA and will withstand a $\mathrm{V}_{\mathrm{CE}}$ of 50 V in the OFF state. Outputs can be paralleled for higher current capability. Because of limitations on package power dissipation, simultaneous operation of all drivers at maximum rated current can only be accomplished with a reduction of duty cycle.

Type UCS- 4401 H , the four-latch device, is furnished in a standard 14-pin side-brazed hermetic package. Type UCS-4801H, the eight-latch device, is furnished in a 22 -pin side-brazed hermetic package with row centers 0.400 -inch ( 10.16 mm ) apart.

Both devices meet all processing and environmental requirements of Military Standard MIL-STD883, Methods 5004 and 5005.


DWG.NO. A-10, 499A
UCS-4401H


UCS-4801H

## abSolute maximum ratings

Output Voltage, $\mathrm{V}_{\mathrm{CE}}$ ..... 50 V
Supply Voltage, $\mathrm{V}_{\text {DO }}$ ..... 18 V
Input Voltage Range, $\mathrm{V}_{\mathbb{N}}$ ..... $+0.3 \mathrm{~V}$
Continuous Collector Current, $I_{C}$ ..... 500 mA
Package Power Dissipation, $P_{D}$ ..... See Graph
Operating Ambient Temperature Range, $T_{A}$ ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ ..... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

CAUTION: Sprague CMOS devices have input static protection but are still susceptible to damage when exposed to extremely high static electrical charges.

FUNCTIONAL BLOCK DIAGRAM


## ALLOWABLE AVERAGE PACKAGE POWER DISSIPATION AS A FUNCTION OF TEMPERATURE



ELECTRICAL CHARACTERISTICS at $T_{A}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{l}_{\text {cex }}$ | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}$ | - | - | 50 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CESSAII }}$ | $\mathrm{I}_{\mathrm{C}}=100 \mathrm{~mA}$ | - | 0.9 | 1.1 | V |
|  |  | $\mathrm{I}_{\mathrm{c}}=200 \mathrm{~mA}$ | - | 1.1 | 1.3 | V |
|  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{~V}_{00}=7.0 \mathrm{~V}$ | - | 1.3 | 1.6 | V |
| Input Voltage | $V_{\text {W(0) }}$ |  | - | - | 1.0 | V |
|  | $V_{\text {m(1) }}$ | $V_{00}=15 \mathrm{~V}$ | 13.5 | - | - | V |
|  |  | $V_{\text {DD }}=10 \mathrm{~V}$ | 8.5 | - | - | V |
|  |  | $\mathrm{V}_{\text {Do }}=5.0 \mathrm{~V}$ (See note) | 3.5 | - | - | V |
| Input Resistance | $\mathrm{R}_{\text {w }}$ | $\mathrm{V}_{00}=15 \mathrm{~V}$ | 50 | 200 | - | $k \Omega$ |
|  |  | $\mathrm{V}_{00}=10 \mathrm{~V}$ | 50 | 300 | - | $\mathrm{k} \Omega$ |
|  |  | $\mathrm{V}_{\text {Do }}=5.0 \mathrm{~V}$ | 50 | 600 | - | $\mathrm{k} \Omega$ |
| Supply Current | $\begin{aligned} & I_{\text {opoon }} \\ & \text { (Each stage) } \end{aligned}$ | $\mathrm{V}_{\text {D0 }}=15 \mathrm{~V}$, Outputs Open | - | 1.0 | 2.0 | mA |
|  |  | $\mathrm{V}_{00}=10 \mathrm{~V}$, Outputs Open | - | 0.9 | 1.7 | mA |
|  |  | $\mathrm{V}_{00}=5.0 \mathrm{~V}$, Outputs Open | - | 0.7 | 1.0 | mA |
|  | $\mathrm{l}_{\text {Oo(of) }}$ | All Drivers OFF, $\mathrm{V}_{\mathbb{W}}=0 \mathrm{~V}$ | - | 50 | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Leakage Current | $\mathrm{I}_{\mathrm{R}}$ | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | - | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{\text {F }}$ | $\mathrm{T}_{\mathrm{F}}=350 \mathrm{~mA}$ | - | 1.7 | 2.0 | V |

Note: Operation of these devices with standard TTL or DTL may require the use of appropriate pull-up resistors to insure the minimum logic " $\mid$ ".

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=-55^{\circ} \mathrm{C}, \mathrm{V}_{00}=5 \mathrm{~V}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | ICXX | $\mathrm{V}_{\mathrm{ct}}=50 \mathrm{~V}$ | - | - | 50 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {ceisat }}$ | $\mathrm{I}_{\mathrm{c}}=100 \mathrm{~mA}$ | - | - | 1.3 | V |
|  |  | $\mathrm{I}_{\mathrm{c}}=200 \mathrm{~mA}$ | - | - | 1.5 | V |
|  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{~V}_{\text {D }}=7.0 \mathrm{~V}$ | - | - | 1.8 | V |
| Input Voltage | $V_{\text {IN(0) }}$ |  | - | - | 1.0 | V |
|  | $V_{\text {INII }}$ | $\mathrm{V}_{00}=15 \mathrm{~V}$ | 14 | - | - | V |
|  |  | $\mathrm{V}_{00}=10 \mathrm{~V}$ | 9.0 | - | - | V |
|  |  | $\mathrm{V}_{\text {D0 }}=5.0 \mathrm{~V}$ (See note) | 3.6 | - | - | V |
| Input Resistance | $\mathrm{R}_{\text {W }}$ | $V_{\text {DO }}=15 \mathrm{~V}$ | 35 | - | - | $\mathrm{k} \Omega$ |
|  |  | $\mathrm{V}_{\text {DO }}=10 \mathrm{~V}$ | 35 | - | - | k $\Omega$ |
|  |  | $\mathrm{V}_{00}=5.0 \mathrm{~V}$ | 35 | - | - | k $\Omega$ |
| Supply Current |  | $\mathrm{V}_{00}=15 \mathrm{~V}$, Outputs Open | - | 1.0 | 2.0 | mA |
|  |  | $\mathrm{V}_{\text {DO }}=10 \mathrm{~V}$, Outputs Open | - | 0.9 | 1.7 | mA |
|  |  | $\mathrm{V}_{\text {DD }}=5.0 \mathrm{~V}$, Outputs Open | - | 0.7 | 1.0 | mA |
|  | $I_{\text {000FF }}$ | All Drivers OFF, $\mathrm{V}_{\mathrm{iN}}=0 \mathrm{~V}$ | - | 50 | 100 | $\mu \mathrm{A}$ |
| Clamp Diode Leakage Current | $I_{R}$ | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | - | - | 50 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | $\mathrm{I}_{\mathrm{f}}=350 \mathrm{~mA}$ | - | - | 2.1 | V |

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+125^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Output Leakage Current | $\mathrm{I}_{\text {cex }}$ | $\mathrm{V}_{\text {CE }}=50 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {cef(Sar }}$ | $\mathrm{I}_{\mathrm{c}}=100 \mathrm{~mA}^{*}$ | - | - | 1.3 | V |
|  |  | $\mathrm{I}_{\mathrm{c}}=200 \mathrm{~mA}^{*}$ | - | - | 1.5 | V |
|  |  | $\mathrm{I}_{\mathrm{C}}=350 \mathrm{~mA}, \mathrm{~V}_{D D}=7.0 \mathrm{~V}^{*}$ | - | - | 1.8 | V |
| Tnput Voltage | $\mathrm{V}_{\text {(NWO) }}$ |  | - | - | 1.0 | V |
|  | $V_{\text {W(1) }}$ | $V_{\text {DD }}=15 \mathrm{~V}$ | 13.5 | - | - | V |
|  |  | $\mathrm{V}_{\text {DD }}=10 \mathrm{~V}$ | 8.5 | - | - | V |
|  |  | $\mathrm{V}_{\text {00 }}=5.0 \mathrm{~V}$ (See note) | 3.5 | - | - | V |
| Input Resistance | $\mathrm{R}_{\text {IN }}$ | $V_{\text {DO }}=15 \mathrm{~V}$ | 50 | - | - | k $\Omega$ |
|  |  | $\mathrm{V}_{\text {D0 }}=10 \mathrm{~V}$ | 50 | - | - | $k \Omega$ |
|  |  | $\mathrm{V}_{\text {OD }}=5.0 \mathrm{~V}$ | 50 | - | - | $\mathrm{k} \Omega$ |
| Supply Current | $\begin{aligned} & T_{\text {opoon }} \\ & \text { (Each stage) } \end{aligned}$ | $\mathrm{V}_{\text {DO }}=15 \mathrm{~V}$, Outputs Open | $\cdots$ | 1.0 | 2.2 | mA |
|  |  | $\mathrm{V}_{\text {DO }}=10 \mathrm{~V}$, Outputs Open | - | 0.9 | 1.9 | mA |
|  |  | $\mathrm{V}_{\text {DD }}=5.0 \mathrm{~V}$, Outputs Open | - | 0.7 | 1.2 | mA |
|  | $\mathrm{l}_{\text {Dopoff }}$ | All Drivers OFF, $\mathrm{V}_{\text {IN }}=0 \mathrm{~V}$ | - | 50 | 150 | $\mu \mathrm{A}$ |
| Clamp Diode Leakage Current | $I_{\text {R }}$ | $\mathrm{V}_{\mathrm{R}}=50 \mathrm{~V}$ | - | - | 500 | $\mu \mathrm{A}$ |
| Clamp Diode Forward Voltage | $V_{F}$ | $\mathrm{I}_{\mathrm{f}}=350 \mathrm{~mA}{ }^{*}$ | - | - | 2.0 | V |

[^34]
## TIMING CONDITIONS

$T_{A}=+25^{\circ} \mathrm{C}$; Logic Levels are $\mathrm{V}_{D 0}$ and $V_{S S}$

A. Minimum data active time before strobe enabled (data set-up time) ............... 100 ns
B. Minimum data active time after strobe disabled (data hold time) .................. 100 ns
C. Minimum strobe pulse width . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 300 ns
D. Typical time between strobe activation and output on to off transition ............ 500 ns
E. Typical time between strobe activation and output off to on transition ........... 500 ns
F. Minimum clear pulse width . . ....................................................... . . . . 300 ns
G. Minimum data pulse width ................. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 500 ns

Information present at an input is transferred to its latch when the STROBE is high. A high CLEAR input will set all latches to the output OFF condition regardless of the data or STROBE input levels. A high OUTPUT ENABLE will set all outputs to the OFF condition regardless of any other input conditions. When the OUTPUT ENABLE is low, the outputs depend on the state of their respective latches.

TRUTH TABLE

| $\mathrm{IN}_{\mathrm{N}}$ | STROBE | CLEAR | OUTPUT <br> ENABLE | $\mathrm{OUT}_{\mathrm{N}}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | t-1 | t |
| 0 | 1 | 0 | 0 | X | OFF |
| 1 | 1 | 0 | 0 | X | ON |
| X | X | 1 | X | X | OFF |
| X | X | X | 1 | X | OFF |
| X | 0 | 0 | 0 | ON | ON |
| X | 0 | 0 | 0 | OFF | OFF |

$\mathrm{X}=$ irrelevant
$t-1=$ previous output state
$t=$ present output state

# SERIES UDS-5700H QUAD 2-INPUT PERIPHERAL and POWER DRIVERS - Hermetically Sealed 

## features

- Four Logic Types
- DTL/TTL/PMOS/CMOS Compatible Inputs
- Low Input Current
- Sustaining Voltage of 80 V
- Hermetically Sealed Package to MIL-M-38510
- High-Reliability Screening to MIL-STD-883, Class B


## Description

These 16 -Lead quad 2 -input peripheral and power drivers are bi-polar monolithic integrated circuits incorporating AND, NAND, OR, and NOR logic gates, high-current switching transistors, and transient suppression diodes on the same chip. The four output transistors are capable of simultaneously sinking 150 mA continuously at an ambient temperature of $+70^{\circ} \mathrm{C}$. In the OFF state, these drivers will sustain at least 80 V .

## Applications

The Series UDS -5700 H quad drivers are ideally suited for interface between low-level or high-level logic and high-current/high-voltage loads. Typical applications include driving peripheral loads such as incandescent lamps, light-emitting diodes, memories, and heaters.
The integral transient suppression diodes allow their use with inductive loads such as relays, solenoids, or stepping motors without the need for discrete diodes. For non-inductive loads, the diode common bus can be used as a convenient lamp test.
ABSOLUTE MAXIMUM RATINGS
Supply Voltage, VCC. ..... 7.0 V
Input Voltage, Vin. ..... 30 V
Output Off-State Voltage, Voff. ..... 80 V
Output On-State Sink Current, Ion. ..... 600 mA
Suppression Diode Off-State Voltage, $V_{\text {off }}$ ..... 80 V
Suppression Diode On-State Current, Ion ..... 600 mA
Power Dissipation, $P_{D}$. ..... 1.0 W
Package Power Dissipation, $P_{D}$ ..... See Graph
Ambient Temperature Range (operating), $\mathrm{T}_{\mathrm{A}}$. ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Storage Temperature Range, IS. ..... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## POWER DISSIPATION AS A FUNCTION OF TEMPERATURE



## RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :--- | :--- | :--- | :--- | :--- |
| Supply Voltage (VCC) | 4.5 | 5.0 | 5.5 | V |
| Operating Temperature Range | -55 | +25 | +125 | ${ }^{\circ} \mathrm{C}$ |
| Current into any output (ON state) | - | - | 300 | mA |

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{C C}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Input Voltage | $V_{\text {in( }}$ (1) |  | MIN |  |  |  | 2.0 |  |  | V |  |
| "0" Input Voltage | $V_{\text {in(0) }}$ |  | MIN |  |  |  |  |  | 0.7 | V |  |
| "0" Input Current | $\operatorname{lin}(0)$ |  | MAX | 0.4 V | 30 V |  |  | 50 | 100 | $\mu \mathrm{A}$ | 2 |
| "1" Input Current | 1 in(1) |  | MAX | 30 V | 0 V |  |  |  | 10 | $\mu \mathrm{A}$ | 2 |
| Input Clamp Voltage | $\mathrm{V}_{1}$ |  | MIN | -12 mA |  |  |  |  | -1.5 | V |  |

SWITCHING CHARACTERISTICS at $V_{\text {cC }}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

|  | Symbol | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Characteristic |  |  | Min. | Typ. | Max. | Units |  |
| Turn-on Delay Time | $\mathrm{t}_{\mathrm{pdO}}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{S}}=70 \mathrm{~V}_{i} \mathrm{R}_{\mathrm{L}}=465 \Omega \mathrm{~s}(10 \mathrm{Watts}) \\ & \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF} \end{aligned}$ |  | 200 | 500 | ns | 3 |
| Turn-off Delay Time | $t_{p d 1}$ | $\begin{aligned} & V_{S}=70 \mathrm{~V}, R_{\mathrm{L}}=465 \Omega \text { (10 Watts) } \\ & \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF} \end{aligned}$ |  | 300 | 750 | ns | 3 |

1. Typical values are at $\mathrm{V}_{C C}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each input tested separately.
3. Voltage values shown in the test circuit waveforms are with respect to network ground terminal.
4. Capacitance values specified include probe and test fixture capacitance.

INPUT PULSE CHARACTERISTICS

| $V_{\text {in }(0)}=0 V$ | $t_{f}=7 \mathrm{~ns}$ | $t_{p}=1 \mu \mathrm{~S}$ |
| :--- | :--- | :---: |
| $V_{\text {in }(1)}=3.5 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{r}}=14 \mathrm{~ns}$ | $P R R=500 \mathrm{kHz}$ |

## Type UDS-5703H Quad OR Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | Ioff |  | MIN | 2.0 V | 0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | 0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 0.8 V | 0.8 V | 150 mA |  | 0.4 | 0.5 | V |  |
|  |  |  | MIN | 0.8 V | 0.8 V | 300 mA |  | 0.6 | 0.8 | V |  |
| Diode Leakage Current | ILK | NOM | NOM | 0 V | 0 V | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | VCc | Vcc |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | $\mathrm{I}_{\mathrm{CC}}(1)$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 16 | 25 | mA | 1,2 |
| "0" Level Supply Current | ICC(0) | NOM | MAX | OV | 0 V |  |  | 72 | 100 | mA | 1,2 |



NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $\mathrm{V}_{\mathrm{R}}=\mathrm{V}_{\text {off(min) }}$.
4. Diode forward voltage drop measured at $I_{f}=300 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.

## Type UDS-5706H Quad AND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)




NOTES:

1. Typical values are at $V_{C C}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off(min) }}$.
4. Diode forward voltage drop measured at $I_{f}=300 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.

## Type UDS-5707H Quad NAND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | VCc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | loff |  | MIN | 0.8 V | VCC | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  | \% | OPEN | 0.8 V | $V_{\text {cc }}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | 2.0 V | 150 mA |  | 0.4 | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | 2.0 V | 300 mA |  | 0.6 | 0.8 | $V$ |  |
| Diode Leakage Current | ILK | NOM | NOM | VCC | VCC | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | OV | 0 V |  |  | 1.5 | 1.75 | $V$ | 4 |
| "1" Level Supply Current | ICC(1) | NOM | MAX | 0 V | 0 V |  |  | 24 | 30 | mA | 1,2 |
| "0" Level Supply Current | $\operatorname{ICC}(0)$ | NOM | MAX | 5.0 V | 5.0 V |  |  |  | 106 | mA | 1,2 |



NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off(min) }}$.
4. Diode forward voltage drop measured at $I_{f}=300 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.

## Type UDS-5733H Quad NOR Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | - Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | loff |  | MIN | 0.8 V | 0.8 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 0.8 V | 0.8 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | $V$ on |  | MIN | 2.0 V | 0 V | 150 mA |  | 0.4 | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | 0 V | 300 mA |  | 0.6 | 0.8 | V |  |
| Diode Leakage Current | lik | NOM | NOM | $\mathrm{V}_{\text {cc }}$ | VCC | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | $V_{D}$ | NOM | NOM | OV | OV |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | $I_{\text {cc( }} 11$ | NOM | MAX | OV | 0 V |  |  | 24 | 30 | mA | 1,2 |
| "0" Level Supply Current | Icc(0) | NOM | MAX | 5.0 V | 5.0 V |  |  | 80 | 100 | mA | 1,2 |



NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off(min). }}$.
4. Diode forward voltage drop measured at $\mathrm{I}_{\mathrm{f}}=300 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.

# SERIES UDS-5710H DUAL PERIPHERAL and POWER DRIVERS - Hermetically Sealed 

## FEATURES

- Four Logic Types
- DTL/TTL/PMOS/CMOS Compatible Inputs
- Low Input Current
- Sustaining Voltage of 80 V
- Transient-Protected Outputs
- High-Reliability Screening to MIL-STD-883, Class B


## Description

These dual peripheral and power drivers are bipolar monolithic integrated circuits incorporating AND, NAND, OR, or NOR logic gates, highcurrent switching transistors, and transient suppression diodes on the same chip. The two output transistors are capable of simultaneously sinking 200 mA continuously at ambient temperatures of up to $+85^{\circ} \mathrm{C}$. In the OFF state, these drivers will sustain at least 80 V . Units are supplied in 8 -pin hermetically sealed mini-DIP packages.


Type UDS-5711H Dual AND Driver


Type UDS-5712H Dual NAND Driver


Type UDS-5713H
Dual OR Driver

## ABSOLUTE MAXIMUM RATINGS

Supply Vo̊ltage, VCC ..... 7.0 V
Input Voltage, $\mathrm{V}_{\text {in }}$ ..... 30 V
Output Off-State Voltage, $\mathrm{V}_{\text {off }}$ ..... 80 V
Output On-State Sink Current, Ion ..... 500 mA
Suppression Diode Off-State Voltage, $V_{\text {off }}$ ..... 80 V
Suppression Diode On-State Current, Ion ..... 500 mA
Power Dissipation, $P_{D}$ (one output) ..... 1.0 W
(total package) ..... See Graph
Ambient Temperature Range (operating), $\mathrm{T}_{\mathrm{A}}$ ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Storage Temperature Range, IS $_{S}$ $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## Applications

The Series UDS-5710H dual drivers are ideally suited for interface between low-level or high-level logic and high-current/high-voltage loads. Typical applications include driving peripheral loads such as incandescent lamps, light-emitting diodes, memories, and heaters with a load current of up to a 500 mA peak value.

The integral transient suppression diodes allow the use of these drivers with inductive loads such as relays, solenoids, or stepping motors without the need for discrete diodes. When not required for transient suppression, the diode common bus can be used to perform the "lamp test" function.


Type UDS-5714H Dual NOR Driver

## POWER DISSIPATION AS A FUNCTION OF TEMPERATURE



## RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :--- | :--- | :--- | :--- | :---: |
| Supply Voltage $\left(V_{\text {cc }}\right)$ | 4.5 | 5.0 | 5.5 | V |
| Operating Temperature Range | -55 | +25 | +125 | ${ }^{\circ} \mathrm{C}$ |
| Current into any output (ON state) | - | - | 300 | mA |

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | $V_{\text {cc }}$ | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Input Voltage | $V_{\text {in( }}$ ( $)$ |  | MIN |  |  |  | 2.0 |  |  | V |  |
| "0" Input Voltage | $V_{\text {in(0) }}$ |  | MIN |  |  |  |  |  | 0.8 | V |  |
| " 0 " Input Current at all Inputs except Strobe | $\mathrm{I}_{\text {in(0) }}$ |  | MAX | 0.4 V | 30 V |  |  | 50 | 100 | $\mu \mathrm{A}$ | 2 |
| " 0 " Input Current at Strobe | $1{ }_{\text {in }(0)}$ |  | MAX | 0.4 V | 30 V |  |  | 100 | 200 | $\mu \mathrm{A}$ |  |
| " 1 " Input Current at all Inputs except Strobe | $\mathrm{I}_{\text {in(1) }}$ |  | MAX | 30 V | 0 V |  |  |  | 10 | $\mu \mathrm{A}$ | 2 |
| "1" Input Current at Strobe | $\operatorname{lin}(1)$ |  | MAX | 30 V | 0 V |  |  |  | 20 | $\mu \mathrm{A}$ | 2 |
| Input Clamp Voltage | V |  | MIN | -12 mA |  |  |  |  | -1.5 | V |  |

SWITCHING CHARACTERISTICS at $V_{\text {cC }}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |  |
| Turn-on Delay Time | $\mathrm{t}_{\text {pdo }}$ | $\begin{aligned} & V_{S}=70 V_{,} R_{L}=465 \Omega \text { (10 Watts) } \\ & C_{L}=15 \mathrm{pF} \end{aligned}$ |  | 200 | 500 | ns | 3 |
| Turn-off Delay Time | $\mathrm{T}_{\mathrm{pd} 1}$ | $\begin{aligned} & V_{S}=70 \mathrm{~V}, R_{L}=465 \Omega \text { (10 Watts) } \\ & C_{L}=15 \mathrm{pF} \end{aligned}$ |  | 300 | 750 | ns | 3 |

NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Each input tested separately.
3. Voltage values shown in the test circuit waveforms are with respect to network ground terminal.
4. Capacitance values specified include probe and test fixture capacitance.

INPUT PULSE CHARACTERISTICS

| $V_{\text {in(0) }}=0 V$ | $t_{f}=7 \mathrm{~ns}$ | $t_{p}=1 \mu \mathrm{~s}$ |
| :--- | :--- | :---: |
| $V_{\text {in(1) }}=3.5 \mathrm{~V}$ | $\mathrm{t}_{\mathrm{r}}=14 \mathrm{~ns}$ | PRR $=500 \mathrm{kHz}$ |

UDS-5711 H Dual AND Driver
ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | loff |  | MIN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | 2.0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 0.8 V | $V_{\text {cc }}$ | 150 mA |  | 0.4 | 0.5 | V |  |
|  |  |  | MIN | 0.8 V | $V_{\text {cc }}$ | 300 mA |  | 0.6 | 0.8 | V |  |
| Diode Leakage Current | ILK | NOM | NOM | 0 V | 0 V | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | VCC | Vcc |  |  | 1.5 | 1.75 | V | 4 |
| " 1 " Level Supply Current | $I_{C C(1)}$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 8.0 | 12 | mA | 1,2 |
| "0" Level Supply Current | ICC(0) | NOM | MAX | 0 V | 0 V |  |  | 35 | 49 | mA | 1,2 |



NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off(fin) }}$.
4. Diode forward voltage drop measured at $\mathrm{I}_{\mathrm{f}}=300 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.

## UDS-57 12H Dual NAND Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | loff |  | MIN | 0.8 V | $V_{C C}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 0.8 V | $V_{C C}$ | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 0 " Output Voltage | $V$ on |  | MIN | 2.0 V | 2.0 V | 150 mA |  | 0.4 | 0.5 | V |  |
|  |  |  | MIN | 2.0 V | 2.0 V | 300 mA |  | 0.6 | 0.8 | V |  |
| Diode Leakage Current | lik | NOM | NOM | V cc | VCC | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | 0 V | 0 V |  |  | 1.5 | 1.75 | $V$ | 4 |
| "1" Level Supply Current | ICC(1) | NOM | MAX | 0 V | 0 V |  |  | 12 | 15 | mA | 1, 2 |
| "0" Level Supply Current | ICC(0) | NOM | MAX | 5.0 V | 5.0 V |  |  | 40 | 53 | mA | 1,2 |




NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathbf{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off }}$ min).
4. Diode forward voltage drop measured at $I_{f}=300 \mathrm{~mA}$
5. Capacitance values specified include probe and test fixture capacitance.

## UDS-5713H Dual OR Driver

ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | Vcc | Driven Input | Other Input | Output | Min. | Typ. | Max. | Units |  |
| "1" Output Reverse Current | Ioff |  | MIN | 2.0 V | 0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 2.0 V | 0 V | 80 V |  |  | 100 | $\mu \mathrm{A}$ |  |
| " 0 " Output Voltage | Von |  | MIN | 0.8 V | 0.8 V | 150 mA |  | 0.4 | 0.5 | $V$ |  |
|  |  |  | MIN | 0.8 V | 0.8 V | 300 mA |  | 0.6 | 0.8 | V |  |
| Diode Leakage Current | ILK | NOM | NOM | 0 V | 0 V | OPEN |  |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | $V_{C C}$ | Vcc |  |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | $I_{\text {cc(1) }}$ | NOM | MAX | 5.0 V | 5.0 V |  |  | 8.0 | 13 | mA | 1,2 |
| "0" Level Supply Current | ICC(0) | NOM | MAX | 0 V | 0 V |  |  | 36 | 50 | mA | 1,2 |



NOTES:

1. Typical values are at $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{\text {off(min) }}$.
4. Diode forward voltage drop measured at $I_{f}=300 \mathrm{~mA}$.
5. Capacitance values specified include probe and test fixture capacitance.

## UDS-57 14 H Dual NOR Driver

## ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Test Conditions |  |  |  |  | Limits |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Temp. | VCC | Driven Input | Other Input | Output | Min. Typ. | Max. | Units |  |
| "1" Output Reverse Current | Ioff |  | MIN | 0.8 V | 0.8 V | 80 V | , | 100 | $\mu \mathrm{A}$ |  |
|  |  |  | OPEN | 0.8 V | 0.8 V | 80 V |  | 100 | $\mu \mathrm{A}$ |  |
| "0" Output Voltage | Von |  | MIN | 2.0 V | 0 V | 150 mA | 0.4 | 0.5 | $V$ |  |
|  |  |  | MIN | 2.0 V | 0 V | 300 mA | 0.6 | 0.8 | V |  |
| Diode Leakage Current | lik | NOM | NOM | $V_{C C}$ | V cc | OPEN |  | 200 | $\mu \mathrm{A}$ | 3 |
| Diode Forward Voltage Drop | V | NOM | NOM | 0 V | OV |  | 1.5 | 1.75 | V | 4 |
| "1" Level Supply Current | ICC(1) | NOM | MAX | 0 V | 0 V |  | 12 | 15 | mA | 1,2 |
| " 0 " Level Supply Current | ICClO) | NOM | MAX | 5.0 V | 5.0 V |  | 40 | 50 | mA | 1,2 |




NOTES:

1. Typical values are at $V_{C C}=5.0 \mathrm{~V}, T_{\mathbf{A}}=25^{\circ} \mathrm{C}$.
2. Per package.
3. Diode leakage current measured at $V_{R}=V_{o f f(\text { min })}$.
4. Diode forward voltage drop measured at $I_{f}=300 \mathrm{~mA}$
5. Capacitance values specified include probe and test fixture capacitance.

## UDS-5790H and UDS-5791 H QUAD PIN DIODE POWER DRIVERS

## FEATURES

- Inverting or Non-Inverting
- Low Input Current
- TTL, DTL, MOS Compatible
- Wide Operating Voltage Range
- High Output Breakdown Voltage

CONSISTING of four high-voltage NPN output stages and associated logic and level shifting, these monolithic, planar integrated circuits offer an easy solution to many PIN diode driving applications.

The UDS-5790H and UDS-5791H quad power drivers are designed to replace discrete or hybrid PIN diode drivers. They provide significant reductions in cost and space with improved reliability. The UDS5790 H driver uses a grounded-base input stage for non-inverting operation while the UDS-5791H driver uses a common-emitter input stage for inverting operation. Both devices are capable of sustaining OFF voltages of 120 V and will switch currents to 500 mA .

The input buffer circuitry has been designed to utilize external discrete resistors. The one-resistor-per-driver effectively reduces total package power dissipation and junction temperature while allowing user selection of output base drive current, power supply voltages, and output current.

All devices are rated for operation over an extended temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. They are customarily supplied in 16-pin hermetic dual in-line packages. All units are subjected to the $100 \%$ production screen tests specified in MIL-STD-883, Method 5004, Class B, paragraphs 3.1.1 through 3.1.6. On special order, 160 hours of burn-in to Method 1015, Condition A, can also be performed.


## ABSOLUTE MAXIMUM RATINGS <br> over free-air operating temperature range

Supply Voltage, $\mathrm{V}_{\mathrm{cc}}$ ..... $+6.0 \mathrm{~V}$
Supply Voltage, $\mathrm{V}_{\mathrm{EE}}$ ..... $-6.0 \mathrm{~V}$
Input Voltage, $\mathrm{V}_{\mathbb{I N}}$ .....  $\mathrm{V}_{\mathrm{cc}}$
Output OFF-State Voltage, $\mathrm{V}_{\text {OFF }}$ (ref. $\mathrm{V}_{\text {EE }}$ ) ..... $+120 \mathrm{~V}$
Output ON-State Current, Ion. ..... 500 mA
Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ ..... See Graph
Operating Ambient Temperature Range, $\mathrm{T}_{\mathrm{A}}$ ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{s}}$ $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## PARTIAL SCHEMATICS



ONE OF FOUR DRIVERS
UDS-5790H


ONE OF FOUR DRIVERS
UDS-5791H

RECOMMENDED OPERATING CONDITIONS

|  | Min. | Nom. | Max. | Units |
| :---: | :---: | :---: | :---: | :---: |
| Supply Voltage, $\mathrm{V}_{\text {cc }}$ | 4.5 | 5.0 | 5.5 | V |
| Supply Voltage, $\mathrm{V}_{\mathrm{EE}}$ | -1.5 | $-3.0$ | -5.5 | $V$ |
| Output ON-State Current, Ion |  |  | 300 | mA |
| Operating Ambient Temperature Range, $\mathrm{T}_{\mathrm{A}}$ | -55 | +85 | +125 | ${ }^{\circ} \mathrm{C}$ |

## POWER DISSIPATION AS A FUNCTION OF TEMPERATURE



ELECTRICAL CHARACTERISTICS over operating temperature range (unless otherwise noted)

| Characteristic | Symbol | Temp. ${ }^{\circ} \mathrm{C}$ | $\begin{aligned} & V_{c c} \\ & +V \end{aligned}$ | $V_{E E}$ | $\begin{aligned} & V_{\mathbb{N}} \\ & +V \end{aligned}$ | $V_{\text {OFF }}$ or $I_{\text {ON }}$ $+V \quad \mathrm{~mA}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{X}} \\ & \Omega \end{aligned}$ | Limits |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | Min. | Max. | Units |  |
| " 1 " Input Voltage | $V_{\text {IN(1) }}$ |  | 4.5 |  |  |  |  | 2.0 | 4.0 | V |  |
| "0" Input Voltage | $\mathrm{V}_{\text {IN(0) }}$ |  | 4.5 |  |  |  |  | - | 0.8 | V |  |
| "1" Input Current | $\mathrm{I}_{\ln (1)}$ |  | 5.5 | 3.0 | 5.0 |  |  | - | 1.0 | mA | 1 |
|  |  |  | 5.5 | 3.0 | 5.0 |  |  | - | 50 | $\mu \mathrm{A}$ | 2 |
| "0" Input Current | $\mathrm{I}_{\text {IN(0) }}$ |  | 5.5 | 3.0 | 0.4 |  |  | - | 50 | $\mu \mathrm{A}$ | 1 |
|  |  |  | 5.5 | 3.0 | 0.4 |  |  | - | 1.0 | mA | 2 |
| OFF-State Reverse Current | Ioff | +25 | 4.5 | 3.0 |  | 115 |  | - | 50 | $\mu \mathrm{A}$ | 3 |
|  |  | +125 | 4.5 | 3.0 |  | 115 |  | - | 100 | $\mu \mathrm{A}$ | 3 |
| ON -State Output Voltage (ref. $V_{E E}$ ) | $V_{O N}$ | -55 | 4.5 | 1.5 |  | 150 | 720 | - | 400 | mV | 4,5 |
|  |  |  |  |  |  | 300 | 360 | - | 600 | mV | 4,5 |
|  |  | +85 | 4.5 | 1.5 |  | 150 | 720 | - | 400 | mV | 4,5 |
|  |  |  |  |  |  | 300 | 360 | - | 700 | mV | 4,5 |
|  |  | +125 | 4.5 | 1.5 |  | 150 | 720 | - | 500 | mV | 4,5 |
|  |  |  |  |  |  | 300 | 360 | - | 850 | mV | 4,5 |
| Predriver Collector Voltage (ref. $\mathrm{V}_{\text {EE }}$ ) | $\mathrm{V}_{\mathrm{x}}$ |  | 4.5 | 1.5 |  | 150 | 720 | - | 1.3 | V | 4,5 |
|  |  |  |  |  |  | 300 | 360 | - | 1.5 | V | 4,5 |
| Output Short-Circuit Current | los |  | 4.5 | 3.0 |  | -2.3 | 510 | 20 | 50 | mA | 3,5 |
| OFF-State Supply Current | Icc |  | 5.5 | 5.5 |  |  |  | - | 3.4 | mA | 3 |
| ON -State Supply Current | Icc |  | 5.5 | 5.5 | * |  |  | - | 4.1 | mA | 4 |
| Turn-On Delay | $\mathrm{t}_{\text {n }}$ | - | 5.0 | 3.0 | - | - - | 510 | - | 500 | ns |  |
| Storage Delay | $\mathrm{t}_{5}$ | - | 5.0 | 3.0 | - | - - | 510 | - | 5.0 | $\mu \mathrm{S}$ |  |
| Fall Time | $t_{f}$ | - | 5.0 | 3.0 | - | - - | 510 | - | 100 | ns |  | NOTES:

1. Type UDS-5790H only.
2. Type UDS-5791H only.
3. $V_{I N}=2.4 \mathrm{~V}$ for UDS-5790H or 0.4 V for UDS-5791H.
4. $\mathrm{V}_{\mathrm{IN}}=0.4 \mathrm{~V}$ for UDS-5790H or 2.4 V for UDS-5791H.
5. Each output tested separately.

## SWITCHING TEST CIRCUIT <br> AND WAVEFORMS



## GENERAL DESIGN NOTES

$$
\begin{aligned}
& I_{R X}=\frac{I_{O N}}{B} \\
& R_{X}=\frac{B\left(V_{C C}-V_{E E}-V_{X}\right)}{I_{O N}}
\end{aligned}
$$

where
$B=30$, the minimum output current gain over the operating temperature range
$V_{x}=1.5$, the maximum predriver voltage
It is recommended that a minimum overdrive of $25 \%$ to be used $\left(1.25 I_{R X}\right.$ or $\left.0.8{ }_{R X}\right)$.

QUALITY ASSURANCE FLOW CHART



DWG. NO. B. 1474

# THE SPRAGUE ELECTRIC 'DOUBLE-DEUCE' BURN-IN PROGRAM FOR INTEGRATED CIRCUITS 

THE EXPENSE OF DEVICE FAILURE is more than the time and money spent locating and replacing a defective integrated circuit. The total cost can include the price of assembly rework, system downtime, service calls, warranty claims and lost customer goodwill.

Costs of $\$ 25$ for each in-house failure and $\$ 250$ for each field failure are not uncommon. At a relatively low cost, Sprague


#### Abstract

Electric Company's "Double-Deuce" screening program removes marginal devices before shipment. Improved customer satisfaction with performance and reliability is an immeasurable but certain bonus of the program. "Double-Deuce" screening is done during the last stage of production. Because Sprague does the screening, only qualified devices are received by the user.


## QUALITY AND RELIABILITY

Quality and reliability are terms that are often used interchangeably. Quality implies reliability, but a product's merit should always be defined by both.

Quality is the extent to which a device conforms to specifications when it is shipped to the user. Quality is verified by testing. Inspections at every step of production of Sprague integrated circuits ensure the devices meet demanding standards for workmanship and materials.

Inspections of integrated circuits under the "Double-Deuce" program have been made even more stringent to secure a higher level of quality.

Reliability is the measure of an integrated circuit's ability to meet specifications over time. Reliability is a product of design and process control. Acceleratedlife tests provide the manufacturer and user with an indication of the reliability of a device. Normally, a small number of integrated circuits exhibit signs of early failure or infant mortality. This statistic, taken from the steepest part of the IC
lifetime probability curve, is often used to project time-to-failure for integrated circuits. Because the "Double-Deuce" program eliminates early failures, Sprague integrated circuits delivered after the screening process have a higher degree of reliability.

PROBABILITY OF FAILURE
AS A FUNCTION OF TIME


## OUTLINE OF THE 'DOUBLE-DEUCE' PROCESS

The "Double-Deuce" burn-in program uses high stress levels to accelerate the failure mechanisms associated with infant mortality. These normally occur within the first few hours of user application. Although typically less than 1 per cent of a lot will be rejected, user confidence in lot integrity is greatly improved. The screening program is designed to eliminate the following failure modes:

## Stress

High-Temp. Bake
Temp. Cycling
Burn-In
High-Temp. Testing

## Failure Mode

Contamination
Package-Related
Process-Related
Electrical Degradation

The majority of early integrated circuit failures (infant mortality or ionic contamination) can be attributed to manufacturing defects, package or assembly defects, or final test escapes. The "DoubleDeuce" program is designed to eliminate weaker parts, reduce or eliminate user shipment inspection, assembly rework, system checkout, and warranty returns.


DWG.NO. A-11,418A

## TEST PROCEDURES

The "Double-Deuce" burn-in program includes five test procedures:

## 1. High-Temperature Bake

This is a process designed to stabilize electrical drift and to accelerate chemical degradation such as surface contamination. It is a four-hour bake at $+175^{\circ} \mathrm{C}$ without electrical stress (similar to MIL-STD-883, Method 1008).

## 2. Temperature Cycling

This is a screening process designed to mechanically stress the integrated circuit by alternately heating and cooling it.

Potential failures are seal or bond failure, cracked packages or chips.

The process has 10 cycles with 10 minutes of dwell at $-65^{\circ} \mathrm{C}$ and 10 minutes of dwell at $+150^{\circ} \mathrm{C}$ (air to air), with a maximum transfer time of five minutes (MIL-STD-883, Method 1010, Condition C). At Sprague's option, this process may be changed to thermal shock (liquid to liquid) for 10 cycles, five minutes at $0^{\circ} \mathrm{C}$ and five minutes at $+100^{\circ} \mathrm{C}$ with a transfer time of 10 seconds (MIL-STD-883, Method 1011, Condition A).

## TEST PROCEDURES

## 3. Burn-In

The burn-in, or accelerated-life test, is performed to screen out marginal devices, those with inherent defects, or defects resulting from manufacturing deviations that can cause time-dependent or stressdependent failures. Without this conditioning, marginal circuits that initially meet all specifications could exhibit early lifetime failures under normal operating conditions. The test is conducted for 96 hours at a junction temperature of $+150^{\circ} \mathrm{C}$ under electrical stress conditions (similar to MIL-STD-883, Method 1015) such as:

## Type of Device

Bipolar Interface Linear Devices
$1^{2}$ L and MOS Logic

## Electrical Stress

Steady-State Reverse Bias Steady-State Forward Bias Clocked

The burn-in conditions (96 hours at $\mathrm{T}_{\mathrm{J}}$ $=+150^{\circ} \mathrm{C}$ ) are equivalent to 525 hours at
$\mathrm{T}_{\mathrm{J}}=+125^{\circ} \mathrm{C}$ for ionic contamination ( $\mathrm{E}_{\mathrm{A}}$ $=1.0 \mathrm{eV}$ ) or for 192 hours at $\mathrm{T}_{\mathrm{J}}=+125^{\circ} \mathrm{C}$ for infant mortality defects ( $\mathrm{E}_{\mathrm{A}}=0.4 \mathrm{eV}$ ).

## 4. High-Temperature Test

Every device is subjected to complete electrical tests at $+70^{\circ} \mathrm{C}$ for function and d-c parameters (similar to MIL-STD-883, Methods 3001 through 3014 and 4001 through 4007, as applicable). Relaxed $+25^{\circ} \mathrm{C}$ limits or published hightemperature limits, are used to remove devices with circuit anomalies such as beta mismatch, high leakage current, and intermittent bonds, which may only affect the circuit at higher temperatures.

## 5. Outgoing Quality Control Inspection

All "Double-Deuce" product is inspected to an outgoing sampling plan which guarantees that the product will meet an acceptable quality level of $0.25 \%$.

## HOW TO ORDER

All standard Sprague integrated circuits are branded with the Sprague registered trademark, (2).

Integrated circuits screened to the added requirements of the "Double-Deuce" program are marked:

## (2) (2)

The double "circle-deuce" identifies a
part subjected to the screening program for extra reliability.

Devices processed in the "DoubleDeuce" burn-in program are specified by adding the suffix "BU" to the end of the part number. For example, to order ULN2023A with this processing, specify ULN2023ABU; to order UDN-6116R-2, specify UDN-6116R-2BU.

## INTERFACE DRIVERS WITH MIL-STD-883 HIGH-RELIABILITY SCREENING

Interface drivers with high-reliability screening can be ordered by adding the suffix 'MIL'' to the part number, for example, ULS-2064H-MIL. If marking with the customers part number is necessary in place of the Sprague Electric part number, this must be stated on the purchase order with the marking desired.

Table I - $100 \%$ Production Screen Tests (All Hermetic Parts) MIL-STD-883, Method 5004, Class B, Paragraphs 3.1.1 through 3.1.6

|  | MIL-STD-883 <br> Test Method | Conditions |
| :--- | :--- | :--- |
| Screen | 2010. Cond. B | - |
| Internal Visual | 1008, Cond. C | $150^{\circ} \mathrm{C} .24$ Hours |
| Stabilization Bake | 1011. Cond. A | 0 to $100^{\circ} \mathrm{C}, 15$ Cycles |
| Thermal Shock | 2001. Cond. E | $30,000 \mathrm{G}$ 's, Y1 Plane |
| Constant Acceleration | 1014, Cond. A | $5 \times 10^{-7} \mathrm{~atm} \cdot \mathrm{~cm}^{3} / \mathrm{s}$ Maximum |
| Fine Seal | 1014, Cond. C | - |
| Gross Seal | - | Per Specification |
| Electrical | - | Sprague or customer part number, date code, |
| Marking |  | lot identification, index point |
|  |  |  |

Table II $-100 \%$ High-Reliability Screening ("MIL" Suffix Parts Only) MIL-STD-883, Method 5004, Class B, Paragraphs 3.1.9 through 3.1.15 \& 3.1.18

|  | MIL-STD-883 <br> Sest Method | Conditions |
| :--- | :--- | :--- |
| Screen | 5005, Gp A, Subgp. 1 | $25^{\circ} \mathrm{C}$ per Specification |
| Interim Electrical | 1015, Cond. A | $125^{\circ} \mathrm{C}, 160$ Hours |
| Burn-In | 5005, Gp A, Subgp. 1 | $25^{\circ} \mathrm{C}$ per Specification |
| Static Electrical | 5005, Gp A, Subgp. $2 \& 3$ | $-55^{\circ} \mathrm{C} \&+125^{\circ} \mathrm{C}$ per Specification |
|  | 5005, Gp A, Subgp. $4,7 \& 9$ | $25^{\circ} \mathrm{C}$ per Specification |
| Dynamic \& Functional Electrical | 1014, Cond. A | $5 \times 10^{-7} \mathrm{~atm} \mathrm{~cm}^{3} / \mathrm{S}$ Maximum |
| Fine Seal | 1014, Cond. C | - |
| Gross Seal | 2009 | - |
| External Visual |  |  |

Table III - High-Reliability Qualification and Quality Conformance Inspection MIL-STD-883, Method 5004, Class B, Paragraph 3.1.17

|  | MIL-STD-883 <br> Test Method | Description |
| :--- | :--- | :--- |
| Group A Subgp. 1-4, 7\& | 5005, Table I | Each production lot |
| Group B | 5005, Table II | Each production lot |
| Group C | 5005, Table III | End points, Gp. A, Subgp. 1, every 90 days |
| Group D | 5005, Table IV | End points, Gp. A, Subgp. 1. every 6 months |

Some of this material has been taken from Military Specification MIL-M-38510D and Military Standard MIL-STD-883B, Methods 1008.1, 1011.2, 1014.3, 1015.2, 2001.2, 2009.2, 2010.4, 5004.4, and 5005.6.

Unless otherwise specified, the latest issues of these military documents shall apply to the extent specified herein.


GENERAL INFORMATION

HIGH-VOLTAGE INTERFACE DRIVERS

HIGH-CURRENT INTERFACE DRIVERS

BiMOS AND COMPLEX ARRAY INTERFACE DRIVERS

INDUSTRIAL, MILITARY, AND AEROSPACE DEVICES

## RADIO INTEGRATED CIRCUITS

TELEISION INTEGRATED CIRCUITS

AUDIO INTEGRATED CIRCUITS

HALL EFFECT DEVICES

TRANSISTOR ARRAYS AND MISCELLANEOUS DEVICES

CUSTOM DEVICES

## SECTION 6 - RADIO INTEGRATED CIRCUITS

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ULN-2204A Applications and Operation ..... 6-86
A-M/F-M Radio Design Using the ULN-2240/41/42A ..... 6-97
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SELECTION GUIDE TO RADIO INTEGRATED CIRCUITS

| Device Type | R-F Mixer | $\begin{aligned} & \text { F-M } \\ & \text { I-F } \end{aligned}$ | $\begin{aligned} & \text { F-M } \\ & \text { Det. } \end{aligned}$ | Mute/ Squelch | $\Delta f$ Mute | F-M Meter | Stereo Decode | A-M <br> Radio | A-M Meter | Audio Amp. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ULN-2111A | - | X | $\chi$ | - | - | - | - | - | - | - |
| ULN-2136A | - | X | X | - | - | - | - | - | - | - |
| ULN-2204A | - | X | X | - | - | - | - | X | - | X |
| ULN-2240A | - | X | X | X | X | $X$ | - | $X$ | - | - |
| ULN-2241A | - | $X$ | X | - | - | - | - | X | - | - |
| ULN-2242A | - | X | X | X | - | X | - | X | - | - |
| ULN-2243A | X | X | - | - | - | - | $\bar{\chi}$ | - | - | - |
| ULN-2245A | - | - | - | - | - | - | X | - | - | - |
| ULN-2249A | - | - | - | - | - | - | - | X | - | - |
| ULX-3804A | - | X | X | - | - | - | - | X | - | - |
| ULN-3809A | - | - | $\underline{-}$ | - | - | - | $x$ | - | - | - |
| ULN-3810A | - | - | - | - | - | - | $\chi$ | - | - | - |
| ULX-3840A | - | X | X | X | $X$ | X | - | X | X | - |
| ULN-3859A | X | X | X | X | - | - | - | - | - | - |
| ULN-3889A | - | X | X | X | X | - | - | - | - | - |

NOTE: Additional devices for use as F-M radios may be found in Section 7; audio amplifiers may be found in Section 8.

## ULN-2111A F-M I-F AMPLIFIER/LIMITER and QUADRATURE DETECTOR

## FEATURES

- Good Sensitivity
- Excellent A-M Rejection
- Low Harmonic Distortion
- Single-Adjustment Tuning
- High Gain to 50 MHz
- 500 mV Recovered Audio at 10.7 MHz
- Wide Operating Voltage Range
- Direct Replacement for ULN-2113A, MC1357, SN76643
- 14-Pin Dual In-Line Plastic Package

PROVIDING a multi-stage wideband amplifier/ limiter, an F-M quadrature detector, and an emit-ter-follower audio output stage, the Type ULN-2111A is designed for use in F-M receivers or in the sound I-F of TV receivers.

The Type ULN-2111A amplifier/limiter and quadrature detector is a Sprague-originated design. This circuit was the original monolithic integrated circuit F-M detector and was the first integrated circuit to be used in entertainment electronics. Its outstanding feature is that only a single low-cost tuned circuit is required instead of the previous triple-winding transformer.


ABSOLUTE MAXIMUM RATINGS
Supply Voltage, $\mathrm{V}_{\mathrm{cc}}$ 15 V
Package Power Dissipation, $P_{D}$.................. 670 mW *
Operating Temperature Range, $T_{A} \ldots \ldots .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{S} \ldots \ldots .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $8.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.


STATIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+12 \mathrm{~V}$

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Supply Current | $l_{\text {cc }}$ | 13 |  | 12 | 17 | 27 | mA |
| Terminal Voltage | $V_{1}$ $V_{2}$ $V_{6}$ $V_{9}$ $V_{10}$ | $\begin{array}{r} 1 \\ 2 \\ 6 \\ 9 \\ 10 \end{array}$ |  | 4.3 - | $\begin{aligned} & 5.0 \\ & 3.65 \\ & 1.45 \\ & 150 \\ & 1.45 \end{aligned}$ | 6.3 $=$ $=$ | $\begin{aligned} & V \\ & V \\ & V \\ & \mathrm{mV} \\ & V \end{aligned}$ |
| Resistance, Detector Output <br>  I-F Input <br>  I-F Output <br>  Detector Input <br>  De-Emphasis | $\begin{aligned} & R_{1} \\ & R_{1} \\ & R_{1} \\ & R_{12} \\ & R_{14} \end{aligned}$ | $\begin{array}{r} 1 \\ 4 \\ 10 \\ 12 \\ 14 \end{array}$ |  | $\overline{-}$ | $\begin{gathered} 200 \\ 5.0 \\ 60 \\ 70 \\ 9.0 \end{gathered}$ | E | $\begin{aligned} & \hline \Omega \\ & \mathrm{k} \Omega \\ & \Omega \\ & \mathrm{k} \Omega \\ & \mathrm{k} \Omega \end{aligned}$ |
| Capacitance, I-F Input | $\begin{aligned} & C_{4} \\ & C_{12} \end{aligned}$ | $\begin{gathered} 4 \\ 12 \end{gathered}$ |  | - | $2.7$ | $\overline{-}$ | pF |

DYNAMIC ELECTRICAL CHARACTERISTICS at $T_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+12 \mathrm{~V}, \mathrm{f}_{\mathrm{o}}=10.7 \mathrm{MHz}$, $f_{m}=400 \mathrm{~Hz}, \Delta \mathrm{f}= \pm 75 \mathrm{kHz}$, Peak Separation $=550 \mathrm{kHz}$

| Characteristic | Symbol | $\begin{aligned} & \text { Test } \\ & \text { Pin } \end{aligned}$ | Test Figure | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |  |
| Amplifier Voltage Gain | $\mathrm{A}_{0}$ | 10 | 1 | $\mathrm{V}_{\text {in }} \leq 300 \mu \mathrm{~V}_{\mathrm{rms}}$ | - | 53 | - | dB |  |
| Amplifier Output Voltage | $\mathrm{V}_{\text {out }}$ | 10 | 1 | $\mathrm{V}_{\text {in }}=10 \mathrm{mV} \mathrm{rms}$ | - | 1.45 | - | $\mathrm{V}_{\mathrm{pp}}$ |  |
| Input Limiting Threshold | $V_{T H}$ | 4 | 2 |  | - | 400 | 800 | $\mu \mathrm{V}_{\text {rms }}$ | 1,3 |
| Recovered Audio Output | $V_{\text {out }}$ | 1 | 2 | $\mathrm{V}_{12}=60 \mathrm{mV} \mathrm{rms}$ | - | 500 | - | $\mathrm{mV}_{\mathrm{rms}}$ | 3 |
| Output Distortion | THD | 1 | 2 | 100\% F-M Modulation | - | 1.0 | - | \% | 3 |
| A-M Rejection | AMR | 1 | 3 | $\mathrm{V}_{\text {in }}=10 \mathrm{mV} \mathrm{rms}$ | - | 40 | - | dB | 2 |

NOTES:

1. The input limiting threshold is the F-M input voltage for a recovered audio output which is 3 dB less than the recovered audio output for an F-M input voltage of $200 \mathrm{mV}_{\mathrm{rms}}$.
2. The amplitude modulation rejection is determined by: $\quad A M R_{d B}=20 \log \frac{V_{\text {out }} \text { for } 100 \% F-M V_{\text {in }}}{V_{\text {out }} \text { for } 30 \% A-M V_{\text {in }}}$
3. See also, General Design Note No. 9.

COMPONENT CHART

|  | Component Value |  |
| :--- | :---: | :---: |
|  | TV $(4.5 \mathrm{MHz})$ | $\mathrm{F}-\mathrm{M}(10.7 \mathrm{MHz})$ |
| L - Inductance | $7.0-14 \mu \mathrm{H}$ | $1.5-3.0 \mu \mathrm{H}$ |
| Unloaded Q |  |  |
| D-C Resistance |  |  |
| Type | 50 | 50 |
| $\mathrm{C}_{1}$ - Capacitance | $<50 \Omega$ | $<50 \Omega$ |
| TCC | Mill \#9052 | Miller \#9050 |
| $\mathrm{C}_{2}$ - Capacitance | 120 pF | 120 pF |
| R - Resistance | 3.0 pF | NPO |
| Loaded Network Q | $20 \mathrm{k} \Omega$ | 4.7 pF |



TEST FIGURE 1


TEST FIGURE 2


TEST FIGURE 3

## F-M I-F AMPLIFIER/LIMITER and QUADRATURE DETECTOR

## TYPICAL APPLICATION



GENERAL DESIGN NOTES

1. Phase shift network is aligned by applying F-M signal through decoupling network to pin $4\left(V_{4}=5 \mathrm{mV}_{\text {rms }}\right)$. Tune for maximum recovered audio at pin 1 or maximum I-F voltage at pin 11.
2. A d-c path of less than $100 \Omega$ must be provided between pins 2 and 12. No other biasing provisions are required.
3. A d-c path of less than $300 \Omega$ must be provided between pins 4 and 6 . No other biasing provisions are required.
4. The maximum a-c load current can be increased by adding an external resistor between pin 1 and ground. The minimum value for this resistor is $800 \Omega$, giving a maximum load current of $4 \mathrm{~mA}_{\text {rms }}$.
5. All decoupling capacitors should be of the ceramic type with minimum inductance at the operating frequency.
6. Decoupling capacitor leads at pins 2,5 , and 6 should be as short as possible.
7. Keep appropriate distance between the input (pin 4 and the input network) and the phase shift network (pins 9,10 , and 12 , and the phase shift inductor).
8. If a high impedance power supply is used (voltage dropping resistor), decouple pin 13 for the lowest audio frequency.
9. The linear detection mode (low signal level at pin 12), as shown, is preferred for communications and other commercial applications, due to the preservation of the tuned circuit bandwidth and better rejection of Gaussian noise. The combination of coupling capacitor $\left(C_{2}\right)$ and I-F amplifier output (pin 9) was chosen for optimum quieting. The bandwidth of the phase shift network (peak separation) is primarily defined by the Damping resistor ( R ). A higher value resistor will decrease bandwidth, increase the recovered audio output, reduce the capture ratio, and increase harmonic distortion.
10. The switching detection mode (high signal level at pin 12) features a greater linear range, increased insensitivity to amplitude variations, and is recommended for AFC applications or where side responses must be avoided. Limiting in the quadrature detector will produce slightly more audio output, but will increase the noise bandwidth and degrade quieting.

## I-F AMPLIFIER GAIN AS A FUNCTION OF FREQUENCY


SCHEMATIC

## ULN-2 136A F-M I-F AMPLIFIER/LIMITER and QUADRATURE DETECTOR

## FEATURES

- Single Tuning Coil Design
- Good Line and Load Regulation
- Low Harmonic Distortion
- Good Sensitivity
- Excellent A-M Rejection
- 400 mV Recovered Audio at 10.7 MHz
- Pin-for-Pin Replacement for MC1356P, LM1841, SN76669

FEATURING improved detector temperature stability, the Type ULN-2136A F-M, I-F amplifier/ limiter and quadrature detector is used wherever AFC stability and off-station noise are important considerations. These devices consist of a three-stage I-F amplifier/limiter, a quadrature F-M detector, an emitterfollower audio output stage, and a regulated power supply capable of furnishing up to 20 mA to external circuitry. Except for the voltage regulator, the Type ULN-2136A is similar to the original Type ULN2111A amplifier/limiter and detector.

The Type ULN-2136A is housed in a standard 14pin dual in-line plastic ' $A$ ' package.



ABSOLUTE MAXIMUM RATINGS
Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ (Note 1) 670 mW
Operating Temperature Range, $T_{A} \ldots \ldots . .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Maximum Voltage and Current Ratings at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ :

| Pin | Voltage Range <br> in Volts | Current in mA |  |
| :---: | :---: | :---: | :---: |
|  |  | Input | Output |
| 1 | 0 to +7.0 | 20 | 15 |
| 2 | -6.0 to +4.0 | 5.0 | 10 |
| 3 | -1.0 to +20 | 22 | 1.0 |
| 4 | -6.0 to +2.0 | 1.0 | 0 |
| 5 | -6.0 to +2.0 | 0.5 | 2.0 |
| 6 | -6.0 to +2.0 | 1.0 | 0 |
| 7 | reference | 1.0 | 22 |
| 8 | no connection | - | - |
| 9 | -1.0 to +1.0 | 10 | 2.0 |
| 10 | -6.0 to +2.0 | 10 | 5.0 |
| 11 | 0 to +3.0 | 5.0 | 10 |
| 12 | -6.0 to +7.0 | 1.0 | 0 |
| 13 | -1.0 to +15 | 22 | 20 |
| 14 | -6.0 to +7.0 | 1.0 | 3.0 |

NOTES:

1. Derate at the rate of $8.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.

STATIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+12 \mathrm{~V}$, Test Figure 4.

| Characteristic | Symbol | $\begin{aligned} & \text { Test } \\ & \text { Pin } \end{aligned}$ | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Supply Current | $l_{\text {cc }}$ | 3 | No Load at Pin 13 | 12 | 17 | 23 | mA |
| Terminal Voltage | $V_{1}$ | 1 |  | 3.0 | 3.8 | 4.6 | V |
|  | $V_{2}$ | 2 |  | - | 3.65 | - | V |
|  | $V_{0}$ | 6 |  | - | 1.45 | - | V |
|  | V, | 9 |  | 125 | 150 | 180 | mV |
|  | $V_{10}$ | 10 |  | 1.25 | 1.45 | 1.65 | V |
|  | $V_{\text {REG }}$ | 13 | $\mathrm{I}_{13}=5 \mathrm{~mA}$ | 7.2 | 7.8 | 8.3 | V |
| Resistance, Detector Output | $\mathrm{R}_{1}$ | 1 |  | - | 200 | - | $\Omega$ |
| I-F Input | $\mathrm{R}_{4}$ | 4 |  | - | 5.0 | - | $\mathrm{k} \Omega$ |
| 1-F Output | $\mathrm{R}_{10}$ | 10 |  | - | 60 | - | $\Omega$ |
| Detector Input | $\mathrm{R}_{12}$ | 12 |  | - | 70 | - | k $\Omega$ |
| Power Supply | $\mathrm{R}_{13}$ | 13 |  | - | 4.0 | - | $\Omega$ |
| De-Emphasis | $\mathrm{R}_{14}$ | 14 |  | 8.4 | 10.5 | 12.6 | k $\Omega$ |
| Capacitance, I-F InputDetector Input | $\mathrm{C}_{4}$ | 4 |  | - | 11 | - | pF |
|  | $\mathrm{C}_{12}$ | 12 |  | - | 2.7 | - | pF |
| Voltage Regulation |  | 13 | $\mathrm{I}_{13}=20 \mathrm{~mA}$ | - | 5.0 | 10 | $\mathrm{mV} / \mathrm{V}$ |
| Load Regulation |  | 13 | $\mathrm{I}_{13}=0$ to 20 mA | - | -30 | - | mV |
| Voltage Temp. Coefficient |  | 1 |  | - | +1.5 | - | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
|  |  | 13 | $\mathrm{I}_{13}=0$ | - | +1.5 | - | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |

DYNAMIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+12 \mathrm{~V}, \mathrm{f}_{0}=10.7 \mathrm{MHz}$, $\mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \Delta \mathrm{f}= \pm 75 \mathrm{kHz}$, Peak Separation $=600 \mathrm{kHz}$

| Characteristic | Symbol | Test <br> Pin | Test Figure | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |  |
| Amplifier Voltage Gain | $\mathrm{A}_{\text {e }}$ | 10 | 1 | $V_{\text {in }} \leq 300 \mu V_{\text {rms }}$ | - | 53 | - | dB |  |
| Amplifier Output Voltage | $V_{\text {out }}$ | 10 | 1 | $\mathrm{V}_{\text {in }}=10 \mathrm{mV}_{\text {rms }}$ | - | 1.45 | - | $\mathrm{V}_{\mathrm{pp}}$ |  |
| Input Limiting Threshold | $V_{T H}$ | 4 | 2 |  | - | 400 | 800 | $\mu \mathrm{V}_{\text {rms }}$ | 1,3 |
| Recovered Audio Output | $V_{\text {out }}$ | 1 | 2 | $\mathrm{V}_{12}=60 \mathrm{mV}_{\text {rms }}$ | 300 | 400 | 500 | $\mathrm{mV}_{\mathrm{rms}}$ | 3 |
| Output Distortion | THD | 1 | 2 | $100 \%$ F-M Modulation | - | 1.0 | 3.0 | \% | 3 |
| A-M Rejection | AMR | 1 | 3 | $\mathrm{V}_{\text {in }}=10 \mathrm{mV} \mathrm{V}_{\text {rss }}$ | - | 40 | - | dB | 2 |

NOTES:

1. The input limiting threshold is the F-M input voltage for a recovered audio output which is 3 dB less than the recovered audio output for an F -M input voltage of $200 \mathrm{mV}_{\mathrm{rms}}$.
2. The amplitude modulation rejection is determined by: $A M R_{d B}=20 \log \frac{V_{\text {out }} f o r ~}{V_{\text {out }} f 00 \% ~ F-M V_{\text {in }}}$
3. See also, General Design Note No. 9.


TEST FIGURE 1


TEST FIGURE 2


TEST FIGURE 3


TEST FIGURE 4

## F-M I-F AMPLIFIER/LIMITER and QUADRATURE DETECTOR

## GENERAL DESIGN NOTES

1. Phase shift network is aligned by applying F-M signal through decoupling network to pin $4\left(V_{4}=5 \mathrm{mV} V_{\text {rms }}\right)$. Tune for maximum recovered audio at pin 1 or maximum I-F voltage at pin 11.
2. A d-c path of less than $100 \Omega$ must be provided between pins 2 and 12. No other biasing provisions are required.
3. A d-c path of less than $300 \Omega$ must be provided between pins 4 and 6 . No other biasing provisions are required.
4. The maximum a-c load current can be increased by adding an external resistor between pin 1 and ground. The minimum value for this resistor is $800 \Omega$, giving a maximum load current of $4 \mathrm{~mA}_{\text {rms }}$.
5. All decoupling capacitors should be of the ceramic type with minimum inductance at the operating frequency.
6. Decoupling capacitor leads at pins 2,5 , and 6 should be as short as possible.
7. Keep appropriate distance between the input (pin 4 and the input network) and the phase shift network (pins 9,10 , and 12 , and the
phase shift inductor).
8. If a high impedance power supply is used (voltage dropping resistor), decouple pin 13 for the lowest audio frequency.
9. The linear detection mode (low signal level at pin 12), as shown, is preferred for communications and other commercial applications, due to the preservation of the tuned circuit bandwidth and better rejection of Gaussian noise. The combination of coupling capacitor ( $\mathrm{C}_{2}$ ) and I-F amplifier output (pin 9) was chosen for optimum quieting. The bandwidth of the phase shift network (peak separation) is primarily defined by the Damping resistor (R). A higher value resistor will decrease bandwidth, increase the recovered audio output, reduce the capture ratio, and increase harmonic distortion.
10. The switching detection mode (high signal level at pin 12) features a greater linear range, increased insensitivity to amplitude variations, and is recommended for AFC applications or where side responses must be avoided. Limiting in the quadrature detector will produce slightly more audio output, but will increase the noise bandwidth and degrade quieting.

## TRANSFER CHARACTERISTICS




## ULN-2204A A-M/F-M RADIO SYSTEM

## FEATURES

- Low Harmonic Distortion
- Wide Operating Voltage Range
- Low Power Drain
- D.C A-M/F-M Switching
- $30 \mu \mathrm{~V}$ Limiting Threshold
- Excellent A-M Rejection
- Interchangeable With HA12402, TA7613, TDA1083, U417B


PROVIDING ALL radio functions except VHF tuning, Type ULN-2204A A-M/F-M radio system excels in low-cost applications requiring a minimal parts count and high performance.

In the A-M mode of operation, the device is a complete single-conversion superheterodyne broadcast or shortwave receiver with AGC and peak envelope detection. In the F-M mode, Type ULN-2204A operates as a high-gain I-F amplifier/limiter and phase-shift detector. A simple d-c switch is used to change mode of operation.

A single external capacitor at pin 16 provides the A-M AGC time constant, the F-M AFC time constant, and R-F decoupling. A single resistor at the same pin will adjust the A-M gain for optimal system performance.

The audio power amplifier will work into any speaker load of $8 \Omega$ or greater. Class B operation of the audio power amplifier yields high efficiency at rated output with very low quiescent power drain. The amplifier exhibits little crossover distortion. Its output impedance is significantly less than one ohm.

Type ULN-2204A will work with a wide range of supply voltages, and is suitable for use in a-c powered table radios and in battery-powered ( 6 or 9 V ) portable radios.

This system will operate at supply voltages as low as 2 V at reduced volume without significant increase in distortion. Brown-outs or weak batteries need no longer be a major concern.

Type ULN-2204A is housed in a 16-pin dual in-line plastic package with a copper lead frame that eliminates many decoupling problems and allows maximum power dissipation.

## ABSOLUTE MAXIMUM RATINGS

[^35]ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$,
$V_{C C}=6.0 \mathrm{~V}, \mathbf{R}_{\mathbf{8}}=\infty, \mathbf{R}_{16}=1.2 \mathrm{k} \Omega$ (unless otherwise noted)

| Characteristic | Limits |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | Test Conditions | Min. $\quad$ Typ. $\quad$ Max. | Units |

F.M MODE: $f_{0}=10.7 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm \mathbf{7 5} \mathrm{kHz}$, Peak Separation $=550 \mathrm{kHz}$

| Input Limiting Threshold | $V_{\text {th }}$ |  | - | 30 | 60 | $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector Recovered Audio | $V_{0}$ |  | - | 250 | - | mV |
| Detector Output Distortion | THD ${ }_{\text {d }}$ | $\mathrm{V}_{\text {in }}=10 \mathrm{mV}$ ims | - | 1.0 | - | \% |
| A-M Rejection | AMR | $\begin{aligned} & \mathrm{V}_{\text {in }}=10 \mathrm{mV} \mathrm{rms}, 30 \% \mathrm{~A}-\mathrm{M}, \\ & \mathrm{f}_{\mathrm{a}-\mathrm{m}}=400 \mathrm{~Hz} \end{aligned}$ | 35 | 50 | - | dB |
| I-F Input Impedance | $z_{2}$ |  | - | 40 | - | $\mathrm{k} \Omega$ |
| I-F Input Capacitance | $\mathrm{C}_{2}$ |  | - | 4.0 | - | pF |
| Quiescent Terminal Voltage | $V_{1}$ |  | - | 2.1 | - | V |
|  | $\mathrm{V}_{8}$ |  | - | 1.7 | - | V |
| Quiescent Supply Current | $I_{\text {cc }}$ | $\mathrm{V}_{\text {CC }}=6.0 \mathrm{~V}$ | - | 14 | 20 | mA |
|  |  | $\mathrm{V}_{C C}=9.0 \mathrm{~V}$ | - | 18 | - | mA |

A-M MODE: $f_{0}=1 \mathrm{MHz}, f_{\mathrm{if}}=455 \mathrm{kHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, 30 \% \mathrm{~A}-\mathrm{M}$

| Sensitivity |  | $V_{\text {out(8) }}=20 \mathrm{mV} V_{\text {ms }}$ | - | 5.0 | 10 | $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector Recovered Audio | $\mathrm{V}_{0}$ |  | - | 150 | - | mV |
| Overload Distortion |  | 80\% A-M, also see "ULN-2204A Variations" | - | 10 | - | mV |
| Usable Sensitivity |  | $20 \mathrm{~dB} \mathrm{~S}+\mathrm{N} / \mathrm{N}$ | - | 25 | 35 | $\mu \mathrm{V}$ |
| Mixer Input Impedance | $\mathrm{Z}_{6}$ | See Note | - | 4.5 | - | $\mathrm{k} \Omega$ |
| Mixer Input Capacitance | $\mathrm{C}_{6}$ |  | - | 5.5 | - | pF |
| Mixer Output Impedance | $\mathrm{Z}_{4}$ |  | - | 25 | - | $\mathrm{k} \Omega$ |
| Mixer Output Capacitance | $\mathrm{C}_{4}$ |  | - | 3.0 | - | pF |
| I-F Input Impedance | $\mathrm{Z}_{2}$ |  | - | 100 | - | $k \Omega$ |
| I-F Input Capacitance | $\mathrm{C}_{2}$ |  | - | 3.0 | - | pF |
| Quiescent Terminal Voltage | $V_{1}$ |  | - | 1.3 | - | V |
|  | $V_{8}$ |  | - | 1.7 | - | V |
| Quiescent Supply Current | $I_{\text {cC }}$ | $V_{C C}=6.0 \mathrm{~V}$ | - | 10 | - | mA |
|  |  | $V_{C C}=9.0 \mathrm{~V}$ | - | 13 | - | mA |

AUDIO AMPLIFIER: $f_{0}=400 \mathrm{~Hz}, \mathrm{R}_{\mathrm{L}}=8 \Omega$

| Audio Gain | $\mathrm{A}_{\mathrm{e}}$ |  | 36 | 40 | 44 | dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Output Power | $\mathrm{P}_{0}$ | $\mathrm{V}_{\text {CC }}=3.0 \mathrm{~V}, 10 \%$ THD | - | 50 | - | mW |
|  |  | $\mathrm{V}_{C C}=6.0 \mathrm{~V}, 10 \% \mathrm{THD}$ | 250 | 350 | - | mW |
|  |  | $\mathrm{V}_{\text {CC }}=9.0 \mathrm{~V}, 10 \%$ THD | 500 | 650 | - | mW |
| Output Distortion | THD | $\mathrm{P}_{0}=50 \mathrm{~mW}$ | - | 2.0 | - | \% |
| A-F Input Impedance | $z_{9}$ |  | - | 250 | - | k $\Omega$ |
| Quiescent Terminal Voltage | $\mathrm{V}_{10}$ |  | - | 1.1 | - | V |
|  | $\mathrm{V}_{12}$ |  | - | 2.6 | - | V |

NOTE: For optimum noise match, source impedance should be $2.5 \mathrm{k} \Omega$.

## TEST CIRCUIT



## COIL WINDING INFORMATION



|  |  |  |  |
| :---: | :--- | :--- | :--- |
| T1 A-M First I-F | $\mathrm{Qu}=120$ | General Instrument | Toko Part No. |
| 455 kHz | $\mathrm{N} 1: \mathrm{N} 2: \mathrm{N} 3=15.5: 2.8: 1$ | Part No. EX 27835 | RMC-2A7641A |
|  | $\mathrm{Ct}=180 \mathrm{pF}$ |  |  |
| T2 A-M Second I-F | $\mathrm{Qu}=70$ | General Instrument | Toko Part No. |
| 455 kHz | $\mathrm{N}: \mathrm{N} 2=2: 1$ | Part No. EX 27836 | RLE-4A7642G0 |
|  | $\mathrm{Ct}=430 \mathrm{pF}$ |  |  |
| T3 F-M Detector | $\mathrm{Qu}=50$ | General Instrument | Toko Part No. |
| 10.7 MHz | $\mathrm{Ct}=100 \mathrm{pF}$ | Part No. EX 27640 | BKAC-K3651HM |
| T4 F-M Detector | $\mathrm{Qu}=50$ | General Instrument | Toko Part No. |
| 10.7 MHz | $\mathrm{Ct}=100 \mathrm{pF}$ | Part No. EX 27640 | BKAC-K3651HM |
| L1 A-M Oscillator | $\mathrm{Qu}=50$ | General Instrument | Toko Part No. |
| 1455 kHz | $\mathrm{NL}: \mathrm{N3}=10.711$ | Part No. EX 27641 | RWO-6A7640BM |
|  | $\mathrm{Ct}=39 \mathrm{pF}$ |  |  |

FUNCTIONAL BLOCK DIAGRAM


PIN 16 OUTPUT VOLTAGE, $\mathbf{V}_{16}$

| A-M <br> Operation | Complete Part Number Including Suffix |  |  |
| :---: | :---: | :---: | :---: |
|  | F-M Operation |  |  |
|  | $2.20-2.65 \mathrm{~V}$ | $2.55-3.05 \mathrm{~V}$ | $2.95-3.40 \mathrm{~V}$ |
| $1.40-1.75 \mathrm{~V}$ | ULN-2204A-11 | ULN-2204A-21 | ULN-2204A-31 |
| $1.65-2.00 \mathrm{~V}$ | ULN-2204A-12 | ULN-2204A-22 | ULN-2204A-32 |
| $1.90-2.25 \mathrm{~V}$ | ULN-2204A-13 | ULN-2204A-23 | ULN-2204A-33 |

TYPICAL QUIESCENT SUPPLY CURRENT


DrG. No. A-10.325A

TYPICAL AUDIO POWER OUTPUT


DWG. No. A-10. 327

# ULN-2204A VARIATIONS FOR OPTIMAL SYSTEM PERFORMANCE 

The receiver system's performance can be kept within tighter performance limits by matching bias groupings and appropriate external resistors ( $\mathrm{R}_{8}$ and $\mathrm{R}_{16}$ ). With proper matching of parts and lots, consistent device performance can be obtained. Bias groups for Type ULN2204 A are shown in the table below. There are three selections for each mode of operation and nine possible combinations.

Sprague Electric Company recommends that customers do not specify particular selections except in unusual circumstances. All parts manufactured with Sprague part numbers are branded with appropriate part-number suffixes. Any shipment to a customer will consist of parts from a single selection (single suffix).

The first digit of the suffix (the " 3 " ' in ULN-2204A-31) refers to F-M performance. It indicates F-M gain and pin 16 output voltage as functions of the pin 16 load resistance. (See graph on next page.)

F-M circuit stability is inversely related to gain or sensitivity and is affected by source and load impedances, decoupling, and printed wiring board layout. After an optimal F-M I-F gain is determined for a particular circuit design, that gain can be attained by matching the partnumber suffix and the pin 16 load.

In addition, some system designs derive the F-M tuner supply, tuner bias, or AFC voltage from pin 16 output of Type ULN-2204A. For example, if the tuner design requires 2.4 V at 2.0 mA (an equivalent $\mathrm{R}_{16}$ of 12008), the graph below indicates a Type ULN-2204A-1X is required. A - 2 X or -3 X device could also be used by paralleling the equivalent $1200 \Omega$ tuner load with a fixed resistance for an $830 \Omega$ load or a $520 \Omega$ load, respectively. For AFC applications, note that as frequency increases, $\mathrm{V}_{16}$ voltage decreases. The amount of change is a factor of load impedance, detector coil characteristics, and part grouping.

In A-M operation, stability is seldom a problem. However, large-signal overload can be optimized (to typically 30 mV ) by matching the particular part group with an appropriate load resistor at pin 8. The A-M grouping of a device is identified by the second digit of the partnumber suffix (the " 1 " in ULN-2204A-31).

For - $\mathrm{X} 1, \mathrm{R}_{8}$ should be $\infty$.
For -X2, $\mathrm{R}_{8}$ should be $47 \mathrm{k} \Omega$.
For - $\mathrm{X} 3, \mathrm{R}_{8}$ should be $33 \mathrm{k} \Omega$.
Additional loading may raise the overload point slightly, but AGC and sensitivity will be compromised. For any fixed value of $\mathrm{R}_{8},-\mathrm{X} 3$ parts will exhibit slightly higher A-M gain, while -X1 parts will have slightly lower A-M gain.

TYPICAL F-M I-F GAIN CHARACTERISTIC


## TYPICAL APPLICATION

An A-M/F-M radio using the ULN-2204A receiver system, designed for a usable F-M sensitivity of about $4 \mu \mathrm{~V}$ and an A-M sensitivity of $350 \mu \mathrm{~V} / \mathrm{m}$, appears on the next page.

The two-stage F-M tuner is operated at about 4 V . Reducing the pin 16 voltage to 1.8 V (by changing $\mathrm{R}_{16}$ ) reduces interstation noise and the F-M I-F gain. An inductor at pin 12 (L6) prevents the wide-band audio amplifier from
radiating $\mathrm{R}-\mathrm{F}$ noise in the $\mathrm{A}-\mathrm{M}$ spectrum.
The tuning indicator below may be added to the radio circuit to provide an LED indication when the received signal strength exceeds $7 \mu \mathrm{~V}$ in the F-M mode or $700 \mu \mathrm{~V} / \mathrm{m}$ in the A-M mode. The tuning indicator circuit reduces the I-F gain by about 2 dB . The sensitivity may be adjusted by changing the value of C 1 or C 2 .


## COIL AND TRANSFORMER INFORMATION FOR TYPICAL APPLICATION

| L1 | F-M Antenna Coil | 41/2 turns, \#20 AWG $(0.8 \mathrm{~mm}), 0.216^{\prime \prime}(5.5 \mathrm{~mm}) 0$ |
| :--- | :--- | :--- |
| L2 | F-M R-F Coil | $31 / 2$ turns, \#20 AWG $(0.8 \mathrm{~mm}), 0.177^{\prime \prime}(4.5 \mathrm{~mm}) 0$ |
| L3 | F-M I-F Trap | $16^{1 / 2}$ turns, \#24 AWG $(0.5 \mathrm{~mm}), 0.177^{\prime \prime}(4.5 \mathrm{~mm}) 0$ |
| L4 | F-M Oscillator Coil | $21 / 2$ turns, \#20 AWG $(0.8 \mathrm{~mm}), 0.177^{\prime \prime}(4.5 \mathrm{~mm}) 0$ |
| L5 | F-M Detector Coil | $15 \mu \mathrm{H}, \mathrm{Qu}=120 @ 2.52 \mathrm{MHz}$ |
| L6 | Audio Choke | $10 \mu \mathrm{H}, \mathrm{Qu}=2 @ 2.52 \mathrm{MHz} ;$ |
|  |  | 3 turns through ferrite bead |
| L7 | A-M Antenna Coil | Qu $=250,110: 10$ turns ratio; |
|  |  | Q2B core, $3.5^{\prime \prime}(90 \mathrm{~mm}) \times 0.394^{\prime \prime}(10 \mathrm{~mm}) 0$ |
| T1 | F-M I-F Transformer | $82 \mathrm{pF}, \mathrm{Qu}=90 @ 10.7 \mathrm{MHz}, 11: 3$ turns ratio |
| T2 | F-M I-F Transformer | $390 \mathrm{pF}, \mathrm{Qu}=75 @ 10.7 \mathrm{MHz}, 5: 2$ turns ratio |
| T3 | A-M Detector Coil | $390 \mathrm{pF}, \mathrm{Qu}=130 @ 455 \mathrm{kHz}, 100$ turns center-tapped |
| T4 | F-M Detector Coil | $150 \mathrm{pF}, \mathrm{Qu}=90 @ 10.7 \mathrm{MHz}$ |
| T5 | A-M Oscillator | $460 \mu \mathrm{H}, \mathrm{Qu}=120 @ 796 \mathrm{kHz}, 110: 11$ turns ratio |
| T6 | A-M I-F Transformer | $180 \mathrm{pF}, \mathrm{Qu}=145 @ 455 \mathrm{kHz}, 155: 10$ turns ratio; |
|  |  | primary tapped at 127 turns |


*Required only for $V_{C C} \geq 9 V$.
**I-F gain-dependent: See "ULN-2204A Variations",


ULN-2204A A-M/F-M RADIO SYSTEM

## ULN-2240A A-M/F-M SIGNAL PROCESSOR

## FEATURES

- $12 \mu \mathrm{~V}$ Limiting Threshold
- Tuning-Error and Signal-Level Muting
- Zero-Tune Meter Drive
- Balanced A-M Mixer
- $5 \mu \mathrm{~V}$ A-M Sensitivity
- D-C Mode Switching
- Internal Voltage Regulator
- Meets Dolby ${ }^{\circledR}$ Noise Requirements
- 20-Pin Dual In-Line Plastic Package

PREMIUM PERFORMANCE features such as delayed AGC for the R-F stage, an AFC drive circuit, interstation (signal level) muting, and offchannel (tuning error) muting, are offered by Type ULN-2240A.


The signal processor combines F-M I-F receiver functions and all A-M radio functions in a single monolithic integrated circuit. The system's audio output stage uses low-noise biasing that meets Dolby ${ }^{\circledR}$ receiver noise requirements.

[^36]

The A-M mixer is a balanced low-current analog multiplier with very low local oscillator feedthrough, high I-F rejection and freedom from spurious responses. It can be used in the long, medium, and shortwave bands.

A balanced four-stage differential I-F amplifier is used in both A-M and F-M modes. It gives maximum gain without common-mode interference and noise. The delayed AGC output (pin 15) can be used for a discrete R-F stage or for stereo switching logic.

In the F-M mode of operation, the detector is a high-level, four-quadrant analog multiplier. In the A-M mode, the detector is operated as a balanced peak detector.

The low-level audio output is common to both operating modes and can be used to drive an audio
power amplifier (ULN-3701Z) or stereo decoder (ULN-3810A).

A-M gain is controlled with AVC to the I-F and delayed AVC to the mixer. Switching between modes is done with a single-pole d-c switch.

Type ULN-2240A signal processor excels in signal-seeking or scanning applications. False triggers on adjacent channels or strong mistuned signals are eliminated since off-tune mute voltage changes are more pronounced than the usual signal-level voltage changes. In standard F-M radio applications, tuning-error muting eliminates the low-frequency "thump" and noise-tail associated with tuning through a strong signal.

Internal voltage regulators assure consistent performance with wide variations in supply voltage ( 8.5 to 16 V ) and temperature.

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\mathrm{cc}}$. ..... 18 V
Mute Input Voltage, $\mathrm{V}_{8}$ ..... 5.0 V
Regulator Current, $\mathrm{I}_{\text {REG }}$ ..... 5.0 mA
Package Power Dissipation, $P_{0}$ (see note) ..... 750 mW
Operating Temperature Range, $T_{A}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{s}}$ ..... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

[^37]
## TYPICAL A-M/F-M STEREO RECEIVER

 FOR AUTOMOTIVE APPLICATIONS

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{Cc}}=12.8 \mathrm{~V}$

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Operating Voltage Range | $\mathrm{V}_{\text {cc }}$ | 10 |  | 8.5 | 12.8 | 16 | V |
| Audio Output Voltage | $V_{6}$ | 6 | No Signal | - | 5.8 | - | V |
| Regulator Output Voltage | $V_{\text {Reg }}$ | 13 | No Signal | - | 6.4 | - | V |
| Avail. Reg. Output Current | $\mathrm{I}_{\text {REG }}$ | 13 |  | 2.0 | - | - | mA |

F-M MODE: $\mathrm{f}_{\mathrm{o}}=10.7 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm 75 \mathrm{kHz}, \mathrm{V}_{\mathrm{in}}=10 \mathrm{mVrms}$, Non-Muted (unless otherwise specified)

| Input Limiting Threshold | $\mathrm{V}_{\text {TH }}$ | 2 |  | - | 12 | 25 | $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Recovered Audio | $V_{\text {out }}$ | 6 |  | 350 | 425 | 600 | mV |
| Output Distortion | THD | 6 |  | - | 0.3 | 0.7 | \% |
| Output Noise | $\mathrm{S}+\mathrm{N} / \mathrm{N}$ | 6 |  | 74 | 80 | - | dB |
| A-M Rejection | AMR | 6 | See Note | 40 | $>55$ | - | dB |
| Mute | $\Delta \nu_{\text {out }}$ | 6 | $V_{\text {in }}=100 \mu \mathrm{~V}$, max. mute | - | - | -1.0 | dB |
|  |  |  | $\mathrm{V}_{\text {in }}=5.0 \mu \mathrm{~V}$, max. mute | -45 | - | - | dB |
| Mute Bandwidth | $\Delta \mathrm{f}_{\text {u }}$ | 6 | Max. mute | - | 100 | - | kHz |
| I-F Input Voltage | $V_{2}$ | 2 | No Signal | - | 3.5 | - | V |
| Mute Output Voltage | $V_{14}$ | 14 | No Signal | 3.6 | 4.2 | - | V |
| AGC Output Voltage | $\mathrm{V}_{15}$ | 15 | No Signal | 4.2 | 4.8 | 5.5 | V |
|  |  |  | $\mathrm{V}_{\text {in }}=10 \mathrm{mVrms}$ | - | - | 0.5 | V |
| Mute Output Current | $1{ }_{16}$ | 14 | No Signal | 0.5 | - | - | mA |
| Avail. AGC Output Current | $\mathrm{I}_{15}$ | 15 | No Signal | 1.0 | - | - | mA |
| Supply Current | $\mathrm{I}_{\mathrm{cc}}$ |  | No Signal | - | 26 | 40 | mA |

A-M MODE: $\mathrm{f}_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{if}}=455 \mathrm{kHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, 30 \% \mathrm{~A}-\mathrm{M}, \mathrm{V}_{\mathrm{in}}=1.0 \mathrm{mVrms}$ (unless otherwise specified)

| Sensitivity | $\mathrm{V}_{\text {in }}$ | 18 | $\mathrm{~V}_{\text {out }}=50 \mathrm{mVrms}$ | - | 5.0 | 8.5 | $\mu \mathrm{~V}$ |
| :--- | :---: | ---: | :--- | :--- | :--- | :---: | :---: |
| Usable Sensitivity |  | 18 | $20 \mathrm{~dB} \mathrm{~S}+\mathrm{N} / \mathrm{N}$ | - | 6.0 | - | $\mu \mathrm{V}$ |
| Recovered Audio | $\mathrm{V}_{\text {out }}$ | 6 | $80 \% \mathrm{~A}-\mathrm{M}$ | 250 | 325 | 600 | mV |
| Input Overload | $\mathrm{V}_{\text {in }}$ | 18 | $80 \% \mathrm{~A}-\mathrm{M}, \mathrm{THD}=10 \%$ | 25 | 50 | - | mV |
| A-M Decoupling Voltage | $\mathrm{V}_{1}$ | 1 | No Signal | - | 1.0 | - | V |
| I-F Input Voltage | $\mathrm{V}_{2}$ | 2 | No Signal | - | 3.7 | - | V |
| Mute Output Voltage | $\mathrm{V}_{14}$ | 14 | No Signal | - | 0.5 | V |  |
| AGC Output Voltage | $\mathrm{V}_{15}$ | 15 | No Signal | - | 0.5 | V |  |
| A-M Bias Voltage | $\mathrm{V}_{17}$ | 17 | No Signal | - | - | 1.8 | 2.1 |
| Supply Current | $\mathrm{I}_{\mathrm{cc}}$ |  | No Signal | V |  |  |  |

Note:
Amplitude Modulation Rejection is specified as $20 \log \frac{V_{\text {out }} \text { for } 100 \% \mathrm{~F}-\mathrm{M} \cdot \mathrm{V}_{\text {in }}}{\mathrm{V}_{\text {out }}}$ for $30 \% \mathrm{~A}-\mathrm{M} \cdot \mathrm{V}_{\text {in }}$

## COIL WINDING INFORMATION

| T1 | A-M 1-F 455 kHz | $\begin{aligned} & \mathrm{Qu}=45 \\ & \mathrm{Ct}=1000 \mathrm{pF} \end{aligned}$ | General Instrument <br> Part No. EX 27765 | Toko Part No. RXN-6A6909HM |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T2 | F-M Detector 10.7 MHz | $\begin{aligned} & \mathrm{Qu}=60 \\ & \mathrm{Ct}=82 \mathrm{pF} \end{aligned}$ | General Instrument Part No. EX 27975 | Toko Part No. TKAC-17044Z |  |
| L1 | $\begin{aligned} & \text { A-M Oscillator } \\ & 1455 \mathrm{kHz} \end{aligned}$ | $\begin{aligned} & \mathrm{Qu}=50 \\ & \mathrm{~N} 1: \mathrm{N} 2=11: 1 \\ & \mathrm{Ct}=39 \mathrm{pF} \end{aligned}$ | General Instrument Part No. EX 27641 | Toko Part No. RW0-6A7640BM |  |
| L2 | F-M Detector 10.7 MHz | $\begin{aligned} & \mathrm{L}=18 \mu \mathrm{H} \\ & \mathrm{Qu}=55 \end{aligned}$ | Coilcraft Type V |  |  |

SMALL-SIGNAL A-C CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | $\begin{aligned} & \text { Test } \\ & \text { Pin } \end{aligned}$ | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| I-F Input Capacitance | $\mathrm{C}_{2}$ | 2 |  | - | 6.0 | - | pF |
| I-F Output Resistance | $\mathrm{R}_{12}$ | 12 |  | - | 250 | - | k $\Omega$ |
| I-F Output Capacitance | $\mathrm{C}_{12}$ | 12 |  | - | 2.5 | - | pF |
| Audio Output Impedance | $\mathrm{Z}_{6}$ | 6 |  | - | 6.2 | - | k $\Omega$ |

## F-M MODE: $\mathrm{f}_{0}=10.7 \mathrm{MHz}$

| I-F Input Resistance | $\mathrm{R}_{2}$ | 2 |  | - | 10 |
| :--- | :--- | :---: | :---: | :---: | :---: |
| I-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ | $2-12$ |  | - | $\mathrm{k} \Omega$ |
| Detector Input Resistance | $\mathrm{R}_{11}$ | 11 |  | -0 | $\mathrm{mh} 0^{*}$ |
| Detector Input Capacitance | $\mathrm{C}_{11}$ | 11 |  | 100 | - |
| $\mathrm{k} \Omega$ |  |  |  |  |  |

A-M MODE: $\mathrm{f}_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{if}}=455 \mathrm{kHz}$

| A-M Input Resistance | $\mathrm{R}_{18}$ | 18 |  | - | 5.0 | - | k $\Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A-M Input Capacitance | $\mathrm{C}_{18}$ | 18 |  | - | 20 | - | pF |
| Mixer Transconductance | $\mathrm{g}_{\mathrm{m}}$ | 18-19 |  | - | 15 | - | mmho* |
| Mixer Output Resistance | $\mathrm{R}_{19}$ | 19 |  | - | 500 | - | k $\Omega$ |
| Mixer Output Capacitance | $\mathrm{C}_{19}$ | 19 |  | - | 5.0 | - | pF |
| 1-F Input Resistance | $\mathrm{R}_{2}$ | 2 |  | - | 15 | - | k $\Omega$ |
| I-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ | 2-12 |  | - | 160 | - | mmho* |
| Detector Input Resistance | $\mathrm{R}_{11}$ | 11 |  | - | 250 | - | $\mathrm{k} \Omega$ |
| Detector Input Capacitance | $\mathrm{C}_{11}$ | 11 |  | - | 1.0 | - | pF |

*The International Electrotechnical Commission recommends the use of siemens ( $S$ ) as the standard international unit of conductance, admittance and susceptance.

## TEST CIRCUIT



## Filter Assembly: <br> Toko Part No. CFU455C-82BR

A-M CHARACTERISTICS
AS FUNCTIONS OF INPUT VOLTAGE


F-M CHARACTERISTICS
AS FUNCTIONS OF INPUT VOLTAGE


## A-M CONTROL VOLTAGES

 AS FUNCTIONS OF INPUT VOLTAGE

F-M CONTROL VOLTAGES AS FUNCTIONS OF INPUT VOLTAGE


F-M TUNING-ERROR DETECTOR RESPONSE



SCHEMATIC

## ULN-2241A A-M/F-M SIGNAL PROCESSING SYSTEM

## FEATURES

- Low External Parts Count
- D-C A-M/F-M Switching
- $12 \mu \mathrm{~V}$ Limiting Threshold
- $5 \mu \mathrm{~V}$ A-M Sensitivity
- Low Harmonic Distortion
- Balanced A-M Mixer
- Internal Regulator
- 16-Pin Dual In-Line Plastic Package

THIS SIGNAL PROCESSING SYSTEM was designed with careful attention to the total system costs and performance requirements of modern automotive and high-quality home entertainment broadcast receivers. All F-M I-F functions and all A-M functions are provided by Sprague Type ULN-2241A with a minimal external parts count.


The use of an analog multiplier as a balanced low-current mixer results in freedom from spurious responses and gives the system high tweet rejection, low feedthrough (I-F rejection), and low noise, as well as very low local oscillator feedthrough.
(Continued on next page)


Although primarily intended for use in A-M broadcast reception, the $\mathrm{A}-\mathrm{M}$ mixer is also suitable for use at long-wave or shortwave frequencies. Delayed AGC is available for use with an optional discrete $\mathrm{R}-\mathrm{F}$ stage.

A fully-balanced, four stage differential I-F amplifier gives maximum gain with freedom from interference and noise. It is used in both the A-M and F-M modes of operation with approximately 82 dB gain in the $\mathrm{F}-\mathrm{M}$ mode and controlled AGC gain of 26 dB in the A-M mode.

The detector in the F-M mode is a fourquadrant analog multiplier operating in the high-level injection mode. Again, interference and noise are rejected through the use of balanced current-mirror outputs.

The delayed AGC output provides a d-c voltage for control of signal level-related func-
tions. The detector is biased to a no-signal value of 4.7 V , that approaches 0 V with increasing signal input.

In the A-M mode of operation, the detector is configured as a balanced peak detector resulting in low audio distortion. A-M gain control is achieved with AVC applied to the I-F and with delayed AVC applied to the mixer.

Switching between modes can be accomplished with a simple single-pole d-c switch. The common low-level audio output can be used to drive any suitable audio power amplifier or stereo decoder (e.g. Sprague Types ULN-3701Z and ULN-3810A, respectively).

Internal voltage regulators and bias supplies assure premium performance despite variations in external supply voltage ( 8.5 to 16 V ) or temperature $\left(-20^{\circ} \mathrm{C}\right.$ to $\left.+85^{\circ} \mathrm{C}\right)$. Separate ground leads minimize possible decoupling problems.

## ABSOLUTE MAXIMUM RATINGS

[^38]
## TYPICAL APPLICATION

 (High-Performance Table Radio)
(DW3.: no. A- 10.974

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=12.8 \mathrm{~V}$

| Characteristic | Symbol | $\begin{aligned} & \hline \text { Test } \\ & \text { Pin } \end{aligned}$ | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Operating Voltage Range | $\mathrm{V}_{\text {c }}$ | 6 |  | 10 | 12.8 | 16 | V |
| Differential Audio Output | $V_{\text {out }}$ | 5 | See Note 1 | - | - | $\pm 3.0$ | dB |
| Audio Ouput Voltage | $V_{5}$ | 5 | No Signal | - | 5.8 | - | V |
| Avail. Reg. Output Voltage | $\mathrm{V}_{\text {REG }}$ | 9 | No Signal | - | 6.4 | - | V |
| Avail. Reg. Output Current | $\mathrm{I}_{\text {REG }}$ | 9 |  | 2.0 | - | - | mA |

F-M MODE: $f_{0}=10.7 \mathrm{MHz}_{\mathrm{f}} \mathrm{f}_{\mathrm{m}}=\mathbf{4 0 0 ~ H z}, \mathrm{f}_{\mathrm{d}}= \pm \mathbf{7 5} \mathrm{kHz}, \mathrm{V}_{\mathrm{in}}=10 \mathrm{mV} \mathrm{rms}$, Non-Muted (unless otherwise specified)

| Input Limiting Threshold | $V_{\text {IH }}$ | 1 |  | - | 12 | 25 | $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Recovered Audio | $\mathrm{V}_{\text {out }}$ | 5 |  | 350 | 425 | 600 | mV |
| Output Distortion | THD | 5 |  | - | 0.3 | 0.7 | \% |
| A-M Rejection | AMR | 5 | See Note 2 | 40 | $>55$ | - | dB |
| I-F Input Voltage | $V_{1}$ | 1 | No Signal | - | 3.5 | - | $V$ |
| AGC Output Voltage | $V_{10}$ | 10 | No Signal | 4.2 | 4.8 | 5.5 | V |
|  |  |  | $\mathrm{V}_{\text {in }}=10 \mathrm{mV}$ ms | - | - | 0.5 | V |
| Avail. AGC Output Current | $1{ }_{10}$ | 10 | No Signal | 1.0 | - | - | mA |
| Supply Current | $\mathrm{I}_{\text {c }}$ |  | No Signal | - | 23 | 35 | mA |

A-M MODE: $f_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{if}}=455 \mathrm{kHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, 30 \% \mathrm{~A} \cdot \mathrm{M}, \mathrm{V}_{\text {in }}=1.0 \mathrm{mV} \mathrm{V}_{\mathrm{ms}}$ (unless otherwise specified)

| Sensitivity | $\mathrm{V}_{\text {in }}$ | 13 | $\mathrm{~V}_{\text {out }}=50 \mathrm{~m} \mathrm{~V}_{\text {Ims }}$ | - | 5.0 | 8.5 | $\mu \mathrm{~V}$ |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: |
| Useable Sensitivity |  | 13 | $20 \mathrm{~dB} \mathrm{~S}+\mathrm{N} / \mathrm{N}$ | - | 6.0 | - | $\mu \mathrm{V}$ |
| Recovered Audio | $\mathrm{V}_{\text {out }}$ | 5 | $80 \% \mathrm{~A}-\mathrm{M}$ | 250 | 325 | 550 | mV |
| Input Overload | $\mathrm{V}_{\text {in }}$ | 13 | $80 \% \mathrm{~A}-\mathrm{M}, \mathrm{THD}=10 \%$ | 25 | 50 | - | mV |
| A-M Decoupling Voltage | $\mathrm{V}_{16}$ | 16 | No Signal | - | 1.0 | - | V |
| I-F Input Voltage | $\mathrm{V}_{1}$ | 1 | No Signal | - | 3.7 | - | V |
| AGC Output Voltage | $\mathrm{V}_{10}$ | 10 | No Signal | - | - | 0.5 | V |
| A-M Input Voltage | $\mathrm{V}_{12}$ | 12 | No Signal | 1.6 | 1.8 | 2.1 | V |
| Supply Current | $\mathrm{I}_{\mathrm{cc}}$ |  | No Signal | - | 16 | 30 | mA |

Notes: 1. Differential Audio Output is specified as $20 \log \frac{V_{\text {out }} \text { for } 10 \mathrm{mV} \mathrm{F}-\mathrm{M} \mathrm{V}_{\text {in }}}{\mathrm{V}_{\text {out }}}$
2. Amplitude Modulation Rejection is specified as $20 \log \frac{V_{\text {out }} \text { for } 100 \% \mathrm{~F}-\mathrm{M} \mathrm{V}_{\text {in }}}{\mathrm{V}_{\text {out }} \text { for } 30 \% \mathrm{~A}-\mathrm{M} \mathrm{V}_{\text {in }}}$

## COIL WINDING INFORMATION

| T1 A-M I-F | Qu $=45$ | General Instrument | Toko Part No. |
| :---: | :--- | :--- | :--- |
| 455 kHz | $\mathrm{Ct}=1000 \mathrm{pF}$ | Part No. EX 27765 | RXN-6A6909HM |
| T2 F-M Detector | $\mathrm{Qu}=60$ | General Instrument | Toko Part No. |
| 10.7 MHz | $\mathrm{Ct}=82 \mathrm{pF}$ | Part No. EX 27975 | TKAC-170442 |
| L1 A-M Oscillator | $\mathrm{Qu}=50$ | General Instrument | Toko Part No. |
| 1455 kHz | $\mathrm{N}: \mathrm{N} 2=11: 1$ | Part No. EX 27641 | RWO-6A7640BM |
|  | $\mathrm{Ct}=39 \mathrm{pF}$ |  |  |
| L2 F-M Detector | $\mathrm{L}=27 \mu \mathrm{H}$ | General Instrument | Toko Part No. |
| 10.7 MHz | $\mathrm{Qu}=55 @ 2.5 \mathrm{MHz}$ | Part No. EX 27764 | 154A0-7A6115HM |

SMALL-SIGNAL A-C CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | $\begin{aligned} & \text { Test } \\ & \text { Pin } \end{aligned}$ | Test Conditions | Lımits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| I-F Input Capacitance | $\mathrm{C}_{1}$ | 1 |  | - | 6.0 | - | pF |
| I-F Output Resistance | $\mathrm{R}_{8}$ | 8 |  | - | 250 | - | k $\Omega$ |
| 1-F Output Capacitance | $\mathrm{C}_{8}$ | 8 |  | - | 2.5 | - | pF |
| Audio Output Impedance | $Z_{5}$ | 5 |  | - | 860 | - | $\Omega$ |

F-M MODE: $\mathrm{f}_{0}=\mathbf{1 0 . 7} \mathbf{~ M H z}$

| I-F Input Resistance | $\mathrm{R}_{1}$ | 1 |  | - | 10 | - | $\mathrm{k} \Omega$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ | $1-8$ |  | - | 8.0 | - | $\mathrm{mho}^{*}$ |
| Detector Input Resistance | $\mathrm{R}_{7}$ | 7 |  | - | 100 | - | $\mathrm{k} \Omega$ |
| Detector Input Capacitance | $\mathrm{C}_{7}$ | 7 |  | - | 1.5 | - | pF |

A-M MODE: $f_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{H}}=455 \mathrm{kHz}$

| A-M Input Resistance | $\mathrm{R}_{13}$ | 13 |  | - | 5.0 | - | $\mathrm{k} \Omega$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A-M Input Capacitance | $\mathrm{C}_{13}$ | 13 |  | - | 20 | - | pF |
| Mixer Transconductance | $\mathrm{g}_{\mathrm{m}}$ | $13-14$ |  | - | 15 | - | $\mathrm{mmho}^{*}$ |
| Mixer Output Resistance | $\mathrm{R}_{14}$ | 14 |  | - | 500 | - | $\mathrm{k} \Omega$ |
| Mixer Output Capacitance | $\mathrm{C}_{14}$ | 14 |  | - | 5.0 | - | pF |
| I-F Input Resistance | $\mathrm{R}_{1}$ | 1 |  | - | 15 | - | $\mathrm{k} \Omega$ |
| I-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ | $1-8$ |  | - | 160 | - | mmho |
| Detector Input Resistance | $\mathrm{R}_{7}$ | 7 |  | - | 250 | - | $\mathrm{k} \Omega$ |
| Detector Input Capacitance | $\mathrm{C}_{7}$ | 7 |  | - | 1.0 | - | pF |

*The International Electrotechnical Commission recommends the use of siernens $(S)$ as the standard international unit of conductance, admittance and susceptance.

ilter Assembly:
Toko Part No. CFU455C-82BR


## F-M CHARACTERISTICS

AS FUNCTIONS OF INPUT VOLTAGE


A-M CHARACTERISTICS
AS FUNCTIONS OF INPUT VOLTAGE


AGC OUTPUT VOLTAGE AS A FUNCTION OF INPUT VOLTAGE


AVC VOLTAGE
AS A FUNCTION OF INPUT VOLTAGE



ULN-2241A A-M/F-M SIGNAL PROCESSING SYSTEM

## ULN-2242A/TDA1 090 A-M/F-M SIGNAL PROCESSING SYSTEM

## FEATURES

- Low External Parts Count
- D-C A-M/F-M Switching
- $12 \mu \mathrm{~V}$ Limiting Threshold
- $5 \mu \mathrm{~V}$ A-M Sensitivity
- Low Harmonic Distortion
- Balanced A-M Mixer
- Meter Drive
- Internal Regulator
- Self-Contained Muting (Squelch)

SUBSTANTIAL SIMPLIFICATION of A-M/F-M receiver design is possible with Type ULN-2242A signal processing system with improved system performance and a minimal external parts count. All F-M I-F functions and all A-M functions are provided by this monolithic integrated circuit.


The use of an analog multiplier as a balanced low-current mixer results in freedom from spurious responses, high tweet rejection, low feedthrough (I-F rejection), and low noise, as well as very low local oscillator radiation.


Although primarily intended for use in A-M broadcast reception, the A-M mixer is also suitable for use at long-wave or short-wave frequencies. Delayed AGC is available for use with an optional, discrete R-F stage.

A fully-balanced, four-stage differential I-F amplifier gives maximum gain with freedom from common-mode signals. It is used in both the A-M and F-M modes of operation with approximately 82 dB gain in the F-M mode and controlled AGC gain of 26 to 82 dB in the $\mathrm{A}-\mathrm{M}$ mode.

The detector in the F-M mode is a four-quadrant analog multiplier operating in the high-level injection mode. Interference and noise are rejected. AFC and meter-drive signals (pin 7) are generated for use with any reference voltage between $\mathrm{V}_{\mathrm{cc}}$ and ground, with AFC gain determined by the choice of load resistor.

The mute and delayed AGC outputs provide d-c voltages for control of signal-level-related functions. Both detectors are biased to a no-signal value of
4.7 V and approach zero with increasing signal input.

In the A-M mode of operation, the detector is configured as a balanced peak detector for low audio distortion. A-M gain control is achieved with AVC applied to the I-F and delayed AVC applied to the mixer.
Switching between modes can be accomplished with a simple single-pole d-c switch. The common low-level audio output can be used to drive any suitable audio power amplifier or stereo decoder (Sprague Type ULN-3703Z and ULN-3810A, respectively).

Internal voltage regulators and bias supplies assure premium performance despite variations in external supply voltage ( 8.5 to 16 V ) or temperature ( $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ). Separate ground leads minimize possible decoupling problems.

Type ULN-2242A A-M/F-M signal processing system is housed in a 20 -pin dual in-line plastic package. Parts are marked with the Sprague Electric part number (ULN-2242A) unless the Pro-Electron marking (TDA1090) is requested.

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $V_{c c}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 18 V
Mute Input Voltage, $\mathrm{V}_{8}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 5.0 V
Package Power Dissipation, $P_{D}$ (see note) . . . . . . . . . . . . . . . . . . . . . . . . . . . 750 mW
Operating Temperature Range, $T_{A}$. . . . . . . . . . . . . . . . . . . . . . . . . . . $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$. .............................. $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Note: $P_{D}$ is derated at the rate of $9.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{Cc}}=12.8 \mathrm{~V}$

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Operating Voltage Range | $V_{c c}$ | 10 |  | 8.5 | 12.8 | 16 | V |
| Audio Output Voltage | $V_{6}$ | 6 | No Signal | - | 5.8 | - | V |
| Regulator Output Voltage | $V_{\text {ReG }}$ | 13 | No Signal | - | 6.4 | - | V |
| Regulator Output Current | $\mathrm{I}_{\text {REG }}$ | 13 |  | 2.0 | - | - | mA |

F-M MODE: $\mathrm{f}_{0}=10.7 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm \mathbf{7 5} \mathrm{kHz}, \mathrm{V}_{\text {in }}=10 \mathrm{mVrms}$, Non-Muted (unless otherwise specified)

| Input Limiting Threshold | $\mathrm{V}_{\text {TH }}$ | 2 |  | - | 12 | 25 | $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Recovered Audio | $V_{\text {out }}$ | 6 |  | 350 | 425 | 600 | mV |
| Output Distortion | THD | 6 |  | - | 0.3 | 0.7 | \% |
| A-M Rejection | AMR | 6 | See Note | 40 | >55 | - | dB |
| Mute | $\Delta V_{\text {out }}$ | 6 | $\mathrm{V}_{\mathrm{in}}=100 \mu \mathrm{~V}$, max. mute | - | - | -1.0 | dB |
|  |  |  | $V_{\text {in }}=5 \mu \mathrm{~V}$, max. mute | -45 | - | - | dB |
| AFC Output Voltage | $V_{\text {atc }}$ | 7 |  | 220 | - | 600 | mV |
| I-F Input Voltage | $\mathrm{V}_{2}$ | 2 | No Signal | - | 3.5 | - | V |
| Mute Output Voltage | $V_{14}$ | 14 | No Signal | 3.6 | 4.2 | - | V |
| AGC Output Voltage | $V_{15}$ | 15 | No Signal | 4.2 | 4.8 | 5.5 | V |
|  |  |  | $\mathrm{V}_{\text {in }}=10 \mathrm{mVrms}$ | - | - | 0.5 | V |
| Mute Output Current | $\mathrm{I}_{14}$ | 14 | No Signal | 0.5 | - | - | mA |
| AGC Output Current | $\mathrm{I}_{15}$ | 15 | No Signal | 1.0 | - | - | mA |
| Supply Current | $\mathrm{I}_{\mathrm{cc}}$ |  | No Signal | - | 23 | 35 | mA |

A-M MODE: $\mathrm{f}_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{if}}=455 \mathrm{kHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, 30 \% \mathrm{~A}-\mathrm{M}, \mathrm{V}_{\mathrm{in}}=1.0 \mathrm{mVrms}$ (unless otherwise specified)

| Sensitivity | $V_{\text {in }}$ | 18 | $V_{\text {out }}=50 \mathrm{mVrms}$ | - | 5.0 | 8.5 | $\mu \mathrm{~V}$ |
| :--- | :--- | ---: | :--- | :--- | :---: | :---: | :---: |
| Usable Sensitivity |  | 18 | $20 \mathrm{~dB} \mathrm{~S}+\mathrm{N} / \mathrm{N}$ | - | 6.0 | - | $\mu \mathrm{V}$ |
| Recovered Audio | $\mathrm{V}_{\text {out }}$ | 6 | $80 \% \mathrm{~A}-\mathrm{M}$ | 250 | 325 | 600 | mV |
| Input Overload | $V_{\text {in }}$ | 18 | $80 \% \mathrm{M}-\mathrm{M}, \mathrm{THD}=10 \%$ | 25 | 50 | - | mV |
| A-M Decoupling Voltage | $\mathrm{V}_{1}$ | 1 | No Signal | - | 1.0 | - | V |
| I-F Input Voltage | $\mathrm{V}_{2}$ | 2 | No Signal | - | 3.7 | - | V |
| Mute Output Voltage | $\mathrm{V}_{14}$ | 14 | No Signal | - | 0.5 | V |  |
| AGC Output Voltage | $\mathrm{V}_{15}$ | 15 | No Signal | - | 0.5 | V |  |
| A-M Input Voltage | $\mathrm{V}_{17}$ | 17 | No Signal | - | - | 1.8 | 2.1 |
| Supply Current | $\mathrm{I}_{\mathrm{cc}}$ |  | No Signal | V |  |  |  |

Note:
Amplitude Modulation Rejection is specified as $20 \log \frac{V_{\text {out }} V_{\text {out }} \text { for } 100 \% \text { F-M V in }}{V_{\text {out }}}$

SMALL-SIGNAL A-C CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| T-F Tnput Capacitance | $\mathrm{C}_{2}$ | 2 |  | - | 6.0 | - | pF |
| I-F Output Resistance | $\mathrm{R}_{12}$ | 12. |  | - | 250 | - | $\mathrm{k} \Omega$ |
| I-F Output Capacitance | $\mathrm{C}_{12}$ | 12 |  | - | 2.5 | - | pF |
| Audio Output Impedance | $\mathrm{Z}_{6}$ | 6 |  | - | 860 | - | $\Omega$ |

## F-M MODE: $\mathrm{f}_{0}=10.7 \mathrm{MHz}$

| I-F Input Resistance | $\mathrm{R}_{2}$ | 2 |  | -10 | - | $\mathrm{k} \Omega$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| I-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ | $2-12$ |  | - | 18 | - |
| Detector Input Resistance | $\mathrm{R}_{11}$ | 11 |  | $\mathrm{mh} 0^{*}$ |  |  |
| Detector Input Capacitance | $\mathrm{C}_{11}$ | 11 |  | - | 100 | - |
| $\mathrm{k} \Omega$ |  |  |  |  |  |  |

A-M MOOE: $f_{0}=1$ MHz, $f_{i f}=455 \mathrm{kHz}$

| A-M Input Resistance | $\mathrm{R}_{18}$ | 18 |  | - | 5.0 | - | $\mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A-M Input Capacitance | $\mathrm{C}_{18}$ | 18 |  | - | 20 | - | pF |
| Mixer Transconductance | $\mathrm{g}_{\mathrm{m}}$ | 18-19 |  | - | 15 | - | mmho* |
| Mixer Output Resistance | $\mathrm{R}_{19}$ | 19 |  | - | 500 | - | $\mathrm{k} \Omega$ |
| Mixer Output Capacitance | $\mathrm{C}_{19}$ | 19 |  | - | 5.0 | - | pF |
| 1-F Input Resistance | $\mathrm{R}_{2}$ | 2 |  | - | 15 | - | $\mathrm{k} \Omega$ |
| 1-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ | 2-12 |  | - | 300 | -- | mmho* |
| Detector Input Resistance | $\mathrm{R}_{11}$ | 11 |  | - | 250 | - | $\mathrm{k} \Omega$ |
| Detector Input Capacitance | $\mathrm{C}_{11}$ | 11 |  | - | 1.0 | - | pF |

*The International Electrotechnical Commission recommends the use of siemens $(S)$ as the standard international unit of conductance, admittance and susceptance.

## TEST CIRCUIT



COIL WINDING INFORMATION


OW3. N0. A-10. 428

| T1 | A-M I-F | Qu $=45$ | General Instrument | Toko Part No. |
| :--- | :--- | :--- | :--- | :--- |
|  | 455 kHz | $\mathrm{Ct}=1000 \mathrm{pF}$ | Part No. EX 27765 | RXN-6A6909HM |
| T2 | $\mathrm{F}-\mathrm{M}$ Detector | $\mathrm{Qu}=60$ | General Instrument | Toko Part No. |
|  | 10.7 MHz | $\mathrm{Ct}=82 \mathrm{pF}$ | Part No. EX 27975 | TKAC-17044Z |
| L1 | A-M Oscillator | $\mathrm{Qu}=50$ | General Instrument | Toko Part No. |
|  | 1455 kHz | $\mathrm{N1:N2}=11: 1$ | Part No. EX 27641 | RWO-6A7640BM |
|  |  | $\mathrm{Ct}=39 \mathrm{pF}$ |  |  |
| L2 | $\mathrm{F}-\mathrm{M}$ Detector | $\mathrm{L}=18 \mu \mathrm{H}$ |  | Coilcraft |
|  | 10.7 MHz | $\mathrm{Qu}=55$ |  | Type V |

Filter Assembly:
Toko Part No. CFU455C-82BR


## A-M CHARACTERISTICS

AS FUNCTIONS OF INPUT VOLTAGE


F-M CHARACTERISTICS
AS FUNCTIONS OF INPUT VOLTAGE


A-M CONTROL VOLTAGES
AS FUNCTIONS OF INPUT VOLTAGE


F-M CONTROL VOLTAGES
AS FUNCTIONS OF INPUT VOLTAGE



SCHEMATIC

ULN-2243A

## MIXER/I-F FOR F-M RADIO APPLICATIONS

## FEATURES

- Doubly-Balanced Linear Mixer
- Very-High I-F Rejection
- 32 mmho (millisiemens) Conversion Gain at 100 MHz
- $330 \Omega$ I-F Input/Output Impedance
- 46 dB I-F Gain at 10.7 MHz
- AGC Detector for MOSFET R-F Stage
- Low External Component Count
- 16-Pin Dual In-Line Plastic Package


PROVIDING AN IMPORTANT basic building block for use in F-M radio applications, the ULN2243A mixer/I-F minimizes spurious responses from strong off-channel signals while providing an excellent noise figure, maximum desired signal gain and very-high I-F rejection.

The linear fully-balanced mixer is an analog multiplier which will outperform discrete mixers. The low local oscillator and received frequency feedthrough greatly reduces the outband rejection requirements.

I-F gain is furnished by a 2-stage amplifier with the
gain set at typically 46 dB . Input and output impedances are $330 \Omega$ to allow the use of inexpensive ceramic filter coupling.

Both bias and AGC voltages, for use with a dualgate MOSFET R-F stage, are provided by the wideband AGC detector. An inhibit connection (pin 14) allows for maximum wide-band R-F gain up to the signal level at which the AGC action of the following narrow-band I-F amplifier/limiter and detector (ULN-3840A or ULN-3889A) starts operating. For strong on-channel signal levels, the wide-band R-F gain is determined by the strongest in-band signal.


FUNCTIONAL BLOCK DIAGRAM

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Fig. | $\begin{aligned} & \text { Test } \\ & \text { Pin } \\ & \hline \end{aligned}$ | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Min. | Typ. | Max. | Units |
| Quiescent Supply Current | Icc |  | $5+6$ | $V_{c c}=+12 \mathrm{~V}$ | 5.0 | - | 11 | mA |
|  |  |  | $12+15$ | $\mathrm{V}_{\mathrm{cc}}=+8 \mathrm{~V}$ | 18 | - | 38 | mA |
| MIXER: $\mathrm{f}_{\text {in }}=100 \mathrm{MHz}, \mathrm{V}_{\text {osc }}=200 \mathrm{mV}, \mathrm{f}_{\text {osc }}=110.7 \mathrm{MHz}, \mathrm{f}_{\text {out }}=10.7 \mathrm{MHz}$ |  |  |  |  |  |  |  |  |
| Input Impedance | $\mathrm{Z}_{\text {in }}$ | 1 | 9 or 10 | $V_{\text {in }}=25 \mathrm{mV}$ | - | 525 | - | $\Omega$ |
| Input Capacitance | $\mathrm{C}_{\text {m }}$ | 1 | 9 or 10 | $V_{\text {in }}=25 \mathrm{mV}$ | - | 9.0 | - | pF |
| Osc. Impedance | $\mathrm{Z}_{\text {osc }}$ | 1 | 7 or 8 | $\mathrm{V}_{\mathrm{in}}=0$ | - | 170 | - | $\Omega$ |
| Osc. Capacitance | $\mathrm{C}_{\text {osc }}$ | 1 | 7 or 8 | $\mathrm{V}_{\mathrm{in}}=0$ | - | 10 | - | pF |
| Output Impedance | $Z_{\text {out }}$ | 2 | 5 or 6 | $V_{\text {in }}=0$ | - | 120 | - | $\mathrm{k} \Omega$ |
| Output Capacitance | $\mathrm{C}_{\text {out }}$ | 2 | 5 or 6 | $\mathrm{V}_{\text {in }}=0$ | - | 3.2 | - | pF |
| Conversion Gain | $\mathrm{g}_{\mathrm{m}}$ | 3 |  | $\mathrm{V}_{\text {in }}=1.0 \mathrm{mV}$ | - | 32 | - | mmho |
| I-F AMPLIFIER: $\mathbf{V}_{\text {in }}=100 \mu \mathbf{V}, \mathrm{f}_{\text {in }}=10.7 \mathrm{MHz}$ |  |  |  |  |  |  |  |  |
| Input Resistance | $\mathrm{R}_{\text {iN }}$ |  | 1 |  | - | 330 | - | $\Omega$ |
| Output Resistance | $\mathrm{R}_{\text {out }}$ |  | 16 |  | - | 280 | - | $\Omega$ |
| I-F Gain | $\mathrm{A}_{\mathrm{e}}$ |  | 16 |  | - | 46 | - | dB |
| AGC DETECTOR: $\mathrm{f}_{\text {in }}=10.7 \mathrm{MHz}, \mathrm{V}_{\text {in }}=\operatorname{Pin} 4, \mathrm{~V}_{\text {IN }}=\operatorname{Pin} 14$ |  |  |  |  |  |  |  |  |
| Detector Threshold | $V_{\text {in }}$ |  | 4 | $\mathrm{V}_{\mathrm{N}}=3.5 \mathrm{~V}$ | - | 150 | - | mV |
| Inhibit Threshold | $V_{\text {IN }}$ |  | 14 | $\mathrm{V}_{\text {in }}=350 \mathrm{mV}, \mathrm{V}_{\text {out }}=2.0 \mathrm{~V}$ | 0.8 | - | 2.0 | V |
| Quiescent Output Voltage | $V_{\text {out }}$ |  | 13 | $V_{\text {in }}=0$ and/or $V_{\text {iN }}=0$ | - | 7.7 | - | V |
| Output Voltage | $V_{\text {Out }}$ |  | 13 | $\mathrm{V}_{\text {in }}=350 \mathrm{mV}, \mathrm{V}_{\text {IN }}=3.5 \mathrm{~V}$ | - | 0.7 | - | V |



Figure 1


Figure 2


Figure 3

## APPLICATION INFORMATION

The ULN-2243A mixer/I-F performs a variety of functions especially suitable for automobile radios and other receivers required to handle an extremely wide range of input signal levels. It has been designed to use some of the inherent advantages of an integrated circuit to improve F-M front end designs instead of simply attempting to replace discrete devices with integrated ones. This allows the tuner designer to select an R-F amplifier and oscillator circuit best-suited to the particular application.

The double-balanced mixer $\left(Q_{1}\right.$ through $Q_{7}$, Figure 4) is internally biased so that all inputs can be capacitively coupled. this mixer possesses several advantages over discrete devices.:

1. High inherent I-F rejection,
2. Good I-F/2 rejection,
3. Less oscillator drive required than with FET mixers,
4. Low oscillator feed through,
5. Less oscillator modulation with large signals, and
6. Balanced inputs eliminate ground loops which can cause stray coupling paths in discrete mixers.
Note that the oscillator input can be to either pin 7 or pin 8, the R-F input to either pin 9 or pin 10, to suit the circuit board layout.

The I-F transformer used with the ULN-2243A has been made to utilize both outputs of the mixer and was wound on a bobbin type coil form (Toko Type 10EZ) to maintain close couplings between windings. This eliminates the high cost of a bifilar-wound transformer. A conventional tuner with two R-F tuned circuits will typically have an I-F/2 rejection of at least 100 dB and a low noise figure. A single-ended output from either pin 5 or pin 6 could have been used (with degradation in rejection and noise figure) with the remaining output connected directly to $\mathrm{V}_{\mathrm{CC}}$.

The limiting amplifier consists of transistors $\mathrm{Q}_{8}$ through $\mathrm{Q}_{15}$ and has about 46 dB of gain at 10.7 MHz . The input and output impedances are $330 \Omega$ for easy ceramic filter connection. The differential input again avoids the low-impedance ground loops associated with discrete common emitter I-F input stages. This makes the construction of a stable amplifier much easier. Since the I-F amplifier is an independent element, various combinations of filters before and after the amplifier are possible.

The relatively high gain of the ULN-2243A I-F amplifier allows the circuit designer to use surface wave or cascaded ceramic filters between it and the
amplifier/detector integrated circuit. The resistive matching pad between ceramic filter elements prevents interactions which can cause undersirable group delay variations.

The AGC detector between pins 4, 13, and 14 has some unique properties which can be used in different ways. If the R-F amplifier is a dual-gate MOSFET (Figure 5), only the minimum in external discrete components is required.

The AGC detector input (pin 4) is connected through a small coupling capacitor to the mixer output. Internally is an R-F peak detector $\left(\mathrm{Q}_{20}\right)$ and d-c amplifier $\left(Q_{21}\right.$ through $\left.Q_{24}\right)$. If the $A G C$ inhibit voltage (pin 14) is greater than approximately 1 volt, the AGC output voltage (pin 13) will change from typically 7.7 V with no applied signal to 0.5 V if an R-F signal of more than 150 mV is present at the input. This allows the tuner designer several design possibilities:

1. Connecting the AGC inhibit to the meter drive output of the limiter/detector (pin 13, ULN3840A or ULN-3889A), the R-F stage will be AGC'd when tuned to a strong signal or when tuned to a weak signal with a strong adjacent channel signal, or
2. Pin 14 can be connected to a fixed bias voltage (typically +5 V ). The R-F stage would then be AGC'd by any signal falling within the mixer coil bandpass, or
3. Combinations of fixed bias and signal-dependent levels (AFC, deviation mute, or delayed AGC) will then allow almost an unlimited number of AGC possibilities.
The AGC characteristics of the ULN-2243A mixer/I-F can be used with many other types of R-F amplifier. By adding a discrete transistor amplifier at pin 13, the AGC signal can be inverted and/or amplified to drive a bipolar R-F stage into forward AGC or to drive a PIN diode attenuator. A simplified graphical illustration of the most common AGC characteristic is shown in Figure 6.

A typical application of the ULN-2243A mixer/I-F in an F-M tuner was shown in Figure 5. Note that an output from the high-frequency oscillator has been provided with no increase in cost. This is one advantage to having the oscillator external to the integrated circuit. Also, by not including the R-F amplifier within the device, a wide variety of R-F amplifiers can be used depending on the wishes of the designer or the particular constraints of the application.


Figure 4 SCHEMATIC


Figure 5
TYPICAL APPLICATION


Owq. No. A-11.039

Figure 6
AGC CHARACTERISTICS

## ULN-2245A PHASE-LOCKED LOOP STEREO DECODER

## FEATURES

- Excellent Channel Separation
- Low Total Harmonic Distortion
- Power Supply Decoupling
- VCO Frequency Stable
- High Gain
- Operating Voltage - 10.5 to 16 V
- 70 dB SCA Rejection
- 16-Pin Dual In-Line Plastic Package

STEREO multiplexed F-M signals are decoded by Sprague Type ULN-2245A without the use of tuning coils required for operation of previous stereo processors in F-M receivers.

The monolithic integrated circuit creates a signal in phase with and exactly twice the frequency of the 19 kHz pilot signal provided by stereo transmissions. This 38 kHz subcarrier is used to demodulate F-M stereo broadcast information.

The stereo portion of the circuit is disabled during reception of weak signals or monaural broadcasts.

Additional features include emitter-follower outputs for driving low impedance loads and a voltage regulator for increased stability. Type ULN-2245A is suitable for both line-operated and automotive


F-M stereo receivers.
Except for a reduced audio output impedance, Type ULN-2245A is interchangeable with Type ULN-2244A, $\mu \mathrm{A} 758$, LM1800, and MC1311.

## ABSOLUTE MAXIMUM RATINGS

$$
\text { Supply Voltage, Vcc . . . . . . . . . . . . . . . . . . . . . . . . . }+16 \mathrm{~V}
$$

Supply Voltage ( $\leq 15 \mathrm{~s}$ ) ..... $+22 V$
Lamp Supply Voltage, $\mathrm{V}_{\mathrm{L}}$ ..... $+22 \mathrm{~V}$
Lamp Current, $\mathrm{I}_{\text {Lamp }}$ ..... 150 mA
Output Current, $I_{4}$ or $I_{5}$ ..... 10 mA
Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ ..... 1.33 W
Operating Temperature Range, $T_{A}$ ..... $+85^{\circ} \mathrm{C}$


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+12 \mathrm{~V}$, Composite Input $=300 \mathrm{mV} \mathrm{V}_{\mathrm{rms}}(\mathrm{L}=\mathrm{R}$, pilot OFF),
Pilot level $=30 \mathrm{mV} \mathrm{V}_{\text {rms }}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}$ or 1 kHz , unless otherwise specified.

| Characteristics | Symbol | Test Condition | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |  |
| Supply Current | $\mathrm{I}_{\mathrm{CC}}$ | Lamp "OFF" | - | 26 | 40 | mA |  |
| Lamp Current | $\mathrm{T}_{\text {amp }}$ | Short Circuit, Lamp "ON" | 50 | 100 | - | mA |  |
|  |  | Lamp "OFF" | - | 30 | 100 | $\mu \mathrm{A}$ |  |
| Lamp Driver Terminal Voltage | $V_{7}$ | $\mathrm{I}_{\text {lamp }}=50 \mathrm{~mA}$ | - | 1.3 | 2.0 | V |  |
| Stereo Lamp "0N" | $\mathrm{S}_{\mathrm{H}}$ | 19 kHz Input | - | 15 | 25 | mV ms |  |
| Stereo Lamp "0FF", | $\mathrm{S}_{1}$ | 19 kHz Input | 2.0 | 7.0 | - | mV ms |  |
| Stereo Channel Separation | $\frac{e_{\text {out }}}{\hat{e}_{\text {out } 2}}$ | $\mathrm{f}=10 \mathrm{kHz}$ | - | 30 | - | dB |  |
|  |  | $\mathrm{f}=400 \mathrm{~Hz}$ | - | 30 | - | dB |  |
|  |  | $\mathrm{f}=100 \mathrm{~Hz}$ | - | 30 | - | dB |  |
| Output Voltage Shift |  | Stereo to Mono Operation | - | $\pm 30$ | - | mV |  |
| 19 kHz Rejection |  |  | 25 | 35 | - | dB |  |
| 38 kHz Rejection |  |  | 25 | 45 | - | dB |  |
| SCA Rejection | $A_{\text {SCA }}$ |  | - | 70 | - | dB | 1 |
| Power Supply Rejection | $V_{\text {SR }}$ | $200 \mathrm{~Hz}, 200 \mathrm{mV}$ ms | - | 45 | - | dB |  |
| Total Harmonic Distortion | THD | $\begin{aligned} & \hline \text { Multiplex Level }= \\ & 600 \mathrm{mV} \\ & \hline \end{aligned}$ | - | 0.4 | 1.5 | \% |  |
| Input Resistance | $\mathrm{R}_{\text {in }}$ |  | 20 | 35 | - | k $\Omega$ |  |
| Monaural Audio Balance |  |  | - | 0.3 | 1.5 | dB |  |
| Voltage Gain | $\mathrm{A}_{v}$ | $\mathrm{f}=1 \mathrm{kHz}$ | 0.5 | 0.9 | 1.4 | V/V |  |
| Capture Range |  |  | 2.0 | 4.0 | 8.0 | \% |  |
| Stereo Lamp Hysteresis |  | Lamp " 0 FF" to Lamp "ON" | 3.0 | 5.0 | - | dB |  |
| Output Resistance | $\mathrm{R}_{\text {out }}$ |  | - | 50 | - | $\Omega$ |  |
| VCO Tuning Resistance | $\mathrm{R}_{15}$ | $\square$ | 20 | 23 | 26 | k $\Omega$ | 2 |
| VC0 Frequency Drift |  | $0^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<25^{\circ} \mathrm{C}$ | - | +0.1 | $\pm 2.0$ | \% |  |
|  |  | $25^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<70^{\circ} \mathrm{C}$ | - | -0.4 | $\pm 2.0$ | \% |  |

## NOTES:

1. Measured with a stereo composite signal of $80 \%$ stereo, $10 \%$ pilot, and $10 \%$ SCA.
2. Total resistance from pin 15 to ground, in the test circuit, required to set reference frequency at pin 11 to $19 \mathrm{kHz} \pm 10 \mathrm{~Hz}$.



## ULN-2249A A-M RADIO SYSTEM FOR AUTOMOTIVE APPLICATIONS

## FEATURES

- Low External Parts Count
- Internal Bias Regulator
- High AGC Ratio
- Low Distortion
- Good Sensitivity
- Direct Replacement for HA1199

satisfactorily under wide variations in signal level. A typical AGC ratio of 63 dB , a usable sensitivity of approximately $8 \mu \mathrm{~V}$, and an overload point in excess of 3 V , all contribute to the excellent performance of these devices under real conditions. Moreover, the ULN-2249A A-M radio system is rated for operation over the broad supply voltage range of 10.8 V to 15.6 V although the selfcontained local oscillator will continue to function at much lower voltages. : ... . .

SPECIFICALLY DESIGNED for automotive A-M radio applications, the ULN-2249A A-M radio system consists of an $\mathrm{R}-\mathrm{F}$ amplifier, converter, I-F amplifier, A-M detector, AGC amplifier, and bias voltage regulator. The low-level audio output can be used to drive a standard audio power amplifier, such as the Sprague Type ULN-3701Z.

Of particular significance in automotive applications is the ability of this integrated circuit to perform

FUNCTIONAL BLOCK DIAGRAM


## ABSOLUTE MAXIMUM RATINGS

```Supply Voltage, \(\mathrm{V}_{\text {cc }}\)18 V
```

Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ ..... 670 mW*
Operating Temperature Range, $T_{A}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ ..... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
${ }^{*}$ Derate at the rate of $8.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{Cc}}=13.5 \mathrm{~V}, \mathrm{f}_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{if}}=262.5 \mathrm{kHz}$, $\mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, 30 \% \mathrm{~A}-\mathrm{M}$, Figure 2 (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Quiescent Supply Current | $\mathrm{I}_{\text {c }}$ | Figure 1 | - | 15 | - | mA |
| Sensitivity | $V_{\text {in }}$ | $V_{\text {out }}=20 \mathrm{mV}$ | - | 3.0 | 6.0 | $\mu \mathrm{V}$ |
| Detector Output Voltage | $V_{8}$ | $\mathrm{V}_{\text {in }}=5.0 \mathrm{mV}$ | 50 | - | - | mV |
| Output Distortion | THD | $V_{\text {in }}=500 \mathrm{mV}$ | - | 0.4 | 5.0 | \% |
| Signal-to-Noise Ratio | $\mathrm{S}+\mathrm{N} / \mathrm{N}$ | $V_{\text {in }}=50 \mu \mathrm{~V}$ | 26 | 30 | - | dB |
| AGC Ratio* |  | $\mathrm{V}_{\mathrm{in}}=20 \mathrm{mV}$ | 60 | 63 | - | dB |

*AGC Ratio is defined as the ratio of the input voltages for a reduction in output voltage of 10 dB with the high level input as specified.

SMALL-SIGNAL A-C CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=13.5 \mathrm{~V}, \mathrm{f}_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{if}}=262.5 \mathrm{kHz}$, $\mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, 30 \% \mathrm{~A}-\mathrm{M}, \mathrm{V}_{\mathrm{in}} \leq 27 \mathrm{mVrms}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| R-F Input Impedance | $\mathrm{Z}_{1}$ | Also, see note | - | 6.0 | - | $\mathrm{k} \Omega$ |
| R-F Output Impedance | $\mathrm{Z}_{16}$ |  | - | 100 | - | $\mathrm{k} \Omega$ |
| R-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ |  | - | 16 | - | mmho |
| Conv. Input Impedance | $\mathrm{Z}_{14}$ |  | - | 12 | - | $\mathrm{k} \Omega$ |
| Osc. Input Impedance | $\mathrm{Z}_{13}$ | $\mathrm{f}_{\text {osc }}=1.262 \mathrm{MHz}$ | - | 3.6 | - | $\mathrm{k} \Omega$ |
| Conv. Output Impedance | $\mathrm{Z}_{12}$ |  | - | 100 | - | $k \Omega$ |
| Conv. Transconductance | $\mathrm{g}_{\mathrm{m}}$ | Pin 14-12, $\mathrm{V}_{13}=300 \mathrm{mVrms}$ | - | 0.2 | - | mmho |
|  |  | Pin 13-12, $\mathrm{V}_{13} \leqq 27 \mathrm{mVrms}$ | - | 1.4 | - | mmho |
| Osc. Input Voltage | $V_{13}$ | For optimum conv. performance | 300 | - | - | mVrms |
| I-F Input Impedance | $\mathrm{Z}_{10}$ |  | - | 2.8 | - | k $\Omega$ |
| I-F Output Impedance | $\mathrm{Z}_{5}$ | \% | - | 50 | - | $\Omega$ |
| I-F Gain | Ae |  | - | 24 | - | dB |
| Det. Input Impedance | $\mathrm{Z}_{6}$ |  | - | 310 | - | $\Omega$ |
| Det. Output Impedance | $\mathrm{Z}_{8}$ |  | - | 100 | - | $\Omega$ |
| Det. Gain | Ae |  | - | 25 | - | dB |

NOTE: For optimum noise match, source impedance should be $1.2 \mathrm{k} \Omega$.

## TEST CIRCUITS



Ding. Ko. A- 10.430
FIGURE 1


FIGURE 2

## COIL WINDING INFORMATION



| T1 First I-F | $Q_{\mathrm{up}}=80, Q_{\mathrm{us}}=75$ | Toko Part No. |
| :--- | :--- | :--- |
| 262.5 kHz | $\mathrm{Nt}: \mathrm{Np}: \mathrm{Ns}=13: 2.3: 1$ | B124FCS-1013PYG/ |
|  | $\mathrm{Ct}=150 \mathrm{pF}$ | B124FCS-1014STB |
| T2 Second l-F | $\mathrm{Q}_{\mathrm{up}}=80, \mathrm{Q}_{\mathrm{us}}=75$ | Toko Part No. |
| 262.5 kHz | $\mathrm{Nt}: \mathrm{Np}: \mathrm{Ns}=13: 5.6: 1$ | B124FCS-60001PYG/ |
|  | $\mathrm{Ct}=150 \mathrm{pF}$ | B124FCS-1014STB |



RECOVERED AUDIO, NOISE, AND DISTORTION AS FUNCTIONS OF SIGNAL INPUT


OUTPUT VOLTAGE
AS A FUNCTION OF INTERFERENCE FREQUENCY


# ULX-3804A <br> A-M/F-M SIGNAL PROCESSOR 

## FEATURES

- Good Sensitivity
- Low Harmonic Distortion
- Wide Operating Voltage Range
- Excellent A-M Rejection
- Low Power Drain
- D-C A-M/F-M Switching
- $30 \mu \mathrm{~V}$ Limiting Threshold
- 16-Pin Dual In-Line Plastic Package


DESIGNED for use in battery-powered portable radios or line-driven table radios, Type ULX3804A works well in low-cost applications requiring high performance with few external parts. An entire A-M/F-M stereo receiver can be built with a Type ULX-3804A, a Type ULN-3809A stereo decoder, and two Type ULN-2283B audio amplifiers, for operation over a supply range of 4.5 to 12 V .

The signal processor includes the A-M oscillator and mixer and the A-M/F-M I-F amplifier and detector from the popular radio system, Sprague Type ULN-2204A. Radio designs using Type ULN2204 A can be revised for greater power output or for stereo operation (without reworking the printed wiring board layout) by replacement of Type ULN2204A with Type ULX-3804A and addition of appropriate stereo decoders and audio power amplifiers.

In the A-M mode of operation, Type ULX-3804A provides all high-frequency circuitry, including AGC and envelope peak detection, for a singleconversion superheterodyne broadcast or shortwave receiver. In the F-M mode, the signal processor operates as a high-gain amplifier /limiter and phaseshift detector. A d-c switch is used to change modes.

A single external capacitor at pin 16 provides the A-M AGC time constant, the F-M AFC time constant, and R-F decoupling.

## ABSOLUTE MAXIMUM RATINGS

## FUNCTIONAL BLOCK DIAGRAM

OSC. OUT IN A-M GAIN ADJ.

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$,
$V_{C C}=6.0 \mathrm{~V}, R_{8}=\infty, R_{16}=1.2 \mathrm{k} \Omega$ (unless otherwise noted)


F-M MODE: $f_{0}=10.7 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm 75 \mathrm{kHz}$, Peak Separation $=550 \mathrm{kHz}$

| Input Limiting Threshold | $\mathrm{V}_{\text {ti }}$ |  | - | 30 | 60 | $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector Recovered Audio | V |  | - | 250 | - | mV |
| Detector Output Distortion | THD | $\mathrm{V}_{\mathrm{in}}=10 \mathrm{mV} \mathrm{m}_{\text {ms }}$ | - | 1.0 | - | \% |
| A-M Rejection | AMR | $\begin{aligned} & V_{\text {in }}=10 \mathrm{mV} \mathrm{I}_{\text {mss }} 30 \% \mathrm{~A}-\mathrm{M}, \\ & \mathrm{f}_{\mathrm{am}}=400 \mathrm{~Hz} \end{aligned}$ | 35 | 50 | - | dB |
| I-F Input Impedance | $\mathrm{Z}_{2}$ |  | - | 40 | - | k $\Omega$ |
| I-F Input Capacitance | $\mathrm{C}_{2}$ |  | - | 4.0 | - | pF |
| Quiescent Terminal Voltage | $V_{1}$ |  | - | 2.1 | - | V |
|  | $\mathrm{V}_{8}$ |  | - | 1.7 | - | V |
| Quiescent Supply Current | $\mathrm{I}_{\mathrm{cc}}$ |  | - | 10 | 15 | mA |

A-M MODE: $f_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{n}}=455 \mathrm{kHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, 30 \% \mathrm{~A}-\mathrm{M}$

| Sensitivity |  | Maximum Volume | - | 5.0 | 10 |
| :--- | :--- | :--- | :--- | :--- | :---: |
| Detector Recovered Audio | $\mathrm{V}_{0}$ |  | - | 150 | - |
| Overload Distortion |  | $80 \% \mathrm{~A}-\mathrm{M}$ | mV |  |  |
| Usable Sensitivity |  |  | - | 10 | - |
| Mixer Input Impedance | $\mathrm{Z}_{6}$ | See Note | mV |  |  |
| Mixer Input Capacitance | $\mathrm{C}_{6}$ |  | - | 4.5 | 35 |
| Mixer Output Impedance | $\mathrm{Z}_{4}$ |  | - | kV |  |
| Mixer Output Capacitance | $\mathrm{C}_{4}$ |  | - | 25 |  |
| I-F Input Impedance | $\mathrm{Z}_{2}$ |  | - | 3.5 | - |
| I-F Input Capacitance | $\mathrm{C}_{2}$ |  | - | pF |  |
| Quiescent Terminal Voltage | $\mathrm{V}_{1}$ |  | - | 100 | - |
|  | $\mathrm{V}_{8}$ |  | - | 1.3 | $\mathrm{k} \Omega$ |
| Quiescent Supply Current | $\mathrm{I}_{\mathrm{cc}}$ |  | - | - | pF |

NOTE: For optimum noise match, source impedance should be $2.5 \mathrm{k} \Omega$.

## TEST CIRCUIT



COIL WINDING INFORMATION


| T1 A-M First I-F 455 kHz | $\begin{aligned} & \mathrm{Qu}=120 \\ & \mathrm{~N} 1: \mathrm{N} 2: \mathrm{N} 3=15 \cdot 5: 2.8: 1 \\ & \mathrm{Ct}=180 \mathrm{pF} \end{aligned}$ | General Instrument Part No: EX 27835 | Toko Part No. RMC-2A7641A |
| :---: | :---: | :---: | :---: |
| T2 A-M Second I-F 455 kHz | $\begin{aligned} & \mathrm{Qu}=70 \\ & \mathrm{~N} 1: \mathrm{N} 2=2: 1 \\ & \mathrm{Ct}=430 \mathrm{pF} \end{aligned}$ | General Instrument Part No. EX 27836 | Toko Part No. RLE-4A7642G0 |
| T3 F-M Detector 10.7 MHz | $\begin{aligned} & \mathrm{Qu}=50 \\ & \mathrm{Ct}=100 \mathrm{pF} \end{aligned}$ | General Instrument Part No. EX 27640 | Toko Part No. BKAC-K3651HM |
| T4 F-M Detector 10.7 MHz | $\begin{aligned} & \mathrm{Qu}=50 \\ & \mathrm{Ct}=100 \mathrm{pF} \end{aligned}$ | General Instrument Part No. EX 27640 | Toko Part No. BKAC-K3651HM |
| L1 A-M Oscillator 1455 kHz | $\begin{aligned} & \mathrm{Qu}=50 \\ & \mathrm{~N}: \mathrm{N} 3=10.7: 1 \\ & \mathrm{Ct}=39 \mathrm{pF} \\ & \hline \end{aligned}$ | General Instrument Part No. EX 27641 | Toko Part No. RWO-6A7640BM |

# Device Classification and Design Considerations 

The A-M /F-M receiver system's operation can be kept within tighter performance limits by matching bias groupings and appropriate external resistors (R8 and R16). With proper matching of parts and lots, consistent device performance can be obtained. The groupings, shown in the table below, are based on A-M and F-M operation. There are three selections for each mode and nine possible combinations:

PIN 16 OUTPUT VOLTAGE, $\mathrm{V}_{16}$

| $*$ <br> A-M <br> Operation | Complete Part Number Including Suffix |  |  |
| :---: | :---: | :---: | :---: |
|  | F-M Operation |  |  |
|  | $2.20-2.65 \mathrm{~V}$ | $2.55-3.05 \mathrm{~V}$ | $2.95-3.40 \mathrm{~V}$ |
| $1.40-1.75 \mathrm{~V}$ | ULN-3804A-11 | ULN-3804A-21 | ULN-3804A-31 |
| $1.65-2.00 \mathrm{~V}$ | ULN-3804A-12 | ULN-3804A-22 | ULN-3804A-32 |
| $1.90-2.25 \mathrm{~V}$ | ULN-3804A-13 | ULN-3804A-23 | ULN-3804A-33 |

Sprague recommends that customers not specify particular selections except in unusual circumstances. All parts manufactured with the Sprague part number will be marked with the complete number, including the appropriate suffix. In addition, any one shipment to a customer will consist of a single selection (single suffix).

The first digit of the suffix (such as the ' 3 '" in " -31 '") applies to F-M performance. It indicates the F-M gain and pin 16 output voltage as functions of the pin 16 load resistance, as shown in the graph on the next page.

F-M circuit stability is inversely related to gain or sensitivity and is also affected by source and load impedances, decoupling, and printed wiring board layout. After an optimal F-M I-F gain is determined for a particular circuit design, the gain can be controlled with proper matching of the suffix and the pin 16 load.

## Design Considerations (Continued)

In addition, certain system designs derive the F-M tuner supply, tuner bias, or AFC voltage at pin 16 of Type ULN3804 A . As an example, if the tuner design requires 2.4 V at 2.0 mA (an equivalent R16 of 1200 ), Type ULN-3804A-1X is required. A -2 X or -3 X device can also be used by paralleling the equivalent $1200 \Omega$ tuner load with a fixed resistor to present an $830 \Omega$ load or a $520 \Omega$ load.

For AFC applications, note that as the frequency is increased, the $\mathrm{V}_{16}$ voltage will decrease. The amount of change is a function of load impedance, detector coil characteristics, and part grouping.

## TYPICAL F-M I-F GAIN CHARACTERISTICS



Stability is seldom a problem with A-M operation. However, large-signal overload can be held to typically 30 mV by matching the particular part group with an appropriate load resistor at pin 8. The A-M grouping is identified by the second digit of the part number suffix (such as the " 2 " in " -32 ").

$$
\begin{aligned}
& \text { For }-\mathrm{X} 1, \mathrm{R} 8 \text { should be an open circuit; } \\
& \text { for }-\mathrm{X} 2, \mathrm{R} 8 \text { should be } 47 \mathrm{k} \Omega \text {; } \\
& \text { for }-\mathrm{X} 3, \mathrm{R} 8 \text { should be } 33 \mathrm{k} \Omega
\end{aligned}
$$

Additional loading may raise the overload point slightly, but AGC and sensitivity will be compromised. For any fixed value of R8, the -X3 parts will exhibit slightly higher A-M gain, the -X1 parts slightly lower A-M gain.


## ULN-3809A PHASE-LOCKED LOOP STEREO DECODER

## FEATURES

- Unity Voltage Gain
- $I^{2} L$ and Ion Implant Technology
- Wide Dynamic Range
- Low Distortion
- Excellent Channel Separation
- No Tuning Coils
- Automatic Stereo/Mono Switching
- Stereo Indicator Lamp Driver
- Direct Replacement for MC1309
- 14-Pin Dual In-Line Plastic Package

SPRAGUE Type ULN-3809A phase-locked loop decoder demodulates standard composite F-M stereo input signals within the range of 0.25 to 1.7 Vpp without the use of tuning coils.

Integrated circuit design allows tuning with a single resistive adjustment. The decoder automatically switches between stereo and monaural operation by detection and evaluation of the $19-\mathrm{kHz}$ pilot carrier signal.


Type ULN-3809A exhibits 35 dB suppression of the $19-\mathrm{kHz}$ pilot and 45 dB rejection of the regenerated $38-\mathrm{kHz}$ subcarrier at demodulator output terminals. Stereo channel separation is typically 47 dB . With a composite input signal of 850 mV , total harmonic distortion for the unit is typically $0.06 \%$.

Type ULN-3809A is designed to work within a range of supply voltages from 4.5 to 16 V .


## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage, $\mathrm{V}_{\text {cc }}$ | 16 V |
| :---: | :---: |
| Nominal Lamp Current, I ImM | 50 mA |
| Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ | 670 mW* |
| Operating Temperature Range, $T_{A}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage, Temperature Range, $\mathrm{T}_{\mathrm{S}}$ | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{Cc}}=9.0 \mathrm{~V}$,
$V_{\text {in }}=1.7 \mathrm{Vpp}, \mathrm{f}_{\mathrm{m}}=1.0 \mathrm{kHz}$ (L or R only), Pilot Level $=10 \%$ unless otherwise specified

| Characteristic | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. | Units |
| Max. Standard Composite Input Signal | $\mathrm{V}_{\mathrm{cc}}=6.0 \mathrm{~V}, 0.5 \%$ THD | 0.85 | 1.7 | - | Vpp |
|  | $\mathrm{V}_{\text {cc }}=9.0 \mathrm{~V}, 0.5 \%$ THD | 1.7 | 2.1 | - | Vpp |
| Max. Monaural Input Signal | $\mathrm{V}_{\mathrm{cc}}=6.0 \mathrm{~V}, 1.0 \%$ THD | 0.85 | 1.7 | - | Vpp |
|  | $\mathrm{V}_{\text {cc }}=9.0 \mathrm{~V}, 1.0 \%$ THD | 1.7 | 2.2 | - | Vpp |
| Input Impedance |  | 15 | 30 | - | k $\Omega$ |
| Stereo Channel Separation | $\mathrm{f}=100 \mathrm{~Hz}$ | - | 45 | - | dB |
|  | $\mathrm{f}=1.0 \mathrm{kHz}$ | 30 | 47 | - | dB |
|  | $\mathrm{f}=10 \mathrm{kHz}$ | - | 40 | - | dB |
| Monaural Gain |  | 0.6 | 0.9 | - | V/V |
| Channel Balance |  | - | 0 | 1.0 | dB |
| Total Harmonic Distortion | Stereo, $\mathrm{V}_{\text {in }}=850 \mathrm{mVpp}$ | - | 0.06 | - | \% |
|  | Mono, $\mathrm{V}_{\text {in }}=850 \mathrm{mVpp}$ | - | 0.08 | - | \% |
| Ultrasonic Frequency Rejection | 19 kHz | - | 35 | - | dB |
|  | 38 kHz | - | 45 | - | dB |
| SCA Rejection |  | - | 75 | - | dB |
| Stereo Switch Level | Lamp ON | - | 9.0 | 12 | mV |
|  | Lamp OFF | 2.0 | 4.5 | - | mV |
| Mono/Stereo Switch Transient | No Lamp | - | 0 | - | mV |
| Capture Range | Pilot $=60 \mathrm{mVrms}$ | - | 7.0 | - | \% |
| Supply Current |  | - | 11 | - | mA |

NOTE: THD and channel separation are measured after a bandpass filter ( 200 Hz to 10 kHz ).

## APPLICATIONS INFORMATION



TEST CIRCUIT AND TYPICAL APPLICATION

1. If relaxed performance is acceptable, the external circuit can be simplified by decreasing the value of $C_{1}$ (reduces separation at low frequencies), decreasing the values of $\mathrm{C}_{4}$ and $\mathrm{R}_{3}$ while eliminat-
ing $C_{5}$, and decreasing the value of $C_{6}$ while increasing the values of $R_{4}$ and $R_{5}$ (increases capture-range and beat-note distortion).
2. Typical I-F amplifier frequency response restricts channel separation to about 32 dB . This restriction can be counteracted by the network shown below. Exact circuit values will be determined by the I-F amplifier design.


DWG. No. A-10.656
3. To manually disable the stereo decoder, ground pin 8 and connect pin 14 to ground through a resistance of $3.3 \mathrm{k} \Omega$.
4. Capacitor $\mathrm{C}_{6}$ should be temperature-stable (NPO).

MINIMUM-COST APPLICATION IN A-MF-M STEREO RADIO


## ULN-3810A <br> PHASE-LOCKED LOOP STEREO DECODER

## FEATURES

- No Tuning Coils Required
- $1^{2} L$ and Ion Implant Technology
- Single-Adjustment Tuning
- Automatic Stereo/Mono Switching
- Stereo Indicator Lamp Driver
- Excellent SCA Rejection
- Direct Replacement for TA7157, KB4409, CA1310, XR1310, LM1310, SN76115, MC1310 \& ULN-2110A
- 14-Pin Dual In-Line Plastic Package

R
ECOVERY of left- and right-channel audio from the standard F-M composite signal by this phase-locked loop decoder yields stereo channel separation of 40 dB and total harmonic distortion of less than $0.3 \%$.

Type ULN-3810A is designed to operate over a supply voltage range of 6 to 16 V .


## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage, $\mathrm{V}_{\text {cc }}$ | V |
| :---: | :---: |
| Nominal Lamp Current, $\mathrm{I}_{\text {IAM }}$ | 75 mA |
| Package Power Dissipation, $\mathrm{P}_{0}$ | 670 mW* |
| Operating Temperature Range, $T_{A}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage, Temperature Range, $\mathrm{T}_{\mathrm{s}}$ | to $+150^{\circ} \mathrm{C}$ |

${ }^{*}$ Derate at the rate of $8.3 \mathrm{~mW} / \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.


ELECTRICAL CHARACTERISTICS at $T_{A}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+12 \mathrm{~V}$,
$V_{\text {in }}=560 \mathrm{mVrms}\left(2.8 \mathrm{~V}_{\mathrm{pp}}\right), \mathrm{f}_{\mathrm{m}}=1.0 \mathrm{kHz}$ (L or R only),
Pilot Level $=\mathbf{1 0 0} \mathbf{m V r m s}(\mathbf{1 0 \%})$ unless otherwise specified

| Characteristic | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. | Units |
| Max. Standard Composite Input Signal | THD $=0.5 \%$ | 2.8 | - | - | $\mathrm{V}_{\mathrm{pp}}$ |
| Max. Monaural Input Signal | THD $=1.0 \%$ | 2.8 | - | - | $\mathrm{V}_{\mathrm{pp}}$ |
| Input Impedance | Pin 2 | 20 | 25 | - | k $\Omega$ |
| Stereo Channel Separation |  | 30 | 40 | - | dB |
| Audio Output Voltage | Desired Channel | - | 485 | - | mVrms |
| Monaural Channel Balance | Pilot Level $=0 \mathrm{~V}$ | - | - | 1.5 | dB |
| Total Harmonic Distortion |  | - | $<0.3$ | - | \% |
| Ultrasonic Freqency Rejection | 19 kHz | - | 34.4 | - | dB |
|  | 38 kHz | - | 45 | - | dB |
| SCA Rejection | 67 kHz , No Modulation, Measure 9 kHz Beat | - | 75 | - | dB |
| Stereo Switch Level | Pilot Only, Lamp ON | - | 18 | 25 | mVrms |
|  | Pilot Only, Lamp OFF | 5.0 | 9.0 | - | mVrms |
| Capture Range | Permissible Tuning Error | - | 3.5 | - | \% |
| Supply Current | Lamp OFF | - | 12 | 22 | mA |

## APPLICATION INFORMATION



## TEST CIRCUIT AND TYPICAL APPLICATION

1. If relaxed performance is acceptable, the external circuit can be simplified by decreasing the value of $\mathrm{C}_{1}$ (reduces separation at low frequencies), decreasing the values of $C_{4}$ and $R_{3}$ while eliminating $C_{5}$,
and decreasing the value of $\mathrm{C}_{6}$ while increasing the values of $\mathrm{R}_{4}$ and $\mathrm{R}_{5}$ (increases capture-range and beat-note distortion).
2. Typical I-F amplifier frequency response restricts channel separation to about 32 dB . This restriction can be counteracted by the network shown below. Exact circuit values will be determined by the I-F amplifier design.

3. To manually disable the stereo decoder, ground pin 8 and connect pin 14 to ground through a resistance of $3.3 \mathrm{k} \Omega$.
4. Capacitor $\mathrm{C}_{6}$ should be temperature stable (NPO).


# ULX-3840A HIGH-PERFORMANCE A-M/F-M SIGNAL PROCESSING SYSTEM 

## FEATURES

- $12 \mu \mathrm{~V}$ Limiting Threshold
- Tuning-Error/Level Muting
- Meter Drive
- Balanced A-M Mixer
- $5 \mu \mathrm{~V}$ A-M Sensitivity
- D-C Mode Switching
- Internal Voltage Regulator
- Meets Dolby Noise Requirements
- 20 -Pin Dual In-Line Plastic Package

IDEALLY SUITED FOR TOP-NOTCH A-M/ F-M radios, Type ULX-3840A provides sophisticated operating features highly desired by the modern consumer at a price that allows it to be used in budget receivers.
A combination of inter-station (signal-level) muting and off-channel (tuning-error) muting is useful in signal-seeking or scanning applications. The circuit design eliminates annoying lowfrequency thump and noise tail when the system is manually tuned through a strong signal.

Outputs are available for directly driving a peak reading meter and a zero-tune meter. The peak meter output also is useful in controlling external system functions, such as blending multiplexers, stereo decoders, noise blankers, or in providing positive-going AGC for the tuner.

All standard F-M I-F functions and all A-M functions are provided by this single monolithic integrated circuit. The low-level audio output stages have been designed to meet stringent Dolby ${ }^{\circ}$ noise requirements.


The A-M mixer is a balanced low-current analog multiplier with very-low local oscillator feedthrough, high I-F rejection, and freedom from spurious responses. This mixer can be used in the long-wave, medium-wave, and shortwave bands.

A fully-balanced, four-stage differential I-F amplifier gives maximum gain with freedom from common mode signals. It is used in both the A-M and F-M modes of operation with approximately 82 dB of gain in the F-M mode and controlled AGC gain of 26 dB in the A-M mode.

The detector in the F-M mode is a fourquadrant analog mutliplier operating in the high-level injection mode. Common mode signals are rejected through the use of balanced current-mirror outputs.

In the A-M mode of operation, the detector is configured as a balanced peak detector for low audio distortion. A-M gain control is achieved with AVC applied to the I-F and delayed AVC applied to the mixer.
(Continued next page)

[^39][^40] writing by authorized Sprague personnel.

Switching between modes can be accomplished with a simple single-pole d-c switch. The common low-level audio output can be used to drive an audio power amplifier (Type ULN3703Z) or stereo decoder (Type ULN-3810A).

Internal voltage regulators and bias supplies assure premium performance despite variations in external supply voltage ( 8.5 to 16 V ) or temperature $\left(-20^{\circ} \mathrm{C}\right.$ to $\left.+85^{\circ} \mathrm{C}\right)$. Separate ground leads minimize decoupling problems.

## ABSOLUTE MAXIMUM RATINGS

$$
\begin{aligned}
& \text { Mute Input Voltage, } V_{8}
\end{aligned}
$$

"Derated at $9.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$

FUNCTIONAL BLOCK DIAGRAM


ELECTRICAL CHARACTERISTICS at $T_{A}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=12.8 \mathrm{~V}$

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Operating Voltage Range | $V_{c c}$ | 10 |  | 8.5 | 12.8 | 16 | V |
| Audio Output Voltage | $V_{6}$ | 6 | No Signal | - | 5.8 | - | $V$ |
| Regulator Output Voltage | $V_{\text {REG }}$ | 13 | No Signal | - | 6.4 | - | $V$ |
| Avail. Reg. Output Current | ReG | 13 |  | 2.0 | - | - | mA |

F-M MODE: $f_{0}=10.7 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm 75 \mathrm{kHz}, \mathrm{V}_{\mathrm{in}}=10 \mathrm{mVrms}$, Non-Muted (unless otherwise specified)

| Input Limiting Threshold | $\mathrm{V}_{\text {IH }}$ | 2 |  | - | 12 | 25 | $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Recovered Audio | $V_{\text {out }}$ | 6 |  | 350 | 425 | 600 | mV |
| Output Distortion | THD | 6 |  | - | 0.3 | 0.7 | \% |
| Output Noise | $\mathrm{S}+\mathrm{N} / \mathrm{N}$ | 6 |  | 74 | 80 | - | dB |
| A-M Rejection | AMR | 12 | See Note | 40 | $>55$ | - | dB |
| Mute | $\Delta V_{\text {out }}$ | 6 | $\mathrm{V}_{\mathrm{in}}=100 \mu \mathrm{~V}$, Max. Mute | - | - | -1.0 | dB |
|  |  |  | $\mathrm{V}_{\text {in }}=5.0 \mu \mathrm{~V}$, Max. Mute | -45 | - | - | dB |
| AFC Output Voltage | $V_{\text {afc }}$ | 7 |  | 220 | - | 600 | mV |
| I-F Input Voltage | $V_{2}$ | 2 | No Signal | - | 3.5 | - | V |
| Mute Output Voltage | $\mathrm{V}_{14}$ | 14 | No Signal | 3.6 | 4.2 | - | $\checkmark$ |
| Mute Output Current | $\mathrm{I}_{14}$ | 14 | No Signal | 0.5 | - | - | mA |
| Supply Current | 1 Cc |  | No Signal | - | 23 | 35 | mA |

A-M MODE: $f_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{if}}=455 \mathrm{kHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, 30 \% \mathrm{~A}-\mathrm{M}, \mathrm{V}_{\mathrm{in}}=1.0 \mathrm{mVrms}$ (unless otherwise specified)

| Sensitivity | $V_{\text {in }}$ | 18 | $\mathrm{V}_{\text {out }}=50 \mathrm{mVrms}$ | - | 5.0 | 8.5 | $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Usable Sensitivity |  | 18 | $20 \mathrm{~dB} \mathrm{~S}+\mathrm{N} / \mathrm{N}$ | - | 6.0 | - | $\mu \mathrm{V}$ |
| Recovered Audio | $V_{\text {out }}$ | 6 | 80\% A-M | 250 | 325 | 600 | mV |
| Input Overload | $V_{\text {in }}$ | 18 | 80\% A-M, THD $=10 \%$ | 25 | 50 | - | mV |
| A-M Decoupling Voltage | $V_{1}$ | 1 | No Signal | - | 1.0 | - | V |
| I-F Input Voltage | $V_{2}$ | 2 | No Signal | - | 3.7 | - | V |
| Mute Output Voltage | $\mathrm{V}_{14}$ | 14 | No Signal | - | - | 0.5 | V |
| Peak Meter | $\mathrm{V}_{15}$ | 15 | No Signal | - | $<0.5$ | - | V |
|  |  |  | $\mathrm{V}_{\text {in }}=10 \mathrm{mV}$ | - | 3.0 | - | V |
| A-M Input Voltage | $V_{17}$ | 17 | No Signal | 1.6 | 1.8 | 2.1 | V |
| Supply Current | $\mathrm{I}_{\text {c }}$ |  | No Signal | - | 16 | 30 | mA |

Note: Amplitude Modulation Rejection is specified as $20 \log \frac{V_{\text {out }} \text { for } 100 \% \text { F-M } V_{\text {in }}}{V_{\text {out }} \text { for } 30 \% \text { A-M } V_{\text {in }}}$

SMALL-SIGNAL A-C CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

|  |  | Test |  | Limits |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Characteristic | Symbol | Pin |  | Test Conditions |  | Min. |
| I-F Input Capacitance | $\mathrm{C}_{2}$ | 2 |  | - | 6.0 | - | pF |
| I-F Output Resistance | $\mathrm{R}_{12}$ | 12 |  | - | 250 | - | $\mathrm{k} \Omega$ |
| I-F Output Capacitance | $\mathrm{C}_{12}$ | 12 |  | - | 2.5 | - | pF |
| Audio Output Impedance | $\mathrm{Z}_{6}$ | 6 |  | - | 350 | - | $\mathrm{k} \Omega$ |

F-M MODE: $f_{0}=10.7 \mathbf{M H z}$

| I-F Input Resistance | $\mathrm{R}_{2}$ | 2 |  | -10 | - | $\mathrm{k} \Omega$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| I-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ | $2-12$ |  | - | 8.0 | - |
| Detector Input Resistance | $\mathrm{R}_{11}$ | 11 |  | - | 100 | - |
| Detector Input Capacitance | $\mathrm{C}_{11}$ | 11 |  | - | 1.5 | - |

A-M MODE: $f_{0}=1 \mathrm{MHz}, \mathrm{f}_{\mathrm{if}}=455 \mathrm{kHz}$

| A-M Input Resistance | $\mathrm{R}_{18}$ | 18 |  | - | 5.0 | - | $\mathrm{k} \Omega$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A-M Input Capacitance | $\mathrm{C}_{18}$ | 18 |  | - | 20 | - | pF |
| Mixer Transconductance | $\mathrm{g}_{\mathrm{m}}$ | $18-19$ |  | - | 15 | - | $\mathrm{mmh} 0^{*}$ |
| Mixer Output Resistance | $\mathrm{R}_{19}$ | 19 |  | - | 500 | - | $\mathrm{k} \Omega$ |
| Mixer Output Capacitance | $\mathrm{C}_{19}$ | 19 |  | - | 5.0 | - | pF |
| I-F Input Resistance | $\mathrm{R}_{2}$ | 2 |  | - | 15 | - | $\mathrm{k} \Omega$ |
| I-F Transconductance | $\mathrm{g}_{\mathrm{m}}$ | $2-12$ |  | - | 160 | - | $\mathrm{mmho}^{* *}$ |
| Detector Input Resistance | $\mathrm{R}_{11}$ | 11 |  | - | 250 | - | $\mathrm{k} \Omega$ |
| Detector Input Capacitance | $\mathrm{C}_{11}$ | 11 |  | - | 1.0 | - | pF |

*The International Electrotechnical Commission recommends the use of siemens ( $S$ ) as the standard international unit of conductance, admittance and susceptance.

F-M TUNING-ERROR DETECTOR RESPONSE


## TEST CIRCUIT


*In application, $R=0 \Omega, C=0.008 \mu \mathrm{~F}$ for $50 \mu \mathrm{~s}$ de-emphasis (Europe) or $0.012 \mu \mathrm{~F}$ for $75 \mu \mathrm{~s}$ de-emphasis (U.S.A.)

Filter Assembly:
Toko Part No. CFU455C-82BR


COIL WINDING INFORMATION


| T1 A-M I-F | $\mathrm{Qu}=45$ | General Instrument | Toko Part No. |
| :---: | :--- | :--- | :--- |
| 455 kHz | $\mathrm{Ct}=1000 \mathrm{pF}$ | Part No. EX 27765 | RXN-6A6909HM |
| T2 F-M Detector | $\mathrm{Qu}=60$ | General Instrument | Toko Part No. |
| 10.7 MHz | $\mathrm{Ct}=82 \mathrm{pF}$ | Part No. EX 27975 | TKAC-170442 |
| L1 A-M Oscillator | $\mathrm{Qu}=50$ | General Instrument | Toko Part No. |
| 1455 kHz | $\mathrm{N}: \mathrm{N} 2=11: 1$ | Part No. EX 27641 | RW0-6A7640BM |
|  | $\mathrm{Ct}=39 \mathrm{pF}$ |  |  |
| L2 F-M Detector | $\mathrm{L}=18 \mu \mathrm{H}$ | Coilcraft |  |
| 10.7 MHz | $\mathrm{Qu}=55 @ 2.5 \mathrm{MHz}$ | Type V |  |

A-M CONTROL VOLTAGES AS FUNCTIONS OF INPUT SIGNAL


F-M CONTROL VOLTAGES AS FUNCTIONS OF INPUT SIGNAL


## A-M CHARACTERISTICS AS FUNCTIONS OF INPUT SIGNAL



F-M CHARACTERISTICS AS FUNCTIONS OF INPUT SIGNAL


# ULN-3859A <br> F-M COMMUNICATIONS I-F SYSTEM 

## FEATURES

- Dual Conversion
- Low Current Drain
- Wide Operating Voltage Range
- High Sensitivity
- Replaces MC3359P
- 18-Pin Dual In-Line Plastic Package


THIS low-power, narrow-band F-M I-F system provides the second converter, second I-F, demodulator and squelch circuitry for communications and scanning receivers.

Type ULN-3859A's double-balanced mixer permits low-noise operation while eliminating spurious responses, effectively rejecting tweet and I-F feedthrough, and reducing local oscillator radiation. The mixer's high input impedance matches popular 10.7 MHz crystal filters while its output impedance matches most 455 kHz ceramic filters. Although designed for use with a 10.7 MHz first I-F and a 455 kHz second I-F, the mixer operates at other R-F or I-F input frequencies through 30 MHz .

A multi-stage 1 MHz differential amplifier/ limiter following the second I-F filter operates as
a high gain stage with excellent common-mode rejection.

Audio is recovered by a quadrature F-M detector that requires only a single low-cost tuned circuit.

Type ULN-3859A has both a low-impedance emitter-follower audio output and an AFC output. Few external components are needed for operation with noise-activated or tone squelch.

This communications I-F system meets the stability requirements of many automotive applications, and also meets the low-power demands of portable radio design. Internal voltage regulators and bias supplies ensure stable performance despite variations in external supply voltage ( 4 to 9 V ) or temperature $\left(-20^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$ ).

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $V_{C 0}$ ..... 12 V
Mixer Terminal Voltage, $\mathrm{V}_{\text {in }}$ ..... 1.0 V
Mute Terminal Voltage Range, $\mathrm{V}_{16}$ ..... -0.5 V to +12 V
Operating Temperature Range, $T_{A}$ $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=8.0 \mathrm{~V}$,

$f_{0}=10.7 \mathrm{MHz}, f_{m}=1.0 \mathrm{kHz}, \mathrm{f}_{\mathrm{d}}= \pm 3.0 \mathrm{kHz}$ (unless otherwise noted)

| Characteristic | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Operating Voltage Range | 4 |  | 4.0 | 8.0 | 9.0 | $V$ |
| Quiescent Supply Current | 4 | $\mathrm{V}_{14}=0$, Mute OFF | - | 3.0 | 6.0 | mA |
|  |  | $\mathrm{V}_{14} \geq 0.7 \mathrm{~V}$, Mute ON | - | 4.0 | 7.0 | mA |
| Input Limiting Threshold | 18 | -3 dB Limiting | - | 2.0 | 6.0 | $\mu \mathrm{V}$ |
| Mixer Conversion Gain | 3 | See Note 1, Next Page | - | 24 | - | dB |
| Mixer Input Resistance | 18 |  | - | 3.6 | - | k $\Omega$ |
| Mixer Input Capacitance | 18 | See Note 2, Next Page | - | 2.2 | - | pF |
| Mixer Output Impedance | 3 |  | - | 1.8 | - | k $\Omega$ |
| Limiter Input Impedance | 5 |  | - | 1.8 | - | k $\Omega$ |
| Quiescent D-C Output Voltage | 10 | $\mathrm{V}_{\text {in }}=0$ | 2.4 | 3.6 | 4.4 | V |
| Audio Output Impedance | 10 |  | - | 500 | - | $\Omega$ |
| Recovered Audio Output | 10 | $\mathrm{V}_{\mathrm{in}}=3.0 \mathrm{mV}$ | 450 | 700 | - | mV rms |
| Amplifier Gain | 13 | $\mathrm{f}=4.0 \mathrm{kHz}, \mathrm{V}_{\text {in }}=5.0 \mathrm{mV}$ | $40^{\circ}$ | 53 | - | dB |
| Quiescent D-C Output Voltage | 13 | $\mathrm{V}_{\text {in }}=0$ | - | 1.7 | - | V |
| Mute Switch Resistance | 16 | $\mathrm{I}_{16}=2.5 \mathrm{~mA}, \mathrm{~V}_{14} \geq 0.7 \mathrm{~V}$ | - | 4.0 | 10 | $\Omega$ |
| Scan Source Current | 15 | $\mathrm{V}_{14}=\mathrm{V}_{15}=0$, Mute OFF | 2.0 | 4.0 | - | mA |

## TEST CIRCUIT



## APPLICATION INFORMATION

1. In a typical application, with a $3.6 \mathrm{k} \Omega$ crystal filter source, Type ULN-3859A will give 23 dB conversion gain.
2. Because crystal filters are extremely sensitive to reactive loading, radio designers frequently have added a coil and/or capacitor at pin 18 to cancel the input reactance component. This practice is not required with Type ULN-3859A, since its input is designed to match typical 10.7 MHz crystal filters. However, if an external reactive component is used, it is important to adjust it for optimal passband shape and not simply to peak it for maximum sensitivity.
3. Pin 11 provides AFC. If AFC is not required, pin 11 should be grounded, or tied to pin 9 to double the available recovered audio.
4. Pin 10 may require an external resistor ( $2 \mathrm{k} \Omega$ minimum) to ground to prevent audio rectification with some capacitive loads.

## ULN-3889A/TDA3 189 I-F SYSTEM FOR F-M RECEIVER APPLICATIONS

## FEATURES

- Tuning-Error Muting
- Improved A-M Rejection
- Signal-Level Muting
- Direct Tuning-Meter Drives
- Single Coil Tuning
- Isolated AFC Output
- Internal Voltage Regulator
- Programmable AGC Output
- Direct Replacement for CA3189E
- 16-Pin Dual In-Line Plastic Package

EQUIPPED WITH FEATURES such as programmable delayed AGC for the R-F tuner, an AFC drive circuit, outputs for tuning meters and stereo switching logic, signal-level and tuning-error muting, Type ULN-3889A is a comprehensive F-M I-F system.

This monolithic integrated circuit excels in signal-seeking and scanning applications. False triggers on adjacent channels and strong mistuned signals are eliminated by its off-tune muting, which exhibits a greater voltage change than that of commonly used signal-level muting. In standard F-M radio applications, tuning-error muting eliminates the low-frequency thump and the noise tail associated with tuning through a strong signal.

Three balanced stages of I-F amplification and limiting, each with its own level detector, and a double-balanced quadrature detector give the system high gain and effective common-mode rejection.

In automotive and communications applications,

low-level injection (with the mute detector disabled) permits operation of the F-M detector as an analog multiplier. This mode of operation dramatically reduces off-station noise without sacrificing gain.
The I-F system's audio amplifier, with muting or squelch, can directly drive an audio power amplifier (such as Sprague Type ULN-3703Z) or a stereo decoder (such as Sprague Type ULN-3810A).

An internal voltage regulator and bias supply ensures reliable operation with supply variation between 8.5 and 16 V and temperature variations between $-20^{\circ} \mathrm{C}$ and $+85^{\circ} \mathrm{C}$.

## ABSOLUTE MAXIMUM RATINGS

[^41]
## FUNCTIONAL BLOCK DIAGRAM



STATIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{Cc}}=12 \mathrm{~V}$,
Figures 1 and 2A or Figures 1 and 2B, non-muted

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Supply Current | $\mathrm{I}_{\text {cre }}$ | 11 |  | 20 | 31 | 40 | mA |
| Terminal Voltage | $V_{1}$ | 1 |  | 1.2 | 1.9 | 2.4 | V |
|  | $V_{2}$ | 2 |  | 1.2 | 1.9 | 2.4 | V |
|  | $V_{3}$ | 3 |  | 1.2 | 1.9 | 2.4 | V |
|  | $V_{4}$ | 4 |  | reference |  |  |  |
|  | $V_{6}$ | 6 |  | - | 5.9 | - | V |
|  | $V_{10}$ | 10 |  | 5.4 | 5.9 | 6.4 | V |
|  | $V_{11}$ | 11 |  | - | 12 | - | V |
|  | $V_{12}$ | 12 |  | 4.5 | 5.3 | 7.0 | V |
|  | $V_{14}$ | 14 |  |  | feren |  |  |

DYNAMIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{c c}=12 \mathrm{~V}$,
Figures 1 and 2A or Figures 1 and 2B non-muted, $\mathrm{V}_{\mathrm{in}}=100 \mathrm{mV}$ rms,
$f_{0}=10.7 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm 75 \mathrm{kHz}$ (unless otherwise noted)

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Input Limiting Threshold | $\mathrm{V}_{\text {TH }}$ | 1 |  | - | 15 | 25 | $\mu \mathrm{V}$ |
| Recovered Audio Output | $V_{\text {out }}$ | 6 |  | 325 | 500 | 650 | mV |
| Output Distortion (See Note) | THD | 6 | Figures 1 \& 2A | - | 0.5 | 1.0 | \% |
|  |  |  | Figures 1 \& 2B | - | 0.1 | - | \% |
| A-M Rejection | AMR | 6 | See Note | 45 | 65 | - | dB |
| Noise Level | S+N/N | 6 |  | 65 | 72 | - | dB |
| Meter Drive Voltage | $V_{13}$ | 13 | $\mathrm{V}_{\text {in }}=0 \mathrm{mV}$ ms | - | 0.1 | 0.5 | V |
|  |  |  | $\mathrm{V}_{\text {in }}=100 \mathrm{mV}_{\text {rms }}$ | - | 3.5 | - | V |
| AGC Output Voltage | $\mathrm{V}_{15}$ | 15 | $V_{16}=1.0 \mathrm{~V}$ | 7.5 | 9.5 | 11 | V |
|  |  |  | $V_{16}=1.6 \mathrm{~V}$ | - | 0.1 | 0.3 | V |
| Level Mute | $\Delta V_{\text {out }}$ | 6 | $\mathrm{V}_{\text {in }}=1.0 \mathrm{mV}$ rms , Max. Mute | - | 0 | -1.0 | dB |
|  |  |  | $\mathrm{V}_{\mathrm{in}}=\mathrm{V}_{\text {TH }}-6 \mathrm{~dB}$, Max. Mute | -45 | -65 | - | dB |
| On-Channel Step | $\mathrm{V}_{12}$ | 12 | $\mathrm{f}_{0}=10.7 \mathrm{MHz}$ | - | 0 | 1.0 | V |
|  |  |  | $\mathrm{f}_{0}=10.7 \pm 0.15 \mathrm{MHz}$ | - | 5.6 | - | V |
| R-F AGC Threshold | $\mathrm{V}_{16}$ | 16 | $\mathrm{V}_{15}=2.0 \mathrm{~V}$ | - | 1.25 | - | V |
| Mute Bandwidth | $\Delta f_{w}$ |  | $\mathrm{V}_{12}=2.0 \mathrm{~V}, \mathrm{f}_{\mathrm{m}}=0$, Figs. $1 \& 2 \mathrm{~A}$ | - | $\pm 40$ | - | kHz |

NOTES: Audio Distortion is primarily a function of the phase linearity characteristic of the detector tuned circuit.
Amplitude Modulation Rejection is specified as $20 \log \frac{V_{\text {out }} \text { for } 100 \% \mathrm{~F}-\mathrm{M} \mathrm{V}_{\text {in }}}{\mathrm{V}_{\text {out }} \text { for } 30 \% \mathrm{~A}-\mathrm{M} \mathrm{V}_{\text {in }}}$


Dwg. No. A-11,387
Figure 1
*Decoupling capacitors should be of the ceramic type with minimum inductance at the operating frequency.
${ }^{* *}$ Capacitor value is $0.01 \mu \mathrm{~F}$ for $50 \mu$ s de-emphasis (Europe) or $0.015 \mu \mathrm{~F}$ for $75 \mu \mathrm{~s}$ de-emphasis (U.S.A.).

## PHASE SHIFT NETWORKS



Figure 2A
L is selected to resonate with $C$ at 10.7 MHz and has an unloaded $Q$ of approximately 75 . R (approximately $3.9 \mathrm{k} \Omega$ ) is selected for a voltage across $L$ of 160 mV with an input signal of $100 \mu \mathrm{~V}$.


Figure 2B
L is selected to resonate with $C$ at 10.7 MHz and has an unloaded $Q$ of approximately $75 . R$ (approximately $8.2 \mathrm{k} \Omega$ ) is selected for a voltage across $L_{p}$ of 150 mV with an input signal of $100 \mu \mathrm{~V}$; KQ , or per cent of critical coupling (approximately $70 \%$ ), is adjusted for minimum output distortion.

## GENERAL DESIGN NOTES

1. The phase shift network is aligned by applying an F-M signal through a decoupling network to pin 1 and tuning for maximum recovered audio at pin 6.
2. A low-resistance path must be provided between pins 9 and 10 . No other biasing provisions are required.
3. A low-resistance path must be provided between pins 1 and 3 . No other biasing provisions are required.
4. Keep appropriate distance between the input (pin 1 and the input network) and the phase shift network (pins 8, 9, and 10, and the phase shift inductor).
5. If a high-impedance power supply is used (voltage dropping resistor), decouple pin 11 for the lowest audio frequency.
6. The level of recovered audio increases with higher values of loaded Q and higher values of resistance between pins 6 and 10. It decreases with lower values of loaded $Q$ and lower values of resistance between pins 6 and 10 .
7. Mute bandwidth decreases with higher values of loaded $Q$ and higher values of resistance between pins 7 and 10. It increases with lower values of loaded Q and lower values of resistance between pins 7 and 10 .

RECOVERED AUDIO
AND A-M REJECTION LEVELS AS FUNCTIONS OF I-F SIGNAL INPUT



F-M TUNING ERROR RESPONSE


NOTE: Outside the I-F filter passband, pin 12 voltage will be reduced as a function of system gain.
Dwg. No. A-11,382

## AFC OUTPUT

AS A FUNCTION OF FREQUENCY SHIFT


AGC AMPLIFIER RESPONSE


TUNING-ERROR MUTE THRESHOLD AS A FUNCTION OF LOAD RESISTANCE


Dwg. No. A-11,384


SCHEMATIC

## ULN-2204A A-M/F-M RECEIVER SYSTEM - TYPICAL APPLICATIONS AND OPERATION

## Introduction

Through the relatively short history of bipolar monolithic circuits, several revolutionary new circuits have been developed for $a-m / f-m$ receiver design. A. Bilotti pioneered the original monolithic f-m-quadrature detector/I-F gainblock in the form of the Sprague ULN-2111A.

Subsequent devices have included gain-control stages, output drivers, and voltage regulators. During this same period a-m integrated circuitry showed far less inspiration. Numerous a-m circuits were developed which in essence attempted to combine the active elements of a discrete bipolar a-m receiver in a monolithic circuit. To no surprise, the resulting chips were at best capable of performance no better than the parent discrete design, and with the uneconomical displacement of three discrete transistors with one integrated circuit. In addition to the a-m-only circuits and f-m-only circuits, a-m/f-m circuits were also attempted using the same design approaches used for the a-m-only circuit, that of combining an existing discrete receiver circuitry in a monolthic device. The results were much like the a-m only efforts, a bewildering collection of economically unattractive circuits of modest performance.

To achieve useful cost and performance objectives, the ULN-2204A was designed with careful attention to the cost and performance objectives of the modern portable and table model broadcast receiver. Concern for low external component count, low power consumption, wide supply voltage range, and versatility remained foremost as design objectives.

## Power Amplifier

To achieve the desired performance objectives of high power output and efficiency from a 2 to 12 V supply requires that the power amplifier be capable
of peak-to-peak voltage swings approaching the available supply. To meet these performance objectives a new power amplifier design was required having no more than one $\mathrm{V}_{\mathrm{BE}}$ of swing restriction.

As shown in Figure 1, the output stage is comprised of 2 NPN transistors (Q42 and Q49) plus a phase inverter (Q54). Quiescent operating current is set up by the current source (I).


Figure 1

Assuming $\mathrm{V}_{\mathrm{oq}}=\mathrm{V}_{\mathrm{CC} / 2}$ then the collector current of Q54 $=\mathrm{I}$, ignoring base currents, and if Q54 is matched to Q49 as is possible in a monolithic circuit, then the collector current of Q49 equals the collector current of Q54. The circuit in Figure 1 achieves an excellent voltage swing capability of $\mathrm{V}_{\mathrm{CC}}$ $-\mathrm{V}_{\mathrm{BE}}-2 \mathrm{~V}_{\mathrm{CE}}$ (SAT). This totally NPN configuration also has good freedom from the highfrequency problems that often occur with quasicomplementary composite NPN-PNP configurations.

Although the circuit in Figure 1 has been incorporated in production monolithic circuits in essentially the form shown, in practice it has unacceptable design restrictions. Since $I$ is also the base drive current for Q 42 , the ratio of available base drive current I to idling current is proportional to the ratio of the emitter areas of Q49 to Q54. For practical values of IQ54/IQ49, i.e. one, the circuit has a serious implementation problem; it requires three output transistors (Q42, Q49, and Q54).

To reduce the size of Q54, an additional transistor (Q48) is added to the circuit as shown in Figure 2. Transistor Q48 divides I by its beta +1 allowing Q54 to be reduced in area by a similar value. In the practical realization of the ULN-2204A, Q54 is chosen as $1 / 5$ the emitter area of Q49 with a typical beta for Q48 of 6 .


Figure 2

Figure 3 illustrates other refinements in the practical realization of the output circuit. The drive and idling current I is derived from a $\mathrm{V}_{\mathrm{CC}}$ dependent source allowing maximum drive under maximum supply conditions while affording reduced drive and associated current conservation under minimum supply conditions. In addition, the Q48 divider circuit is refined to reduce PNP beta dependence. Finally with the addition of an input emitter follower (Q53) and a local negative feedback loop (R36), the output is completed as it appears in the ULN-2204A.

The input stage of the power amplifier (Figure 4) is comprised of a PNP differential pair (Q44 and Q45) preceded by a PNP emitter follower (Q43) which allows $d-c$ referencing of the source signal to ground. This eliminates the need for an input coupling


Figure 3
capacitor. Overall negative feedback, set by the ratio of R33 to R32, is applied to the inverting input Q45 through an NPN emitter follower (Q46) which also provides d-c level shifting.


Figure 4
The $\mathrm{V}_{\mathrm{CC} / 2}$ output tracking is achieved by summing the current flow through R33 and R32, with the current through R41 "reflected off of ground". Thus $\mathrm{V}_{\mathrm{CC} / 2}$ tracking is maintained by the voltage drop across 2 resistors. This allows the current from R41 to be bypassed at Pin 10, thereby combining the ripple bypass capacitor with the audio feedback capacitor.

Figure 5 illustrates the complete power amplifier as realized in the ULN-2204A, including the external components. The remarkably-low external component count, (only two capacitors including the output coupling) reflects concern for simplicity in implementation, yet the device achieves excellent performance. Typical output power can be as high as 850 mW from a 9 volt supply and useful output power at supply voltages of as low as 2 volts, with minimum of distortion as the curves in Figure 6 illustrate.


Figure 6


Figure 5

## Receiver

The a-m signal is processed from the antenna to the detector output via the traditional blocks of mixer, I-F, and detector enclosed in a reverse A-G-C loop. However, closer examination reveals certain very important advantages that can be afforded only by the monolithic design.

The a-m mixer is a fully-balanced mixer based on a four-quadrant multiplier as shown in Figure 7. This affords rejection of both the oscillator and input signal as observed at the output. In addition, an analog multiplier is (as the name implies) a true linear device. Balanced operation of the mixer provides typically 25 dB of I-F rejection at the input, with a similar rejection of the associated noise passband. Also, the linear operation of the circuit affords good freedom from intermodulation product responses.

I-F gain is provided for both a-m and f-m by a common I-F amplifier (Figure 8) using "stacked" selectivity. In f-m operation the gain of stages 1, 2, 3 , and 4 (Q1 thru Q 8$)$ is set at typically 76 dB providing a typical limiting threshold of $40 \mu \mathrm{~V}$.

For a-m the gain is lowered by reducing stage current. This is accomplished by reducing the current applied to the I-F amplifier by the current source Q17. The fifth I-F stage (Q9 and Q10) is operated at maximum gain and current to provide full signal to the $a-m$ and $f-m$ detector.

## A-M/F-M Detector

The detector is also a combination circuit. It recovers a-m audio by peak detection and $\mathrm{f}-\mathrm{m}$ audio by phase discrimination.

The a-m signal from the I-F output appears at Pin 15 across $T_{2}$ as shown in Figure 9. The signal is applied to the base of Q18 and after phase inversion by $\mathrm{T}_{2}$ is applied also to the base of Q19. Full wave detection occurs at the emitter of Q18 and Q19, utilizing the on-chip junction capacity for integration. This requires only that the stage current be chosen at a low value (typically $1 \mu \mathrm{~A}$ ) to produce the desired integration.

The f-m detection process relies on the phase/frequency relationship of a tuned external circuit for demodulation. The device converts phase


Figure 7

## RADIO INTEGRATED CIRCUITS (Continued)

variation, as observed across the tuned network, to a proportional voltage. The basic phase detection process combines the positive-going portions of the quadrature and reference signals (Pin 14 and 15, respectively), and evaluating the duty cycle of the resulting waveform as shown in Figure 10. The combining action occurs at the emitters of Q18 and Q19 resulting in the waveform shown. Subsequent processing involves squaring up the signal in a limiter, comprised of Q24 and Q27, resulting in the constant-amplitude plus train which is also shown. This pulse train is then applied to a PNP gain stage which, owing to the PNP's low $f_{T}$ of typically 1 MHz , integrates the pulse train into an average d-c
voltage which appears at Pin 8 , the detector audio output. Figure 11 illustrates the complete $a-m / f-m$ detector of the ULN-2204A, including the external components.

To complete the circuit, the a-m stages also require A-G-C. This is implemented in the ULN2204 A by internally setting the I-F supply voltage (Pin 16) equal to the voltage at the detector audio output. As carrier appears, a corresponding reduction in the d-c voltage occurs at the audio output terminal and at Pin 16, where an external bypass capacitor removes audio from the A-G-C line and sets the time constant.


Figure 8


Figure 9


Figure 10


Figure 11

## Application

The primary application, but certainly not the only application, for the ULN-2204A is the broadcast band $\mathrm{a}-\mathrm{m} / \mathrm{f}-\mathrm{m}$ table or portable radio as illustrated in Figure 12.

## Power Amplifier

Selection of power supply voltage and speaker impedance allow the designer to choose audio power levels up to almost 1 watt as the curves in Figure 6 illustrated. No unique precautions are necessary when designing with the ULN-2204A power amplifier. The device is stable and short-circuit immune.

External component choice for the power amplifier involves only two capacitors; one for the speaker coupling and one for the feedback and ripple by-passing. The coupling capacitor value should be
selected to provide the desired low-frequency cutoff with the chosen speaker impedance. The feedback and ripple bypass capacitor at Pin 10 should be chosen for both low-frequency audio rolloff and supply ripple rejection.

Ripple rejection is not practical to calculate due to the large number of mechanisms involved. The 220 $\mu \mathrm{F}$ capacitor indicated in Figure 12 achieves typically 35 dB rejection.

The high gain of typically 43 dB and the high input impedance ( $200 \mathrm{k} \Omega$ ) of the power amplifier allow utilization of this stage for other applications such as ceramic cartridge phono amplifiers.

Typical ceramic phono cartridges develop approximately 400 mV . However, the recommended

## RADIO INTEGRATED CIRCUITS (Continued)

load impedance for the most economical cartridges is usually $1 \mathrm{M} \Omega$. This poses no problem with the $200 \mathrm{k} \Omega$ input impedance of the ULN-2204A since the cartridge manufacturer specifies the load impedance for full low-frequency response to less than 40 Hz . Decreasing the load impedance produces an increased low end cutoff frequency.
In a ULN-2204A based application employing a cost and space conscious loudspeaker, 40 Hz program material capability is not only unnecessary but undesirable, and therefore a mismatch of the cartridge to increase the lower cutoff frequency to a value more in keeping with the other components of the system is recommended.
The ULN-2204A audio amplifier stage has other input considerations to be taken into account for best results. The input is referenced to ground for internal biasing and must be provided with a d-c path to ground. A current of typically $0.1 \mu \mathrm{~A}$ flows from Pin 9 through the volume control producing an IR drop which is multiplied by the closed loop d-c gain of the amplifier (1), and appears as an error in output centering at Pin 12. This recommends a value of $200 \mathrm{k} \Omega$ or less for the volume control, with values of less than $100 \mathrm{k} \Omega$ preferred.
The selection of power amplifier load impedance involves more consideration than just the desired power output. Ideally an $8 \Omega$ speaker impedance would produce the highest power outputs for any one supply voltage as the curves in Figure 6 illustrated. However, operation with a $16 \Omega$ load can produce as much power as with an $8 \Omega$ load as is also shown in Figure 6. The higher impedance load will also furnish a significant reduction in harmonic distortion and improvement in overall repeatability in power output capacity. In applications which allow the selection of the power supply voltage it is therefore recommended that a $16 \Omega$ load impedance be utilized in applications up to 0.75 watt. For applications having fixed power supply values, i.e. batteries, device selections can be had that produce the maximum power level into $8 \Omega$.

## Receiver Section - F-M

The f-m intermediate frequency input transformer, comprised of $T_{5}$ and $T_{6}$, provides both selectivity and coupling. $\mathrm{T}_{5}$ should present a source impedance to the device of approximately $500 \Omega$ for optimal stability. $\mathrm{T}_{6}$, the primary, is governed primarily by the characteristics of the tuner head feeding it, and should be selected for those considerations. $\mathrm{T}_{5}$ and $\mathrm{T}_{6}$ comprise a double tuned section which for monaural f-m should have a bandwidth of 150 kHz .

The ULN-2204A also provides a regulated and decoupled d-c bias voltage to be used as the $\mathrm{V}_{\mathrm{CC}}$ supply for the tuner head. This bias voltage is obtained at Pin 16 and provides typically 2.5 mA . The current drain loads Pin 16 significantly and must appear for Pin 16 to operate at the correct voltage of 2.2 V . The voltage at Pin 16 determines the gain of the f-m intermediate frequency with higher values producing increased gain. The voltage at Pin 16 also varies with the voltage at Pin 8 (the detector output voltage), and therefore applies some A-F-C to the tuner head through the oscillators' $\mathrm{V}_{\mathrm{CC}}$ supply.

As described earlier, the f-m detector is a phase detector which detects the phase shift of an external network appearing between Pin 14 and Pin 15. The preferred network is a double-tuned transformer as shown in Figure 10. This network is selected to provide the correct recovered audio and minimum distortion by choosing the loaded and coupled "Q's. In Figure 12, $\mathrm{T}_{3}$ (the primary) and $\mathrm{T}_{4}$ (the secondary) are loaded by resistors of $2.2 \mathrm{k} \Omega$ and $4.7 \mathrm{k} \Omega$, respectively, and top coupled by a 4.7 pF capacitor giving an S curve peak to peak separation of 400 kHz . Coupling factor $(\mathrm{Qk})$ is slightly greater than 1 to improve harmonic distortion. The bandwidth has been selected to place the carrier of an adjacent channel interfering station (standard f-m broadcasting) on the peaks of the $S$ curve, thereby improving selectivity. Using the circuitry shown, a typical recovered audio value of 250 millivolts at Pin 8 and total harmonic distortion value of 0.7 percent are achieved with 75 kHz deviation. It should be noted that the network, particularly the coupling capacitor value, is affected by layout and may require optimization for a particular application. Extremely high values of coupling factor should be avoided as this produces an undesirable voltage gain from Pin 15 to Pin 14 which manifests itself as $S$ curve inbalance at low signal levels.

The f-m de-emphasis is formed by the $0.01 \mu \mathrm{~F}$ capacitor connected at Pin 8 with an internal $7.5 \mathrm{k} \Omega$ resistor.

## Receiver Section - A-M

The a-m section requires two external coils for I-F matching and selectivity, plus the local oscillator coil. The a-m detector transformer ( $\mathrm{T}_{2}$ ) and mixer load coil ( $\mathrm{T}_{1}$ ) are stacked with the corresponding $\mathrm{f}-\mathrm{m}$ components to form the composite. The selection of bandwidth for the two-coil system shown in Figure 12 is restricted primarily by the practical coil Qs available. The unloaded Q of the first transformer ( $\mathrm{T}_{1}$ ) being selected as 120 and loaded to ap-


## COIL WINDING INFORMATION

| T1 | A-M First I-F 455 kHz | $\begin{aligned} & \mathrm{Qu}=120 \\ & \mathrm{~N} 1: \mathrm{N} 2: \mathrm{N} 3=15 \cdot 5: 2.8: 1 \\ & \mathrm{Ct}=180 \mathrm{pF} \end{aligned}$ | General Instrument Part No. 27835 | Toko <br> 7MC-A4018A or RMC2A7641A |
| :---: | :---: | :---: | :---: | :---: |
| T2 | $\begin{aligned} & \text { A-M Second I-F } \\ & 455 \mathrm{kHz} \end{aligned}$ | $\begin{aligned} & \mathrm{Qu}=70 \\ & \mathrm{~N} 1: \mathrm{N} 2=2: 1 \\ & \mathrm{Ct}=430 \mathrm{pF} \end{aligned}$ | General Instrument Part No. 27836 | Toko 7B0-A4017BM or RLE4A7642G0 |
| T3 | F-M Detector 10.7 MHz | $\begin{aligned} & \mathrm{Qu}=50 \\ & \mathrm{Ct}=100 \mathrm{pF} \end{aligned}$ | General Instrument Part No. EX 27639 | Toko <br> BKAC-K3651HM |
| T4 | F-M Detector 10.7 MHz | $\begin{aligned} & \mathrm{Qu}=50 \\ & \mathrm{Ct}=100 \mathrm{pF} \end{aligned}$ | General Instrument <br> Part No. EX 27640 | Toko <br> BKAC-K3651HM |
| L1 | A-M Oscillator 1455 kHz | $\begin{aligned} & \mathrm{Qu}=50 \\ & \mathrm{~N}: \mathrm{N} 3=10.7: 1 \\ & \mathrm{Ct}=39 \mathrm{pF} \end{aligned}$ | General Instrument Part No. EX 27641 | Toko 7B0-A4017BM or RWO-6A7640BM |



6V BATTERY (4'AA' CELLS) - 250 mW OUTPUT
9V BATTERY (NEDA 1604) - 750 mW OUTPUT

Figure 12

## RADIO INTEGRATED CIRCUITS (Continued)

proximately 90 in the circuit, and the second transformer $\mathrm{T}_{2}$ as 70 with virtually no load presented by the circuit. Impedances are selected based on two constraints: a-m gain and overload. One additional point to consider is the behavior of the a-m component when the receiver is in the f -m mode.

The available I-F current at Pin 15 is $200 \mu \mathrm{~A}$ peak, $100 \mu \mathrm{~A}$ at its quiescent point. (See Figure 9). Maximum permissable swing at Pins 14 and 15 is limited to 0.5 volt positive with respect to Pin 13. This restricts peak voltage swing at Pin 15 to $1 \mathrm{~V}_{\mathrm{pp}}$, considering the inverting action of $\mathrm{T}_{2}$. This restricts the impedance of $T_{2}$, as seen by the I-F output, to values greater than $15 \mathrm{k} \Omega$ to permit maximum dynamic range. Including all worst case conditions, a value of $18 \mathrm{k} \Omega$ is chosen for $\mathrm{T}_{2}$ in the example. Considered were temperature variations and internal device tolerances. In addition, a 470 pF capacitor has been added to assure an adequate a-c return for the $\mathrm{f}-\mathrm{m}$ coil.

Transformer $\mathrm{T}_{1}$ (Figure 7) is chosen for the correct overload characteristics of the mixer. It also features a $100 \mu \mathrm{~A}$ quiescent state and a 0.5 volt peak swing restriction for primary impedance considerations, and the secondary winding chosen as the lowest practical impedance for desired system gain. Unlike $\mathrm{T}_{2}$ which is not loaded to any degree by the circuit, $\mathrm{T}_{1}$ is loaded by both the mixer output impedance of approximately $50 \mathrm{k} \Omega$ and the I-F input impedance of approximately $30 \mathrm{k} \Omega$. Both must be taken into consideration in calculating the loaded Q of the transformer. In addition, the effect of the a-m components on the f-m I-F stability must be considered - the device must be stable at both the intermediate frequencies in both modes of operation. Although no practical method exists for evaluating stability criteria for an integrated circuit as is commonly done for discrete circuits, the practical ground rules are much the same - mismatching of the input at the first transformer to achieve stability.

The oscillator coil ( $\mathrm{L}_{1}$ ) has a secondary impedance selected to be approximately $800 \Omega$ at resonance. This provides typically 150 millivolts of injection voltage to the mixer driving the upper differential pairs of the four-quadrant multiplier into hard limiting. The oscillator is also restricted to a $1 \mathrm{~V}_{\mathrm{pp}}$ swing and operates with a quiescent current of 0.5 mA .

## Printed Wiring Board Layout and Special Considerations

Special on-chip considerations for minimizing tendencies towards instabilities of all types were taken in the design of the ULN-2204A. However, like all
complex high-gain circuits, considerable care and forethought should still be given to a printed wiring board layout to avoid undesirable effects. Inputs and outputs should be well separated and should avoid common mode impedances wherever possible. Much of the signal-processing circuitry is referenced off of the supply line, and this should avoid being in a common mode loop caused by current drain of the power amplifier through Pin 13. Reference points for the local oscillator, a-m mixer, and the detector coils should be connected to Pin 13 very close to the device and away from the $\mathrm{V}_{\mathrm{CC}}$ connection to the power supply bypass capacitor.

The Pin 13 common mode resistance will also interfere with device operation in a socket. In the f-m mode of operation, current drawn by the power amplifier will cause the Pin 13 voltage to drop slightly with respect to the reference for Pin 14 and 15. This will cause a variation in gain of the $\mathrm{f}-\mathrm{m}$ detector. The effect also causes an apparent increase in distortion when the power amplifier is loaded, with distortion figures approaching several percent under worst case conditions. The effect is negligible, however, when the device is soldered into a printed wiring board.

Connections between Pins 14, 15, and transformers $T_{2}, T_{3}$, and $T_{4}$ should be kept as short as possible as should connections for Pins 1 and 2, those associated with the transformers. The ground return for the audio bypass at Pin 10 should be kept reasonably close to the volume control ground as Pin 9 and 10 represent the inverting and non-inverting inputs to the amplifier and enjoy about 40 dB of common mode rejection.

## Other Applications - TV Sound Channel

Beyond the obvious applications of the ULN2204A as an a-m/f-m receiver it has much to offer as a sound system for television. The device offers ex-ceptionally-low current consumption and a wide operating supply voltage range. Its high a-m rejection and low external component count will make it
practical for use in many power conscious applications. Most of the comments which apply to the $\mathrm{f}-\mathrm{m}$ application of the ULN-2204A also apply to its application at 4.5 MHz or 5.5 MHz with suitable adaptations of the external selectivity components. (See Figure 13)

## Multiband Receiver

The ULN-2204A A-Mcircuitry is not restricted to conventional broadcast band applications. The


Figure 13

ULN-2204A mixer and oscillator are both capable of operation from the very-long wave band to well above the medium wave bands. Only the antenna and oscillator coils need to be switched or adapted
for use at other frequencies. The useful limits of the mixer-oscillator combination extend to approximately 50 MHz with excellent performance up through and including the citizens' band at 28 MHz .



Figure 15

# A-M/F-M RECEIVER DESIGNS USING ULN-2240A, ULN-2241A, and ULN-2242A INTEGRATED CIRCUITS 

## THREE MONOLITHIC INTEGRATED

 circuits, Types ULN-2240A, ULN-2241A and ULN-2242A, each contain all the active circuit elements required for the A-M tuner, F-M I-F amplifier and detector functions. Only an F-M tuner, filter elements, and a minimum of additional external components are necessary for a complete A-M/F-M receiver.This Application Note discusses several circuits and options for a number of A-M/F-M receiver applications. Each of the three Sprague integrated circuits used provides performance characteristics equivalent to or better than systems using discrete components for A-M and $\mathrm{F}-\mathrm{M}$ functions.

The circuits are ideal for special receivers such as scanners which must be able to detect A-M and F-M signals at one I-F frequency. Also, the three devices lend themselves to shortwave receiver designs because of the simplicity of their A-M oscillator systems.

The various receiver designs covered here include an A-M tuner using a ferrite antenna, and a permeability-tuned automobile radio. Enhanced sensitivity and overload performance is obtained with the addition of an R-F amplifier, easily accomplished using the AGC voltage for the A-M mixer to control an R-F amplifier stage. The discussion covers a table model receiver with a ferrite antenna and R-F stage, and an R-F stage for an automobile receiver. The concept is extended to varactor-tuned automobile radios with the addition of an FET-bipolar cascode R-F stage and an AGC driver.


## General Performance Considerations

Internal voltage regulators and bias supplies assure consistent performance despite variations in external supply voltage ( 8.5 to 16 V ) or operating temperature $\left(-40^{\circ} \mathrm{C}\right.$ to $\left.+85^{\circ} \mathrm{C}\right)$. Separate ground leads minimize decoupling problems.

The A-M sections of all three devices are the same. Use of an analog multiplier as a balanced low-current mixer results in freedom from spurious responses, high tweet rejection, low feedthrough, and low noise and very low local oscillator feedthrough. A fully-balanced fourstage differential amplifier gives maximum gain with freedom from common-mode interference
and noise. A-M gain control is achieved with AVC applied to the I-F and delayed AVC applied to the mixer.

The differences in these three circuits are found in the F-M sections, with packaging variations to accomodate the different features. Type ULN-2241A is supplied in a 16-pin plastic dual in-line package. This circuit has no mute, and no AFC/tuning meter output (the audio output can be used for AFC). Type ULN-2242A, in a 20-pin package, incorporates the $\mathrm{F}-\mathrm{M}$ mute and AFC/tuning meter output. Type ULN-2240A, also in a 20-pin package, adds tuning-error mute, and higher F-M S/N.

## Input-Filter Coupling

The common A-M and F-M I-F inputs for all three devices are basically the same. Note that terminals 1,2 and 3 for Type ULN-2241A correspond to terminals 2,3 and 4 respectively for Types ULN-2240A and ULN-2242A.

The method of arranging the I-F filters
depends entirely on the type of filters used. For example, coils placed in series may be used for $\mathrm{A}-\mathrm{M}$ and $\mathrm{F}-\mathrm{M}$ connected as shown in Figure 1.

A ceramic filter may be used for F-M with an A-M filter incorporating a tuned coil in its output. This arrangement is illustrated in Figure 2.


Figure 1


Figure 2

The I-F input impedance is very high ( $10 \mathrm{k} \Omega$ @ $10.7 \mathrm{MHz} ; 15 \mathrm{k} \Omega$ at 455 kHz ) and can be ignored when selecting loading resistors for different types of I-F filters. Additionally, the input stage bias currents are very low, therefore a relatively high-value resistor can be connected between pins 1 and 3 of Type ULN-2241A, or pins 2 and 4 of Type ULN-2240A or ULN2242A, without significantly affecting the limiter balance.

These characteristics simplify the input filter coupling to accomodate ceramic filters used for both A-M and F-M I-Fs as shown in Figure 3.

Most 455 kHz filters are terminated by a 1 to 3 $k \Omega$ resistor in parallel with a capacitor of less


Figure 3
than 50 pF . The 10.7 MHz filter requires a $330 \Omega$ termination. If the capacitance of the 455 kHz filter is high at 10.7 MHz , the circuit will work properly as shown. However, if the capacitance of the 455 kHz filter is low, it would be advantageous to add an inductance in series with the $330 \Omega$ resistor to form a series resonant circuit with the output capacitance of the 455 kHz filter. Such a modification is shown in Figure 4.

If the inductance required is very small, it might be possible to incorporate it as an integral part of the printed wiring board.


Figure 4

## A-M Detector Considerations

Passive diode detectors are still used in many low-cost receiver designs. The A-M detector functions of Types ULN-2240A, ULN-2241A and ULN-2242A, however, are entirely selfcontained. Several drawbacks to the passive diode detector design are overcome; the load presented to the detector coil does not change with signal level, the detected output is not distorted at low signal levels, and the detector coil is not loaded down, so overall receiver selectivity is unaffected.

The self-contained detector design produces excellent A-M performance without external filtering elements. There is virtually no 910 kHz and 1365 kHz tweet. Distortion at $30 \%$ modula-
tion is only $0.3 \%$, and at $80 \%$ modulation the distortion is still under $1 \%$.

The design of the detector coil is strictly dependent on the type of receiver desired. The detector input impedance is about $250 \mathrm{k} \Omega$. For optimum detector operation, the coil should present an impedance of $4.7 \mathrm{k} \Omega$. An inexpensive detector coil can be loaded with an external resistor or tapped to obtain the $4.7 \mathrm{k} \Omega$ impedance.

It should be noted that the A-M detector works very well at 455 kHz and also at 10.7 MHz . Switching from $\mathrm{A}-\mathrm{M}$ to $\mathrm{F}-\mathrm{M}$ is as simple as grounding one pin of the integrated circuit.

## F-M Detector Options

The F-M detector functions in these three integrated circuits are very similar to those of Type ULN-3889A and the same type of circuit arrangements may be used. For low-cost receivers where distortion up to $0.4 \%$ at $100 \%$ modulation can be tolerated, the single-tuned coil detector illustrated in Figure 5 is most appropriate.


Figure 6
Usually the primary coil is adjusted for the maximum audio output while the secondary coil is adjusted for minimum distortion. Perfect detector balance at minimum distortion is desirable; however, a signal lag caused by excess parasitic capacitance from the I-F output to ground could prevent this.
The parasitic capacitance of the A-M detector coil may effectively compensate for this signal lag or it can be eliminated by placing a small inductance ( 0.1 to $1.0 \mu \mathrm{H}$ ) in series with the $220 \Omega$ load resistor.

Any of the three signal processing systems can be used as phase-locked F-M detectors. An external, voltage-controlled oscillator signal must be applied to the F-M detector. If the audio output is used, the phase detector constant $\mathrm{K}_{\mathrm{D}}=$ 4.8 volts/radian. If the AFC output is used, then:

$$
K_{D}=785 \times 10^{-6} \times R_{L}
$$

$\mathrm{R}_{\mathrm{L}}$ is the value of the resistor connected to $\mathrm{V}_{\text {REG }}$.

The AFC output is preferred because the audio can then still be muted without affecting the loop operation. More detailed information can be found in a paper published by Jon P. GrosJean. See Reference 2.

## High-Performance A-M/F-M Tuner

A high-performance A-M/F-M tuner illustrated in Figure 7 uses an R-F stage controlled by the mixer bias on pin 17 . This is 1.7 V with no
input signal and 0.6 V with large input signals. The circuit also includes mute, a tuning meter, and an AFC output to the F-M tuner.


Figure 7

## PARTS LIST FOR FIGURE 7

```
F1
F2
Q1
Q2
T1
T2
T3
T4
T5
SFE10.7MA, F-M I-F Filter CFZ455C, A-M I-F Filter MPS3563, F-M Converter MPSH-04, A-M R-F Amplifier Ferrite Loop, \(571 \mu \mathrm{H}, \mathrm{Qu}=150,17: 1\) turns ratio RWO-6A7640BM, A-M Osc., \(\mathrm{Qu}=50,11: 1\) turns ratio RLCS-4A7893GO, A-M Det., \(256 \mu \mathrm{H}, \mathrm{Qu}=75,5.4: 1\) turns ratio BKAC-K3651HM, F-M Det., \(\mathrm{Qu}=65\) BKACS-K4551AO, F-M Input, \(\mathrm{Qu}=90,7: 1\) turns ratio
```


## Low-Cost Receiver Design

A simplified receiver design illustrated in Figure 8 can produce excellent performance at very low cost using Type ULN-2241A. This simple A-M/F-M system uses a Type ULN-2283B audio amplifier and a Toko CY2-22124 PT Polyvaricon type of tuning capacitor.
The A-M section tunes from 540 to 1610 kHz . The ferrite antenna T1 has an inductance of 571 $\mu \mathrm{H}$, and 6 turns on the secondary. Twenty dB quieting sensitivity is $180 \mu \mathrm{~V} / \mathrm{m}$ and the maximum signal is about $1.0 \mathrm{~V} / \mathrm{m}$. The A-M oscillator is a negative resistance type needing only an impedance greater than $1.5 \mathrm{k} \Omega$ across pins 9 and 15 to oscillate. The oscillator coil T2 has been designed for a secondary impedance of about 5 k .

In order to obtain good A-M selectivity, a low-cost ceramic I-F filter F2 and a relatively high-Q detector coil T3 are used. The tap impedance T3 is $4.7 \mathrm{k} \Omega$.

The CFZ455C filter F2 contains a tuned circuit and ceramic resonator and has sufficient input impedance for a good mixer gain. It must be loaded with $2 \mathrm{k} \Omega$. The output capacitance of 250 pF at 10.7 MHz is large enough to terminate the F-M I-F filter F1 through $330 \Omega$. A slightly better termination for $F 1$ can be produced using a small inductance $(0.88 \mu \mathrm{H})$ placed in series
with the output of F 2 , the 455 kHz filter. At 10.7 MHz , this inductance will form a series resonant circuit with the F2 output capacitance.

The single-tuned detector coil T4 is easily aligned by simply tuning for maximum audio output. Note that AFC has been included even though Type ULN-2241A has no AFC output pin. It is only necessary to filter the audio output at pin 5 with a $1 \mathrm{M} \Omega$ resistor and a $0.05 \mu \mathrm{~F}$ capacitor for AFC.
The F-M tuner design is relatively straightforward, except: the autodyne converter is designed so that the F-M oscillator signal does not appear across the primary of the mixer coil T5, and the oscillator coil is grounded. This circuit configuration prevents the F-M oscillator signal from coupling across T5 through F1 into the ULN-2241A (pin 1). Excessive oscillator input would cause the limiters to be driven by the oscillator producing undesirable offsets with weak signals.

Note the AGC output of Type ULN-2241A is used to drive the R-F amplifier Q1. This eliminates any problems with large signals overdriving the converter Q2. Consequently, the oscillator frequency in this tuner will not change even when the input voltage rises as high as $300,000 \mu \mathrm{~V}$.

## LOW-COST TUNER PERFORMANCE CHARACTERISTICS

 (Figure 8)F-M $\quad 20 \mathrm{~dB}(\mathrm{~S}+\mathrm{N}) / \mathrm{N}=5 \mu \mathrm{~V}$
$\mathrm{f}_{\mathrm{O}}+\mathrm{I}-\mathrm{F} / 2=64 \mathrm{~dB}$
Image $=27 \mathrm{~dB}$
1 dB Limiting $=10 \mu \mathrm{~V}$
Interstation Noise $=20 \mathrm{~dB}$ below $\mathbf{3 0 \%}$
A-M $\quad 20 \mathrm{~dB}(\mathrm{~S}+\mathrm{N}) / \mathrm{N}=180 \mu \mathrm{~V} / \mathrm{m}$


Figure 8

## PARTS LIST FOR FIGURE 8

| D1 | Siemens TA314, F-M Varactor Diode |
| :--- | :--- |
| F1 | SFE10.7MA, F-M I-F Filter |
| F2 | CFZ455C, A-M I-F Filter |
| Q1 | MPS3563, F-M R-F Amplifier |
| Q2 | MPS3563, F-M Converter |
| T1 | Ferrite Loop, $571 \mu \mathrm{H}, \mathrm{Qu}=150,17: 1$ turns ratio |
| T2 | RWO-6A7640BM, A-M Osc., $\mathrm{Qu}=50,11: 1$ turns ratio |
| T3 | RLCS-4A7893GO, A-M Det., $256 \mu \mathrm{H}, \mathrm{Qu}=75,5.4: 1$ turns ratio |
| T4 | BKAC-K3651HM, F-M Det., $\mathrm{Qu}=65$ |
| T5 | BKACS-K4551AO, F-M Input, $\mathrm{Qu}=90,7: 1$ turns ratio |

## Low-Cost Automobile Radio

Automobile radios usually have two tuned R-F circuits in addition to the local oscillator. In this case Type ULN-2242A can be used in an A-M/F-M automobile radio without an A-M R-F amplifier. The R-F circuit can be doubletuned with minimal loss in sensitivity. The inductive tuning circuit is easily connected to the mixer of Type ULN-2242A as shown in Figure 9.

Note that L51 and L53 are not tapped and only the oscillator coil L55 needs a secondary winding. The $150 \mu \mathrm{H}$ coil L54 forms an inductive tap with L53 to provide a desired sensitivity and
overload level. The A-M sensitivity of the tuner with the $30 \mathrm{pF} / 30 \mathrm{pF}$ dummy antenna shown is $10 \mu \mathrm{~V}$ for $10 \mathrm{~dB}(\mathrm{~S}+\mathrm{N}) / \mathrm{N}$, and the maximum input at $80 \%$ modulation is 300 mV .

The I-F uses a ceramic filter and a singletuned high-Q detector coil. The I-F collector load resistor of $150 \Omega$ on pin 13 has been reduced from the usual $220 \Omega$ (pin 9, Figure 8) to reduce the interstation noise and to increase the limiting level for better tuning feel. An F-M tuner of the designer's choice can be added to this circuit to form a complete A-M/F-M tuner.


Figure 9

## PARTS LIST FOR FIGURE 9

F1 SFE10.7MA, F-M I-F Filter
F2 CFZ455C, A-M I-F Filter
T1 RWO-6A7640BM, A-M Osc., $\mathrm{Qu}=50,11: 1$ turns ratio
T2 RLCS-4A7893GO, A-M Det., $256 \mu \mathrm{H}, \mathrm{Qu}=75,5.4: 1$ turns ratio T3 BKAC-K3651HM, F-M Det., $\mathrm{Qu}=65$

## LOW-COST AUTO RADIO PERFORMANCE CHARACTERISTICS

(Figure 9)
A-M $\quad 10 \mathrm{~dB}(\mathrm{~S}+\mathrm{N}) / \mathrm{N}=10 \mu \mathrm{~V}$ with $30 \%$ modulation Maximum Signal $=300 \mathrm{mV}$ with $80 \%$ modulation

## Automobile Tuner With A-M R-F Stage

Improved sensitivity and excellent overload performance with the radio tuner illustrated in Figure 9 may be obtained by adding the R-F stage of Figure 10. A secondary winding has been added to L53 to couple it to the mixer of Type ULN-2241A. The emitter of the R-F stage is biased up to 0.5 V when it is turned off to im-
prove the overload. This condition causes the R-F stage to be turned OFF at a lower R-F level. Large signals are not rectified in the R-F stage.

This circuit will handle input signals to 1 volt into the $30 \mathrm{pF} / 30 \mathrm{pF}$ dummy antenna.


Figure 10

## Varactor-Tuned Automobile Radio

The tuner in Figure 11 was specifically designed for a digital synthesized A-M/F-M automobile radio. A large area, low-noise JFET, Q1, provides a reasonable broad-band match to the antenna. Tuning the antenna with a varactor diode would require a capacitance change of 9 times the total of antenna, input cable, minimum diode and stray capacitance. Because Q1 has about 5 pF feedback capacitance, Q 3 is added to form a cascode input.

Q2 provides the interface between the AGC of Type ULN-2242A and Q1, reducing the $\mathrm{g}_{\mathrm{m}}$ of Q1 by dropping the drain current as the signal level increases. This arrangement produces excellent large-signal and cross-modulation characteristics. L1 and R1 provide a static current discharge path for the antenna while L2 reduces interference from VHF signals.

T1, T2 and L4 form a double-tuned R-F circuit, an arrangement with several advantages over single-tuned circuits. The bandwidth is greater, especially at the low end of the band, so that receiver bandwidth is not determined by the R-F stages and image rejection is maintained. Mistracking caused by the matched tuning diodes is much less of a problem with the wider R-F bandwidth. The primary voltage of T 1 increases as the receiver is tuned off a station, producing better local AGC action.

As the receiver is tuned off a strong station, the AGC supplied by Q2 is normally removed from the R-F stage Q1. Large signals applied to the diodes will cause oscillations heard as whistles when the receiver is tuned in and out of a strong station. Local AGC is therefore required, and is provided by Q4 and associated components.

Q4 is coupled to T 1 by C 2 and C 3 so minimum additional capacitance is added to T 1 . The output of Q4 is rectified by a voltage doubler and filtered to remove audio frequencies produced by the voltage doubler. This arrangement coupled with the very good AGC characteristics of Type ULN-2242A, results in a receiver with large-signal capabilities better than most conventional automobile radios.

An A-M oscillator signal of about 200 mV at pin 20 can be used to drive a synthesizer if desired. Most synthesized radios mute the audio when changing stations. Since A-M and F-M are common in Type ULN-2242A, the mute works for both. A 3 to 4 -volt signal applied to pin 8 will mute either A-M or F-M.

The A-M AGC and F-M mute signals applied to Q5 provide a stop signal for use with signalseeking receivers. The collector of Q5 goes high when a signal is reached and is limited to 6.5 V to interface with 5 V digital logic circuits.

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Figure 11

## PARTS LIST FOR FIGURE 11

| D1-3 | Toko KV1215 or Sanyo SVC311 A-M Varactor Diode (3) |
| :--- | :--- |
| D4-7 | 1N914 or 1N4148 General Purpose Diode (4) |
| F1 | SFJ10.7MA, F-M I-F Filter |
| F2 | CFU455C, A-M I-F Filter |
| T1 | RWOS-6A7894AO, A-M R-F, $178 \mu \mathrm{H}, \mathrm{Qu}=120,10: 1$ turns ratio |
| T2 | RWOS-6A7894AO, A-M R-F, $178 \mu \mathrm{H}, \mathrm{Qu}=120,10: 1$ turns ratio |
| T3 | RWOS-6A7892AO, A-M Osc., $\mathrm{Qu}=120, \mathrm{Q} 1=80,5: 1$ turns ratio |
| T4 | RLCS-4A7893GO, A-M Det., $256 \mu \mathrm{H}, \mathrm{Qu}=75,5.4: 1$ turns ratio |
| T5 | BKAC-K3651HM, F-M Det., $\mathrm{Qu}=65$ |
| Q1 | MPF820 A-M R-F Amplifier |
| Q2-5 | 2N4124 General Purpose Amplifier |

# THE ULN-2242A, <br> A COMPLETE AM/FM SIGNAL PROCESSING SYSTEM 

## Introduction

This paper describes a monolithic integrated circuit which makes possible substantial simplification of AM/FM receiver design, while at the same time improving system performance.

Prior attempts at monolithic implementation started with the quadrature detector/IF gain block which was first described by A. Bilotti in 1967. ${ }^{1}$ Other devices were developed for AM circuits which in essence attempted to combine the active elements of a descrete bipolar AM receiver. The resulting monolithic devices were capable of performance no better than the original discrete design, and with the very uneconomical displacement of three discrete transistors with one integrated circuit.

To achieve useful cost and performance objectives, a new monolithic AM/FM signal processing system ${ }^{2}$ was designed with careful attention to the total system costs and performance objectives of modern
automotive and high quality home entertainment broadcast receivers. In addition to providing state-of-the-art receiver performance, this "one-chip" receiver also provides for meter drive, interstation muting, delayed AGC (for control of external AM and FM RF stages), and simple AM/FM switching.

## Circuit Description-AM Mixer

An analog multiplier is used for the AM mixer. It substantially outperforms discrete mixers in the areas of noise and spurious response rejection. As an AM mixer this circuit provides both local oscillator and received frequency rejection. The local oscillator is suppressed by approximately 40 dB and the intermediate frequency feedthrough is down by 26 dB . Spurious response suppression is important as a receiver performance objective, and also the receiver's ability to reject undesired noise passbands. The mixer's freedom from oscillator signal in


Figure 1
the IF also reduces the outband rejection requirement for the IF selectivity elements, simplifying the use of low-cost ceramic filters. The mixer current is chosen to provide 20 mmho of gain with an acceptable output overload capability.

## The AM Detector

The AM signal is peak detected, recovering audio and a d-c voltage to control AGC. Low audio distortion of $1 \%$ is achieved by maintaining a relatively constant current and resistance load, presented by the emitter-base junction of Q82 as shown in Figure 2. The recovered audio is taken off in a balanced configuration and summed at a node to cancel stage current.

## AM AGC

AM gain control is achieved by reverse AGC of the first IF by cutting off stage current to the first IF stage. AGC to the mixer is by the same method, but with a 14 dB delay to optimize gain distribution for noise considerations, and allow a better match to the input to the mixer. Gain reduction as a function of signal level is shown in the graph of Figure 3.

## Combined AM/FM IF

Stacking of the AM and FM selectivity components allows the use of a common IF amplifier.

The IF (Figure 5) is a fully-balanced amplifier having each stage differentially coupled to the succeeding stage. In addition to providing a 6 dB per stage increase in gain over single-ended coupling, this maintains constant stage and emitter follower currents to prevent signal current from appearing in on-chip grounds or supplies. Attendant signals or noise appearing on ground or supplies will be rejected as common mode by the balanced stages.

The differential coupling approach also balances capacitive effects to minimize phase delay modulation with various signal levels. To further control AC effects and reduce device input capacitance, the first IF stage is a cascode configuration to reduce Miller effect.
In the FM configuration, the IF stages are operated as limiters and provide 76 dB of gain with a corner frequency of 36 MHz . Coupled with the detector section, the combination achieves a 3 dB limiting threshold of $15 \mu \mathrm{~V}$.


Figure 2


DWG. No. A-10637

Figure 3


Figure 4


Figure 5

AM operation utilizes the same IF section as used for FM with a gain reduction and redistribution. To accomplish this, stage current is reduced in the second, third, and fourth IF stages. This puts 20 dB of gain in the first, and only 6 dB total in the remaining three stages, and also maintains a reasonably low input impedance to the IF.

## The FM Detector

The FM detector (Figure 6) is an analog multiplier operating in the high-level injection mode. In this mode, a multiplier provides high recovered audio with low audio distortion. Like the IF, the detector is also driven differentially. In addition, the inphase and quadrature signals are passed through the same number of stages. This assures good freedom from a-c offset, i.e. detector d-c offset caused by unequal phase delay in the two applied signals.

Recovered audio is processed through the same current mirrors, summing resistor, and output pin as was used for AM. AFC and meter information is provided open collector for use with an external load. This allows the AFC to be used with any reference voltage between $\mathrm{V}+$ and ground, and also permits adjustment of AFC gain by the choice of load resistor value.

## FM Mute and AGC Detectors

The mute and AGC provide d-c voltages for control of signal level related functions. The basic detector (Figure 7) is biased as a triple Darlington current source, with a quiescent state value of $10 \mu \mathrm{~A}$. Detector operation is accomplished by applying an a-c signal to C3 which forms a voltage doubler with the emitter-base junctions of Q61 and Q62 plus the smoothing Miller capacitors of convenient size for integration.


Figure 6


Figure 7

Signal for the mute detector is taken out of the quadrature coil to limit bandwidth and allow mute detector operation at the approximate limiting threshold of the device. The mute attenuation is obtained by cutting off the current mirrors to the audio. This achieves greater than 60 dB of attenuation with a minimum disturbance in d-c levels.

The AGC detector is basically the same as the mute detector, with the exception of the source of the a-c signal. This detector responds with a 2 mV signal input. Both detectors are biased to a no-signal value of 4.7 volts, and approach zero with increasing signal input as shown in Figure 8.

## Typical Application

Figure 9 illustrates a typical home entertainment receiver application for this new AM/FM signal processing system.
Sufficient FM IF gain is provided by the device to eliminate the need for any additional external gain besides that of the tuner. A 3 dB limiting sensitivity of about $2 \mu \mathrm{~V}$ is easily achieved.

All AM signal processing is performed within the device. The gain AGC and noise performance of the device in the AM mode is sufficient to achieve a useable sensitivity of $150 \mu \mathrm{~V} / \mathrm{m}$ while featuring an overload capability of $2 \mathrm{~V} / \mathrm{m}$ with a 15 cm ferrite antenna.

## Conclusion

Much of the original design for this new device was to define its operation as a system rather than as a simple component. To achieve the same revolutionary impact in AM/FM radio receivers as the design by A. Bilotti did for FM only, the new device required more than simple assembly of discrete components into an integrated circuit. Despite the integrated circuit's limitations on pin count and component values, the monolithic process with ion implantation is capable of fabricating superior circuit implementations such as fully-balanced mixers, multi-rate AGC systems, linear AM detectors, etc. at costs comparable to inferior circuits constructed with discrete components.


Figure 8


Figure 9

The device is most often specified in a standardized test fixture, eliminating as many variables as possible including AM antenna and FM tuner characteristics. Typical overall performance in such a fixture is illustrated in the following curves.

This new monolithic AM/FM signal processing system which has been described, provides the radio designer with a modern cost-effective approach to
the "one-chip" radio receiver without the performance tradeoffs so common with previous AM/FM integrated circuits.
(1) A. Bilotti and R. S. Pepper, A Monolithic Limiter and Balanced Discriminator for FM AND TV Receivers, National Electronics Conference, October (1967).
(2) Sprague Electric part number ULN-2242A.


Figure 10


Figure 11

# DEVELOPMENT OF HIGH-QUALITY RECEIVERS FOR A-M STEREO 

## Introduction

Almost all current designs for A-M receivers or tuners use a ferrite antenna and /or a tuned R-F stage with one or two separate tuned R-F circuits. These are basically just slight modifications of the old fivetube radio. Because of this, almost all literature written on the subject of A-M receiver design was written when large tube-type receivers were popular.

When a receiver must have an audio-frequency response greater than about 4 kHz , this arrangement is not satisfactory and a new approach is required. This does not, however, necessitate the design of new integrated circuits for the R-F and I-F portions of high-quality A-M stereo tuners. Presently available integrated circuits can be used (with minor circuit variations) to produce A-M tuners with performance that compete with that of the receiver's F-M section.

## Design Parameters

A-M stereo testing of many different types of A-M receivers indicates that receivers performing well with monophonic signals also perform well with stereophonic signals. A good criterion appears to be total harmonic distortion and audio frequency response. In addition to the usual requirements of good sensitivity, selectivity, image rejection, and the ability to handle large signals, distortion, signal-to-noise ratio, and audio fidelity are important parameters when designing $\mathrm{A}-\mathrm{M}$ receivers for stereo or mono. Fortunately, if the I-F filter response can be kept symmetrical, current A-M integrated circuits will give very low distortion for a large range of signal levels. In addition, most of them have also had their gains apportioned properly so that under AGC conditions, signal-to-noise ratios are not degraded and high ultimate $\mathrm{S}+\mathrm{N} / \mathrm{N}$ ratios can be reached. This eliminates some problems for the designer, but does not solve all of the possible problems.

As a guide, the following receiver parameters have been chosen: (The modulation is $30 \%$ at 1 kHz unless otherwise noted.)

1. $20 \mathrm{~dB} \mathrm{~S}+\mathrm{N} / \mathrm{N} \leq 200 \mu \mathrm{~V} / \mathrm{M}$
2. Adjacent Channel Attenuation $\geq 35 \mathrm{~dB}$
3. Image Rejection $\geq 50 \mathrm{~dB}$
4. Maximum Input Signal $1 \mathrm{~V} / \mathrm{M}$
5. THD $<0.5 \%$ and $1 \%$ at $80 \%$ Modulation
6. Maximum $\mathrm{S} / \mathrm{N} \geq 50 \mathrm{~dB}$
7. Audio Response: $20 \mathrm{~Hz}-15 \mathrm{kHz}$

Unfortunately, items 2 and 7 are incompatible with channel spacings of 10 kHz , so either a dualbandwidth I-F or poorer frequency response must be accepted.

## I-F Filters

The audio distortion and receiver selectivity are essentially determined by the I-F filter of a receiver. (Some other factors degrading the audio frequency response will be discussed under R-F circuits.) The traditional approach of using LC networks in a good quality receiver becomes very difficult because of Q limitations.

As an example, consider a transitional filter with a 40 dB bandwidth of 20 kHz and center frequency of 455 kHz .

| Number of | Max. | Min. |
| :---: | :---: | :---: |
| Sections | 3 dB BW | Coil Q |
| 3 | 3.2 kHz | 211 |
| 4 | 5.0 kHz | 180 |
| 5 | 6.7 kHz | 238 |
| 6 | 8.0 kHz | 322 |
| 7 | 9.1 kHz | 411 |
| 8 | 10.5 kHz | 483 |

[^42]The maximum available coil Q is only about 140 , so it is almost imperative that the I-F filter be a ceramic filter designed specifically for that purpose. Suitable communications ceramic filters are available, but at a cost 3 to 10 times greater than that of standard I-F transformers. There is, however, a good compromise available. Reasonably priced ceramic ladder filters with zeros in their transfer function are available with the following response (Figure 1):


Figure 1
The zeros can be selected to fall at $\pm 10 \mathrm{kHz}$ for narrow-band I-Fs, and at $\pm 20 \mathrm{kHz}$ for wide-band I-Fs. The minimum attenuation beyond the zeros of only 27 dB is too small, but this falls within a range where supplemental inductive filters can be used. This requires buffers between the coil and ceramic filters, but, as we shall see later, some integrated circuit designs easily accommodate this arrangement.

It has been found by experiment that a full 20 kHz or even 15 kHz audio response is not necessarily desirable in a high quality A-M tuner, and might even be undesirable. So much background noise and interference from other stations is present even during local daytime listening that a narrower bandwidth is more acceptable. A good compromise appears to be about 20 kHz for 3 dB bandwidth. This is degraded by other filtering in the set plus the necessary 10 kHz notch filter in the audio output to give an overall audio frequency response of about 7 to 8 kHz . In the narrow bandwidth mode for nighttime listening, the $\pm 10 \mathrm{kHz}$ attenuation must be greater than 40 dB , restricting the audio response to about 4 kHz . It should be noted that this is considerably better than the 1.6 kHz to 3 kHz audio response of current receivers.

## R-F Circuits

The R-F circuits of a high-quality A-M tuner present difficult challenges. The first occurs because the R-F stage bandwidth should not degrade the audio
frequency response. A few calculations will demonstrate the problem:

If the $\mathrm{R}-\mathrm{F}$ circuit loaded Q is 60 :

$$
1400 \mathrm{kHz}-3 \mathrm{~dB} \mathrm{BW}=23 \mathrm{kHz} \text {, Audio }=
$$ 12 kHz

At $600 \mathrm{kHz}-3 \mathrm{~dB} \mathrm{BW}=10 \mathrm{kHz}$, Audio $=5 \mathrm{kHz}$ 600 kHz Image rejection $=48 \mathrm{~dB}$

If the $Q$ of the ferrite antenna or R-F tuned circuit is reduced to improve the audio response, the image rejection suffers. In the case of the ferrite antenna, the sensitivity also suffers:

$$
\mathrm{E}_{\mathrm{g}}=\frac{\mathrm{n} \mu \mathrm{Af}}{60} \mathrm{E} \quad \mathrm{~V}=\mathrm{QE}_{\mathrm{g}}
$$

$\mathrm{V}=$ Voltage Across Antenna Circuit
$\mathrm{n}=$ Number of Turns
$\mu=$ Antenna Permeability
A $=$ Antenna Cross Sectional Area
$\mathrm{f}=$ Received Frequency
$\mathrm{Q}=$ Antenna Q
$\mathrm{E}=$ Electric Field Strength
$\mathrm{E}_{\mathrm{g}}=$ Induced Voltage
This situation can be improved by using a large loop of a few turns of wire. In this case, the formula is the same with $\mu$ being replaced with $\mu_{0}$. This antenna must, however, be very large in crosssectional area (typically $1 \mathrm{~m}^{2}$ ) before it is effective. It is also directional.

The only other alternative is the old-fashioned wire antenna which turns out to be much better in terms of signal reception. For this type:

$$
\begin{aligned}
& \mathrm{E}_{8}=\frac{\ell}{2} \mathrm{E} \quad \mathrm{~V}=\mathrm{Q}_{\mathrm{g}} \\
& \ell=\text { Antenna Length }
\end{aligned}
$$

Now, the received signal can be increased to offset reduced Q simply by making the wire longer.

This still leaves the problem of how to deal with the loss in image rejection when the $\mathrm{R}-\mathrm{F}$ circuit Q is reduced. The most obvious solution is to use a double-tuned R-F circuit. This can be manipulated to have constant bandwidth with different center frequencies so almost any desired result (without severe loss in image rejection) can be obtained. Additionally, the wider R-F bandwidth reduces tracking problems which are not usually serious for A-M mono signals, but which will cause problems with A-M stereo signals because of the group delay variations they produce.

This leaves two possibilities for antenna input circuits:

1. Couple the antenna directly to the double-tuned circuit and suffer a 6 dB insertion loss.
2. Use an untuned FET input and put the doubletuned circuit between the FET and the mixer.
Option 2 also eliminates the need for an antenna trimming capacitor. This can be a significant cost savings in automobile receivers. In both cases, however, the Q of the antenna circuit will be quite low at the low end of the A-M band, and the receiver will have somewhat poor I-F rejection. This can easily be solved by using an integrated circuit with a doublebalanced mixer.

## Receiver Designs

Illustrations of two high quality A-M tuned designs which use currently available parts are shown in Figures 2 and 3.

Both achieve the following performance levels.

$$
20 \mathrm{~dB} \frac{\mathrm{~S}+\mathrm{N}}{\mathrm{~N}} 100 \mu \mathrm{~V} / \mathrm{m}
$$

(depends on antenna length)
Image Rejection $=55 \mathrm{~dB}$
-3 dB audio frequency response from 550 to 1600 kHz : wide -7.5 kHz narrow -4 kHz
THD $<0.5 \%$ at $30 \%$ modulation
Maximum signal level $>1 \mathrm{~V} / \mathrm{m}$
Max signal-to-noise at $30 \%$ modulation $=47$ to 50 dB

The first design shown in Figure 2 uses a combination A-M/F-M integrated circuit (1) with a balanced mixer for A-M. A junction FET must be used for the $\mathrm{R}-\mathrm{F}$ stage to obtain a reasonable sensitivity (MOSFETs are very noisy at these low frequencies), but since it has a high feedback capacitance, a transistor is also used to form a cascode stage. AGC is derived from the IC and is used to reduce the current of the R-F stage. Since the IC has enough gain, the R-F stage gain can be kept low to reduce overloading. The ceramic filters in the IF stage are separated by low-cost buffer transistor stages which also perform the bandwidth switching. Added to the ceramic filters are double-tuned input (pin 14) and output coils (pin 1) to suppress the spurious responses of the filters.

The audio output terminal (pin 4) includes a 10 kHz notch filter and a 15 kHz low-pass filter to reduce unwanted noise in wideband operation. Note the simplicity of the double-tuned R-F filter. The two coils are identical and a mutual coupling capacitor is used to give greater coupling at low frequencies.

The second tuner shown in Figure 3 uses a very popular A-M-only integrated circuit (2). This IC, while not having a balanced mixer, has a separate I-F stage perfectly suited to driving the ceramic I-F filter. The R-F stage is slightly different here but retains the double-tuned interstage filter. The required R-F gain is higher because of the lower overall gain of the IC.

Instead of two double-tuned I-F filters, a 3-section filter is used and transistors are again used for bandwidth switching. The lowpass and notch filters are also retained in the audio output.

## Conclusion

It has been shown that high-quality A-M tuners using existing monolithic integrated circuits can be designed and their cost is reasonable. They are suitable for driving A-M stereo decoders and should produce very good A-M mono or stereo results. In the case of the first tuner, the 455 kHz signal to the decoder can be taken from the last I-F collector, or from a secondary winding on the detector coil. A 455 kHz signal of high-enough level is somewhat harder to obtain from the second tuner. The easiest approach appears to be to amplify the approximately 5 mV detector input signal. The internal detector then serves to generate AGC signals.

The advent of A-M stereo may hopefully serve as a catalyst for the re-development of good A-M tuners which died out when the 'all-American'' five-tube table radio was first introduced.

## References

[^43]

Figure 2


Figure 3


## SECTION 7 - TELEVISION INTEGRATED CIRCUITS

Selection Guide ..... 7-2
ULN-2211B 2-Watt TV Sound Channel ..... 7-3
ULN-2224A Chroma Demodulator ..... 7-8
ULN-2260A AGC Control, Sync Separator, and Scan Processor ..... 7-12
ULN-2261A Luminance Processor ..... 7-15
ULN-2270B and 2270Q (TDA1170) Vertical Deflection System ..... 7-19
ULN-2290B (TDA3190) and 2290Q (TDA1190Z) 4-Watt TV Sound Channel ..... 7-25
ULN-3914A Chroma/Luma Processor ..... 7-32
See Also:
ULN-3702Z for use as Vertical Output Driver ..... 8-22
Application Notes:
ULN-2211B F-M Sound System ..... 7-34
ULN-2260A Signal, Sync, and Scan Processor ..... 7-50

## SELECTION GUIDE TO TELEVISION INTEGRATED CIRCUITS

| Device Type | Chroma | Luma | Sound | Sync | Defl. |
| :--- | :---: | :---: | :---: | :---: | :---: |
| ULN-2211B | - | - | $X$ | - | - |
| ULN-2224A | $\bar{X}$ | - | - | $\bar{X}$ | - |
| ULN-2260A | - | - | - | - |  |
| ULN-2261A | - | $X$ | - | - | $\bar{X}$ |
| ULN-2270B/Q | - | - | $\bar{X}$ | - | $\overline{-}$ |
| ULN-2290B/Q | - | - | $X$ | - | $X$ |
| ULN-3702Z* | - | - | - | - | - |
| ULN-3914A | $X$ | $X$ | - |  |  |

NOTE: Additional devices for use as sound channels may be found in Section 6 and audio amplifiers may be found in Section 8.
*See page 8-22.

## ULN-2211B TV SOUND CHANNEL 2-WATT OUTPUT

## FEATURES

- Low Limiting Threshold
- Low External Parts Count
- Wide Operating Voltage Range
- 70 dB Limiter Gain
- 70 dB D-C Volume Control Range
- Automatic Thermal Shutdown
- Output Current Limiting
- 20 dB Ripple Rejection

DESIGNED for use as the entire sound function in television receivers or F-M table radios, the ULN-2211B sound channel will directly drive a 16 ohm speaker with more than 2 watts output. This monolithic integrated circuit will operate from a single 18 V to 28 V power supply and can also function (with reduced power output) with supplies as low as 12 V if additional decoupling is provided.

The ULN-2211B is supplied in an improved 16-lead plastic dual in-line package with heat-sink contact tabs. A copper alloy lead frame allows maximum

power dissipation with standard cooling methods. The unique lead configuration allows easy attachment of a heat sink and yet permits the use of a standard I.C. socket or printed wiring board layout.


FUNCTIONAL BLOCK DIAGRAM

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\mathrm{cc}} \ldots \ldots \ldots \ldots . . . . . . . . . . . . . . .+28 \mathrm{~V}$
Regulator Output Current, $\mathrm{I}_{\text {REG }} \ldots \ldots . . . . . . . . . . . . . . .10 \mathrm{~mA}$

Package Power Dissipation, $P_{D} \ldots \ldots \ldots \ldots$.......... See Graph
Operating Temperature Range, $T_{A} \ldots \ldots .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{S} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$


STATIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=24 \mathrm{~V}$

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Quiescent Supply Current | ICC | 7 | $V_{\text {in }}=0$ | 25 | 45 | 60 | mA |
| Terminal Voltage | $V_{2}$ | 2 |  | - | 10 | - | V |
|  | $V_{3}$ | 3 |  | - | 2.6 | - | V |
|  | $V_{\text {OUT }}$ | 6 |  | - | 12 | - | V |
|  | $V_{\text {REG }}$ | 8 |  | 14 | 15 | 16 | V |
|  | $\mathrm{V}_{\text {IN }}$ | 10,11 |  | - | 1.4 | - | V |
|  | $V_{14,15}$ | 14, 15 |  | - | 4.0 | - | V |
|  | $V_{16}$ | 16 |  | - | 8.0 | - | V |

DYNAMIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\text {CC }}=24 \mathrm{~V}, \mathrm{f}_{0}=4.5 \mathrm{MHz}$, $\mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}=25 \mathrm{kHz}, \mathrm{V}_{\text {in }}=10 \mathrm{mV}$ (unless otherwise specified)

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Input Limiting Threshold | $\mathrm{V}_{\text {TH }}$ | 6 | Note 1 | - | 150 | 400 | $\mu \mathrm{V}$ |
| A-M Rejection | AMR | 6 | Note 2 | 30 | $>50$ | - | dB |
| Recovered Audio | $V_{\text {out }}$ | 16 |  | 500 | 700 | 900 | mV |
| Output Distortion | THD ${ }_{\text {D }}$ | 16 |  | - | <1.0 | 3.0 | \% |
| Volume Control Voltage | $V_{1}$ | 1 | -3 dB , Note 3 | 6.0 | 7.5 | 10 | V |
|  |  |  | -20 dB , Note 3 | 2.0 | 2.8 | 4.0 | V |
|  |  |  | -40 dB, Note 3 | 0.75 | 1.2 | 1.8 | V |
| Playthrough | - | 6 | $\mathrm{V}_{1}=0 \mathrm{~V}$ | - | 5.0 | 25 | mV |
| Power Amp. Voltage Gain | $\mathrm{A}^{\text {e }}$ | 3.6 | $\mathrm{V}_{\text {out }}=1.0 \mathrm{~V}$ | 25 | 27 | 29 | dB |
| Output Distortion | THD ${ }_{0}$ | 6 | $\mathrm{P}_{\text {OUt }}=2.0 \mathrm{~W}$ | - | 2.5 | 10 | \% |
| Output Current Limiting | Iout | 6 | $\mathrm{R}_{\mathrm{L}}=0 \Omega$ | - | 800 | - | mA |
| Output Tracking | $V_{\text {OUT }} / V_{\text {cC }}$ | 6/7 | $\mathrm{V}_{\mathrm{CC}}=18 \mathrm{~V}$ to 27 V | - | 0.5 | - | V/V |
| Output Noise | $\mathrm{e}_{\mathrm{n}}$ |  | $\mathrm{V}_{\text {in }}=0 \mathrm{~V}, \mathrm{~V}_{1}=10 \mathrm{~V}$ | - | 5.0 | 25 | mV |
| Power Amp. Input Impedance | $Z_{\text {in }}$ | 3 | $\mathrm{f}=1.0 \mathrm{kHz}$ | - | 50 | - | k $\Omega$ |

NOTES:

1. Adjust $V_{1}$ for $V_{\text {out }}=2.0 \mathrm{~V}$, then reduce $\mathrm{V}_{\text {in }}$ until $\mathrm{V}_{\text {out }}=1.4 \mathrm{~V}(-3 \mathrm{~dB})$.
2. Adjust $V_{1}$ for $V_{\text {out }}=2.0 \mathrm{~V}$.
3. Reference is $\mathrm{V}_{\text {out }}$ at pin 6 with $\mathrm{V}_{1}=12 \mathrm{~V}$.

## TEST CIRCUIT AND TYPICAL APPLICATION



SUPPLY CURRENT
AS A FUNCTION OF SUPPLY VOLTAGE

A-M REJECTION
AS A FUNCTION OF INPUT VOLTAGE



ATTENUATION AS A FUNCTION OF VOLUME CONTROL VOLTAGE

OUTPUT POWER AS A FUNCTION OF SUPPLY VOLTAGE


RECOVERED AUDIO AND NOISE AS FUNCTIONS OF INPUT VOLTAGE



THD AS A FUNCTION OF DETUNING FREQUENCY

AUDIO OUTPUT
AS A FUNCTION OF FREQUENCY


## POWER DISSIPATION AND EFFICIENCY AS FUNCTIONS OF OUTPUT POWER



## THD AS A FUNCTION

 OF OUTPUT POWER

## SCHEMATIC



## ULN-2224A CHROMA DEMODULATOR WITH RGB OUTPUT

## FEATURES

- Luminance and Blanking Inputs
- Good Chroma Sensitivity
- $3 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ Typical Temperature Stability
- 600 mV Maximun Offset Voltage
- 10 Vpp Typical Blue Output Voltage
- Output Short-Circuit Protection
- Pin-for-Pin Replacement for MC1324P

PROVIDING direct red-green-blue (RGB) outputs. the Sprague ULN-2224A Chroma Demodulator contains two doubly-balanced demodulators, a resis tor matrix to derive the G-Y signal, luminance and blanking stages, and three high-level output emitter follower stages.

The ULN-2224A Chroma Demodulator is supplied


## ABSOLUTE MAXIMUM RATINGS

at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$
Package Power Dissipation, $P_{D}$ (Note 1) ........... 670 mW
Operating Temperature Range, $T_{A} \ldots \ldots . .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{s} \ldots \ldots . .-60^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

|  | Voltage Range | Current in mA |  |
| :---: | :---: | :---: | :---: |
| Pin | < in volts. | Input | Output |
| 1 | (0 to +20 | 0 | Note 2 |
| 2 | 0 to +20 |  | Note 2 |
| 3 | -0.5 to Vcc |  | 0 |
| 4 | 0 to +20 |  | Note 2 |
| 5 | 0 to +12 |  | 10 |
| 6 | -0.5 to +10 |  | - |
| 7 | reference |  | lote 3 |
| 8 | 0 to +8.0 |  | - |
| 9 | 0 to +8.0 |  | - |
| 10 | 0 to +8.0 |  |  |
| 11 | no connection |  | - |
| 12 | 0 to +10 | - | - |
| 13 | 0 to +10 | - | - |
| 14 | 0 to +30 | Note 3 | 1.0 |

NOTES:

1. Derate at the rate of $8.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.
2. Maximum continuous current output is 20 mA and is limited by package power dissipation. Short circuit current is typically 50 mA .
3. Limited by package power dissipation.

## STATIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+24 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=3.3 \mathrm{k} \Omega$

Reference Input Voltage $=1.0 \mathrm{~V}$, Figure 1 (unless otherwise noted)

| Characteristic | Test Pin | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |  |
| Quiescent Output Voltage | 1,2, 4 |  | 14.3 | - | 16.3 | V |  |
| Quiescent Input Current |  | $R_{L}=\infty$, chroma and reference input voltage $=0$. | - | 5.0 | - | mA |  |
|  |  | Chroma and reference input voltage $=0$. | 16.5 | 19 | 25 | mA |  |
| Reference Input Voltage | 12, 13 |  | - | 6.2 | - | V |  |
| Chroma Input Voltage | 8, 9, 10 |  | - | 3.4 | - | V |  |
| Differential Output Voltage | 1, 2, 4 | Figure 2. | - | 300 | 600 | mV | 1 |
| Output Temperature Coefficient | 1, 2, 4 | No output differential voltage. Figure 2. | - | 3.0 | - | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ | 1 |

DYNAMIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+24 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=3.3 \mathrm{k}_{\Omega}$
Reference Input Voltage $=1.0 \mathrm{~V}$, Figure 3 (unless otherwise noted)

| Characteristic | Test Pin | Test Conditions | Limits |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |  |
| Detector Output Voltage (B) | 4 |  | 8.0 | 10 | - | $V_{\text {PP }}$ | 2 |
| Chroma Input Voltage | 8 | B output $=5.0 \mathrm{~V}_{\text {PP }}$ | - | 300 | 700 | $\mathrm{mV}_{\mathrm{PP}}$ | 3 |
| Detector Output Voltage (G) | 1 | Adjust B output to 5.0 $\mathrm{V}_{\text {Pp }}$ | 0.75 | 1.0 | 1.25 | $\mathrm{V}_{\text {Pp }}$ | 4 |
| Detector Output Voltage (R) | 2 | Adjust B output to 5.0 V Pp | 3.5 | 3.8 | 4.2 | $\mathrm{V}_{\text {Pp }}$ | 4 |
| Relative Output Phase (B to R) | 4-2 | B output $=5.0 \mathrm{~V}_{\text {Pp }}$ | 101 | 106 | 111 | Degrees | 5 |
| Relative Output Phase (B to G) | 4-1 | B output $=5.0 \mathrm{~V}_{\text {Pp }}$ | 248 | 256 | 264 | Degrees | 5 |
| Demodulator Unbalance Voltage | 1, 2, 4 | No chroma input voltage and normal reference signal input voltage | - | 250 | 500 | $\mathrm{m} \mathrm{V}_{\text {pp }}$ | 6 |
| Residual Carrier and Harmonics | 1,2,4 | With input signal voltage, normal reference signal voltage and $\mathrm{B}=5.0 \mathrm{~V}_{\mathrm{PP}}$ | - | 0.7 | 1.5 | $V_{\text {PP }}$ | 7 |
| Reference Input Resistance | 12, 13 | Chroma input $=0$ | - | 2.0 | - | $k \Omega$ |  |
| Reference Input Capacitance | 12, 13 | Chroma input $=0$ | - | 6.0 | - | pF |  |
| Chroma Input Resistance | 9, 10 |  | - | 1.0 | - | $k \Omega$ |  |
| Chroma Input Capacitance | 9, 10 |  | - | 2.0 | - | pF |  |
| Luma Input Resistance | 3 |  | 100 | - | - | $k \Omega$ |  |

NOTES:

1. With chroma input signal voltage $=0$ and normal reference input signal voltage $=1.0 \mathrm{~V}_{\mathrm{Pp}}$, all output voltages will be within specified limits and will not differ from each other by greater than 600 mV .
2. With normal reference input signal voltage, adjust chroma input signal voltage to $1.2 \mathrm{~V}_{\mathrm{pp}}$.
3. With normal reference input signal voltage, adjust chroma input signal voltage until the $B$ output voltage $=5 V_{\text {PP: }}$. The chroma input voltage at this point should be equal to or less than $700 \mathrm{~m}_{\mathrm{PP}}$.
4. With normal reference input signal voltage, adjust the chroma input signal until the $B$ output voltage $=5 V_{\text {pp }}$. At this point, the $R$ and G voltages will fall within the specified limits. Luma voltage $=23 \mathrm{~V}$.
5. Tested with $B$ output $=5.0 \mathrm{~V}$ Pp, luma voltage $=23 \mathrm{~V}$.
6. No chroma input voltage and normal reference signal input voltage.
7. Tested with input signal voltage, normal reference signal voltage and $B$ output $=5.0 \mathrm{~V}_{\mathrm{P}}$.


Figure 1


Figure 2


Figure 3

## VECTOR DIAGRAM



Figure 4

CIRCUIT SCHEMATIC


## ULN-2260A AGC CONTROL, SYNC SEPARATOR and SCAN PROCESSOR

## features

- Excellent AGC Noise Immunity
- High Output Sync Level
- Balanced Phase Detector
- Stable Master Oscillator
- 16-Pin Dual-In-Line Plastic Package


TELEVISION-CIRCUIT SIMPLIFICATION and high performance are primary advantages of designs using Type ULN-2260A. NTSC or PAL television receivers, color or monochrome, with countdown or conventional synchronization, can be flexibly and efficiently partitioned through use of this device.

The AGC detector of Type ULN-2260A employs a coincidence gate approach that minimizes noise effects. The circuit maintains constant AGC levels despite temporary losses of synchronization and temporary horizontal timing disturbances. The AGC-synchronization loop has both the high gain and high slew rate needed for fast channel-to-channel gain equalization and reduction of airplane flutter. Both forward and reverse delayed AGC currents are developed.

The sync separator uses an external passive network. The designer chooses the sampling level and time constants. The 10 Vpp output is short-circuit limited at approximately 25 mA .

The phase detector of Type ULN-2260A compares the sync separator's output to the integrated horizontal flyback pulse. Its output is a voltage proportional to the phasing error. Static phase error attributable to detector imbalance is minimized.

The designer is able to define the free-running frequency, control sensitivity and temperature compensation of the integrated circuit's oscillator. A wide range of frequencies can be generated, accomodating any of several TV or video display terminal deflection systems.

## TYPICAL APPLICATION



## TYPICAL VCO CHARACTERISTIC



OWG. NO. A-11,221


DWG. NO. A-11,223


## ULN-2261A LUMINANCE PROCESSOR

## FEATURES

- Luma/chroma Tracking
- Automatic Bearn Limiter
- D-C Restoration
- Luma/Chroma Ventical Blanking
- Single D-C Gain Control
- Low External Component Count
- Direct Replacement for CA3135
- 16-Pin Dual In-Line Plastic Package

ASINGLE d-c picture control adjusts the gain of both the low-level video and chroma amplification in color TV receivers which employ the ULN2261A Luminance Processor. Automatic brightness limiting (ABL) and vertical blanking also take place on both channels while maintaining a constant black level. During the horizontal blanking interval, the black level is determined by clamping the black-level reference (the "back porch"). This allows for $100 \%$ d-c restoration.


## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{c c}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . 15 V
Luma Sink Current, $I_{9}$. . . . . . . . . . . . . . . . . . . . . . . . . 30 mA
Package Power Dissipation, $P_{D}$. . . . . . . . . . . . . . . $670 \mathrm{~mW}^{*}$
Operating Temperature Range, $T_{A} \ldots \ldots . .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{S} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $8.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$


STATIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Test Figure 1


DYNAMIC ELECTRICAL CHARACTERISTICS at $T_{A}=25^{\circ}$, Test Figure 2

| Video Output, $\begin{aligned} & \text { Minimum } \\ & \text { Mid } \\ & \text { Maximum }\end{aligned}$ | 9 | $\begin{array}{lllll}1 & 1 & 1 & 2 & \text { (Test 1) }\end{array}$ | 0.20 | 0.56 | Vrms |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 9 | 2112 | 0.80 | 1.50 | Vrms |
|  | 9 | $\begin{array}{lllll}3 & 1 & 1 & 2 & \text { (Test 2) }\end{array}$ | 1.50 | 2.60 | Vrms |
| Video Gain Ratio | - | Test 2/Test 1 (Test A) | 5.0 | 8.5 | - |
| Video Frequency Response | 9 | $\begin{array}{llllll}3 & 1 & 1 & \mathrm{f}=3.58 \mathrm{MHz}\end{array}$ | 1.0 | 2.6 | Vrms |
| Limited Video Gain | 9 | 3122 | 0.2 | 0.4 | Vrms |
| Chroma Output, Minimum Mid Maximum | 6 | $\begin{array}{llllll}1 & 2 & 1 & 1 & \text { (Test 3) }\end{array}$ | 50 | 150 | mVrms |
|  | 6 | 2211 | 260 | 440 | mVrms |
|  | 6 | $\begin{array}{lllll}3 & 2 & 1 & \text { (Test 4) }\end{array}$ | 400 | 750 | mVrms |
| Chroma Gain Ratio | - | Test 4/Test 3 (Test B) | 5.0 | 8.5 | - |
| Limited Chroma Gain | 6 | 3221 | 35 | 150 | mVrms |
| Video/Chroma Gain Ratio | - | Test A/Test B | 0.85 | 1.15 | - |

## TEST FIGURE 1



TEST FIGURE 2


TYPICAL APPLICATION



SCHEMATIC

## ULN-2270B AND ULN-2270Q/TDA 1170 VERTICAL DEFLECTION SYSTEM

## FEATURES

- Internal Reference
- Positive or Negative Sync Input
- Vertical Ramp Generator
- Vertical Driver
- Flyback Generator
- Single-Supply Operation

use of a standard integrated circuit socket or printed wiring board layout.

Type ULN-2270Q/TDA1170 is supplied in a 16 -pin quad in-line plastic package. It uses the printed wiring board on which it is mounted as a heat sink. Small heat sinks can also be attached to the center tabs of the device. The device carries the Sprague Electric Company part number (ULN2270Q) unless the Pro-Electron marking (TDA1170) is requested.

## ABSOLUTE MAXIMUM RATINGS


Peak Flyback Voltage, $V_{6}-V_{7} \ldots . . . . . . . . . . . . . . . . . . . . . ~ 58 \mathrm{~V}$
Sync Input Voltage, $\mathrm{V}_{10} \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots . \ldots 2 \mathrm{~V}$
Amp. Input Voltage Range, $V_{14} \ldots \ldots \ldots . .-0.5 \mathrm{~V}$ to +10 V
Peak Output Current, $\mathrm{I}_{6}(50 \mathrm{~Hz}, \quad \leq 10 \mu \mathrm{~s}) \ldots . . . . . . . .2 .5 \mathrm{~A}$
$(50 \mathrm{~Hz},>10 \mu \mathrm{~s}) \ldots \ldots \ldots \ldots 1.5 \mathrm{~A}$
(non-repetitive, 2 ms ) .......... 2.0 A
Package Power Dissipation, $P_{0}$................ See Graph
Junction Temperature Range, $T_{1} \ldots . . . .-40^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS at $T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{Cc}}=25 \mathrm{~V}, \mathrm{f}=50 \mathrm{~Hz}$ (unless otherwise specified)

| Characteristic | Test <br> Pin | Test <br> Fig. | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. |  |
| Operating Supply Voltage Range | 2 |  | : | 10 | - | 27 | V |
| Sync Input Voltage | 10 | 3 | Positive or negative | 1.0 | - | - | $V_{p}$ |
| Sync Input Resistance | 10 | 3 | $\mathrm{V}_{10}=1.0 \mathrm{~V}$ | - | 3.5 | - | k $\Omega$ |
| Oscillator Bias Current | 11 | 1 |  | - | 0.2 | 1.0 | $\mu \mathrm{A}$ |
| Oscillator Voltage | 11 | 3 |  | - | 2.4 | - | $\mathrm{V}_{\mathrm{pp}}$ |
| Oscillator Pull-In Range | 10-11 | 3 | Below 50 Hz | - | 7.0 | - | Hz |
| Oscillator Frequency Drift | 11 | 3 | $\mathrm{V}_{\mathrm{cc}}=10 \mathrm{~V}$ to 27 V | - | 0.01 | - | Hz/V |
|  |  |  | $\mathrm{T}_{\text {TAB }}=40^{\circ} \mathrm{C}$ to $120^{\circ} \mathrm{C}$ | - | 0.015 | - | $\mathrm{Hz} /{ }^{\circ} \mathrm{C}$ |
| Ramp Generator Bias Current | 16 | 1 |  | - | 50 | 500 | nA |
| Amplifier Input Current | 14 | 2 |  | - | 0.15 | 1.0 | $\mu \mathrm{A}$ |
| Quiescent Output Voltage | 6 | 1 | $\mathrm{V}_{\text {cc }}=10 \mathrm{~V}, \mathrm{R}_{2}=10 \mathrm{k} \Omega$ | 4.0 | 4.4 | 4.8 | V |
|  |  |  | $\mathrm{V}_{\text {cc }}=25 \mathrm{~V}, \mathrm{R}_{2}=30 \mathrm{k} \Omega$ | 8.0 | 8.8 | 9.6 | V |
| Flyback Voltage |  | 3 | $\mathrm{I}_{\text {YoKE }}=1.0 \mathrm{~A}$ | - | 51 | - | V |
| Flyback Time |  | 3 | $\mathrm{I}_{\text {YOKE }}=1.0 \mathrm{~A}$ | - | 0.6 | 0.8 | ms |
| Yoke Current |  | 3 |  | - | - | 1.6 | $\mathrm{A}_{\text {pp }}$ |
| Regulator Voltage | 8 or 9 | 2 |  | 6.0 | 6.5 | 7.0 | V |
| Line Regulation | 8 or 9 | 2 | $\mathrm{V}_{\mathrm{cc}}=10 \mathrm{~V}$ to 27 V | - | 1.5 | - | $\mathrm{mV} / \mathrm{V}$ |
| Supply Current |  |  | $\mathrm{I}_{\text {YoKE }}=1.0 \mathrm{~A}$ | - | 140 | - | mA |

NOTE: Pin numbering shown is in accordance with U.S. (JEDEC) practice where all positions are numbered (1 thru 16). European (Pro-Electron) practice is to skip the tab positions.

| JEDEC | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pro-Electron | 1 | 2 | 3 | TAB TAB | 4 | 5 | 6 | 7 | 8 | 9 | TAB | TAB | 10 | 11 | 12 |  |

## ALLOWABLE POWER DISSIPATION

 AS A FUNCTION OF AMBIENT TEMPERATURE

## TEST FIGURES



Dwg. No. A-10,992
Figure 1


Dwg. No. A-10,993

Figure 2

*TOLERANCE $\pm 2 \%$
Figure 3

## TYPICAL APPLICATION IN LARGE-SCREEN BLACK-AND-WHITE TV

Supply Current, Icc ..... 140 mA
Flyback Time ..... 0.75 ms
Yoke Current, I Iooke ..... $1.2 \mathrm{~A}_{\mathrm{pD}}$
Operating Supply Voltage Range, $\mathrm{V}_{\mathrm{cc}}$ ..... 20 V to 24 V
Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ ..... 2.2 W


$$
\begin{aligned}
& \text { Flyback Time } \approx \frac{2 \mathrm{~L}_{\mathrm{YOKE}} \mathrm{I}_{\mathrm{YOKE}}}{3 \mathrm{~V}_{\mathrm{CC}}} \\
& \mathrm{I}_{\mathrm{CC}} \approx \frac{\mathrm{I}_{\mathrm{YOKE}}}{8}+0.02 \\
& \mathrm{~V}_{6} \approx \mathrm{~V}_{14} \frac{\mathrm{R}_{1}+\mathrm{R}_{2}}{\mathrm{R}_{1}}
\end{aligned}
$$

Where:
Flyback Time is in seconds;
$\mathrm{L}_{\text {YokE }}$ is in henries;
$\mathrm{I}_{\text {YOKE }}$ is the peak-to-peak current in amperes;
$\mathrm{V}_{\mathrm{cC}}$ and $\mathrm{V}_{6}$ are in volts;
$\mathrm{I}_{\mathrm{CC}}$ is in amperes;
$\mathrm{V}_{14}$ is approximately 2.0 V .

## TYPICAL APPLICATION IN SMALL-SCREEN BLACK-AND-WHITE TV

| Supply Current, $I_{\text {cc }}$ | 150 mA |
| :---: | :---: |
| Flyback Time | 0.7 ms |
| Yoke Current, I Y Yoke | $1.15 \mathrm{~A}_{\mathrm{pp}}$ |
| Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ | 1.3 W |



Flyback Time $\approx \frac{2 L_{\mathrm{YOKE}} \mathrm{I}_{\mathrm{YOKE}}}{3 \mathrm{~V}_{\mathrm{CC}}}$

$$
\begin{aligned}
& \mathrm{I}_{\mathrm{CC}} \approx \frac{\mathrm{I}_{\mathrm{YOKE}}}{8}+0.02 \\
& \mathrm{~V}_{6} \approx \mathrm{~V}_{14} \frac{\mathrm{R}_{1}+\mathrm{R}_{2}}{\mathrm{R}_{1}}
\end{aligned}
$$

Where:
Flyback Time is in seconds;
$\mathrm{L}_{\text {YOKE }}$ is in henries;
$\mathrm{I}_{\text {YOKE }}$ is the peak-to-peak current in amperes;
$\mathrm{V}_{\mathrm{CC}}$ and $\mathrm{V}_{6}$ are in volts;
$\mathrm{I}_{\mathrm{CC}}$ is in amperes;
$\mathrm{V}_{14}$ is approximately 2.0 V .

## CIRCUIT SCHEMATIC



FUNCTIONAL BLOCK DIAGRAM


## ULN-2290B and ULN-2290Q TV SOUND CHANNEL (TDA3190 and TDA1 190Z) - 4 WATT OUTPUT

## FEATURES

- High Sensitivity
- High A-M Rejection
- D-C Volume Control
- High Power Output
- Low Distortion
- Wide Operating Voltage Range (9 to 28 V )
- Low Quiescent Current Drain

CAPABLE OF CARRYING OUT all of the functions of a TV sound channel, the ULN-2290 silicon monolithic integrated circuit consists of a six-stage I-F amplifier/limiter, low-pass filter, differential peak detector, d-c volume control, regulated power supply, audio preamplifier and output stage.

The audio power amplifier will deliver 4 W of low-distortion audio to a $16 \Omega$ load with a supply of 24 V . When used with a 12 V supply, such as is found in many portable TV sets, these ICs will furnish 1.5 W to an $8 \Omega$ loud speaker.

This TV sound channel is available in either of two package configurations. Type ULN-2290Q is supplied in a quad in-line plastic package with a copper lead frame. This device is designed to use the printed wiring board on which it is mounted for heat dissipation and is identical to European Type TDA1190Z. It is marked with its Pro-Electron registration unless otherwise specified on production orders.


Type ULN-2290B is furnished in an improved 16-lead plastic dual in-line package with heat-sink contact tabs. The webbed lead configuration, originated by Sprague Electric, allows an inexpensive heat sink to be easily attached for increased power dissipation capability and yet permits the use of a standard IC socket or printed wiring board hole layout. This device is identical to European Type TDA3190.

## ABSOLUTE MAXIMUM RATINGS


Repetitive Peak Output Current, I I
Package Power Dissipation, $\mathrm{P}_{\mathrm{D}} \ldots \ldots \ldots \ldots \ldots$................ Gee Graph Junction Temperature Range, $\mathrm{T}_{\mathrm{J}} \ldots \ldots . .-40^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## FUNCTIONAL BLOCK DIAGRAM



ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{f}_{0}=4.5 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm 7.5 \mathrm{kHz}$,
$V_{c C}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=8 \Omega, \mathrm{~V}_{\mathrm{in}}=1 \mathrm{mV}$ (unless otherwise specified)

| Characteristic | Symbol | Test <br> Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Quiescent Output Voltage | $V_{\text {out }}$ | 11 | $\mathrm{V}_{\mathrm{in}}=0$ | 5.1 | 6.0 | 6.9 | V |
| Quiescent Supply Current | $\mathrm{T}_{\text {cc }}$ | 14 | $\mathrm{R}_{\mathrm{x}}=22 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{in}}=0$ | - | 19 | 33 | mA |
| Tnput Limiting Threshold | $\mathrm{V}_{\text {TH }}$ | 1 | $\mathrm{R}_{\mathrm{x}}=0$ | - | 40 | 100 | $\mu \mathrm{V}$ |
| A-M Rejection | AMR |  | $\mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}, \mathrm{m}=0.3$ | 40 | 55 | - | dB |
| Signal-to-Noise Ratio | $\mathrm{S}+\mathrm{N} / \mathrm{N}$ |  | $\mathrm{P}_{\text {OUT }}=0.5 \mathrm{~W}, \mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}$ | 50 | 65 | - | dB |
| Recovered Audio | $V_{\text {out }}$ | 16 | $\mathrm{R}_{\mathrm{x}}=0$ | - | 120 | - | mV |
| Output Distortion | THD | 11 | $\mathrm{P}_{\text {our }}=50 \mathrm{~mW}$ | - | 1.0 | - | \% |
| Output Power | $P_{\text {out }}$ | 11 | THD $=2 \%, \mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}$ | - | 1.4 | - | W |
|  |  |  | THD $=10 \%, \mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}$ | - | 1.5 | - | W |
| Power Supply Rejection | PSR |  | $\mathrm{f}=120 \mathrm{~Hz}, \mathrm{R}_{\mathrm{x}}=22 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{L}}=4 \Omega$ | - | 46 | - | dB |
| Input Resistance | $\mathrm{R}_{\text {in }}$ | 1 |  | - | 30 | - | k $\Omega$ |
| Tnput Capacitance | $\mathrm{C}_{\text {in }}$ | 1 |  | - | 5.0 | - | pF |

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{f}_{0}=4.5 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm 7.5 \mathrm{kHz}, \mathrm{V}_{\text {cC }}=24 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=16 \Omega$, $\mathbf{V}_{\text {in }}=1 \mathrm{mV}$ (unless otherwise specified). Heat Sinking is Required

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Quiescent Output Voltage | $V_{\text {orr }}$ | 11 | $V_{\text {in }}=0$ | 11 | 12 | 13 | V |
| Quiescent Supply Current | $\mathrm{I}_{\text {c }}$ | 14 | $\mathrm{R}_{\mathrm{x}}=22 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{in}}=0$ | 11 | 22 | 35 | mA |
| Input Limiting Threshold | $\mathrm{V}_{\text {th }}$ | 1 | $\mathrm{R}_{\mathrm{x}}=0$ | - | 40 | 100 | $\mu \mathrm{V}$ |
| A-M Rejection | AMR |  | $\mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}, \mathrm{m}=0.3$ | 40 | 55 | - | dB |
| Signal-to-Noise Ratio | $\mathrm{S}+\mathrm{N} / \mathrm{N}$ |  | $\mathrm{P}_{\text {Our }}=1.0 \mathrm{~W}, \mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}$ | 50 | 65 | - | dB |
| Recovered Audio | $V_{\text {out }}$ | 16 | $\mathrm{R}_{\mathrm{x}}=0$ | - | 120 | - | mV |
| Output Distortion | THD | 11 | $\mathrm{P}_{\text {ourt }}=50 \mathrm{~mW}$ | - | 0.75 | - | \% |
| Output Power | $\mathrm{P}_{\text {out }}$ | 11 | THD $=2 \%, \mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}$ | - | 3.5 | - | W |
|  |  |  | THD $=10 \%, \mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}$ | - | 4.2 | - | W |
| Power Supply Rejection | PSR |  | $\mathrm{f}=120 \mathrm{~Hz}, \mathrm{R}_{\mathrm{x}}=22 \mathrm{k} \Omega, \mathrm{R}_{1}=4 \Omega$ | - | 46 | - | dB |
| Input Resistance | $\mathrm{R}_{\mathrm{in}}$ | 1 |  | - | 30 | - | k $\Omega$ |
| Input Capacitance | $\mathrm{C}_{\text {in }}$ | 1 |  | - | 5.0 | - | pF |

TEST CIRCUIT


## TYPICAL APPLICATION <br> (Heat Sink Required)



NOTE: Pin numbering shown is in accordance with U.S. (JEDEC) practice where all positions are numbered (1 thru 16). European (Pro-Electron) practice is to skip the tab positions.

| JEDEC | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pro-Electron | 1 | 2 | 3 | TAB TAB | 4 | 5 | 6 | 7 | 8 | 9 | TAB | TAB | 10 | 11 | 12 |  |

## Applications <br> Information

1. Types ULN-2290B and ULN-2290Q have high input impedances, allowing them to be used with a ceramic filter or tuned circuit to provide the necessary input selectivity.
2. The electrical characteristics of these devices will remain relatively constant over the $1-\mathrm{F}$ frequency range of 4.5 MHz to 6 MHz . They can therefore be used with all common television standards.
3. The a-c gain of the audio amplifier is determined by the resistor ratio at pin 9 . The gain should be defined in relation to the frequency deviation at which the output stage of the audio amplifier begins clipping.
4. The resistor between pins 9 and 11 can be replaced with various combinations of resistance and capacitance to provide bass boost or treble attenuation.
5. De-emphasis is determined by the capacitor connected at pin 16 and an internal $10 \mathrm{k} \Omega$ resistor. This pin can also be used to provide a treble-cut type of tone control.
6. The high-frequency audio cutoff is determined by the capacitors connected at pin 10. To increase the audio bandwidth, reduce the values of these capacitors, keeping their ratio constant.

## ALLOWABLE POWER DISSIPATION

 AS A FUNCTION OF AMBIENT TEMPERATURE

## TYPICAL CHARACTERISTICS

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{f}_{0}=4.5 \mathrm{MHz}, \mathrm{f}_{\mathrm{m}}=400 \mathrm{~Hz}, \mathrm{f}_{\mathrm{d}}= \pm 25 \mathrm{kHz}, \mathrm{V}_{\text {in }}=1 \mathrm{mV}$ (unless otherwise shown)

AUDIO OUTPUT and NOISE AS A FUNCTION OF INPUT VOLTAGE


SOUND CHANNEL OUTPUT
AS A FUNCTION OF MODULATING FREQUENCY


## A-M REJECTION

 AS A FUNCTION OF INPUT VOLTAGE

A-M REJECTION
AS A FUNCTION OF TUNING ERROR


## TYPICAL CHARACTERISTICS (Continued)

AUDIO AMPLIFIER OUTPUT AS A FUNCTION OF FREQUENCY


DISTORTION
AS A FUNCTION OF TUNING ERROR


ATTENUATION
AS FUNCTION OF RESISTANCE


DISTORTION AS A FUNCTION OF FREQUENCY DEVIATION


## TYPICAL CHARACTERISTICS (Continued)

DISTORTION
AS A FUNCTION OF OUTPUT POWER


OUTPUT POWER
AS A FUNCTION OF SUPPLY VOLTAGE


DISSIPATION and EFFICIENCY AS FUNCTIONS OF OUTPUT POWER


DISSIPATION
AS A FUNCTION OF SUPPLY VOLTAGE



SCHEMATIC

## ULN-3914A INTEGRATED CHROMA/LUMA PROCESSOR

## CHROMA FEATURES

- D-C Saturation Control (Typ. 40 dB )
- D-C Hue Control (Min. $90^{\circ}$ Range)
- Automatic Chroma Control
- Chroma Matrix
- Dynamic Flesh Correction
- Color Killer
- Overload Control
- Phase-Locked Oscillator (Min. $\pm 350 \mathrm{~Hz}$ Pull-ln)
- Automatic Phase Control

LUMA FEATURES

- D-C Brightness Control
- Keyed Blanking Level Clamp
- Horizontal Blanking
- Vertical Blanking
- Average Beam Limiter


## OTHER FEATURES

- Sand Castle Decoding
- D-C Picture Control
- RGB Outputs
- 10 to 14 V Operation
- Internal Bias Supplies
-28-Pin Dual In-Line Plastic Package

IMPROVED performance, reliability, manufacturing economy, and elimination of a substantial number of discrete components are among advantages offered by this NTSC chrominance/luminance television subsystem.

This monolithic integrated circuit replaces four devices - the chroma amplifier, chroma demodulator, oscillator and luma processor.

Type ULN-3914A derives the three color signals (RGB) from the composite video signal. Viewer

operated controls such as picture control, tint, saturation and brightness remain accessible although feedback loops are employed to eliminate the need for frequent viewer adjustments. The feedback loops provide standard automatic chroma control (ACC), dynamic flesh-color correction, beam limiting and gated black level control.

Complete technical specifications for this complex linear LSI device are available on request.

FUNCTIONAL BLOCK DIAGRAM


## THE ULN-2211 TV - FM SOUND SYSTEM

## Introduction

The sound section of the typical home television receiver has had several stages of development. The earliest vacuum-tube receivers used either a discriminator or a ratio detector. Later, because of cost and ease of tuning, the one-tube locked oscillator (or so-called quadrature detector) came into wide use.

With the advent of linear integrated circuits for the consumer market, methods of performing the F-M detector function, theretofore cost-prohibitive, were utilized to significant advantage. Although phaselocked systems have been introduced, the more classical approaches to the sound function have dominated both TV and F-M radio applications.

In the present monolithic detector, the phase-shift network is a simple one-winding coil. The full task of balancing the output has been taken over by monolithic circuitry. This makes the best use of the integrated components in keeping external components as simple as possible, and lowering costs.

The basic F-M sound system comprises five functional blocks. The first is the limiting amplifier that, together with certain detector characteristics, determines the sensitivity or threshold of the system. The small-signal gain of the limiting amplifier is typically 60 to 80 dB . The volume-control function has usually consisted of a potentiometer for varying the voltage ratio. The electronic attenuator or d-c volume control has gained popularity due to its simplicity in monolithic form and its economic advantages. The audio preamplifier usually has sufficient voltage gain to fully drive an output amplifier at $30 \%$ F-M modulation.

In the past, the output power amplifier consisted of a transformer-coupled discrete transistor or vacuum-tube class A design, although some class B
designs have also been used. Type ULN-2211 sound system includes a quasi-complementary audio power amplifier. Internal biasing and feedback is provided to set the closed loop gain at about 28 dB .

Type ULN-2211 is completely fault-protected by short-circuit current limiting and by thermal overload protection.

## System Description

Type ULN-2211 sound system is designed to satisfy all requirements of the sound-channel portion of a television receiver. In addition, it has adequate sensitivity and, with the addition of a tuner and power supply, can function as a complete monaural F-M receiver. The device features a high outputpower capability of four W (with adequate heat sinking), a wide supply-voltage range ( 12 to 28 V d-c), a minimum number of required external components, and high reliability at low cost.

A block diagram of Type ULN-2211 is shown in Figure 2. The limiting amplifier and true quadrature detector have been designed to provide more than adequate sensitivity (typically $150 \mu \mathrm{~V}$ ). Excellent A-M rejection has been achieved by the use of balanced differential gain stages, interstage decoupling networks, and balanced differential quadrature inputs.

The d-c volume control is capable of providing high attenuation for a low system play-through (typically less than $5 \mathrm{mV}_{\mathrm{rms}}$ ). Its circuit design permits the use of standard linear taper controls in a wide range of resistance values ( $1 \mathrm{k} \Omega$ to $100 \mathrm{k} \Omega$ ). The attenuation is independent of any match between the external control and internal device parameters.


DWG.NO. A-11,497
Figure 1
FM SOUND SYSTEM BLOCK DIAGRAM


DWG.NO. A-11,498
Figure 2
ULN-2211 BLOCK DIAGRAM
An internal voltage regulator provides more than 60 dB of isolation to external signals on the supply line. The regulator also permits device operation over the wide supply-voltage range with virtually no change in characteristics, other than the outputpower rating. The regulated output-voltage is available for possible use in external biasing or as a low level (less than 10 mA ) regulated supply.

The audio power amplifier provides adequate gain and drive capability to produce 4 W of power into a $16 \Omega$ load with a 27 V power supply. A special bias circuit gives a power supply rejection of better than 25 dB without the use of expensive high-value capacitors. Bias voltage is removed from the output amplifier if any overload condition causes the chip temperature to exceed a preset value. This feature, with the emitter-ballasted output-current limiters, permits complete a-c short-circuit protection under any load condition without damage to the device. D-C short-circuits can be tolerated under less severe conditions of supply voltage and drive.
Type ULN-2211 sound system is normally supplied in a modified 16 -pin dual in-line plastic package. Pins 4, 5, 12, and 13 are common and provide a means for attaching an external heat sink. The use of a copper-alloy lead frame permits a low chip to tab thermal resistance of about $15^{\circ} \mathrm{C} / \mathrm{W}$.

## Limiting-Amplifier Description

The limiting-amplifier consists of three differential stages. A fourth stage is used to provide balanced quadrature signals, as well as additional threshold sensitivity. The first two stages have a gain of 24 dB each; the gain of the third is 17 dB ; the fourth adds approximately 10 dB more for a total of 75 dB before limiting. The gain characteristic is flat to at least 10 MHz to permit the device to function at either of the standard F-M I-F frequencies $(4.5 \mathrm{MHz}$ or 10.7 MHz ).

The stages are d-c coupled via emitter followers. These are returned to the supply to keep low-level A-M signals from detector-biasing circuits. The third stage is single-ended. Its output is buffered and level shifted by $\mathrm{Q}_{13}$ and $\mathrm{D}_{3}$ to provide the proper d-c feedback via $\mathrm{R}_{14}$ and pin 11. This arrangement allows the use of only a single decoupling capacitor, saving a capacitor and resistor and requiring one pin less than other approaches.

The feedback reference for the first stage is set by diodes $D_{1}$ and $D_{2}$ which also serve as the bias source for $\mathrm{Q}_{5}, \mathrm{Q}_{6}$, and $\mathrm{Q}_{14}$.

Resistors $R_{1}, R_{2}$, and $R_{3}$ form a T-connection to define the collector loads of the first stage and adjust the output d-c level of the next stage. Similar functions are performed by $\mathrm{R}_{7}, \mathrm{R}_{8}, \mathrm{R}_{9}$, and $\mathrm{R}_{12}, \mathrm{R}_{13}$. Resistors $R_{3}, R_{9}$, and $R_{13}$ also serve a decoupling function with the low impedance at the emitters of $Q_{15}$ and $Q_{16}$ that suppresses any feedback between stages, which would degrade AM rejection, particularly at low levels.

The limiter output at diode $D_{3}$ is coupled through resistor $\mathrm{R}_{15}$ to the quadrature amplifier $\left(\mathrm{Q}_{24}\right.$ and $\left.\mathrm{Q}_{25}\right)$ and to the detector. Resistor $\mathrm{R}_{15}$ compensates for base-current drops in $\mathrm{R}_{14}$ and, together with the input capacitance of $\mathrm{Q}_{24}$ provides higher order harmonic suppression in the detector. The primary function of the quadrature amplifier is to provide balanced, symmetrical inputs to the quadrature network. This improves performance and simplifies board layout, since spurious pickup by the quadrature network is greatly reduced due to the common-mode nature of the circuit. This stage also supplies additional limiting since its output will not be reduced until the limiter output falls below that required to reduce the differential output of $Q_{24}$ and $Q_{25}$.

## F-M Detector Description

Type ULN-2211 uses a quadrature detector as shown in Figure 4. Transistors $\mathrm{Q}_{27}$ through $\mathrm{Q}_{32}$ form the actual detector. They are biased by the stabilized voltage regulator to prevent any ripple from the supply from appearing in the recovered audio. The limiter output drives the bottom pair ( $\mathrm{Q}_{31}$ and $\mathrm{Q}_{32}$ ), while the upper pairs are used as the quadrature inputs.

The detector output is developed across the balanced loads, $\mathrm{R}_{28}$ and $\mathrm{R}_{29}$. A direct audio output is available from this point via pin 16 . The impedance is set at $10 \mathrm{k} \Omega$, which provides a suitable point for de-emphasis and a tone-control function, if desired.

## TELEVISION INTEGRATED CIRCUITS (Continued)



The audio signal is directly coupled to the attenuator circuitry via the d-c level shift circuit consisting of $\mathrm{Q}_{35}, \mathrm{Q}_{36}$, and $\mathrm{R}_{39}$.

## D-C Volume Control

The primary requirements of an attenuator, or d-c volume control, are: A dynamic range of better than 70 dB , temperature stability, and independence of external component tolerances.
The d-c volume control consists of two currentsteering differential pairs $\left(\mathrm{Q}_{38}\right.$ through $\left.\mathrm{Q}_{41}\right)$. The left pair is driven by current source $Q_{37}$ from the levelshifted detector output. Current source $\mathrm{Q}_{47}$ acts as a $\mathrm{d}-\mathrm{c}$ reference to maintain the output Q-point. Attenuator output is obtained from the attenuator load resistor, $\mathrm{R}_{40}$, which is returned to the regulated supply. The other side of the attenuator is returned to $\mathrm{V}_{\mathrm{cc}}$ to minimize play-through. Transistor $\mathrm{Q}_{65}$ forms a simple emitter-follower buffer to give a low impedance output at pin 2 .

The current-steering attenuator is controlled by a d -c control voltage applied to the bases of $\mathrm{Q}_{38}$ through $\mathrm{Q}_{41}$. The signal output of the attenuator follows the relation:

$$
\begin{equation*}
\frac{\mathrm{I}_{\mathrm{O}}}{\mathrm{I}_{\mathrm{S}}}=\frac{1}{1+\mathrm{e} \frac{-\mathrm{V}_{\mathrm{BB}}}{\mathrm{KT} / \mathrm{q}}} \tag{1}
\end{equation*}
$$

where $\mathrm{KT} / \mathrm{q}$ is equal to 0.026 V . As can be seen, 6 dB of attenuation occurs at $\mathrm{V}_{\mathrm{BB}}=0$. Also, 70 dB of attenuation requires a $\mathrm{V}_{B B}$ of $8 \mathrm{KT} / \mathrm{q}$. This is a minimum figure, which more typically would be $9 \mathrm{KT} / \mathrm{q}$ or 234 mV .

All d-c volume controls now in use have some form of this attenuator to control the audio gain. The configuration provides the required 70 dB attenuation. The derivation of the control voltage $\left(\mathrm{V}_{\mathrm{BB}}\right)$ requires careful consideration, since it will directly determine the terminal characteristics of the device.

Many designs use an external resistance to control an internal bridge configuration and produce the control voltage. In spite of the problems introduced because of the wide attenuation spreads of these devices in production ( 15 to 20 dB ), they have been widely used. This attests to the value of the function itself. Some designs have derived the control voltage completely externally, relying on external component tolerances to control gain spreads and reduce thermal interactions.

The shape of the control curve has been the subject of much debate. Resistor-divider controls vary the attenuation as a logarithmic function of the control, while other techniques yield linear relationships.


Figure 4
QUADRATURE DETECTOR


Figure 5
D-C VOLUME CONTROL


Figure 6
ATTENUATION AS A FUNCTION OF $V_{B B}$

The slope, linearity, polarity and control range are different in each system proposed. However, a consensus among designers is that a control offering both a wide operating range and independence of device loading is desirable. In addition, the shape of the output voltage versus control setting curve should be ' S ' shaped. Type ULN-2211 control circuit results in an approximately linear response over most of the operating range, with a cubic response at low levels.
The control circuit used to generate this characteristic is shown in Figure 7. An external potentiometer sets the input voltage $\left(\mathrm{V}_{\mathrm{c}}\right)$.
The control uses a PNP input stage $\left(\mathrm{Q}_{66}\right.$ and $\left.\mathrm{Q}_{67}\right)$ to guarantee an input impedance of greater than $500 \mathrm{k} \Omega$. If the control impedance is significantly less than the input impedance, the loading factor is negligible. The base-emitter voltages of $\mathrm{Q}_{66}$ and $\mathrm{Q}_{67}$ are cancelled by $\mathrm{Q}_{72}$ and $\mathrm{D}_{18}$, causing the input voltage $\left(\mathrm{V}_{\mathrm{c}}\right)$ to appear across the resistor combination $\mathrm{R}_{43}$ and $\mathrm{R}_{44}$ and establish a current in $\mathrm{Q}_{45}$ that is defined as the control current:

$$
I_{C}=\left(\frac{V_{C}}{R_{43}+R_{44}}\right)\left(\frac{R_{44}}{R_{45}}\right)
$$

(2)


Figure 7
D-C VOLUME CONTROL INPUT CIRCUIT

This control current directly affects the current in $\mathrm{Q}_{43}, \mathrm{D}_{17}$, and $\mathrm{D}_{17 \mathrm{~A}}$ causing the base-emitter voltage $\left(3 \mathrm{~V}_{\mathrm{BE}}\right)$ to vary according to the familiar relation:

$$
\begin{equation*}
\mathrm{I}_{\mathrm{C}}=\mathrm{I}_{\mathrm{s}_{\mathrm{C}}} \mathrm{e}\left(\frac{\mathrm{q}^{\mathrm{V}} \mathrm{E}_{\mathrm{c}}}{\mathrm{KT}}\right)-1 \approx \mathrm{I}_{\mathrm{s}_{\mathrm{C}}} \mathrm{e}\left(\frac{\mathrm{q}^{\mathrm{V}} \mathrm{BE}}{\mathrm{~K}} \mathrm{~K}_{\mathrm{c}}\right) \tag{3}
\end{equation*}
$$

Similarly, current source $Q_{46}$ sets up a reference current $\left(I_{R}\right)$ in $D_{16}, D_{16 A}$, and $Q_{42}$. The control function can be developed as follows:

$$
\begin{equation*}
I_{C}=I_{s_{c}} e\left(\frac{q^{v} B E_{c}}{K T}\right) \tag{4}
\end{equation*}
$$

and

$$
\mathrm{V}_{\mathrm{BE}_{\mathrm{C}}}=\frac{\mathrm{KT}}{\mathrm{q}} \ell_{\mathrm{n}} \frac{\mathrm{I}_{\mathrm{C}}}{\mathrm{I}_{\mathrm{S}_{\mathrm{C}}}}
$$

> Similarly,

$$
\begin{equation*}
I_{R}=I_{S_{R}} e\left(\frac{q^{v} B E_{R}}{K T}\right) \tag{6}
\end{equation*}
$$

and

$$
\begin{equation*}
\mathrm{V}_{\mathrm{BE}_{\mathrm{R}}}=\frac{\mathrm{KT}}{\mathrm{q}} \ell_{\mathrm{n}} \frac{\mathrm{I}_{\mathrm{R}}}{\mathrm{I}_{\mathrm{S}_{\mathrm{R}}}} \tag{7}
\end{equation*}
$$

Since

$$
\begin{equation*}
V_{B_{1}}=V_{B I A S}-3 V_{B_{E_{C}}} \tag{8}
\end{equation*}
$$

substituting (5),

$$
\mathrm{V}_{\mathrm{B}_{1}}=\mathrm{V}_{\mathrm{BIAS}}-\frac{3 \mathrm{KT}}{\mathrm{q}} \ell_{\mathrm{n}} \frac{\mathrm{I}_{\mathrm{C}}}{\mathrm{I}_{\mathrm{S}_{\mathrm{C}}}}
$$

## (9)

Similarly,

$$
\begin{equation*}
V_{B_{2}}=V_{B I A S}-3 V_{\mathrm{BE}_{\mathrm{R}}} \tag{10}
\end{equation*}
$$

and substituting (7),

$$
\begin{equation*}
\mathrm{V}_{\mathrm{B}_{2}}=\mathrm{V}_{\mathrm{BIAS}}-\frac{3 \mathrm{KT}}{\mathrm{q}} \ell_{\mathrm{n}} \frac{\mathrm{I}_{\mathrm{R}}}{\mathrm{I}_{\mathrm{S}_{\mathrm{R}}}} \tag{11}
\end{equation*}
$$

Since

$$
\begin{equation*}
V_{B B}=V_{B_{1}}-V_{B_{2}} \tag{12}
\end{equation*}
$$

substituting (9) and (11) and simplifying,

$$
\begin{equation*}
\mathrm{V}_{\mathrm{BB}}=\frac{3 \mathrm{KT}}{\mathrm{q}} \ell_{\mathrm{n}} \frac{\mathrm{I}_{\mathrm{R}}}{\mathrm{I}_{\mathrm{C}}} \tag{13}
\end{equation*}
$$

Returning to (1), substituting (13), and simplifying,

$$
\frac{I_{o}}{I_{S}}=\frac{\left(I_{C} / I_{R}\right)^{3}}{\left(I_{C} / I_{R}\right)^{3}+1}
$$

If the control resistance is defined as

$$
\begin{equation*}
\mathrm{R}_{\mathrm{C}}=\left(\mathrm{R}_{43}+\mathrm{R}_{44}\right) \frac{\mathrm{R}_{45}}{\mathrm{R}_{44}} \tag{15}
\end{equation*}
$$

and (2) is reduced to

$$
\begin{equation*}
\mathrm{I}_{\mathrm{C}}=\frac{\mathrm{V}_{\mathrm{c}}}{\mathrm{R}_{\mathrm{C}}} \tag{16}
\end{equation*}
$$

then (14) can be further simplified to

$$
\begin{equation*}
\frac{I_{0}}{I_{\mathrm{S}}}=\frac{V_{\mathrm{C}}{ }^{3}}{\mathrm{~V}_{\mathrm{C}}{ }^{3}+\left(R_{\mathrm{C}} I_{\mathrm{R}}\right)^{3}} \tag{17}
\end{equation*}
$$

The parameter $\mathrm{R}_{\mathrm{C}} \mathrm{I}_{\mathrm{R}}$ will be a constant, independent of resistor variations, since $I_{R}$ is determined by the regulated voltage and another internal resistor.

Let

$$
\begin{equation*}
\mathrm{C}_{1}=\mathrm{R}_{\mathrm{C}} \mathrm{I}_{\mathrm{R}}=5 \tag{18}
\end{equation*}
$$

Therefore,

$$
\begin{equation*}
\frac{I_{0}}{I_{s}}=\frac{V_{c}{ }^{3}}{V_{c}{ }^{3}+125} \tag{19}
\end{equation*}
$$

The characteristic will be affected by variations in the internal regulator voltage and by the matching of internal resistors ( $\mathrm{R}_{43}, \mathrm{R}_{44}$, and $\mathrm{R}_{45}$ ). A maximum spread in $\mathrm{C}_{1}$ of about $\pm 10 \%$ is to be expected. The nominal and expected spread of the gain-control characteristic is shown in Figure 8. The actual output variations of the sound system, for a fixed $V_{c}$, will also be affected by changes in the detector output $\left(\mathrm{I}_{\mathrm{s}}\right)$ and gain variation of the output amplifier. Worstcase system variations under actual operating conditions are described in the applications section (see Figure 15).

## Output-Amplifier Description

The audio output amplifier of the ULN-2211 sound system is a high-gain amplifier with internal feedback that sets the closed loop gain at 25 (or 28 dB ). The biasing is such that the output d-c level (pin 6 ) is maintained at approximately $\mathrm{V}_{\mathrm{cc}} / 2$. The relationship for determining a more accurate d-c output voltage level is:

$$
\begin{equation*}
\mathrm{V}_{\mathrm{OQ}}=\left[\frac{\mathrm{V}_{\mathrm{CC}}-3 \mathrm{~V}_{\mathrm{BE}}}{\mathrm{R}_{48}+\mathrm{R}_{50}} \times \frac{\mathrm{R}_{50}}{\mathrm{R}_{56}} \times\left(\mathrm{R}_{56}+\mathrm{R}_{54}\right)\right]+3 \mathrm{~V}_{\mathrm{BE}} \tag{20}
\end{equation*}
$$

## TELEVISION INTEGRATED CIRCUITS (Continued)



Figure 8
D-C VOLUME-CONTROL CHARACTERISTIC

Inserting the resistor values, this simplifies to

$$
\begin{equation*}
\mathrm{V}_{\mathrm{OQ}}=0.45 \mathrm{~V}_{\mathrm{CC}}+1.6 \mathrm{~V}_{\mathrm{BE}} \tag{21}
\end{equation*}
$$

The unique input biasing (pat. U.S. $3,896,383$ ) provides internal ripple rejection without the use of a separate large external decoupling capacitor. Supply ripple voltage appears at the amplifier input via divider $\mathrm{R}_{48}$ and $\mathrm{R}_{50}$ and divider $\mathrm{R}_{49}$ and $\mathrm{C}_{\mathrm{c}}+\mathrm{R}_{\text {out }}$, where $\mathrm{R}_{\text {out }}$ is the output impedance of the attenuator at pin 2 . The amplifier input therefore sees only a greatly attenuated ripple component. The following expressions define the ripple rejection.

The input ripple voltage is:

$$
V_{r_{i}} \approx V_{r}\left(\frac{R_{50}}{R_{48}+R_{50}}\right) \frac{\left(R_{0 U T}^{2}+\left(1 / \omega_{\mathrm{r}} C_{c}\right)^{2}\right)^{1 / 2}}{R_{49}}
$$

(22)

The output ripple voltage is:
(23)

$$
V_{r_{0}}=V_{r_{\mathrm{i}}} A_{\mathrm{v}_{\mathrm{CL}}}
$$

The ripple rejection is:

$$
\begin{equation*}
\mathrm{S}_{\mathrm{r}}=20 \log \frac{\mathrm{~V}_{\mathrm{r}}}{\mathrm{~V}_{\mathrm{r}_{\mathrm{o}}}} \tag{24}
\end{equation*}
$$

Assuming

$$
\begin{equation*}
\mathrm{R}_{\mathrm{ouT}} \ll \frac{1}{\omega_{\mathrm{r}} \mathrm{C}_{\mathrm{c}}} \tag{25}
\end{equation*}
$$

and

$$
\begin{equation*}
\mathrm{R}_{48} \gg \mathrm{R}_{50} \tag{26}
\end{equation*}
$$

then

$$
\begin{equation*}
\frac{V_{r}}{V_{r_{0}}}=\frac{R_{48} R_{49} \omega_{\mathrm{r}} C_{\varepsilon}}{25 R_{50}} \tag{27}
\end{equation*}
$$

Inserting the component values and simplifying, the ripple rejection at 120 Hz becomes

$$
\begin{equation*}
S_{\mathrm{r}}=20 \log 39.8=32 \mathrm{~dB} \tag{28}
\end{equation*}
$$

and at 60 Hz

$$
\begin{equation*}
S_{\pi}=20 \log 19.9=26 \mathrm{~dB} \tag{29}
\end{equation*}
$$

The amplifier input stage is a Darlington differential stage biased by $\mathrm{Q}_{64}$. A diode-connected current mirror $\left(\mathrm{Q}_{54}\right)$ converts the differential output of $\mathrm{Q}_{51}$ and $Q_{52}$ to a single-ended output for the final amplifier. The final amplifier's idling current is set by a $3 \mathrm{~V}_{\mathrm{BE}}$ diode network consisting of $\mathrm{D}_{19}, \mathrm{Q}_{55}$, and $\mathrm{Q}_{56}$.

The output stage is a quasi-complementary class B design. The drivers are $\mathrm{Q}_{58}$ and $\mathrm{Q}_{61}$, while the output power transistors are $\mathrm{Q}_{59}$ and $\mathrm{Q}_{62}$. Transistor $\mathrm{Q}_{60}$ is a unity gain PNP that provides the phase reversal function. The internal closed loop gain is set by $\mathrm{R}_{54}$ and $\mathrm{R}_{56}$. A dominant pole is introduced in the amplifier's open-loop response by means of $\mathrm{R}_{55}, \mathrm{C}_{3}$, and $\mathrm{C}_{4}$. This pole can be determined by

$$
\begin{equation*}
\mathrm{f}_{\mathrm{d}}=\frac{1}{2 \pi \mathrm{~A}_{\mathrm{v}_{\mathrm{OL}}} \mathrm{C}_{3} \mathrm{R}_{55}} \tag{30}
\end{equation*}
$$



Figure 9
OUTPUT AMPLIFIER

This puts the pole at approximately 500 Hz , limiting the amplifier's closed-loop response ( $\mathrm{f}_{\mathrm{H}}$ ) to about 50 kHz .

The low-frequency pole ( $f_{L}$ ), defined by the input coupling capacitor and $\mathrm{R}_{49}$; is specified as:

$$
\begin{equation*}
\mathrm{f}_{\mathrm{L}}=\frac{1}{2 \pi \mathrm{C}_{\mathrm{C}} \mathrm{R}_{49}} \tag{31}
\end{equation*}
$$

It should be noted that the output-load coupling capacitor will also influence the low-frequency response.

A plot of the output amplifier's frequency response is shown in Figure 10.

Overload protection for the output amplifier is accomplished by limiting the output-transistor current and by removing the bias from the amplifier input when chip temperature exceeds $150^{\circ} \mathrm{C}$. Transistors $\mathrm{Q}_{57}$ and $\mathrm{Q}_{63}$ perform the current-limiting function while $Q_{21}$ senses chip temperature and acts to ground the input to the amplifier, removing bias from the output devices.


Figure 10
OUTPUT-AMPLIFIER FREQUENCY RESPONSE

Current limiting is defined by the emitter ballast resistors ( $R_{57}$ and $R_{60}$ ) as simply

$$
\begin{equation*}
\mathrm{I}_{\mathrm{SC}}=\frac{\mathrm{V}_{\mathrm{BE}}}{\mathrm{R}} \tag{32}
\end{equation*}
$$



Figure 11
INTERNAL REGULATOR

The short-circuit current is typically 1 A at $+25^{\circ} \mathrm{C}$, decreasing by approximately $3500 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ due to the reduction of $V_{B E}$ and the increase of $R_{57}$ and $\mathrm{R}_{60}$ with temperature. At the maximum chip temperature $\left(150^{\circ} \mathrm{C}\right)$, the short-circuit current will be about 560 mA .

Thermal shutdown is programmed by the voltage divider, $\mathrm{R}_{18}$ and $\mathrm{R}_{19}$. The base-emitter bias of transistor $\mathrm{Q}_{21}$ is related to the shutdown temperature as

$$
\begin{equation*}
\mathrm{T}_{\mathrm{S}} \approx \mathrm{~T}_{\mathrm{A}}\left(2-\frac{\mathrm{V}_{\mathrm{BE}_{\mathrm{S}}}}{\mathrm{~V}_{\mathrm{BE}_{\mathrm{A}}}}\right) \tag{33}
\end{equation*}
$$

where:
$\mathrm{T}_{\mathrm{s}}=$ chip shutdown temperature in ${ }^{\circ} \mathrm{K}$;
$\mathrm{T}_{\mathrm{A}}=$ reference temperature ( $293{ }^{\circ} \mathrm{K}$ );
$\mathrm{V}_{\mathrm{BE}_{\mathrm{S}}}=$ shutdown bias voltage;
$\mathrm{V}_{\mathrm{BE}_{\mathrm{A}}}=$ bias at reference temperature $(600 \mathrm{mV})$.
If $\mathrm{T}_{\mathrm{S}}$ is $423{ }^{\circ} \mathrm{K}\left(150^{\circ} \mathrm{C}\right)$, then $\mathrm{V}_{\mathrm{BE}}$ is equal to 334 mV . The circuit design actually requires a temperature of about $180^{\circ} \mathrm{C}$ to produce complete shutdown. This ensures a smooth, stable transition.

## Internal Regulator Description

The internal voltage regulator in Type ULN-2211 provides bias stabilization necessary for critical input, detector, and control functions. In addition, the regulator provides stabilization of the output bias currents and provides bias for the thermal shutdown
circuit. The first stage of the regulator consists of resistor $R_{21}$ and diodes $D_{14}$ and $D_{21}$ to provide a stable voltage for current source $Q_{20}$. The emitter resistor ( $\mathrm{R}_{19}$ ) is tapped to establish the thermal shutdown reference. The current source is mirrored in $\mathrm{Q}_{18}$, which drives diodes $D_{10}$ through $D_{13}$ to set the regulator output voltage. Transistor $Q_{17}$ is the series-pass output of the regulator. It is capable of driving all of the internal bias loads and is available at pin 8 for driving up to 10 mA (at 15 V ) into an external load.

## Characteristics and Applications

A typical application of Type ULN-2211 is shown in Figure 12. The input selectivity network can be any of several types. However, the total network impedance (pin 10-pin 11) must be less than 500 ohms to guarantee stable operation. The bypass capacitor on pin 11 should be as close to the pin as possible to assure good bypassing. It is also advisable to keep the input grounds (pin 9) separate from the output grounds (tabs) to prevent ground-current interaction at low input levels.

The detector characteristics can be varied by changing the values of $\mathrm{R}, \mathrm{L}$, and C in the quadrature tuning network. The output level and THD of the detector will depend on the $Q$ of the network. The loaded $\mathrm{Q}\left(\mathrm{Q}_{\mathrm{L}}\right)$ of the network can be found from

$$
\begin{equation*}
\mathrm{Q}_{\mathrm{L}}=\frac{\mathrm{Q}_{\mathrm{C}}}{1+\frac{\omega_{\mathrm{o}} \mathrm{~L} \mathrm{Q}_{\mathrm{C}}}{\mathrm{R}}} \tag{34}
\end{equation*}
$$



Figure 12
TYPICAL APPLICATION
where:
$\mathrm{Q}_{\mathrm{C}}=$ the unloaded coil Q ;
$R=$ the parallel combination of the equivalent $20 \mathrm{k} \Omega$ internal resistance and any additional external resistance.

Lower Q results in lower THD and recovered audio. The output of the detector is given by:

$$
\begin{equation*}
\mathrm{V}_{\mathrm{o}}=\frac{2}{\pi} \quad \arctan \left(\frac{2 \mathrm{Q}_{\mathrm{L}} \mathrm{f}_{\mathrm{d}}}{\mathrm{f}_{\mathrm{o}}}\right) \tag{35}
\end{equation*}
$$

The detector THD is given by:

$$
\begin{equation*}
\mathrm{THD} \approx 8.4\left(\frac{2 \mathrm{Q}_{\mathrm{L}} \mathrm{f}_{\mathrm{d}}}{\mathrm{f}_{\mathrm{o}}}\right)^{2} \tag{36}
\end{equation*}
$$

By substituting and solving for $Q_{C}=50(R=20 \mathrm{k} \Omega$, $\mathrm{f}_{\mathrm{o}}=4.5 \mathrm{MHz}$, and $\mathrm{f}_{\mathrm{d}}=25 \mathrm{kHz}$ ), $\mathrm{Q}_{\mathrm{L}}=30$ and THD $\approx 1 \%$. By adding an external resistor to reduce $Q_{L}$ to 20 , the THD is reduced to about $0.4 \%$ and the detector output is reduced by about $35 \%$.

The capacitor at pin 16 provides system deemphasis. The internal impedance at pin 16 is $10 \mathrm{k} \Omega$. A $0.01 \mu \mathrm{~F}$ capacitor sets de-emphasis at $100 \mu$ s or 1.6 kHz . A high-cut (low-pass) tone control can be added at pin 16. Typical values would be $25 \mathrm{k} \Omega$ and $0.22 \mu \mathrm{~F}$. Alternatively, the tone control can be added between the attenuator output and the audio input with some degradation in ripple rejection, as discussed previously.

A volume-control value between $10 \mathrm{k} \Omega$ and $100 \mathrm{k} \Omega$ is recommended. The control can be returned to $\mathrm{V}_{\mathrm{CC}}$ or returned to the regulated output on pin 8 . In the former case, some decoupling may be necessary to prevent ripple feedthrough.

The output amplifier requires only the output load capacitor and a $0.1 \mu \mathrm{~F}$ output bypass to suppress any tendency for the composite output current-sinking transistor to oscillate with inductive loads.

The input coupling capacitor $\left(\mathrm{C}_{\mathrm{C}}\right)$ is selected in accordance with previous discussions. A small capacitor, typically $0.01 \mu \mathrm{~F}$, is used at pin 2 to remove any residual high-frequency content.

The supply voltage for Type ULN-2211 may range from 12 to 27 V . However, in order to obtain a nominal 2 W output with the recommended 24 V supply, the supply impedance must be kept below $25 \Omega$ ( 19 V minimum full-load supply voltage).

The most important typical characteristics of the sound system are summarized in Table I.

Figure 13 shows the input-limiting threshold and signal-to-noise performance for the entire system (IF input to audio output). As shown, the typical limiting threshold is at $\mathrm{V}_{\mathrm{in}}=150 \mu \mathrm{~V}$.

Figure 14 shows the excellent A-M rejection characteristics of the sound system over three decades of input signal variation. The performance for the entire system is shown. The output level is set by the volume control to produce 4 V across the $16 \Omega$ load ( 1 W ) with an input voltage of $10 \mathrm{mV}_{\mathrm{rms}}$.

Figure 15 shows the output volume-control characteristic with $30 \%$ F-M modulation.

The three curves in Figure 16 show the system's residual output under conditions of $30 \% \mathrm{~A}-\mathrm{M}$ signal, continuous unmodulated carrier, and no-input signal as a function of the volume-control voltage. The curves are very similar to that of the volume-control characteristic shown in Figure 8, illustrating the uniform A-M rejection and signal-to-noise performance of the sound system as the control is varied over its full range.

Figures 17 and 18 illustrate the output capabilities of Type ULN-2211 over a wide variety of supply voltage and load conditions. As shown, a power output of up to 4 W can be obtained with a 27 V supply while a more nominal 24 V supply will allow up to 3.6 W at $10 \%$ total harmonic distortion. Care should be taken to allow for supply-voltage sag when calculating maximum output power. For example, the typical 24 V supply, with an equivalent impedance of $25 \Omega$, will sag to 19.5 V at full audio power output (approximately 2 W ). Figure 19 shows device dissipation and efficiency curves for the nominal 24 V supply.

TABLE I
TYPICAL ELECTRICAL CHARACTERISTICS at $\mathrm{f}_{0}=4.5 \mathrm{MHz}, \mathrm{V}_{\mathrm{CC}}=24 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Test Conditions | Value |
| :--- | :--- | :---: |
| Standty Current |  | 40 mA |
| Limiting Threshold |  | $150 \mu \mathrm{~V}$ |
| Deviation Sensitivity | $P_{0}=1 \mathrm{~W}, \mathrm{~V}_{1}=12 \mathrm{~V}$ | 3.5 kHz |
| A-M Rejection | $V_{\text {in }}=10 \mathrm{mV}, \mathrm{f}_{\mathrm{d}}=25 \mathrm{kHz}, \mathrm{m}=0.3$ | 55 dB |
| Play-through | $V_{1}=0, \mathrm{f}_{\mathrm{d}}=25 \mathrm{kHz}$ |  |
| THD | $V_{\text {in }}=10 \mathrm{mV}, \mathrm{f}_{\mathrm{d}}=25 \mathrm{kHz}, \mathrm{R}_{\mathrm{L}}=16 \Omega, \mathrm{P}_{0}=2 \mathrm{~W}$ | 5 mV |
| Signal-to-Noise Ratio | $\mathrm{V}_{\text {in }}=10 \mathrm{mV}, \mathrm{f}_{\mathrm{d}}=25 \mathrm{kHz}$ | $1 \%$ |



Figure 13 OUTPUT AND NOISE AS A FUNCTION OF SIGNAL INPUT


Figure 14
AM REJECTION AS A FUNCTION OF SIGNAL INPUT


Figure 15
VOLUME CONTROL CHARACTERISTIC


Figure 16 RESIDUAL OUTPUT AS A FUNCTION OF VOLUME CONTROL


Figure 17
THD AS A FUNCTION OF OUTPUT POWER


Figure 18
OUTPUT POWER
AS A FUNCTION OF SUPPLY VOLTAGE


Figure 19
DISSIPATION AND EFFICIENCY AS A FUNCTION OF OUTPUT POWER


Figure 20
16-LEAD DUAL IN-LINE ‘B' PACKAGE

## Package Design

Type ULN-2211 is furnished in a modified 16lead plastic dual in-line ' $B$ ' package shown in Figure 20. The tabs (pins $4,5,12$, and 13) allow easy attachment of various inexpensive heat sinks or can be directly soldered into the printed wiring board for low power applications.

The power dissipation of the package is ultimately limited by the chip-to-tab thermal resistance ( $\Theta_{\mathrm{JT}}$ ) of approximately $15^{\circ} \mathrm{C} / \mathrm{W}$, and the absolute maximum chip temperature of $+150^{\circ} \mathrm{C}$. The allowable power dissipation can be determined from the following equation:

$$
\begin{equation*}
P_{D}=\frac{T_{J}-T_{A}}{\Theta_{\mathrm{JT}}+\Theta_{\mathrm{TA}}} \tag{37}
\end{equation*}
$$

Figure 21 shows the allowable power dissipation as a function of ambient temperature for various tab-to-ambient thermal resistances $\left(\Theta T_{A}\right)$. The two extremes are for an infinite heat sink, which is ideal but impossible to attain, and normal unsinked printed wiring board mounting.

In practice, an intermediate condition usually exists. This is illustrated with the Staver Type V-8 heat sink. An approximate equivalent can be constructed by allowing about two square inches of excess ground foil on the printed wiring board in close proximity to the tabs.


Figure 21
POWER DISSIPATION vs AMBIENT TEMPERATURE

## Reliability

Extensive reliability testing has been performed on the single-chip sound system. These tests have included pressure-cooker, temperature, dynamic operation, and power cycling at elevated ambient temperatures. These tests have shown an excellent reliability for use in all expected environments.

## Conclusion

Type ULN-2211 sound system is designed to provide all functions required for consumer television and FM radio applications. It combines high performance with the lowest possible cost in both manufacture and application. It is capable of operating over a broad range of supply and load conditions, including repeated output short-circuits. The device has a highly stable remote $\mathrm{d}-\mathrm{c}$ volume control and a superior front end performance. The output stage provides more-than-adequate power output and high ripple rejection, without the need for a separate bypass capacitor and pin.

## References

1. Bilotti, A. and Pepper, R.S., A Monolithic Limiter and Balanced Discriminator for FM AND TV Receivers, Sprague Technical Paper TP-67-21.
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3. Mack, P. H. and Palazzini, N. S., Characteristics and Applications of the Type ULN-2111A FM Detector and Limiter, Sprague Technical Paper TP-69-3.
4. Bilotti, A. and Lutz, R. W., An Integrated Two Watt Sound System for Television Applications, Sprague Technical Paper TP-72-5.
5. Dewey, R. and Marshall, S. B., Thermal Design for Plastic Integrated Circuits, Sprague Technical Paper TP-74-1.

## TABLE II RELIABILITY TEST RESULTS

| Sample Size | Test | Test Conditions | Test Duration | Number of Failures | Cause of Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 180 | Pressure Cooker | 15 psig | 24 Hours | 1 | Lifted Ball Bond |
| 83 | Temperature Cycle | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ | 25 Cycles | 0 |  |
| 50 | Thermal Shock | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ | 25 Cycles | 0 |  |
| 60. | Dynamic Operating Life at $60^{\circ} \mathrm{C}$ | 10 @ 1/4W | 1000 Hours | 0 |  |
|  |  | 10 @ 1/2W |  | 0 |  |
|  |  | 10@1W |  | 1 | Oxide Defect |
|  |  | 30 @ 2 W |  | 0 |  |
| 12 | Power Cycling | 2 W | 21,614 Cycles | 0 |  |

# THE ULN-2260A SIGNAL, SYNC, and SCAN PROCESSOR 

## Introduction

The monolithic integrated circuit provides high performance by careful selection of circuit techniques, and efficient partitioning of the AGC, sync separator, and master-scan phase-locked loop.

This grouping of circuit functions is particularly efficient. Since the video input is common to both AGC and sync separator, the separated sync can be internally coupled to the phase detector of the scan phase-locked loop; the flyback waveform is required for AGC gating and the phase detector.


Figure 1 RECEIVER PARTITIONING


DWG.NO. A-11,485
Figure 2

AGC
When the scan is synchronized, current is supplied to the AGC detector (comparator) during the separated sync. The negative-going sync video waveform at pin 1 is compared with a 4.0 V level during this time. As a result of the AGC loop, the tip of the sync is clamped to 4.0 V .


Figure 3
AGC DETECTOR

The AGC detector is a high gain comparator with an asymetrical active load (Figures 3 and 4). The active load provides approximately 3.2 mA of primary filter capacitor charge current and 1.0 mA of discharge current.


Figure 4
AGC DETECTOR CHARACTERISTICS

The high AGC-loop gain provides the high slew rate necessary for fast channel-to-channel gain equalization and response to airplane flutter variations.
The AGC detector is gated ON by a pulse defined by coincidence of horizontal flyback and sync. Coincidence-gating provides improved AGC noise immunity over systems only are flyback-gated. Coincidence-gating maintains AGC levels in the event of temporary loss of horizontal sync or disturbance of horizontal timing.

Coincidence-gating demands the use of two additional internal circuits to compensate for two extremes of video input level at pin 1. The first is a sync recovery system (Figure 5).


Figure 5 SYNC RECOVERY SYSTEM

Extremes occur in the transition from a strong to a weak signal. The AGC loop requires time to respond to new signal level. In the meantime, system gain is too low, and the video amplitude at pin 1 is too low for the sync separator to provide sync pulses for coincidence-gating. The resulting condition would be lockout of the signal. However, a threshold detector composed of $\mathrm{Q}_{35}$ and $\mathrm{Q}_{36}$ senses sync-separator (pin 2) voltages less than 3.8 V . When this occurs, the AGC detector is gated by flyback only, allowing the AGC system to respond to the new signal level. As the video amplitude at pin 1 increases to its nominal value, the AGC detector returns to the coincidence-gating mode.
The second extreme of video input level occurs in the transition from a weak to a strong signal. In the transition, the I-F amplifier overloads, resulting in a low d-c level at pin 1, Figure 6. The sync separator at pin 2 charges to a higher d-c level, and no sync pulses are generated for coincidence-gating. Lockout of the signal is again possible, being dependent on both AGC-loop response and sync-separator time constants.


DWG.NO. A-11,489

The threshold detector, $\mathrm{Q}_{6}$ and $\mathrm{Q}_{4}$, senses when the d-c level at pin 1 is below 3.4 V . When this occurs, the AGC detector is gated by flyback only, allowing the AGC system to respond to the new signal level. As the video level at pin 1 decreases to its nominal value, the AGC detector returns to the coincidence-gating mode.
The AGC primary filter at pin 15 integrates the AGC-detector output into a d-c voltage, which drives the AGC control circuit. A low d-c level at pin 15 corresponds to a low received-signal level. Conversely, a high d-c level at pin 15 corresponds to a high received-signal level.
Figure 7 is a simplification of the I-F portion of the AGC control circuit. As is common practice, the I-F amplifier is gain-reduced prior to the tuner under increasing signal levels.


The maximum-gain voltage of the AGC primary filter is defined by the circuit designer as

$$
\mathrm{V}_{14}-0.7 \mathrm{~V}
$$

since this level is internally clamped by $\mathrm{Q}_{18}$. Under gain reduction, $\mathrm{Q}_{16}$ and $\mathrm{Q}_{\mathrm{i7}}$ force the voltage at pin 14 to follow 1.4 V below the primary filter voltage.

Produced by a series of emitter-followers, the I-F AGC output has a gain of 1 , referenced to the AGC primary filter.

Choice of the external voltage-divider level, $\mathrm{V}_{\mathrm{x}}$, at pin 13 (I-F AGC output) defines the maximum I-F gain-reduction level, or AGC delay point, at which the tuner is called upon for further gain reduction. As there is a finite dead zone in the cross-over between I-F AGC and tuner AGC, a capacitor between pin 14 (a buffered primary AGC filter a-c voltage source) and pin 13 will decrease AGC recovery time in the transition between I-F and tuner AGC.

At the maximum I-F AGC level, $\mathrm{V}_{\mathrm{x}}$, the values of resistors $R_{27}$ and $R_{30}$ are such that the voltage at the base of $\mathrm{Q}_{27}$ is 1.4 V (Figure 8). This defines the point at which tuner AGC action is initiated. The collector current of $\mathrm{Q}_{27}$ is mirrored to provide forward-tuner AGC with a trans-conductance gain of $2.1 \mathrm{~mA} / \mathrm{V}$, referenced to the AGC primary filter. The emitter current of $\mathrm{Q}_{27}$ is mirrored to provide reverse-tuner AGC with a gain of $3.1 \mathrm{~mA} / \mathrm{V}$.


Figure 8
TUNER CONTROL CIRCUIT

## Sync Separator

Since $\mathrm{Q}_{4}$, (Figure 6), clamps the video waveform to 0.5 V below the level of the sync tip, noise accompanying the incoming video is prevented from severely altering the sampling level of the sync separator.

The negative-going sync video waveform at pin 1 is inverted and amplified by 6 dB . This waveform is
buffered and applied to the base of $\mathrm{Q}_{33}$, which has as its emitter load a dual time-constant sync-separator network (Figure 9). Since this network is external to the device, the circuit designer has freedom to choose the sampling level and sync-separator time constants.


Figure 9
SINGLE PIN SYNC SEPARATOR
The separated sync-voltage waveform at the collector of $\mathrm{Q}_{33}$ is clamped to 7.3 V by $\mathrm{Q}_{38}$, and is amplified by approximately 20 dB (Figure 10). Complementary emitter-followers buffering the sync waveform have an amplitude of $10 \mathrm{~V}_{\mathrm{pp}}$. The sync output is provided at pin 3, protected by shortcircuit current-limiting of approximately 25 mA . It is internally coupled to the scan-phase detector. In addition to protecting the device against accidental shorts, grounding pin 3 also provides a convenient method of adjusting the oscillator's free-run frequency.


Figure 10 SYNC OUTPUT CIRCUIT

## Scan Processing

The scan-phase detector consists of a differential amplifier that is gated ON by separated sync. An integrated flyback waveform is applied to the input of the differential amplifier (Figure 11). The differential amplifier has an active load, providing singleended output of the phase-detector currents.


Figure 11
PHASE DETECTOR CIRCUIT
The positive and negative-output currents $(500 \mu \mathrm{~A})$ of the phase detector are internally balanced to within approximately $5 \%$ of the absolute value of these currents. This limits the static phaseerror attributable to phase-detector imbalance. Since the phase-detector output filter is external to the device, pull-in characteristics can be defined by the choice of external filter components at pin 10.

A simplification of the master-scan VCO of Type ULN-2260A is shown in Figure 12. The VCO is designed to minimize the effects of device parameter variations on free-run frequency and VCO characteristics. Components defining phase-shift and filter


DWG.NO. A-11,495
Figure 12
MASTER SCAN VCO
functions are external to the device. This provides the circuit designer with freedom to define the characteristics of the oscillator: Free-run frequency, control sensitivity and temperature compensation. Control of free-run frequency allows operation of the circuit in both countdown-synchronized and conventionally synchronized receivers.

The oscillator is controlled by weighted summing of quadrature components of feedback-signal current. The quadrature is inherently defined by the external resistor and capacitor of the tank circuit at the input of each of the two differential amplifiers. These external components are series connected. Therefore, the capacitor voltage waveform lags that of the resistor by $90^{\circ}$. VCO characteristics for a $503.5-\mathrm{KHz}$ L-C oscillator, vertical countdown receiver, are shown in Figure 13.


DWG.NO. A-11,496
Figure 13
VCO CHARACTERISTICS

Because it is a low-impedance source-point, pin 8 is internally short-circuit current-limited to approximately 70 mA .

## Conclusions

The device presented above was designed to provide, with as much flexibility as possible, efficient partitioning of AGC, sync, and scan-control functions. Coincidence AGC-gating was utilized to improve AGC noise immunity. The circuit provides a high-level separated-sync output for sync integrators. The scan-phase detector is accurately balanced internally. The scan VCO was chosen to minimize the effects of device-parameter variations on oscillator characteristics, and is adaptable to both countdown-synchronized and conventionally synchronized receivers.

BIMOS AND COMPLEX ARRAY INTERFACE DRIVERS

INDUSTRIAL, MILITARY, AND AEROSPACE DEVICES

## RADIO INTEGRATED CIRCUITS

## TELEVISION INTEGRATED CIRCUITS

AUDIO INTEGRATED CIRCUITS

HALL EFFECT DEVICES

TRANSISTOR ARRAYS AND MISCELLANEOUS DEVICES
10

CUSTOM DEVICES

8

## SECTION 8 - AUDIO INTEGRATED CIRCUITS

Selection Guide ..... 8-2
ULN-2231A Dual Audio Preamplifier ..... 8-3
ULN-2280B 2.5-Watt Audio Power Amplifier ..... 8-5
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ULX-3777W Dual 10-Watt Audio Power Amplifier ..... 8-29
ULX-3788W 20-Watt Audio Power Amplifier ..... 8-31
selection guide to audio integrated circuits

| Device Type | Monophonic | Stereo | $P_{\text {out }}$ | $V_{\text {CC }}$ |
| :---: | :---: | :---: | :---: | :---: |
| ULN-2231A | - | $X$ | - | $10.5-16 \mathrm{~V}$ |
| ULN-2280B | $X$ | - | 2.5 W | $8-26 \mathrm{~V}$ |
| ULN-2283B | $X$ | - | 1.2 W | $3-18 \mathrm{~V}$ |
| ULN-3701Z | $X$ | - | 10 W | $8-18 \mathrm{~V}$ |
| ULN-3702Z | $X$ | - | 12 W | $8-26 \mathrm{~V}$ |
| ULN-3703Z | X | - | $8-18 \mathrm{~V}$ |  |
| ULX-3777W | - | $X$ | 10 W | $8-18 \mathrm{~V}$ |
| ULX-3788W | X | - | 18 W | $8-18 \mathrm{~V}$ |

## ULN-2231A DUAL PREAMPLIFIER

## FEATURES

- Single Power Supply Operation
- Wide Supply Voltage Range
- Matched Open Loop Voltage Gain
- Turn-On Delay
- Low External Parts Count



## o

 FFERING OUTSTANDING VALUE in low-noise amplification of low-level signals, Type ULN-2231A is a reliable performer incensumer and industrial products such as stereo tape players, microphone amplifiers. phonograph preamplifiers and stereo receivers.This dual preamplifier has an internal voltage regulator. Internal feedback resistors are provided for NAB equalization.

Type ULN-2231A is supplied in a 14 -pin dual in-line plastic package.

## ABSOLUTE MAXIMUM RATINGS

| Power Supply, V ${ }_{\text {cc }}$ | +16 V |
| :---: | :---: |
| Operating Temperature Range | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature Range. | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ | 670 mW * |

${ }^{\frac{3}{2}}$ Derate at the rate of $8.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ at $\mathrm{T}_{\mathrm{A}}$ above $+25^{\circ} \mathrm{C}$.


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+\mathbf{2 5}{ }^{\circ} \mathrm{C}, \boldsymbol{+ 1 0 . 5} \mathbf{V} \leq \mathbf{V}_{\mathrm{cc}} \leq+\mathbf{1 6} \mathbf{V}$ (unless otherwise noted)

| Parameter | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. |  |
| Voltage Gain | Figure $1, f=1 \mathrm{kHz}$ | 40 | - | 46 | dB |
| Total Harmonic Distortion | $\begin{aligned} & f=1 \mathrm{kHz} \\ & V_{\text {out }}=500 \mathrm{mV} \mathrm{~V}_{\mathrm{rms}} \end{aligned}$ | - | 0.5 | 1.0 | \% |
| Noise Out | $\mathrm{R}_{\mathrm{s}}=620 \Omega$ | - | 1.5 | - | mV |
| Gain Balance |  | - | - | 2.0 | dB |
| Channel Separation |  | 40 | - | - | dB |
| Input Impedance |  | - | 40 | - | k $\Omega$ |
| Ripple Rejection | $\mathrm{f}=1 \mathrm{kHz}$ | - | 35 | - | dB |
| Input Bias Current |  | - | - | 3.0 | $\mu \mathrm{A}$ |
| Turn-On Delay |  | - | 1.0 | - | $s$ |
| ${ }^{\text {cC }}$ |  | - | - | 12 | mA |

TYPICAL RESPONSE CURVE
TEST CIRCUIT
AND TYPICAL APPLICATION


Figure 1


FREQUENCY, $\mathrm{f}, \mathrm{INHz}$
Dwg. No. A-9554A

## ULN-2280B AUDIO POWER AMPLIFIER

## FEATURES

- Low Distortion
- Low Quiescent Current
- A-C Short-Circuit Protection
- 34 dB Internally Fixed Gain
- High Input Impedance
- Thermal Overload Protection
- Replaces LM38ON

F
TEW SUPPLEMENTAL discrete components are needed to use Sprague Type ULN-2280B audio power amplifier in automotive, communication and consumer designs.

With an 18 V supply, the amplifier delivers 2.5 W of low-distortion audio into an $8 \Omega$ load. Output power with a 24 V supply is 2.5 W into a $16 \Omega$ load.


The audio amplifier is supplied in an improved 14-pin dual in-line plastic package with heat sink contact tabs. The webbed lead configuration, originated by. Sprague Electric, permits attachment of an inexpensive heat sink for increased power dissipation capability and use of a standard integrated circuit socket or printed wiring board layout.


## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage. $\mathrm{V}_{\text {cc }}$ | 26 V |
| :---: | :---: |
| Peak Output Current, Iour | 1.2 A |
| Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ | See Graph |
| Operating Temperature Range, $\mathrm{T}_{A}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$,
$V_{C C}=18 \mathrm{~V}, R_{L}=8 \Omega, f_{\text {in }}=1 \mathrm{kHz}$ (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Supply Voltage Range | $\mathrm{V}_{\mathrm{cc}}$ |  | 8.0 | 18 | 26 | V |
| Quiescent Supply Current | $\mathrm{I}_{\mathrm{cc}}$ | $\mathrm{V}_{\text {in }}=0 \mathrm{~V}$ | - | 15 | - | mA |
| Quiescent Output Voltage | $\mathrm{V}_{00}$ | $\mathrm{V}_{\text {in }}=0 \mathrm{~V}$, See Note 1 | - | 9.0 | - | V |
| Output Voltage Swing | $V_{\text {out }}$ | $\mathrm{P}_{\text {out }}=2 \mathrm{~W}$ | - | 12 | - | Vpp |
| Voltage Gain | $\mathrm{A}_{\mathrm{v}}$ | $\mathrm{P}_{\text {out }}=0 \mathrm{~W}$ | 31 | 34 | 37 | dB |
| Total Harmonic Distortion | THD | $\mathrm{P}_{\text {out }}=50 \mathrm{~mW}, \mathrm{R}_{\mathrm{L}}=8 \Omega, \mathrm{~V}_{\text {cC }}=18 \mathrm{~V}$ | - | <0.2 | 1.0 | \% |
|  |  | $P_{\text {out }}=50 \mathrm{~mW}, \mathrm{R}_{\mathrm{L}}=16 \Omega, \mathrm{~V}_{\text {cc }}=24 \mathrm{~V}$ | - | - | 0.5 | \% |
|  |  | $\mathrm{P}_{\text {out }}=2 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=8 \Omega, \mathrm{~V}_{\text {cc }}=18 \mathrm{~V}$ | - | $<1.0$ | 2.0 | \% |
| Audio Power Output | $\mathrm{P}_{\text {out }}$ | $\mathrm{R}_{\mathrm{L}}=8 \Omega, \mathrm{~V}_{\mathrm{cc}}=18 \mathrm{~V}, \mathrm{THD}=2 \%$ | 2.0 | 2.5 | - | W |
|  |  | $\mathrm{R}_{\mathrm{L}}=16 \Omega, \mathrm{~V}_{\text {cc }}=24 \mathrm{~V}, \mathrm{THD}=2 \%$ | 2.0 | 2.5 | - | W |
| Input Impedance | $Z_{\text {in }}$ | Each Input | 140 | 170 | - | $\mathrm{k} \Omega$ |
| Power Supply Rejection | PSRR | $\mathrm{P}_{\text {out }}=0 \mathrm{~W}, \mathrm{f}=120 \mathrm{~Hz}$ | - | 35 | - | dB |
| Equiv. Input Noise |  | $\mathrm{f}=20 \mathrm{~Hz}$ to 20 kHz | - | 60 | - | $\mu \mathrm{V}_{\text {ms }}$ |
| Bandwidth ( -3 dB ) | BW | $\mathrm{P}_{\text {out }}=1 \mathrm{~W}$, See Note 2 | - | 100 | - | kHz |

NOTES: 1 . The quiescent output voltage typically equals $1 / 2$ the supply voltage.
2. Unity gain typically occurs between 10 MHz and 100 MHz .

## TEST CIRCUIT



## TYPICAL CHARACTERISTICS

DISTORTION AS A FUNCTION OF OUTPUT POWER


PSRR AS A FUNCTION OF FREQUENCY


DISTORTION AS A FUNCTION OF FREQUENCY


VOLTAGE GAIN AS A FUNCTION OF FREQUENCY


## THERMAL FACTORS

## AND ULN-2280B OPERATION

Thermal factors must be considered in achieving reliable operation of Type ULN-2280B. Guidelines given here provide the circuit design engineer with information on maintaining IC junction temperature below safe limits when the audio power amplifier is operated at maximum ambient temperature and power dissipation.

The graphs below show package power dissipation as a function of output power over a wide range of supply voltage with a load resistance of $8 \Omega$ or $16 \Omega$. Lines indicating $3 \%$ distortion and $10 \%$ distortion are shown as guides to trade-offs between supply voltages, package power dissipation and upper-limit distortion.

As the power supply voltage increases for any output power requirement, distortion decreases and package power dissipation increases. Package power dissipation figures must be taken from the highest point on the supply voltage curve.

DISSIPATION AS A FUNCTION OF OUTPUT POWER ( $8 \Omega$ LOAD)


DISSIPATION AS A FUNCTION OF OUTPUT POWER ( $16 \Omega$ LOAD)


## CIRCUIT DESIGN

If design values of audio output power, distortion and maximum ambient temperature have been selected, optimal speaker impedance and supply voltage, as well as heat-sink requirements, can be determined from curves below and on page 4 .

For an output of 2.5 W with $3 \%$ distortion and a maximum ambient temperature of $+50^{\circ} \mathrm{C}$ :

| $R_{\perp}$ | $8 \Omega$ | $16 \Omega$ |
| :--- | :--- | :--- |
| $T H D$ | $3 \%$ | $3 \%$ |
| $P_{\text {our }}$ | 2.5 W | 2.5 W |
| $V_{c c}$ | 16.7 V | 22 V |
| $P_{0}(\max )$ | 1.9 W | 1.75 W |
| $P_{0}+P_{\text {our }}$ | 4.4 W | 4.25 W |
| $\mathrm{I}_{\mathrm{cc}}$ | 263 mA | 193 mA |

The preceding appears to indicate the best choice is an output impedance of $16 \Omega$ with a 22 V supply. However, if an unregulated supply is used, the designer may prefer an $8 \Omega$ load with a 16 V supply, since the absolute maximum $\mathrm{V}_{\mathrm{CC}}$ rating of Type ULN-2280B is 26 V and since maximum package dissipation must be calculated using the no-load voltage level.

The graph below (left) shows that the Staver V-8 heat sink would be just adequate for design conditions outlined above at an ambient temperature of $50^{\circ} \mathrm{C}$. The Staver V-7 heat sink would provide a wider margin of safety.

## DISSIPATION AS A FUNCTION OF AMBIENT TEMPERATURE



SUPPLY CURRENT AS A FUNCTION OF SUPPLY VOLTAGE

wh. :0. .. 11,0

## TYPICAL APPLICATIONS



Dwg. No. A-11,403

[IW1. No. A-11,40


## ULN-2283B LOW POWER AUDIO AMPLIFIER

## FEATURES

-Wide Operating Voltage Range (3 to 18 V )

- Low Quiescent Current Drain
- A-C Short Circuit Protected
- Low External Parts Count
-Low Distortion
-42 dB Voltage Gain

DESIGNED primarily for use in low-cost phonographs and radio receivers, the ULN2283B audio power amplifier is well-suited for use in battery-operated portable equipment. It will function with supply voltages as low as 2 volts (at reduced volume) without any significant increase in distortion. Weak batteries need no longer be a major concern for users in sets with this device. The class AB audio amplifier also features low quiescent current drain for maximum battery life.

The ULN-2283B is rated for operation over the supply voltage range of 3.0 to 15 volts. Selected devices, for operation with supply voltages of up to 18 volts, are available as ULN-2283B-1. Except for the maximum allowable supply voltage specification, the ULN-2283B and the ULN-2283B-1 are identical.

The ULN-2283B audio power amplifier is supplied in an improved 8 -lead dual in-line plasticpackage with two webbed tabs. A copper alloy lead frame results in maximum power dissipation without need for an external heat sink. Lead configuration is compatible with standard IC sockets or printed wiring board hole layouts.


## ABSOLUTE MAXIMUM RATINGS

$$
\text { Supply Voltage, } \mathrm{V}_{\text {cc }} \text { (ULN-2283B) . . . . . . . . . . . . . . . . } 15 \mathrm{~V}
$$

(ULN-2283B-1) . . . . . . . . . . . . . . . 18 V
Package Power Dissipation, $P_{D} \ldots \ldots . . . . . .$. . See Graph
Operating Temperature Range, $T_{A} \ldots \ldots-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{s} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+\mathbf{2 5}{ }^{\circ} \mathrm{C}, \mathrm{f}_{\text {in }}=400 \mathrm{~Hz}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Supply Voltage Range | $V_{c c}$ | ULN-2283B | 3.0 | - | 15 | V |
|  |  | ULN-2283B-1 | 3.0 | - | 18 | V |
| Quiescent Supply Current | $I_{\text {cc }}$ | $\mathrm{V}_{\text {cc }}=6.0 \mathrm{~V}$ | - | 12 | 16 | mA |
|  |  | $\mathrm{V}_{\mathrm{cc}}=12 \mathrm{~V}$ | - | 24 | 28 | mA |
| Voltage Gain | $\mathrm{A}_{\mathrm{e}}$ | $\mathrm{P}_{\text {out }}=0 \mathrm{~W}$ | 39 | 42 | 46 | dB |
| Audio Power Output | $\mathrm{P}_{\text {OUT }}$ | $\mathrm{V}_{C C}=6.0 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=8 \Omega$, THD $=10 \%$ | 0.25 | 0.35 | - | W |
|  |  | $V_{C C}=9.0 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=8 \Omega$, THD $=10 \%$ | 0.80 | 1.1 | - | W |
|  |  | $\mathrm{V}_{\text {cc }}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=16 \Omega, \mathrm{THD}=10 \%$ | 0.80 | 1.2 | - | W |
| Input Resistance | $\mathrm{R}_{\text {IN }}$ | Pin 8 | - | 250 | - | k , |
| Power Supply Rejection | PSRR | $\mathrm{C}_{0}=500 \mu \mathrm{~F}, \mathrm{f}_{\text {ripple }}=120 \mathrm{~Hz}$ | 28 | 34 | - | dB |

## TEST CIRCUIT



TYPICAL FREQUENCY RESPONSE


## ALLOWABLE PACKAGE POWER DISSIPATION

 Printed Wiring Board Copper is $20 \mathrm{oz} . / \mathrm{f}^{2}, 2.5 \mathrm{sq}$. in. ( $610 \mathrm{~g} / \mathrm{m}^{2}, 16.1 \mathrm{~cm}^{2}$ )

## TYPICAL CHARACTERISTICS

QUIESCENT SUPPLY CURRENT AS A FUNCTION OF SUPPLY VOLTAGE

OUTPUT POWER
AS A FUNCTION OF SUPPLY VOLTAGE

POWER SUPPLY REJECTION
AS A FUNCTION OF FREQUENCY


DWG.NO. A-11,238



PACKAGE POWER DISSIPATION AS A FUNCTION OF OUTPUT POWER


AT $4 \Omega$ LOAD


AT $\mathbf{8 \Omega}$ LOAD


AT $16 \Omega$ LOAD

TOTAL HARMONIC DISTORTION AS A FUNCTION OF OUTPUT POWER


AT $8 \Omega$ LOAD


AT 168 LOAD

## CIRCUIT DESCRIPTION

To achieve the desired performance objectives of high power output and efficiency from a 2 to 18 V supply requires that the amplifier be capable of peak-to-peak voltage swings approaching the available supply. To meet these performance objectives, a power amplifier design is required having no more than one $\mathrm{V}_{\mathrm{BE}}$ of swing restriction.
As shown in Figure 1, the output stage is comprised of 2 NPN transistors (Q17 and Q18) plus a phase inverter (Q15). Quiescent operating current is set up by the current source (I).
Assuming $\mathrm{V}_{\mathrm{oq}}=\mathrm{V}_{\mathrm{cc}} / 2$ then the collector current of Q15 = I, ignoring base currents, and if Q15 is matched to Q18 as is possible in a monolithic circuit, then the collector current of Q18 equals the collector current of Q15.
The circuit in Figure 1 achieves an excellent voltage swing capability of $\mathrm{V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{BE}}-2 \mathrm{~V}_{\mathrm{CESAAT}}$. This totally NPN configuration also has good freedom from the high-frequency problems that often occur with quasi-complementary composite NPN-PNP configurations.


Figure 1

Although the circuit in Figure 1 has been incorporated in production monolithic circuits in essentially the form shown, in practice it has unacceptable design restrictions. Since I is also the base drive current for Q17, the ratio of available base drive current I to idling current is proportional to the ratio of the emitter areas of Q18 to Q15. For practical values of $\mathrm{I}_{\mathrm{Q} 15} / \mathrm{I}_{\text {Q18 }}$, i.e. one, the circuit has a serious implementation problem; it requires three output transistors (Q15, Q17, and Q18).


Figure 2
To reduce the size of Q15, an additional transistor (Q16) is added to the circuit as shown in Figure 2. Transistor Q16 divides I by its beta +1 allowing Q15 to be reduced in area by a similar value. In the practical realization of the ULN-2283B, Q15 is chosen as $1 / 5$ the emitter area of Q18 with a typical beta for Q16 of 6 .


Figure 3
Figure 3 illustrates other refinements in the practical realization of the output circuit. The drive and idling current I is derived from a $\mathrm{V}_{\mathrm{cc}}$ dependent source allowing maximum drive under maximum supply conditions while affording reduced drive and associated current conservation under minimum supply conditions. In addition, the Q16 divider circuit is refined to reduce PNP beta dependence. Finally with the addition of an input emitter follower (Q11) and a local negative feedback loop (R8), the output is completed as it appears in the ULN-2283B.


Figure 4
The input stage of the power amplifier (Figure 4) is comprised of a PNP differential pair (Q2 and Q3) preceded by a PNP emitter follower (Q1) which allows d-c referencing of the source signal to ground. This eliminates the need for an input coupling capacitor. Overall negative feedback, set by the ratio of R 4 to R 5 , is applied to the inverting input Q3 through an NPN emitter follower (Q7) which also provides d-c level shifting.

The $\mathrm{V}_{\mathrm{CC}} / 2$ output tracking is achieved by summing the current flow through R4 and R5, with the current through R13 "reflected off of ground." Thus $\mathrm{V}_{\mathrm{CC}} / 2$ tracking is maintained by the voltage drop across 2 resistors. This allows the current from R13 to be bypassed at Pin 1, thereby combining the ripple bypass capacitor with the audio feedback capacitor.

Figure 5 illustrates the complete power amplifier as realized in the ULN-2283B, including the external components. The remarkably-low external component count, (only two capacitors including the output coupling) reflects concern for simplicity in implementation, yet the device achieves excellent performance. Typical output power can be as high as 2.1 W from a 12 volt supply and useful output power at supply voltages of as low as 2 volts.

## APPLICATIONS

Selection of power supply voltage and speaker impedance allow the designer to choose audio power levels. No unique precautions are necessary when designing with the ULN-2283B power amplifier. The device is stable and a-c short-circuit immune.


Figure 5

External component choice for the power amplifier involves only two capacitors; one for the speaker coupling and one for the feedback and ripple by-passing. The coupling capacitor value should be selected to provide the desired low-frequency cutoff with the chosen speaker impedance. The feedback and ripple bypass capacitor at Pin 1 should be chosen for both low-frequency audio rolloff and supply ripple rejection.

Ripple rejection is not practical to calculate due to the large number of mechanisms involved. A $500 \mu \mathrm{~F}$ capacitor at Pin 1 achieves typically 34 dB rejection.

The high gain of typically 42 dB and the high input impedance ( $250 \mathrm{k} \Omega$ ) of the power amplifier allow utilization of this device for applications such as ceramic cartridge phono amplifiers.

Typical ceramic phono cartridges develop approximately 400 mV . However, the recommended load impedance for the most economical cartridges is usually $1 \mathrm{M} \Omega$. This poses no problem with the $250 \mathrm{k} \Omega$ input impedance of the ULN-2283B since the cartridge manufacturer specifies the load impedance for full low-frequency response to less than 40 Hz . Decreasing the load impedance produces an increased low end cutoff frequency.

In a ULN-2283B based application employing a cost and space conscious loudspeaker, 40 Hz program material capability is not only unnecessary but undesirable, and therefore a mismatch of the cartridge to increase the lower cutoff frequency to a value more in keeping with the other components of the system is recommended.

The ULN-2283B audio amplifier stage has other input considerations to be taken into account for best results. The input is referenced to ground for internal biasing and must be provided with a d-c path to ground. A current of typically $0.1 \mu \mathrm{~A}$ flows from Pin 8 through the volume control producing an IR drop which is multiplied by the closed loop d-c gain of the amplifier (1), and appears as an error in output centering at Pin 4. This recommends a value of $200 \mathrm{k} \Omega$ or less for the volume control, with values of less than $100 \mathrm{k} \Omega$ preferred.

The selection of amplifier load impedance involves more consideration than just the desired power output. Ideally a low speaker impedance would produce the highest power outputs for any one supply voltage as the curves illustrated. However, operation with a $16 \Omega$ load can produce as much power as with an $8 \Omega$ load. The higher impedance load will also furnish a significant reduction in harmonic distortion and improvement in overall repeatability in power output capacity. In applications which allow the selection of the power supply voltage it is therefore recommended that a $16 \Omega$ load impedance be utilized in applications up to 1.2 watt.

## PRINTED WIRING BOARD LAYOUT \& SPECIAL CONSIDERATIONS

Special on-chip considerations for minimizing tendencies towards instabilities of all types were taken in the design of the ULN-2283B. However, like all high-gain circuits, care and forethought should still be given to a printed wiring board layout to avoid undesirable effects. Input and output should be well separated and should avoid common mode impedances wherever possible. The ground return for the audio bypass at Pin 1 should be kept reasonably close to the volume control ground as Pins 1 and 8 represent the inverting and non-inverting inputs to the amplifier and enjoy about 40 dB of common mode rejection.

Device dissipation vs. output power and supply voltage for 4,8 , and 16 ohm loads is shown in the curves on page 4 . With no heat sinking (free air), the ULN-2283B audio power amplifier will withstand the worst case conditions ( $4 \Omega$ at 9 V ) for ambient temperatures to $+42.5^{\circ} \mathrm{C}$. For conditions not shown, for higher ambient temperatures, or for improved device reliability, a minimum heat sink is recommended. As illustrated in the allowable package power dissipation curves, with the heat sink tabs (Pins 2, 3, 6, and 7) soldered into a 2.5 square inch ( $16.13 \mathrm{~cm}^{2}$ ) copper area of a printed circuit board, adequate heat sinking is easily obtained.

## ULN-3701Z/TDA2002 5- to 10-WATT AUDIO POWER AMPLIFIER

## FEATURES

- Low External Parts Count
- Low Distortion
- Class B Operation
- Short-Circuit Protected
- Thermal Overload Protected
- Low Noise
- High Output-Voltage Swing
- T0-220 Style Package
- Direct Replacement for LM383 and CA2002


DESIGNED specifically for driving lowimpedance loads down to $1.6 \Omega$, the ULN$3701 \mathrm{Z} / \mathrm{TDA} 2002$ audio power amplifier is ideal for automotive radio, tape player, and CB applications and can deliver 15 W of audio in the bridge configuration or 5 W to 10 W single-ended. Operating in the extremely harsh automotive environment, these devices are capable of withstanding high ambient temperatures, output overloads, and repeated power supply transient voltages without damage.

The ULN-3701Z /TDA2002 is supplied in a modified 5-lead JEDEC Style TO-220 plastic package. The heat sink tab is at ground potential and therefore no insulation is required. Lead forming for either vertical or horizontal mounting (suffix letter " $V$ '" or ' H ,' ' respectively) is available on special order.

These integrated circuits will be marked with their U.S. part number unless the European TDA number is specified on production orders.

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $V_{c c}$ ..... 28 V
Peak Supply Voltage ( 50 ms ) ..... 40 V
Peak Output Current, I Iout ..... 3.5 A
Non-Repetitive Peak Output Current ..... 4.5 A
Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ ..... 15 W*
Storage Temperature Range, $T_{S}$ ..... $-40^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

[^44]ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{cc}}=14.4 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=4 \Omega, \mathrm{f}=1 \mathrm{kHz}$ (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Supply Voltage Range | $V_{c c}$ |  | 8.0 | 14.4 | 18 | $V$ |
| Quiescent Supply Current | $\mathrm{I}_{\mathrm{Cc}}$ | No signal applied | - | 45 | 80 | mA |
| Quiescent Output Voltage | $V_{4}$ | No signal applied | 6.4 | 7.2 | 8.0 | V |
| Open Loop Gain | A |  | - | 80 | - | dB |
| Closed Loop Gain | A |  | 39.5 | 40 | 40.5 | dB |
| Total Harmonic Distortion | THD | $\mathrm{P}_{\text {Out }}=0.05$ to 3.5 W | - | 0.2 | - | \% |
|  |  | $\mathrm{P}_{\text {OUT }}=0.05$ to $5.0 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | - | 0.2 | - | \% |
| Audio Power Output | Pout | THD $=10 \%$ | 4.8 | 5.2 | - | W |
|  |  | THD $=10 \%, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | 7.0 | 8.0 | - | W |
|  |  | THD $=10 \%, \mathrm{~V}_{\text {cc }}=16 \mathrm{~V}$ | - | 6.5 | - | W |
|  |  | THD $=10 \%, \mathrm{R}_{\mathrm{L}}=2 \Omega, \mathrm{~V}_{C C}=16 \mathrm{~V}$ | - | 10 | - | W |
| Efficiency | $\cdots$ | $\mathrm{P}_{\text {Out }}=5.2 \mathrm{~W}$ | - | 68 | - | \% |
|  |  | $\mathrm{P}_{\text {OUT }}=8.0 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | - | 58 | - | \% |
| Input Impedance | $Z_{1}$ |  | 70 | 150 | - | k $\Omega$ |
| Power Supply Rejection | PSR | $\mathrm{f}_{\text {ripple }}=120 \mathrm{~Hz}, \mathrm{~V}_{\text {ripple }}=0.5 \mathrm{~V}$ | 30 | 35 | - | dB |
| Equiv. Input Noise Voltage | $\mathrm{e}_{\mathrm{N}}$ | $\mathrm{f}=40 \mathrm{~Hz}$ to 15 kHz | - | 4.0 | - | $\mu \mathrm{V}$ |
| Equiv. Input Noise Current | $\mathrm{i}_{\mathrm{N}}$ | $\mathrm{f}=40 \mathrm{~Hz}$ to 15 kHz | - | 60 | - | pA |
| Input Sensitivity | $\mathrm{e}_{\text {in }}$ | $\mathrm{P}_{\text {Out }}=0.5 \mathrm{~W}$ | - | 15 | - | mV |
|  |  | $\mathrm{P}_{\text {OUT }}=0.5 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | - | 11 | - | mV |
|  |  | $\mathrm{P}_{\text {Out }}=5.2 \mathrm{~W}$ | - | 55 | - | mV |
|  |  | $\mathrm{P}_{\text {OUT }}=8.0 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | - | 50 | - | mV |
| Input Saturation Voltage | $\mathrm{e}_{\text {in }}$ |  | - | 600 | - | mV |
| Frequency Response ( -3 dB ) |  | $\mathrm{C}_{\mathrm{fb}}=0.039 \mu \mathrm{~F}, \mathrm{R}_{\mathrm{fb}}=39 \Omega$ | 40 | - | 15 k | Hz |
| Thermal Resistance | $\mathrm{R}_{\text {өл }}$ |  | - | - | 4.0 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

TYPICAL OUTPUT POWER
AS A FUNCTION OF SUPPLY VOLTAGE



15 W BRIDGE APPLICATION


# ULN-3702Z/TDA2002A 12-WATT AUDIO POWER AMPLIFIER 

FEATURES<br>- Low External Parts Count<br>- Low Distortion<br>- Class B Operation<br>- Short-Circuit Protected<br>- Thermal Overload Protected<br>- Low Noise<br>- T0-220 Style Package

THE ABILITY TO DRIVE high-power loads in consumer and industrial electronics expands the field of application for Type ULN-3702Z/ TDA2002A.

The high-gain power amplifier can be used as a vertical output driver in television receivers and video terminals or as a linear d-c motor driver. Its operational-amplifier configuration, with high input impedance and low output impedance, makes it adaptable to many input, output and feedback arrangements.

One modification sets this audio power amplifier apart from Sprague Type ULN-3701Z/TDA2002: The integrated circuit's internal high-voltage shutdown has been disabled. The change allows continuous operation with supply voltages of up to 26 V . With a d-c load current rating of 2.5 A , Type ULN3702 Z /TDA2002A can handle up to 60 watts of power with an appropriate heat sink. It is able to withstand high ambient temperatures, output overloads, and repeated power supply transients without damage.

The amplifier is supplied in a modified five-lead JEDEC Style TO-220 plastic package. The heat sink tab is at ground potential; no insulation is required.

Special lead configurations for vertical mounting (ULN-3702ZV) and for horizontal mounting (ULN-3702ZH) are available on special order. Parts are branded with the Sprague Electric part number (ULN-3702Z) unless Pro-Electron marking (TDA2002A) is requested.



## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\text {cc }}$ ..... 28 V
Peak Supply Voltage ( 50 ms ) ..... 40 V
Peak Output Current, I ${ }_{\text {out }}$ ..... 3.5 A
Non-Repetitive Peak Output Current ..... 4.5 A
Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ ..... 15 W*
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ ..... $-40^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

[^45]ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$,
$V_{\text {cc }}=+24 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=8 \Omega, \mathrm{f}=1 \mathrm{kHz}$ (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Supply Voltage Range | $\mathrm{V}_{c c}$ |  | 8.0 | 24 | 26 | V |
| Quiescent Supply Current | $\mathrm{I}_{\text {cc }}$ | No signal applied | - | 80 | 120 | mA |
| Quiescent Output Voltage | $V_{4}$ | No signal applied | - | 12 | - | V |
| Open Loop Gain | $\mathrm{A}_{\text {e }}$ |  | - | 80 | - | dB |
| Closed Loop Gain | $\mathrm{A}_{\mathrm{e}}$ |  | 39.5 | 40 | 40.5 | dB |
| Total Harmonic Distortion | THD | $\mathrm{P}_{\text {oun }}=0.05$ to $3.5 \mathrm{~W}, \mathrm{R}_{\text {L }}=8 \Omega$ | - | 0.2 | - | \% |
|  |  | $\mathrm{P}_{\text {OUI }}=0.05$ to $5.0 \mathrm{~W}, \mathrm{R}_{\text {L }}=4 \Omega$ | - | 0.2 | - | \% |
| Audio Power Output | $\mathrm{P}_{\text {out }}$ | THD $=10 \%, \mathrm{R}_{1}=8 \Omega$ | - | 8.0 | - | W |
|  |  | THD $=10 \%, \mathrm{R}_{\perp}=4 \Omega$ | 10 | 12 | - | W |
| Input Impedance | $\mathrm{Z}_{1}$ |  | 70 | 150 | - | k $\Omega$ |
| Power Supply Rejection | PSRR | $\mathrm{f}_{\text {riple }}=120 \mathrm{~Hz}, \mathrm{~V}_{\text {dionle }}=0.5 \mathrm{~V}$ | 30 | 35 | - | dB |
| Equiv. Input Noise Voltage | $\mathrm{e}_{\mathrm{N}}$ | $\mathrm{f}=40 \mathrm{~Hz}$ to 15 kHz | - | 4.0 | - | $\mu \mathrm{V}$ |
| Equiv. Input Noise Current | $\mathrm{i}_{N}$ | $f=40 \mathrm{~Hz}$ to 15 kHz | - | 60 | - | pA |
| Input Sensitivity | $\mathrm{e}_{\text {in }}$ | $\mathrm{P}_{\text {OUI }}=0.5 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=4 \Omega$ | - | 15 | - | mV |
|  |  | $\mathrm{P}_{\text {Out }}=0.5 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=8 \Omega$ | - | 21 | - | mV |
|  |  | $\mathrm{P}_{\text {out }}=8.0 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=4 \Omega$ | - | 71 | - | mV |
| Input Saturation Voltage | $\mathrm{e}_{\text {in }}$ |  | 400 | 600 | - | $\mathrm{mV}_{\text {rms }}$ |
| Frequency Response ( -3 dB ) |  | $\mathrm{C}_{\mathrm{fb}}=0.039 \mu \mathrm{~F}, \mathrm{R}_{\mathrm{fb}}=39 \Omega$ | 40 | - | 15 k | Hz |
| Thermal Resistance | $\mathrm{R}_{\text {өл }}$ |  | - | - | 4.0 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

TEST CIRCUIT AND TYPICAL APPLICATION

TYPICAL LOW-COST APPLICATION


Dwg. No. A $-10,466 \mathrm{~A}$

OUTPUT POWER
AS A FUNCTION OF SUPPLY VOLTAGE


Dwg. No. A-11,409

## POWER DISSIPATION <br> AS A FUNCTION OF OUTPUT POWER



## TYPICAL D-C MOTOR DRIVE APPLICATIONS



TYPICAL MOTOR CONTROL CURVE



## ULN-3703Z / TDA2003 10-WATT AUDIO POWER AMPLIFIER

## FEATURES

- Low External Parts Count
- Low Distortion
- Class B Operation
- Short-Circuit Protected
- Thermal Overload Protected
- Low Noise
- High Output-Voltage Swing
- T0-220 Style Package

DESIGNED to drive low-impedance loads down to $1.6 \Omega$, Type ULN-3703Z / TDA2003 audio power amplifier is ideal for automotive radio, tape player, and CB applications and can deliver 15 W of audio in the bridge configuration or 5 W to 10 W single-ended.

Operating in the harsh automotive environment, this device is capable of withstanding high ambient temperatures, output overloads, and repeated power supply transient voltages without damage. It is protected against a-c/d-c short-circuits, polarity inversions, or open grounds.

Type ULN-3703Z/TDA2003 is supplied in a modified five-lead JEDEC Style TO-220 plastic package. The heat sink tab is at ground potential; no insulation is required. Lead forming for either vertical or horizontal mounting (suffix letter " V " or ' H ,', respectively) is standard.

These integrated circuits will be marked with their Pro-Electron registrations (TDA2003H or TDA2003V) unless U.S. part-number marking is specified on production orders.

## ABSOLUTE MAXIMUM RATINGS


Peak Supply Voltage ( 50 ms ) ........................ 40 V
Peak Output Current, $\mathrm{I}_{\text {out }}$. . . . . . . . . . . . . . . . . . . . . . 3.5 A
Non-Repetitive Peak Output Current . . . . . . . . . . . . . . . 4.5 A
Package Power Dissipation, $P_{D}$. . . . . . . . . . . . . . . . . 20 W*
Storage Temperature Range, $T_{s} \ldots . . . .-40^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=+14.4 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=4 \Omega, \mathrm{f}=1 \mathrm{kHz}$ (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Supply Voltage Range | $V_{c c}$ |  | 8.0 | - | 18 | V |
| Quiescent Supply Current | 1 lc | No signal applied | - | 44 | - | mA |
| Quiescent Output Voltage | $V_{4}$ | No signal applied | 6.1 | 6.9 | 7.7 | V |
| Open Loop Gain | $\mathrm{A}_{\mathrm{e}}$ |  | - | 80 | - | dB |
| Closed Loop Gain | $\mathrm{A}_{\text {e }}$ |  | 39.5 | 40 | 40.5 | dB |
| Total Harmonic Distortion | THD | $\mathrm{P}_{\text {out }}=0.05$ to 4.5 W | - | 0.15 | - | \% |
|  |  | $\mathrm{P}_{\text {out }}=0.05$ to $7.0 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | - | 0.15 | - | \% |
| Audio Power Output | Pout | THD $=10 \%$ | 5.5 | 6.0 | - | W |
|  |  | THD $=10 \%, \mathrm{R}_{\mathrm{L}}=3.2 \Omega$ | - | 7.5 | - | W |
|  |  | THD $=10 \%, \mathrm{R}_{\mathrm{l}}=2 \Omega$ | 9.0 | 10 | - | W |
|  |  | THD $=10 \%, \mathrm{R}_{\mathrm{L}}=1.6 \Omega$ | - | 12 | - | W |
| Efficiency | $\eta$ | $\mathrm{P}_{\text {out }}=6.0 \mathrm{~W}$ | - | 69 | - | \% |
|  |  | $\mathrm{P}_{\text {our }}=10 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | - | 65 | - | \% |
| Input Impedance | $\mathrm{Z}_{1}$ |  | 70 | 150 | - | $\mathrm{k} \Omega$ |
| Power Supply Rejection | PSR | $\mathrm{f}_{\text {fiple }}=120 \mathrm{~Hz} \mathrm{~V}_{\text {ippope }}=0.5 \mathrm{~V}$ | 30 | 36 | - | dB |
| Equiv, Input Noise Voltage | $\mathrm{e}_{\mathrm{N}}$ | $\mathrm{f}=22 \mathrm{~Hz}$ to 22 kHz | - | 1.0 | 5.0 | $\mu \mathrm{V}$ |
| Equiv. Input Noise Current | ${ }_{\text {N }}$ | $\mathrm{f}=22 \mathrm{~Hz}$ to 22 kHz | - | 60 | 200 | pA |
| Input Sensitivity | $e_{\text {in }}$ | $\mathrm{P}_{\text {out }}=0.5 \mathrm{~W}$ | - | 14 | - | mV |
|  |  | $\mathrm{P}_{\text {OUT }}=0.5 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | - | 10 | - | mV |
|  |  | $\mathrm{P}_{\text {our }}=6.0 \mathrm{~W}$ | - | 55 | - | mV |
|  |  | $\mathrm{P}_{\text {our }}=10 \mathrm{~W}, \mathrm{R}_{\mathrm{L}}=2 \Omega$ | - | 50 | - | mV |
| Input Saturation Voltage | $\mathrm{e}_{\text {in }}$ |  | 300 | - | - | mV |
| Frequency Response ( -3 dB ) |  | $\begin{aligned} & \mathrm{C}_{\text {fib }}=0.039 \mu \mathrm{~F}, \mathrm{R}_{\mathrm{ib}}=39 \Omega, \\ & \mathrm{P}_{\mathrm{out}}=1.0 \mathrm{~W} \end{aligned}$ | 40 | - | 15 k | Hz |
| Thermal Resistance | $\mathrm{R}_{\text {өा }}$ |  | - | - | 3.0 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |



## ULX-3777W DUAL 10-WATT AUDIO POWER AMPLIFIER



## Preliminary Information

## FEATURES

- High-Voltage Protection
- Operating Voltage Range: 8 to 18 V
- Thermal Shutdown
- Low Distortion
- Excellent Channel Separation
- Replacement for HA1377A

DELIVERING up to 10 watts per channel into low impedance loads, Type ULX-3777W is designed for the demanding domain of automobile stereo sound systems.

This monolithic integrated circuit carries built-in protection from temporary high voltages, automotive transients and excessive power dissipation.

An internal voltage regulator allows amplifier operation with power supply levels between 8.0 and 18 V . As supply voltages exceed that maximum, a protective circuit shuts down the device until the supply level falls below the 18 V limit.

Frequency response of Type ULX-3777W is flat from 40 Hz to 25 kHz . Channel separation is typically 58 dB .

Type ULX-3777W is supplied in a 12 -pin single in-line power tab plastic package that permits dissipation of up to 18 W .


The ULX prefix to the part number denotes an integrated circuit presently in development and undergoing engineering evaluation. If and when the device becomes a production item, the prefix will be changed to ULN. Sprague Electric assumes no obligation for future manufacture of any products presently in development unless such obligation is specifically undertaken in writing by authorized Sprague personnel.

ABSOLUTE MAXIMUM RATINGS
Supply Voltage, V Vc $_{\text {c }}$ (continueus) $\ldots \ldots \ldots . . .18 \mathrm{~V}$

## (30 s) <br> 26 V

(200 ms) ..... 50 V

Output Current, $I_{0}$
4.5 A Package Power Dissipation, $\mathrm{P}_{\mathrm{D}} \ldots .$. . . .... $18 \mathrm{~W}^{*}$ Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots .-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$

[^46]ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+\mathbf{2 5}{ }^{\circ} \mathrm{C}$,
$V_{\text {cC }}=13.2 \mathrm{~V}, \mathrm{~V}_{\text {in }}=2.45 \mathrm{mV}, f=1 \mathrm{kHz}, \mathrm{R}_{\mathrm{L}}=4 \Omega$,
Any One Amplifier (unless otherwise specified)

| Characteristic | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. | Units |
| Quiescent Supply Current | $V_{\text {in }}=0$ | - | 80 | 160 | mA |
| Input Bias Voltage | $\mathrm{V}_{\text {in }}=0$ | - | - | 40 | mV |
| Input Resistance |  | - | 30 | - | k $\Omega$ |
| Voltage Gain |  | 53 | 55 | 57 | dB |
| Differential Volt. Gain |  | - | - | 1.5 | dB |
| Audio Power Output | $\mathrm{R}_{\mathrm{L}}=4 \Omega, \mathrm{~V}_{\text {CC }}=13.2 \mathrm{~V}, \mathrm{THD}=10 \%$, Note 1 | 5.0 | 5.8 | - | W |
|  | $R_{L}=4 \Omega, V_{C C}=14.4 \mathrm{~V}, \mathrm{THD}=10 \%$, Note 1 | - | 7.0 | - | W |
|  | $\mathrm{R}_{\mathrm{L}}=2 \Omega, \mathrm{~V}_{\text {CC }}=13.2 \mathrm{~V}, \mathrm{THD}=10 \%$, Note 1 | - | 9.0 | - | W |
|  | $\mathrm{R}_{\mathrm{L}}=2 \Omega, \mathrm{~V}_{C C}=14.4 \mathrm{~V}, \mathrm{THD}=10 \%$, Note 1 | - | 10 | - | W |
| Total Harmonic Distortion | $\mathrm{P}_{0}=500 \mathrm{~mW}$ | - | 0.15 | 1.0 | \% |
| Noise Output | $\mathrm{R}_{\mathrm{S}}=10 \mathrm{k} \Omega, \mathrm{BW}=20 \mathrm{~Hz}$ to 20 kHz | - | - | 2.0 | mV |
| Channel Separation | $\mathrm{R}_{\mathrm{S}}=600 \Omega, \mathrm{f}=500 \mathrm{~Hz}$ | 40 | 58 | - | dB |
| Rolloff Frequency | $\mathrm{f}_{\mathrm{L}}$ at -3 dB ref. 1 kHz | - | 40 | - | Hz |
|  | $\mathrm{f}_{\mathrm{H}}$ at -3 dB ref. 1 kHz | - | 25 | - | kHz |
| Power Supply Rejection | $\mathrm{R}_{\mathrm{S}}=600 \mathrm{~S}, \mathrm{f}=500 \mathrm{~Hz}$ | 30 | 40 | - | dB |

Note 1: $V_{\text {in }}$ increased until THD $=10 \%$.

## TEST CIRCUIT AND TYPICAL APPLICATION



DWG.NO. A-11,373

# ULX-3788W <br> 20-WATT AUDIO POWER AMPLIFIER 

## FEATURES

- Operating Voltage Range: 8 to 18 V
- Short Circuit Protected - Outputs and Speaker
- High-Voltage Protection
- Thermal Shutdown
- Minimal External Circuitry
- Low Distortion
- Replacement for HA1388

DEVELOPED to meet demanding performance standards in automotive applications, this monolithic integrated circuit offers high-power, low-noise, low-distortion audio with a minimum of external circuitry.

When used in automobile sound systems, Sprague Type ULX-3788W delivers up to 18 W of output power to a $4 \Omega$ load and up to 11 W into an $8 \Omega$ load impedance. Audio output of 20 W is available with higher levels of supply voltage.

The amplifier's frequency response is flat from 20 Hz to 25 kHz .

Type ULX-3788W has built-in protection against damage by automotive transients, temporary surges in supply voltage and excessive power dissipation levels. Its internal voltage regulator ensures stable operation with variations in supply voltage ( 8 to 18 V ) and temperature $\left(-20^{\circ} \mathrm{C}\right.$ to $\left.+85^{\circ} \mathrm{C}\right)$.

The audio amplifier is supplied in a 12 -pin single in-line plastic package with a power dissipation rating of 18 W .


The ULX prefix to the part number denotes an integrated dircuit presently in development and undergoing engineering evaluation. If and when the device becomes a production item, the prefix will be changed to ULN. Sprague Electric assumes no obligation for future manufacture of any products presently in development unless such obligation is specifically undertaken in writing by authorized Sprague personnel


| ABSOLUTE MAXIMUM RATINGS <br> ${ }^{*}$ Derate at the rate of $3^{\circ} \mathrm{C} / \mathrm{W}$ above $\mathrm{T}_{\mathrm{TAB}}=+70^{\circ} \mathrm{C}$ |
| :---: |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=13.2 \mathrm{~V}$, $f=1 \mathrm{kHz}, \mathrm{R}_{\mathrm{L}}=4 \Omega$ (unless otherwise specified)

| Characteristic | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. | Units |
| Quiescent Supply Current | $V_{\text {in }}=0$ | 40 | 80 | 160 | mA |
| Input Bias Voltage | $V_{\text {in }}=0$ | - | 20 | 40 | mV |
| Input Resistance |  | 20 | 30 | 40 | k $\Omega$ |
| Voltage Gain | $\mathrm{V}_{\mathrm{in}}=2.45 \mathrm{mV}$ | - | 55 | - | dB |
| Audio Power Output | $R_{L}=4 \Omega$, THD $=10 \%$ | 15 | 18 | - | W |
|  | $\mathrm{R}_{\mathrm{L}}=8 \Omega, \mathrm{THD}=10 \%$ | - | 11 | - | W |
| Output Offset Voltage | $V_{\text {in }}=0$ | - | - | 330 | mV |
| Total Harmonic Distortion | $P_{0}=1.5 \mathrm{~W}$ | - | 0.2 | 1.0 | \% |
| Noise Output | $\mathrm{R}_{\mathrm{s}}=10 \mathrm{k} \Omega, \mathrm{BW}=20 \mathrm{~Hz}$ to 20 kHz | - | 1.0 | 2.0 | mV |
| Rolloff Frequency | $\mathrm{f}_{\mathrm{L}}$ at -3 dB ref. 1 kHz | - | 20 | - | Hz |
|  | $\mathrm{f}_{\mathrm{H}}$ at -3 dB ref. 1 kHz | - | 25 | - | kHz |
| Power Supply Rejection | $\mathrm{f}=500 \mathrm{~Hz}$ | 33 | 44 | - | dB |

## TEST CIRCUIT <br> AND TYPICAL APPLICATION



Dwg. No. A-11,371

BIMOS AND COMPLEX ARRAY INTERFACE DRIVERS

INDUSTRIAL, MILITARY, AND AEROSPACE DEVICES

## RADIO INTEGRATED CIRCUITS

TELEVISION INTEGRATED CIRCUITS

AUDIO INTEGRATED CIRCUITS

HALL EFFECT DEVICES

TRANSISTOR ARRAYS AND MISCELLANEOUS DEVICES

## CUSTOM DEVICES

$\square$

## SECTION 9 - hall effect devices

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UGN-3013T/U Ultra Low-Cost Digital Switch ..... 9-3
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Hall Effect Integrated Circuit Application Guide ..... 9-27

## SELECTION GUIDE TO HALL EFFECT DEVICES

| Device Type | Switch Points (Gauss) |  | Outputs |
| :---: | :---: | :---: | :---: |
| UGN-3013T/U | 225 | 300 | 1 |
| UGN/UGS-3019T/U | 300 | 420 | 1 |
| UGN/UGS-3020T/U | 165 | 220 | 1 |
| UGN/UGS-3030T/U | 110 | 160 | 1 |
| UGN-3040T/U | 100 | 150 | 1 |
| UGN-3201M | 300 | 450 | 2 |
| UGN-3203M | 100 | 235 | 2 |
| UGN-3220S | 160 | 220 | 2 |
| UGN-3501M | Linear |  | Push-Pull |
| UGN-3501T/U | Linear |  | 1 |
| UGN-3604M | Linear | Push-Pull |  |
| UGN-3605M | Linear |  | Push-Pull |

NOTE: Information on UGN-3075T, UGS-3075T, UGN-3075U, UGS-3075U, UGN-3076T, UGS-3076T, UGN-3076U, and UGS-3076U, bipolar latching circuits, is available from the Semiconductor Division, Concord, N.H.

## UGN-3013T SOLID-STATE ULTRA LOW-COST HALL EFFECT DIGITAL SWITCHES

## FEATURES

- Operate from 4.5 V to 16 V D-C Power Source
- Activates With Small, Commercially Available Permanent Magnets
- Solid-State Reliability - No Moving Parts
- Small Size
- Constant Amplitude Output
- Output Compatible With All Digital Logic Families

THE SPRAGUE TYPE UGN-3013T is a low-cost magnetically-activated electronic switch. Each device consists of a voltage regulator, a Hall voltage generator, amplifier, Schmitt trigger, and an open collector output stage integrated in a single monolithic silicon chip.

The on-board regulator permits operation over a wide variation of supply voltages. The circuit output can be interfaced directly with bipolar or MOS logic circuits.

UGN-3013T integrated circuits are packaged in the miniature 3-pin single output plastic " T " pack.


## ABSOLUTE MAXIMUM RATINGS

| Power Supply, $\mathrm{V}_{\text {cc }}$ | 17 V |
| :---: | :---: |
| Magnetic Flux Density, B | Unlimited |
| Output "OFF" Voltage, $\mathrm{V}_{\text {out(off) }}$ | 17 V |
| Output "ON" Current, $\mathrm{I}_{\text {SINK }}$ | 25 mA |
| Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS at $\mathbf{V}_{\mathrm{CC}}=4.5 \mathrm{~V}$ to $16 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Magnetic Flux Density "Operate Point" "Release Point" | $\mathrm{B}_{0 \text { p }}$ |  | - | 300 | 450 | Gauss |
|  | $\mathrm{B}_{\text {RP }}$ |  | 25 | 225 | - | Gauss |
| Hysteresis | $\mathrm{B}_{\mathrm{H}}$ |  | 30 | 75 | - | Gauss |
| Output Saturation Voltage | $V_{\text {SAT }}$ | $B \geq 450$ Gauss, $\mathrm{I}_{\text {SINK }}=15 \mathrm{~mA}$ | - | 120 | 400 | mV |
| Output Leakage Current | $\mathrm{I}_{\text {OfF }}$ | $\mathrm{B} \leq 25$ Gauss, $\mathrm{V}_{\text {out }}=16 \mathrm{~V}$ | - | . 1 | 20 | $\mu \mathrm{A}$ |
| Supply Current | $\mathrm{I}_{\text {c }}$ | $V_{C C}=5 \mathrm{~V}$, output open | - | 7 | 9 | mA |
|  |  | $\mathrm{V}_{\mathrm{cc}}=12 \mathrm{~V}$, output open | - | 12 | 16 | mA |
| Output Rise Time | $\mathrm{t}_{\mathrm{r}}$ | $\begin{aligned} & V_{C E}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=820 \Omega, \\ & C_{\mathrm{L}}=20 \mathrm{pF} \end{aligned}$ | - | 15 | - | ns |
| Output Fall Time | $\mathrm{t}_{\text {f }}$ | $\begin{aligned} & V_{c C}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=820 \Omega, \\ & C_{L}=20 \mathrm{pF} \end{aligned}$ | - | 100 | - | ns |

## OPERATION

The output transistor is normally 'off', when the magnetic field perpendicular to the surface of the chip is below the threshold or "operate point." When the field exceeds the "operate point," the output transistor switches "on'" and is capable of sinking 25 mA of current.

The output transistor switches "off"' when the magnetic field is reduced below the "release point", which is less than the "operate point." This is illustrated graphically in the transfer characteristics curve. The hysteresis characteristic provides for unambiguous or non-oscillatory switching.

The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located and $0.032^{\prime \prime} \pm 0.002^{\prime \prime}(0.81 \pm 0.05 \mathrm{~mm})$ below the branded surface of the T package and $0.012^{\prime \prime} \pm 0.002^{\prime \prime}(0.30 \pm 0.05 \mathrm{~mm})$ below the branded surface of the $U$ package.

For reference purposes, both an Alnico VIII magnet, $0.212^{\prime \prime}(5.38 \mathrm{~mm})$ in diameter and $0.187^{\prime \prime}$ ( 4.75 mm ) long and a samarium cobalt magnet, $0.100^{\prime \prime}(2.54 \mathrm{~mm})$ square and $0.040^{\prime \prime}(1.02 \mathrm{~mm})$ thick, are approximately 1200 gauss at its surface.

The flux density decays at a high rate as the distance from a pole increases.

As an example, using the Alnico VIII magnet referenced above in good alignment and the pole surface in contact with the branded surface of the package, the flux density at the active Hall sensing area of the device would be approximately 850 gauss.

The flux density would drop to approximately 600 gauss with an air-gap between the package and the magnet of $0.031^{\prime \prime}(0.79 \mathrm{~mm})$.

## TRANSFER CHARACTERISTICS SHOWING HYSTERESIS



Dwg. No. A-11,003

These Hall effect devices are also available in a miniature 3-pin plastic ' $U$ '" package. The ' $T$ '' package is 0.080 ' ( 2.03 mm ) thick; the ' $U$ '" package is $0.061^{\prime \prime}$ (1.54 mm) thick. All other dimensions are identical.

## UGN-3019T and UGS-3019T SOLID-STATE LOW-COST HALL EFFECT DIGITAL SWITCHES

## FEATURES

- Operate from 4.5 V to 16 V D-C Power Source
- Operable With a Small Permanent Magnet
- High Reliability - Eliminates Contact Wear, Contact Bounce
- No Moving Parts
- Small Size
- Constant Amplitude Output
- Output Compatible With All Digital Logic Families

THE TYPE UGN-3019T and UGS-3019T are lowcost magnetically-activated electronic switches utilizing the Hall effect for sensing a magnetic field. Each circuit consists of a voltage regulator, Hall cell, signal amplifier, Schmitt trigger, and current sinking output stage integrated into a monolithic silicon chip.

The circuit output can be interfaced directly with bipolar or MOS logic circuits. The on-board regulator insures stable operation over a wide range of supply voltages. Operation over an extended temperature range is made possible by the careful matching of components which can be done economically only on a monolithic chip.

These devices are packaged in the 3-pin single output plastic " $T$ " package.

The UGN-3019T was originally introduced as the ULN-3006T.


## abSolute maximum ratings

Power Supply, $V_{c c}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . 25 V
Magnetic Flux Density, B . . . . . . . . . . . . . . . . . . . . Unlimited
Output "OFF" Voltage, $\mathrm{V}_{\text {outioff }}$. . . . . . . . . . . . . . . . . . . . . 20 V

Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots . . . .5^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Temperature Range, $T_{A}$
UGS-3019T $T_{A}$
UGN-3019T
$-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
-
ELECTRICAL CHARACTERISTICS at $\mathrm{V}_{\mathrm{CC}}=4.5 \mathrm{~V}$ to $16 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Magnetic Flux Density "Operate Point" "Release Point" | $\mathrm{B}_{0}$ |  |  | 420 | 500 | Gauss |
|  | $B_{\text {RP }}$ |  | 100 | 300 | - | Gauss |
| Hysteresis | $\mathrm{B}_{\mathrm{H}}$ |  | 50 | 120 | - | Gauss |
| Output Saturation Voltage | $\mathrm{V}_{\text {SII }}$ | $\mathrm{B} \geq 500$ Gauss, $\mathrm{I}_{\text {smu }}=15 \mathrm{~mA}$ | - | 150 | 400 | mV |
| Output Leakage Current | $\mathrm{I}_{\text {off }}$ | $\mathrm{B} \leq 100$ Gauss, $\mathrm{V}_{\text {ort }}=16 \mathrm{~V}$ | - | 1 | 20 | $\mu \mathrm{A}$ |
| Supply Current | $\mathrm{I}_{\mathrm{cc}}$ | $\mathrm{V}_{\text {cc }}=5 \mathrm{~V}$, output open | - | 7 | 9 | mA |
|  |  | $\mathrm{V}_{\mathrm{cc}}=12 \mathrm{~V}$, output open | - | 12 | 16 | mA |
| Output Rise Time | $\mathrm{t}_{\text {t }}$ | $\begin{aligned} & V_{c c}=12 \mathrm{~V}, R_{\mathrm{L}}=820 \Omega, \\ & C_{\mathrm{L}}=20 \mathrm{pF} \end{aligned}$ | - | 15 | - | ns |
| Output Fall Time | $t_{\text {t }}$ | $\begin{aligned} & V_{c c}=12 \mathrm{~V}, R_{L}=820 \Omega, \\ & C_{L}=20 \mathrm{pF} \end{aligned}$ | - | 100 | - | ns |

[^47]
## OPERATION

The output transistors are normally "off', when the magnetic field perpendicular to the surface of the chip is below the threshold or "operate point." When the field exceeds the "operate point," each output transistor switches "on" and is capable of sinking 25 mA of current. Selections to 50 mA are available.

The output transistors switch "off" when the magnetic field is reduced below the "release point" (which is less than the "operate point"). This is illustrated graphically in the transfer characteristics curve. The hysteresis characteristic provides for unambiguous or non-oscillatory switching.

The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located and $0.032^{\prime \prime} \pm 0.002^{\prime \prime}(0.81 \pm 0.05 \mathrm{~mm})$ below the branded surface of the T package and $0.012^{\prime \prime} \pm 0.002^{\prime \prime}(0.30 \pm 0.05 \mathrm{~mm})$ below the branded surface of the $U$ package.

For reference purposes, both an Alnico VIII magnet, $0.212^{\prime \prime}(5.38 \mathrm{~mm})$ in diameter and $0.187^{\prime \prime}$

TRANSFER CHARACTERISTICS SHOWING HYSTERESIS

( 4.75 mm ) long and a samarium cobalt magnet, $0.100^{\prime \prime}(2.54 \mathrm{~mm})$ square and $0.040^{\prime \prime}(1.02 \mathrm{~mm})$ thick, are approximately 1200 gauss at its surface.

The flux density decays at a high rate as the distance from a pole increases.

As an example, using the Alnico VIII magnet referenced above in good alignment and the pole surface in contact with the branded surface of the package, the flux density at the active Hall sensing area of the device would be approximately 850 gauss.

The flux density would drop to approximately 600 gauss with an air-gap between the package and the magnet of $0.031^{\prime \prime}(0.79 \mathrm{~mm})$.

Switching point variations with temperature should be considered in applications covering a wide temperature range.


## UGN-3020T and UGS-3020T SOLID-STATE LOW-COST HALL EFFECT DIGITAL SWITCHES

## FEATURES

- Operate from 4.5 V to 24 V D-C Power Source
- Operable With a Small Permanent Magnet
- High Reliability - Eliminates Contact Wear, Contact Bounce
- No Moving Parts
- Small Size
- Constant Amplitude Output
- Output Compatible With All Logic Families

T'HE TYPE UGN-3020T and UGS-3020T are lowcost magnetically-activated electronic switches utilizing the Hall effect for sensing a magnetic field. Each circuit consists of a voltage regulator, Hall cell, signal amplifier, Schmitt trigger, and current sinking output stage integrated in a single monolithic silicon chip.

The on-board regulator permits stable operation over a wide variation of supply voltages. Operation over an extended temperature range is made possible by the careful matching of components which can be done economically only on a monolithic circuit.

Both devices will typically operate up to a 100 kHz repetition rate.

The circuit output can be interfaced directly with bipolar or MOS logic circuits.


These devices are packaged in the 3-pin single output plastic " $T$ " pack.
These devices were originally introduced with ULN and ULS prefixes.

ABSOLUTE MAXIMUM RATINGS

| Power Supply, $\mathrm{V}_{\text {cc }}$ | V |
| :---: | :---: |
| Magnetic Flux Density, B. | Unlimited |
| Output "OFF" Voltage, $\mathrm{V}_{\text {outioff }}$ | 25 V |
| Output "ON" Current, $\mathrm{I}_{\text {SINK }}$ | 25 mA |
| Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ | $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range, $\mathrm{T}_{A}$ |  |
| UGS-3020T | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| UGN-3020T | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS at $\mathrm{V}_{\mathrm{CC}}=4.5 \mathrm{~V}$ to $24 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Magnetic Flux Density "Operate Point" "Release Point" | $\mathrm{B}_{\text {®p }}$ |  | - | 220 | 350 | Gauss |
|  | $\mathrm{B}_{\text {RP }}$ |  | 50 | 165 | - | Gauss |
| Hysteresis | $\mathrm{B}_{\mathrm{H}}$ |  | 20 | 55 | - | Gauss |
| Output Saturation Voltage | $\mathrm{V}_{\text {SAT }}$ | $\mathrm{B} \geq 350$ Gauss, $\mathrm{I}_{\text {SINK }}=15 \mathrm{~mA}$ | - | 85 | 400 | mV |
| Output Leakage Current | $\mathrm{I}_{\text {Off }}$ | $\mathrm{B} \leq 50$ Gauss, $\mathrm{V}_{\text {out }}=24 \mathrm{~V}$ | - | 0.1 | 20 | $\mu \mathrm{A}$ |
| Supply Current | $\mathrm{I}_{\text {c }}$ | $\mathrm{V}_{\text {cc }}=4.5 \mathrm{~V}$, output open | - | 5 | 9 | mA |
|  |  | $\mathrm{V}_{\text {cc }}=24 \mathrm{~V}$, output open | - | 6 | 14 | mA |
| Output Rise Time | $\mathrm{t}_{1}$ | $\begin{aligned} & V_{c \mathrm{C}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=820 \Omega, \\ & \mathrm{C}_{\mathrm{L}}=20 \mathrm{pF} \end{aligned}$ | - | 15 | - | ns |
| Output Fall Time | $t_{\text {f }}$ | $\begin{aligned} & V_{c C}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=820 \Omega, \\ & C_{L}=20 \mathrm{pF} \end{aligned}$ | - | 100 | - | ns |

## OPERATION

The output transistor is normally "off"' when the magnetic field perpendicular to the surface of the chip is below the threshold or "operate point." When the field exceeds the "operate point," the output transistor switches "on"" and is capable of sinking 25 mA of current. Selections to 50 mA are available.

The output transistor switches "off" when the magnetic field is reduced below the "release point" which is less than the "operate point." This is illustrated graphically in the transfer characteristics curve. The hysteresis characteristic provides for unambiguous or non-oscillatory switching.

The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located and $0.032^{\prime \prime} \pm 0.002^{\prime \prime}(0.81 \pm 0.05 \mathrm{~mm})$ below the branded surface of the $T$ package and $0.012^{\prime \prime} \pm 0.002^{\prime \prime}(0.30 \pm 0.05 \mathrm{~mm})$ below the branded surface of the U package.

For reference purposes, both an Alnico VIII magnet, $0.212^{\prime \prime}(5.38 \mathrm{~mm})$ in diameter and $0.187^{\prime \prime}$

## SWITCHING POINT VARIATION WITH TEMPERATURE


( 4.75 mm ) long and a samarium cobalt magnet, $0.100^{\prime \prime}(2.54 \mathrm{~mm})$ square and $0.040^{\prime \prime}(1.02 \mathrm{~mm})$ thick, are approximately 1200 gauss at the pole surfaces.

The flux density decays at a high rate as the distance from a pole increases.

As an example, using the Alnico VIII magnet referenced above in good alignment and the pole surface in contact with the branded surface of the package, the flux density at the active Hall sensing area of the device would be approximately 850 gauss.

The flux density would drop to approximately 600 gauss with an air-gap between the package and the magnet of $0.031^{\prime \prime}(0.79 \mathrm{~mm})$.

Note: Switching point variations with temperature should be considered in applications covering a wide temperature range.

TRANSFER CHARACTERISTICS SHOWING HYSTERESIS


Dwg. No. A-11, 010

These Hall effect devices are also available in a miniature 3-pin plastic ' $U$ " package. The ' $T$ "' package is 0.080 ' ( 2.03 mm ) thick; the " $U$ " package is $0.061^{\prime \prime}(1.54 \mathrm{~mm})$ thick. All other dimensions are identical.

# UGN-3030T and UGS-3030T LOW-COST BIPOLAR HALL EFFECT DIGITAL SWITCHES 

## FEATURES

- Operable With Inexpensive Multi-Pole Ring Magnets
- High Reliability - Eliminates Contact Wear, Contact Bounce
- No Moving Parts
- Small Size
- Constant Amplitude Output - Compatible With All Digital Logic Families

TYPE UGN-3030T and UGS-3030T solid-state switches are designed for use with inexpensive multi-pole ring magnets. Both switches operate within the magnetic field range of +250 to -250 Gauss.

The UGN-3030T operates over the temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ with supply voltages $\left(\mathrm{V}_{\mathrm{CC}}\right)$ of 4.5 to 24 V .

The UGS-3030T, intended for more severe automotive environments, operates from $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.

Circuit output can be interfaced directly with bipolar or MOS logic circuits. These switches provide a constant amplitude output at frequencies to 100 MHz .

Type UGN-3030T and UGS-3030T switches are supplied in a rugged 3-pin plastic ' $T$ ' pack.


## ABSOLUTE MAXIMUM RATINGS

Power Supply, $\mathrm{V}_{c c}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . 25 V Magnetic Flux Density, B . . . . . . . . . . . . . . . . . . . Unlimited
Output off Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . 25 V
Output on Current, $\mathrm{I}_{\text {SNK }}$. . . . . . . . . . . . . . . . . . . . . 25 mA
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ Operating Temperature Range, $T_{A}$

| UGN-3030T | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| :---: | :---: |
| UGS-3030T | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |

These Hall effect devices are also available in a miniature 3-pin plastic ' $U$ '" package. The ' $T$ "' package is 0.080 " ( 2.03 mm ) thick; the ' $U$ "' package is $0.061^{\prime \prime}(1.54 \mathrm{~mm})$ thick. All other dimensions are identical.

ELECTRICAL CHARACTERISTICS at $\mathrm{V}_{C c}=4.5 \mathrm{~V}$ to $24 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ (UGN-3030T) at $V_{C C}=4.5 \mathrm{~V}$ to $24 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ (UGS-3030T)

| Characteristic | Symbol | Test Conditions | Min. | Typ. | Max. | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| "Operate Point"* | $\mathrm{B}_{0}$ |  | - | 160 | 250 | Gauss |
| "Release Point" | $\mathrm{B}_{\text {Rp }}$ |  | -250 | 110 | - | Gauss |
| Hysteresis | $\mathrm{B}_{H}$ |  | 20 | 50 | - | Gauss |
| Output Saturation Voltage | $V_{\text {SAT }}$ | $B \geqslant 250$ Gauss, $\mathrm{I}_{\text {SNK }}=15 \mathrm{~mA}$ | - | 85 | 400 | mV |
| Output Leakage Current | $\mathrm{I}_{\text {Of }}$ | $B \leqslant-250$ Gauss | - | 0.1 | 20 | $\mu \mathrm{A}$ |
| Supply Current | $I_{c c}$ | $\mathrm{V}_{\text {cc }}=4.5 \mathrm{~V}$, output open | - | 4.5 | 9 | mA |
|  |  | UGN-3030T $\mathrm{V}_{\text {cC }}=16 \mathrm{~V}$, output open | - | 5.5 | 12 | mA |
|  |  | UGS-3030T $\mathrm{V}_{\text {cc }}=24 \mathrm{~V}$, output open | - | 6 | 13 | mA |
| Output Rise Time | $\mathrm{t}_{\mathrm{f}}$ | $\mathrm{V}_{\text {cc }}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=820 \Omega, \mathrm{C}_{\mathrm{L}}=20 \mathrm{pF}$ | - | 15 | - | ns |
| Output Fall Time | $\mathrm{t}_{\mathrm{f}}$ | $\mathrm{V}_{\mathrm{cc}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=820 \Omega, \mathrm{C}_{\mathrm{L}}=20 \mathrm{pF}$ | - | 100 | - | ns |

[^48]
## OPERATION

The output transistor is normally off when the magnetic field perpendicular to the surface of the chip is below the threshold or "operate point." When the field exceeds the "operate point," the output transistor switches on and is capable of sinking 25 mA of current. Selections to 50 mA are available.

The output transistor switches off when the magnetic field is reduced below the "release point" which is less than the 'operate point.' 'This is illustrated graphically in the transfer characteristics curve. The hysteresis characteristic provides for unambiguous or non-oscillatory switching.

TRANSFER CHARACTERISTICS SHOWING HYSTERESIS


The simplest form of magnet which will operate the Hall effect bipolar digital switch is a multiple pole ring magnet as shown. Such magnets are commercially available and are quite inexpensive.

The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located and $0.032^{\prime \prime} \pm 0.002^{\prime \prime}(0.81 \pm 0.05 \mathrm{~mm})$ below the top surface of the T package and $0.012^{\prime \prime}$ $\pm 0.002^{\prime \prime}(0.30 \pm 0.05 \mathrm{~mm})$ below the top surface of the U package. The magnetic circuit must provide a +250 Gauss to -250 Gauss magnetic flux density range at this point for all conditions to insure reliable operation; + Gauss indicates the South pole is toward the branded face of the package; - Gauss indicates the North pole is toward the branded package face.


BASIC MODES OF ACTIVATION USING A MULTIPLE-POLE RING MAGNET

[^49]
## UGN-3040T

## ULTRA-SENSITIVE HALL EFFECT DIGITAL SWITCHES

## FEATURES

- Operate from 4.5 V to 24 V D-C Power Source
- Operable With Small Permanent Magnets
- Solid-State Reliability - No Moving Parts
- Small Size
- Constant Amplitude Output
- Output Compatible With All Digital Logic Families

TTHE SPRAGUE TYPE UGN-3040T is a magnetically-activated electronic switch with extreme sensitivity for use with small, inexpensive magnets, or with relatively large magnet-toswitch distances.

Each circuit consists of a voltage regulator, Hall voltage generator, signal amplifier, Schmitt trigger circuit, and an open collector output driver integrated in a single silicon chip.

The on-board regulator permits operation over a wide range of supply voltages. Circuit output can be interfaced directly with bipolar or MOS logic circuits, and will typically operate up to a 100 kHz repetition rate.

The UGN-3040T is packaged in a miniature 3-pin single-output plastic " $T$ " pack.


## ABSOLUTE MAXIMUM RATINGS

Power Supply, VCC . . . . . . . . . . . . . . . . . . . . . . . . 25 V
Magnetic Flux Density, B. . . . . . . . . . . . . . . . . Unlimited
Output "OFF" Voltage, Vout(OFF) . ..................... . 25 V
Output "ON" Current, ISINK ...................... 25 mA
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots \ldots .0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS at $\mathrm{V}_{\mathrm{CC}}=4.5 \mathrm{~V}$ to $24 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Magnetic Flux Density "Operate Point" | $\mathrm{B}_{0}$ |  | - | 150 | 200 | Gauss |
| "Release Point" | Brp |  | 50 | 100 | - | Gauss |
| Hysteresis | $\mathrm{B}_{\mathrm{H}}$ |  | 20 | 50 | - | Gauss |
| Output Saturation Voltage | $V_{\text {SAT }}$ | $B \geq 200$ Gauss, $\mathrm{I}_{\text {SINK }}=20 \mathrm{~mA}$ | - | 85 | 400 | mV |
| Output Leakage Current | Ioff | $\mathrm{B} \leq 50$ Gauss, $\mathrm{V}_{\text {OUT }}=24 \mathrm{~V}$ | - | 0.1 | 20 | $\mu \mathrm{A}$ |
| Supply Current | $\mathrm{I}_{\text {CC }}$ | $\mathrm{V}_{C C}=4.5 \mathrm{~V}$, output open | - | 5 | 9 | mA |
|  |  | $\mathrm{V}_{\text {CC }}=24 \mathrm{~V}$, output open | - | 6 | 14 | mA |
| Output Rise Time | $\mathrm{t}_{\mathrm{r}}$ | $\begin{aligned} & V_{C C}=12 \mathrm{~V}, R_{L}=820 \Omega \\ & C_{L}=20 \mathrm{pF} \end{aligned}$ | - | 15 | - | ns |
| Output Fall Time | $\mathrm{t}_{\mathrm{f}}$ | $\begin{aligned} & V_{C C}=12 \mathrm{~V}, R_{L}=820 \Omega, \\ & C_{L}=20 \mathrm{pF} \end{aligned}$ | - | 100 | - | ns |

## GUIDE TO INSTALLATION

1. All Hall effect integrated circuits are susceptible to mechanical stress effects. Caution should be exercised to minimize the application of stress to the leads or the epoxy package.
2. To prevent permanent damage to the Hall cell, heat sink the leads during hand soldering. For wave soldering, the part should not experience more than $230^{\circ} \mathrm{C}$ for more than five seconds and solder should be no closer than $0.125^{\prime \prime}$ to the epoxy package.

## SWITCHING POINT AS A FUNCTION OF TEMPERATURE



These Hall effect devices are also available in a miniature 3-pin plastic " $U$ '" package. The ' $T$ "' package is 0.080 ' ( 2.03 mm ) thick; the " $U$ "' package is $0.061^{\prime \prime}$ (1.54 mm) thick. All other dimensions are identical.

## OPERATION

The simplest form of magnet which will operate the Hall Effect digital sensor is a bar magnet as shown. Other methods are possible.

In the illustration, the magnet's axis is on the center line of the packaged device and the magnet is moved toward and away from the device. Also, note the orientation of the magnet's south pole in relation to the branded face of the package.


Dwg. No. A-11, 200
basic 'head.on' mode of operation

TRANSFER CHARACTERISTICS SHOWING HYSTERESIS



## OPERATION (Continued)

The output transistor is normally 'off"' when the magnetic field perpendicular to the surface of the chip is below the threshold or "operate point." When the field exceeds the "operate point," the output transistor switches "on"' and is capable of sinking 25 mA of current. A 50 mA unit is available upon special order.

The output transistor switches "off" when the magnetic field is reduced below the "release point" which is less than the "operate point." This is illustrated graphically in the transfer characteristics curve. The hysteresis characteristic provides for unambiguous or nonoscillatory switching.

The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located $0.032^{\prime \prime} \pm 0.005^{\prime \prime} \quad$ ( 0.81 $\pm 0.127 \mathrm{~mm}$ ) below the branded surface of the T package and $0.012 \pm 0.005^{\prime \prime}(0.30 \pm 0.127 \mathrm{~mm})$ below the branded surface of the $U$ package.

A variety of magnets are commercially available, each exhibiting unique field characteristics. The curves presented below are flux density values for the magnets measured for switch activation in a head-on mode (along the magnet axis). The curves are also pertinent for peak flux density for a given clearance in the slide-by mode of actuation.

FLUX DENSITY AS A FUNCTION OF AIR GAP


## UGN-3201M and UGN-3203M DUAL OUTPUT HALL EFFECT DIGITAL SWITCHES

## FEATURES

- Operate from 5 V to 16 V D-C Power Supply
- Operate With a Small Permanent Magnet
- High Reliability - No Contact Wear or Bounce
- Small Size - 8-Pin DIP
- Constant Amplitude Output
- Dual Open-Collector Outputs

INTENDED for use in position sensing and contactless switching applications, the Types UGN3201 M and UGN-3203M switches utilize the Hall Effect for detecting a magnetic field.

Both devices feature identical electrical and environmental characteristics. However, the UGN3201 M has a typical Operate Point of 450 gauss and Release Point of 300 gauss; the UGN-3203M is more sensitive, with a typical Operate Point of 235 gauss and Release Point of 100 gauss. The UGN3203M may be activated by smaller magnets, or at a greater magnet-device spacing.

The UGN-3201M and UGN-3203M Hall Effect digital switches are supplied in 8-pin dual in-line plastic packages. These switches were originally introduced as device numbers ULN-3006M and ULN-3007M, respectively.


FUNCTIONAL BLOCK DIAGRAM

## abSOLUTE MAXIMUM RATIMGS

Power Supply, $V_{c c}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20 V
Magnetic Flux Density, B . . . . . . . . . . . . . . . . . . . . Unlimited
Output "OFF" Voltage, V $_{\text {ourroff }}$. . . . . . . . . . . . . . . . . . . . . 20 V
Output "ON" Current, I $_{\text {SINK }}$. . . . . . . . . . . . . . . . . . . . . . 25 mA
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots 0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS at $\mathbf{V}_{C C}=12$ VDC, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| "Operate Point" | Bop | UGN-3201M | - | 450 | 750 | Gauss |
| "Release Point" | $\mathrm{B}_{\text {RP }}$ | UGN-3201M | 100 | 300 | - | Gauss |
| Hysteresis | $\mathrm{B}_{\mathrm{H}}$ | UGN-3201M | - | 150 | - | Gauss |
| "Operate Point" | $\mathrm{B}_{\text {OP }}$ | UGN-3203M | - | 235 | 350 | Gauss |
| "Release Point" | $\mathrm{B}_{\text {RP }}$ | UGN-3203M | 25 | 100 | - | Gauss |
| Hysteresis | $\mathrm{B}_{\mathrm{H}}$ | UGN-3203M | - | 135 | - | Gauss |
| Output Saturation Voltage | $V_{\text {SAI }}$ | $B \geq 350$ Gauss, $I_{\text {smk }}=20 \mathrm{~mA}$ | - | - | 400 | mV |
| Output Leakage Current | $\mathrm{I}_{\text {OFF }}$ | $\mathrm{B} \leq 25$ Gauss, $\mathrm{V}_{\text {Out }}=12 \mathrm{~V}$ | - | - | 100 | $\mu \mathrm{A}$ |
| Supply Current | $\mathrm{ICCl}_{\text {(1) }}$ | $\mathrm{B} \leq 25$ Gauss, outputs open | - | 20 | 25 | mA |
|  | $I_{\text {cc(0) }}$ | $B \geq 350$ Gauss, outputs open | - | 20 | 25 | mA |

## GUIDE TO INSTALLATION

1. All Hall effect integrated circuits are susceptible to mechanical stress effects. Caution should be exercised to minimize the application of stress to the leads or the epoxy package.
2. To prevent permanent damage to the Hall cell I.C., heat sink the leads during hand soldering. For wave soldering, the part should not experience more than $230^{\circ} \mathrm{C}$ for more than 5 seconds and no closer than $0.125^{\prime \prime}$ to the epoxy package.

## 'M' PACKAGE

## DIMENSIONS IN INCHES



DIMENSIONS IN MILLIMETRES
Based on $1 \mathrm{in} .=25.4 \mathrm{~mm}$


## OPERATION

The output transistors are normally 'off', when the magnetic field perpendicular to the surface of the chip is below the threshold or "operate point." When the field exceeds the "operate point," the output transistors switch 'on'" and will each typically sink 20 mA .

The output transistors switch "off" when the magnetic field is reduced below the "release point" which is less than the "operate point." This is illustrated graphically in the transfer characteristic curves. The hysteresis characteristic provides for unambiguous or non-oscillatory switching regardless of the rate of change of the magnetic field.

The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located and $0.037^{\prime \prime} \pm 0.001^{\prime \prime}(0.94 \pm 0.05$ mm ) below the top surface of the package.

For reference purposes, both an Alnico VIII magnet, $0.212^{\prime \prime}(5.38 \mathrm{~mm})$ in diameter and $0.187^{\prime \prime}$ ( 4.75 mm ) long and a samarium cobalt magnet, $0.100^{\prime \prime}(2.54 \mathrm{~mm})$ square and $0.040^{\prime \prime}(1.02 \mathrm{~mm})$ thick, are approximately 1200 gauss at its surface.

The flux density decays at a high rate as the distance from a pole increases.

As an example, using the Alnico VIII magnet referenced above in good alignment and the pole surface in contact with the branded surface of the package, the flux density at the active Hall sensing area of the device would be approximately 850 gauss ( $0.032^{\prime \prime}$ below the package surface).

The flux density would drop to approximately 600 gauss with an air-gap between the package and the magnet of $0.031^{\prime \prime}(0.79 \mathrm{~mm})$.


## UGN-3220S <br> LOW-COST DUAL OUTPUT HALL EFFECT DIGITAL SWITCHES

## features

- Operate from 4.5 V to 16 V D-C Power Source
- Operable With a Small Permanent Magnet
- High Reliability - Eliminates Contact Wear, Contact Bounce
- No Moving Parts
- Small Size
- Outputs Compatible With All Logic Families
- Operation to 100 kHz
- Dual Output Transistors Can Drive Independent Loads

TYPE UGN-3220S INTEGRATED CIRCUITS are low-cost magnetically-activated electronic switches which utilize the Hall Effect for sensing a magnetic field.

Each circuit consists of a voltage regulator, Hall sensor, signal amplifier, Schmitt trigger, and current sinking output stage, integrated onto a single monolithic silicon chip.

The on-board regulator permits operation over a wide variation of supply voltages. Operation over an extended temperature range is made possible by the careful matching of circuit components - something which can be done economically only on a monolithic circuit.

The circuit output can be interfaced directly with bipolar or MOS logic circuits.


These devices are supplied in a 4-pin single inline molded package.

## ABSOLUTE MAXIMUM RATINGS

Power Supply, $\mathrm{V}_{\text {cc }} \ldots \ldots . . \ldots . . . . . . . . . . . . . . . . . . . . . .17 \mathrm{~V}$ Magnetic Flux Density, B . . . . . . . . . . . . . . . . . . . Unlimited Output "OFF" Voltage, $\mathrm{V}_{\text {ourroff) . . . . . . . . . . . . . . . . . . } 17 \text { V }}$ Output "ON" Current, $I_{\text {smk }}$. ....................... 25 mA Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ Operating Temperature Range, $T_{A}$ UGN-3220S $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS at $\mathrm{V}_{\mathrm{CC}}=4.5 \mathrm{~V}$ to $16 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Magnetic Flux Density "Operate Point" | $\mathrm{B}_{0 \text { P }}$ |  | - | 220 | 350 | Gauss |
| "Release Point" | $\mathrm{B}_{\mathrm{RP}}$ |  | 50 | 160 | - | Gauss |
| Hysteresis | $\mathrm{B}_{\mathrm{H}}$ |  | 20 | 60 | - | Gauss |
| Output Saturation Voltage | $\mathrm{V}_{\text {SAT }}$ | $B \geqslant 350$ Gauss, $I_{\text {sink }}=15 \mathrm{~mA}$ | - | 110 | 400 | mV |
| Output Leakage Current | $\mathrm{I}_{\text {off }}$ | $\mathrm{B} \leqslant 50$ Gauss, $\mathrm{V}_{\text {out }}=16 \mathrm{~V}$ | - | 0.1 | 20 | $\mu \mathrm{A}$ |
| Supply Current $B \leqslant 50$ Gauss | $\mathrm{I}_{\mathrm{cc}}$ | $\mathrm{V}_{\text {cc }}=5 \mathrm{~V}$ | - | 3.5 | 9.0 | mA |

## OPERATION

The output transistors are normally "off", when the magnetic field perpendicular to the surface of the chip is below the threshold or "operate point." When the field exceeds the "operate point," each output transistor switches "on"' and is capable of sinking 25 mA of current. Selections to 30 mA are available.

The output transistors switch "off" when the magnetic field is reduced below the "release point"" (which is less than the 'operate point''). This is illustrated graphically in the transfer characteristics curve. The hysteresis characteristic provides for unambiguous or non-oscillatory switching.

The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located and $0.032^{\prime \prime} \pm 0.002^{\prime \prime}(0.81 \pm 0.05$ mm ) below the branded surface of the package.

For reference purposes, both an Alnico VIII magnet, $0.212^{\prime \prime}(5.38 \mathrm{~mm})$ in diameter and $0.187^{\prime \prime}$ ( 4.75 mm ) long and a samarium cobalt magnet, $0.100^{\prime \prime}$ ( 2.54 mm ) square and $0.040^{\prime \prime}$ ( 1.02 mm ) thick, are approximately 1200 gauss at its surface.

The flux density decays at a high rate as the distance from a pole increases.

As an example, using the Alnico VIII magnet referenced above in good alignment and the pole surface in contact with the branded surface of the package, the flux density at the active Hall sensing area of the device would be approximately 850 gauss ( $0.032^{\prime \prime}$ below the package surface).

The flux density would drop to approximately 600 gauss with an air-gap between the package and the magnet of $0.031^{\prime \prime}(0.79 \mathrm{~mm})$.
transfer characteristics showing hysteresis


BASIC 'HEAD-ON' MODE OF OPERATION


## UGN-3501M SOLID-STATE LINEAR OUTPUT HALL EFFECT SENSORS

## FEATURES

- Excellent Sensitivity
- Flat Response to 25 kHz (typ.)
- Internal Voltage Regulation
- Excellent Temperature Stability

UJTILIZING THE HALL EFFECT for sensing a magnetic field, Type UGN-3501M ICs provide a linear differential output which is a function of magnetic field intensity.

These devices are intended for applications requiring accurate measurement and/or control of position, weight, thickness, velocity, etc.

The Type UGN-3501M Hall Effect IC includes a monolithic Hall cell, linear differential amplifier, differential emitter follower output, and a voltage regulator. Integrating the Hall cell and the amplifier into one monolithic device minimizes problems related to the handling of millivolt analog signals.

Provisions are included for output offset null. This sensor is supplied as a 8-pin dual in-line plastic package and is rated for continuous operation over the temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ and a voltage range of 8 to 16 volts $\mathrm{d}-\mathrm{c}$.


## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage, VCC | $+16 \mathrm{~V}$ |
| :---: | :---: |
| Output Current, IOUT | 2 mA |
| Magnetic Flux Density, B | No Limit |
| Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Storage Temperature Range, IS. | .$^{6} 5^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS at $V_{c C}=12 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Min. | Typ. | Max. | Units | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Voltage | VCC |  | 8.0 | - | 16 | $V$ | - |
| Supply Current | ICC | $\mathrm{V}_{\text {CC }}=16 \mathrm{~V}$ | - | 10 | 18 | mA | - |
| Output Offset Voltage | V0FF | $\mathrm{B}=0$ Gauss, R-5-6-7 $=0 \Omega$ | - | 100 | 400 | mV | 1 |
| Output Common Mode Voltage | VCM | $\mathrm{B}=0$ Gauss | - | 3.6 | - | $v$ | 1 |
| Sensitivity | $\triangle V_{\text {OUT }}$ | $B=1000$ Gauss, $\mathrm{R} 5-6-7=0 \Omega$ | 700 | 1400 | - | mV | 1,2 |
| Sensitivity | $\triangle V_{\text {OUT }}$ | $\mathrm{B}=1000$ Gauss, $\mathrm{R} 5-6=15 \Omega$ | 650 | 1300 | - | mV | 1,2 |
| Frequency Response | f(-3dB) | R5-6-7 $=0 \Omega$ | - | 25 | - | kHz | - |
| Broadband Output Noise | $\mathrm{e}_{\mathrm{n}}$ | 3dB B.W. 10 Hz to 10 kHz $\mathrm{R} 5-6-7=0 \Omega$ | - | 0.15 | - | mV | - |
| Output Offset Voltage vs $\mathrm{T}\left({ }^{\circ} \mathrm{C}\right)$ | $\Delta V_{\text {OFF }} / \Delta \mathrm{T}$ | R5-6-7 $=0 \Omega$ | - | 0.2 | - | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ | - |

## NORMALIZED SENSITIVITY AS A FUNCTION OF VCC



RELATIVE OUTPUT VOLTAGE AS A FUNCTION OF LOAD RESISTANCE


NORMALIZED SENSITIVITY AS A FUNCTION OF TEMPERATURE


OUTPUT VOLTAGE
AS A FUNCTION OF MAGNETIC FLUX DENSITY


OUTPUT VOLTAGE AS A FUNCTION OF AIR GAP

NOISE SPECTRAL DENSITY


## GUIDE TO INSTALLATION

1. All Hall Effect integrated circuits are susceptible to mechanical stress effects. Caution should be exercised to minimize the application of stress to the leads or the epoxy package.
2. To prevent permanent damage to the Hall cell IC, heat sink the leads during hand soldering. For wave soldering, the part should not experience more than $230^{\circ} \mathrm{C}$ for more than 5 seconds and no closer than $0.125^{\prime \prime}$ to the epoxy package.
3. If a zeroing potentiometer is used, minimize lead lengths from it and isolate these leads from out-

## DIMENSIONS IN INCHES



Dwa. No. A-9000 IN
put leads if possible. In some cases, it may be more practical to limit the frequency response with an output RC network to prevent oscillation:


## DIMENSIONS IN MILLIMETRES

Based on $1 \mathrm{in} .=25.4 \mathrm{~mm}$


## UGN-3501T SOLID-STATE LINEAR OUTPUT HALL EFFECT SENSORS

## FEATURES

- Excellent Sensitivity
- Flat Response to 25 kHz (typ.)
- Internal Voltage Regulation
- Excellent Temperature Stability

UJTILIZING THE HALL EFFECT for sensing a magnetic field, Type UGN-3501T integrated circuits provide a linear single-ended output which is a function of magnetic field intensity.

These devices are used principally to sense relatively small changes in a magnetic field changes which are too small to operate a Hall effect switching device. They are customarily capacitively coupled to an amplifier, which boosts the output to a higher level.

The Type UGN-3501T Hall Effect IC includes a monolithic Hall cell, linear amplifier, emitter follower output, and a voltage regulator. Integrating the Hall cell and the amplifier into one monolithic device minimizes problems related to the handling of millivolt analog signals.

This sensor is supplied a a 3-pin plastic package and is rated for continuous operation over the temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ and a voltage range of 8 to 12 volts d -c.


## ABSOLUTE MAXIMUM RATINGS

$\qquad$
Output Current, IOUT . . . . . . . . . . . . . . . . . . . . . . . . . . . 4mA
Magnetic Flux Density, B . . . . . . . . . . . . . . . . . . . . . . No Limit
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots . . . . . . . .0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ Storage Temperature Range, TS . . . . . . . . . . . . $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

These Hall effect devices are also available in a miniature 3-pin plastic ' $U$ '" package. The " $T$ "' package is 0.080 " ( 2.03 mm ) thick; the " $U$ '' package is $0.061^{\prime \prime}$ ( 1.54 mm ) thick. All other dimensions are identical.

ELECTRICAL CHARACTERISTICS at $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Min. | Typ. | Max. | Units | Notes |
| :--- | :--- | :--- | :---: | :--- | :--- | :--- | :--- |
| Operating Voltage | VCC |  | 8.0 | - | 12 | V | - |
| Supply Current | ICC | VCC $=12 \mathrm{~V}$ | - | 10 | 20 | mA | - |
| Quiescent Output Voltage | $\mathrm{V}_{\text {OUT }}$ | $\mathrm{B}=0$ Gauss | 2.5 | 3.6 | 5.0 | V | 1 |
| Sensitivity | $\Delta V_{\text {OUT }}$ | $\mathrm{B}=1000$ Gauss | 350 | 700 | - | mV | 1,2 |
| Frequency Response | $\mathrm{f}(-3 \mathrm{~dB})$ |  | - | 25 | - | kHz | - |
| Broadband Output Noise | $\mathrm{e}_{\mathrm{n}}$ | 3 dB B.W. 10 Hz to 10 kHz | - | 0.10 | - | mV | - |
| Output Resistance | $\mathrm{R}_{0}$ |  | - | 100 | - | $\Omega$ | - |

[^50]normalized sensitivity as a function of $\mathbf{V}_{\text {CC }}$


OUTPUT VOLTAGE AS A FUNCTION OF MAGNETIC FLUX DENSITY


NORMALIZED SENSITIVITY AS A FUNCTION OF TEMPERATURE


OUTPUT VOLTAGE AS A FUNCTION OF AIR GAP


NOISE SPECTRAL DENSITY


# Typical Applications of Hall Effect Linear Sensors 

SENSITIVE PROXIMITY DETECTOR

$$
\begin{aligned}
& \Delta V_{0} \simeq 10 \mathrm{mV} \\
& D=0.250^{\prime \prime}
\end{aligned}
$$

NOTCH OR HOLE SENSOR


For reference only - an Alnico VIII permanent magnet, $0.212^{\prime \prime}$ $(5.38 \mathrm{~mm})$ in diameter and $0.187^{\prime \prime}(4.75 \mathrm{~mm})$ long is approximately 800 gauss at the surface. A samarium cobalt perma-
nent magnet, $0.100^{\prime \prime}(2.54 \mathrm{~mm})$ square and $0.040^{\prime \prime}(1.02 \mathrm{~mm})$ thick is approximately 1200 gauss at its surface.

## GUIDE TO INSTALLATION

1. All 'Hall Effect' integrated circuits are susceptible to mechanical stress effects. Caution should be exercised to minimize the application of stress to the leads or the epoxy package.
2. To prevent permanent damage to the Hall cell IC, heat sink the leads during hand soldering. For wave soldering, the part should not experience more than $230^{\circ} \mathrm{C}$ for more than 5 seconds and no closer than $0.125^{\prime \prime}$ to the epoxy package.

## UGN-3604M and UGN-3605M HALL EFFECT SENSORS

THE MOST BASIC Hall Effect magnetic field sensors are the Type UGN-3604M and UGN3605 M . The differential output of the devices is a function of the magnetic flux density present at the sensor. Sensitivity is a function of the control current: sensitivity increases as the control current increases.

The UGN-3604M and UGN-3605M are most often used for magnetic circuit design, analysis, testing and alignment, and for calibrating magnetic sensing devices.

The UGN-3604M is supplied in an 8 -pin DIP package, with a calibration chart. The UGN-3605M is the same device without the calibration chart.

Each Type UGN-3604M Hall Effect sensor is individually calibrated at a temperature of $+25^{\circ} \mathrm{C}$ using a supply voltage of 5 -volts. The calibration chart supplied indicates differential output values for a magnetic flux density range from 0 gauss to 1000 gauss. Sensitivity at this supply voltage level is typically 40 mV per 1000 gauss.

Since the differential output voltage is a linear function of the magnetic flux density, other readings are easily interpolated.


The UGN-3605M is intended to be used primarily as a sensing device. When operated from a constant current source of 3 mA the device provides a typical sensitivity of 60 mV per 1000 gauss. This is the preferred biasing method, to achieve the most stable output voltage vs. temperature.

## ABSOLUTE MAXIMUM RATING

Supply Voltage, $\mathrm{V}_{\mathrm{cc}} \ldots . . . . . . . . . . . . . . . . . . . . . . . . . .+7 \mathrm{~V}$
Supply Current, Icc ................................. 10 mA
Magnetic Flux Density, B . . . . . . . . . . . . . . . . . . . . No Limit
Operating Temperature Range, $T_{A} \ldots \ldots \ldots .0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{s}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Condition | Min. | Typ. | Max. | Notes |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Current | $\mathrm{I}_{\mathrm{cc}}$ | - | - | 3 mA | 7 mA | 1,2 |
| Control Resistance | $\mathrm{R}_{1-3}$ | - | $1 \mathrm{k} \Omega$ | $2.2 \mathrm{k} \Omega$ | $4.5 \mathrm{k} \Omega$ |  |
| Control Resistance vs. Temperature | $\Delta \mathrm{R}_{1-3} / \Delta \mathrm{T}$ | - | - | $+.8 \% /{ }^{\circ} \mathrm{C}$ | - |  |
| Differential Output Resistance | $\mathrm{R}_{2 \cdot 4}$ | - | $2 \mathrm{k} \Omega$ | $4.4 \mathrm{k} \Omega$ | $9 \mathrm{k} \Omega$ |  |
| Output Offset Voltage | $\mathrm{V}_{\text {off }}$ | $\mathrm{B}=0$ Gauss | - | $\leq 5 \mathrm{mV}$ | - |  |
| Output Offset Voltage vs. Temperature | $\Delta \mathrm{V}_{\text {off }} / \Delta \mathrm{T}$ | $\mathrm{B}=0$ Gauss | - | $\leq\left( \pm 30 \mu \mathrm{~V} / /^{\circ} \mathrm{C}\right)$ | - |  |
| Sensitivity | $\Delta \mathrm{V}_{\text {our }} / \Delta \mathrm{B}$ | $\mathrm{I}_{\mathrm{cc}}=7 \mathrm{~V} / \mathrm{R}_{1.3}$ | - | $60 \mathrm{mV} / 1000 \mathrm{Gauss}$ | - |  |
| Sensitivity vs. Temperature | $\Delta \frac{\mathrm{V}_{\text {ouv }} / \Delta \mathrm{B}}{}$ | $\mathrm{I}_{\mathrm{cc}}=1.5 \mathrm{~mA}$ | - | $+.1 \% /{ }^{\circ} \mathrm{C}$ | - |  |
| Product Sensitivity | $\mathrm{\Delta T}$ | $\mathrm{~V} / \mathrm{Ax} \mathrm{kG}$ | $\mathrm{I}_{\mathrm{cc}}=7 \mathrm{~V} / \mathrm{R}_{1-3}$ | - | 20 | - |

[^51]
## APPLICATION NOTES

1. All Hall effect integrated circuits are susceptible to mechanical stress effects. Caution should be exercised to minimize the application of stress to the leads or to the epoxy package.
2. To prevent permanent damage to a Hall cell I.C., heat sink the leads during hand soldering. For wave soldering, the part should not experience more than $230^{\circ} \mathrm{C}$ for more than 5 seconds and no closer than $0.125^{\prime \prime}(3.28 \mathrm{~mm})$ to the epoxy package.
3. The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located and $0.037^{\prime \prime} \pm 0.001^{\prime \prime}(0.94 \pm 0.03 \mathrm{~mm})$ below the top surface of the package.
4. For reference purposes, an Alnico VIII magnet, $0.212^{\prime \prime}(5.38 \mathrm{~mm})$ in diameter and $0.187^{\prime \prime}$ $(4.75 \mathrm{~mm})$ long or a samarium cobalt magnet, $0.100^{\prime \prime}(2.54 \mathrm{~mm})$ square and $0.040^{\prime \prime}(1.02 \mathrm{~mm})$ thick, is approximately 1200 gauss at its surface.

Note that the flux density decays at a high rate as the distance from a pole increases. In most cases, this is a relatively linear decrease in the region of interest, and it may range from 5 to 20 gauss $/$ mil.

## DIMENSIONS IN INCHES

## DIMENSIONS IN MILLIMETRES

Based on $1 \mathrm{in} .=25.4 \mathrm{~mm}$


## Hall Effect IC Application Guide

SPRAGUE ELECTRIC uses the latest linear integrated circuit technology in combination with the $100^{+}$year old Hall Effect to produce Hall Effect ICs. These are magnetically activated switches and sensors with the potential to simplify and improve systems designed for switch and sensor applications.

## Simplified Switching At Low Cost

Simplified switching is a Hall switch feature. Sprague Hall Effect ICs combine Hall voltage generators, signal amplifiers, Schmitt trigger circuits and transistor output circuits on an IC chip. Output is clean, fast, and switched with no bounce, an inherent problem in mechanical contact switches. A Sprague Hall Effect IC switch costs less than many common electromechanical switches.

## Efficient, Effective Low-Cost Sensors

A Hall Effect sensor detects the motion, position, or change in field strength of an electromagnet, a permanent magnet, or a ferromagnetic material with an applied magnetic bias. Output is linear and temperature stable. Energy consumption is significantly low. Response is independent of the velocity of the field being sensed.
A Sprague Hall Effect IC sensor can be more efficient and effective than inductive or optoelectronic sensors and at lower cost.

## Sensitive Circuits For Rugged Service

The Hall Effect IC is virtually immune to environmental contaminants, is particularly rugged, and is suitable for use under severe service conditions. These circuits are very sensitive, providing reliable, repetitive operations in close tolerance applications. The Hall Effect IC can 'see"' precisely through dirt and darkness.

Sprague Hall Effect IC switches and sensing systems cost less than most optoelectronic switch and sensor circuits.

HALL EFFECT SWITCH OUTPUT WAVEFORM


REED RELAY OUTPUT WAVEFORM


HALL EFFECT SENSOR LINEAR OUTPUT


## HISTORY AND THE HALL EFFECT

E. H. Hall, at Johns Hopkins University in 1879, first noted the effect that bears his name. A magnetic field applied to a conductor carrying current produces a voltage across the conductor as shown in Figure 6.

The effect is caused by electron deflection within the solid, concentrating the negative charges to one side or the other depending on the influence of the magnetic lines of force. The difference in potential is called the Hall voltage.

The ratio $V t / I H$ is the Hall Coefficient. ( $V$ is the Hall voltage, $t$ the material thickness, $I$ the primary current flow, and $H$ the magnetic field.) This ratio is a constant for a given material.
H. A. Lorentz and Paul Drude developed theories of conduction which apparently accounted for the Hall Effect early in this century. Subsequently the Hall Effect was widely used to study conductivity of materials, with a Hall Coefficient assigned as a means of classification.

Attempts to classify some specific materials such as lead sulphide and silicon produced baffling, contradictory data. The introduction of quantum mechanics in 1926 provided a means for clarification of these problems and other difficulties associated with semiconductor materials.

A proper understanding of semiconductor theory, impurity conduction, junction theory and the fundamental approaches to semiconductor device design did evolve out of studies using the Hall Effect.

The Hall voltage is proportional to the crossproduct $I x H$ (Current x Field). A device that exhibits the Hall Effect is a multiplier: if current flow is constant, the Hall voltage will be proportional to the magnetic field applied; if the magnetic field is constant, the Hall voltage will be proportional to the current flow.

Early Hall Effect devices found limited application as wattmeters or gaussmeters. Such devices were complex, expensive, and susceptible to noise and temperature variations. It was difficult to achieve useful Hall voltage levels.

Production of Hall Effect integrated circuits have eliminated the problems associated with discrete component circuit designs. The Hall Effect ICs are simple, inexpensive, virtually immune to noise, and are temperature stable. Amplifier circuits integral to the devices produce useful electrical output levels.


A MAGNETIC FIELD IS APPLIED TO THE CONDUCTOR CARRYING CURRENT. THE NEGATIVE CHARGES ARE DEFLECTED BY THE MAGNETIC FIELD PRODUCING A DIFFERENCE IN POTENTIAL CALLED THE HALL VOLTAGE (VhaL). THIS PRINCIPLE IS APPLIED IN HALL EFFECT IC'S TO PRODUCE MAGNETICALLY ACTIVATED SWITCHES AND SENSORS.

## SOME CURRENT HALL EFFECT IC APPLICATIONS -

## Ignition Systems

Speed Controls
Speedometer Pickups
Security Systems
Alignment Controls
Mechanical Limit Switches (computers) (printers)
(floppy discs)
(sewing machines)
(record players) (machine tools)

Current Sensors
Current Limit Switches
Linear Potentiometers
Position Detectors
Keyboard/Keyswitch
Selector Switches
Pushbutton Switches
Micrometers

## HALL EFFECT SWITCH and SENSOR APPLICATIONS AREAS -

## Appliances

Automotive OEM
Automotive Aftermarket
Business Machines
Communications
Computers/Peripherals
Controls
Entertainment Products
Industrial and Commercial Switches
Instrumentation
Keyboard/Keyswitch
Machinery
Machine Tools
Military Systems and Equipment
Power Supplies
Test Equipment

## TYPICAL APPLICATIONS



## What Does A Hall Effect Switch Do?

Switch designers have obtained high performance switching characteristics with the use of photoelectric switching, capacitive circuits, mercury wetting switches, proximity devices and magnetic pickup techniques. Such designs have unique characteristics suitable for one or more specific applications. In general these designs are usually more complex and more expensive than Hall Effect IC switches performing similar functions.

Snap-action or reed switches have been used wherever the switch life, speed and reliability per-
mitted, primarily because of their low cost. Some applications require performance standards not available in electro-mechanical switches.

Sprague Electric Hall Effect IC switches provide high-performance switching characteristics at costs comparable with snap-action or reed switches.

The devices are very small. The 3-lead ' $T$ '' pack units are $0.18^{\prime \prime} \times 0.18^{\prime \prime} \times 0.08^{\prime \prime}$. The cost is as low as the devices are small.

## Whatever Turns Them On...

The application of Hall Effect switches is not very different from other switching methods. A means for mounting and making electrical connections must be provided. Supply voltage, load, environment and ambient temperature range must fall within limits specified in the applicable engineering bulletin.

Hall Effect switches incorporate a voltage regulator, a Hall voltage generator, a signal amplifier, trigger circuits and output drivers on a single silicon chip.


Dwg. No. A-11,007

Switching is dependent on the proximity of an external magnet whose field passes perpendicularly through the Hall voltage generator on the chip face. The Hall generator produces an analog voltage amplified and converted by the trigger circuit to a digital output.

Hall Effect IC switches feature such characteristics as high-speed response and very high cycle rates. Typical rise time (turn-on) is 15 nanoseconds, fall time (turn-off) 100 nanoseconds. These units have the capability for cycling at $100,000 \mathrm{~Hz}$ (cycles-per-second).

Hall Effect IC switches feature constant amplitude output without the bounce characteristics of electromechanical switches. Hall Effect ICs also feature low power consumption: 7 mA is typical.

The magnetic characteristics of the Hall Effect switch are specified in terms of magnetic flux density (in gauss). Typical, maximum, and minimum operate and release points and hysteresis factors are specified.

A built-in hysteresis feature insures that stray magnetic fields from transformers, solenoids, or other associated circuitry will not cause unwanted switch operation. The graph below shows typical hysteresis characteristics for the UGN-3019T switch.

## TRANSFER CHARACTERISTICS SHOWING HYSTERESIS



The maximum operate point for the UGN-3019T switch is specified at 500 gauss and the minimum release point at 100 gauss. The maximum hysteresis factor for this switch, however, is 275 gauss. Should the operate point fall near the maximum, the release point will move up as well. Similarly, if the release point falls near the minimum, the operate point will have a correspondingly lower value. The hysteresis factor will remain close to a typical value.

Basic fixed element switch designs will take the maximum and minimum operate and release points into account. However, a configuration which permits adjustment of switch and magnet elements in assembly or operation can take advantage of the closer tolerance hysteresis limits to achieve even more precise switching characteristics.

## Head-On Mode of Operation

The simplest form of magnet which will operate the Hall Effect switch is a rod or bar. The curves below illustrate typical flux density (in gauss) as a function of air gap distance for two rod magnets.

In each case, the magnet is oriented with its axis perpendicular to, and on the center line of, a Hall Effect IC switch. Flux density and air gap distance are measured along the magnet axis and switch centerline.


The magnet is moved toward the switch to activate it and away to release it. This method of operation is commonly referred to as the head-on mode.

The switch used is the Sprague UGN-3019T. The typical operate and typical release points are 420 and 300 gauss, respectively.
An ALNICO V rod magnet $0.25^{\prime \prime}$ in diameter by $1.25^{\prime \prime}$ in length must be $0.18^{\prime \prime}$ or less from the switch to insure operation at the 420 gauss typical operate point. The magnet must be moved to a distance $0.25^{\prime \prime}$ from the switch to insure release, an "operate-release" distance of $1 / 16^{\prime \prime}$.
The UGN-3019T can be switched with a larger or stronger magnet over greater distances. Or, the device can be switched with a smaller or weaker magnet provided the air gap between the magnet and the switch is properly decreased.
An ALNICO VIII rod magnet $0.212^{\prime \prime}$ in diameter by $0.187^{\prime \prime}$ in length must be $0.05^{\prime \prime}$ or less from the switch to insure operation at the 420 gauss typical operate point. The magnet must be moved to a distance $0.085^{\prime \prime}$ from the switch to insure release at the 300 gauss typical release point.
Use of the smaller ALNICO VIII rod magnet reduced the on-to-off motion from approx. $1 / 16^{\prime \prime}$ to $1 / 32^{\prime \prime}$.

## magnetic flux density as a function of air gap Head-On Mode of Operation




DW. NO. A 10.969

## Slide-By Mode of Operation

Hall Effect switches are often activated by means of a slide-by movement of the magnet past the switch as illustrated below.

The axis of the magnet remains perpendicular to the face of the switch, the air gap remains constant, and the magnet passes close enough to the switch to activate it. The maximum flux density is obtained when the magnet axis is on the switch centerline.

The graph at bottom left shows slide-by characteristics for the same magnet used in the previous head-on mode example. The air gap is $0.01^{\prime \prime}$. Flux density at the switch is a function of the distance between the magnet axis and the switch centerline.

Movement from the operate point to the release point covers only $0.018^{\prime \prime}$. Movement continuing past the switch covers an "operate-release'" distance of $0.24^{\prime \prime}$, but no change in direction is required.


## Slide-By With Actuator

Magnetic fields may be distorted, interrupted, squeezed, squashed, or focused by various ferromagnetic concentrators, shunts, vanes, flux returns, and actuators. The magnetic circuit improves the efficiency of the magnet by concentrating the magnetic field.

The extent of field distortion can be seen in a comparison of flux density at the switch for a magnet with and without the actuator. Flux density is plotted in a slide-by mode, with a $0.05^{\prime \prime}$ air gap for an ALNICO VIII rod magnet $0.188^{\prime \prime}$ in diameter by $0.938^{\prime \prime}$ in length.

Without the actuator, the flux density across the $0.05^{\prime \prime}$ air gap is not sufficient to activate a UGN3019 T , as illustrated in the graph at bottom right. With the actuator, the 420 gauss operate point is obtained with the magnet axis $0.15^{\prime \prime}$ from the switch centerline.



DWG. NO. 11,117-A

MAGNETIC FLUX DENSITY AS A FUNCTION OF MAGNET AXIS-TO-CENTERLINE DISTANCE Slide-By Mode of Operation


DISTANCE (D) OF MAGNET FROM CENTERLINE (¢) INCHES
Dwg. No. A-10,956


DISTANCE (D) OF MAGNET FROM CENTERLINE (q) INCHES
Dwg. No. A-9011C

## Vane Activation

A ferromagnetic plate or vane moved between the magnet and switch will shunt the field, shielding the switch from the magnet. A movable vane, as shown below, is a most practical device for switching a Hall Effect IC.

Vane activation is often accomplished in a fixed assembly incorporating a magnetic conductor to concentrate and focus the magnetic field through the switch. A ferrous vane is used to shunt the flux, turning the switch off. The magnet, switch and magnetic conductor may be molded in place, eliminating alignment problems, and often producing an extremely rugged completed switch.

A fixed assembly designed for vane activation lends itself to a wide variety of possible switch configurations.

Note the curve at bottom left is an approximation. Several factors influence the switching characteristics of a vane activated Hall Effect switch. The relative position of the vane leading and trailing edges and the strength of the magnet used are of primary importance.

The flux density, vane dimensions, and material

all affect the slope of the flux density curve. $A$ steeper curve will minimize the effect of switching point tolerance and temperature and voltage variation. A stronger magnet reduces the vane travel required to switch the Hall Effect switch.

Switch designers have utilized strong magnets with efficient magnetic circuit design in a fixed element molded assembly to provide a very high flux density and a steep curve. This approach minimizes operate-release point variations with changes in temperature.

A different design approach has used an adjustable air gap, permitting use of a smaller magnet in the magnetic circuit design. This design approach produces a shallow flux density curve, and places severe operate-release point restrictions on the Hall switch required. Vane material is typically greater than $1 / 32^{\prime \prime}$ thick to result in a minimum flux density. This leaves little clearance.

Generally, the physical position of the vane leading and trailing edges, (which determine switch points), the switch characteristics, and the magnet specifications should all be considered as part of an overall switch design. Independent selection of any element can severely restrict the possibilities for designing an effective switch.

The graph at bottom right is a generalization of the principle involved in reducing switching distances and tolerances for vane activated switches. A stronger magnet produces a higher initial flux density and a steeper curve. Note that a steep slope minimizes the effect of temperature changes on the operate point.

## FLUX DENSITY AS A FUNCTION OF VANE POSITION




## Ring Magnets and Bipolar Switches

Multiple-pole ring magnets and Hall Effect bipolar switches are used to monitor or measure rotary motion and are especially useful in high-speed applications: speedometer pickups, rpm indicators, angle indicators, etc.

Rugged inexpensive ceramic or plastic ring magnets incorporate up to 20 magnetic pole pairs per inch of ring diameter. The useful field strength available in this type of magnet construction is approximately 250 gauss to 1000 gauss.

Sprague UGN-3030T and UGS-3030T bipolar digital switches operate in the magnetic field range of 250 gauss (South) to -250 gauss (North) and are intended specifically for operation with multiplepole ring magnets.

Note below that exposure to a single pair of opposite magnetic poles accomplishes a single switching cycle.

## A SINGLE SWITCHING CYCLE FOR A MULTIPLE POLE

 RING MAGNET USING A UGN-3030T SWITCH

The curves shown are approximations. Actual magnetic field exposure at the switch depends on the field strength available and the magnet-to-switch spacing.

Ring magnets are available with radially-oriented poles or with axially-oriented poles.

The output voltage wave form will be determined by the specific distribution of the operate and release points within the switching range. As with other Hall Effect switches, both points move together within the switching range so that the hysteresis factor remains close to the typical value in all cases, as illustrated in the graph at bottom.

RADIAL OR AXIAL ORIENTED POLES FOR SWITCH ACTUATION WITH A RING MAGNET


TRANSFER CHARACTERISTICS SHOWING HYSTERESIS


## MODEL OF A MAGNET

An inexpensive commercially available standard ALNICO VIII magnet* is shown in the scale drawing. The solid lines are maximum operate and minimum release points for a Sprague UGN-3019T switch. The field strength levels indicated by dotted lines are maximum operate and minimum release points for other Sprague Hall Effect IC switches.

The field is unique to this magnet, and is a function of the material used and the geometry and dimensions of the magnet. Increasing the diameter would tend to spread the field. Extending the length of the magnet would strengthen the field.

A variety of magnet materials are commercially available, each exhibiting unique field characteristics. A samarium-cobalt magnet only $0.085^{\prime \prime}$ square by $0.04^{\prime \prime}$ long will produce up to 1200 gauss at its pole surface, more than adequate field strength to operate all Sprague Hall Effect IC switches. The strongest known field available in a permanent magnet is that generated by an ALNICO V magnet capped with a samarium-cobalt rare earth magnet.

The curves below left are flux density values for the magnet measured for switch activation in a head-on mode (along the magnet axis), and for slide-by modes with air gaps of $0.01^{\prime \prime}$ and $0.025^{\prime \prime}$.

FLUX DENSITY CURVES


Dwg. No. A-11,065

## MAGNETIC FIELD MODEL OF AN ALNICO VIII SINTERED ROD MAGNET



The slide-by curves cross each other, reflecting the fact that the field strength contours are not concentric circles.

The magnetic flux density is indicated for the most sensitive area of the device. This area is centrally located and $0.032^{\prime \prime} \pm 0.002^{\prime \prime}$ below the branded surface of the T package and $0.012^{\prime \prime} \pm 0.002^{\prime \prime}$ below the branded face of the U package.

Note that Sprague Hall Effect ICs are designed to be activated by the field generated by a magnetic South pole, applied to the face or branded side of the switch package. The Hall Effect switches will operate with a magnetic North pole of sufficient strength applied to the back of the switch.

A magnetic South pole at the face, and a magnetic North pole at the back of the switch at the same time produce a concentrated field through the switch. A magnetic South pole applied to the reverse side of the switch will offset the effects of a South pole applied to the switch face. Conversely, a North pole may be applied to the back side of the switch so the device is normally on, and a North pole approaching the switch face will turn it off.

[^52]
## LOW-COST HALL EFFECT DIGITAL SWITCHES

Sprague offers 10 different Hall Effect switches from its automated high-volume production, packaging and test facilities in Concord, N.H. These rugged solid-state switches operate with small lowcost commercially available permanent magnets.

The devices feature 'no-bounce" contactless switching to $100,000 \mathrm{~Hz}$, circuit operation over a wide range of specified supply voltages ( 4.5 to 25 V ), and constant amplitude output. Output stages are easily interfaced with a variety of output loads.

Each Hall Effect switch is a plastic-packaged monolithic integrated circuit: a voltage regulator,

FUNCTIONAL BLOCK DIAGRAM TYPE UGN-3013, UGN-3019, UGN-3020, and UGN-3030 "T" Pack


Ow. No. 4-10.313

Hall voltage generator, signal amplifier, trigger circuit and output transistors on a single silicon chip.

Output transistors are normally off until a magnetic activating field exceeds a specified operate point. Switched on the transistors will sink up to 25 mA . See Electrical Characteristics below.

The output transistors switch off when the activating field drops below a specified release point that is a lower value than the operate point. This switching hysteresis characteristic insures unambiguous, non-oscillatory switching.

FUNCTIONAL BLOCK DIAGRAM TYPE UGN-3201 and UGN-3203 8-Pin DIP and UGN-3220 "S" Pack


OK'G. NO. A-10.898

ELECTRICAL CHARACTERISTICS

| Characteristics | UGN-3013T/U | $\begin{array}{\|l\|} \hline \text { UGN-3019T/U } \\ \text { UGS-3019T/U } \end{array}$ | UGN-3201M | UGN-3203M | UGN-3020T/U UGS-3020T/U | $\begin{array}{\|l\|l} \hline \text { UGN-3030T/U } \\ \text { UGS-3030T/U } \end{array}$ | UGN-3040T/U | UGN-3220S |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{\text {cc }}$ Max. <br> $V_{\text {out }}$ Max. <br> (Logical 1) | 17 V | 25 V | 20 V |  | 25 V |  |  | 17V |
| $\begin{aligned} & I_{\text {IINK Max. }} \\ & (\text { Logical } 0) \end{aligned}$ | 25 mA |  | 2(25) mA* |  | 25 mA |  |  | 2(25) mA* |
| Operate Max. <br> Point $\qquad$ Gauss Typ. | $\frac{450}{300}$ | $\frac{500}{420}$ | $\frac{750}{450}$ | $\frac{350}{235}$ | $\frac{350}{220}$ | $\frac{250}{160}$ | $\frac{200}{150}$ | $\frac{350}{220}$ |
| Release Typ. <br> Point $\qquad$ <br> Gauss Min. | $\frac{225}{25}$ | $\frac{300}{100}$ | $\frac{300}{100}$ | $\frac{100}{25}$ | $\frac{165}{50}$ | $\frac{110}{-250}$ | $\frac{100}{50}$ | $\frac{160}{50}$ |
| Package | 3-Pin "T" or "U' Pack |  | 8-Pin DIP |  | 3-Pin "T" or "U" Pack |  |  | 4-Pin "S" Pack |

$T_{A}$ Max. Operating Temperature for UGN prefix devices is $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.
$T_{A}$ Max. Operating Temperature for UGS prefix devices is $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.
*Dual Outputs

## SUGGESTED OUTPUT LOADS FOR HALL EFFECT SWITCHES

The output of each Sprague Hall Effect switch is a grounded-emitter, open-collector structure. In the absence of a magnetic field the output transistor is OFF and switches ON when the proper field is applied to the associated Hall voltage generator.


With a simple external resistor network the output can be interfaced with transistors, triacs, SCRs or common DTL, TTL, RTL and MOS logic circuits. Any type of load within specified current and voltage limitations is possible. Transient suppression may be required on all inductive loads.

Output is specified in the engineering bulletins in terms of positive logic: low or on voltage level $=0$; high or $\operatorname{FFF}$ voltage level $=1$. In the logic " 1 " state, the output is guaranteed to sustain a specified voltage level. The UGN-3019T is capable of sinking up to 15 mA with a voltage drop of less than 400 mV .


The graph at bottom left illustrates the typical output ON voltage level as a function of temperature for the UGN-3019T.

Below are some suggested interfacing approaches. Many techniques can be used and are discussed in the following pages.


Specific device type numbers are referenced in this section in discussion of applications, loads and interfacing techniques. However, all Sprague Hall Effect switches may be used in the same way provided the total sink current and maximum off voltage levels do not exceed values specified for each device.

## Switching Common Loads With The UGN-3020T

The UGN-3020T is supplied in a 3-pin plastic " T "' Pack. The branded side of the package is the face. Terminals are, from left-to-right facing the package, the input ( $\mathrm{V}_{\mathrm{CC}}$ ) terminal, common ground and output terminals.

Supply voltage is any value between +4.5 and +24 volts applied between the $\mathrm{V}_{\mathrm{CC}}$ terminal and common ground. The absolute maximum output terminal sink current is 25 mA . Voltage drop at 25 mA is typically 0.2 volts.

Note that the voltage on the output terminal must always be positive ( + ).

The South pole of the magnet shown below will activate the UGN-3020T in a head-on mode, at a typical distance of $0.12^{\prime \prime}$ from the switch face (typical operate point is 220 gauss). The switch is turned OFF by removing the magnet to a distance of $0.16^{\prime \prime}$ from the switch (typical release point is 165 gauss).

## Light-Emitting-Diode

Let's connect a load, a light-emitting-diode. We have a +12 volt supply. We must connect a currentlimiting resistor in series with the diode to keep the ON current under 50 mA maximum, as illustrated below.

If the LED drops 1.4 volt, we need a resistor of $\frac{12 \mathrm{v}-1.4 \mathrm{v}}{.05 \mathrm{~A}}=212 \mathrm{ohms}$. The closest standard value is 220 ohms.


## 40669 Triac

The RCA 40669 triac is often used to control a-c loads up to 8 amperes rms maximum. We must add a current gain stage between the UGN-3020T and the 40669 triac.

When the Hall switch is turned on, it supplies 9 mA of base current to the 2N5811 which turns on and supplies 80 mA of drive to the triac. Note that
the +12 volt supply common ground is connected to the low side of the a-c line. Be careful. If the high and low are mixed up the Hall switch could be hot!


## D-C Load 4 Amperes

When the UGN-3030T is activated, base drive is pulled away from the 2N5812. Collector current then flows to the base of the 2 N 3055 . A 4 ampere load can be activated.


## TTL/DTL

The popular TTL 7400 series is quite simple to drive. The UGN-3020T, switched ON, will sink the 1.6 mA maximum to operate the 7400 .


## Isolating The Switch From The A-C Line

It is desirable to isolate the Hall Effect switch from the a-c line for many control applications driving line-operated loads. A Fairchild MC-232 photoisolator may be used to accomplish this design.

The activated UGN-3020T will draw current through the LED. The current must be limited to 50 mA . A 5-volt supply is used. The calculation is

$$
R=\frac{V_{C C}-V_{F}(L E D)}{I}=\frac{5 V-1.4 \mathrm{~V}}{.05 \mathrm{~A}}=72 \mathrm{ohms} .
$$

The resistor selected is the closest standard value 68 ohms. The LED drives the detector which supplies 70 mA to drive the triac. Note that the 10 volt power supply, consisting of the 6.3 -volt transformer, diode and capacitor, can supply detector bias for several of these control circuits.


Types UGN-3013T, UGN-3019T, UGS-3019T, UGN-3020T, UGS3020T, UGN-3030T, UGS-3030T, UGN-3040T, and UGN-3501T are supplied in 3-pin plastic " $T$ '" packages 0.080 " ( 2.03 mm ) thick. These Hall effect devices are also available in 3-pin plastic ' $U$ '" packages 0.061 ' ( 1.54 mm ) thick. The ' $U$ '' package is specified by replacing the ' $T$ ', suffix to the part number with a ' $U$ ', (UGN-3013U).

## LINEAR OUTPUT HALL EFFECT SENSORS

## TYPE UGN-3501T

Utilizing the Hall Effect for sensing a magnetic field, Type UGN-3501T integrated circuits provide a linear single-ended output which is a function of magnetic field intensity. Integrating the Hall cell and the amplifier into one monolithic device minimizes problems related to the handling of millivolt analog signals.

This sensor, supplied in a 3-pin plastic package, is rated for continuous operation over the temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ and a voltage range of 8 to 12 volts d-c.

The functional block diagram for the UGN-3501T is shown below.

FUNCTIONAL BLOCK DIAGRAM


TYPE UGN-3501M
The Type UGN-3501M Hall Effect IC includes a monolithic Hall cell, linear differential amplifier, differential emitter follower output, and a voltage regulator.

Provisions are included for output offset null. This sensor is supplied in an 8-pin dual in-line plastic package and is rated for continuous operation over the temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ and a voltage range of 8 to 16 volts d-c.

The figure below shows the functional block diagram for the UGN-3501M Hall Effect Sensor.

FUNCTIONAL BLOCK DIAGRAM


OUTPUT VOLTAGE AS A FUNCTION OF AIR GAP FOR HEAD-ON MODE OF OPERATION



## APPLICATIONS FOR TYPE UGN-3501T SENSORS

These devices are used principally to sense relatively small changes in a magnetic field - changes which are too small to operate a 'Hall Effect' switching device. They are customarily capacitively coupled to an amplifier, which boosts the output to a higher level.

The UGN-3501T is a single output linear device having a sensitivity of $700 \mathrm{mV} / 1000$ gauss, and output offset which is typically +3.6 volts, at a $\mathrm{V}_{\mathrm{cc}}$ of +12 volts.

The device will respond to magnetic North and South poles directed to the face or reverse side of the 3-pin ' $T$ '" package, as illustrated below.


OUTPUT VOLTAGE AS A FUNCTION OF MAGNETIC FLUX DENSITY


## ABSOLUTE MAXIMUM RATINGS

| Supply Voltage, VCC | +16V |
| :---: | :---: |
| Output Current, IOUT | 4 mA |
| Magnetic Flux Density, B | No Limit |
| Operating Temperature Range, $\mathrm{T}_{A}$ | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Storage Temperature Range, TS. | $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS at $\mathbf{V}_{\mathrm{CC}}=12 \mathrm{VDC}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Min. | Typ. | Max. | Units | Notes |
| :--- | :--- | :--- | ---: | :--- | :--- | :--- | :--- |
| Operating Voltage | $\mathrm{V}_{\mathrm{CC}}$ |  | 8.0 | - | 12 | V | - |
| Supply Current | ICC | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}$ | - | 10 | 20 | mA | - |
| Quiescent Output Voltage | $\mathrm{V}_{0 \mathrm{OT}}$ | $\mathrm{B}=0$ Gauss | 2.5 | 3.6 | 5.0 | V | 1 |
| Sensitivity | $\Delta_{\mathrm{V}} \mathrm{OUT}$ | $\mathrm{B}=1000$ Gauss | 350 | 700 | - | mV | 1,2 |
| Frequency Response | $\mathrm{F}(-3 \mathrm{~dB})$ |  | - | 25 | - | kHz | - |
| Broadband Output Noise | $\mathrm{e}_{\mathrm{n}}$ | 3 dB B.W. 10 Hz to 10 kHz | - | 0.10 | - | mV | - |
| Output Resistance | $\mathrm{R}_{0}$ |  | - | 100 | - | $\Omega$ | - |

[^53]
## Ferrous Metal Detector

Two similar detector designs are illustrated below. One senses the presence of a ferrous metal, the other senses an absence of the metal. The two sensing modes are accomplished simply by reversing the magnet poles relative to the UGN-3501T. The pole of the magnet is fixed in contact with the reverse side of the UGN-3501T in both cases.

Frequency response characteristics of this circuit are easily controlled by changing the input decoupling capacitor value for the low-frequency breakpoint. If high-frequency attenuation is desired a capacitor may be used to shunt the feedback resistor.


## Metal Sensor

The North pole of the magnet is fixed to the reverse side of the UGN-3501T. The sensor is in contact with the bottom of a ${ }^{3} / 32^{\prime \prime}$ epoxy board. A 20 mV peak output change (decrease) is produced as
the $1^{\prime \prime}$ steel ball rolls over the sensor. This signal is amplified by the $\mu \mathrm{A} 741 \mathrm{C}$ to drive the 2 N 8512 ON to carry a 0.5 A collector current.


## Notch Sensor

The South pole of the magnet is fixed to the reverse side of the UGN-3501T. The sensor is $1 / 32^{\prime \prime}$ from the edge of the steel rotor. $\mathrm{A}^{1 / 16^{\prime \prime}}$ wide by $1 / 8^{\prime \prime}$ ' deep slot in the rotor edge passing the sensor causes a 10 mV peak output change (decrease). This signal is amplified by the $\mu \mathrm{A} 741 \mathrm{C}$ to drive the 2N5812 on, carrying a 0.5 A collector current.

Note that in both examples the branded side of the UGN-3501T faces the material (or lack of material) to be sensed. In both cases the presence (or absence) of the ferrous metal changes the flux density at the Hall Effect sensor so as to produce a negative going output pulse. This pulse is inverted by the amplifier to drive the transistor ON.

## Printer Application For The UGN-3501T

The application below is for a sensor that will sense lobes on the character drum. Lobes are spaced
$\approx 3 / 16^{\prime \prime}$ apart around the circumference, are $\approx 14^{\prime \prime}$ long and rise 10 to 15 mils from the surface of the drum.
 used with an Indiana General Magnet Products Co. SR8522 magnet. The North pole is fixed to the reverse side of the " T "' pack. A flux concentrator is fixed to the branded face of the ' T '" pack. Though it does not provide a flux return path, a concentrator will "focus" the magnetic field through the switch.

The concentrator "blade" at right is aligned with the drum lobe at an air gap distance of $0.01^{\prime \prime}$. The output change is 10 mV peak, amplified as shown to develop a +3 volt output from the operational amplifier, driving the transistor ON.

Sensitivity is so great in this configuration the UGN-3501T output signal base line tracked the eccentricities in the drum quite closely. This affected the lobe resolution, but the lobe position may still be measured.


DWG. NO. A- 11073

## APPLICATIONS FOR TYPE UGN-3501M SENSORS

Type UGN-3501M sensors are well-suited for accurate measurement and/or control of position, weight, thickness, velocity, current, etc. The device provides a linear differential output which is a function of magnetic field intensity, with a typical sensitivity of 1.4 volts/ 1000 gauss.

Either magnetic pole can be used. Pins 1 and 8 are sinking and sourcing terminals for the differential output. Changing poles inverts the output. Connections may be reversed to account for this change.

The figure below shows a $20 \Omega$ trimmer potentiometer being used for output offset nulling. Pins 5, 6 , and 7 may be shorted if an output offset voltage of up to $\pm 400 \mathrm{mV}$ can be tolerated.


## OUTPUT VOLTAGE

 AS A FUNCTION OF MAGNETIC FLUX DENSITY

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, VCC . . . . . . . . . . . . . . . . . . . . . . . . . +16 V
Output Current, IOUT . . . . . . . . . . . . . . . . . . . . . . . . . . . 2mA
Magnetic Flux Density, B . . . . . . . . . . . . . . . . . . . . . No Limit
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots \ldots \ldots 0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature Range, TS $\ldots \ldots \ldots \ldots .65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

DWi. No. A- 10.972
ELECTRICAL CHARACTERISTICS at $V_{C C}=12$ VDC, $T_{A}=+25^{\circ}$ (unless otherwise specified)

| Characteristic | Symbol | Test Conditions | Min. | Typ. | Max. | Units | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Voltage | VCC |  | 8.0 | - | 16 | $V$ | - |
| Supply Current | ICC | $\mathrm{V}_{\text {CC }}=16 \mathrm{~V}$ | - | 10 | 18 | mA | - |
| Output Offset Voltage | V0FF | $\mathrm{B}=0$ Gauss, $\mathrm{R}-5-6-7=0 \Omega$ | - | 100 | 400 | mV | 1 |
| Output Common Mode Voltage | $V_{C M}$ | $B=0$ Gauss | - | 3.6 | - | $V$ | 1 |
| Sensitivity | $\triangle V_{\text {OUT }}$ | $\mathrm{B}=1000$ Gauss, R5-6-7 $=0 \Omega$ | 700 | 1400 | - | mV | 1,2 |
| Sensitivity | $\Delta V_{\text {OUT }}$ | $\mathrm{B}=1000$ Gauss, R5-6 $=15 \Omega$ | 650 | 1300 | - | mV | 1,2 |
| Frequency Response | $\mathrm{f}(-3 \mathrm{~dB})$ | R5-6-7 $=0 \Omega$ | - | 25 | - | kHz | - |
| Broadband Output Noise | $\mathrm{e}_{\mathrm{n}}$ | 3dB B.W. 10 Hz to 10 kHz $R 5-6-7=0 \Omega$ | - | 0.15 | - | mV | - |
| Output Offset Voltage vs $\mathrm{T}\left({ }^{\circ} \mathrm{C}\right)$ | $\Delta V_{\text {OFF }} / \Delta \mathrm{T}$ | R5-6-7 $=0 \Omega$ | - | 0.2 | - | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ | - |

NOTE 1. All output voltage measurements are made with a voltmeter having an input impedance of $10 \mathrm{k} \Omega$ or greater and a common mode rejection ratio greater than 60 dB .
2. Magnetic flux density is measured at the most sensitive area of the device, which is on the top center, $0.037 \pm 0.001^{\prime \prime}(0.94 \pm 0.03 \mathrm{~mm})$ below the surface.

## Motion Measurement With Permanent Magnets

The UGN-3501M, properly biased, will produce the output voltage values shown below when activated in a head-on mode of operation.

Note the output voltage curve is almost linear over the first $0.04^{\prime \prime}$ of travel. The change rate here is 10 $\mathrm{mV} / 0.001^{\prime \prime}$ air gap change.


The same magnet used in a 'slide-by'" mode of operation will produce the three curves presented at bottom.

Movement measurements would generate the largest outputs and most accurate readings where they are centered on the steepest portion of each curve, and are confined to the linear segment of that curve. This is the case for the head-on and the slideby curves.

For example, in a slide-by mode of operation with an $0.03^{\prime \prime}$ air gap, movement to be measured could be centered at a "zero"' of 0.1 ' from the centerline. The voltage rate of change would be linear at 5 $\mathrm{mV} / 0.001^{\prime \prime}$ movement, for a movement distance of $\pm 0.02^{\prime \prime}$.

The rate of change is, of course, a function of the flux density gradient across the magnetic field for the particular magnet used. A samarium-cobalt magnet, with its relatively compact field, can produce voltage change rates to $30 \mathrm{mV} / 0.001^{\prime \prime}$ movement.


## UGN-3501M Output Circuit Design

The output current handling capability of the UGN- 3501 M is 0.5 mA . In the differential connection one output pin sources load current, the other must sink it. A simple method for increasing drive capability is illustrated below.


A $4.3 \mathrm{k} \Omega$ resistor is connected from each output pin to ground. The quiescent bias current of the output stage is increased, and the sinking capability is increased to 1 mA .

If even higher current drive capability is required, the simplest solution is the addition of a pair of emitter-followers:


Up to 30 mA of load current can be sourced by the circuit as shown, and this can be increased considerably by using Darlington power transistors and lower resistance in the emitter circuits.

Note that the emitter-followers have no voltage gain. The output voltage differential is essentially the same as that of the UGN-3501M.

An operational amplifier will supply a voltage gain and a current gain, and transform the differential output of the UGN-3501M to a single-ended output. (The circuit will drive a load which has one side grounded.)


The LM-324 quad operational amplifier will operate from a single power supply if the output does not swing in the negative direction. Pin 1 of the UGN3501M does swing negative when a magnetic South pole approaches the device surface. Pin 1, therefore, is connected to the negative or inverting input of the LM-324, and its output swings in the positive direction. Reversing connections to pins 1 and 8 allows the output to respond to a magnetic North pole. If the application requires the output be capable of swing both negative and positive, then a dual $\pm$ power supply would have to be used.

Voltage amplification $\approx \frac{R_{2}}{R_{1}}$
with

$$
\begin{aligned}
& R_{1}=R_{3} \\
& R_{2}=R_{4}
\end{aligned}
$$

The LM- 324 can source 40 mA . Other operational amplifiers suitable for single supply operation are MC-3403P, MC-3458P1, CA-3160E.

## Current Sensing Applications

The UGN-3501M is ideally suited for current measurement applications. Typical applications are overload detectors for electric motors, current limiters for high-current power supplies, clamp-on current probes for high-current d-c loads, etc.

The standard toroid is typical of small commercially-available electromagnetic devices which can be used with the UGN-3501M:


UGN3501M

With this toroid, the UGN-3501M, fixed in the gap, would "see" 5.6 gauss per ampere-turn. To "read" from zero to 20 amperes, 9 turns would develop $9 \times 20 \times 5.6=1008$ gauss. The UGN3501 M would have a 1.4 volt output with a 20 ampere activating current.

## Gaussmeter Applications

A typical UGN-3501M has a differential output of 1400 mV in a 1000 gauss field. Using a $100 \mu \mathrm{~A}$ movement, with a series calibrating trimmer potentiometer, a simple gaussmeter suitable for many applications can be easily produced:


The UGN-3501M is quite linear to $\approx 1000$ gauss. The input differential stage gain must be reduced to maintain linearity beyond this range.

A $47 \Omega \pm 5 \%$ resistor in series with pins 5 and 6 extends the useful linear range to 3000 gauss:


## Calibrating The UGN-3501M Gaussmeter

Where applications require the differential output voltage at pins 1 and 8 be calibrated, dual precision 100 ohm variable resistors may be used:


A calibration field can be constructed using standard Stancor C-2709 filter chokes, with the pole pieces removed and the center magnetic path completed with a section of the pole piece removed. Brass stock ${ }^{1 / 16^{\prime \prime}} \mathrm{x}^{1 / 2^{\prime \prime}} \times 43 / 8^{\prime \prime}$ was used for mechanical support, 2 pieces in the front and 2 pieces in the rear, plus $41^{1 /{ }^{\prime \prime}} \times 1^{\prime \prime}$ No. $6-32$ threaded standoffs. The air gap was set at $3 / 8^{\prime \prime}$ as depicted below.


5\%. 20. 410.348

The chokes are wired in series opposing, and are driven from a constant current source. Initial calibration may be accomplished with a UGN- 3600 Hall generator supplied with a calibration curve. The current is fixed at the value which produces 1000 gauss.

The UGN-3501M to be calibrated is "zeroed" and placed in the 1000 gauss field. The dual precision variable resistor is adjusted until the output is 1 volt. The UGN-3501M circuit is re-zeroed out of the field and the calibration rechecked.

The value of the precision variable resistor is then measured. Two $1 \%$ resistors of the closest standard value replace these in the final circuit configuration.

## Check Oscillation Problems

The UGN-3501M has a relatively wide band width. Oscillation is the most common problem encountered in applications for the device, caused by excessive lead lengths ( $2^{\prime \prime}$ ) on the zero control, and coupling between the zero control leads and the output leads from pins 1 and 8 . (If moving your hand near the zero control changes the output voltage there are oscillation problems.)

Solutions to oscillation problems are: 1) cut the zero control lead lengths; 2) separate the zero control and output leads; and 3) (in extreme cases) use a low-pass filter on the output:


## Sensitivity Variations

Note that the UGN-3501M is specified with a typical sensitivity of $1.4 \mathrm{mV} /$ gauss and a minimum sensitivity of $.7 \mathrm{mV} /$ gauss. Unless a special 'sort'" is ordered, plan on this variation.

Note also that the ' 0 ', output varies typically $1 \mathrm{mV} /{ }^{\circ} \mathrm{C}$, a major factor in determining a minimum detectable long term signal.

The sensitivity varies with temperature and $\mathrm{V}_{\mathrm{CE}}$. The output voltage is a function of the load resistance. These factors are illustrated in the graphs at right.

NORMALIZED SENSITIVITY AS A FUNCTION OF TEMPERATURE


NORMALIZED SENSITIVITY AS A FUNCTION OF V $\mathbf{c c}$


RELATIVE OUTPUT VOLTAGE AS A FUNCTION OF LOAD RESISTANCE


## Type UGN-3604M/UGN-3605M Hall Cells

The UGN-3604M is a basic Hall voltage generator in an 8-pin DIP package, supplied with a calibration chart. Intended for use as a design or production test aid, the UGN-3604M permits accurate measurement of magnetic field inlensity as a means of aligning magnet/Hall switch positions, and for calibrating Hall Effect sensor circuits.

A UGN-3605M is the same Hall voltage generator without a calibration chart. Supply voltage for these units is 5 volts. Below is the terminal pinning diagram for UGN-3605M.


## Applications at Sprague Electric Co.

(We use them . . . and love them)
Hall Effect ICs are designed into Sprague's own production and test equipment. Position-sensing digital switches control and monitor high-speed automatic machine operations. Hall Effect switch output provides direct input to a microprocessor-based control unit.

Data is compiled continuously from critical points in the production process. The control informs the machine operator, makes automatic adjustments, indicates manual adjustments which may be necessary, and reports on production.

Hall Effect ICs perform simultaneous control and reporting functions. Extremely reliable precise repetitive operation of these switches helps to achieve and maintain very high levels of process control and product quality.

## PACKAGE INFORMATION

Sprague's Hall Effect IC's are packaged in a special epoxy material formulated to handle severe service environments. It is impervious to all commercially available consumer and industrial solvents and degreasing compounds, oils and alkaline chemicals. It is susceptible only to hot $\left(+150^{\circ} \mathrm{C}\right)$ concentrated fuming red nitric acid applied under pressure.

The material has a continuous thermal rating of $+150^{\circ} \mathrm{C}$, and a hot-spot rating ( 100 hours) of $+170^{\circ} \mathrm{C}$. It is classed by Underwriters' Laboratories, Inc. as a self-extinguishing material. Its resistivity is $10^{15}$ ohms. Thermal coefficient of expansion ( $\mathrm{T}_{\mathrm{G}}$ ) is $30 \times 10^{-6} \mathrm{ppm} /{ }^{\circ} \mathrm{C}$.

Device leads will meet solderability requirements of Military Standard MIL-STD-202 (95\% or better solder-wetting without special preparation).

Catalog Numbering System


## 3-Pin "T" Pack or "U" Pack*

TERMINAL LEAD DESIGNATION
LOCATION OF SENSOR CIRCUIT


UGN-3013T/U
UGN-3019T/U
UGS-3019T/U UGN-3020T/U UGS-3020T/U UGN-3030T/U UGS-3030T/U UGN-3501T/U
UGN-3075T/U
UGS-3075T/U
UGN-3076T/U
UGS-3076T/U

*The " $T$ " package is $0.080^{\prime \prime}$ ( 2.03 mm ) thick; the " V " package is $0.061^{\prime \prime}$ ( 1.54 mm ) thick; All other dimensions are identical.

4-Pin "S" Pack
TERMINAL LEAD DESIGNATION
LOCATION OF SENSOR CIRCUIT


## 8-Pin "M" Package

TERMINAL LEAD DESIGNATION


UGN-3201M
UGN-3203M

UGN-3501M

## Magnet Marketplace

A strong field of magnetic components manufacturers can supply parts suitable for use in virtually any conceivable Hall Effect IC application. Comprehensive listings of these suppliers are presented in reference documents such as the Thomas Register.
Many of these firms are familiar with Hall Effect ICs application.

Magnetic components available from these manufacturers include ALNICO, rare-earth, ceramic, and plastic permanent magnets in a variety of form factors such as rods, bars, rings, sheets, etc. Ferromagnetic components for use as electro-magnets, concentrators, actuators, etc. are also available.

## SENSOR CIRCUIT LOCATION



A representative listing:
Indiana General Magnet Products Co. 405 Elm St.
Valparaiso, Indiana 46383
(219) 462-3131

Hitachi Magnetics Corporation
Edmore, Michigan 48829
(517) 427-5151

Xolox Corporation
3111 Covington Rd.
Ft. Wayne, Indiana 46804
(219) 432-4532

The Electrodyne Company, Inc. 4188 Taylor Rd.
Ontavia, Ohio 45103
(513) 732-2822

Stackpole Carbon Company
Magnet Division
Kane, Pennsylvania 16735
(814) 837-7000

Spectra-Flux, Inc.
124 Manfre Rd.
Watsonville, California 95076
(408) 722-8133

The Arnold Engineering Co.
Railroad Ave. \& West, Box G
Marengo, Illinois 60152
(815) 568-2000



## SECTION 10 - TRANSISTOR ARRAYS AND MISCELLANEOUS DEVICES

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## ULN-2031A, ULN-2032A, and ULN-2033A HIGH-CURRENT DARLINGTON TRANSISTOR ARRAYS

SPRAGUE TYPE ULN-2031A, ULN-2032A, and
ULN-2033A High-Current Darlington Transistor Arrays are comprised of seven silicon Darlington pairs on a common monolithic substrate. The Type ULN-2031A consists of 14 NPN transistors connected to form seven Darlington pairs with NPN action. The Type ULN-2032A ( $\mathrm{h}_{\mathrm{FE}}=500 \mathrm{~min}$.) and the Type ULN-2033A ( $\mathrm{h}_{\mathrm{FE}}=50 \mathrm{~min}$.) consist of seven NPN and seven PNP transistors connected to form seven Darlington pairs with PNP action. All


ULN-2031A devices feature a common emitter configuration.

These devices are especially suited for interfacing between MOS, TTL, or DTL outputs and 7-segment LED or tungsten filament indicators. Peak inrush currents to 100 mA are allowable. They are also ideal for a variety of other driver applications such as relay control and thyristor firing.
Type ULN-2031A, ULN-2032A, and ULN-2033A transistor arrays are housed in 16-lead DIP plastic packages which include a separate substrate connection for maximum circuit design flexibility.


ULN-2032A
ULN-2033A

## ABSOLUTE MAXIMUM RATINGS at $+25^{\circ} \mathrm{C}$ Free-Air Temperature (unless otherwise noted)

Power Dissipation (any one Darlington pair) ..... 500 mW
(total package). ..... 750 mW
Derating Factor Above $+25^{\circ} \mathrm{C}$ ..... $6.67 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$
Ambient Temperature Range (operating), $T_{A}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{s}}$ ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$Individual Darlington Pair Ratings:
Collector-to-Emitter Voltage, $\mathrm{V}_{\mathrm{CEO}}$ ..... 16V
Collector-to-Base Voltage, $\mathrm{V}_{\text {сво }}$ ..... 40V
Collector-to-Substrate Voltage, $\mathrm{V}_{\mathrm{c} 1}$ ..... 40V
Emitter-to-Base Voltage, $\mathrm{V}_{\text {EBO }}$
Type ULN-2031A .....  5 V
Type ULN-2032A and ULN-2033A ..... 40V
Continuous Collector Current, Ic ..... 80 mA
Continuous Base Current, $I_{B}$ ..... 5 mA

## NOTE:

The substrate must be connected to a voltage which is more negative than any collector or base voltage so as to maintain isolation between transistors, and to provide normal transistor action.

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Collector-Base Breakdown Voltage | $\mathrm{BV}_{\text {c80 }}$ | $\mathrm{I}_{\mathrm{c}}=500 \mu \mathrm{~A}$ | 40 | - | - | V |
| Collector-Substrate Breakdown Voltage | $\mathrm{BV}_{\text {clo }}$ | $\mathrm{I}_{\mathrm{c}}=500 \mu \mathrm{~A}$ | 40 | - | - | V |
| Collector-Emitter Breakdown Voltage | $\mathrm{BV}_{\text {ceo }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}$ | 16 | - | - | V |
| Emitter-Base Breakdown Voltage <br> Type ULN-2031A <br> Type ULN-2032A and ULN-2033A | $\mathrm{BV}_{\text {EBO }}$ | $\mathrm{I}_{\mathrm{E}}=500 \mu \mathrm{~A}$ | $\begin{array}{r} 5 \\ 40 \\ \hline \end{array}$ | - | - | $\begin{aligned} & V \\ & v \end{aligned}$ |
| $\begin{aligned} & \text { D-C Forward Current Transfer Ratio } \\ & \text { Type ULN-2031A and ULN-2032A } \\ & \text { Type ULN-2033A } \end{aligned}$ | $\mathrm{h}_{\text {FE }}$ | $\mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=20 \mathrm{~mA}$ | $\begin{array}{r} 500 \\ 50 \\ \hline \end{array}$ | - | 500 | - |
| Base-Emitter Saturation Voltage <br> Type ULN-2031A <br> Type ULN-2032A and ULN-2033A | $\mathrm{V}_{\text {BEISAT }}$ | $\mathrm{I}_{\mathrm{C}}=20 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=500 \mu \mathrm{~A}$ |  | - | 1 | V |
| Collector-Emitter Saturation Voltage Type ULN-2C31A and ULN-2032A Type ULN-2033A | $\mathrm{V}_{\text {CEISAT }}$ | $\begin{aligned} & I_{C}=20 \mathrm{~mA}, I_{B}=40 \mu \mathrm{~A} \\ & I_{C}=80 \mathrm{~mA}, I_{B}=1 \mathrm{~mA} \\ & I_{C}=20 \mathrm{~mA}, I_{B}=40 \mu \mathrm{~A} \\ & I_{C}=80 \mathrm{~mA}, I_{B}=2 \mathrm{~mA} \\ & \hline \end{aligned}$ | - | - | $\begin{aligned} & 1.2 \\ & 1.5 \\ & 1.2 \\ & \hline 1.5 \\ & \hline \end{aligned}$ | V V V |
| Collector Cutoff Current | $\begin{aligned} & \begin{array}{l} \mathbf{l}_{\text {ceo }} \\ \mathbf{I}_{\text {cBO }} \end{array} \\ & \hline \end{aligned}$ | $\begin{aligned} & V_{C E}=8 \mathrm{~V} \\ & V_{C B}=10 \mathrm{~V} \end{aligned}$ | - | - | $\begin{array}{r} 100 \\ 10 \\ \hline \end{array}$ | ${ }_{\mu \mathrm{A}}^{\mu \mathrm{A}}$ |

# ULS-2045H and ULN-2046A TRANSISTOR ARRAYS (Three Isolated Transistors and One Differential Amplifier) 

THE ULS-2045H and ULN-2046A are general-purpose transistor arrays each consisting of five silicon N-P-N transistors on a single monolithic chip. Two transistors are internally connected to form a differential pair. Integrated circuit construction provides close electrical and thermal matching between each transistor.

These arrays are well-suited for a wide range of applications such as: DC to VHF signal processing systems; temperature-compensated amplifiers; custom designed differential amplifiers and discrete transistors in conventional circuits.

Two package configurations are available. Type ULS-2045H is supplied in a hermetic 14-lead dual inline ceramic package and is rated for operation over the military temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.


Type ULN-2046A is electrically identical to the ULS2045 H but is supplied in a dual in-line plastic package rated for $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ambients.

## ABSOLUTE MAXIMUM RATINGS at $+25^{\circ} \mathrm{C}$ Free-Air Temperature (unless otherwise noted)

|  | ULS-2045H |  | ULN-2046A |  | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Power Dissipation: | EACH TRANSISTOR | TOTAL PACKAGE | EACH TRANSISTOR | TOTAL PACKAGE |  |
| $\mathrm{T}_{\mathrm{A}}$ to $+55^{\circ} \mathrm{C}$ |  |  | 300 | 750 | mW |
| $\mathrm{T}_{\mathrm{A}}$ to $+75^{\circ} \mathrm{C}$ | 300 | 750 | - | - | mW |
| Derating Factor: |  |  |  |  |  |
| $\mathrm{T}_{\mathrm{A}}>+55^{\circ} \mathrm{C}$ | - | - | - | 6.67 | $\mathrm{mW} /{ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{A}}>+75^{\circ} \mathrm{C}$ | - | 8 | - | - | $\mathrm{mW} /{ }^{\circ} \mathrm{C}$ |

Collector-Base Voltage, $\mathrm{V}_{\text {(BR) Сво }}$ ..... 30V
Collector-Emitter Voltage, $\mathrm{V}_{\text {(BR)CEO }}$ ..... 20V
Collector-Substrate Voltage, $\mathrm{V}_{\text {(BR)CIO }}$ (See note 2) ..... 20V
Emitter-Base Voltage, $\mathrm{V}_{(B R) \in B O}$ ..... 6 V
Collector Current, Ic ..... 50 mA
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ :
Type ULS-2045H ..... $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Type ULN-2046A
Type ULN-2046A ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ..... $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ : ..... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

## Notes:

1. The maximum ratings are limiting absolute values above which the serviceability may be impaired from the viewpoint of life or satisfactory performance. The breakdown voltages may be far above the maximum voltage ratings. To avoid permanent damage to the transistor, do not attempt to measure these characteristics above the maximum ratings.
2. Pin 13 is connected to the substrate. This terminal must be tied to the most negative point in the external circuit to maintain isolation between transistors and to provide for normal transistor action.

STATIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Collector-Base Breakdown Voltage | $V_{\text {briceo }}$ | $\mathrm{I}_{\mathrm{C}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{E}}=0$ | 20 | 60 |  | V |
| Collector-Emitter Breakdown Voltage | $V_{\text {briceo }}$ | $\mathrm{I}_{\mathrm{c}}=1 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=0$ | 15 | 24 |  | V |
| Collector-Substrate Breakdown Voltage | $\mathrm{V}_{\text {Ibecio }}$ | $\mathrm{I}_{\mathrm{c}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{Cl}}=0$ | 20 | 60 |  | V |
| Emitter-Base Breakdown Voltage | $V_{\text {IBREE }}$ | $\mathrm{I}_{\mathrm{E}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{C}}=0$ | 5 | 7 |  | V |
| Collector Cutoff Current | $\mathrm{I}_{680}$ | $\mathrm{V}_{\text {CB }}=10 \mathrm{~V}, \mathrm{~T}_{\mathrm{E}}=0$ |  |  | 40 | nA |
|  | $\mathrm{I}_{\text {cto }}$ | $\mathrm{V}_{\text {CE }}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{B}}=0$ |  |  | 0.5 | $\mu \mathrm{A}$ |
| Static Forward Current Transfer Ratio | $\mathrm{h}_{\text {fE }}$ | $\mathrm{I}_{\mathrm{C}}=10 \mu \mathrm{~A}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ |  | 54 |  | - |
|  |  | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\text {CF }}=3 \mathrm{~V}$ | 40 | 100 |  | - |
|  |  | $\mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ |  | 100 |  | - |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {ces(at) }}$ | $\mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=1 \mathrm{~mA}$ |  | 0.23 |  | V |
| Base-Emitter Voltage | $V_{\text {BE }}$ | $\mathrm{I}_{\mathrm{E}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}$ |  | 0.715 |  | V |
|  |  | $\mathrm{I}_{\mathrm{E}}=10 \mathrm{~mA}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ |  | 0.800 |  | V |
| Input Offset Current for Matched Pair $Q_{1}$ and $Q_{2}$ | $\mathrm{I}_{101} \mathrm{I}_{102}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}$ |  | 0.3 | 2 | $\mu \mathrm{A}$ |
| Magnitude of Input Offset Voltage for Differential Pair | $\mathrm{V}_{\text {BE1 } 1}-\mathrm{V}_{\mathrm{BE} 2}$ | $\mathrm{T}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ |  | 0.45 | 5 | mV |
| Magnitude of Input Offset Voltage for Isolated Transistors | $V_{\text {BE }}-V_{\text {BE }}$ | $\mathrm{I}_{\mathrm{c}}=1 \mathrm{~mA}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ |  | 0.45 | 5 | mV |
|  | $\mathrm{V}_{\text {BE } 4}-V_{\text {BES }}$ | $\mathrm{I}_{\mathrm{c}}=1 \mathrm{~mA}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ |  | 0.45 | 5 | mV |
|  | $\mathrm{V}_{\text {BE5 } 5}-\mathrm{V}_{\text {BE3 }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ |  | 0.45 | 5 | mV |
| Temperature Coefficient of Base-Emitter Voltage | $\frac{\Delta V_{B E}}{\Delta T}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}$ |  | -1.9 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Temperature Coefficient Magnitude of Input-Offset Voltage | $\frac{\Delta V_{10}}{\Delta T}$ | $\mathrm{I}_{\mathrm{c}}=1 \mathrm{~mA}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ |  | 1.1 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |

DYNAMIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Small-Signal Common-Emitter Forward Current Transfer Ratio | $\mathrm{ht}_{\text {fe }}$ | $\mathrm{T}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  | 110 |  | - |
| Small-Signal Common-Emitter Short-Circuit Input Impedance | $\mathrm{h}_{\text {i }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  | 3.5 |  | k $\Omega$ |
| Small-Signal Common-Emitter Open-Circuit Output Impedance | $\mathrm{h}_{\mathrm{oe}}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  | 15.6 |  | $\mu \mathrm{mho}$ |
| Small-Signal Common-Emitter Open-Circuit Reverse Voltage-Transfer Ratio | $\mathrm{hte}_{\text {te }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  | $1.8 \times 10^{-4}$ |  | - |
| Gain-Bandwidth Product | $\mathrm{f}_{\text {T }}$ | $\mathrm{I}_{\mathrm{c}}=3 \mathrm{~mA}, \mathrm{~V}_{\text {CE }}=3 \mathrm{~V}$ | 300 | 550 |  | MHz |
| Emitter-to-Base Capacitance | $\mathrm{C}_{\text {EB }}$ | $V_{E B}=3 \mathrm{~V}, \mathrm{I}_{\mathrm{E}}=0, \mathrm{f}=1 \mathrm{MHz}$ |  | 0.6 |  | pF |
| Collector-to-Base Capacitance | $\mathrm{C}_{\text {c }}$ | $\mathrm{V}_{C B}=3 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=0, \mathrm{f}=1 \mathrm{MHz}$ |  | 0.6 |  | pF |
| Collector-to-Substrate Capacitance | $\mathrm{Cal}_{\text {a }}$ | $\mathrm{V}_{\text {cs }}=3 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=0, \mathrm{f}=1 \mathrm{MHz}$ |  | 2.8 |  | pF |
| Noise Figure | N.F. | $\begin{aligned} & T_{\mathrm{c}}=100 \mu \mathrm{~A}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{R}_{\mathrm{g}}=1 \mathrm{k} \Omega \\ & \mathrm{f}=1 \mathrm{kHz}, \mathrm{BW}=15.7 \mathrm{kHz} \end{aligned}$ |  | 3.25 |  | dB |

NOTE:
Characteristics apply for each transistor unless otherwise specified.

## ULN-2046A-1 TRANSISTOR ARRAY

TYPE ULN-2046A-1 general-purpose transistor array consists of five silicon NPN transistors, two of which are connected as a differential amplifier. The monolithic construction provides close electrical and thermal matching between all transistors.

Except as shown in the following electrical characteristics, Type ULN-2046A-1 transistor array is identical to Type ULN-2046A.


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Collector-Base Breakdown Voltage | $\mathrm{BV}_{\text {cB0 }}$ | $\mathrm{I}_{\mathrm{C}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{E}}=0$ | 40 | 60 | - | V |
| Collector-Emitter Breakdown Voltage | $\mathrm{BV}_{\text {CEO }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=0$ | 30 | - | - | V |
| Collector-Substrate Breakdown Voltage | $\mathrm{BV}_{\text {cio }}$ | $\mathrm{I}_{\mathrm{C}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{Cl}}=0$ | 40 | 60 | - | V |
| Collector Cutoff Current | $\mathrm{I}_{\text {CBO }}$ | $\mathrm{V}_{\text {CB }}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{E}}=0$ | - | - | 100 | nA |
|  | $\mathrm{I}_{\text {ceo }}$ | $\mathrm{V}_{\text {CE }}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{B}}=0$ | - | - | 5.0 | $\mu \mathrm{A}$ |
| Static Forward Current Transfer Ratio | $\mathrm{h}_{\mathrm{FE}}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}$ | 30 | 100 | - |  |

NOTE:
Pin 13 is connected to the substrate. This terminal must be tied to the most negative point in the external circuit to maintain isolation between transistors and to provide for normal transistor action.

# ULN-2047A TRANSISTOR ARRAY (Three Differential Amplifiers) 

TYPE ULN-2047A is a silicon NPN multiple transistor array comprising three independent differential amplifiers. It is specifically intended for use in switching applications such as electronic organ keyboards. All base leads are brought out on one side of the 16-lead plastic dual in-line package to simplify printed wiring board layout. A separate substrate connection permits maximum circuit design flexibility.

Type ULN-2047A is supplied in a 16-pin dual in-line plastic package.


## ABSOLUTE MAXIMUM RATINGS <br> at $25^{\circ} \mathrm{C}$ Free-Air Temperature


*Derate at the rate of $6.67 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$.

| ELECTRICAL CHARACTERISTICS at $25^{\circ} \mathrm{C}$ Free-Air Temperature |  |
| :---: | :---: |
| Collector-Emitter Breakdown Voltage, $\mathrm{BV}_{\text {cEO }}$ (note 1) <br> at $I_{c}=5 \mathrm{~mA}$. |  |
| Emitter Cutoff Current, $\mathrm{I}_{\text {EBO }}$ (note 2) at $V_{E B}=5 \mathrm{~V}$ | . 100 nA Max. |
| Collector Cutoff Current, I ICES (note 1) at $\mathrm{V}_{\mathrm{CE}}=25 \mathrm{~V}$. | . 100 nA Max. |
| D-C Forward Current Transfer Ratio, $\mathrm{h}_{\mathrm{FE}}$ (note 1) $\begin{aligned} & \text { at } V_{C E}=2 V, I_{C}=0.1 \mathrm{~mA} \\ & \text { at } V_{C E}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA} . \end{aligned}$ | 30 Min . 75 Min . |
| Differential Input Offset Voltage, $\mathrm{V}_{10}$ (note 1) $\text { at } \mathrm{V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C} 1}=\mathrm{I}_{\mathrm{C} 2}=1 \mathrm{~mA}$ | 5 mV Max. |

## NOTES:

1. All other pins common to emitter of transistor under test.
2. Base and collector of associated transistor connected to emitter, all other pins common to base of transistor under test.

## ULN-2054A TRANSISTOR ARRAY (Dual Independent Differential Amplifiers)

THE ULN-2054A is a transistor array consisting of six silicon NPN transistors on a single monolithic chip. The transistors are internally interconnected to form two independent differential amplifiers.

The ULN-2054A is intended for a wide range of applications requiring extremely close electrical and thermal matching characteristics. Some applications are: cascade limiter circuits; balanced mixer circuits; balanced quadrature/synchronous detector circuits; balanced (push-pull) cascade/sense/IF amplifier circuits; or in almost any multifunction system requiring RF / Mixer/Oscillator, converter/IF functions.

Available in a 14 -lead dual in-line plastic package the ULN-2054A is rated for operation over a $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ambient temperature range.


Other features are:

- Input Offset Voltage -5 mV max.
- Input Offset Current - $2 \mu \mathrm{~A}$ max.
- Voltage gain (single-stage double ended output) - 32 dB typ.
- Common-Mode Rejection Ratio (each amplifier) - 100 dB typ.


## ABSOLUTE MAXIMUM RATINGS at $+25^{\circ} \mathrm{C}$ Free-Air Temperature (unless otherwise noted)

Power Dissipation $\mathrm{T}_{\mathrm{A}}$ to $+55^{\circ} \mathrm{C}$ :

Each Transistor.
.300 mW
Total Package .750 mW
Derating Factor, Total Package, $\mathrm{T}_{\mathrm{A}} \geq 55^{\circ} \mathrm{C}$ $6.67 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$
Collector-Base Voltage, $\mathrm{V}_{\text {(вв) } \text { )во }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20 V
Collector-Substrate Voltage, $\mathrm{V}_{\text {(BR)CIO }}$ (See note 2) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20 V

Emitter-Base Voltage, $\mathrm{V}_{(\mathrm{BR}) \text { EBO }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 5 V
Collector Current, $\mathrm{I}_{\mathrm{c}}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 50 mA
Base Current $I_{B} \ldots \ldots$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 5 mA



[^54]STATIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Collector-Base Breakdown Voltage | $\mathrm{V}_{\text {Bricgo }}$ | $\mathrm{I}_{\mathrm{C}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{E}}=0$ | 20 | 60 |  | V |
| Collector-Substrate Breakdown Voltage | $\mathrm{V}_{\text {(8RCIIO }}$ | $\mathrm{I}_{\mathrm{c}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{Cl}}=0$ | 20 | 60 |  | V |
| Collector-Emitter Breakdown Voltage | $V_{\text {briceo }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{I}_{\mathrm{B}}=0$ | 15 | 24 |  | V |
| Emitter-Base Breakdown Voltage | $V_{\text {Brebeio }}$ | $\mathrm{I}_{\mathrm{E}}=10 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{c}}=0$ | 5 | 7 |  | V |
| Collector Cutoff Current | $\mathrm{I}_{\text {c80 }}$ | $\mathrm{V}_{\text {CB }}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{E}}=0$ |  |  | 100 | nA |
| Base-Emitter Voltage | $\mathrm{V}_{\text {BE }}$ | $\mathrm{I}_{\mathrm{C}}=50 \mu \mathrm{~A}, \mathrm{~V}_{\text {CB }}=3 \mathrm{~V}$ |  | 0.630 | 0.700 | V |
|  |  | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\text {CB }}=3 \mathrm{~V}$ |  | 0.715 | 0.800 | V |
|  |  | $\mathrm{I}_{\mathrm{c}}=3 \mathrm{~mA}, \mathrm{~V}_{\text {cB }}=3 \mathrm{~V}$ |  | 0.750 | 0.850 | V |
|  |  | $\mathrm{I}_{\mathrm{c}}=10 \mathrm{~mA}, \mathrm{~V}_{\text {CB }}=3 \mathrm{~V}$ |  | 0.800 | 0.900 | V |
| Temperature Coefficient of Base-Emitter Voltage | $\frac{\Delta V_{B E}}{\Delta T}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{C B}=3 \mathrm{~V}$ |  | -1.9 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Input Offset Voltage | $V_{10}$ | $\mathrm{E}_{\mathrm{E}(03)}=\mathrm{I}_{\mathrm{E}_{(04)}=2 \mathrm{~mA}, \mathrm{~V}_{C B}=3 \mathrm{~V}}$ |  | 0.45 | 5 | mV |
| Input Offset Current | $0_{10}$ | $\mathrm{I}_{\text {E(03) }}=\mathrm{I}_{\mathrm{E}(04)}=2 \mathrm{~mA}, \mathrm{~V}_{\text {CB }}=3 \mathrm{~V}$ |  | 0.3 | 2 | $\mu \mathrm{A}$ |
| Input Bias Current | 1 | $\mathrm{I}_{\mathrm{E}(03)}=\mathrm{I}_{\mathrm{E}(04)}=2 \mathrm{~mA}, \mathrm{~V}_{\text {CB }}=3 \mathrm{~V}$ |  | 10 | 24 | $\mu \mathrm{A}$ |
| Quiescent Operating Current Ratio | $\frac{I_{\text {coli }}}{I_{\text {coue }}}$ | $\mathrm{I}_{\text {E(3) }}=2 \mathrm{~mA}, \mathrm{~V}_{\text {CB }}=3 \mathrm{~V}$ |  | 0.98-1.02 |  | - |
|  | $\frac{I_{\operatorname{cose}}}{T_{\operatorname{cose}}}$ | $\mathrm{I}_{\mathrm{E}(4)}=2 \mathrm{~mA}, \mathrm{~V}_{\text {СВ }}=3 \mathrm{~V}$ |  | 0.98-1.02 |  | - |
| Temperature Coefficient Magnitude of Input-Offset Voltage | $\frac{\Delta V_{10}}{\Delta \mathrm{~T}}$ | $I_{E(03)}=I_{E(04)}=2 \mathrm{~mA}, \mathrm{~V}_{C B}=3 \mathrm{~V}$ |  | 1.1 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |

DYNAMIC ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. |  |
| Common-Mode Rejection Ratio For Each Amplifier | CMR | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-6 \mathrm{~V}, \mathrm{~V}_{\mathrm{X}}=3.3 \mathrm{~V}, \\ & \mathrm{f}=1 \mathrm{kHz} \text { (See figure 1) } \end{aligned}$ |  | 100 |  | dB |
| AGC Range, One Stage | AGC | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-6 \mathrm{~V}, \mathrm{~V}_{\mathrm{X}}=3.3 \mathrm{~V} \\ & \mathrm{f}=1 \mathrm{kHz} \text { (See figure 2) } \end{aligned}$ |  | 75 |  | dB |
| Voltage Gain, Single Stage Double-Ended Output | $\mathrm{A}_{v}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-6 \mathrm{~V}, \mathrm{~V}_{\mathrm{X}}=3.3 \mathrm{~V}, \\ & \mathrm{f}=1 \mathrm{kHz} \text { (See figure 2) } \end{aligned}$ |  | 32 |  | dB |
| AGC Range, Two Stage | AGC | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-6 \mathrm{~V}, \mathrm{~V}_{\mathrm{X}}=3.3 \mathrm{~V} ; \\ & \mathrm{f}=1 \mathrm{kHz}(\text { See figure 3) } \end{aligned}$ |  | 105 |  | dB |
| Voltage Gain, Two Stage <br> Double-Ended Output | $\mathrm{A}_{v}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-6 \mathrm{~V}, \mathrm{~V}_{\mathrm{x}}=3.3 \mathrm{~V}, \\ & \mathrm{f}=1 \mathrm{kHz} \text { (See figure 3) } \end{aligned}$ |  | 60 |  | dB |
| Small-Signal Common-Emitter Forward Current Transfer Ratio | $\mathrm{h}_{\text {fe }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  | 110 |  | - |
| Small-Signal Common-Emitter Short-Circuit Input Impedance | $\mathrm{h}_{\mathrm{ie}}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  | 3.5 |  | k $\Omega$ |
| Small-Signal Common-Emitter Open-Circuit Output Impedance | $\mathrm{h}_{\text {oe }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  | 15.6 |  | $\mu \mathrm{mho}$ |
| Small-Signal Common-Emitter Open-Circuit Reverse Voltage-Transfer Ratio | $\mathrm{h}_{\text {re }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}, \mathrm{~V}_{C E}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  | $1.8 \times 10^{-4}$ |  | - |
| Gain-Bandwidth Product (for Single Transistor) | $\mathrm{f}_{\text {T }}$ | $\mathrm{I}_{\mathrm{C}}=3 \mathrm{~mA}, \mathrm{~V}_{\mathrm{CE}}=3 \mathrm{~V}$ |  | 550 |  | MHz |
| Noise Figure (for Single Transistor) | N.F. | $\begin{aligned} & \mathrm{V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}, \mathrm{I}_{\mathrm{C}}=100 \mu \mathrm{~A}, \\ & \mathrm{R}_{\mathrm{g}}=1 \mathrm{k} \Omega, \mathrm{BW}=15.7 \mathrm{kHz} \end{aligned}$ |  | 3.25 |  | dB |
| Noise Figure (for each Amplifier) | N.F. | $\mathrm{f}=100 \mathrm{MHz}$ |  | 8 |  | dB |

NOTE:
Characteristics apply for each transistor unless otherwise specified.

## AMPLIFIER TEST CIRCUITS



COMMON MODE REJECTION RATIO
Figure 1


SINGLE-STAGE VOLTAGE GAIN
Figure 2


TWO-STAGE VOLTAGE GAIN
Figure 3

## ULN-2081A and ULN-2082A GENERAL PURPOSE HIGH-CURRENT TRANSISTOR ARRAYS

$S^{P}$PRAGUE TYPE ULN-2081A and ULN-2082A Transistor Arrays are comprised of seven highcurrent silicon NPN transistors on a common monolithic substrate. The Type ULN-2081A is connected in a common-emitter configuration and the Type ULN-2082A is connected in a common-collector configuration.

Both arrays are capable of directly driving seven segment displays and LED displays. They are ideal for a variety of other driver applications such as relay control and thyristor firing.

Type ULN-2081A and ULN-2082A are housed in 16-lead DIP plastic packages which include a separate substrate connection for maximum circuit design flexibility.


ULN-2081A


ULN-2082A

## ABSOLUTE MAXIMUM RATINGS

| Power Dissipation (any one transistor) (total package). | .500 mW .750 mW |
| :---: | :---: |
| Ambient Temperature Range (operating) | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Individual Transistor Ratings: |  |
| Collector-to-Emitter Voltage, $\mathrm{V}_{\text {ceo }}$ | 16 V |
| Collector-to-Base Voltage, $\mathrm{V}_{\text {CBO }}$ | 20 V |
| Collector-to-Substrate Voltage, $\mathrm{V}_{\text {cıo }}$ | 20 V |
| Emitter-to-Base Voltage, $\mathrm{V}_{\text {EBO }}$ | 5 V |
| Collector Current, $\mathrm{I}_{\mathrm{C}}$ | 200 mA |
| Base Current, $I_{B}$ | 20 mA |

NOTE:
The collector of each transistor in the Type ULN-2081A and ULN-2082A is isolated from the substrate by an integral diode. The substrate must be connected to a voltage which is more negative than any collector voitage so as to maintain isolation between transistors, and to provide normal transistor action. Undesired coupling between transistors is avoided by maintaining the substrate terminal ( 5 ) at either $\mathrm{d}-\mathrm{c}$ or signal (a-c) ground. An apprupriate bypass capacitor can be used to establish a signal ground.

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Collector-Emitter Breakdown Voltage | $\mathrm{BV}_{\text {CES }}$ | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}$ | 20 | 80 |  | V |
| Collector-Substrate Breakdown Voltage | $\mathrm{BV}_{\text {CIE }}$ | $\mathrm{I}_{\mathrm{Cl}}=500 \mu \mathrm{~A}$ | 20 | 80 |  | V |
| Collector-Emitter Breakdown Voltage | $\mathrm{BV}_{\text {ceo }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}$ | 16 | 40 |  | V |
| Emitter-Base Breakdown Voltage | $\mathrm{BV}_{\text {EBO }}$ | $\mathrm{I}_{\mathrm{C}}=500 \mu \mathrm{~A}$ | 5 | 7 |  | V |
| Forward Current Transfer Ratio | $h_{\text {FE }}$ | $\mathrm{V}_{C E}=0.5 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=30 \mathrm{~mA}$ | 30 | 80 |  |  |
|  |  | $\mathrm{V}_{\mathrm{CE}}=0.8 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=50 \mathrm{~mA}$ | 40 | 85 |  |  |
| Base-Emitter Saturation Voltage | $\mathrm{V}_{\text {be(SAT) }}$ | $I_{c}=30 \mathrm{~mA}$ |  | 0.75 | 1 | V |
| Collector-Emitter Saturation Voltage | $V_{\text {CEISAT }}$ | $\mathrm{I}_{\mathrm{C}}=30 \mathrm{~mA}$ |  | 0.13 | 0.5 | V |
|  |  | $\mathrm{I}_{\mathrm{C}}=50 \mathrm{~mA}$ |  | 0.2 | 0.7 | V |
| Collector Cutoff Current | $\mathrm{I}_{\text {ceo }}$ | $V_{C E}=10 \mathrm{~V}$ |  |  | 10 | $\mu \mathrm{A}$ |
|  | $\mathrm{I}_{\text {cBO }}$ | $V_{C B}=10 \mathrm{~V}$ |  |  | 1 | $\mu \mathrm{A}$ |

# ULN-2083A and ULS-2083H TRANSISTOR ARRAYS (Five Independent NPN Transistors) 

DESIGNED for use in general purpose, medium current (to 100 mA ) switching and differential amplifier applications, the ULN-2083A and ULS2083 H transistor arrays each consist of five NPN transistors on a single monolithic chip. Two transistors are matched at low currents ( 1 mA ) making them ideal for use in balanced mixer circuits, push-pull amplifiers, and other circuit functions requiring close thermal and offset matching.

A separate substrate connection permits maximum circuit design flexibility. In order to maintain isolation between transistors and provide normal transistor action, the substrate must be connected to a voltage which is more negative than any collector voltage. The substrate terminal (pin 5) should therefore be maintained at either d-c ground or suitably bypassed to a-c ground to avoid undesired coupling between transistors.

Two package configurations are available. The Type ULN-2083A is supplied in a 16 -lead dual in-line plastic package for operation over the temperature range of $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. This package is similar to


JEDEC style MO-001AC. The Type ULS-2083H is electrically identical to the ULN-2083A but is supplied in a hermetic dual in-line package for operation over the temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. This package conforms to the dimensional requirements of Military Specification MIL-M-38510 and can meet all of the applicable environmental requirements of Military Standard MIL-STD-883.

## ABSOLUTE MAXIMUM RATINGS at $+25^{\circ} \mathrm{C}$ Free-Air Temperature

| Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ (any one transistor) <br> (total package) | $\begin{aligned} & .500 \mathrm{~mW} \\ & .750 \mathrm{~mW}^{*} \end{aligned}$ |
| :---: | :---: |
| Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ (ULN-2083A) | $20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| (ULS-2083H) | $55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Storage Temperature Range, $\mathrm{T}_{\mathbf{S}}$ | $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

*Derate at the rate of $6.67 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$.

ELECTRICAL CHARACTERISTICS at $+25^{\circ}$ C Free-Air Temperature

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Collector-Base Breakdown Voltage | $\mathrm{BV}_{\text {cBO }}$ | $\mathrm{I}_{\mathrm{C}}=100 \mu \mathrm{~A}$ | 20 | 60 | - | V |
| Collector-Emitter Breakdown Voltage | $\mathrm{BV}_{\text {CEO }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}$ | 15 | 24 | - | V |
| Collector-Substrate Breakdown Voltage | $\mathrm{BV}_{\mathrm{ClO}}$ | $\mathrm{T}_{\mathrm{Cl}}=100 \mu \mathrm{~A}$ | 20 | 60 | - | V |
| Emitter-Base Breakdown Voltage | $\mathrm{BV}_{\text {EBO }}$ | $\mathrm{I}_{\mathrm{E}}=500 \mu \mathrm{~A}$ | 5.0 | 6.9 | - | V |
| Collector Cutoff Current | $\mathrm{I}_{\text {ceo }}$ | $\mathrm{V}_{\mathrm{CE}}=10 \mathrm{~V}$ | - | - | 10 | $\mu \mathrm{A}$ |
|  | $\mathrm{I}_{\text {CBO }}$ | $\mathrm{V}_{\mathrm{CB}}=10 \mathrm{~V}$ | - | - | 1.0 | $\mu \mathrm{A}$ |
| Base-Emitter Voltage | $V_{\text {BE }}$ | $\mathrm{V}_{C E}=3 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA}$ | 650 | 740 | 850 | mV |
| Collector-Emitter Saturation Voltage | $\mathrm{V}_{\text {CEISAT }}$ | $\mathrm{T}_{\mathrm{C}}=50 \mathrm{~mA} . \mathrm{I}_{\mathrm{B}}=5 \mathrm{~mA}$ | - | 400 | 700 | mV |
| D-C Forward Current Transfer Ratio | $h_{\text {FE }}$ | $\mathrm{V}_{C E}=3 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=10 \mathrm{~mA}$ | 40 | 76 | - |  |
|  |  | $\mathrm{V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=50 \mathrm{~mA}$ | 40 | 75 | - |  |
| Differential Input Offset Voltage* | $V_{10}$ | $\mathrm{V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}$ | - | 1.2 | 5.0 | mV |
| Differential Input Offset Current* | 10 | $\mathrm{V}_{\mathrm{CE}}=3 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}$ | - | 0.7 | 2.5 | $\mu \mathrm{A}$ |

[^55]D-C FORWARD CURRENT TRANSFER RATIO AS A FUNCTION OF COLLECTOR CURRENT


BASE-EMITTER SATURATION VOLTAGE AS A FUNCTION OF COLLECTOR CURRENT


DIFFERENTIAL INPUT OFFSET VOLTAGE AS A FUNCTION OF COLLECTOR CURRENT


COLLECTOR-EMITTER SATURATION VOLTAGE AS A FUNCTION OF COLLECTOR CURRENT



BASE-EMITTER VOLTAGE AS A FUNCTION OF COLLECTOR CURRENT


DIFFERENTIAL INPUT OFFSET CURRENT AS A FUNCTION OF COLLECTOR CURRENT


## ULN-2083A-1 TRANSISTOR ARRAY

This device is a general-purpose transistor array for use in medium-current switching and differential amplifier applications. With the exception of the increased breakdown voltages shown below, Type ULN-2083A-1 is identical to Type ULN-2083A transistor array.


ELECTRICAL CHARACTERISTICS at $+25^{\circ}$ C Free-Air Temperature

|  |  | Limits |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Characteristic | Test Conditions | Min. | Typ. | Max. | Units |
| Collector-Base Breakdown Voltage | $\mathrm{BV}_{\text {CB0 }}$ | $\mathrm{I}_{\mathrm{C}}=100 \mu \mathrm{~A}$ | 40 | 60 | - | V |
| Collector-Emitter Breakdown Voltage | $\mathrm{BV}_{\text {сЕ }}$ | $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~mA}$ | 30 | - | - | V |

## ULN-2086A TRANSISTOR ARRAY

Type ULN-2086A general-purpose transistor array consists of five silicon NPN transistors, two of which are connected as a differential amplifier. The monolithic construction provides close electrical and thermal matching between all transistors.

With the exception of the collector cutoff current specifications listed below and the omission of guaranteed limits on input offset voltage and input offset current, Type ULN-2086A is identical to Type ULN-2046A transistor array.


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic |  | Limits |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Symbol | Test Conditions | Min. | Typ. | Max. | Units |
|  | $\mathrm{I}_{\text {CBO }}$ | $\mathrm{V}_{\mathrm{CB}}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{E}}=0$ | - | - | 100 | nA |
|  | $\mathrm{I}_{\text {CEO }}$ | $\mathrm{V}_{\mathrm{CE}}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{B}}=0$ | - | - | 5.0 | $\mu \mathrm{~A}$ |

NOTE: The substrate terminal must be tied to the most negative point in the external circuit to maintain isolation between transistors and to provide for
normal transistor action.

# SERIES 2140 HIGH-PERFORMANCE QUAD CURRENT SWITCHES 

FEATURES<br>- Variable Reference: -3 to - 10 Volts<br>- Low Temperature Coefficient: $5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$<br>- Fast Settling: 300 ns to $0.01 \%$<br>- TTLCMOS Compatible Inputs

SERIES 2140 quad current switches are high precision monolithic integrated circuits for use in digital-to-analog converters. Each device contains four logic-controlled current switches and a reference transistor. Continuously running current sources and superior thermal layout, maximize speed and accuracy by reducing transitional anomalies. Series 2140 switches accept a wide range of d-c references or an a-c reference for two-quadrant mutiplying D/A applications. Inputs may be driven from TTL, or similar sources and are independent of reference voltage level.

Type ULN-2140A switches are rated for operation over the temperature range of $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$; the ' A ' suffix indicates a 14 -pin dual in-line plastic package. Type ULS-2140H switches are rated for operation over the extended temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$; the ' H ' suffix indicates a dual in-line hermetic package to Military Specification MIL-M-38510. Devices in unpackaged, chip form, for use in hybrid circuit applications, are designated by changing the suffix letter from A or H to C .
On special order, hermetically sealed quad current switches with highreliability screening to MIL-STD-883 are available by adding the suffix 'MIL' to the part number, for example, ULS-2140H-MIL. Also, on special order, devices with improved linearity and drift can be supplied.

## ABSOLUTE MAXIMUM RATINGS

[^56]ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{cc}}=+5 \mathrm{to}+15 \mathrm{~V}, \mathbf{V}_{\mathrm{EE}}=-15 \mathrm{~V}, \mathrm{I}_{\mathrm{mSB}}=1 \mathrm{~mA}$, Operational Amplifier Summing Junction Load (unless otherwise noted)

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| " 0 " Input Voltage | $\mathrm{V}_{\text {(NO) }}$ |  | - | - | 0.8 | V |
| "1" Input Voltage | $V_{\text {N(w) }}$ |  | 2.0 | - | - | V |
| "0" Input Current | $1{ }^{\text {ma }}$ ( $)$ | $V_{\text {N }}=0.8 \mathrm{~V}$ | - | - | -1.0 | $\mu \mathrm{A}$ |
| "1" Input Current | $\mathrm{I}_{\text {(1) }}$ | $\mathrm{V}_{\mathrm{N}}=2.4 \mathrm{~V}$ | - | - | 10 | $\mu \mathrm{A}$ |
| Output Voltage | $\mathrm{V}_{\text {out }}$ | $\mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega$ | See Note |  |  |  |
| Output Voltage Swing | $\Delta V_{\text {out }}$ | $\mathrm{R}_{\perp}=1 \mathrm{k} \Omega_{\text {, }}$ Logic $=0000$ to 1111 | -2.0 | - | - | V |
| Output Current | $l_{\text {MSB }}$ | Logic $=0111$ | 2.0 | 1.0 | - | mA |
|  | $\mathrm{I}_{\mathrm{BII} 2}$ | Logic $=1011$ | 1.0 | 0.5 | - | mA |
|  | $\mathrm{I}_{\text {BII } 3}$ | Logic $=1101$ | 0.5 | 0.25 | - | mA |
|  | ILSB | Logic $=1110$ | 0.25 | 0.125 | - | mA |
| Settling Time |  | $\mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega$, To $0.01 \%$, Logic $=1000$ to 0111 | - | 300 | - | ns |
| Output Leakage Current | Iout | Logic $=1111$ | - | - | 10 | $\mu \mathrm{A}$ |
| Ref. Transistor Static Forward Current Gain | $\mathrm{hfe}_{\text {fe }}$ | $\mathrm{I}_{\mathrm{C}}=125 \mu \mathrm{~A}$ | 100 | - | - | - |
| Non-Linearity |  | Over Operating Temperature Range | - | - | 0.5 | \% |
| TC of Non-Linearity |  | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ (ULN-2140 Devices) | - | - | 20 | ppm/ ${ }^{\circ} \mathrm{C}$ |
|  |  | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ (ULS-2140 Devices) | - | - | 10 | ppm/ ${ }^{\circ} \mathrm{C}$ |
| Scale Factor Drift |  | Over Operating Temperature Range | - | 5.0 | - | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Supply Current | $\mathrm{I}_{\mathrm{cc}}$ | $V_{\text {cc }}=+15 \mathrm{~V}$ | - | 8.0 | - | mA |
|  | $\mathrm{I}_{\text {EE }}$ |  | - | -8.0 | - | mA |

Note: Output voltage with a resistive load will be a negative voltage.

## TYPICAL APPLICATION



10
$10-17$

## ULN-2401A AUTOMOTIVE LAMP MONITOR

## FEATURES

- No Standby Power
- Completely Integral to Wiring Assembly
- Monitor 1 to 8 Lamps per Channel
- Fail-Safe
- Reverse Voltage Protected
- 14-Pin Dual In-Line Plastic Package

OFFERING SEVERAL ADVANTAGES for a lamp monitoring system, the ULN-2401A monolithic integrated circuit is versatile, easily connected, and does not affect normal lamp operation. Little additional wiring is required for installation since the system is completely integral to the wiring assembly.

The ULN-2401A electronic lamp monitor was specifically designed for application in the severe automotive environment. Lateral PNP transistors provide high-frequency noise immunity and differential transient voltage protection. Reverse voltage protection, internal voltage regulators, and temperature compensation are all incorporated in the design. A failure within the device will not affect lamp operation. As a quad comparator, the ULN-2401A can also be used to monitor multiple low-voltage power supplies or, with appropriate sensors, industrial processes.

This lamp monitor operates by sensing the voltage drop in the wiring ( 50 to 100 mV ) for each lamp circuit. If any of the four comparators sees a differential input voltage of greater than 26 mV , a failure lamp is turned on. Lamp and wiring tolerances causing differential input voltages of up to 7 mV are permitted. Each comparator is capable of monitoring a mixture of one to eight similar lamps. No standby power is required because the operating voltage is obtained from the sense leads and is energized only when the lamps are turned on.


ABSOLUTE MAXIMUM RATINGS
Supply Voltage, $\mathrm{V}_{\mathrm{cc}} \ldots . .$. . . . . . . . . . . . . . . . . . . . . . . . 16 V
Peak Reverse Voltage ( 30 s ) . . . . . . . . . . . . . . . . . . . . . 6.0 V
(0.1 s) . . . . . . . . . . . . . . . . . . . 30 V

Output Current, $\mathrm{I}_{\text {out }}$. . . . . . . . . . . . . . . . . . . . . . . . . 500 mA
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots . .-35^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

EQUIVALENT LOGIC CIRCUITRY


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Operating Voltage Range | $\mathrm{V}_{\mathrm{cc}}$ |  | 10 | 13 | 16 | V |
| Output Saturation Voltage | $V_{\text {oution }}$ | $V_{\text {cC }}=10 \mathrm{~V}, \Delta V_{\text {IN }}=26 \mathrm{mV}$ | - | - | 2.2 | V |
|  |  | $\mathrm{V}_{\mathrm{CC}}=13 \mathrm{~V}, \Delta \mathrm{~V}_{\text {IN }}=26 \mathrm{mV}$ | - | - | 2.4 | V |
|  |  | $\mathrm{V}_{\mathrm{cc}}=16 \mathrm{~V}, \Delta \mathrm{~V}_{\text {iv }}=26 \mathrm{mV}$ | - | - | 2.6 | V |
| Output Leakage Current | $\mathrm{I}_{\text {ouroff }}$ | $\mathrm{V}_{\mathrm{cc}}=16 \mathrm{~V}, \Delta \mathrm{~V}_{\mathrm{IN}}=0 \mathrm{mV}$ | - | - | 6.0 | mA |
|  |  | $\mathrm{V}_{\mathrm{cc}}=16 \mathrm{~V}, \Delta \mathrm{~V}_{\mathrm{IN}}=7 \mathrm{mV}$ | - | - | 10 | mA |
|  |  | $\mathrm{V}_{\mathrm{cc}}=16 \mathrm{~V}, \Delta \mathrm{~V}_{\mathrm{IN}}=0 \mathrm{mV}$ (all inputs) | - | - | 15 | mA |

NOTE: Electrical characteristics (unless otherwise specified) apply to any one pair of comparator inputs (pins $1 \& 2$, or $9 \& 10$, or $11 \& 12$ ) with all remaining comparator inputs (including pins $3 \& 4$ ) open-circuited. To test the comparator at pins $3 \& 4$, pins $9,10,11 \& 12$ must be connected to $V_{c c}$. In application, pins 10 and 11 must both be at or near $V_{C C}$ for the comparator at pins $3 \& 4$ to be operative.

TEST CIRCUIT


SCHEMATIC


DWG.NO. B-1384

## ULN-2429A FLUID DETECTOR

## FEATURES

- High Output Current
- A-C or D-C Output
- Single-Wire Probe
- Low External Parts Count
- Internal Voltage Regulator
- Reverse Voltage Protection
- 14-Pin Dual In-Line Plastic Package


PPRIMARILY DESIGNED for use as an automotive low coolant detector, the ULN-2429A monolithic bipolar integrated circuit is ideal for detecting the presence or absence of many different types of liquids in automotive, home, or industrial applictions. Especially useful in harsh environments, reverse voltage protection, internal voltage regulation, temperature compensation, and high-frequency noise immunity are all incorporated in the design.
A simple probe, immersed in the fluid being monitored, is driven with an a-c signal to prevent plating problems. The presence, absence, or condition of the fluid is determined by comparing the loaded probe resistance with an internal (pin 8) or external (pin 6) resistance. Typical conductive fluids which can be sensed are tap water, sea water, weak acids and bases, wet soil, wine, beer, and coffee. Non-conductive fluids include most petroleum products, distilled water, dry soil, and vodka. The probe can be replaced with any variable-resistance element such as a photodiode or photoconductive cell, rotary or linear position sensor, or thermistor for detecting solids, non-conducting liquids, gases, etc.

The high-current output is typically a square wave signal for use with an LED, incandescent lamp, or loudspeaker. A capacitor can be connected (pin 12) to provide a d-c output for use with inductive loads such as relays and solenoids.

The ULN-2429A is rated for operation with a load voltage of up to 30 volts. Selected devices, for operation up to 50 V are available as the ULN-2429A-1. In all other respects, the ULN-2429A and the ULN-2429A-1 fluid detectors are identical.

These devices are furnished in an improved 14-lead dual in-line plastic package with a copper alloy lead frame for superior thermal characteristics. However, in order to realize the maximum current-handling capability of these devices, both of the output pins ( 1 and 14) and both ground pins ( 3 and 4) should be used.


FUNCTIONAL BLOCK DIAGRAM

## ABSOLUTE MAXIMUM RATINGS

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=-25^{\circ} \mathrm{C}, \mathrm{V}_{\text {CC }}=\mathbf{V}_{\text {OUT }}=+12 \mathrm{~V}$
(unless otherwise specified)

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| Supply Voltage Range | $V_{\text {cc }}$ | 13 | - | 10 | - | 16 | $V$ |
| Supply Current | $\mathrm{I}_{\mathrm{C}}$ | 13 | $\mathrm{V}_{\text {CC }}=+16 \mathrm{~V}$ | - | - | 10 | mA |
| Oscillator Output Voltage | $V_{\text {osc }}$ | 6 | $\mathrm{R}_{\mathrm{L}}=18 \mathrm{k} \Omega$ | - | 3.0 | - | $V_{p p}$ |
| Output ON Voltage | $V_{\text {Out }}$ | 1,14 | $R_{L} \geq 30 \mathrm{kS}$, OUUT $=500 \mathrm{~mA}$ | - | 0.9 | 1.5 | V |
| Output OFF Current | Iout | 1,14 | $\mathrm{R}_{\mathrm{L}} \leq 10 \mathrm{k} \Omega, \mathrm{V}_{\text {OUT }}=\mathrm{V}_{\text {OUT }}(\mathrm{max})$ | - | - | 100 | $\mu \mathrm{A}$ |
| Oscillator Frequency | $\mathrm{f}_{\text {osc }}$ | 6 | $R_{L}=18 \mathrm{k} \Omega$ | - | 2.4 | - | kHz |

## TEST CIRCUIT



## CIRCUIT SCHEMATIC



TYPICAL APPLICATIONS


## ULN-2430M TIMER

## FEATURES

- Microseconds to Minutes
- Temperature Compensated
- 400 mA Output
- 8-Pin Dual In-Line Plastic Package

PROVIDING time delays from several microseconds to approximately 10 minutes, the ULN-2430M timer was originally designed for use as a rear window heater timer in automotive applications. In typical system designs, this device will meet all of the stringent automotive environmental and transient requirements, including 'load dump'. The rugged design, the high output current rating, and an internal voltage regulator and reference allow the ULN-2430M timer to be used in many industrial applications.


## ABSOLUTE MAXIMUM RATINGS



[^57]

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ (unless otherwise noted), Fig. 1

| Characteristic | $\begin{aligned} & \hline \text { Test } \\ & \text { Pin } \end{aligned}$ | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Operating Voltage Range |  |  | 10 | - | 16 | V |
| Regulator Voltage | 5 |  | 8.4 | 9.0 | 10.1 | V |
| Output Breakdown Voltage | 2 | $\mathrm{I}_{\text {LEAK }}=100 \mu \mathrm{~A}$ | 30 | - | - | V |
| Output Saturation Voltage | 2 | $\mathrm{T}_{\text {OUT }}=400 \mathrm{~mA}$ | - | - | 2.5 | V |
|  |  | $\mathrm{I}_{\text {orr }}=250 \mathrm{~mA}$ | - | - | 1.3 | V |
| Latch Voltage | 4 | Over Op. Temp. Range | 5.5 | 7.0 | 8.0 | V |
| Trigger Threshold | 7 | $\mathrm{V}_{7} \mathrm{~N}_{5}$ | 0.60 | 0.63 | 0.67 |  |
| Reference | 8 | $\mathrm{V}_{8} / V_{5}$ | 0.58 | 0.63 | 0.68 |  |
| Temp. Coeff. of Trigger Threshold | 7 |  | -2.0 | - | -4.0 | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Trigger Input Current | 7 |  | - | 20 | 200 | nA |
| Capacitor Discharge Time | 7 | $\mathrm{C}_{1}=220 \mu \mathrm{~F}, \pm 10 \%$ | - | - | 2.0 | S |
| Supply Current | 5 | $\mathrm{V}_{\mathrm{cc}}=16 \mathrm{~V}$ | - | - | 10 | mA |

## CIRCUIT OPERATION

The basic system shown in Figure 1 provides power for the timer after the momentary closure of the 'rear window heater switch"' $S_{1}$. Momentary closure provides an input to pin 4 which turns ON the outpui driver, energizes the relay, and (through the relay contacts) provides power to the timer and the heater element. Waveforms are shown in Figure 2.
The output remains ON, supplying power to the heater until $\mathrm{V}_{7}=62 \% \mathrm{~V}_{5}$, which occurs at time $\mathrm{t}=$ $\mathrm{R}_{1} \times \mathrm{C}_{1}$. The time delay can be adjusted from several microseconds to approximately 10 minutes by the choice of $R_{1}$ and $C_{1}$. When $t=R_{1} \times C_{1}$, the comparator changes state and the relay de-energizes, returning the circuit to the quiescent condition.
Timing accuracy is primarily a function of capacitor leakage for long time delays. Hard switching of
the comparator necessitates low input bias currents on the comparator and low capacitor leakage current. The worst case comparator input is 200 nA and the charge current at $\mathrm{V}_{7}=62 \% \mathrm{~V}_{5}$ is approximately $1.7 \mu \mathrm{~A}$ for $\mathrm{R}_{1}=2 \mathrm{M} \Omega$. For these reasons, it is recommended that $R_{1}$ not exceed $2 M \Omega$ and $C_{1}$ leakage be less than 500 nA .

Diode $D_{1}$ and the circuitry associated with pin 4 provide start-stop capability for the timer. When the voltage at pin 4 is larger than 8 V timing is initiated. When less than 5.5 V , timing is stopped. Transient protection against load dump and other automotive environmental hazards is provided by the integrated circuit design and discrete components $\mathrm{Z}_{1}, \mathrm{C}_{2}, \mathrm{R}_{3}$, $R_{4}$, and $D_{1}$.

## TYPICAL APPLICATION

(Figure 1)


TIMER WAVEFORMS


## ULN-3304M SCHMITT TRIGGER <br> - ZENER CLAMPED OUTPUT

## FEATURES

- 2.2 to 6V Supply Voltage Range
- Wide Operating Temperature Range
- Stable Predictable Switching Levels
- Input to Output Isolation
- 10\% Hysteresis


DWG. NO. A-9425A

TNTENDED for driving inductive loads, the Type 1 ULN-3304M is a threshold detector with a Zener diode clamped output. The high gain circuitry can control a 150 mA load with less than 50 nA input current. This monolithic integrated circuit is often used as a low voltage relay driver in battery operated consumer electronic equipment. An important feature for these applications is that the Type ULN-3304M Schmitt trigger will sustain battery reversal indefinitely without damage.

| $E$ MAXI | GS |
| :---: | :---: |
| Supply Voltage, $\mathrm{V}_{\text {cc }}$ | 6.5 V |
| Output Current, Iour | 160 mA |
| Input Voltage, $\mathrm{V}^{\text {IN }}$ | $\mathrm{V}_{\mathrm{cc}}$ |
| Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ | 750 mW |
| Operating Temperature Range, $T_{A}$ | $-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$ |
| Storage Temperature Range, $\mathrm{T}_{\mathbf{s}}$. | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |


Output Current, Iout . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 160 mA

Power Dissipation, $\mathrm{P}_{\mathrm{D}}$. ................................. . 750 mW
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots . .-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{s}} \ldots \ldots \ldots .-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$

## SCHEMATIC



## ELECTRICAL CHARACTERISTICS at $V_{c c}=2.2$ to 6.0 V and $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ <br> (Unless Otherwise Specified)

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| "Off" Input Voltage | $V_{\text {IN(H) }}$ | 7 |  | 0.56 | 0.62 | 0.66 | $V_{\text {IN }} / V_{\text {ce }}$ |
| "On" Input Voltage | $V_{\operatorname{IN}(L)}$ | 7 |  | 0.50 | 0.55 | 0.58 | $\mathrm{V}_{\text {IN }} / \mathrm{V}_{\text {CC }}$ |
| Output Clamp Voltage | $\mathrm{V}_{\mathrm{Z}}$ | 3 | $V_{\text {IN }}=V_{C C}$ | 12 | 14 | 16 | V |
| Output Saturation Voltage | $V_{\text {CE(SAT }}$ | 3 | $V_{\text {IN }}=0$, I OUT $=100 \mathrm{~mA}$ |  |  | 0.5 | V |
|  |  |  | $\mathrm{V}_{\text {IN }}=0, \mathrm{I}_{\text {OUT }}=150 \mathrm{~mA}$ |  |  | 0.8 | V |
| Input Current | IIN | 7 | $V_{\text {IN }}=V_{C C}$ |  | 10 | 50 | nA |
| Supply Current | $\mathrm{ICC}(\mathrm{H})$ | 6 | $V_{\text {IN }}=V_{C C}=5.0 \mathrm{~V}$ |  |  | 5 | mA |
|  | $\mathrm{ICCO}_{(L)}$ | 6 | $\mathrm{V}_{\mathbb{N}}=0, \mathrm{~V}_{\text {CC }}=5.0 \mathrm{~V}$ |  |  | 13 | mA |
| Output Fall Time | $t_{f}$ | 3 |  |  |  | 0.2 | $\mu \mathrm{S}$ |
| Output Rise Time | $\mathrm{t}_{\mathrm{r}}$ | 3 |  |  |  | 0.2 | $\mu \mathrm{S}$ |
| Propagation Delay Time | $t_{\text {pd }}$ | 3 |  |  |  | 2.0 | $\mu \mathrm{S}$ |
| Threshold Stability |  |  | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$ |  | $\pm 2$ | $\pm 5$ | \% |

## TYPICAL APPLICATIONS

## 1. Sine Wave To Square Wave Converter

The input is biased to within the hysteresis region. An input with a peak-to-peak voltage greater than
$\mathrm{V}_{\text {IN(H) }}-\mathrm{V}_{\text {IN(1) }}$ (typically 70 mV ) will cause the output to switch ON and OFF producing a square wave. The symmetry of the square wave can be changed by varying the ratio of the input biasing resistors.


## TYPICAL APPLICATIONS <br> (Continued)

## 2. Light-Actuated Switch

Light falling on the photo-sensitive resistor reduces its resistance and lowers the input bias voltage causing the output to switch ON. The sensitivity can be varied by adjusting the value of the fixed resistor. For the output to switch OFF in the presence of light, interchange the two resistors.

## 3. Automotive Headlight Timer

Switch $\mathrm{S}_{1}$ controls the headlights in the normal fashion. However, if momentary switch $S_{2}$ is operated

prior to opening $S_{1}$, the self-latching contact of the relay will apply power to the headlights for the time determined by the values of R and C . For example, if R is $3.6 \mathrm{M} \Omega$ and C is $100 \mu \mathrm{~F}$, then t is 6 minutes.


## ULN-3305M DUAL SCHMITT TRIGGER - COMPLEMENTARY OUTPUTS

## FEATURES

- Stable Predictable Switching Levels
- Input to Output Isolation
- High Output Breakdown Voltage
- $10 \%$ Hysteresis

DESIGNED for use as an interface between high impedance networks and digital or resistive loads of up to 75 mA , this monolithic dual threshold detec tor features complementary outputs. The Type ULN 3305M dual Schmitt trigger is especially useful in lowcost consumer battery operated equipment and will sustain battery reversal indefinitely without damage. It is capable of operation over a supply voltage range of 2.2 to 6.0 volts and a temperature range of $-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$.

Typical applications for this device include level detectors, time delay, photoelectric controls, touch operated switches, sine to square wave converters, temperature sensitive alarms, and thyristor triggering.


ELECTRICAL CHARACTERISTICS at $\mathbf{V}_{\mathrm{cc}}=\mathbf{2 . 2}$ to $\mathbf{6 . 0 V}$ and $\mathrm{T}_{\mathrm{A}}=+\mathbf{2 5}{ }^{\circ} \mathrm{C}$ (Unless Otherwise Specified)

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| "Off" Input Voltage | $\mathrm{V}_{\text {IN( }} \mathrm{H}$ ) | 5,7 |  | 0.56 | 0.62 | 0.66 | $V_{\text {IN }} / V_{C C}$ |
| "On" Input Voltage | $V_{\operatorname{IN}(L)}$ | 5,7 |  | 0.50 | 0.55 | 0.58 | $\mathrm{V}_{\mathrm{IN}} / V_{\text {CC }}$ |
| Output Breakdown Voltage | BVCEX | 4,8 | $V_{\text {IN }}=0$ | 30 |  |  | V |
| Output Leakage Current* | $\mathrm{I}_{1}$ | 1,3 | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CC }}, \mathrm{V}_{\text {OUT }}=5.5 \mathrm{~V}$ |  |  | 12.5 | mA |
| Output Saturation Voltage | $\mathrm{V}_{\text {CEI }}$ SAT $)$ | 1,3 | $\mathrm{V}_{\mathrm{IN}}=0, \mathrm{I}_{\text {OUT }}=50 \mathrm{~mA}$ |  |  | 0.5 | V |
|  |  | 1,3 | $\mathrm{V}_{\text {IN }}=0$, I OUT $=75 \mathrm{~mA}$ |  |  | 0.8 | V |
|  |  | 4,8 | $V_{\text {IN }}=V_{\text {CC, }}$, IOUT $=50 \mathrm{~mA}$ |  |  | 0.5 | V |
|  |  | 4,8 | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CC }}$, I OUT $=75 \mathrm{~mA}$ |  |  | 0.8 | V |
| Input Current | IIN | 5,7 | $V_{\text {IN }}=V_{C C}$ |  | 10 | 50 | nA |
| Supply Current | $\operatorname{ICC}(\mathrm{H})$ | 6 | $V_{\text {IN }}=V_{\text {CC }}=5.0 \mathrm{~V}$ |  |  | 10 | mA |
|  | $\mathrm{ICC}(4)$ | 6 | $\mathrm{V}_{\mathrm{IN}}=0, \mathrm{~V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ |  |  | 25 | mA |
| Output Fall Time | $\mathrm{t}_{\mathrm{f}}$ | 1,3,4,8 |  |  |  | 0.2 | $\mu \mathrm{S}$ |
| Output Rise Time | $\mathrm{tr}_{\mathrm{r}}$ | 1, 3, 4, 8 |  |  |  | 0.2 | $\mu \mathrm{S}$ |
| Propagation Delay Time | $t_{\text {pd }}$ | 1,3,4,8 |  |  |  | 2.0 | us |
| Threshold Stability |  |  | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$ |  | $\pm 2$ | $\pm 5$ | \% |

*Output leakage current is a measure of the non-inverting output leakage current plus the base current of the inverting output.

## SCHEMATIC



## ULN-3306M DUAL SCHMITT TRIGGER

## FEATURES

- High Output Current of 150 mA
- Stable Predictable Switching Levels
- Input to Output Isolation
- $10 \%$ Hysteresis



## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\mathrm{cc}} \ldots . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . .6 .5 \mathrm{~V}$
Output Current, lout (pin 3,4)...................... 160 mA
Output Voltage, Vout (pin 4) . ........................... 20 V

Power Dissipation, $P_{D} \ldots . . . . . . . . . . . . . . . . . . . . . . . .750 \mathrm{~mW}$
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots . .-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$
Storage Temperature Range, $T_{s} \ldots \ldots . .-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$

THE Type ULN-3306M is a monolithic dual threshold detector with one output Zener diode clamped for driving inductive loads. This device is specifcally intended for use in battery operated equipments and will sustain battery reversal indefinitely without damage. It is capable of operation over a supply voltage range of 2.2 to 6.0 volts and a temperature range of $-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$.


## ELECTRICAL CHARACTERISTICS at $\mathbf{V}_{\mathrm{cc}}=2.2$ to $\mathbf{6 . 0 V}$ and $\mathrm{T}_{\mathrm{A}}=+\mathbf{2 5}{ }^{\circ} \mathrm{C}$ (Unless Otherwise Specified)

| Characteristic | Symbol | Test Pin | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. | Units |
| "Off" Input Voltage | $\mathrm{V}_{1 \mathrm{~N}}(\mathrm{H})$ | 5,7 |  | 0.56 | 0.62 | 0.66 | $V_{\text {IN }} / V_{\text {ce }}$ |
| "On" Input Voltage | $\mathrm{V}_{1}(1)$ | 5, 7 |  | 0.50 | 0.55 | 0.58 | $\mathrm{V}_{\mathbf{I N}} / V_{\text {ce }}$ |
| Output Clamp Voltage | $V_{z}$ | 3 | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CC }}$ | 12 | 14 | 16 | V |
| Output Breakdown Voltage | BVCEX | 4 | $V_{\text {IN }}=V_{\text {cc }}$ | 30 |  |  | V |
| Output Saturation Voltage | $V_{\text {CEISAT }}$ | 3,4 | $V_{\text {IN }}=0$, I $_{\text {OUt }}=100 \mathrm{~mA}$ |  |  | 0.5 | V |
|  |  |  | $\mathrm{V}_{\text {IN }}=0, \mathrm{I}_{\text {OUT }}=150 \mathrm{~mA}$ |  |  | 0.8 | V |
| Input Current | IIN | 5,7 | $V_{\text {IN }}=V_{\text {CC }}$ |  | 10 | 50 | nA |
| Supply Current | $I_{\text {CC(H) }}$ | 6 | $V_{\text {IN }}=V_{\text {CC }}=5.0 \mathrm{~V}$ |  |  | 10 | mA |
|  | $\mathrm{ICC}(1)$ | 6 | $V_{1 N}=0, V_{C C}=5.0 \mathrm{~V}$ |  |  | 25 | mA |
| Output Fall Time | $t_{t}$ | 3,4 |  |  |  | 0.2 | $\mu \mathrm{S}$ |
| Output Rise Time | $t_{r}$ | 3,4 |  |  |  | 0.2 | $\mu \mathrm{S}$ |
| Propagation Delay Time | $t_{\text {pd }}$ | 3,4 |  |  |  | 2.0 | $\mu \mathrm{S}$ |
| Threshold Stability |  |  | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$ |  | $\pm 2$ | $\pm 5$ | \% |

## TYPICAL APPLICATIONS

## 1. Sine Wave To Square Wave Converter

The input is biased to within the hysteresis region. An input with a peak-to-peak voltage greater than
$\mathrm{V}_{\text {IN(H) }}-\mathrm{V}_{\text {IN(L) }}$ (typically 70 mV ) will cause the output to switch ON and OFF producing a square wave. The symmetry of the square wave can be changed by varying the ratio of the input biasing resistors.


## TYPICAL APPLICATIONS

## (Continued)

## 2. Light-Actuated Switch

Light falling on the photo-sensitive resistor reduces its resistance and lowers the input bias voltage causing the output to switch ON. The sensitivity can be varied by adjusting the value of the fixed resistor. For the output to switch OFF in the presence of light, interchange the two resistors.

## 3. Automotive Headlight Timer

Switch $\mathrm{S}_{1}$ controls the headlights in the normal fashion. However, if momentary switch $S_{2}$ is operated

prior to opening $S_{1}$, the self-latching contact of the relay will apply power to the headlights for the time determined by the values of $\mathbf{R}$ and C . For example, if $R$ is $3.6 \mathrm{M} \Omega$ and C is $100 \mu \mathrm{~F}$, then t is 6 minutes.


## ULN-3330Y OPTOELECTRONIC SWITCH

## FEATURES

- On-Chip Photodiode
- On-Chip Amplifier
- On-Chip Trigger
- On-Chip Power Driver
- On-Chip Regulator
- Operation to 30 kHz
- T0-92 Clear Plastic Package

POOVIDING all of the necessary circuitry in a single 3-lead clear plastic package, Type ULN3330 Y Optoelectronic Switch is a monolithic integrated circuit containing a photodiode, low-level amplifier, level detector, output power driver, and voltage regulator. It can be used as a low-cost photo-detector in consumer or industrial applications and requires only the absolute minimum in external components for operation.

The photodiode has an enhanced blue response for improved sensitivity to visible light. The switch typically turns ON as illumination of the device falls below $5 \mathrm{~lm} / \mathrm{ft}^{2}$. An internal latch provides hysteresis so that the output will not turn OFF until the illumina-

tion increases by approximately $18 \%$. For comparative purposes, twilight is about $1 \mathrm{~lm} / \mathrm{ft}^{2}$ while an overcast day is about $100 \mathrm{~lm} / \mathrm{ft}^{2}$. Typical loads include an incandescent lamp, LED, sensitive relay, d-c motor, TTL or CMOS (with appropriate pull-up resistor).

## absolute maximum ratings


Output Voltage, $\mathrm{V}_{\text {out }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . 15 V
Output Current, I Iout . . . . . . . . . . . . . . . . . . . . . . . . . . 50 mA
Package Power Dissipation, $P_{0}$. . . . . . . . . . . . . . . See Graph
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots \ldots 0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . .-60^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{cc}}=6.0 \mathrm{~V}, \lambda=555 \mathrm{~nm}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Supply Voltage Range | $V_{c c}$ |  | 4.0 | 6.0 | 15 | V |
| Supply Current | $\mathrm{I}_{\mathrm{cc}}$ |  | - | 4.0 | 8.0 | mA |
| Light Threshold Level | $\mathrm{E}_{\text {ON }}$ | Output ON | 4.25 | 5.00 | 5.75 | $1 \mathrm{~m} / \mathrm{ft}^{2 *}$ |
|  | $\mathrm{E}_{\text {off }}$ | Output OFF | - | 5.90 | - | $1 \mathrm{~m} / \mathrm{ft}^{2 *}$ |
| Hysteresis | $\Delta \mathrm{E}$ | ( $E_{\text {off }}-E_{\text {on }} / E_{\text {off }}$ | 16 | 18 | 20 | \% |
| Output ON Voltage | $V_{\text {out }}$ | $\mathrm{I}_{\text {OUT }}=15 \mathrm{~mA}$ | - | 300 | 500 | mV |
|  |  | $\mathrm{I}_{\text {OUT }}=25 \mathrm{~mA}$ | - | 500 | 800 | mV |
| Output OFF Current | $\mathrm{I}_{\text {OUT }}$ | $V_{\text {OUT }}=15 \mathrm{~V}$ | - | - | 1.0 | $\mu \mathrm{A}$ |
| Output Fall Time | $t_{f}$ | 90\% to 10\% | - | 200 | 500 | ns |
| Output Rise Time | $\mathrm{t}_{\mathrm{f}}$ | 10\% to $90 \%$ | - | 200 | 500 | ns |

*10.76 $\mathrm{lx}=1 \mathrm{Im} / \mathrm{ft}^{2}$

## APPLICATIONS INFORMATION

Type ULN-3330Y characteristics are specified at a light wavelength of 555 nm . This wavelength is the peak of the human eye response for normal light levels (photopic or day-vision). At very low light

POWER DISSIPATION AS A FUNCTION OF TEMPERATURE

levels (scotopic or night-vision), the human eye response peaks at 507 nm .

Other light wavelengths will result in usually increased sensitivity (decreased light threshold levels) for silicon photodiode detectors. For example:

| Wavelength (nm) | Typical Source | Sensitivity |  |
| :---: | :---: | :---: | :---: |
| $507 r e s h o l d$ |  |  |  |
| 507 | Scotopic Vision | 0.87 | 1.14 |
| 555 | Photopic Reference | 1.00 | 1.00 |
| 560 | Green (GaP) LED | 1.01 | 0.99 |
| 590 | Yellow (GaAsP) LED | 1.03 | 0.97 |
| 660 | Red (GaASP) LED | 1.20 | 0.84 |
| 700 | Red (GaP) LED | 1.32 | 0.76 |
| 800 | Diode Peak Response | 1.57 | 0.64 |
| 900 | Infrared (GaAs) LED | 1.19 | 0.84 |

OUTPUT VOLTAGE AS A FUNCTION OF ILLUMINATION


RELATIVE SPECTRAL RESPONSE
AS A FUNCTION OF WAVELENGTH OF LIGHT


RELATIVE SWITCH RESPONSE
AS A FUNCTION OF THE ANGLE OF INCIDENCE


## SERIES 8126 <br> (SG3526J, SG2526J AND SG1526J) SWITCHED-MODE POWER SUPPLY CONTROL CIRCUITS

## FEATURES

- 8 V to 35 V Operation
- Dual 100 mA Source/Sink Outputs
- Internal Regulator
- Current Limiting
- Temperature-Compensated

Reference Source

- Sawtooth Generator
- Low Supply-Voltage Protection
- External Synchronization
- Double-Pulse Suppression
- Programmable Dead-Time
- Programmable Soft-Start


ULN-8126A
ULQ-8126A


ULN-8126R/SG3526J
ULQ-8126R/SG2526J
ULS-8126R/SG1526J

## ABSOLUTE MAXIMUM RATINGS <br> of $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$



Logic Input Voltage Range, $\mathrm{V}_{\mathbb{I}} \ldots \ldots . . .-0.3 \mathrm{~V}$ to +5.5 V
Analog Input Voltage Range, $\mathrm{V}_{\mathrm{IN}} \ldots \ldots . . .$.
Output Current, $\mathrm{I}_{0} \ldots \ldots . . . . . . . . . . . . . . . . . . .200 \mathrm{~mA}$
Reference Load Current, $I_{\text {REF }} \ldots \ldots \ldots \ldots \ldots \ldots . \ldots . \ldots . \ldots \ldots$

Package Power Dissipation, $P_{0}$ (Plastic DIP) .......2.3 W* (Cer-DIP) . ........... 1.9 W* $^{*}$
Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots$. See Ordering Data Storage Temperature Range, $\mathrm{I}_{\mathrm{s}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

[^58]All digital inputs are TTL and CMOS compatible. Active-low logic allows use of wired-OR connections.

Type ULS-8126R is supplied in an 18 -pin glass/ceramic hermetically sealed (cer-DIP) package. It is rated for operation over a temperature range that recommends its use in military and aerospace applications ( $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ ).

Types ULQ-8126A and ULQ-8126R operate over an extended temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ that meets the demands of many industrial applications.

Low-cost Types ULN-8126A and ULN-8126R are rated for continuous operation over a temperature range that recommends them for commercial use $\left(0^{\circ} \mathrm{C}\right.$ to $\left.+70^{\circ} \mathrm{C}\right)$.

Control circuits with commercial and extended temperature ranges are available in both the hermetically sealed cer-DIP package (suffix " $R$ ") and a dual in-line plastic package (suffix " $A$ ") with a copper alloy lead frame that gives them enhanced power dissipation ratings.

Cer-DIP packaged parts normally are marked with original source part numbers shown below. Sprague part numbers appear on plastic packages. Sprague part numbers should be used on orders and correspondence concerning all Series 8126 devices.

ORDERING INFORMATION

| Operating Temperature Range | Package | Original Source Part Number | Sprague Part Number |
| :---: | :---: | :---: | :---: |
| Commercial | Cer-DIP | SG3526J | ULN-8126R |
| $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Plastic | - | ULN-8126A |
| $\begin{gathered} \text { Extended } \\ -40^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{gathered}$ | Cer-DIP | SG2526J | ULQ-8126R |
|  | Plastic | - | ULQ-8126A |
| Full $-55^{\circ} \mathrm{C} \text { to }+125^{\circ} \mathrm{C}$ | Cer-DIP | SG1526J | ULS-8126R |

## RECOMMENDED OPERATING CONDITIONS

| Logic Supply Voltage, $\mathrm{V}_{S}$ | 8 V to 35 V |
| :---: | :---: |
| Collector Voltage, $\mathrm{V}_{\mathrm{c}}$ | 4.5 V to 35 V |
| Output Load Current, $\mathrm{I}_{0}$ | 0 to $\pm 100 \mathrm{~mA}$ |
| Reference Load Current, $I_{L}$ | 0 to 20 mA |
| Oscillator Frequency, f. | 1 Hz to 400 kHz |
| Oscillator Timing Resistance, $\mathrm{R}_{\mathrm{T}}$. | $2 \mathrm{k} \Omega$ to $150 \mathrm{k} \Omega$ |
| Oscillator Timing Capacitance, $\mathrm{C}_{\mathrm{T}}$ | $0.001 \mu \mathrm{~F}$ to $20 \mu \mathrm{~F}$ |
| Programmed Deadtime. | 3\% to 50\% |
| Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ | See Ordering Data |

FUNCTIONAL BLOCK DIAGRAM


## ELECTRICAL CHARACTERISTICS over operating temperature range, $\mathbf{V}_{\mathbf{s}}=15 \mathbf{V}$ (unless otherwise noted)

| Characteristic | Test Pins | Test Conditions | Limits |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Extended \& Full Temperature Devices* |  |  | Commercial Temperature Devices* |  |  | Units |
|  |  |  | Min. | Typ. | Max. | Min. | Typ. | Max. |  |

REFERENCE SECTION ( $I_{L}=0 \mathbf{m A}$ )

| Reference Voltage | 18 | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 4.95 | 5.00 | 5.05 | 4.90 | 5.00 | 5.10 | V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Over recommended conditions | 4.90 | 5.00 | 5.10 | 4.85 | 5.00 | 5.15 | V |
| Reference Voltage Regulation | 18 | $\mathrm{V}_{\mathrm{S}}=8$ to 35 V | - | 10 | 20 | - | 10 | 30 | mV |
|  |  | $\mathrm{I}_{\mathrm{L}}=0$ to 20 mA | - | 10 | 30 | - | 10 | 50 | mV |
|  |  | Over operating temperature range | - | 15 | 50 | - | 15 | 50 | mV |
| Short Circuit Current | 18 | $V_{\text {REF }}=0 \mathrm{~V}$ | 25 | 50 | 100 | 25 | 50 | 100 | mA |
| Stand by Current | 17 | $\mathrm{V}_{\mathrm{S}}=35 \mathrm{~V}, \mathrm{R}_{\mathrm{T}}=4.22 \mathrm{k} \Omega, \mathrm{V}_{8}=0.4 \mathrm{~V}$ | - | 18 | - | - | 18 | - | mA |

OSCILLATOR SECTION ( $f=40 \mathrm{kHz}, \mathrm{R}_{\mathrm{T}}=4.22 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{T}}=0.01 \mu \mathrm{~F}, \mathrm{R}_{\mathrm{D}}=0 \Omega$ )

| Oscillator Frequency | 9,10 | $\mathrm{R}_{\mathrm{T}}=150 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{T}}=20 \mu \mathrm{~F}$ | - | - | 1.0 | - | - | 1.0 | Hz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{R}_{\mathrm{T}}=2 \mathrm{k} \Omega, \mathrm{C}_{\mathrm{T}}=0.001 \mu \mathrm{~F}$ | 400 | - | - | 400 | - | - | kHz |
| Initial Oscillator Accuracy | 9,10 | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | 3.0 | - | - | 3.0 | - | \% |
| Oscillator Stability | 9,10 | $\mathrm{V}_{\mathrm{S}}=8$ to 35 V | - | 0.5 | - | - | 0.5 | - | \% |
|  |  | Over operating temperature range | - | 1.0 | - | - | 1.0 | - | \% |
|  |  | Over recommended conditions | - | 2.0 | - | - | 2.0 | - | \% |
| Sawtooth Peak Voltage | 10 | $\mathrm{V}_{\mathrm{S}}=35 \mathrm{~V}$ | - | 3.0 | 3.5 | - | 3.0 | 3.5 | V |
| Sawtooth Valley Voltage | 10 | $\mathrm{V}_{\mathrm{S}}=8.0 \mathrm{~V}$ | 0.5 | 1.0 | - | 0.5 | 1.0 | - | V |
| Sync Pulse Width | 12 | $\mathrm{C}_{\mathrm{L}}=15 \mathrm{pF}$ | - | 500 | - | - | 500 | - | ns |

## HOUSEKEEPING FUNCTIONS

| Logic Voltage Levels | 5,8,12 | Logic HIGH, $\mathrm{I}_{\text {SOURCE }}=-40 \mu \mathrm{~A}$ | 2.4 | 4.0 | - | 2.4 | 4.0 | - | V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Logic LOW, $\mathrm{I}_{\text {SINK }}=3.6 \mathrm{~mA}$ | - | 0.2 | 0.4 | - | 0.2 | 0.4 | V |
| Input Current | 5,8,12 | $\mathrm{V}_{\mathrm{IN}}=2.4 \mathrm{~V}$ | - | -125 | -200 | - | -125 | -200 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {IN }}=0.4 \mathrm{~V}$ | - | -225 | -360 | - | -225 | -360 | $\mu \mathrm{A}$ |
| Shutdown Delay | $\begin{gathered} \hline 8-13 \\ 16 \end{gathered}$ | 100 mV step, 5 mv overdrive, $\mathrm{R}_{S}=50 \Omega$ | - | 300 | - | - | 300 | - | ns |

NOTES: Negative current is defined as coming out of (sourcing) the specified device pin.
"Commercial, extended, and full temperature-range devices are defined in preceding text and "Ordering Information" table.

## ELECTRICAL CHARACTERISTICS (Continued)

| Characteristic | Test Pins | Test Conditions | Limits |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Extended \& Full Temperature Devices* |  |  | Commercial Temperature Devices* |  |  | Units |
|  |  |  | Min. | Typ. | Max. | Min. | Typ. | Max. |  |

ERROR AMPLIFIER ( $\mathbf{V}_{\mathbf{C M}}=\mathbf{0}$ to 5.2 V )

| Input Offset Voltage | 1,2 | $\mathrm{R}_{\mathrm{S}}=2 \mathrm{k} \Omega$ | - | 2.0 | 5.0 | - | 2.0 | 5.0 | mV |
| :--- | :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Bias Current | 1,2 |  | - | -350 | -1000 | - | -350 | -2000 | nA |
| Input Offset Current | 1,2 |  | - | 35 | 100 | - | 35 | 200 | nA |
| Error Amplifier Gain | $1-3$ | Open loop, $\mathrm{R}_{\mathrm{L}}=10 \mathrm{M} \Omega$ | 64 | 72 | - | 60 | 72 | - | dB |
| Small Signal <br> Randwidth | $1-3$ | $\mathrm{C}_{\mathrm{L}}=30 \mathrm{pF}$ | 0.7 | 1.0 | - | 0.7 | 1.0 | - | MHz |
| Output Voltage Swing | 3 | Positive limit, $\mathrm{R}_{\mathrm{L}}=50 \mathrm{k} \Omega$ | 3.6 | 4.2 | - | 3.6 | 4.2 | - | V |
|  | Negative limit, $\mathrm{R}_{\mathrm{L}}=50 \mathrm{k} \Omega$ | - | 0.2 | 0.4 | - | 0.2 | 0.4 | V |  |
| Common Mode Range | 1,2 | $\mathrm{~V}_{\mathrm{S}}=8.0 \mathrm{~V}$ | 0 | - | 5.2 | 0 | - | 5.2 | V |
| Common Mode <br> Rejection | 1,2 | $\mathrm{R}_{\mathrm{S}}=10 \mathrm{k} \Omega$ |  | 70 | 94 | - | 70 | 94 | - |
| Error Amplifier <br> $V_{S}$ Rejection | 3 | $\mathrm{f}=120 \mathrm{~Hz}, \Delta \mathrm{~V}_{\mathrm{S}}=1.0 \mathrm{~V}_{\mathrm{rms}}$ | 66 | 80 | - | 66 | 80 | - | dB |

## CURRENT LIMITING

| Common Mode Range | 6,7 | $V_{S}=18 \mathrm{~V}$ | 0 | - | 15 | 0 | - | 15 |
| :--- | :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Sense Voltage | 6,7 | $V_{C M}=0$ to 15 V | - | 100 | - | - | 100 | - |
| Input Current | 6,7 | $\mathrm{~V}_{\mathrm{CM}}=0$ to 15 V | mV |  |  |  |  |  |
| Voltage Gain | $7-8$ | $\mathrm{I}_{8}=360 \mu \mathrm{~A}$ | - | -3.0 | - | - | -3.0 | - |

## SOFT-START SECTION

| Error Clamp Voltage | - | $\mathrm{V}_{5}=0.4 \mathrm{~V}$ | - | 100 | 400 | - | 100 | 400 | mV |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\mathrm{S}}$ Charging Current | 4 | $\mathrm{~V}_{5}=2.4 \mathrm{~V}$ | - | 100 | - | - | 100 | - | $\mu \mathrm{A}$ |

## OUTPUT DRIVERS ( $\mathbf{V}_{\mathbf{c}}=15 \mathrm{~V}$ )

| Output Voltage | 13,16 | $\mathrm{I}_{\text {Ouf }}=-20 \mathrm{~mA}$ | 12.5 | 13.5 | - | 12.5 | 13.5 | - | V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{I}_{\text {Out }}=-100 \mathrm{~mA}$ | - | 13 | - | - | 13 | - | V |
|  |  | $\mathrm{I}_{\text {OUT }}=20 \mathrm{~mA}$ | - | 0.2 | 0.3 | - | 0.2 | 0.3 | V |
|  |  | $\mathrm{I}_{\text {OUT }}=100 \mathrm{~mA}$ | - | 1.2 | - | - | 1.2 | - | V |
| Leakage Current | 13,16 | $\mathrm{V}_{\mathrm{C}}=40 \mathrm{~V}$ | - | 0.1 | 100 | - | 0.1 | 100 | $\mu \mathrm{A}$ |
| Rise Time | 13,16 | $\mathrm{C}_{\mathrm{L}}=1000 \mathrm{pF}$ | - | 300 | - | - | 300 | - | ns |
| Fall Time | 13,16 | $\mathrm{C}_{\mathrm{L}}=1000 \mathrm{pF}$ | - | 200 | - | - | 200 | - | ns |

[^59]*Commercial, extended, and full temperature-range devices are defined in preceding text and "Ordering Information" table.

## SERIES 8160 <br> (NE5560N, NE5560F AND SE5560F) SWITCHED-MODE POWER SUPPLY CONTROL CIRCUITS

## fEATURES

- Internal Voltage Regulator
- Current Limiting
- Temperature-Compensated Reference Source
- Sawtooth Generator
- Pulse-Width Modulator
- Remote ON/OFF Switching
- Low Supply-Voltage Protection
- Loop-Fault Protection
- Demagnetization/High-Voltage Protection
- Maximum Duty-Cycle Adjustment
- Feed-Forward Control
- External Synchronization


COMPREHENSIVE CONTROL of state-of-the-art power supplies is offered by Sprague Types ULN-8160A, ULN-8160R and ULS-8160R. Each control circuit has its own temperature-compensated reference source, an internal Zener reference, a sawtooth waveform generator, a pulse-width modulator, an output driver and a variety of protection circuitry.
Type ULN-8160A is supplied in a 16 -pin dual in-line plastic package with a copper lead frame that gives the device enhanced power dissipation ratings. It is rated for operation over a temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$.

Types ULN-8160R and ULS-8160R are furnished in 16-pin hermetically sealed glass/ceramic packages. These devices will withstand severe environmental contamination. In addition, the extended temperature range of Type ULS-8160R $\left(-55^{\circ} \mathrm{C}\right.$ to $\left.+125^{\circ} \mathrm{C}\right)$ recommends it for use in military and aerospace applications.

These devices are normally branded with original source part numbers; however, the Sprague part number should be used on orders and in correspondence.

## ABSOLUTE MAXIMUM RATINGS

$$
\text { AT } \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}
$$

| Supply Voltage, V (Voltage Sourced) | 18 V |
| :---: | :---: |
| Supply Current, IS (Current Sourced) | 30 mA |
| Output Current, $\mathrm{I}_{0}$ | 40 mA |
| Package Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ (ULN-8160A) | $2.1 \mathrm{~W}^{*}$ |
| (ULN-8160R/ULS-8160R) | $1.7 \mathrm{~W}^{*}$ |
| Operating Temperature Range, $\mathrm{T}_{\mathrm{A}}$ (ULN-8160A/R) | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| (ULS-8160R) | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Storage Temperature Range, $\mathrm{T}_{\mathrm{S}}$ | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

*Derate linearly to 0 W at $\mathrm{T}_{\mathrm{A}}=+150^{\circ} \mathrm{C}$.

## ORDERING INFORMATION

| Original Source <br> Part Number | Sprague <br> Part Number | Operating <br> Temperature Range | Package |
| :---: | :---: | :---: | :---: |
| NE5560N | ULN-8160A | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Plastic |
| NE5560F | ULN-8160R | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Cer-DIP |
| SE5560F | ULS-8160R | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | Cer-DIP |

*These devices are manufactured under a cross-license with Signetics Corp. (a subsidary of U.S. Philips Corp.)


ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}=12 \mathrm{~V}$ (unless otherwise noted)

| Characteristic | $\begin{aligned} & \text { Test } \\ & \text { Pin } \end{aligned}$ | Test Conditions | Limits |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | ULS-8160R |  |  | ULN-8160A/R |  |  | Units |
|  |  |  | Min. | Typ. | Max. | Min. | Typ. | Max. |  |
| Supply Voltage Range | 1 | $\mathrm{I}_{\mathrm{S}}=10 \mathrm{~mA}$, current-fed | 20 | - | 23 | 19 | - | 24 | V |
|  |  | $\mathrm{I}_{\mathrm{S}}=30 \mathrm{~mA}$, current-fed | 20 | - | 30 | 20 | - | 30 | V |
| Internal Reference, $\mathrm{V}_{\text {REF }}$ | - |  | 3.69 | 3.76 | 3.84 | 3.69 | 3.76 | 3.84 | V |
| Temperature Coefficient of $V_{\text {ref }}$ | - |  | - | - | $\pm 100$ | - | - | $\pm 100$ | ppm/ ${ }^{\circ} \mathrm{C}$ |
| Zener Reference, $\mathrm{V}_{\mathrm{z}}$ <br> Temperature Coefficient of $V_{2}$ | 2 | $\mathrm{I}_{2}=-7.0 \mathrm{~mA}$ | 7.8 | 8.4 | 9.0 | 7.8 | 8.4 | 9.0 | V |
|  | 2 |  | - | - | $\pm 150$ | - | - | $\pm 150$ | ppm $/{ }^{\circ} \mathrm{C}$ |
| Oscillator Frequency Range | 7.8 |  | 50 | - | 100k | 50 | - | 100k | Hz |
| Initial Oscillator Accuracy | 7, 8 | $\mathrm{R}_{7}=5 \mathrm{kQ}$ | - | 5.0 | - | - | 5.0 | - | \% |
| Duty-Cycle Range | 7,8 | $\mathrm{f}_{0}=20 \mathrm{kHz}$ | 0 | - | 98 | 0 | - | 98 | \% |
| Modulator Input Current | 5 | $V_{5}=1.0 \mathrm{~V}$ | - | 0.2 | 20 | - | 0.2 | 20 | $\mu \mathrm{A}$ |
| Duty-Cycle Control Duty-Cycle Control Current | 6 | For 50\% maximum duty cycle | 38 | 40 | 42 | 37 | 40 | 43 | $\%$ of $\mathrm{V}_{2}$ |
|  | 6 |  | - | 0.2 | 20 | - | 0.2 | 20 | $\mu \mathrm{A}$ |
| Protection Thresholds | 1 | Low supply-voltage protection | 8.5 | 9.1 | 10.5 | 8.5 | 9.1 | 10.5 | $v$ |
|  | 3 | Feedback-loop protection ON | 400 | 500 | 720 | 400 | 500 | 720 | mV |
|  | 13 | Demagnetization/high-voltage protection | 470 | 600 | 720 | 470 | 600 | 720 | mV |
| Sense-Input Current | 3 |  | - | -15 | -35 | - | -15 | -35 | $\mu \mathrm{A}$ |
| Input Current | 13 |  | - | 0.6 | 10 | - | 0.6 | 10 | $\mu \mathrm{A}$ |
| Duty-Cycle Control | 16 | $\mathrm{V}_{16}=2 \mathrm{~V}_{2}$, percent of original duty. cycle | - | 40 | - | - | 40 | - | \% |
| Input Current | 16 |  | - | 0.2 | 5.0 | - | 0.2 | 5.0 | $\mu \mathrm{A}$ |
| Sync Input OFF Voltage | 9 |  | 0 | - | 0.8 | 0 | - | 0.8 | V |
| Sync Input ON Voltage | 9 |  | 2.0 | - | $\mathrm{V}_{7}$ | $2: 0$ | - | $\mathrm{V}_{2}$ | $V$ |
| Sync Input Current | 9 | $\mathrm{V}_{9}=0 \mathrm{~V}$ | - | -65 | -100 | - | -65 | -125 | $\mu \mathrm{A}$ |
| Remote OFF Voltage | 10 |  | 0 | - | 0.8 | 0 | - | 0.8 | $V$ |
| Remote ON Voltage | 10 |  | 2.0 | - | $\mathrm{V}_{2}$ | 2.0 | - | $\mathrm{V}_{2}$ | V |
| Remote Input Current | 10 |  | - | -85 | -100 | - | -75 | -125 | $\mu \mathrm{A}$ |
| Input Current | 11 | $\mathrm{V}_{11}=250 \mathrm{mV}$ | - | -2.0 | -10 | - | -2.0 | -10 | $\mu \mathrm{A}$ |
| Inhibit Delay | 11 | One pulse, $20 \%$ overdrive @ $\mathrm{I}_{0}=40 \mathrm{~mA}$ | - | 700 | 800 | - | 700 | 800 | ns |
| Trip Levels | 11 | Shutdown/slow start | 500 | 600 | 700 | 500 | 600 | 700 | mV |
|  |  | Current limit | 400 | 480 | 560 | 400 | 480 | 560 | mV |
| Error Amplifier Gain | 3-4 | Open loop | - | 60 | - | - | 60 | - | dB |
| Error Amplfier Feedback Resistance | 4 |  | 10 | - | - | 10 | - | - | k8 |
| Small-Signal Bandwidth | 3-4 |  | - | 3.0 | - | - | 3.0 | - | MHz |
| Output-Voltage Swing | 4 | Positive limits | 6.2 | - | - | 6.2 | - | - | V |
|  |  | Negative limits | - | - | 0.7 | - | - | 0.6 | V |
| Output Current | 15 |  | 40 | - | - | 40 | - | - | mA |
| Output Saturation Voltage | 15 | $V_{\text {CESAI }} @ I_{C}=40 \mathrm{~mA}$ | - | - | 0.5 | - | - | 0.5 | v |
| Supply Current | 1 | $\mathrm{T}_{2}=0$, Voltage-fed | - | - | 10 | - | - | 10 | mA |

NOTE: Negative current is defined as coming out of (sourcing) the specified device pin.

# ULX-8161M (NE5561N) SWITCHED-MODE POWER SUPPLY CONTROL CIRCUIT 

## Preliminary Information

## FEATURES

- Stabilized Power Supply
- Current Limiting
- Temperature-Compensated

Reference Source

- Sawtooth Generator
- Pulse-Width Modulator
- Double-Pulse Protection
- Applications in
-Switched-Mode Power Supplies
- Motor Controller-Inverters
-D-C/D-C Converters

DESIGNED AS A CONTROLLER for lowcost switched-mode power supplies, Sprague Type ULX-8161M excels in applications requiring only limited housekeeping functions.

The integrated circuit has its own temperature-compensated reference source, an internal Zener reference, a sawtooth waveform generator, an error amplifier, pulse-width modulator, output driver, current-sensing and low-voltage protection.

Type ULX-8161M is supplied in an 8-pin dual in-line plastic package with a copper lead frame that gives it enhanced power dissipation ratings. It is rated for continuous operation over the temperature range of $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$. Similar devices are available for operation over extended temperature ranges. Control circuits with extensive protective functions (ULN-8160A/R and ULS-8160R) are described in Sprague Engineering Bulletin 27466.


ULX-8161M/NE5561N

Type ULX-8161M is normally marked with the original-source part number, NE5561N; however, the Sprague part number should be used in orders and correspondence.

The ULX prefix to the part number denotes an integrated circuit presently in development and undergoing engineering evaluation. If and when the device becomes a production item, the prefix will be changed to ULN. Sprague Electric assumes no obligation for future manufacture of any products presently in development unless such obligation is specifically undertaken in writing by authorized Sprague personnel.

## ABSOLUTE MAXIMUM RATINGS AT $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

Supply Voltage, $\mathrm{V}_{S}$ (Voltage Sourced) . . . . . . . . . . . . . . . . . . . 18 V
Output Current, $\mathrm{I}_{0} \ldots .$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . 40 mA
Output Duty Cycle . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 98 \%

Operating Temperature Range, $T_{A} \ldots \ldots \ldots . .0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . . . . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $12.5 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.

ORDERING INFORMATION

| Original Source * <br> Part Number | Sprague <br> Part Number | Operating <br> Temperature Range | Package |
| :---: | :---: | :---: | :---: |
| NE5561N | ULX-8161M | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | Plastic |

[^60]ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+\mathbf{2 5}{ }^{\circ} \mathrm{C}, \mathrm{V}_{\mathbf{S}}=\mathbf{1 2} \mathbf{V}$ (unless otherwise noted)

| Characteristic | $\begin{aligned} & \hline \text { Test } \\ & \text { Pin } \end{aligned}$ | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Supply Voltage Range | 1 | $\mathrm{I}_{\mathrm{S}}=10 \mathrm{~mA}$, current-fed | 19 | - | 24 | V |
| Internal Reference, $\mathrm{V}_{\text {REF }}$ | - | Over operating temperature range | 3.55 | - | 3.98 | V |
|  |  | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 3.57 | 3.76 | 3.96 | V |
| Temperature Coefficient of $\mathrm{V}_{\text {REF }}$ | - |  | - | $\pm 100$ | - | ppm $/{ }^{\circ} \mathrm{C}$ |
| Zener Reference, $\mathrm{V}_{2}$ | 2 | $\mathrm{I}_{2}=-7.0 \mathrm{~mA}$ | 7.8 | 8.4 | 9.0 | $\checkmark$ |
| Temperature Coefficient of $\mathrm{V}_{2}$ | 2 |  | - | $\pm 150$ | - | ppm $/{ }^{\circ} \mathrm{C}$ |
| Oscillator Frequency Range | 5 | Over operating temperature range | 50 | - | 100k | Hz |
| Initial Oscillator Accuracy | 5 |  | - | 5.0 | - | \% |
| Duty-Cycle Range | 5 | $\mathrm{f}_{0}=20 \mathrm{kHz}$ | 0 | - | 98 | \% |
| Protection Threshold | 1 | Low supply-voltage protection | 8.5 | 9.1 | 10.5 | V |
| Input Current | 6 | $\mathrm{V}_{6}=250 \mathrm{mV}$, over operating temperature range | - | - | -20 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{6}=250 \mathrm{mV}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | - | -2.0 | -10 | $\mu \mathrm{A}$ |
| Inhibit Delay | 6 | Single pulse, $20 \%$ overdrive at $I_{0}=20 \mathrm{~mA}$ | - | 700 | 800 | ns |
| Trip Level | 6 | Current limit | 400 | 520 | 600 | mV |
| Error Amplifier Gain | 3-4 | Open loop | - | 60 | - | dB |
| Error Amplifier Feed back Resistance | 4 |  | 10 | - | - | k $\Omega$ |
| Small-Signal Bandwidth | 3-4 |  | - | 3.0 | - | MHz |
| Output-Voltage Swing | 4 | Positive limit | 6.2 | - | - | V |
|  |  | Negative limit | - | - | 0.6 | V |
| Output Current | 7 | Over operating temperature range | 20 | - | - | mA |
| Output Saturation Voltage | 7 | $\mathrm{V}_{\text {CESSAT }}$ @ $\mathrm{I}_{\mathrm{C}}=20 \mathrm{~mA}$ | - | - | 0.5 | V |
| Supply Current | 1 | $\mathrm{I}_{2}=0$, over operating temp. range, voltage-fed | - | - | 15 | mA |
|  |  | $T_{Z}=0, T_{A}=+25^{\circ} \mathrm{C}$, voltage-fed | - | - | 9.0 | mA |

## FUNCTIONAL BLOCK DIAGRAM



Dwg. No. A-11,424

## SERIES TPP <br> MEDIUM-POWER DARLINGTON ARRAYS



TPP-1000


TPP-2000

THESE SPRAGUE MEDIUM-POWER arrays consist of one, two, three, or four Darlingtonpairs in a single 14 -pin dual in-line plastic package.

Features of Series TPP, which complements the Sprague TPQ Series of quad transistor arrays, includes a collector-current rating of 4 A , a minimum $\mathrm{h}_{\mathrm{FE}}$ of 2,000 , and a 2 W package power dissipation rating.

The standard molded dual in-line package for Series TPP is identical to the type used for many inte-


TPP-3000


TPP-4000
ircuits. It offers superior mechanical protection for circuit elements during automatic insertion into printed wiring boards.

## ABSOLUTE MAXIMUM RATINGS

Collector Current, $I_{C}$. . . . . . . . . . . . . . . . . . . . . . . . . . 4.0 A
Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ (total package) . . . . . . . . . . . . . . 2 W*
Operating Temperature Range, $T_{A} \ldots \ldots .-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Storage Temperature Range, $\mathrm{T}_{\mathrm{s}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
*Derate at the rate of $16 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

ELECTRICAL CHARACTERISTICS at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Limits |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Typ. | Max. | Units |
| Collector-Emitter Breakdown Voltage | $\mathrm{BV}_{\text {cts }}$ | $\mathrm{I}_{\mathrm{C}}=100 \mu \mathrm{~A}$ | 40 | 50 | - | V |
| Collector-Base Breakdown Voltage | $\mathrm{BV}_{\text {c80 }}$ | $\mathrm{I}_{\mathrm{C}}=100 \mu \mathrm{~A}$ | 50 | 60 | - | V |
| Emitter-Base Breakdown Voltage | $\mathrm{BV}_{\text {E80 }}$ | $\mathrm{I}_{\mathrm{E}}=100 \mu \mathrm{~A}$ | 12 | 14 | - | V |
| CollectorCutoff Current | $I_{\text {c80 }}$ | $\mathrm{V}_{\text {CB }}=30 \mathrm{~V}$ | - | 10 | 100 | nA |
| Emitter-Cutoff Current | $\mathrm{I}_{\text {E80 }}$ | $\mathrm{V}_{\mathrm{EB}}=10 \mathrm{~V}$ | - | 10 | 100 | nA |
| Collector-Emitter Saturation Voltage | $V_{\text {CE (sat) }}$ | $\mathrm{I}_{\mathrm{B}}=1.0 \mathrm{~mA}, \mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}$ | - | 1.0 | 1.5 | V |
| Base-Emitter Saturation Voltage | $V_{\text {BE }}$ (sat) | $\mathrm{I}_{\mathrm{B}}=1.0 \mathrm{~mA}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | - | 1.6 | 2.0 | V |
| Static Forward <br> Current-Transfer <br> Ratio | $\mathrm{h}_{\mathrm{fE}}$ | $\mathrm{V}_{\mathrm{CE}}=5.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=500 \mathrm{~mA}$ | 2000 | - | - | - |
|  |  | $\mathrm{V}_{\text {CE }}=5.0 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~A}$ | 2000 | - | - | - |
|  |  | $\mathrm{V}_{\mathrm{CE}}=5.0 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=2.0 \mathrm{~A}$ | 2000 | - | - | - |

## SERIES TPQ

## QUAD TRANSISTOR ARRAYS

THE SPRAGUE Series TPQ quad transistor arrays are general-purpose silicon transistor arrays consisting of four independent transistors. Shown are eight NPN types, five PNP types, and nine NPN/PNP dual complementary pairs.

All of these devices are furnished in the industry standard TO-116 (or MO-001AA) 14-lead dual in-line plastic package. The molded package is identical to that used in most consumer integrated circuits and offers superior mechanical protection during insertion into printed wiring boards.

## TYPICAL RATINGS (Max.)


*Derate at the rate of $17.9 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+55^{\circ} \mathrm{C}$


Figure 1


Figure 3


Figure 2


Figure 4

## STANDARD RATINGS

| Type No. | $\begin{gathered} B V_{\text {CBO }} \\ V \\ \text { Min. } \end{gathered}$ | $\begin{gathered} B V_{C E O} \\ V \\ M i n . \end{gathered}$ | $\begin{gathered} \mathrm{BV}_{\text {EBO }} \\ V \\ \mathrm{Min} . \end{gathered}$ | $I_{\text {CBO }}$ <br> nA <br> Max. | D-C Current Gain, $\mathrm{h}_{\mathrm{fE}}$ |  |  |  |  |  | $V_{\text {CE(SAT) }}$ |  | Similar Discrete Devices |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Lim | $50$ | $\mathrm{I}_{6} 8$ | $V_{C E}$ | MHz | pF | mV © | ${ }^{I} \mathrm{C}$ |  |
|  |  |  |  |  | Min. | Max. | mA | $\checkmark$ | Min. | Max. | Max. | mA |  |
| Four NPN Devices - Figure 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TPQ2221 | 60 | 40 | 5 | 50 | 40 | - | 150 | 10 | 200 | 8.0 | 400 | 150 | 2N2221 |
| TPQ2222 | 60 | 40 | 5 | 50 | 100 | - | 150 | 10 | 200 | 8.0 | 400 | 10 | 2N2222 |
| TPQ2483 | 60 | 40 | 6 | 20 | 100 | - | 0.1 | 5 | 50 | 6.0 | 350 | 1.0 | 2N2483 |
| TPQ2484 | 60 | 40 | 6 | 20 | 200 | - | 0.1 | 5 | 50 | 6.0 | 350 | 1.0 | 2N2484 |
| TPQ3724 | 50 | 30 | 5 | 500 | 35 | - | 100 | 1 | 250 | 8.0 | 450 | 500 | 2N3724 |
| TPQ3725 | 60 | 40 | 5 | 500 | 35 | 200 | 100 | 1 | 250 | 10.0 | 450 | 500 | 2N3725 |
| TPQ3725A | 70 | 50 | 5 | 500 | 40 | - | 100 | 1 | 200 | 10.0 | 450 | 500 | 2N3725A |
| TPQ3904 | 60 | 40 | 6 | 50 | 75 | - | 10 | 1 | 250 | 4.0 | 200 | 10 | 2N3904 |
| TPQ5550 | 160 | 140 | 6 | 100 | 60 | - | 10 | 5 | 100 | 6.0 | 250 | 50 | 2N5550 |
| TPQ5551 | 180 | 160 | 6 | 50 | 80 | - | 10 | 5 | 100 | 6.0 | 200 | 50 | 2N5551 |
| TPQA05 | 60 | 60 | 4 | 100 | 50 | - | 10 | 1 | 100 | 10.0 | 250 | 100 | MPSA05 |
| TPQA06 | 80 | 80 | 4 | 100 | 50 | - | 10 | 1 | 100 | 10.0 | 250 | 100 | MPSA06 |
| Four PNP Devices - Figure 2 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TPQ2906 | 60 | 40 | 5 | 50 | 40 | - | 150 | 10 | 200 | 8.0 | 400 | 150 | 2N2906 |
| TPQ2907 | 60 | 40 | 5 | 50 | 100 | - | 150 | 10 | 200 | 8.0 | 400 | 150 | 2N2907 |
| TPQ2907A | 60 | 40 | 5 | 20 | 75 | - | 10 | 10 | 200 | 8.0 | 400 | 150 | 2N2907A |
| TPQ3798 | 60 | 40 | 5 | 10 | 150 | - | 0.1 | 5 | 60 | 4.0 | 250 | 1.0 | 2N3798 |
| TPQ3799 | 60 | 60 | 5 | 10 | 300 | - | 0.1 | 5 | 60 | 4.0 | 250 | 1.0 | 2N3799 |
| TPQ3906 | 40 | 40 | 5 | 50 | 75 | - | 10 | 1 | 200 | 4.5 | 250 | 10 | 2N3906 |
| TPQ4258 | 12 | 12 | 4.5 | 10 | 30 | 120 | 10 | 3 | 700 | 3.0 | 150 | 10 | 2N4258 |
| TPQ4354 | 60 | 60 | 5 | 50 | 50 | - | 10 | 10 | 100 | 30.0 | 150 | 15 | 2N4354 |
| TPQ5400 | 130 | 120 | 5 | 100 | 40 | 180 | 10 | 5 | 100 | 6.0 | 200 | 10 | 2N5400 |
| TPQ5401 | 160 | 150 | 5 | 50 | 60 | 240 | 10 | 5 | 100 | 6.0 | 200 | 10 | 2N5401 |
| TPQA56 | 80 | 80 | 4 | 100 | 50 | - | 10 | 5 | 100 | 15.0 | 250 | 100 | MPSA56 |
| Two NPN/Two PNP Devices - Figure 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TPQ6001 | 60 | 30 | 5 | 30 | 40 | - | 150 | 10 | 200 | 8.0 | 400 | 150 | 2N2221/2N2906 |
| TPQ6002 | 60 | 30 | 5 | 30 | 100 | - | 150 | 10 | 200 | 8.0 | 400 | 150 | 2N2222/2N2907 |
| TPQ6100 | 60 | 40 | 5 | 10 | 75 | - | 1.0 | 5 | 50 | 4.0 | 250 | 1.0 | 2N2483/2N3798 |
| TPQ6100A | 60 | 45 | 5 | 10 | 150 | - | 1.0 | 5 | 50 | 4.0 | 250 | 1.0 | 2N2484/2N3799 |


| Two NPN/Two PNP Devices - Figure 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TPQ6501 | 60 | 30 | 5 | 30 | 40 | - | 150 | 10 | 200 | 8.0 | 400 | 150 | 2N2221/2N2906 |
| TPQ6502 | 60 | 30 | 5 | 30 | 100 | - | 150 | 10 | 200 | 8.0 | 400 | 150 | 2N2222/2N2907 |
| TPQ6600 | 60 | 40 | 5 | 10 | 75 | - | 1.0 | 5 | 50 | 4.0 | 250 | 1.0 | 2N2483/2N3798 |
| TPQ6600A | 60 | 45 | 5 | 10 | 150 | - | 1.0 | 5 | 50 | 4.0 | 250 | 1.0 | 2N2484/2N3799 |
| TPQ6700 | 40 | 40 | 5 | 50 | 70 | - | 10 | 1 | 200 | 4.5 | 250 | 10 | 2N3904/2N3906 |

## SERIES ULN-3300M <br> SCHMITT TRIGGER INTEGRATED CIRCUITS - TYPICAL APPLICATIONS AND OPERATION

## Description

Series ULN-3300M Schmitt triggers are monolithic integrated circuits intended for level detection and timing functions.

The three devices making up this series are Type ULN-3304M with a Zener-clamped output, Type ULN-3305M dual Schmitt trigger with complementary outputs, and Type ULN-3306M dual Schmitt trigger with one output Zener-clamped. These three variations of the basic precision threshold detector are shown in Figure 1.

A partial circuit schematic and functional block diagram of the Type ULN-3305M device is shown in Figure 2. Except for the output stage, all other devices in this series are identical.

The differential amplifier $\left(\mathrm{Q}_{1}-\mathrm{Q}_{6}\right)$ is a comparator that "trips" when

$$
\frac{V_{\mathbb{N}}}{V_{c c}} \geq \frac{R_{2}}{R_{1}+R_{2}} \approx 0.62
$$

As long as $\mathrm{V}_{\mathrm{IN}}$ is less than $0.62 \mathrm{~V}_{\mathrm{CC}}$, transistor $\mathrm{Q}_{4}$ will conduct more than $\mathrm{Q}_{3}$ and thus force $\mathrm{Q}_{5}$ into saturation. It follows then that transistors $\mathrm{Q}_{7}$ and $\mathrm{Q}_{8}$ are cut off while $\mathrm{Q}_{9}$ and $\mathrm{Q}_{10}$ are in saturation.

When $\mathrm{V}_{\text {IN }}$ becomes greater than $0.62 \mathrm{~V}_{\mathrm{cc}}$, transistor $Q_{3}$ will conduct more than $Q_{4}$ and $Q_{5}$ and transistors $\mathrm{Q}_{7}$ and $\mathrm{Q}_{8}$ will be driven into saturation. Positive feedback by way of $R_{3}$ will latch the comparator so that it will remain "tripped" until the input drops below $0.55 \mathrm{~V}_{\mathrm{cc}}$. This switching characteristic is illustrated in Figure 3.


TYPE ULN-3304M


TYPE ULN-3305M


TYPE ULN-3306M

Figure 1
SERIES ULN-3300M PINNING DIAGRAMS

ELECTRICAL CHARACTERISTICS at $2.2 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

| Characteristic | Symbol | Test Conditions | Min. | Typ. | Max. | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage | $V_{\text {iN(H) }}$ |  | 0.56 | 0.62 | 0.66 | $V_{\text {WN }} / V_{\text {ci }}$ |
|  | $V_{\text {W(L) }}$ |  | 0.50 | 0.55 | 0.58 | $\mathrm{V}_{\text {W }} / V_{\text {cc }}$ |
| Input Current | $\mathrm{I}_{\text {IN(H) }}$ | $0.66 \mathrm{~V}_{C C} \leq \mathrm{V}_{\mathbb{W}} \leq \mathrm{V}_{C C}$ |  | 10 | 50 | nA |
|  | $\mathrm{I}_{\text {IV() }}$ | $0 \leq \mathrm{V}_{\text {IN }} \leq 0.50 \mathrm{~V}_{\text {cc }}$ |  | 100 |  | pA |
| Clamp Voltage | $V_{2}$ | ULN-3304M, ULN-3306M |  | 14 |  | V |
| Threshold Stability |  |  |  | $\pm 2$ |  | \% |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+100^{\circ} \mathrm{C}$ |  | $\pm 30$ |  | ppm/ ${ }^{\circ} \mathrm{C}$ |
| Output Fall Time | $\mathrm{t}_{\mathrm{f}}$ | $\mathrm{R}_{\mathrm{L}}=1000 \Omega$ |  |  | 200 | ns |
| Output Rise Time | $\mathrm{t}_{\mathrm{i}}$ | $\mathrm{R}_{\mathrm{L}}=1000 \Omega$ |  |  | 200 | ns |

Typical output voltage levels (sometimes referred to as $\mathrm{V}_{\text {CE(SAT) }}$ )vs. ambient temperature and power dissipation vs. supply voltage) are shown in the graphs of Figures 4 and 5.


Figure 2A CIRCUIT SCHEMATIC


Figure 2B
FUNCTIONAL BLOCK DIAGRAM

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage, $\mathrm{V}_{\text {cc }}$. . . . . . . . . . . . . . . . . . . . . . Limited by $P_{D}$
 Input Voltage, $V_{\mathbb{N}} \ldots . .$. Output Current, $\mathrm{I}_{\text {out }}$ (each output) . . . . . . . . . . . . . . . 100 mA $\mathrm{I}_{\text {Out P }}$ (single pulse) . . . . . . . . . . . . . . 300 mA
Power Dissipation, $P_{D}$. . .......................... . 330 mW * Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots . .-40^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$
*Derate at the rate of $4.2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.


10

Figure 3 SERIES ULN-3300M SWITCHING CHARACTERISTIC


Figure 4
TYPICAL OUTPUT VOLTAGE AS A FUNCTION OF TEMPERATURE, SUPPLY VOLTAGE, AND OUTPUT CURRENT

## Operating Characteristics

These devices have several important operating characteristics.

One of the most useful of these features is the reverse voltage handling capability of the entire series. These devices will withstand reverse voltages of up to -20 V indefinitely without damage. Where exact timing is not required ( $\pm 8 \mathrm{~ms}$ ), they can be operated directly from a low-voltage a-c supply without rectification or filtering and thus save a considerable amount in circuit cost.

The output load can be of any form: Resistive, inductive, capacitive, tungsten, LED, etc. For switching inductive loads, Type ULN-3304M or ULN-3306M triggers with their internal Zener diode clamps are recommended. Tungsten or capacitive loads can be handled by any of the devices provided the peak (one-cycle) load current is limited to about 300 mA .


Figure 5
TYPICAL POWER DISSIPATION (EACH TRIGGER) AS A FUNCTION OF SUPPLY VOLTAGE

Output saturation voltage is customarily specified as a function of load current. However, the Type ULN-3305M Schmitt trigger also incorporates a base-emitter voltage drop and a 500 -ohm resistor as part of the non-inverting output. In this case, the output voltage can be shown as:

$$
V_{\text {CE(SAT) }} \approx 0.7+\frac{R_{L} V_{C C}}{500+R_{\mathrm{L}}}
$$

## Threshold Detection

Voltage level detection is easily accomplished with any of the Schmitt triggers in the Series ULN3300M. Shown in Figure 6A is the basic threshold detector. Resistor $R_{1}$ or $R_{2}$ can be replaced with a transducer such as a thermistor or photocell. The circuit of Figure 6B is used when the input voltage is greater than $0.62 \mathrm{~V}_{\mathrm{CC}}$. The circuit of Figure 6 C is


Figure 6A BASIC DETECTOR


Figure 6B HIGH $V_{\text {IN }}$ DETECTOR


DWS. NO. A-10.070


Figure 6C LOW $V_{\text {II }}$ DETECTOR
used for input voltages less than $0.55 \mathrm{~V}_{\mathrm{cc}}$. For the case where $R_{1}=R_{2}$ and $V_{C C}=10 \mathrm{~V}$, the input voltage switching points for Figure 6B are 12.4 and 11.0 volts and for Figure $6 \mathrm{C}, 2.4$ and 1.0 volts.

Switching errors are caused by component tolerances (including $\mathrm{V}_{\mathrm{IN}(\mathrm{H})}$ and $\mathrm{V}_{\mathrm{IN}(\mathrm{L})}$ ), temperature changes (typically only $\pm 30 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ ), and the effect of $I_{\text {IN }}$. Under worse case conditions this should not be more than 50 nA . If the values of $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ are chosen such that the current through them is at least 5 mA under $\mathrm{V}_{\mathrm{IN}(\mathrm{H})}$ conditions, the effect of $\mathrm{I}_{\mathrm{IN}}$ can be ignored. Typical values for $R_{1}$ and $R_{2}$ are usually between $10 \mathrm{k} \Omega$ and $10 \mathrm{M} \Omega$. Resistor $\mathrm{R}_{\mathrm{L}}$ is normally between $1 \mathrm{k} \Omega$ and $100 \mathrm{k} \Omega$.

## Timing

Series ULN-3300M Schmitt triggers can be used in timing applications by connecting an RC integrator to the input as shown in Figure 7. Typical values for $R$ are $10 \mathrm{k} \Omega$ to $10 \mathrm{~m} \Omega$; $C$ is between 100 pF and $10 \mu \mathrm{~F} ; \mathrm{R}_{\mathrm{L}}$ is between $1 \mathrm{k} \Omega$ and $100 \mathrm{k} \Omega$.

Timing accuracy and maximum time delay obtainable are defined by the input characteristics of the device, component tolerances, and the leakage current of the capacitor. Assuming ideal external timing components, the minimum, typical, and maximum switching times are shown as a function of the RC time constant.


Figure 7
RC INTEGRATING TIMERS


Figure 8
RC TIME CONSTANTS

## Astable Multivibrators

Positive feedback from the inverting output $\left(\mathrm{V}_{\text {our }}\right)$ to the RC network will form a relaxation oscillator or astable multivibrator. This connection is possible with Type ULN-3305M.

The basic astable multivibrator illustrated in Figure 9 can be used for the condition where the period $t_{1}$ is less than the period $\mathrm{t}_{2}$. In this configuration, the following design equations apply:

$$
\begin{aligned}
& t_{1}=0.12 R_{1} C \\
& t_{2}=0.17\left(R_{1}+R_{2}\right) C \quad f=\frac{3.45}{\left(R_{1}+0.58 R_{2}\right) C}
\end{aligned}
$$

From the equations several points are evident:
A. Within limits, the supply voltage will have no effect on the frequency.
B. The period $\mathrm{t}_{2}$ can be adjusted, without affecting $t_{1}$, by varying resistor $R_{2}$.
C. If $R_{1}$ is made very large with respect to $R_{2}$, the effect of $R_{2}$ can be minimized or ignored.

With the typical values shown for Figure 7, frequencies of between 4 Hz and 100 kHz are possible.


Figure 9
ASTABLE MULTIVIBRATORS


Figure 10A

If it is desired to have period $t_{1}$ equal to or greater than period $\mathrm{t}_{2}$, a slight circuit change is required as shown in Figures 10A and 10B. In either of these configurations the following design equations apply:

$$
\begin{aligned}
& t_{1}=0.12\left(R_{1}+R_{3}\right) C \\
& t_{2}=0.17\left(R_{1}+R_{2}\right) C \\
& f=\frac{3.45}{\left(R_{1}+0.58 R_{2}+0.41 R_{3}\right)}
\end{aligned}
$$

The output will be symmetrical $\left(t_{1}=t_{2}\right)$ when

$$
R_{3}=0.42 R_{1}+1.42 R_{2}
$$

In each of these astable multivibrators certain limitations should be noted.
A. Any d-c load connector to $\mathrm{V}_{\text {out }}$ will change the period $t_{1}$ because of the loading effect on $R_{2}$. For this reason, the output should probably be taken from $\mathrm{V}_{\text {out }}$.
B. The circuit of Figure 10A has a diode voltage drop in the RC timing network and is therefore not recommended for use with very low supply voltages.
C. The capacitor leakage current can be significant for large values of $R_{1}$ and, as an extreme, can cause the trigger to "latch up."


Figure 10B

## Monostable Multivibrators

The basic monostable multivibrator is shown in Figure 11. In the quiescent state, the input and the output are both "low." If a trigger is applied that raises the input to the Schmitt trigger threshold, $\mathrm{V}_{\text {our }}$ will go "high," applying $\mathrm{V}_{\mathrm{cc}}$ back to the input for a period $t=0.6 \mathrm{RC}$ if resistor R is much greater in value than $R_{L}$. The $1 \mathrm{M} \Omega$ resistor prevents loading of the network by the trigger.

In this circuit, the output loading of $R_{L}$ is desirable, provided the device output current rating is not exceeded. The trigger input voltage should be between $0.66 \mathrm{~V}_{\mathrm{cc}}+0.7 \mathrm{~V}$ and $\mathrm{V}_{\mathrm{cc}}$, and the trigger pulse width must be less than the output pulse width. Output pulse widths of $10 \mu \mathrm{~s}$ to 100 seconds are possible. The input pulse width should be at least 10 ns.

Where output pulse widths are shorter than the trigger pulse width, the circuit shown in Figure 12 is used. In this application, only the leading edge of the trigger pulse is used after being differentiated by one Schmitt trigger. The time constants of the differentiated leading edge then determine the output pulse width as $\mathrm{t}_{1}=0.6 \mathrm{RC}$.

As before, resistor R is much greater in value than $\mathrm{R}_{\mathrm{L}}$, the trigger input voltage must be between 0.66 $\mathrm{V}_{\mathrm{cc}}$ and $\mathrm{V}_{\mathrm{cc}}$, the trigger pulse width must be greater than the output pulse width. In addition, to insure that the timing capacitor completely discharges, period $t_{2}$ should be at least five times period $t_{1}$.


Figure 11
MONOSTABLE MULTIVIBRATOR


Figure 12
MONOSTABLE MULTIVIBRATOR

$V_{\text {thioes }}$



Figure 13
TACHOMETER/DWELL METER


Figure 14
MISSING PULSE DETECTOR


Figure 15
TOUCH-CONTROLLED SWITCH


DWG. No. A- 10.086
$C_{1}$ is chosen for burst frequency, $f=\frac{3.45}{C_{1}\left(R_{1}+R_{2}\right)}$
$\mathrm{C}_{2}$ is chosen for burst duration, $\mathrm{t}=0.6 \mathrm{R}_{2} \mathrm{C}_{2}$

Figure 16
tone-burst generator


Choose $\mathrm{C}_{1}$ to match photocell characteristics.
Choose $R_{1}$ to match shutter characteristics.
Choose $R_{2}$ for desired flash timing ( $S_{2}$ closes in flash mode).
At $t=0$, shutter is released, $S_{1}$ opens.

Figure 17
PHOTO INTEGRATOR


DWG. No. A-10. 089
$t=0.97$ R C Typical (see Figure 7).
Figure 18 BASIC RC TIMER


5WG. 10. 4-10.092
$R_{1}$ and $R_{2}$ may be interchanged for opposite logic (see Figure 6A).
Figure 20 LIGHT-ACTUATED SWITCH


Note: Add resistor at " $X$ " for symmetry (see Figure 10B) when $V_{\mathbb{N}}=0$.
The peak-to-peak signal input must be less than
$V_{\mathbb{N}(H)}$ - $V_{\mathbb{I N L L})}$ or clipping will occur.

$$
f \approx \frac{3.45}{C\left(R_{1}+R_{2}\right)}
$$



Note: A-C coupling to probe is used to prevent electrolysis. Output duty cycle is $50 \%$ unless peak detector is inserted at " X ."


Figure 21
LIQUID-LEVEL DETECTOR


Output current temperature coefficient:

$$
\Delta \mathrm{I}_{\text {OUT }}=\frac{0.002 \Delta \mathrm{~T}}{R}
$$

Where $\mathrm{I}_{\text {out }}$ is in amperes, T is in ${ }^{\circ} \mathrm{C}$, and R is in ohms. Pins 5 and 7 are tied together for single control input. If separated, the $V_{\mathbb{N}(5)}$ and $V_{\mathbb{W}(7)}$ must both go "low" to obtain $I_{\text {our }}$.

Figure 22A
CURRENT MIRROR

D.6. NO. A-10. 095

CURRENT MIRROR

HIGH-VOLTAGE INTERFACE DRIVERS

HIGH-CURRENT INTERFACE DRIVERS

BiMOS AND COMPLEX ARRAY INTERFACE DRIVERS

INDUSTRIAL, MILITARY, AND AEROSPACE DEVICES

RADIO INTEGRATED CIRCUITS

TELEVISION INTEGRATED CIRCUITS

AUDIO INTEGRATED CIRCUITS

## HALL EFFECT DEVICES

TRANSISTOR ARRAYS AND MISCELLANEOUS DEVICES


## SECTION 11 - CUSTOM DEVICES

Custom Circuit Design Capability ..... 11-2
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ULN-2350C and 2351C Tuff Chip ${ }^{(\mathbb{T W}}$ Semi-Custom Integrated Circuits ..... 11-4
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## CUSTOM CIRCUIT DESIGNS

Sprague is active in the design of standard and custom high-volume integrated circuits and subassemblies for both linear and digital applications. A wide range of semiconductor technologies is available to optimize cost and performance. Often, new processes or innovative circuit designs are required.

The first concern of a designer of a custom device is generally one of cost, though performance, reliability, size, and process are also important considerations.

Production Volume: Unit cost is dependent on quantity. A minimum volume of $\$ 250,000$ per year is required after the initial design and development.

Chip Size: Unit cost is directly affected by chip size, which is related to circuit complexity, outputcurrent and output-voltage ratings.

Test Requirements: Logic, d-c, and static measurements are simple, fast, and inexpensive to perform, while linear measurements such as those for distortion, phase and noise affect production rates and increase cost.

Specifications: Well-defined specifications can expedite circuit design. Excessive or arbitrarily tight specifications will reduce yields and increase cost.

## Typical Custom Design Schedule

Task
Time in Weeks

| Define Specifications | - |
| :--- | ---: |
| Circuit Design | 2 to 10 |
| Breadboard Construction | 2 to 8 |
| Breadboard Approval | 3 to 4 |
| Circuit Layout | 2 to 8 |
| Prototype Construction | 3 to 8 |
| Production Pilot Run | 8 to 12 |
| Production Volume | 12 to 16 |

Total 32 to 66 weeks at an engineering cost of between $\$ 20,000$ and $\$ 50,000$, not including special test hardware or assembly tooling.

## Integrated Component Capability

$\begin{array}{ll}\text { Transistors: } & \text { NPN — Beta to } 300, B V_{\text {CES }} \text { to } 120 \mathrm{~V}, \mathrm{f}_{\mathrm{T}} \text { to } 500 \mathrm{MHz} \\ & \mathrm{PNP} \text { — Beta to } 40, B \mathrm{C}_{\text {CES }} \text { to } 100 \mathrm{~V}, \mathrm{f}_{\mathrm{T}} \text { to } 4 \mathrm{MHz}\end{array}$
CMOS - $V_{T H} 0.8$ to $2.5 \mathrm{~V}, B V_{D S}$ to 18 V

Resistors: Diffused $-5 \Omega / \square$, to $100 \Omega, 100 \mathrm{~V}$ $175 \Omega / \square$, to $100 \mathrm{k} \Omega, 100 \mathrm{~V}$ Ion Implant - $500 \Omega / \square$ to $4 \mathrm{k} \Omega / \square$, to $4 \mathrm{M} \Omega, 20 \mathrm{~V}$
Thin Film - $2 \mathrm{k} \Omega / \square$, to $2 \mathrm{M} \Omega, 250 \mathrm{~V}$
Aluminum $-0.025 \Omega / \square$, to $1.0 \Omega, 150 \mathrm{~V}$

Capacitors: Junction - $0.1 \mathrm{pF} / \mathrm{mil}^{2}$, to $30 \mathrm{pF}, 100 \mathrm{~V}$ $0.3 \mathrm{pF} / \mathrm{mil}^{2}$, to $100 \mathrm{pF}, 12 \mathrm{~V}$ $0.9 \mathrm{pF} / \mathrm{mil}^{2}$, to $300 \mathrm{pF}, 6 \mathrm{~V}$
MOS - $0.1 \mathrm{pF} / \mathrm{mil}^{2}$, to $30 \mathrm{pF}, 50 \mathrm{~V}$
$0.2 \mathrm{pF} / \mathrm{mil}^{2}$, to $50 \mathrm{pF}, 20 \mathrm{~V}$

Diodes: $\quad$ Zener -5.7 or $7.0 \mathrm{~V}, \pm 0.3 \mathrm{~V}$
Photo - $0.5 \mathrm{~A} / \mathrm{W}$ or $>300 \mathrm{nA} / \mathrm{fc}$ at 800 nm Schottky - 0.1 to 0.4 V at $1 \mu \mathrm{~A}, 0.3$ to 0.6 V at 1 mA Small Signal - BV $=7.0 \mathrm{~V}$
Varactor $-C_{0} / C_{5} \approx 2$

Other: $\quad$ SCRs - to 1 A , to 60 V
PUTs - to 1 A , to 60 V
$I^{2} L$ - Propogation delay typically 100 ns
BiMOS - High-power bipolar plus low-power MOS
Hall Cells - $35 \mathrm{mV} / \mathrm{kG}$

## Application Areas of Sprague Expertise

TV - NTSC or PAL, video, chroma, sound, sync, I-F
Toy - sound generators and amplifiers, optolinear, timers, controls

Camera - photodiodes, light integrators, timers, controls
Transistor Arrays - small-signal, control, highcurrent, SCR

Control - Schmitt triggers, timers, Hall cells, switching regulators, motor drivers
Radio - A-M, F-M, F-M stereo, A-M stereo
Safety - GFI, smoke detectors, burglar alarms
Audio - 250 mW to 10 W , mono and stereo
Automotive - controls, monitoring, safety, radio
Interface - display drivers, Hall cells, optolinear
Military - communications, fuze, interface
Computer - interface to $\pm 115 \mathrm{~V}$ or 2 A

## SPRAGUE SEMI-CUSTOM, HIGH-VOLTAGE INTEGRATED CIRCUITS

Sprague semi-custom integrated circuits for transient-prone environments such as automobiles and industrial controls include components that can be used to protect operational circuitry from voltage surges of up to 500 V .
Fabrication of a semi-custom integrated circuit begins with the user's design for interconnecting metal that transforms uncommitted components on a finished wafer into a dedicated and original circuit. Among components available to users of Sprague semi-custom arrays are power transistors with a $\mathrm{BV}_{\mathrm{CES}}$ of more than 80 V , a minimum of 53 diffused resistors and 140 thin-film polysilicon resistors, capacitors formed by buried-layer and isolation diffusions, vertical PNP transistors as well as NPN and lateral PNP transistors, and emitter-isolation Zener diodes with a nominal breakdown voltage of 5.8 V .
Power transistors in the component arrays can withstand load-disconnect transients of automobile alternators ( $80 \mathrm{~V}, 200 \mathrm{~ms}$ ) without the use of Zener diode clamping circuits.

The greater part of the resistive element of the arrays is made up of dielectrically isolated thin-film resistors that, with their high resistive values and their ability to withstand transients as high as 500 V ,


Dwg. No. A-11,439
Figure 1
can be used to limit peak transient currents.
Because these polysilicon resistors are not polarity sensitive (no PN junction is formed by the thin-film manufacturing process), they are inherently protected from damage by voltage-supply reversal. The high values of resistance available with these components are particularly useful in applications requiring low levels of power dissipation and standby current.

The arrays also have capacitive elements with typical values of 80 pF for use in applications requiring supply stabilization or noise suppression.

Vertical PNP transistors, with current-gain typically two or three times greater than the $\mathrm{h}_{\mathrm{FE}}$ of lateral PNPs, complement the arrays' standard set of NPN and PNP transistors. Vertical PNPs can be used in a current-mirror (Figures 1 and 2) to reduce error introduced by base currents from $20 \%$ to less than $1 \%$. The devices can also be used in a differential amplifier configuration (Figure 3) to decrease basecurrent requirements.

More complete information on development of these semi-custom, high-voltage integrated circuits is presented in Sprague Technical Paper TP 81-3.


Figure 2

# ULN-2350C and ULN-2351C TUFF CHIP ${ }^{\text {™ }}$ SEMI-CUSTOM INTEGRATED CIRCUITS 

## PRELIMINARY INFORMATION

(Specifications Subject to Change Without Notice)

## FEATURES

- $\mathrm{BV}_{\text {CES }}=80 \mathrm{~V}$ Min.
- 250 mA Outputs
- 500 Volt Resistors
- High-Gain PNP Transistors
- 80 pF Capacitors
- Time and Cost Savings

TUFF CHIP SEMI-CUSTOM integrated circuits offer substantial time and cost savings for custom circuit applications requiring from 5,000 to 200,000 pieces. This is an area that previously was met by hybrid circuits and, in some cases, by printed wiring boards.

The TUFF CHIP semi-custom approach utilizes a standard array of components fabricated on a single silicon chip: the ULN2350C contains 480 separate elements; the ULN-2351C provides 276. Besides the traditional complement of NPN and lateral PNP transistors, high-gain vertical PNP transistors are included.

The user lays out the interconnecting circuit, similar to a printed wiring board layout, on sheets provided by Sprague Electric. The artwork is checked by Sprague engineers, and used to generate the customer's proprietary metal mask. Finished circuits are electrically probed and visually inspected. Chips are tray-packed for hybrid circuit manufacturers or are mounted in plastic, ceramic, or hermetic dual in-line packages with from 8 to 28 pins.

TUFF CHIP components are optimized for a minimum $\mathrm{BV}_{\text {CES }}$ of 80 volts. Two or four 250 mA power transistors are provided, and these may be paralleled for high current requirements. On-chip transient protection of sensitive circuit

$89 \times 104 \mathrm{mils}$
$2.26 \times 2.64 \mathrm{~mm}$ ULN-2351C

$104 \times 150 \mathrm{mils}$ $2.64 \times 3.81 \mathrm{~mm}$
ULN-2350C
components utilizes deposited film resistors with breakdown voltages higher than 500 volts. Onchip capacitors may be used for noise suppression or filtering.

Circuit users can expect prototypes six to ten weeks after submitting initial artwork; production quantities can be shipped eight to ten weeks after prototype approval.

ELECTRICAL CHARACTERISTICS at $\mathbf{T}_{\mathbf{j}} \mathbf{=} \mathbf{+ 2 5}^{\circ} \mathbf{C}$
COMPONENT LIST


|  | Number of Devices |  |
| :---: | :---: | :---: |
|  | ULN-2350C | ULN-2351C |
| Small-Signal NPN Transistors | 70 | 38 |
| NPN Power Transistors | 4 | 2 |
| Lateral PNP Transistors | 27 | 14 |
| Vertical PNP Transistors | 10 | 7 |
| $\begin{aligned} & 5.8 \mathrm{~V} \\ & \text { Zener Diodes } \end{aligned}$ | 5 | 2 |
| $\begin{aligned} & 80 \mathrm{~V} \\ & \text { Zener Diodes } \end{aligned}$ | 20 | 15 |
| Base Resistors: $200 \Omega$ | 10 | 5 |
| $450 \Omega$ | 20 | 12 |
| 900ת | 20 | 12 |
| $1.8 \mathrm{k} \Omega$ | 20 | 12 |
| $3.6 \mathrm{k} \Omega$ | 20 | 12 |
| Deposited Film Resistors: $2.0 \mathrm{k} \Omega$ | 16 | 8 |
| $4.5 \mathrm{k} \Omega$ | 58 | 33 |
| $9.0 \mathrm{k} \Omega$ | 48 | 28 |
| $18 \mathrm{k} \Omega$ | 50 | 29 |
| $36 \mathrm{k} \Omega$ | 72 | 42 |
| 80 pF Capacitors | 10 | 5 |
| Bonding Pads | 28 | 19 |

## Optional Package Capabilities



Standard integrated circuits from Sprague Electric Company are most often furnished in packages meeting industry or military standards (JEDEC TO-87, TO-91, TO-99, TO-100, or TO-116, or MIL-M-38510). However, on special order, other packages or assemblies of packaged devices can also be supplied. A few special order devices are illustrated above, including special heat sink tabs, subminiature plastic packages, printed wiring boards, flexible circuits, and complex assemblies. Devices with photodiodes are furnished in clear plastic cases.

## GENERAL INFORMATION

## HIGH-VOLTAGE INTERFACE DRIVERS

## HIGH-CURRENT INTERFACE DRIVERS

BiMOS AND COMPLEX ARRAY INTERFACE DRIVERS

INDUSTRIAL, MILITARY, AND AEROSPACE DEVICES

RADIO INTEGRATED CIRCUITS

| TELEVISION INTEGRATED CIRCUITS |  |
| :--- | :--- |
|  |  |
| AUDIO INTEGRATED CIRCUITS | $!$ |

HALL EFFECT DEVICES

TRANSISTOR ARRAYS AND MISCELLANEOUS DEVICES

CUSTOM DEVICES
11

PACKAGE INFORMATION
$\begin{array}{cc}8 & 8 \\ 8 & 8 \\ 8 & 8\end{array}$

4
 $\qquad$
$\qquad$

## SECTION 12 - PACKAGE INFORMATION

Package Thermal Characteristics ..... 12-2
Thermal Design for Plastic Integrated Circuits ..... 12-3
Computing Integrated Circuit Temperature Rise ..... 12-9
Operating and Handling Practices for MOS Integrated Circuits ..... 12-13
Package Drawings:
Suffix 'A' Plastic Dual In-Line ..... 12-14
Suffix 'B' Plastic Dual In-Line with Heat Sink Semi-Tabs ..... 12-16
Suffix 'C' Unpackaged Chip or Wafer
Suffix 'H' Glass/Metal Hermetic Side-Brazed Dual In-Line . ..... 12-17
Suffix 'J' Glass/Metal Hermetic 14-Lead Flat-Pack ..... 12-19
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## Package Thermal Characteristics

| Package Designator | Package Type | Frame Material | $\begin{aligned} & R \Theta_{j A} \dagger \\ & \left({ }^{\circ} \mathrm{C} / \mathrm{W}\right) \end{aligned}$ | $\begin{aligned} & \mathrm{R} \Theta_{\mathrm{IJ}} \dagger \\ & \left({ }^{\circ} \mathrm{C} / \mathrm{W}\right) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| A | 14-Lead Plastic DIP | Copper | 60 | 38 |
| A | 16-Lead Plastic DIP | Copper | 60 | 38 |
| A | 18-Lead Plastic DIP | Copper | 55 | 25 |
| A | 20-Lead Plastic DIP | Copper | 55 | 25 |
| A | 22-Lead Plastic DIP | Copper | 50 | 21 |
| A | 28-Lead Plastic DIP | Copper | 40 | 16 |
| B | 8-Lead Webbed | Copper | 75 | 13* |
| B | 14-Lead Webbed | Copper | 45 | 13* |
| B | 16-Lead Webbed | Copper | 45 | 13* |
| H | 8-Lead Hermetic | Kovar | 120 | 40 |
| H | 14-Lead Hermetic | Kovar | 90 | 20 |
| H | 16-Lead Hermetic | Kovar | 90 | 20 |
| H | 18-Lead Hermetic | Kovar | 75 | 20 |
| J | 14-Lead Flat Pack | Kovar | 140 | 80 |
| M | 8-Lead Mini DIP | Copper | 80 | 55 |
| Q | 16-Lead Quad In-Line | Copper | 45 | 13* |
| R | 14-Lead CerDIP | Kovar | 75 | - |
| R | 16-Lead CerDIP | Kovar | 75 | - |
| R | 18-Lead CerDIP | Kovar | 65 | - |
| W | 12-Lead Power Tab SIP | Copper | - | 3.0* |
| $Y$ | 3-Lead Transistor | Copper | 310 | 170 |
| Z | 5-Lead Power Tab SIP | Copper | 40 | 4.5* |

The data given is intended as a general reference only and is based on certain simplifications such as constant chip size, standard bonding methods, and an allowable $+150^{\circ} \mathrm{C}$ junction temperature. Where differences exist, the detail specification takes precedence.
$\dagger G \Theta_{\mathrm{JA}}=1 / R \Theta_{\mathrm{JA}}$ and $\mathrm{G} \Theta_{\mathrm{JC}}=1 / R \Theta_{\mathrm{JC}}$
${ }^{*} \mathrm{RO}_{\mathrm{f}}$

## THERMAL DESIGN FOR PLASTIC INTEGRATED CIRCUITS

PROPER THERMAL DESIGN is essential for reliable operation of many electronic circuits. Under severe thermal stress, leakage currents increase, materials decompose, and components drift in value or fail. Present-day linear integrated circuits are capable of delivering 5 to 10 watts of continuous power. Previously, such power levels came only with discrete metal can power transistors. It was relatively easy to determine the thermal resistance of these devices and attach a massive heat sink. However, in many markets, economic factors now dictate the use of molded dual in-line plastic packaged monolithic circuits. The guidelines to be discussed will provide the circuit design engineer with information on maintaining junction temperature below a safe limit under worst case conditions.

## Design Considerations

Four factors must be considered before the required heat-sinking can be determined. These are:

1. Maximum ambient temperature
2. Maximum allowable chip temperature
3. Junction-to-ambient thermal resistance
4. Continuous chip power dissipation

Maximum ambient temperature for the integrated circuit is normally between $+70^{\circ} \mathrm{C}$ and $+85^{\circ} \mathrm{C}$ and is usually dependent on the case material. In most applications, however, the limiting factor is the associated discrete components and a limit of about
$+50^{\circ} \mathrm{C}$ is specified. The maximum allowable chip temperature is usually $+150^{\circ} \mathrm{C}$ for silicon.
Thermal resistance is the all-important design factor. It is composed of several individual elements, some of which are determined by the integrated circuits manufacturer, and some by the user.

## Chip Power Dissipation

The chip power dissipation should be obtainable from the manufacturer's specifications. In most applications it is a variable and determined by the user when he specifies the circuit variables.

A typical example is the Sprague Type ULN-2277 dual 2 -watt audio power amplifier. Power dissipation is determined by the load impedance, the required peak output power, the acceptable amount of total harmonic distortion (THD), and the supply voltage ( $\mathrm{V}_{\mathrm{cc}}$ ). This is illustrated in Figures 1-3. Note that for a given supply voltage, the chip dissipation may be greatest at some point below the peak output power rating and must be considered.

As shown in the figures, a peak output power of 2 watts per channel with $3 \%$ maximum THD would mean a chip power dissipation of about 2.7 W and a $\mathrm{V}_{\mathrm{CC}}$ of 15 V with a load impedance of $4 \Omega$, or 1.8 W and 15 V at $8 \Omega$, or 1.4 W and 19 V at $16 \Omega$. In general, the highest load impedance for a given output power is the most desirable (within the output voltage capability of the device).


Figure 1


Figure 2


Figure 3

## Heat Dissipation

In any circuit involving power, a major design objective is to reduce the temperature of the components in order to improve reliability, reduce cost, or improve operation. The logical place to start is with the heat-producing component itself. First, keep the amount of heat generated to a minimum. Second, get rid of the heat that must be generated.

Heat generation can be minimized through proper circuit design. Heat dissipation is a function of thermal resistance.

With the typical discrete component, heat dissipation can be accomplished by fastening it directly to the chassis. Dual in-line plastic packaged integrated circuits, however, are quite a bit different. Their shape is not conducive to fastening directly to the chassis, they are normally installed in a plastic socket or on a printed wiring board, and the heat producing chip is not readily accessible.

Some users specify unusual packages so as to get the heat sink as close as possible to the chip and /or provide an attachment point for an external heat sink. A common factor in many of these special designs is that the lead frame is an integral part of the heat sink.

Since the plastic package may have a thermal resistance of between 50 and $100^{\circ} \mathrm{C} / \mathrm{W}$ and the lead frame a thermal resistance of only 10 to $20^{\circ} \mathrm{C} / \mathrm{W}$, this would seem like the best route to go.

## Standard Packages

The most common lead frame material has been Kovar (an iron-nickel-cobalt alloy). Its coefficient of expansion is close to that of silicon thereby minimizing mechanical stresses. However, Kovar has a relatively high thermal resistance and consequently is not suitable for standard lead frames in high power dissipation circuits. For these applications, copper or copper-alloy lead frames should be used. Additionally, some type of added heat sinking may be necessary. Thus lead frame configurations are
being altered from the standard 14 -pin or $16-$ pin designs.

Rapidly becoming an industry standard is the "bat-wing"' package. This package is the same size as a 14 -pin dual in-line package, but the center portion of the frame is left as tabs, measuring about $1 / 4^{\prime \prime}$ square. These tabs can be soldered, welded, or bolted to a heat sink, or inserted directly into some sockets. The worst case thermal resistance of various lead frames $\left(\Theta_{\mathrm{Jc}}\right)$ is given below.

| Lead Frame | Thermal Resistance |
| :---: | :---: |
| 14-pin Kovar | $47^{\circ} \mathrm{C} / \mathrm{W}$ |
| 14 -pin copper | $19^{\circ} \mathrm{C} / \mathrm{W}$ |
| "Bat-wing" | $11^{\circ} \mathrm{C} / \mathrm{W}$ |

## Which Heat Sink?

If the integrated circuit manufacturer has done his job well, the chip-to-ambient thermal resistance will be minimized for maximum chip power dissipation. It would appear that even the Kovar lead frame would be adequate for most applications. However, the total thermal resistance $\left(\Theta_{\mathrm{JA}}\right)$ is also dependent on a stagnant layer of air at the lead frame-ambient interface which will support a temperature gradient. The total thermal resistance of a non-heat sinked dual in-line plastic package is therefore much higher. Since air is a natural thermal insulator, maximum heat transfer is through convection and the total thermal resistance will decrease some at high power levels.

|  | Total <br> Thermal | Max. Power Diss. (W) |
| :--- | :---: | :---: |
| Lead Frame | Resistance | at $50^{\circ} \mathrm{C} \mathrm{T}, 150^{\circ} \mathrm{C} \mathrm{T}$ |
| 14-Pin Kovar | $120^{\circ} \mathrm{C} / \mathrm{W}$ | 0.83 |
| 14-Pin Copper | $72^{\circ} \mathrm{C} / \mathrm{W}$ | 1.39 |
| "Bat-Wing" | $50^{\circ} \mathrm{C} / \mathrm{W}$ | 2.0 |

Ignoring any safety margin and device performance, even the "bat-wing'" is now only barely adequate for most applications. The obvious solution is the use of an external heat sink.

## PACKAGE INFORMATION (Continued)

Referring to Figures 4 and 5, the thermal resistance requirement of the heat sink is found at the junction of the specified chip power dissipation and maximum ambient temperature. These curves are typical of those furnished in many monolithic integrated circuit data sheets. Actual performance in a specific situation depends on factors such as the proximity of objects interfering with air flow, heat radiated or convected from other components, atmospheric pressure, and humidity. A good safety factor is therefore in order.


Figure 4


Figure 5

Heat sinks for plastic dual in-line packages can be of almost unlimited variety in design, material, and finish. Economics will normally play a very important role in the selection of any heat sink.

The least expensive and easiest to fabricate heat sink is the plain copper sheet. It is also very effective in reducing the total thermal resistance. The necessary dimensions can be obtained from Figure 6. These heat sinks are square in geometry, 0.015 inches thick, mounted vertically on each side of the lead frame, and with a dull or painted surface (Figure 7). The heat sinks should be soldered directly to the lead frame (approximately $0.3^{\circ} \mathrm{C} / \mathrm{W}$ interface thermal resistance).

The plain copper sheet heat sink is also available commercially and may be less expensive than inhouse manufacture. Two standard types are the Staver V7 and V8.


Figure 6


Dwg No. A-11,435

Figure 7

## Heat Sink Finishes

Although plain copper is an effective heat sink, it is sometimes desirable to have something that is more appealing to the eye. For this reason, and others, many heat sinks are either painted or anodized.

The most common finish is probably black anodizing. It is economical and offers a good appearance. The black finish will also increase the performance of the heat sink, due to radiation, by as much as $25 \%$. However, since anodizing is an electrical and thermal insulator, the heat sink should have an area free of anodize where the heat-generating device is attached.

Other popular finishes for heat sinks are irridite and chromic acid dips. They are economical and have negligible thermal and electrical resistances. These finishes, however, do not enjoy the $25 \%$ increase in performance that a dull black finish has.

## Forced Air Cooling

The performance of many heat sinks can be increased by as much as $100 \%$ by forcing air over the fins. Where space is a problem, the cost of a small fan can often be justified. If a fan is required for other purposes, it is advantageous to place the semiconductor heat source in the air flow. A rule-of-thumb is that semiconductor failure rate is halved for each $10^{\circ} \mathrm{C}$ reduction in junction operating temperature.

## Chip Design

Proper thermal design by the integrated circuit user can reduce the operating temperature of the semiconductor junction. However, the minimum chip temperature at any power level is determined solely by the device manufacturer. For this reason, care must be taken in choosing the manufacturer. ' Exact equivalent'" integrated circuits are not necessarily identical. Electrically and mechanically they may be the same, but thermal differences can mean that 'identical', audio power amplifiers will not put out the same power without exceeding the rated junction temperature.

The circuit manufacturer must optimize his chip design so that component drift is minimized and /or equalized so that rated performance can actually be obtained under maximum thermal stress.

Note in Figures 8 and 9 that the Darlington input differential pairs are cross-connected so as to minimize differences in gain as a function of output transistor power dissipation. Transistor $Q_{4}$, being closest to the output power transistors is naturally the hottest; $\mathrm{Q}_{3}$ is a degree or two cooler; $\mathrm{Q}_{1}$ and $\mathrm{Q}_{2}$ are about equal and midway between $Q_{3}$ and $Q_{4}$. The gain of the $Q_{1}-Q_{2}$ Darlington pair is about equal to the gain of $Q_{3}-Q_{4}$ at all output power levels because of careful thermal design.


Figure 8


Figure 9

## PACKAGE INFORMATION (Continued)

In certain specialized applications, thermal coupling can be used to a distinct advantage. Experimentally, thermal coupling has been used to provide a low-pass feedback network which otherwise could be obtained only with very large values of capacitance.

The foregoing discussion has covered the average thermal characteristics of today's dual in-line plastic integrated circuits. The specific devices will vary with the different packages and bonding techniques employed, but the concepts will remain the same.

## APPENDIX

The following is intended to review terminology and compare thermal circuits with the more familiar electrical quantities.
The first law of thermodynamics states that energy cannot be created or destroyed but can be converted from one form to another. The second law of thermodynamics states that energy transfer will occur only in the direction of lower energy. In the semiconductor junction, the electrical energy is converted to thermal energy. Since no heat will be stored at the junction, the heat will flow to a lower temperature medium, air. The rate of heat flow is dependent on the resistance to that flow and the temperature difference between the source and the sink.


Figure 10

This thermal electrical analogy is convenient only for conduction problems where heat flow and temperature obey linear equations. The analogy becomes much more complex for situations involving heat flow by convection and radiation. Where these two modes are not negligible, they can be approximated by an equivalent thermal resistance. If ignored, the error introduced will only improve the device reliability.

A simplified thermal flow diagram of a molded dual in-line package and heat sink is shown. The
thermal resistance of the lead frame-heat sinkambient is shown as a variable resistor, because this is under the control of the user and may be varied over a considerable range.


Figure 11

| Material | Thermal Resistance in ${ }^{\circ} \mathrm{C} / \mathrm{W}$ <br> for Unit Area/Unit Length |
| :--- | :---: |
| Silver | 0.09 |
| Copper, Annealed | 0.10 |
| Gold | 0.12 |
| Beryllia Ceramic | 0.20 |
| Aluminum | 0.20 |
| Brass (66 Cu, 34 Zn ) | 0.40 |
| Silicon | 0.50 |
| Germanium | 0.70 |
| Steel, SAE 1045 | 0.80 |
| Solder (60 Sn, 40 Pb ) | 1.5 |
| Alumina Ceramic | 2.0 |
| Kovar (54 Fe, 29 Ni, 17 Co) | 3.0 |
| Glass | 40 |
| Epoxy | 40 |
| Mica | 50 |
| Teflon PTFE | 200 |
| Air | 2000 |

## Computing IC Temperature Rise

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Excessive heat shortens the life of an IC and reduces its operating capability. Until recently, ICs were capable of operating only in low-power applications requiring perhaps a few milliwatts of power. But now, new ICs handle several hundred milliamperes and drive devices such as relays, solenoids, stepping motors, and incandescent lamps. These high power levels may increase IC temperatures substantially and are capable of destroying devices unless appropriate precautions are taken.

## Thermal Characteristics

The thermal characteristics of any IC are determined by four parameters. Maximum allowable IC chip junction temperature $T_{J}$ and thermal resistance $R_{\theta}$ are specified by the IC manufacturer. Ambient temperature $T_{A}$ and the power dissipation $P_{D}$ are determined by the user. Equation 1 expresses the rela-

Heat is the enemy of integrated circuits-particularly power devices. Here's how to use thermal ratings to determine safe IC operation.

tion of these parameters.

$$
\begin{equation*}
T_{J}=T_{A}+P_{D} R_{\theta} \tag{1}
\end{equation*}
$$

Junction temperature $T_{J}$ usually is limited to $150^{\circ} \mathrm{C}$ for silicon ICs. Devices may operate momentarily at slightly higher temperatures, but device life expectancy decreases exponentially for extended hightemperature operation. Usually, the lower the junction operating temperature, the greater the anticipated life of the IC.

Ambient temperature $T_{A}$ is
traditionally limited either to $70^{\circ} \mathrm{C}$ or $85^{\circ} \mathrm{C}$ for plastic dual inline packages (DIPs) or $125^{\circ} \mathrm{C}$ for hermetic devices. Again, the objective is to operate at as low a junction temperature as practical.
Thermal resistance $R_{\theta}$ is the basic thermal characteristic for ICs. It is usually expressed in terms of ${ }^{\circ} \mathrm{C} / \mathrm{W}$ and represents the rise in junction temperature with a unit of power applied in still air. (The reciprocal of thermal resistance is thermal conductance, or derating factor,

## What the Curves Show

The junction temperature of an IC depends on several factors, including the thermal resistance of the IC and the operating duty cycle. Graphs showing the relationship of these factors are often useful in specifying an IC.

## Thermal Ratings




Typical thermal-resistance ratings for ICs in still air range from $60^{\circ} \mathrm{C} / \mathrm{W}$ to $140^{\circ} \mathrm{C} / \mathrm{W}$. The slope of each curve on this graph is equal to the derating factor $G \theta$, which is the reciprocal of thermal resistance $\mathrm{R}_{\boldsymbol{\theta}}$. For an ambient temperature of $50^{\circ} \mathrm{C}$, a typical 14-lead flatpack with an $\mathrm{R} \theta$ of $140^{\circ} \mathrm{C} / \mathrm{W}$ can dissipate about 0.7 W . A typical DIP, however, with 14 copper-alloy leads can dissipate almost 1.7 W at 50"C.

The highest allowable package power dissipation shown here is 2.5 W . Other special-purpose DIP packages are available with power dissipation ratings as high as 3.3 W at $0^{\circ} \mathrm{C}\left(\mathrm{R} \boldsymbol{H} \quad 45^{\circ} \mathrm{C} / \mathrm{W}\right)$. If not for package limitations, IC chip dissipation might be greater than 9 W at an ambient temperature of up to $70^{\circ} \mathrm{C}$.
Although the curve for plastic DIPs goes all the way to $150^{\circ} \mathrm{C}$. they ordinarily are not used in ambients above $85^{\circ} \mathrm{C}$ because of traditional package limitations. Hermetic DIPs are specified to temperatures of $125^{\circ} \mathrm{C}$, and at $150^{\circ} \mathrm{C}$ the device should be derated to 0 W . The higher
specification limits for hermetic devices is the result of their design for use in rigorous, high-reliability military applications.

Duty cycle is important in calculating IC junction temperature because average power-not instantaneous power-is responsible for heating the IC. To convert from peak power to average power, multiply the peak power dissipation by the duty cycle. The average-power rating is then used with the thermal-resistance rating to calculate the IC junction temperature. Thus, short duty cycles allow peak power to be high without exceeding the $150^{\circ} \mathrm{C}$ junction-temperature limit. However, this consideration applies only to ON times of less than 0.5 sec .
$G_{H}$ expressed as $\mathrm{W} /{ }^{\circ} \mathrm{C}$.) Thermal resistance of an IC consists of several distinct components, the sum of which is the specified thermal resistance. For a typical IC, these components of thermal resistance are $0.5^{\circ} \mathrm{C} / \mathrm{W}$ per unit thickness of the silicon chip, 0.1 to $3^{\circ} \mathrm{C} / \mathrm{W}$ per unit length of the lead frame, and up to $2,000^{\circ} \mathrm{C} / \mathrm{W}$ per unit thickness of still air surrounding the 10 . Dips are used more than any
other type of packaging for ICs and newer copper-alloy lead frames provide a superior thermal rating over the standard iron-nickel-cobalt alloy (Kovar) lead frames. However, power l's are also available in other packages such as flatpacks and To-type cans.

The power $P_{l}$, that an IC can safely dissipate usually depends on the size of the IC chip and the type of packaging. Most
common copper-frame DIPs can dissipate about 1.5 W , although some special-purpose types have ratings as high as 5 W .

## Power Dissipation

Total IC power to be dissipated depends on input current, output current, voltage drop, and duty cycle. Thus, for many industrial digital-control ICs, logic-gate power $P_{I}$ (typically less than 0.1 W ) and output
power $P_{o}$ must be determined to find the total power to be dissipated. Total power dissipation for these logic devices is the sum of $P_{l}$ and $P_{o}$.

$$
\begin{align*}
& P_{l}=n\left(V_{C C I} I_{C C}\right)  \tag{2}\\
& P_{0}=n\left(V_{C E(S: I T)} I_{C}\right) \tag{3}
\end{align*}
$$

where $V_{C C}=$ logic-gate supply voltage, $I_{C C}=$ logic-gate ON current, $V_{C E(S A T)}=$ output saturation voltage, $I_{C}=$ output load current, and $n=$ number of logic gates. Manufacturers usually list typical and maximum values for these voltages and currents. For thermal considerations it is best to use the maximum values so that worst-case power dissipation is determined.

If the duty cycle of the device is longer than 0.5 sec , the peak power dissipation is the sum of the logic-gate power $P_{l}$ and output power $P_{o}$ for the logic ON state alone. If the ON time is less than 0.5 sec , however, average power dissipation must be calculated from instantaneous ON and OFF power $P_{O N}$ and

## Finding Safe Operating Limits

Here's how to calculate the safe operating limits for an IC. The first two examples are simple calculations involving maximum allowable power and are straightforward. The third and fourth examples are more complex and involve logic power, output power, and duty cycle.

Problem: Determine the maximum allowable power dissipation that can be handled safely by a 16-lead Kovar DIP with an Rio of $125^{\circ} \mathrm{C} / \mathrm{W}$ in an ambient temperature of $70^{\circ} \mathrm{C}$.

Solution: From Equation 1, the maximum allowable power dissipation $P_{D}$ for this IC is

$$
\begin{aligned}
P_{n} & =\frac{150^{\circ} \mathrm{C}-70^{\circ} \mathrm{C}}{125^{\circ} \mathrm{C} / \mathrm{W}} \\
& =0.64 \mathrm{~W}
\end{aligned}
$$

Problem: Determine the maximum allowable power dissipation that can be handled by a 14 -lead copper DIP
with a derating factor $G_{\theta}$ of 16.67 $\mathrm{mW} /{ }^{\circ} \mathrm{C}$ in an ambient of $70^{\circ} \mathrm{C}$.

Solution: Since the derating factor
$G_{\theta}$ is the reciprocal of thermal
resistance $\mathrm{F}_{\theta}$, the maximum allowable
power dissipation $P_{p}$ from Equation 1 is

$$
\begin{aligned}
P_{D} & =\left(150^{\circ} \mathrm{C}-70^{\circ} \mathrm{C}\right) \\
& X\left(16.67 \mathrm{~mW} / /^{\circ} \mathrm{C}\right) \\
= & 1.33 \mathrm{w}
\end{aligned}
$$

Problem; Calculate the maximum junction temperature for a quad power driver with a thermal resistance of $60^{\circ} \mathrm{CM}$ in an ambient of $70^{\circ} \mathrm{C}$ and which is controlling a 250 mA load on each of the four outputs.

Solution: To determine the maximum (worst case) function ${ }^{-}$ temperature for this IC, the maximum total power dissipation must be. determined from the data listed on the iC data sheet. The specifications are usually listed as typical and minimum or maximum values. It is important to use maximum voltage and current limits to insure an adequate design. Common maximum values for an
$P_{\text {OFF }}$ from

$$
\begin{equation*}
P_{D}=D P_{O N}+(1-D) P_{O F F} \tag{4}
\end{equation*}
$$

## Corrective Actions

If the junction temperature or the required power dissipation
of the IC is calculated to be greater than the maximum values specified by the manufacturer, device reliability and operating characteristics possi-

## Measuring IC Temperature

Sometimes IC junction temperature cannot be calculated readily and instead must be measured. Measurement should be made when there is insufficient data with which to calculate, when the effects of external variables such as forced-air cooling or enclosure size must be determined, or as a check on the manufacturer's specifications regarding package thermal resistance.

The most popular technique for measuring IC temperature uses the characteristic of a diode to reduce its forward voltage with temperature. Many IC chips have some sort of accessible diode-parasitic, input protection, base-emitter junction, or output clamp. With this technique, a "sense" diode is calibrated so that forward voltage is a direct indicator of diode junction temperature. Then, current is applied to some other component on the chip to simulate operating conditions and to produce a temperature rise. Since the thermal resistance of the silicon chip is low, the temperature of the sense diode is assumed to be the same as the rest of the monolithic chip.

The sense diode should be calibrated over at least the expected junction operating temperature chamber. Apply an accurately measured, low current of about 1 mA through the
sense diode and measure the forward voltage in $25^{\circ} \mathrm{C}$ increments after stabilization at each temperature. This calibration provides enough data for at least six points to construct a diode-forward-voltage versus
junction-temperature graph at the specified forward current. A typical $25^{\circ} \mathrm{C}$ forward voltage is between 600 and 750 mV and decreases 1.6 to $2.0 \mathrm{mV} /{ }^{\circ} \mathrm{C}$.

For power levels above 2 W , it may be necessary to use more than a single transistor if only the device saturation voltage and sink current are used. When higher power is desired, keep the output out of saturation.

Measuring the sense-diode forward voltage may require a considerable waiting period ( 10 to 15 minutes) for thermal equilibrium. In any event, at the instant of measurement, the heating power may have to be disconnected since erroneous readings may result from IR drop in circuit common leads. Various circuit connections (such as four-point Kelvin) may be arranged to reduce or eliminate this source of error.

The IC junction temperature can be determined by comparing the voltage measurement with the internal power source against the voltage measurement with the temperature chamber.

PACKAGE INFORMATION (Continued)

Industrial power driver are $\mathrm{V}_{\mathrm{cc}}=5.25 \mathrm{~V}$, $\mathrm{I}_{\mathrm{cc}}=25 \mathrm{~mA}$, and $V_{\text {crsit }}=0.7 \mathrm{~V}$, and $I_{c}=$ 250 mA . From Equations 2 and 3, warst case logic and output power dissipation are

$$
\begin{aligned}
P_{1} & =4(5.25 \mathrm{~V} \times 25 \mathrm{~mA}) \\
& =525 \mathrm{~mW} \\
P_{\mathrm{o}} & =4(0.7 \mathrm{~V} \times 250 \mathrm{~mA}) \\
\mathrm{P}_{\mathrm{l}} & =700 \mathrm{~mW}
\end{aligned}
$$

Thus, the total worst case power dissipation $P_{p}$ is 525 mW plus 700 mW , or 1.225 W. From Equation 1 , maximum junction temperature T, is

$$
\begin{aligned}
T_{J} & =70^{\circ} \mathrm{C}+(1.225 \mathrm{~W}) \\
& \left.=143.67 \mathrm{~mW} /{ }^{\circ} \mathrm{C}\right) \\
& =143.5^{\circ} \mathrm{C}
\end{aligned}
$$

Probiom: Determine the acceptable duty cycle for a hermetic power driver with a thermal resistance of $100^{\circ} \mathrm{C} / \mathrm{W}$ in an amblent of $85^{\circ} \mathrm{C}$ and which is controlling load currents of 250 mA on each of four outputs.

Solution: From Equation 1, the allowable average power dissipation

Pof this ic is

$$
\begin{aligned}
P_{D} & =\frac{150^{\circ} \mathrm{C}-85^{\circ} \mathrm{C}}{100^{\circ} \mathrm{C} / \mathrm{W}} \\
& =0.65 \mathrm{~W}
\end{aligned}
$$

This means that there is 0.65 W limit on average power, but, not instantaneous power. If the duty cycle is low enough. and the ON time is not more than about 0.5 sec, the average power dissipation can be considerably lower than the peak power. The ON, or peak power, is determined from the data sheet maximum values of $V_{C c}, I_{c c}$, and $V_{\text {ceisin }}$ at the specified load current of 250 mA . From Equations 2 and 3, logic-gate power $P_{1}$ and output power $P_{j}$ for the ON state are

$$
\begin{aligned}
P_{t} & =4(5.5 \mathrm{~V} \times 26.5 \mathrm{~mA}) \\
& =583 \mathrm{~mW} \\
P_{o} & =4(0.7 \mathrm{~V} \times 250 \mathrm{~mA}) \\
& =700 \mathrm{~mW}
\end{aligned}
$$

Instantaneous ON power $P_{O N}$ is the sum of $P_{1}$ and $P_{0}$ for the ON state, or 1.283 W. The OFF poweris primarily the
power dissipated by the logic in the OFF state, and isfound by using the $I_{c c}$ maximum rated current listed on the specification sheet. The powor dissipated in the output stape en be calculated from the leakage current $I_{c}$ and supply voltage $V_{C E}$. From Equations 2 and 3, logic-gate power $P_{\text {, }}$ and output power $P$, for the OFF state are

$$
\begin{aligned}
P_{1} & =4(5.5 \mathrm{~V} \times 7.5 \mathrm{~mA}) \\
& =165 \mathrm{~mW} \\
P_{0} & =4(100 \mathrm{~V} \times 0.1 \mathrm{~mA}) \\
& =40 \mathrm{~mW}
\end{aligned}
$$

Instantaneous OFF power $P_{\text {orf }}$ is the sum of $P_{1}$, and $P_{0}$, for the OFF state, or 205 mW . From Equation 4, acceptable duty cycle $D$ is

$$
\begin{aligned}
D & =\frac{P_{D}-P_{\text {OFF }}}{P_{\text {ON }}-P_{\text {OFF }}} \\
& =\frac{0.65 \mathrm{~W}-0.205 \mathrm{~W}}{1.283 \mathrm{~W}-0.205 \mathrm{~W}} \\
& =4.3 \mathrm{~S}
\end{aligned}
$$

bly will be reduced. Possible solutions are: 1. Modify or partition the circuit design so the IC is not required to dissipate as much power. 2. Reduce the
thermal resistance of the IC by using a heat sink or forced-air cooling. 3. Reduce the ambient temperature by moving heatproducing components such as
transformers and resistor away from the IC. 4. Specify different IC with improve thermal or electrical charaı teristics (if available).

Setting Up the Circuit


Input power is negligible compared to output power and is therefore not measured.

Calibrating the Sense Diode


## Operating and Handling Practices for MOS Integrated Circuits

## Handling Practices - Packaged Devices

Sprague Electric incorporates input protection diodes in all of its MOS/CMOS devices. Because of the very high input resistance in MOS devices, the following practices should be observed for protection against high static electrical charges:

1. Device leads should be in contact with a conductive material except when being tested or in actual operation.
2. Conductive parts of tools, fixtures, soldering irons and handling equipment should be grounded.
3. Devices should not be inserted into or removed from test stations unless the power is off.
4. Neither should signals be applied to the inputs while the device power supply is in an off condition.
5. Unused input leads should be committed to either VSS $_{\text {or }}$ VDD. $_{\text {D }}$

## Handling Practices - Die

A conductive carrier should be used in order to avoid differences in voltage potential.

## Automatic Handling Equipment

Grounding alone may not be sufficient and feed mechanisms should be insulated from the devices under test at the point where the devices are connected to the test equipment. Ionized air blowers can be of aide here and are available commercially. This method is very effective in eliminating static electricity problems.

## Ambient Conditions

Dry weather with accompanying low humidity tends to intensify the accumulation of static charges on any surface. In this atmosphere, proper handling procedures take on added importance. If necessary, steam injectors can be procured commercially.

## Alert Failure Modes

The common failure modes that appear when static energy exists and when proper handling practices are not used are:

1. Shorted input protection diodes.
2. Shorted or 'blown' open gates.
3. Open metal runs.

Simple diagnostic checks with curve tracers or similar equipment readily identifies the above failure modes.

## 'A' PACKAGE: 14-Pin Plastic Dual In-Line

## DIMENSIONS IN INCHES



## DIMENSIONS IN MILLIMETRES

Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$



Dwg. No. A-5496G mm

## 'A' PACKAGE: 16-Pin Plastic Dual In-Line

## DIMENSIONS IN INCHES



DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'A' PACKAGE: 18-Pin Plastic Dual In-Line

## DIMENSIONS IN INCHES



Dwg. No. A-9649 in


Dwg. No, A-9649 mm

## 'A' PACKAGE: 20-Pin Plastic Dual In-Line

## DIMENSIONS IN INCHES

## DIMENSIONS IN MILLIMETRES

Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-10,430 in

NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'A' PACKAGE: 22-Pin Plastic Dual In-Line

## DIMENSIONS IN INCHES

## DIMENSIONS IN MILLIMETRES

Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


## 'B' PACKAGE: 8-Pin Plastic Dual In-Line



DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


DWG.NO. A-10,474A MM

## NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.
'B' PACKAGE: 14-Pin Plastic Dual In-Line

DIMENSIONS IN INCHES


DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


## 'B' PACKAGE: 16-Pin Plastic Dual In-Line

DIMENSIONS IN INCHES


DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-10,311B MM
'H' PACKAGE: 8-Pin Hermetic Dual In-Line

DIMENSIONS IN INCHES


DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-10,313A mm

NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'H' PACKAGE: 14-Pin Hermetic Dual In-Line

## DIMENSIONS IN INCHES

## DIMENSIONS IN MILLIMETRES

Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


## 'H' PACKAGE: 16-Pin Hermetic Dual In-Line

## DIMENSIONS IN INCHES

## DIMENSIONS IN MILLIMETRES

Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'H' PACKAGE: 18-Pin Hermetic Dual In-Line

## DIMENSIONS IN INCHES



Dwg. No. A-10,312A in

## 'J' PACKAGE: 14-Pin Hermetic Flat-Pack

DIMENSIONS IN INCHES


## NOTES:

1 INCLUDES OFF-CENTER LID, MENISCUS, + GLASS OVERRUN
2 AlL LEADS WELDABLE AND SOLDERABLE

DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-10,252A mm
Dwg. No. A-10,252A in

NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'M' PACKAGE: 8-Pin Plastic Dual In-Line



## 'Q' PACKAGE: 16-Pin Plastic Quad In-Line

DIMENSIONS IN INCHES


## DIMENSIONS IN MILLIMETRES

Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$



NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'R' PACKAGE: 14-Pin Ceramic Dual In-Line

## DIMENSIONS IN INCHES



DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$

## 'R' PACKAGE: 16-Pin Ceramic Dual In-Line

DIMENSIONS IN INCHES


DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-10,549 mm

NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'R' PACKAGE: 18-Pin Ceramic Dual In-Line

## DIMENSIONS IN INCHES

DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-10,548 in



Dwg. No. A-10,548 mm
'S' PACKAGE: 4-Pin Molded Single In-Line

## DIMENSIONS IN INCHES



Dwg. No. A-9002C in

DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-9002C mm

NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'T' PACKAGE: 3-Pin Plastic Single In-Line

## DIMENSIONS IN INCHES



Dwg. No. $A-11,118 \mathrm{~A}$ in

## DIMENSIONS IN MILLIMETRES

Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-11,118A mm

## 'W' PACKAGE: 12-Pin Plastic Single In-Line

## DIMENSIONS IN INCHES

JWG.NO. A-11,138A IN
DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


DWG.NO. A-11,138A MM

NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## ${ }^{\text {'Y }}$ ' PACKAGE: 3-Pin TO-92/TO-226AA



NOTE:
Lead diameter is controlled in the zone between $0.050^{\prime \prime}(0.13 \mathrm{~mm})$ and $0.250^{\prime \prime}(6.35 \mathrm{~mm})$ from the seating plane. Between $0.250^{\prime \prime}(6.35$ mm ) and $0.500^{\prime \prime}(12.7 \mathrm{~mm})$ from the seating plane. A maximum lead diameter of $0.021^{\prime \prime}(0.53 \mathrm{~mm})$ is specified. Outside of these zones the lead diameter is not controlled.

## 'Z' PACKAGE: 5-Lead TO-220

## DIMENSIONS IN INCHES



DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


NOTES:

1. Lead spacing tolerance is non-cumulative
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## 'ZH' PACKAGE: 5-Lead TO-220 <br> (Horizontal Mount)

DIMENSIONS IN INCHES


DIMENSIONS IN MILLIMETRES
Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


Dwg. No. A-10,462B MM
'ZV' PACKAGE: 5-Lead TO-220 (Vertical Mount)

DIMENSIONS IN INCHES


## DIMENSIONS IN MILLIMETRES

Based on $1^{\prime \prime}=25.4 \mathrm{~mm}$


NOTES:

1. Lead spacing tolerance is non-cumulative.
2. Exact body and lead configuration at vendor's option within limits shown.
3. Leads missing from their designated positions shall also be counted when numbering leads.
4. Terminal lead standoffs may be omitted and replaced by body standoffs.
5. Lead gauge plane is $0.030^{\prime \prime}(0.76 \mathrm{~mm})$ max. below seating plane.

## NOTES

In the construction of the components described, the full intent of the specification will be met. The Sprague Electric Company, however, reserves the right to make, from time to time, such departures from the detail specifications as may be required to permit improvements in the design of its products. Components made under military approvals will be in accordance with the approval requirements.

The information included herein is believed to be accurate and reliable. However, the Sprague Electric Company assumes no responsibility for its use; nor for any infringements of patents or other rights of third parties which may result from its use.



[^0]:    $\ddagger$ European registration; manufactured by various companies including ITT, SGS/ATES, Siemens,
    Thomson-CSF, AEG-Telefunken, \& Valvo.
    ISprague device includes internal pull-down resistors.
    *No longer manufactured - listed for reference only.
    $\dagger$ Some differences in specified switching speed with the Sprague device being superior for use with inductive loads.
    §Sprague engineering bulletin in preparation.

[^1]:    $\ddagger$ European registration; manufactured by various companies including $I T$, SGS/ATES, Siemens, Thomson-CSF, AEG-Telefunken, \& Valvo.
    ISprague device includes internal pull-down resistors.
    *No longer manufactured - listed for reference only.
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    *No longer manufactured - listed for reference only.
    $\dagger$ Some differences in specified switching speed with the Sprague device being superior for use with inductive loads.
    §Sprague engineering bulletin in preparation.

[^4]:    $\ddagger$ European registration; manufactured by various companies including IT, SGS/ATES, Siemens,
    Thomson-CSF, AEG-Telefunken, \& Valvo.
    ISprague device includes internal pull-down resistors.
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    tSome differences in specified switching speed with the Sprague device being superior for use with inductive loads.
    §Sprague engineering bulletin in preparation.

[^5]:    把uropean registration；manufactured by various companies including ITT，SGS／ATES，Siemens，
    Thomson－CSF，AEG－Telefunken，\＆Valvo．
    ISprague device includes internal pull－down resistors．
    ＊No longer manufactured－listed for reference only．
    †Some differences in specified switching speed with the Sprague device being superior for use with inductive loads．
    §Sprague engineering bulletin in preparation．

[^6]:    $\ddagger$ European registration; manufactured by various companies including ITT, SGS/ATES, Siemens;
    Thomson-CSF, AEG-Telefunken, \& Valvo.
    TSprague device includes internal pull-down resistors.
    *No longer manufactured - listed for reference only.
    $\dagger$ Some differences in specified switching speed with the Sprague device being superior for use with inductive loads.
    §Sprague engineering bulletin in preparation.

[^7]:    $\ddagger$ European registration; manufactured by various companies including IT, SGS/ATES, Siemens, Thomson-CSF, AEG-Telefunken, \& Valvo.
    -TSprague device includes internal pull-down resistors.
    *No longer manufactured - listed for reference only.
    +Some differences in specified switching speed with the Sprague device being superior for use with inductive loads.
    $\S$ Sprague engineering bulletin in preparation.

[^8]:    NOTE: 2P (2nd printing) indicates minor changes and/or corrections not normally affecting device performance.

[^9]:    (8) Panaplex is a registered trademark of the Burroughs Corporation
    *) Plasma-Lux is a registered trademark of Cherry Electrical Products Corporation

[^10]:    NOTE: Positive (negative) current is defined as going into (coming out of) the specified device pin.

[^11]:    ${ }^{\text {© }}$ Panaplex is a registered trademark of the Burroughs Corporation
    (1) Plasma-Lux is a registered trademark of Cherry Electrical Products Corporation

[^12]:    *Derate at the rate of $16.7 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$
    **Derate at the rate of $18.2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$

[^13]:    NOTE: Positive (negative) current is defined as going into (coming out of) the specified device pin.

[^14]:    *Specify input voltage $=4.5 \mathrm{~V}$ for devices with " -5 " suffix.
    NOTES:

    1. All voltage measurements are referenced to pin 9 unless otherwise specified.
    2. All voltage measurements made with $10 \mathrm{M}!$ !, DVM or VTVM.
    3. Recommended $V_{K K}$ operating range: -85 to -110 V .
[^15]:    Code: GD $=$ D-C Gas-Discharge \& Glow Transfer ACP $=\mathrm{A}-\mathrm{C}$ Plasma
    $\mathrm{VF}=$ Vacuum Fluorescent

[^16]:    NOTES:

    1. Input voltage is with reference to the substrate (no connection to any other pins) for the ULN-2061/62M and ULN-2074/75/76/77B; reference is ground for all other types. 2. Input current may be limited by maximum allowable input voltage.
[^17]:    *Pulse-Test

[^18]:    *Derate at the rate of $22: 2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $25^{\circ} \mathrm{C}$.

[^19]:    Series ULN-2800A and ULN-2810A devices are also available (with reduced package power capability) in industrial-grade hermetic packages. To order, change the last letter of the part number from ' $A$ ' to ' $R$ '. Note that the high-voltage devices ( $B V_{C E} \geq 95 \mathrm{~V}$ ) are not presently available with this packaging option.

[^20]:    ${ }^{*} I_{A}, I_{\mathbb{N}}$, and $I_{H}$ test conditions and limits for the paralleled SCRs at pin 8-9 or pin 1-16 of the UTN-2886B are twice the value shown

[^21]:    *All Inputs Simultaneously

[^22]:    *Examples and data in this application note applies equally to Series ULN-2800A Darlington arrays.

[^23]:    Caution: Sprague CMOS devices feature input static protection but are still

[^24]:    L = Low Logic Level
    $H=$ High Logic Level
    $X=$ Irrelevant
    $P=$ Present State
    $R=$ Previous State

[^25]:    $X=$ irrelevant
    $\mathrm{T}-1=$ previous output state
    $\mathrm{I}=$ present output state

[^26]:    *Derate at the rate of $16.7 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$

[^27]:    Caution: Sprague CMOS devices have input static protection but are still suscepti ble to damage when exposed to extremely high static electrical charges.

[^28]:    *Complete part number includes a prefix to indicate temperature range and a suffix to indicate package style. See following part number description.

[^29]:    *Complete part number includes a prefix to indicate temperature range and a suffix to indicate package style. See following part number description.

[^30]:    *Complete part number includes a prefix to indicate temperature range and a suffix to indicate package style. See following part number description.

[^31]:    *Complete part number includes a prefix to indicate temperature range and a suffix to indicate package style. See
    following part number description.

[^32]:    ${ }^{*}$ Derate at the rate of $13.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$. above $+25^{\circ} \mathrm{C}$.

[^33]:    *All inputs simultaneously.
    **Pulsed test.

[^34]:    Note: Operation of these devices with standard TTL or DTL may require the use of appropriate pull-up resistors to insure the minimum logic $\mathrm{l}^{1}$
    *Pulsed test.

[^35]:    Supply Voltage, $\mathrm{V}_{\text {cc }} \ldots . . . . . . . . . . . . . . . . . . .$. . (Note 1)
    
    Package Power Dissipation, $P_{D}$ (Note 2) . . . . . . . . . . . . 1.0 W
    Operating Temperature Range, $\mathrm{T}_{\mathrm{A}} \ldots \ldots-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
    Storage Temperature Range, $\mathrm{T}_{\mathrm{S}} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

    ## NOTES:

    1. Dependent on value of external current limiting resistor, 13 V at $0 \Omega$.
    2. Derate at the rate of $15 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.
[^36]:    ${ }^{\text {® }}$ Registered Trademark, Dolby Laboratories, Inc.

[^37]:    Note: $P_{D}$ is derated at the rate of $9.4 \mathrm{~mW} / \mathrm{W}^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.

[^38]:    Supply Voltage, $V_{C C}$18 V

    Regulator Current, $\mathrm{I}_{\text {REG }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 5.0 mA
    Package Power Dissipation, $P_{D}$ (see note) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 640 mW
    
    
    NOTE: $P_{D}$ is derated at the rate of $8.0 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.

[^39]:    ${ }^{(3)}$ Registered Trademark, Dolby Laboratories, Inc.

[^40]:    The ULX prefix to the part number denotes an integrated circuit presently in development and undergoing engineering evaluation. If and when the device becomes a production item, the prefix will be changed to ULN. Sprague Electric assumes no obligation for future manufacture of any products presently in development unless such obligation is specifically undertaken in

[^41]:    Supply Voltage, $\mathrm{V}_{\text {CC }}$. . . . . . . . . . . . . . . . . . . . . . . . . . . 16 V
    
    Package Power Dissipation, $P_{D}$ (see note) .......... 670 mW
    Operating Temperature Range, $T_{A} \ldots \ldots . .-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
    Storage Temperature Range, $T_{S} \ldots \ldots . .-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
    NOTE: $P_{D}$ is derated at the rate of $8.3 \mathrm{~mW} / \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$

[^42]:    Copyright © 1980 IEEE. Reprinted by permission. This paper was originally presented at the IEEE Fall Conference on Consumer Electronics, Chicago, III., November 1980.

[^43]:    (1) Sprague Type ULN2240, $41,42 \mathrm{~A}$, or TDA1090.
    (2) Sprague Type ULN2249A or HA1 199

[^44]:    *Derate at the rate of $0.25 \mathrm{~W} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{TAB}}=90^{\circ} \mathrm{C}$

[^45]:    *Derate at the rate of $0.25 \mathrm{~W} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{TAB}}=90^{\circ} \mathrm{C}$

[^46]:    *Derate at the rate of $3^{\circ} \mathrm{C} / \mathrm{W}$ above $\mathrm{T}_{\mathrm{TAB}}=+70^{\circ} \mathrm{C}$

[^47]:    Note: Magnetic flux density is measured at most sensitive area of device. This area is located $0.032^{\prime \prime} \pm 0.002(0.81 \pm 0.05 \mathrm{~mm})$ below the branded face of the $T$ package and $0.012^{\prime \prime} \pm 0.002^{\prime \prime}(0.30 \pm 0.05 \mathrm{~mm})$ below the branded surface of the $U$ package.

[^48]:    *Magnetic flux density is measured at most sensitive area of device located $0.032^{\prime \prime} \pm 0.002(0.81 \pm 0.05 \mathrm{~mm})$ below the branded face of the T package and $0.012^{\prime \prime} \pm 0.002^{\prime \prime}$ ( $0.30 \pm 0.05 \mathrm{~mm}$ ) below the branded surface of the $U$ package.

[^49]:    NOTE: A rotary magnet may be constructed with poles either on the rim (axial) or on the face (radial) but not both.

[^50]:    NOTE 1. All output voitage measurements are made with a voltmeter having an input impedance of $10 \mathrm{k} \Omega$ or greater.
    NOTE 2. Magnetic flux density is measured at the most sensitive area of the device, which is centered on the branded side of the T package, $0.042 \pm 0.001^{\prime \prime}(1.07 \pm 0.03 \mathrm{~mm})$ below the surface and $0.022^{\prime \prime} \pm 0.001^{\prime \prime}(0.56 \pm 0.03 \mathrm{~mm})$ below the branded side of the $U$ package.

[^51]:    1. I $I_{\text {cc }}$ is limited to a maximum value which produces a 7 -volt drop across the Control Resistance $R_{1-3}$.
    2. Terminal 1 must always be positive in relation to terminal 3.
[^52]:    *Indiana General Magnet Products Co. SR8522.

[^53]:    NOTE 1. All output voltage measurements are made with a voltmeter having an input impedance of $10 \mathrm{k} \Omega$ or greater.
    NOTE 2. Magnetic flux density is measured at the most sensitive area of the device, which is centered on the branded side of the package: $0.042 \pm 0.001^{\prime \prime}(1.07 \pm 0.03 \mathrm{~mm})$ below the surface of the $T$ package or $0.022^{\prime \prime} \pm 0.001^{\prime \prime}(0.56 \pm 0.03 \mathrm{~mm})$ below the surface of the $U$ package.

[^54]:    Notes:

    1. The maximum ratings are limiting absolute values above which the serviceability may be impaired from the viewpoint of life or satisfactory performance. The breakdown voltages may be far above the maximum voltage ratings. To avoid permanent damage to the transistor, do not attempt to measure these characteristics above the maximum ratings.
    2. Pin 5 is connected to the substrate. This terminal must be tied to the most negative point in the external circuit to maintain isolation between transistors and to provide for normal transistor action.
[^55]:    *Applies only to transistors $\mathrm{Q}_{1}$ and $\mathrm{Q}_{2}$ when connected as a differential pair.

[^56]:    
    
    
    
    Operating Temperature Range, $T_{A}$ (ULN-2140A) $\ldots \ldots \ldots \ldots \ldots . . .$.
    (ULS-2140H) $\ldots \ldots . \ldots . . . . .$.
    Storage Temperature Range, $\mathrm{T}_{\mathrm{s}} \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots . . .{ }^{-15} 5^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$

[^57]:    *Derate at the rate of $4.2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$.

[^58]:    *Derate linearly to 0 watts at $T_{A}=+150^{\circ} \mathrm{C}$.

[^59]:    NOTES: Negative current is defined as coming out of (sourcing) the specified device pin.

[^60]:    * These devices are manufactured in accordance with a cross-license with Signetics Corp. (a subsidary of U.S. Philips Corp.).

