



Application Program

GH20-0205-4

System/360 Scientific Subroutine Package

Version III

Programmer's Manual

Program Number 360A-CM-03X

The Scientific Subroutine Package (SSP) is a collection of over 250 FORTRAN subroutines divided, for the sake of presentation, into two groups: statistics and mathematics. Also, over 200 subroutines are presented in both single and double precision mode. SSP is a collection of input/output-free computational building blocks that can be combined with a user's input, output, or computational routines to meet his needs. The package can be applied to the solution of many problems in industry, science, and engineering.

Version 3 of the Scientific Subroutine Package for System/360 incorporates and extends the capabilities of the original SSP/360. This version provides over 40 new mathematical and statistical subroutines 24 of which are in both single- and double-precision FORTRAN. Examples of the new capabilities are the use of the QR iteration for obtaining eigenvalues of a matrix, and the nonparametric test of Kolmogorov-Smirnov.

This manual contains sufficient information to permit the reader to understand and use all of the subroutines of the Scientific Subroutine Package.

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This edition, GH20-0205-4, is a reprint of GH20-0205-3 incorporating TNL GN20-1994. It does not obsolete GH20-0205-3 as updated by that TNL.

This edition applies to Version 3, Modification Level 1, of System/360 Scientific Subroutine Package (360A-CM-03X) and to all subsequent versions and modifications until otherwise indicated in new editions or Technical Newsletters.

Changes are continually made to the information herein. Therefore, before using this publication, consult the latest System/360 SRL Newsletter (GN20-0360) for the editions that are applicable and current.

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This programming package has been developed with the cooperation and assistance of IBM Germany and IBM France.

PURPOSE AND OBJECTIVES OF THE PACKAGE

The Scientific Subroutine Package is a set of basic computational subroutines intended to aid the user in the development of his own FORTRAN subroutine library. While this package may provide many of the tools necessary to solve the more commonly encountered problems in engineering and science, there is no intent to imply that these subroutines represent the current state of the art in statistics or numerical analysis. As with all tools, the user should understand their capabilities and their application to his functional requirements before deciding to use them.

AREAS OF APPLICATION

Individual subroutines, or a combination of them, can be used to carry out the listed functions in the following areas:

Statistics

- Probit analysis
- Analysis of variance (factorial design)
- Correlation analysis
- Multiple linear regression
- Stepwise regression
- Polynomial regression
- Canonical correlation
- Factor analysis (principal components, varimax)
- Discriminant analysis (many groups)
- Time series analysis
- Data screening and analysis
- Nonparametric tests
- Random number generation (uniform, normal)
- Distribution functions

Mathematics

- Inversion
- Eigenvalues and eigenvectors
- Simultaneous linear algebraic equations
- Transpositions
- Matrix arithmetic (addition, product, etc.)
- Matrix partitioning
- Matrix tabulation and sorting of rows or columns
- Elementary operations on rows or columns of matrices
- Matrix factorization
- Integration and differentiation of given or tabulated functions
- Solution of systems of first-order differential equations

- Fourier analysis of given or tabulated functions
- Bessel and modified Bessel function evaluation
- Gamma function evaluation
- Jacobian elliptic functions
- Elliptic, exponential, sine cosine, Fresnel integrals
- Finding real roots of a given function
- Finding real and complex roots of a real polynomial
- Polynomial arithmetic (addition, division, etc.)
- Polynomial evaluation, integration, differentiation
- Chebyshev, Hermite, Laguerre, Legendre polynomials
- Minimum of a function
- Approximation, interpolation, and table construction

CHARACTERISTICS

Some of the characteristics of the Scientific Subroutine Package are:

- All subroutines are free of input/output statements.
- Subroutines do not contain fixed maximum dimensions for the data arrays named in their calling sequences.
- All subroutines are written in FORTRAN.
- Many matrix manipulation subroutines handle symmetric and diagonal matrices (stored in economical, compressed formats) as well as general matrices. This can result in considerable saving in data storage for large arrays.
- The use of the more complex subroutines (or groups of them) is illustrated in the program documentation by sample main programs with input/output.
- All subroutines are documented uniformly.

The subroutines in SSP have been programmed in the subset of the FORTRAN IV language, which is compatible with all of the FORTRAN processors announced for System/360. Many of the larger functions such as those in statistics have been programmed as a series or sequence of subroutines.

An example of the use of sequences of subroutines is the statistical function called factor analysis. Factor analysis is a method of analyzing the inter-correlations within a set of variables. It determines whether the variance in the original set of variables can be accounted for adequately by a

smaller number of basic categories; namely, factors. In the Scientific Subroutine Package, factor analysis is normally performed by calling the following five subroutines in sequence:

1. CORRE - to find means, standard deviations, and correlation matrix
2. EIGEN - to compute eigenvalues and associated eigenvectors of the correlation matrix
3. TRACE - to select the eigenvalues that are greater than or equal to the control value specified by the user

4. LOAD - to compute a factor matrix
5. VARMX - to perform varimax rotation of the factor matrix

The multiple use of subroutines is illustrated by the fact that subroutine CORRE is also utilized in the multiple linear regression and canonical correlation. Subroutine EIGEN is used in canonical correlation as a third-level subroutine.

OVERALL RULES OF USAGE

GENERAL RULES

All subroutines in the Scientific Subroutine Package (SSP) are entered by means of the standard FORTRAN CALL statement. These subroutines are purely computational in nature and do not contain any references to input/output devices. The user must therefore furnish, as part of his program, whatever input/output and other operations are necessary for the total solution of his problem. In addition, the user must define by DIMENSION statements all matrices to be operated on by SSP subroutines as well as those matrices utilized in his program. The subroutines contained in SSP are no different from any user-supplied subroutine. All of the normal rules of FORTRAN concerning subroutines must therefore be adhered to, with the exception that the dimensioned areas in the SSP subroutine are not required to be the same as those in the calling program.

The CALL statement transfers control to the subroutine and replaces the dummy variables in that subroutine with the value of the actual arguments that appear in the CALL statement if the argument is a constant or a variable. When the argument is an array or function subprogram name, the address of the array or subprogram is transmitted to the called subroutine.

The arguments in a CALL statement must agree in order, number, and type with the corresponding arguments in the subroutine. A number may be passed to a subroutine either as a variable name in the argument list or as a constant in the argument list. For example, if the programmer wishes to add matrix AR1 to matrix AR2 in order to form matrix AR3 using the SSP subroutine GMADD, and if AR1 and AR2 are both matrices with ten rows and twenty columns, either of the two following methods can be used:

```
Method 1      .
              CALL GMADD(AR1, AR2, AR3, 10, 20)
              .
Method 2      .
              N = 10
              M = 20
              CALL GMADD(AR1, AR2, AR3, N, M)
              .
```

Many of the subroutines in SSP require the name of a user function subprogram or a FORTRAN-supplied function name as part of the argument list

in the CALL statement. If the user's program contains such a CALL, the function name appearing in the argument list must also appear in an EXTERNAL statement at the beginning of that program.

For example, the SSP subroutine RK2 integrates a function furnished by the user. The user must therefore program the function and give the name of the function to RK2 as a parameter in the CALL statement. If the user wishes to integrate the function $\frac{dy}{dx} = 3.0x + 2.0Y$, his main program may appear as:

```
EXTERNAL DERY
      .
      .
      CALL RK2(DERY, ..... )
      .
      .
      RETURN
      END
```

His function subprogram can be:

```
FUNCTION DERY (X, Y)
      DERY= 3.0*X+2.0*Y
      RETURN
      END
```

The user's main program gives the name of the programmed function to RK2 by including that name in the CALL statement and in an EXTERNAL statement. RK2, in turn, goes to the function DERY each time it requires a value for the derivative. The subroutine RK2 is not modified by the programmer. The dummy function name FUN in subroutine RK2 is, in effect, replaced by the name appearing in the user's CALL statement during execution of the subroutine.

MATRIX OPERATIONS

Special consideration must be given to the subroutines that perform matrix operations. These subroutines have two characteristics that affect the format of the data in storage--variable dimensioning and data storage compression.

Variable Dimensioning

Those subroutines that deal with matrices can operate on any size array, limited in most cases only by the available core storage and numerical analysis considerations. The subroutines do not contain fixed maximum dimensions for data arrays named in their calling sequence. The variable dimension capability

has been implemented in SSP by using a vector storage approach. Under this approach, each column of a matrix is immediately followed in storage by the next column. Vector storage and two-dimensional storage result in the same layout of data in core, so long as the number of rows and columns in the matrix are the same as those in the user's dimension statement. If, however, the matrix is smaller than the dimensioned area, the two forms of storage are not compatible.

Consider the layout of data storage when operating on a 5 by 5 array of numbers in an area dimensioned as 10 by 10. If the programmer has been using double-subscripted variables in the normal FORTRAN sense, the 25 elements of data will appear as shown in Figure 1. FORTRAN stores double-subscripted data by column based on the column length specified in the DIMENSION statement. Thus, in the example, sequential core locations will contain data elements 1 to 5, five blank locations, data elements 6 to 10, five blank locations, and so on. The matrix subroutines take a vector approach in storing arrays by column, which means that they assume the data is stored as shown in Figure 2.

		Column									
		1	2	3	4	5	6	7	8	9	10
Row	1	(1)	(6)	(11)	(16)	(21)					
	2	(2)	(7)	(12)	(17)	(22)					
	3	(3)	(8)	(13)	(18)	(23)					
	4	(4)	(9)	(14)	(19)	(24)					
	5	(5)	(10)	(15)	(20)	(25)					
6											
7											
8											
9											
10											

Figure 1. Double-subscripted data storage

(1)	(11)	(21)
(2)	(12)	(22)
(3)	(13)	(23)
(4)	(14)	(24)
(5)	(15)	(25)
(6)	(16)	
(7)	(17)	
(8)	(18)	
(9)	(19)	
(10)	(20)	

Figure 2. Vector storage

As stated previously, if the dimensioned area is the same as the matrix size, the two approaches will have the same data storage layout, and the user can proceed in a regular double-subscripted fashion. If, however, he is operating in a mode where the dimensioned area is larger than the arrays, and if he wishes to use the SSP subroutines, he must be certain that his data is stored in the vector fashion illustrated by Figure 2. A subroutine called ARRAY is available in SSP to change from one form of storage to the other. In addition, a subroutine called LOC is available to assist in referencing elements in an array stored in the vector fashion.

Storage Compression

Many subroutines in SSP can operate on compressed forms of matrices as well as on the normal form. By using this capability, which is called "storage mode", considerable savings in data storage can be obtained for special forms of large arrays. The three modes of storage are termed general, symmetric, and diagonal. In this context, general mode is one in which all elements of the matrix are in storage. Symmetric mode is one in which only the upper triangular portion of the matrix is retained columnwise in sequential locations in storage. (The assumption is made that the corresponding elements in the lower triangle have the same value.) Diagonal mode is one in which only the diagonal elements of the matrix are retained in sequential locations in storage. (The off-diagonal elements are assumed to be zero.) This capability has been implemented using the vector storage approach.

Figure 3 illustrates the effect of the storage mode capability. A symmetric matrix is shown in Figure 3A. If this array is to be manipulated using the SSP matrix subroutines with storage mode capability, the array may be stored as shown in Figure 3B. This is the upper triangular portion of the array and corresponds to a storage mode code of 1. Symmetric matrices of order N may be stored in a vector of only $N*(N+1)/2$ locations rather than $N*N$ locations. For larger matrices, this will be a saving of almost one half.

The effect of storage mode when dealing with diagonal matrices is even more pronounced. Diagonal matrices of order N may be stored in a vector only N locations long. Figure 3C shows a 3 by 3 diagonal matrix. If this array is to be manipulated using the SSP matrix subroutines with storage mode capability, only the diagonal elements of the array need be stored. This is shown in Figure 3D and corresponds to a storage mode code of 2.

General matrices of order N by M require a vector $N*M$ long and use a storage mode code of 0.

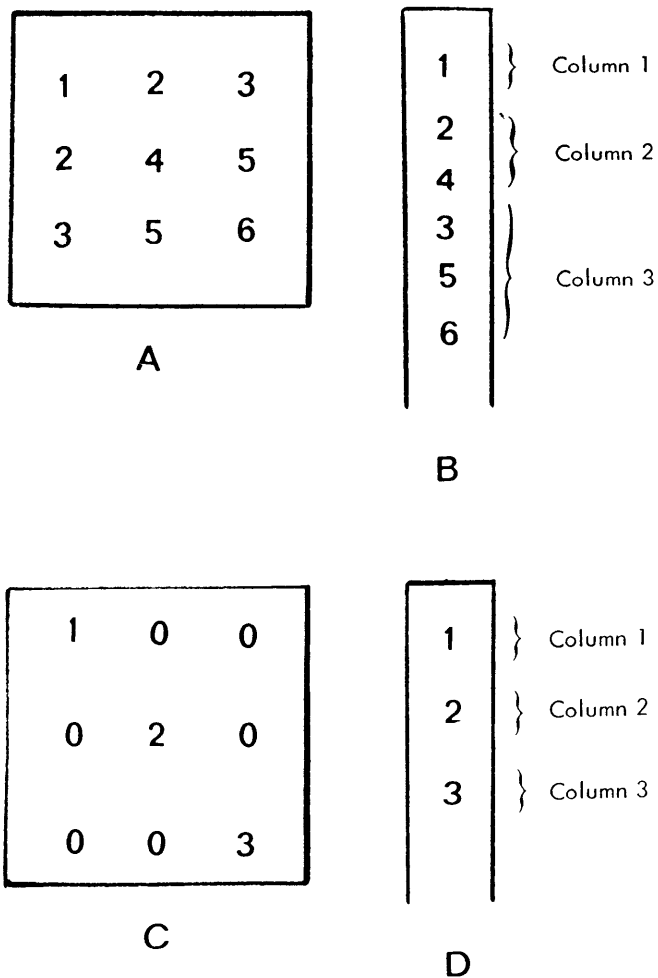


Figure 3. Storage mode

Thus, if the programmer wishes to use SSP subroutines on matrix A, which is general, matrix B, which is symmetric, and matrix C, which is diagonal, and all matrices are 10 by 10 or smaller, the dimension statement in his program can be:

```
DIMENSION A(100), B(55), C(10)
```

Matrix Element References

Subroutine LOC in the Scientific Subroutine Package may be used to reference elements within a matrix stored in a vector fashion, and may involve storage mode compression. The calling sequence for LOC is:

```
CALL LOC (I, J, IJ, N, M, MS)
```

The capabilities of subroutine LOC are as follows. If reference is required to the element at row I and column J of matrix A whose dimensions are N by M, and if the storage mode code is MS, a CALL to the LOC subroutine as shown above will result in the

computation of the subscript IJ such that A(IJ) is the desired element. The parameters represented by I, J, N, M, MS can be either integer variables or integer constants. The parameter represented by IJ is an integer variable. Note that the user must dimension the array A as a single-subscripted variable to meet the restrictions of some FORTRAN systems. To illustrate the use of LOC, if reference is required to the element at row 2, column 2 of the 3 by 3 symmetric matrix illustrated in Figure 3A and stored as shown in Figure 3B (storage mode code 1), the sequence may be:

```
CALL LOC (2, 2, IJ, 3, 3, 1)
```

The value of IJ computed by LOC will be 3, meaning that the proper element is the third element in the specially stored symmetric matrix (Figure 3B). If the storage mode code is for a symmetric matrix where only the upper triangular portion is retained in storage, and if I and J refer to an element in the lower triangular portion, IJ will contain the subscript for the corresponding element in the retained upper triangle. Thus if the user wanted the element in row 3, column 1 of the matrix shown in Figure 3A, and the array was stored as in Figure 3B, the statement:

```
CALL LOC (3, 1, IJ, 3, 3, 1)
```

would result in IJ having the value of 4; that is, the fourth element in Figure 3B. If a matrix is stored as shown in Figure 3D (storage mode 2), and LOC is used to compute the subscript for an off-diagonal element (I not equal to J), the result in IJ will be zero. This is due to the fact that the element does not exist in storage. In this situation, the user must not utilize IJ as a subscript. Following is an illustration of how to take care of this condition and also handle the case where the current storage mode is unknown.

If the user wishes to set a variable X equal to the element in the third row and fourth column of a 10 by 10 array named A, for either a symmetric, diagonal, or general matrix, the required program can be implemented for any storage mode MS as follows:

```
CALL LOC (3, 4, IJ, 10, 10, MS)
X = 0.0
IF(IJ)20, 30, 20
20 X = A(IJ)
30 -----
```

(MS is assumed to have been set at 0, 1, or 2 at some earlier point in the program.) This sequence will then set the proper value for X, given any storage mode that may be encountered. The second and third statements take care of the off-diagonal condition for a matrix with a storage mode of 2.

As a special case, LOC can be used to compute the total length of an array in storage with a statement such as:

```
CALL LOC (N, M, IJ, N, M, MS)
```

For example, if the user has a 3 by 3 matrix whose storage mode is 1 (Figure 3B), the statement:

```
CALL LOC (3, 3, IJ, 3, 3, 1)
```

will result in IJ being set to 6. This is not only the proper subscript to reference element 3, 3, but is also the actual length of the vector in storage.

The information contained in the fifth parameter (number of columns) in the calling sequence for LOC is not actually used in the calculations performed by LOC. It has been included in the calling sequence in case the user wishes to expand LOC to cover other forms of data storage.

PROGRAM MODIFICATION

ADVANCED FORTRAN FEATURES

The user may wish to take advantage of more advanced FORTRAN compiler features. For example, the larger FORTRAN systems include a subroutine multiple entry point capability. Some of the subroutines in SSP can be combined by using this feature. To illustrate this, GMADD and GMSUB (addition and subtraction of general matrices) can be combined as shown in Figure 4. This will in no way affect the programs using these subroutines but will reduce the total program storage requirements.

```

SUBROUTINE GMADD (A,B,R,N,M)
DIMENSION A(1),B(1),R(1)

K=0

GO TO 10

ENTRY GMSUB (A,B,R,N,M)

K=1

10 NM=N*M
DO 40 I=1,NM
IF(K) 20,20,30

20 R(I)=A(I)+B(I)
GO TO 40

30 R(I)=A(I)-B(I)

40 CONTINUE

RETURN

END
    
```

Figure 4. Multiple entry point

OPTIMIZATION OF TIME

The subroutines in SSP are designed to conserve storage for data. If the user wishes to exchange space for time, there are several ways in which SSP may be modified to effect this end. For example, many of the subroutines in SSP make use of the LOC subroutine to handle vector storage and storage mode referencing. The execution time of these subroutines can be substantially reduced by implementing LOC in Assembler Language. (The distributed version of LOC is implemented in FORTRAN.) Another approach is to incorporate the function of

LOC within each subroutine and thus avoid the "set-up" costs of repeated calls to LOC. This has the effect of reducing execution time but at some cost in subroutine storage and in the ease with which other modes of storage, such as triangular matrix storage or storage by row rather than by column, can be implemented. Figure 5 shows how matrix addition and the LOC capabilities can be implemented within the same subroutine.

```

SUBROUTINE MACX(A,B,R,N,M,MSA,MSB)
DIMENSION A(1),B(1),R(1)

C
C TEST FOR SAME STORAGE MODE
C
IF(MSA-MSB) 30,10,30

C
C COMPUTE VECTOR LENGTH
C
10 ND=N*M
IF(MSA-1) 24,22,23
22 ND=(ND+N)/2
GO TO 24
23 ND=N

C
C ADD MATRICES OF SAME STORAGE MODE
C
24 DO 25 I=1,ND
25 R(I)=A(I)+B(I)
RETURN

C
C GET STORAGE MODE OF OUTPUT MATRIX
C
30 MTEST=MSA*MSB
MSR=0
IF(MTEST) 35,35,32
32 MSR=1
35 DO 60 J=1,M
DO 60 I=1,N

C
C LOCATE ELEMENT IN OUTPUT MATRIX
C
KX=-1
MS=MSR
GO TO 65
40 IJR=IR

C
C LOCATE ELEMENT IN MATRIX A
C
KX=0
MS=MSA
GO TO 65
45 IJA=IR
AEL=0.0
IF(IJA) 46,48,46
46 AEL=A(IJA)

C
C LOCATE ELEMENT IN MATRIX B
C
48 KX=1
MS=MSB
GO TO 65
50 IJB=IR
BEL=0.0
IF(IJB) 55,60,55
55 BEL=B(IJB)

C
C ADD MATRICES OF DIFFERENT STORAGE MODES
C
60 R(IJR)=AEL+BEL
RETURN

C
C IN LINE LOC
C
65 IF(MS-1) 70,75,90
70 IR=N*(J-1)+1
GO TO 95
75 IF(I-J) 80,85,85
80 IP=1+(J+J-1)/2
GO TO 95
85 IR=J+(I-1)/2
GO TO 95
90 IP=C
IF(I-J) 95,92,95
92 IR=I
95 IF(KX) 40,45,50
END
    
```

Figure 5. Inline LOC

DOUBLE PRECISION

The accuracy of the computations in many of the SSP subroutines is highly dependent upon the number of significant digits available for arithmetic operations. Matrix inversion, integration, and many of the statistical subroutines fall into this category. The user may, therefore, wish to use double-precision versions of these subroutines.

Many of the subroutines in SSP have been provided in both single- and double-precision versions. In others, instructions for converting to double precision are included as part of the subroutine description. FORTRAN double-precision statements have been included in each of these subroutines in the form of a comments card. In most cases, the double-precision version of the subroutine can be obtained merely by removing the C from column 1 of the double-precision statement card(s) before compilation. In a few cases, additional instructions are given for changing references to FORTRAN-furnished functions; for example, SQRT to DSQRT and ABS to DABS; in other cases, new constants are given.

The use of double-precision subroutines requires a detailed knowledge of the FORTRAN rules concerning double precision. A few of the more basic ones are as follows:

1. Any real variable, vector, or array name contained in the argument list of a CALL to a double-precision subroutine must be declared as double precision in the calling program. For example, if the SSP matrix inversion subroutine MINV has been modified for double precision, and if the user's program contains the statement:

```
CALL MINV (AR1, N, DET, MY1, MY2)
```

where:

AR1 is the array name (real, double-precision array)

N is the dimension (integer variable)

DET is the determinant (real, double-precision variable)

MY1 is a work vector (integer array)

MY2 is a work vector (integer array)

then the program must also have at its beginning the specification statement:

```
DOUBLE PRECISION AR1, DET
```

The other variables are integer variables and should not be included in the specification statement.

2. Any user-supplied function named in the CALL statement for a double-precision SSP subroutine must be programmed as a double-precision function. For example, the sample program for Runge-Kutta integration performs the integration on a sample function called FUN using subroutine RK2. This function is programmed as:

```
FUNCTION FUN (X, Y)
```

```
FUN = 1.1*X
```

```
RETURN
```

```
END
```

If a double-precision version of RK2 is used, the function must also be double precision. The sample function will then be:

```
DOUBLE PRECISION FUNCTION FUN (X, Y)
```

```
DOUBLE PRECISION X, Y
```

```
FUN = 1.1*X
```

```
RETURN
```

```
END
```

FORMAT OF THE DOCUMENTATION

The major portion of this manual consists of the documentation for the individual subroutines and the sample programs.

SUBROUTINE DESCRIPTIONS

Subroutine and sample program guides, both categorical and alphabetic, designed to aid in locating any particular subroutine are given in the pages that follow.

Each of the subroutine descriptions consists of a program listing and, in some cases, a mathematical description. The first part of the program listing is a set of comment cards containing the subroutine name, its calling sequence, description of parameters, remarks, names of other subroutines required, and method. References to books and periodicals will be found under the method section of the description. The mathematical description pages do not, in most cases, indicate the derivation of the mathematics. They are intended to indicate what mathematical operations are actually being performed in the subroutines. Some of the major statistical functions are performed by a sequence of SSP subroutines. An explanation of this sequence will be found just before the description of the first subroutine that is specific to this function.

SAMPLE PROGRAM DESCRIPTIONS

The sample program listings are given in Appendix B.

Each sample program consists of a detailed description including information on the problem, the program, input, output, program modification, operating instructions, error messages, timing and machine listings of the programs, input data and output results. The sample programs have been

chosen to (1) illustrate a sequence of SSP subroutines, (2) illustrate the use of a complex subroutine, or (3) show the way in which one member (such as matrix addition) of a large set of simple subroutines might be used.

As part of the development of the sample programs, some special sample subroutines have been implemented that may prove useful to the programmer. These include:

HIST - print a histogram of frequencies

MATIN - read an input matrix into storage in vector form for use by SSP matrix subroutines

PLOT - plot several variables versus a base variable

MXOUT - print a matrix stored in the SSP vector format

Listings of the above subroutines are included after the sample program documentation in this manual. The source decks are part of the sample program source decks on the distributed magnetic tape.

The sample programs have been implemented for execution on a 32K byte (8K word) System/360 using Basic Programming Support FORTRAN (Tape). Instructions for modifying the sample programs for different data capacities are included in the documentation. In addition, those sample programs that illustrate potentially double-precision subroutines include double-precision statements in the form of comment cards. These comment cards are contained in the sample program source decks.

OPERATING NOTES

It is recommended that those SSP subroutines that will be frequently used in an installation be compiled and the relocatable decks placed on the FORTRAN system's residence device. In the case of Basic Programming Support FORTRAN (Tape), this will be the library portion of the system tape. Information on the method for updating the system to include

user-supplied subroutines will be found in the appropriate FORTRAN programmer's guide. SSP subroutines are handled in the same manner as user-supplied subroutines. If the subroutines are not placed on the FORTRAN system's residence device, those required by a particular program will have to be included in that program each time it is run.

CATEGORIAL GUIDE TO SUBROUTINES AND
SAMPLE PROGRAMS

(Subroutines added in Version III are marked with an asterisk)

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GUIDE TO SAMPLE PROGRAMS

Data Screening

DASCR--Sample Main Program	400
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Illustrates use of:

SUBST--subset selection from observation matrix

TAB1--tabulation of data (one variable)

LOC--location in compressed-stored matrix

Special sample subroutines are:

BOOL--Boolean expression

HIST--histogram printing

MATIN--matrix input

Multiple Linear Regression

REGRE--Sample Main Program	404
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Illustrates use of:

CORRE--means, standard deviations, and correlations

ORDER--rearrangement of intercorrelations

MINV--matrix inversion

MULTR--multiple regression

Special sample subroutine is:

DATA--sample data read

Polynomial Regression

POLRG--Sample Main Program	408
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Illustrates use of:

GDATA--data generation

ORDER--rearrangement of intercorrelations

MINV--matrix inversion

MULTR--multiple regression

Special sample subroutine is:

PLOT--output plot

*Stepwise Multiple Regression

*STEPR--Sample Main Program	413
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Illustrates use of:

CORRE--means, standard deviations, and correlations

MSTR--storage conversion

*STPRG--stepwise multiple regression

LOC--location in compressed-stored matrix

Special sample subroutines used are:

*STOUT--sample stepwise regression output subroutine

DATA--sample data read subroutine

Canonical Correlation

MCANO--Sample Main Program	418
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Illustrates use of:

CORRE--means, standard deviations, and correlations

CANOR--canonical correlation		Special sample subroutine is:	
MINV--matrix inversion		DATA--sample data read	
NROOT--eigenvalues and eigenvectors of a special, nonsymmetric matrix		<u>*Kolmogorov-Smirnov Test:</u>	
EIGEN--eigenvalues and eigenvectors of a symmetric matrix		<u>*KOLM--Sample Main Program</u>	433
Special sample subroutine is:		Illustrates use of:	
DATA--sample data read		*KOLMO--one-sample test	
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AVDAT--data storage allocation		<u>Triple Exponential Smoothing</u>	
AVCAL-- Σ and Δ operations		EXPON--Sample Main Program	439
MEANQ--mean square operation		Illustrates use of:	
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DMATX--means and dispersion matrix		Illustrates use of:	
MINV--matrix inversion		MADD--matrix add	
DISCR--discriminant functions		LOC--location in compressed-stored matrix	
<u>Factor Analysis</u>		Special sample subroutines are:	
FACTO--Sample Main Program	429	MATIN--matrix input	
Illustrates use of:		MXOUT--matrix output	
CORRE--means, standard deviations, and correlations		<u>Numerical Quadrature Integration</u>	
EIGEN--eigenvalues and eigenvectors of a real, symmetric matrix		QDINT--Sample Main Program	443
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VARMX--varimax rotation		<u>Runge-Kutta Integration</u>	
		RKINT--Sample Main Program	445

Illustrates use of:

RK2--Runge-Kutta integration

Special sample function is:

FUN--definition of differential equation

Polynomial Roots

SMPRT--Sample Main Program 447

Illustrates use of:

POLRT--real and complex roots of polynomial

Solution of Simultaneous Equations

SOLN--Sample Main Program 449

Illustrates use of:

SIMQ--solution of simultaneous equations

LOC--location in compressed-stored matrix

Special sample subroutines are:

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MXOUT--matrix output

Special Sample Subroutines

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FUN--definition of differential equation 452

HIST--histogram printing 452

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MXOUT--matrix output 454

*STOUT--stepwise regression output 454

ALPHABETIC GUIDE TO SUBROUTINES WITH STORAGE REQUIREMENTS

The following table lists the number of characters of storage required by each of the subroutines in

the Scientific Subroutine Package. The figures given were obtained by using Basic Programming Support FORTRAN (Tape), Version 3, Level 0. The use of other FORTRAN compilers on System/360 may cause deviations from these figures.

The double-precision version of the subroutines in the Scientific Subroutine Package are listed immediately following their alphabetized single-precision counterparts. Main line routines are asterisked.

Name	(Label)	Storage Required (Bytes)	Page
ABSNT	(ABSN)	428	28
ACFI	(ACFI)	1214	245
DACFI	(DACF)	1286	245
*ADSAM	(ADSA)	13244	443
AHI	(AHI)	1084	243
DAHI	(DAHI)	1116	243
ALI	(ALI)	760	241
DALI	(DALI)	784	241
*ANOVA	(ANOV)	14624	425
APCH	(APCH)	1492	263
DAPCH	(DAPC)	1548	263
APFS	(APFS)	1602	260
DAPFS	(DAPF)	1626	260
APLL	(APLL)	836	271
DAPLL	(DAPL)	860	271
APMM	(APMM)	4694	283
DAPMM	(DAPM)	4728	283
ARAT	(ARAT)	3004	265
DARAT	(DARA)	3090	265
ARRAY	(ARRA)	670	98
ATEIG	(ATEI)	4538	167

Name	(Label)	Storage Required (Bytes)	Page	Name	(Label)	Storage Required (Bytes)	Page
ATSE	(ATSE)	1022	251	CINT	(CINT)	364	109
DATSE	(DTSE)	1050	251	CNP	(CNP)	340	198
ATSG	(ATSG)	852	248	DCNP	(DNP)	364	198
DATSG	(DTSG)	892	248	CNPS	(CNPS)	442	199
ATSM	(ATSM)	1124	250	DCNPS	(DNPS)	482	199
DATSM	(DTSM)	1148	250	CONVT	(CONV)	538	97
AUTO	(AUTO)	624	59	CORRE	(CORR)	2950	32
AVCAL	(AVCA)	802	50	CROSS	(CROS)	750	60
AVDAT	(AVDA)	926	49	CS	(CS)	906	372
BDTR	(BDTR)	3354	78	CSP	(CSP)	352	201
				DCSP	(DSP)	376	201
BESJ	(BESJ)	1466	363	CSPS	(CSPS)	458	202
BESK	(BESK)	2022	366	DCSPS	(DSPS)	506	202
BESY	(BESY)	1968	364	CSRT	(CSRT)	978	113
BISER	(BISE)	1182	87	CSUM	(CSUM)	502	110
BOOL	(BOOL)	164	452	CTAB	(CTAB)	826	112
BOUND	(BOUN)	784	27	CTIE	(CTIE)	746	115
CADD	(CADD)	550	107	*DASCR	(DASC)	6848	403
CANOR	(CANO)	2836	47	DATA	(DATA)	308	452
CCPY	(CCPY)	500	95	DBAR	(DBAR)	1252	327
CCUT	(CCUT)	716	114	DDBAR	(DDBA)	1354	327
CDTR	(CDTR)	3390	81	DCAR	(DCAR)	1308	324
CEL1	(CEL1)	544	374	DDCAR	(DDCA)	1392	324
DCEL1	(DCE1)	584	374	DCLA	(DCLA)	392	106
CEL2	(CEL2)	718	376	DCPY	(DCPY)	394	95
DCEL2	(DCE2)	774	376	DET3	(DET3)	554	320
CHISQ	(CHIS)	1220	68	DDET3	(DDT3)	594	320

Name	(Label)	Storage Required (Bytes)	Page	Name	(Label)	Storage Required (Bytes)	Page
DET5	(DET5)	752	322	GDATA	(GDAT)	1764	39
DDET5	(DDT5)	832	322	GELB	(GELB)	2640	137
DGT3	(DGT3)	738	319	DGELB	(DELB)	2674	137
DDGT3	(DDGT)	770	319	GELG	(GELG)	1882	121
DISCR	(DISC)	2532	53	DGELG	(DELG)	1920	121
DLGAM	(DLGA)	826	362	GELS	(GELS)	1990	133
DMATX	(DMAT)	1170	52	DGELS	(DELS)	2028	133
EIGEN	(EIGE)	2556	164	GMADD	(GMAD)	288	98
ELI1	(ELI1)	836	378	GMMMA	(GMMM)	826	361
DELI1	(DEL1)	900	378	GMPRD	(GMPR)	570	99
ELI2	(ELI2)	1254	380	GMSUB	(GMSU)	288	99
DELI2	(DEL2)	1356	380	GMTRA	(GMTR)	358	100
EXPI	(EXPI)	1032	368	GTPRD	(GTPR)	566	100
*EXPON	(EXPO)	8952	440	HARM	(HARM)	5988	276
EXSMO	(EXSM)	620	62	DHARM	(DHAR)	6070	276
*FACTO	(FCTO)	11212	432	HEP	(HEP)	398	205
FACTR	(FCTR)	1586	126	DHEP	(DHP)	422	205
FMCG	(FMCG)	2820	225	HEPS	(HEPS)	454	206
DFMCG	(DFMC)	2956	225	DHEPS	(DHPS)	486	206
FMFP	(FMFP)	3580	221	HIST	(HIST)	1778	452
DFMFP	(DFMF)	3702	221	HPCG	(HPCG)	5560	337
FORIF	(FRIF)	990	274	DHPCG	(DHCG)	5744	337
FORIT	(FRIT)	946	275	HPCL	(HPCL)	5606	343
FRAT	(FRAT)	912	269	DHPCL	(DHCL)	5798	343
DFRAT	(DFRA)	944	271	HSBG	(HSBG)	1440	169
FUN	(FUN)	186	452	I0	(I0)	546	365
GAUSS	(GAUS)	430	77	INUE	(INUE)	768	366
				JELF	(JELF)	1254	382
				DJELF	(DJEL)	1416	382

Name	(Label)	Storage Required (Bytes)	Page	Name	(Label)	Storage Required (Bytes)	Page
*KOLM	(KOLM)	7952	438	MFGR	(MFGR)	2092	127
KOLMO	(KLMO)	1704	63	DMFGR	(DMGR)	2120	127
KOLM2	(KLM2)	1514	65	MFSD	(MFSD)	904	158
KRANK	(KRAN)	1598	69	DMFSD	(DMSD)	906	158
LAP	(LAP)	408	208	MFSS	(MFSS)	2688	152
DLAP	(DAP)	432	208	DMFSS	(DMSS)	2664	152
LAPS	(LAPS)	472	209	MFUN	(MFUN)	446	117
DLAPS	(DAPS)	512	209	MINV	(MINV)	1874	118
LBVP	(LBVP)	8000	350	MISR	(MISR)	2856	33
DLBVP	(DLBV)	8256	350	MLSS	(MLSS)	2020	145
LEP	(LEP)	400	212	DMLSS	(DMLS)	2004	145
DLEP	(DEP)	424	212	MOMEN	(MOME)	1288	85
LEPS	(LEPS)	464	213	MPAIR	(MPAI)	1380	70
DLEPS	(DEPS)	496	213	MPRC	(MPRC)	810	115
LLSQ	(LLSQ)	2938	160	DMPRC	(DMPR)	822	115
DLLSQ	(DLLS)	2986	160	MPRD	(MPRD)	944	102
LOAD	(LOAD)	490	56	MSTR	(MSTR)	590	96
LOC	(LOC)	492	97	MSUB	(MSUB)	942	101
MADD	(MADD)	942	101	MTDS	(MTDS)	1436	142
MATA	(MATA)	790	103	DMTDS	(DMTD)	1428	142
MATIN	(MATI)	1180	453	MTRA	(MTRA)	552	102
*MCANO	(MCAN)	8196	421	MULTR	(MULT)	1356	37
MCHB	(MCHB)	2286	148	MXOUT	(MXOU)	1440	454
DMCHB	(DMCH)	2270	148	NDTR	(NDTR)	488	78
MCPY	(MCPY)	410	94	NDTRI	(NTRI)	758	83
*MDISC	(MDIS)	15368	428	NROOT	(NROO)	1940	166
MEANQ	(MEAN)	1708	51	ORDER	(ORDE)	682	36

Name	(Label)	Storage Required (Bytes)	Page	Name	(Label)	Storage Required (Bytes)	Page
PADD	(PADD)	474	171	PROBT	(PROB)	2466	44
PADDM	(PDDM)	510	173	PRQD	(PRQD)	4572	183
PCLA	(PCLA)	282	173	DPRQD	(DPRQ)	4636	183
PCLD	(PCLD)	314	177	PSUB	(PSUB)	476	171
PDER	(PDER)	350	175	PVAL	(PVAL)	302	174
PDIV	(PDIV)	794	172	PVSUB	(PVSU)	714	174
PECN	(PECN)	848	178	QATR	(QATR)	1128	297
DPECN	(DPCN)	862	178	DQATR	(DQAT)	1190	297
PECS	(PECS)	746	180	QA2	(QA2)	330	314
DPECS	(DPCS)	766	180	QA3	(QA3)	376	314
PERM	(PERM)	1024	232	QA4	(QA4)	422	314
PGCD	(PGCD)	566	177	DQA4	(DQA4)	462	315
PHI	(PHI)	1390	88	QA5	(QA5)	468	315
PILD	(PILD)	402	175	QA6	(QA6)	514	315
PINT	(PINT)	344	176	QA7	(QA7)	560	315
PLOT	(PLOT)	2500	452	QA8	(QA8)	606	316
PMPY	(PMPY)	506	172	DQA8	(DQA8)	678	316
PNORM	(PNOR)	258	178	QA9	(QA9)	652	316
POINT	(POIN)	1144	89	QA10	(QA10)	698	316
*POLRG	(PLRG)	9282	411	DQA12	(DA12)	894	317
POLRT	(PLRT)	2086	181	DQA16	(DA16)	1110	317
PPRCN	(PPRC)	704	231	DQA24	(DA24)	1542	318
PQFB	(PQFB)	2252	193	DQA32	(DA32)	1974	318
DPQFB	(DPQF)	2384	193	*QDINT	(QDIN)	2916	445
PQSD	(PQSD)	382	176	QG2	(QG2)	442	299
PRBM	(PRBM)	2400	189	QG3	(QG3)	468	299
DPRBM	(DPRB)	2476	189	QG4	(QG4)	538	300

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DQG4	(DQG4)	598	300	DQH8	(DQH8)	622	310
QG5	(QG5)	576	300	QH9	(QH9)	616	310
QG6	(QG6)	638	300	QH10	(QH10)	652	310
QG7	(QG7)	676	301	DQH16	(DH16)	982	311
QG8	(QG8)	738	301	DQH24	(DH24)	1342	311
DQG8	(DQG8)	814	301	DQH32	(DH32)	1702	312
QG9	(QG9)	776	301	DQH48	(DH48)	2422	312
QG10	(QG10)	838	302	DQH64	(DH64)	3142	313
DQG12	(DG12)	1030	302	QL2	(QL2)	330	303
DQG16	(DG16)	1246	302	QL3	(QL3)	376	304
DQG24	(DG24)	1678	302	QL4	(QL4)	422	304
DQG32	(DG32)	2110	303	DQL4	(DQL4)	462	304
QHFE	(QHFE)	434	294	QL5	(QL5)	468	304
DQHFE	(DQHE)	482	294	QL6	(QL6)	514	305
QHFG	(QHFG)	414	293	QL7	(QL7)	560	305
DQHFG	(DQHG)	454	293	QL8	(QL8)	606	305
QHSE	(QHSE)	478	296	DQL8	(DQL8)	678	305
DQHSE	(DQHS)	542	296	QL9	(QL9)	652	306
QHSG	(QHSG)	462	295	QL10	(QL10)	698	306
DQHSG	(DHSG)	514	295	DQL12	(DL12)	894	306
QH2	(QH2)	324	308	DQL16	(DL16)	1110	306
QH3	(QH3)	370	308	DQL24	(DL24)	1542	307
QH4	(QH4)	406	309	DQL32	(DL32)	1974	307
QH5	(QH5)	452	309	QSF	(QSF)	1286	291
QH6	(QH6)	488	309	DQSF	(DQSF)	1358	291
QH7	(QH7)	534	309	QTEST	(QTES)	710	71
QH8	(QH8)	570	310	QTFE	(QTFE)	382	290

Name	(Label)	Storage Required (Bytes)	Page	Name	(Label)	Storage Required (Bytes)	Page
DQTFE	(DTFE)	422	290	RTWI	(RTWI)	770	215
QTFG	(QTFG)	370	289	DRTWI	(DRTW)	804	215
DQTFG	(DTFG)	402	289	SADD	(SADD)	434	104
RADD	(RADD)	538	107	SCLA	(SCLA)	420	106
RANDU	(RAND)	310	77	SCMA	(SCMA)	430	108
RANK	(RANK)	672	71	SDIV	(SDIV)	470	105
RCPY	(RCPY)	500	94	SE13	(SE13)	460	255
RCUT	(RCUT)	716	113	DSE13	(DE13)	500	255
RECP	(RECP)	224	117	SE15	(SE15)	588	256
*REGRE	(REGR)	13736	407	DSE15	(DE15)	620	256
RHARM	(RHAR)	1660	281	SE35	(SE35)	564	258
DRHARM	(DRAR)	1762	281	DSE35	(DSE3)	604	258
RINT	(RINT)	376	109	SG13	(SG13)	648	253
RKGS	(RKGS)	2878	333	DSG13	(DSG1)	696	253
DRKGS	(DRKG)	3018	333	SICI	(SICI)	1192	370
*RKINT	(RKIN)	2704	446	SIGNT	(SIGN)	1170	72
RK1	(RK1)	1420	331	SIMQ	(SIMQ)	1286	120
RK2	(RK2)	770	332	SINV	(SINV)	1092	119
RSLMC	(RSLM)	1830	124	DSINV	(DSIN)	1080	119
RSRT	(RSRT)	1034	112	SMIRN	(SMIR)	700	66
RSUM	(RSUM)	502	110	SMO	(SMO)	542	61
RTAB	(RTAB)	826	111	*SMPRT	(SMPR)	1792	449
RTIE	(RTIE)	778	114	SMPY	(SMPY)	434	105
RTMI	(RTMI)	1510	217	*SOLN	(SOLN)	11754	451
DRTMI	(DRTM)	1582	217	SRANK	(SRAN)	1260	73
RTNI	(RTNI)	724	220	SRATE	(SRAT)	1534	92
DRTNI	(DRTN)	770	220	SRMA	(SRMA)	442	108

Name	(Label)	Storage Required (Bytes)	Page	Name	(Label)	Storage Required (Bytes)	Page
SSUB	(SSUB)	434	104	DTEUL	(DTEU)	924	238
*STEPR	(STEP)	11584	417	THEP	(THEP)	712	207
STOUT	(STOU)	1684	454	DTHEP	(DTHE)	768	207
STPRG	(STPR)	3200	41	TIE	(TIE)	640	74
SUBMX	(SUBM)	512	31	TLAP	(TLAP)	776	210
SUBST	(SUBS)	888	28	DTLAP	(DTLA)	820	210
TAB1	(TAB1)	1636	29	TLEP	(TLEP)	716	214
TAB2	(TAB2)	2806	30	DTLEP	(DTLE)	772	214
TALLY	(TALL)	1206	27	TPRD	(TPRD)	904	103
TCNP	(TCNP)	678	200	TRACE	(TRAC)	560	55
DTCNP	(DTCN)	726	200	TTEST	(TTES)	1794	86
TCSP	(TCSP)	706	203	TWOAV	(TWOA)	1108	74
DTCSP	(DTCS)	754	203	UTEST	(UTES)	1064	75
TEAS	(TEAS)	2024	234	VARMX	(VARM)	2914	56
DTEAS	(DTEA)	2096	234	WTEST	(WTES)	1488	76
TETRA	(TETR)	2038	90	XCPY	(XCPY)	670	96
TEUL	(TEUL)	844	238				

SUBROUTINE DESCRIPTIONS AND LISTINGS

Listed below are the subroutines. A brief description precedes those subroutines that require further clarification.

STATISTICS

Data Screening

Subroutine TALLY

```

C ..... TALL 10
C ..... TALL 20
C ..... TALL 30
C ..... TALL 40
C ..... TALL 50
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C ..... TALL 940
C ..... TALL 950
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C ..... TALL 970
C ..... TALL 980
C ..... TALL 990
C ..... TALL 1000

```

Subroutine BOUND

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C ..... ROUN 10
C ..... ROUN 20
C ..... ROUN 30
C ..... ROUN 40
C ..... ROUN 50
C ..... ROUN 60
C ..... ROUN 70
C ..... ROUN 80
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C ..... ROUN 770
C ..... ROUN 780
C ..... ROUN 790
C ..... ROUN 800
C ..... ROUN 810
C ..... ROUN 820

```

Subroutine SUBST

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C ..... SUBS 10
C ..... SUBS 20
C ..... SUBS 30
C ..... SUBS 40
C ..... SUBS 50
C ..... SUBS 60
C ..... SUBS 70
C ..... SUBS 80
C ..... SUBS 90
C ..... SUBS 100
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C ..... SUBS 980
C ..... SUBS 990
C ..... SUBS1000
C ..... SUBS1010
C ..... SUBS1020
C ..... SUBS1030
C ..... SUBS1040
C ..... SUBS1050
C ..... SUBS1060
C ..... SUBS1070
C ..... SUBS1080
C ..... SUBS1090
C ..... SUBS1100
C ..... SUBS1110
C ..... SUBS1120
C ..... SUBS1130
C ..... SUBS1140
C ..... SUBS1150
C ..... SUBS1160
C ..... SUBS1170

```

Subroutine ABSNT

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C ..... ABSN 10
C ..... ABSN 20
C ..... ABSN 30
C ..... ABSN 40
C ..... ABSN 50
C ..... ABSN 60
C ..... ABSN 70
C ..... ABSN 80
C ..... ABSN 90
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C ..... ABSN 130
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C ..... ABSN 410
C ..... ABSN 420
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C ..... ABSN 440
C ..... ABSN 450
C ..... ABSN 460
C ..... ABSN 470
C ..... ABSN 480
C ..... ABSN 490
C ..... ABSN 500

```


Subroutine TAB1

This subroutine tabulates, for a selected variable in an observation matrix, the frequencies and percent frequencies over class intervals. Interval size is computed as follows:

$$k = \frac{UBO_3 - UBO_1}{UBO_2 - 2} \quad (1)$$

- where UBO_1 = given lower bound
- UBO_2 = given number of intervals
- UBO_3 = given upper bound

If $UBO_1 = UBO_3$, the subroutine finds and uses the minimum and maximum values of the variable.

A table lookup is used to obtain the frequency of the i^{th} class interval for the variable, where $i = 1, 2, \dots, UBO_2$. Then each frequency is divided by the number of observations, n , to obtain the percent frequency:

$$P_i = \frac{100F_i}{n} \quad (2)$$

In addition, the following statistics are calculated for the variable:

$$\text{Total: } T = \sum_{i=1}^n X_{ij} \quad (3)$$

where j = selected variable

$$\text{Mean: } \bar{X} = \frac{T}{n} \quad (4)$$

Standard deviation:

$$s = \sqrt{\frac{\sum_{i=1}^n X_{ij}^2 - \left(\sum_{i=1}^n X_{ij}\right)^2 / n}{n - 1}} \quad (5)$$

C		TAB1 10
C	-----	TAB1 20
C		TAB1 30
C		TAB1 40
C	SLRCLTNE TAB1	TAB1 50
C		TAB1 60
C	FLRPFCE	TAB1 70
C	TABULATE FOR ONE VARIABLE IN AN OBSERVATION MATRIX (OR A	TAB1 80
C	MATRIX SUBSET), THE FREQUENCY AND PERCENT FREQUENCY OVER	TAB1 90
C	GIVEN CLASS INTERVALS. IN ADDITION, CALCULATE FOR THE SAME	TAB1 100
C	VARIABLE THE TOTAL, AVERAGE, STANDARD DEVIATION, MINIMUM,	TAB1 110
C	AND MAXIMUM.	TAB1 120
C		TAB1 130
C	LSAGE	TAB1 140
C	CALL TAB1(A,S,NOVAR,UBC,FREQ,PCT,STATS,NO,NV)	TAB1 150
C		TAB1 160
C	DESCRIPTION OF PARAMETERS	TAB1 170
C	A - OBSERVATION MATRIX, NO BY NV	TAB1 180
C	S - INPUT VECTOR GIVING SUBSET OF A. ONLY THOSE	TAB1 190
C	OBSERVATIONS WITH A CORRESPONDING NON-ZERO S(I) ARE	TAB1 200
C	CONSIDERED. VECTOR LENGTH IS NO.	TAB1 210
C	NOVAR - THE VARIABLE TO BE TABULATED. NOVAR MUST BE GREATER	TAB1 220
C	THAN CR EQUAL TO 1 AND LESS THAN OR EQUAL TO NV.	TAB1 230
C	AND UPPER LIMIT OF VARIABLE TO BE TABULATED	TAB1 240
C	IN UBC(1), UBC(2) AND UBC(3) RESPECTIVELY. IF	TAB1 250
C	LOWER LIMIT IS EQUAL TO UPPER LIMIT, THE PROGRAM	TAB1 260
C	USES THE MINIMUM AND MAXIMUM VALUES OF THE VARIABLE.	TAB1 270
C	NUMBER OF INTERVALS. UBC(2), MUST INCLUDE TWO CELLS	TAB1 280
C	FOR VALUES UNDER AND ABOVE LIMITS. VECTOR LENGTH	TAB1 290
C	IS 3.	

```

C      FREQ - OUTPUT VECTOR OF FREQUENCIES. VECTOR LENGTH IS 300     TAB1 300
C      UBC(2).                                                         TAB1 310
C      PCT - OUTPUT VECTOR OF RELATIVE FREQUENCIES. VECTOR           TAB1 320
C      LENGTH IS UBC(2).                                             TAB1 330
C      STATS - OUTPUT VECTOR OF SUMMARY STATISTICS, I.E., TOTAL,    TAB1 340
C      AVERAGE, STANDARD DEVIATION, MINIMUM AND MAXIMUM.          TAB1 350
C      VECTOR LENGTH IS 5. IF S IS NULL, THEN TOTAL,AVERAGE,TAB1 360
C      AND STANDARD DEVIATION = 0, MIN=1.E75 AND MAX=-1.E75,TAB1 361
C      NV - NUMBER OF OBSERVATIONS. NV MUST BE > CR = TO 1        TAB1 370
C      NC - NUMBER OF VARIABLES FOR EACH OBSERVATION. NV MUST    TAB1 380
C      BE GREATER THAN CR EQUAL TO 1.                               TAB1 381
C      REMARKS                                                         TAB1 390
C      NCAE                                                           TAB1 400
C      SLRCLTINES AND FLACION SUBPROGRAMS REQUIRED                    TAB1 410
C      AFRE                                                           TAB1 420
C      METPCE                                                         TAB1 430
C      THE INTERVAL SIZE IS CALCULATED FROM THE GIVEN INFORMATION  TAB1 440
C      CR OPTICALLY FROM THE MINIMUM AND MAXIMUM VALUES FOR     TAB1 450
C      VARIABLE NOVAR. THE FREQUENCIES AND PERCENT FREQUENCIES ARE  TAB1 460
C      THEN CALCULATED ALONG WITH SUMMARY STATISTICS.            TAB1 470
C      THE DIVISOR FOR STANDARD DEVIATION IS ONE LESS THAN THE    TAB1 480
C      NUMBER OF OBSERVATIONS USED.                                  TAB1 490
C      -----
C      SLRCLTNE TAB1(A,S,NOVAR,UBC,FREQ,PCT,STATS,NC,NV)          TAB1 500
C      DIMENSION A(1),S(1),UBC(1),FREQ(1),PCT(1),STATS(1)         TAB1 510
C      DIMENSION WEC(1)                                             TAB1 520
C      CC 5 I=1,2                                                    TAB1 530
C      5 WEC(I)=UBC(I)                                              TAB1 540
C      CALCULATE MIN AND MAX                                         TAB1 550
C      VMIN=1.CE75                                                  TAB1 560
C      VMAX=-1.CE75                                                TAB1 600
C      IJ=NCR(INCVAR-1)                                            TAB1 610
C      CC 3C J=1,AC                                                TAB1 620
C      IJ=IJ+1                                                      TAB1 630
C      IF(S(I)) IC,3C,1C                                           TAB1 640
C      1C IF(A(IJ)-VMIN) 15,2C,2C                                  TAB1 650
C      15 VMIN=A(IJ)                                               TAB1 660
C      2C IF(A(IJ)-VMAX) 3C,3C,25                                  TAB1 670
C      25 VMAX=A(IJ)                                               TAB1 680
C      3C CONTINUE                                                TAB1 690
C      STATS(4)=VMIN                                              TAB1 700
C      STATS(5)=VMAX                                              TAB1 710
C      DETERMINE LIMITS                                           TAB1 720
C      IF(LBC(1)-UBC(3)) 4C,35,4C                                  TAB1 730
C      35 LBC(1)=VMIN                                             TAB1 740
C      LBC(3)=VMAX                                                 TAB1 750
C      4C IAN=LBC(2)                                              TAB1 760
C      CLEAR OUTPUT AREAS                                          TAB1 770
C      CC 45 I=1,IAN                                               TAB1 780
C      FREQ(I)=C,C                                                 TAB1 790
C      45 PCT(I)=C,C                                               TAB1 800
C      CC 5C I=1,2                                                TAB1 810
C      5C STATS(I)=C,C                                             TAB1 820
C      CALCULATE INTERVAL SIZE                                       TAB1 830
C      SINT=ABS(LBC(3)-UBC(1))/(UBC(2)-2.0)                       TAB1 840
C      TEST SUBSET VECTOR                                           TAB1 850
C      SCAT=C,C                                                    TAB1 860
C      IJ=NCR(INCVAR-1)                                            TAB1 870
C      CC 75 J=1,AC                                               TAB1 880
C      IJ=IJ+1                                                      TAB1 890
C      IF(S(I)) 55,75,55                                          TAB1 900
C      55 SCAT=SCAT+1.C                                             TAB1 910
C      DEVELOP TOTAL AND FREQUENCIES                                TAB1 920
C      STATS(1)=STATS(1)+A(IJ)                                     TAB1 930
C      STATS(3)=STATS(3)+A(IJ)*A(IJ)                              TAB1 940
C      TEPP=LBC(1)-SINT                                           TAB1 950
C      IATX=IAN-1                                                  TAB1 960
C      CC 60 I=1,IATX                                             TAB1 970
C      TEPP=TEPP+SINT                                             TAB1 980
C      IF(A(IJ)-TEPP) 7C,6C,60                                     TAB1 990
C      6C CONTINUE                                                TAB11000
C      65 FREQ(IAN)=FREQ(IAN)+1.0                                  TAB11010
C      CC TC 75                                                 TAB11020
C      7C FREQ(IJ)=FREQ(IJ)+1.C                                   TAB11030
C      75 CONTINUE                                                TAB11040
C      IF (SCAT)75,1C5,75                                         TAB11050
C      CALCULATE RELATIVE FREQUENCIES                               TAB11060
C      75 CC EC I=1,IAN                                           TAB11070
C      8C PCT(I)=FREQ(I)*100./SCAT                                 TAB11080
C      CALCULATE MEAN AND STANCARD DEVIATION                        TAB11090
C      IF(SCAT-1.0) 85,65,5C                                       TAB11100
C      85 STATS(2)=STATS(1)                                       TAB11110
C      STATS(3)=C,C                                               TAB11120
C      CC TC 55                                                 TAB11130
C      9C STATS(2)=STATS(1)/SCAT                                   TAB11140
C      STATS(3)=SQRT(ABS((STATS(3)-STATS(1)*STATS(1)/SCAT)/(SCAT-1.0)))  TAB11150
C      95 CC ICC I=1,3                                           TAB11160
C      1CC LBC(I)=WEC(I)                                           TAB11170
C      105 RETURN                                                 TAB11180
C      ENCL                                                         TAB11190

```

Subroutine TAB2

This subroutine performs a two-way classification of the frequency, percent frequency, and other statistics over given class intervals, for two selected variables in an observation matrix.

Interval size for each variable is computed as follows:

$$k_j = \frac{UBO_{3j} - UBO_{1j}}{UBO_{2j} - 2} \quad (1)$$

where UBO_{1j} = given lower bound
 UBO_{2j} = given number of intervals
 UBO_{3j} = given upper bound
 $j = 1, 2$

If $UBO_{1j} = UBO_{3j}$, the subroutine finds and uses the minimum and maximum values of the j^{th} variable.

A frequency tabulation is then made for each pair of observations in a two-way table as shown in Figure 6.

Symbols \geq and $<$ in Figure 6 indicate that a count is classified into a particular interval if the data point is greater than or equal to the lower limit of that interval but less than the upper limit of the same interval.

Then, each entry in the frequency matrix, F_{ij} , is divided by the number of observations, N , to obtain the percent frequency:

$$P_{ij} = \frac{100F_{ij}}{N} \quad (2)$$

where $i = 1, 2, \dots, UBO_{21}$
 $j = 1, 2, \dots, UBO_{22}$

As data are classified into the frequency matrix, the following intermediate results are accumulated for each class interval of both variables:

1. Number of data points, n
2. Sum of data points, $\sum_{i=1}^n X_i$
3. Sum of data points squared, $\sum_{i=1}^n X_i^2$

From these, the following statistics are calculated for each class interval:

$$\text{Mean: } \bar{X} = \frac{\sum_{i=1}^n X_i}{n} \quad (3)$$

Standard deviation:

$$s = \sqrt{\frac{\sum_{i=1}^n X_i^2 - \left(\sum_{i=1}^n X_i\right)^2 / n}{n - 1}} \quad (4)$$

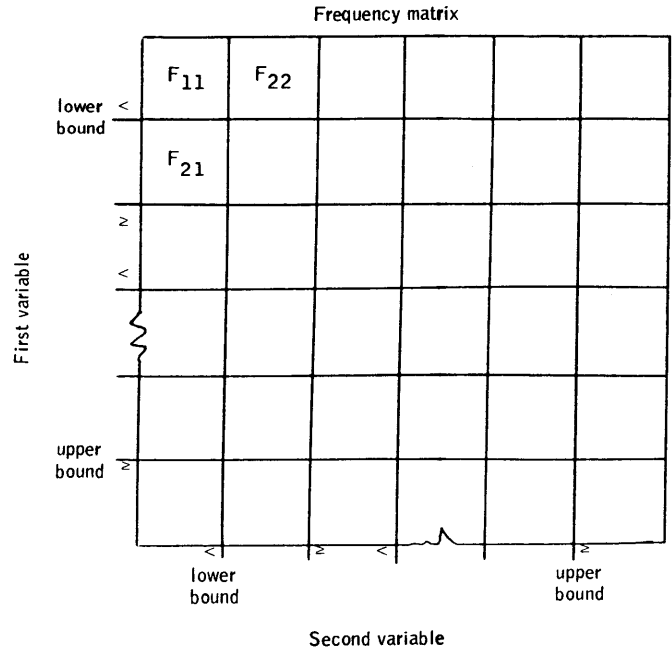


Figure 6. Frequency matrix

```

C
C ..... TAB2 10
C ..... TAB2 20
C ..... TAB2 30
C ..... TAB2 40
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C ..... TAB2 180
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C ..... TAB2 200
C ..... TAB2 210
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C ..... TAB2 220
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C ..... TAB2 290
C ..... TAB2 300
C ..... TAB2 310
C ..... TAB2 320
C ..... TAB2 330
C ..... TAB2 340
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C ..... TAB2 360
C ..... TAB2 370
C ..... TAB2 380
C ..... TAB2 390
C ..... TAB2 400
C ..... TAB2 410
C ..... TAB2 420
C ..... TAB2 430
C ..... TAB2 431
C ..... TAB2 440
C ..... TAB2 441
C ..... TAB2 450
C ..... TAB2 460
C ..... TAB2 470
C ..... TAB2 480
C ..... TAB2 490
C ..... TAB2 500
C ..... TAB2 510
C ..... TAB2 520
C ..... TAB2 530
C ..... TAB2 540
C ..... TAB2 550
C ..... TAB2 560
C ..... TAB2 570
C ..... TAB2 580
C ..... TAB2 590
C ..... TAB2 600
C ..... TAB2 610
C ..... TAB2 620
C ..... TAB2 630
C ..... TAB2 640
C ..... TAB2 650
C ..... TAB2 660
C ..... TAB2 670
C ..... TAB2 680
C ..... TAB2 690
C ..... TAB2 700
C ..... TAB2 710
C ..... TAB2 720
C ..... TAB2 730
C ..... TAB2 740
C ..... TAB2 750
C ..... TAB2 760
C ..... TAB2 770
C ..... TAB2 780
C ..... TAB2 790
C ..... TAB2 800
C ..... TAB2 810
C ..... TAB2 820
C ..... TAB2 830
C ..... TAB2 840
C ..... TAB2 850
C ..... TAB2 860
C ..... TAB2 870
C ..... TAB2 880
C ..... TAB2 890
C ..... TAB2 900
C ..... TAB2 910
C ..... TAB2 920
C ..... TAB2 930
C ..... TAB2 940
C ..... TAB2 950
C ..... TAB2 960
C ..... TAB2 970
C ..... TAB2 980
C ..... TAB2 990
C ..... TAB2 1000

```

```

C VALLES. THE FREQUENCY AND PERCENT FREQUENCY MATRICES ARE
C DEVELOPED. MATRICES STAT1 AND STAT2 SUMMARIZING TOTALS,
C MEANS, AND STANDARD DEVIATIONS ARE THEN CALCULATED.
C THE DIVISOR FOR STANDARD DEVIATION IS ONE LESS THAN THE
C NUMBER OF OBSERVATIONS USED IN EACH CLASS INTERVAL.
C
C .....
C SLRCLTINE TAB2(A,S,NOV,LOC,FREQ,PCT,STAT1,STAT2,NC,NV)
C DIMENSION A(1),S(1),NOV(2),UBC(3,2),FREQ(1),PCT(1),STAT1(1),
C STAT2(2),SINT(2)
C DIMENSION NRC(3,2)
C DO 3 I=1,3
C DO 5 J=1,2
C 5 NRC(I,J)=UBC(I,J)
C
C DETERMINE LIMITS
C
C CC 4C I=1,2
C IF(UBC(1,1)-UBC(3,1)) 4C, 1C, 4C
C 1C VPIA=1,CE75
C VPAK=-1,CE75
C IJ=NO(INCV(1)-1)
C CC 35 J=1,NC
C IJ=I+J
C IF(S(I)) 15,35,15
C 15 IF(I(1J)-VPIA) 2C,25,25
C 2C VPIA=A(IJ)
C 25 IF(A(IJ)-VPAK) 35,35,3C
C 3C VPAK=A(IJ)
C 35 CCNTLINE
C UBC(1,1)=VPIA
C UBC(3,1)=VPAK
C 4C CCNTLINE
C
C CALCULATE INTERVAL SIZE
C
C 45 CC 5C I=1,2
C 5C SINT(1)=#5((UBC(3,1)-UBC(1,1))/(UBC(2,1)-2,C))
C
C CLEAR OUTPUT AREAS
C
C INT1=UBC(2,1)
C INT2=UBC(2,2)
C INT1=INT1+INT2
C CC 55 I=1,INT1
C FREQ(I)=C,C
C 55 FCT(I)=C,C
C INTY=0,INT1
C CC 6C I=1,INTY
C 6C STAT1(I)=C,C
C INTZ=0,INT2
C CC 65 I=1,INTZ
C 65 STAT2(I)=C,C
C
C TEST SUBSET VECTOR
C
C SCAT=C,C
C INTY=INT1-1
C INTX=INT2-1
C IJ=NO(INCV(1)-1)
C IJ=NO(INCV(2)-1)
C CC 55 J=1,NC
C IJ=I+J
C IJX=IJ+1
C IF(S(IJ)) 7C,55,7C
C 7C SCAT=SCAT+1,C
C
C CALCULATE FREQUENCIES
C
C TEMP1=UBC(1,1)-SINT(1)
C CC 75 IY=1,INTY
C TEMP1=TEMP1+SINT(1)
C IF(A(IJ)-TEMP1) 8C,75,75
C 75 CCNTLINE
C IY=INT1
C 8C STAT1(IY)=STAT1(IY)+A(IJ)
C IY=IY+1
C STAT1(IY)=STAT1(IY)+1,C
C IY=IY+1
C STAT1(IY)=STAT1(IY)+A(IJ)+A(IJ)
C TEMP2=UBC(1,2)-SINT(2)
C CC 85 IZ=1,INTZ
C TEMP2=TEMP2+SINT(2)
C IF(A(IJX)-TEMP2) 9C,85,85
C 85 CCNTLINE
C IZ=INT2
C 9C IJF=INT1+(IZ-1)+IY
C FREQ(IJF)=FREQ(IJF)+1,C
C IZ=IZ+1
C STAT2(IZ)=STAT2(IZ)+A(IJX)
C IZ=IZ+1
C STAT2(IZ)=STAT2(IZ)+1,C
C IZ=IZ+1
C STAT2(IZ)=STAT2(IZ)+A(IJX)+A(IJX)
C 95 CCNTLINE
C IF(1SCAT)50,151,68
C
C CALCULATE PERCENT FREQUENCIES
C
C 95 CC 10C I=1,INT1
C 10C FCT(I)=FREQ(I)*100,C/SCAT
C
C CALCULATE TOTALS, MEANS, STANDARD DEVIATIONS
C
C IXX=1
C CC 12C I=1,INT1
C IXX=IXX+2
C ISC=IXX+1
C TEMP1=STAT1(IXX)
C SLP=STAT1(IXX-1)
C IF(TEMP1-1,C) 12C,1C5,11C
C 1C5 STAT1(ISC)=C,C
C CC TC 115
C 115 STAT1(ISC)=SLP+ABS((STAT1(ISC)-SLP)*SUM/TEMP1)/(TEMP1-1,C)
C 11C STAT1(IXX)=SUM/TEMP1
C 12C CCNTLINE
C IXX=1
C CC 14C I=1,INT2
C IXX=IXX+2
C ISC=IXX+1
C TEMP2=STAT2(IXX)
C SLP=STAT2(IXX-1)
C IF(TEMP2-1,C) 14C,125,13C
C 125 STAT2(ISC)=C,C
C CC TC 135
C 13C STAT2(ISC)=SCH1+ABS((STAT2(ISC)-SUM*SLP/TEMP2)/(TEMP2-1,C))
C 135 STAT2(IXX)=SLP/TEMP2

```

TAB2 550
TAB2 560
TAB2 570
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TAB21120
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TAB21190
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TAB21600
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TAB21750
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TAB21770
TAB21780
TAB21790
TAB21800
TAB21810
TAB21820

```

14C CCNTLINE
CC 15C I=1,3
CC 15C J=1,2
15C UBC(I,J)=UBC(I,J)
151 RETLRA
EAC
TAB21830
TAB21840
TAB21850
TAB21860
TAB21870
TAB21880

Subroutine SUBMX

SUBM 10
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SUBM 550
SUBM 560
SUBM 570
SUBM 580
SUBM 590
SUBM 600
SUBM 610
SUBM 620

C .....
C SLRCLTINE SLEPM
C
C PLRFRCE
C BASEL CA VECTOR S DERIVED FROM SUBRCLTINE SUBST OR ABSNT.
C THIS SUBROUTINE COPIES FROM A LARGER MATRIX OF OBSERVATION
C DATA A SUBSET MATRIX OF THESE OBSERVATIONS WHICH HAVE
C SATISFIED CERTAIN CONDITIONS. THIS SUBROUTINE IS NORMALLY
C USED PRIOR TO STATISTICAL ANALYSES (E.G., MULTIPLE REGRES-
C SION, FACTOR ANALYSIS).
C
C LSABE
C CALL SLEPM (A,C,S,NO,NV,N)
C
C DESCRIPTION OF PARAMETERS
C A - INPLT MATRIX OF OBSERVATIONS, NG BY NV.
C L - OUTPLT MATRIX OF OBSERVATIONS, N BY NV.
C S - INPLT VECTOR OF LENGTH NG CONTAINING THE CODES DERIVED
C FROM SUBRCLTINE SLEST OR ABSNT.
C AC - NUMBER OF OBSERVATIONS. AC MUST BE > OR = TO L.
C NV - NUMBER OF VARIABLES. NV MUST BE > OR = TO 1.
C N - OUTPLT VARIABLE CONTAINING THE NUMBER OF NON-ZERO CODES IN
C VECTOR S.
C
C REMARKS
C MATRIX C CAN BE IN THE SAME LOCATION AS MATRIX A.
C
C SLRCLTINES AND FUNCTION SLEPFRCGRAMS REQUIRED
C NONE
C
C PETHCC
C IF S(1) CONTAINS A NON-ZERO CODE, 1-TH OBSERVATION IS
C COPIED FROM THE INPUT MATRIX TO THE OUTPUT MATRIX.
C
C .....
C SLRCLTINE SLEPM (A,C,S,NO,NV,N)
C DIMENSION A(1),C(1),S(1)
C
C L=C
C LL=C
C CC 2C J=1,NV
C CC 15 I=1,NC
C L=L+1
C IF(S(1)) 15, 15, 1C
C 1C LL=LL+1
C 15 CCNTLINE
C 2C CCNTLINE
C
C CCLAT NON-ZERO CODES IN VECTOR S
C
C A=C
C CC 3C I=1,AC
C IF(S(I)) 3C, 3C, 25
C 25 A=A+1
C 3C CCNTLINE
C
C RETLRA
C EAC
SUBM 620

```

Correlation and Regression (see Smoothing, Factorization)

Subroutine CORRE

This subroutine calculates means, standard deviations, sums of cross-products of deviations from means, and product moment correlation coefficients from input data X_{ij} , where $i = 1, 2, \dots, n$ implies observations and $j = 1, 2, \dots, m$ implies variables.

The following equations are used to calculate these statistics.

Sums of cross-products of deviations:

$$S_{jk} = \sum_{i=1}^n (X_{ij} - T_j) (X_{ik} - T_k) - \frac{\sum_{i=1}^n (X_{ij} - T_j) \sum_{i=1}^n (X_{ik} - T_k)}{n} \quad (1)$$

where $j = 1, 2, \dots, m; k = 1, 2, \dots, m$

$$T_j = \frac{\sum_{i=1}^m X_{ij}}{m} \quad (2)$$

(These temporary means T_j are subtracted from the data in equation (1) to obtain computational accuracy.)

Means: $\bar{X}_j = \frac{\sum_{i=1}^n X_{ij}}{n} \quad (3)$

where $j = 1, 2, \dots, m$

Correlation coefficients:

$$r_{jk} = \frac{S_{jk}}{\sqrt{S_{jj}} \sqrt{S_{kk}}} \quad (4)$$

where $j = 1, 2, \dots, m; k = 1, 2, \dots, m$

Standard deviations:

$$s_j = \frac{\sqrt{S_{jj}}}{\sqrt{n-1}} \quad (5)$$

where $j = 1, 2, \dots, m$

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CORR 10
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CORR 950
CORR 960
CORR 970
CORR 980
CORR 990
CORR1000
CORR1010
CORR1020
CORR1030
CORR1040
CORR1050
CORR1060
CORR1070
CORR1080
CORR1090
CORR1100
CORR1110
CORR1120
CORR1130
CORR1140
CORR1150
CORR1160
CORR1170
CORR1180
CORR1190
CORR1200
CORR1210
CORR1220
CORR1230
CORR1240
CORR1250
CORR1260
CORR1270
CORR1280
CORR1290
CORR1300
CORR1310

```

```

C      CALCULATE SUMS OF CROSS-PRODUCTS OF DEVIATIONS
C      FROM TEMPORARY MEANS FOR M OBSERVATIONS
C
L=C
CC 18C I=1, KK
JK=C
CC 17C J=1, P
L=L+1
17C E(I)=R(I)-T(I)
CC 18C J=1, P
E(J)=E(I)+C(I)
CC 18C K=1, J
JK=JK+1
18C R(IJK)=R(IJK)+C(I)*D(K)
C
IF(A-KK) 205, 205, 165
C
READ THE REST OF OBSERVATIONS ONE AT A TIME, SUM
C THE OBSERVATION, AND CALCULATE SUMS OF CROSS-
C PRODUCTS OF DEVIATIONS FROM TEMPORARY MEANS
C
185 K=K+KK
CC 20C I=1, KK
JK=C
CALL DATA (P,C)
CC 19C J=1, P
XEAR(J)=XEAR(J)+C(I)
E(I)=E(I)-T(I)
19C E(J)=E(I)+C(I)
CC 20C J=1, P
CC 20C K=1, J
JK=JK+1
20C R(IJK)=R(IJK)+C(I)*D(K)
C
CALCULATE MEANS
C
205 JK=C
CC 21C J=1, P
XEAR(J)=XEAR(J)/FA
C
ADJUST SUMS OF CROSS-PRODUCTS OF DEVIATIONS
C FROM TEMPORARY MEANS
C
CC 21C K=1, J
JK=JK+1
21C R(IJK)=R(IJK)-E(I)*R(K)/FA
C
CALCULATE CORRELATION COEFFICIENTS
C
JK=C
CC 22C J=1, P
JK=JK+J
22C STC(I)=SQRT(AES(R(IJK)))
CC 23C J=1, P
CC 23C K=J, P
JK=J+(K-K)/2
L=PP+(J-1)*K
R(I)=R(IJK)
L=PP+(K-1)*J
R(L)=R(IJK)
IF(STC(I)*STC(L)) 225, 222, 225
222 R(IJK)=C,C
CC 7C 22C
225 R(IJK)=R(IJK)/(STC(I)*STC(L))
22C CCATINLE
C
CALCULATE STANDARD DEVIATIONS
C
FA=SQRT(FA-1,C)
CC 24C J=1, P
24C STC(I)=STC(I)/FA
C
COPY THE DIAGONAL OF THE MATRIX OF SUMS OF CROSS-PRODUCTS OF
C DEVIATIONS FROM MEANS.
C
L=-P
CC 25C I=1, P
L=L+P+1
25C R(I)=R(I)
RETURN
END

```

```

CCRR1320
CCRR1330
CCRR1340
CCRR1350
CCRR1360
CCRR1370
CCRR1380
CCRR1390
CCRR1400
CCRR1410
CCRR1420
CCRR1430
CCRR1440
CCRR1450
CCRR1460
CCRR1470
CCRR1480
CCRR1490
CCRR1500
CCRR1510
CCRR1520
CCRR1530
CCRR1540
CCRR1550
CCRR1560
CCRR1570
CCRR1580
CCRR1590
CCRR1600
CCRR1610
CCRR1620
CCRR1630
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CCRR1670
CCRR1680
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CCRR1790
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CCRR1910
CCRR1920
CCRR1930
CCRR1940
CCRR1950
CCRR1960
CCRR1970
CCRR1980
CCRR1990
CCRR2000
CCRR2010
CCRR2020
CCRR2030
CCRR2040
CCRR2050
CCRR2060
CCRR2070
CCRR2080
CCRR2090
CCRR2100
CCRR2110
CCRR2120
CCRR2130

```

Subroutine MISR

This subroutine computes means, standard deviations, third and fourth moments, correlation coefficients, third and fourth moments, regression coefficients, and standard errors of regression coefficients when there is missing data. Effective sample sizes are also provided. Missing observations or certain values of the data can be skipped at the user's option. The computational steps are as follows:

1. Compute means:

$$\bar{x}_j = \frac{\sum_{\alpha=1}^n x_{\alpha j}}{n} \tag{1}$$

where $j = 1, 2, \dots, m$ implies variables
 n = number of nonmissing values for the j th variable

2. Compute sums of cross-products of deviations from means for complete sets of i th and j th variables:

$$S_{ij} = \sum_{\alpha=1}^{n'} (x_{\alpha i} - \bar{x}_i) (x_{\alpha j} - \bar{x}_j) - \frac{\sum_{\alpha=1}^{n'} (x_{\alpha i} - \bar{x}_i) \sum_{\alpha=1}^{n'} (x_{\alpha j} - \bar{x}_j)}{n'} \tag{2}$$

where \bar{x}_i, \bar{x}_j = means of i th and j th variables computed as above
 n' = number of sets where the i th and j th variables are both present

3. Compute product-moment correlations:

$$r_{ij} = \frac{S_{ij}}{\sqrt{S_{ii}} \sqrt{S_{jj}}} \tag{3}$$

4. Compute regression coefficients, intercepts, and standard errors of regression coefficients:

- a. i th variable as independent and j th variable as dependent:

$$\text{Regression coefficient: } b_{ij} = \frac{S_{ij}}{S_{ii}} \tag{4}$$

$$\text{Intercept: } a_{ij} = \bar{x}_j' - b_{ij} \bar{x}_i' \tag{5}$$

Standard error regression coefficient:

$$s_{b_{ij}} = \frac{S_{jj} - r_{ij}^2 S_{jj}}{(n' - 2) S_{ii}} \quad (6)$$

b. jth variable as independent and ith variable as dependent:

$$\text{Regression coefficient: } b_{ji} = \frac{S_{ij}}{S_{jj}} \quad (7)$$

$$\text{Intercept: } a_{ji} = \bar{x}_i' - b_{ji} \bar{x}_j' \quad (8)$$

Standard error of regression coefficient:

$$s_{b_{ji}} = \frac{S_{ii} - r_{ij}^2 S_{ii}}{(n' - 2) S_{jj}} \quad (9)$$

5. Compute standard deviations:

$$s_j = \sqrt{\frac{S_{jj}}{n - 1}} \quad (10)$$

where n = number of nonmissing values for jth variable

6. Compute skewness and kurtosis, s and k:

$$\text{Let } \mu_{ij} = \sum_{\alpha=1}^n (x_{\alpha j} - \bar{x}_j)^i / n$$

$$\text{Then } s_j = \mu_{3j} / (\mu_{2j})^{3/2} \quad (11)$$

$$\text{and } k_j = (\mu_{4j} / \mu_{2j}^2) - 3 \quad (12)$$

Note: This subroutine cannot distinguish between a blank and a zero. Therefore, if a blank is specified as a missing data code in input cards, it will be treated as 0 (zero).

For reference see B. Ostle, Statistics in Research. The Iowa State College Press, 1954, chapter 6.

```

C-----MISR 10
C-----MISR 20
C-----MISR 30
C-----MISR 40
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C-----MISR 210
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C-----MISR 380
C-----MISR 390
C-----MISR 400
C-----MISR 410
C-----MISR 420
C-----MISR 430
C-----MISR 440
C-----MISR 450
C-----MISR 460
C-----MISR 470
C-----MISR 480
C-----MISR 490
C-----MISR 500
C-----MISR 510
C-----MISR 520
C-----MISR 530
C-----MISR 540
C-----MISR 550
C-----MISR 560
C-----MISR 570
C-----MISR 580
C-----MISR 590
C-----MISR 600
C-----MISR 610
C-----MISR 620
C-----MISR 630
C-----MISR 640
C-----MISR 650
C-----MISR 660
C-----MISR 670
C-----MISR 680
C-----MISR 690
C-----MISR 700
C-----MISR 710
C-----MISR 720
C-----MISR 730
C-----MISR 740
C-----MISR 750
C-----MISR 760
C-----MISR 770
C-----MISR 780
C-----MISR 790
C-----MISR 800
C-----MISR 810
C-----MISR 820
C-----MISR 830
C-----MISR 840
C-----MISR 850
C-----MISR 860
C-----MISR 870
C-----MISR 880
C-----MISR 890
C-----MISR 900
C-----MISR 910
C-----MISR 920
C-----MISR 930
C-----MISR 940
C-----MISR 950
C-----MISR 960
C-----MISR 970
C-----MISR 980
C-----MISR 990
C-----MISR1000
C-----MISR1010
C-----MISR1020
C-----MISR1030
C-----MISR1040
C-----MISR1050
C-----MISR1060
C-----MISR1070
C-----MISR1080
C-----MISR1090
C-----MISR1100
C-----MISR1110
C-----MISR1120
C-----MISR1130
C-----MISR1140
C-----MISR1150
C-----MISR1160
C-----MISR1170
C-----MISR1180
C-----MISR1190
C-----MISR1200
C-----MISR1210
C-----MISR1220
C-----MISR1230
C-----MISR1240
C-----MISR1250
C-----MISR1260
C-----MISR1270
C-----MISR1280
C-----MISR1290
C-----MISR1300
C-----MISR1310
SUBROUTINE MISR
PURPOSE
  COMPUTE MEANS, STANDARD DEVIATIONS, SKEWNESS AND KURTOSIS,
  CORRELATION COEFFICIENTS, REGRESSION COEFFICIENTS, AND
  STANDARD ERRORS OF REGRESSION COEFFICIENTS WHEN THERE ARE
  MISSING DATA POINTS. THE USER IDENTIFIES THE MISSING DATA
  BY MEANS OF A NUMERIC CODE. THOSE VALUES HAVING THIS CODE
  ARE SKIPPED IN COMPUTING THE STATISTICS. IN THE CASE OF THEMSE
  CORRELATION COEFFICIENTS, ANY PAIR OF VALUES ARE SKIPPED IF
  EITHER ONE OF THEM ARE MISSING.
USAGE
  CALL MISR (ND,M,X,CODE,XBAR,STD,SKEW,CURT,R,N,A,B,S,IER)
DESCRIPTION OF PARAMETERS
  ND - NUMBER OF OBSERVATIONS
  M - NUMBER OF VARIABLES
  X - INPUT DATA MATRIX OF SIZE ND X M.
  CODE - INPUT VECTOR OF LENGTH M, WHICH CONTAINS A NUMERIC
  MISSING DATA CODE FOR EACH VARIABLE. ANY OBSERVATION
  FOR A GIVEN VARIABLE HAVING A VALUE EQUAL TO THE CODE
  WILL BE DROPPED FOR THE COMPUTATIONS.
  XBAR - OUTPUT VECTOR OF LENGTH M CONTAINING MEANS
  STD - OUTPUT VECTOR OF LENGTH M CONTAINING STANDARD DEVI-
  ATIONS
  SKEW - OUTPUT VECTOR OF LENGTH M CONTAINING SKEWNESS
  CURT - OUTPUT VECTOR OF LENGTH M CONTAINING KURTOSIS
  R - OUTPUT MATRIX OF PRODUCT-MOMENT CORRELATION
  COEFFICIENTS. THIS WILL BE THE UPPER TRIANGULAR
  MATRIX ONLY, SINCE THE M X M MATRIX OF COEFFICIENTS
  IS SYMMETRIC. (STORAGE MODE 1)
  N - OUTPUT MATRIX OF NUMBER OF PAIRS OF OBSERVATIONS USED
  IN COMPUTING THE CORRELATION COEFFICIENTS. ONLY THE
  UPPER TRIANGULAR PORTION OF THE MATRIX IS GIVEN.
  (STORAGE MODE 1)
  A - OUTPUT MATRIX (M BY M) CONTAINING INTERCEPTS OF
  REGRESSION LINES (A) OF THE FORM Y=A+BX. THE FIRST
  SUBSCRIPT OF THIS MATRIX REFERS TO THE INDEPENDENT
  VARIABLE AND THE SECOND TO THE DEPENDENT VARIABLE.
  FOR EXAMPLE, A(1,3) CONTAINS THE INTERCEPT OF THE
  REGRESSION LINE FOR TWO VARIABLES WHERE VARIABLE 1
  IS INDEPENDENT AND VARIABLE 3 IS DEPENDENT. NOTE
  THAT MATRIX A IS STORED IN A VECTOR FORM.
  B - OUTPUT MATRIX (M BY M) CONTAINING REGRESSION
  COEFFICIENTS (B) CORRESPONDING TO THE VALUES OF
  INTERCEPTS CONTAINED IN THE OUTPUT MATRIX A.
  S - OUTPUT MATRIX (M BY M) CONTAINING STANDARD ERRORS
  OF REGRESSION COEFFICIENTS CORRESPONDING TO THE
  COEFFICIENTS CONTAINED IN THE OUTPUT MATRIX B.
  IER - 0, NO ERROR.
  1, IF NUMBER OF NON-MISSING DATA ELEMENTS FOR J-TH
  VARIABLE IS TWO OR LESS. IN THIS CASE, STD(J),
  SKEW(J), AND CURT(J) ARE SET TO 10**75. ALL
  VALUES OF R, A, B, AND S RELATED TO THIS VARIABLE
  ARE ALSO SET TO 10**75.
  2, IF VARIANCE OF J-TH VARIABLE IS LESS THAN
  10**(-20). IN THIS CASE, STD(J), SKEW(J), AND
  CURT(J) ARE SET TO 10**75. ALL VALUES OF R, A,
  B, AND S RELATED TO THIS VARIABLE ARE ALSO SET TO
  10**75.
REMARKS
  THIS SUBROUTINE CANNOT DISTINGUISH A BLANK AND A ZERO.
  THEREFORE, IF A BLANK IS SPECIFIED AS A MISSING DATA CODE IN
  INPUT CARDS, IT WILL BE TREATED AS 0 (ZERO).
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
METHOD
  LEAST SQUARES REGRESSION LINES AND PRODUCT-MOMENT CORRE-
  LATION COEFFICIENTS ARE COMPUTED.
-----
SUBROUTINE MISR (ND,M,X,CODE,XBAR,STD,SKEW,CURT,R,N,A,B,S,IER)
DIMENSION X(1),CODE(1),XBAR(1),STD(1),SKEW(1),CURT(1),R(1),N(1)
DIMENSION A(1),B(1),S(1)
COMPUTE MEANS
IER=0
L=0
DO 20 J=1,M
  FN=0.0
  XBAR(J)=0.0
  DO 15 I=1,ND
    L=L+1
    IF(X(L)-CODE(J)) 12, 15, 12
  12 FN=FN+1.0
  XBAR(J)=XBAR(J)+X(L)
  15 CONTINUE
  IF (FN) 16, 16, 17
  16 XBAR(J)=0.0
  GO TO 20
  17 XBAR(J)=XBAR(J)/FN
  20 CONTINUE
SET-UP WORK AREAS AND TEST WHETHER DATA IS MISSING
L=0
DO 55 J=1,M
  LJJ=NO*(J-1)
  SKEW(J)=0.0
  CURT(J)=0.0
  K1=M*(J-1)
  KJ=J-M
  DO 54 I=1,J
    K1=K1+1
    KJ=KJ+M
  SUMK=0.0
  SUMY=0.0
  TI=0.0
  TJ=0.0
  TII=0.0
  TJJ=0.0
  TIIJ=0.0
  NI=0
  LI=NO*(I-1)
  LJ=LJJ
  L=L+1
  DO 38 K=1,NO
    LI=LI+1
    LJ=LJ+1
    IF(X(LI)-CODE(1)) 30, 38, 30
    IF(X(LJ)-CODE(J)) 35, 38, 35

```

```

C
C      BOTH DATA ARE PRESENT
C
35 XX=X(L1)-XBAR(I1)
   YY=X(LJ)-XBAR(J1)
   TI=TI+XX
   TII=TI+XX**2
   TJJ=TJJ+YY
   TJJ=TJJ+YY**2
   TIJ=TI+XX*YY
   NIJ=NIJ+1
   SUMX=SUMX+X(L1)
   SUMY=SUMY+X(LJ)
   IF(I-J) 36, 37, 37
37 SKEW(J)=SKEW(J)+YY**3
   CURT(J)=CURT(J)+YY**4
38 CONTINUE
C
C      COMPUTE SUM OF CROSS-PRODUCTS OF DEVIATIONS
C
C      IF(NIJ) 40, 40, 39
39 FN=NIJ
   R(L)=TIJ-TI*TJ/FN
   N(L)=NIJ
   TII=TII-TI*TI/FN
   TJJ=TJJ-TJ*TJ/FN
C
C      COMPUTE STANDARD DEVIATION, SKEWNESS, AND KURTOSIS
C
40 IF(I-J) 47, 41, 47
41 IF(NIJ-2) 42,42,43
42 IER=1
   R(L)=1.0E75
   A(KI)=1.0E75
   B(KI)=1.0E75
   S(KI)=1.0E75
   GO TO 45
C
43 STD(J)=R(L)
   R(L)=1.0
   A(KI)=0.0
   B(KI)=1.0
   S(KI)=0.0
C
44 IF(STD(J)-(1.0E-20)) 44,44,46
45 STD(J)=1.0E75
   SKEW(J)=1.0E75
   CURT(J)=1.0E75
   GO TO 55
MISF1320
MISF1330
MISF1340
MISF1350
MISF1360
MISF1370
MISF1380
MISF1390
MISF1400
MISF1410
MISF1420
MISF1430
MISF1440
MISF1450
MISF1460
MISF1470
MISF1480
MISF1490
MISF1500
MISF1510
MISF1520
MISF1530
MISF1540
MISF1550
MISF1560
MISF1570
MISF1580
MISF1590
MISF1600
MISF1610
MISF1620
MISF1630
MISF1640
MISF1650
MISF1660
MISF1670
MISF1680
MISF1690
MISF1700
MISF1710
MISF1720
MISF1730
MISF1740
MISF1750
MISF1760
MISF1770
MISF1780
MISF1790
MISF1800
MISF1810
C
46 WOPK=STD(J)/FN
   SKEW(J)=(SKEW(J)/FN)/(WOPK*SQRT(WOPK))
   CURT(J)=((CURT(J)/FN)/(WOPK**2))-3.0
   STD(J)=SQRT(STD(J)/(FN-1.0))
   GO TO 55
C
C      COMPUTE REGRESSION COEFFICIENTS
C
47 IF(NIJ-2) 48,48,50
48 IER=1
49 R(L)=1.0E75
   A(KI)=1.0E75
   B(KI)=1.0E75
   S(KI)=1.0E75
   A(KJ)=1.0E75
   B(KJ)=1.0E75
   S(KJ)=1.0E75
   GO TO 54
C
50 IF(TII-(1.0E-20)) 52,52,51
51 IF(TJJ-(1.0E-20)) 52,52,53
52 IER=2
   GO TO 49
C
53 SUMX=SUMX/FN
   SUMY=SUMY/FN
   B(KI)=R(L)/TII
   A(KI)=SUMY-B(KI)*SUMX
   B(KJ)=R(L)/TJJ
   A(KJ)=SUMY-B(KJ)*SUMY
C
C      COMPUTE CORRELATION COEFFICIENTS
C
R(L)=R(L)/(SQRT(TII)*SQRT(TJJ))
C
C      COMPUTE STANDARD ERRORS OF REGRESSION COEFFICIENTS
C
RR=P(L)**2
SUMX=(TJJ-TJJ**PP)/(FN-2)
S(KI)=SQRT(SUMX/TII)
SUMY=(TII-TII**PP)/(FN-2)
S(KJ)=SQRT(SUMY/TJJ)
C
54 CONTINUE
55 CONTINUE
C
RETURN
END
MISF1820
MISF1830
MISF1840
MISF1850
MISF1860
MISF1870
MISF1880
MISF1890
MISF1900
MISF1910
MISF1920
MISF1930
MISF1940
MISF1950
MISF1960
MISF1970
MISF1980
MISF1990
MISF2000
MISF2010
MISF2020
MISF2030
MISF2040
MISF2050
MISF2060
MISF2070
MISF2080
MISF2090
MISF2100
MISF2110
MISF2120
MISF2130
MISF2140
MISF2150
MISF2160
MISF2170
MISF2180
MISF2190
MISF2200
MISF2210
MISF2220
MISF2230
MISF2240
MISF2250
MISF2260
MISF2270
MISF2280
MISF2290
MISF2300

```

Multiple Linear Regression

In the Scientific Subroutine Package, multiple linear regression is normally performed by calling four subroutines in sequence.

1. CORRE - to find means, standard deviations, and correlation matrix

2. ORDER - to choose a dependent variable and a subset of independent variables from a larger set of variables

3. MINV - to invert the correlation matrix of the subset selected by ORDER

4. MULTR - to compute the regression coefficients $b_0, b_1, b_2, \dots, b_m$, and various confidence measures

The subroutine CORRE works in either of two ways: (1) it expects all observations in core, or (2) it triggers a user-provided input subroutine, DATA, to read one observation at a time into a work area. In either case, the user must provide a subroutine named DATA (see "Subroutines Required" in the comment cards description of subroutine CORRE).

Subroutine ORDER

```

C .....ORDE 10
C .....ORDE 20
C .....ORDE 30
C .....ORDE 40
C .....ORDE 50
C .....ORDE 60
C .....ORDE 70
C .....ORDE 80
C .....ORDE 90
C .....ORDE 100
C .....ORDE 110
C .....ORDE 120
C .....ORDE 130
C .....ORDE 140
C .....ORDE 150
C .....ORDE 160
C .....ORDE 170
C .....ORDE 180
C .....ORDE 190
C .....ORDE 200
C .....ORDE 210
C .....ORDE 220
C .....ORDE 230
C .....ORDE 240
C .....ORDE 250
C .....ORDE 260
C .....ORDE 270
C .....ORDE 280
C .....ORDE 290
C .....ORDE 300
C .....ORDE 310
C .....ORDE 320
C .....ORDE 330
C .....ORDE 340
C .....ORDE 350
C .....ORDE 360
C .....ORDE 370
C .....ORDE 380
C .....ORDE 390
C .....ORDE 400
C .....ORDE 410
C .....ORDE 420
C .....ORDE 430
C .....ORDE 440
C .....ORDE 450
C .....ORDE 460
C .....ORDE 470
C .....ORDE 480
C .....ORDE 490
C .....ORDE 500
C .....ORDE 510
C .....ORDE 520
C .....ORDE 530
C .....ORDE 540
C .....ORDE 550
C .....ORDE 560
C .....ORDE 570
C .....ORDE 580
C .....ORDE 590
C .....ORDE 600
C .....ORDE 610
C .....ORDE 620
C .....ORDE 630
C .....ORDE 640
C .....ORDE 650
C .....ORDE 660
C .....ORDE 670
C .....ORDE 680
C .....ORDE 690
C .....ORDE 700
C .....ORDE 710
C .....ORDE 720
C .....ORDE 730
C .....ORDE 740
C .....ORDE 750
C .....ORDE 760
C .....ORDE 770
C .....ORDE 780
C .....ORDE 790
C .....ORDE 800
C .....ORDE 810
C .....ORDE 820
C .....ORDE 830
C .....ORDE 840
C .....ORDE 850
C .....ORDE 860
C .....ORDE 870
C .....ORDE 880
C .....ORDE 890
C .....ORDE 900
C .....ORDE 910
C .....ORDE 920
C .....ORDE 930
C .....ORDE 940
C .....ORDE 950
C .....ORDE 960
C .....ORDE 970
C .....ORDE 980
C .....ORDE 990

```

.....ORDE 10
.....ORDE 20
.....ORDE 30
.....ORDE 40
.....ORDE 50
.....ORDE 60
.....ORDE 70
.....ORDE 80
.....ORDE 90
.....ORDE 100
.....ORDE 110
.....ORDE 120
.....ORDE 130
.....ORDE 140
.....ORDE 150
.....ORDE 160
.....ORDE 170
.....ORDE 180
.....ORDE 190
.....ORDE 200
.....ORDE 210
.....ORDE 220
.....ORDE 230
.....ORDE 240
.....ORDE 250
.....ORDE 260
.....ORDE 270
.....ORDE 280
.....ORDE 290
.....ORDE 300
.....ORDE 310
.....ORDE 320
.....ORDE 330
.....ORDE 340
.....ORDE 350
.....ORDE 360
.....ORDE 370
.....ORDE 380
.....ORDE 390
.....ORDE 400
.....ORDE 410
.....ORDE 420
.....ORDE 430
.....ORDE 440
.....ORDE 450
.....ORDE 460
.....ORDE 470
.....ORDE 480
.....ORDE 490
.....ORDE 500
.....ORDE 510
.....ORDE 520
.....ORDE 530
.....ORDE 540
.....ORDE 550
.....ORDE 560
.....ORDE 570
.....ORDE 580
.....ORDE 590
.....ORDE 600
.....ORDE 610
.....ORDE 620
.....ORDE 630
.....ORDE 640
.....ORDE 650
.....ORDE 660
.....ORDE 670
.....ORDE 680
.....ORDE 690
.....ORDE 700
.....ORDE 710
.....ORDE 720
.....ORDE 730
.....ORDE 740
.....ORDE 750
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.....ORDE 770
.....ORDE 780
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.....ORDE 930
.....ORDE 940
.....ORDE 950
.....ORDE 960
.....ORDE 970
.....ORDE 980
.....ORDE 990

Subroutine MULTR

This subroutine performs a multiple regression analysis for a dependent variable and a set of independent variables.

Beta weights are calculated using the following equation:

$$\beta_j = \sum_{i=1}^k r_{iy} \cdot r_{ij}^{-1} \quad (1)$$

where r_{iy} = intercorrelation of i^{th} independent variable with dependent variable

r_{ij}^{-1} = the inverse of intercorrelation r_{ij}

$i, j = 1, 2, \dots, k$ imply independent variables

r_{iy} and r_{ij}^{-1} are input to this subroutine.

Then, the regression coefficients are calculated as follows:

$$b_j = \beta_j \cdot \frac{s_y}{s_j} \quad (2)$$

where s_y = standard deviation of dependent variable

s_j = standard deviation of j^{th} independent variable

$j = 1, 2, \dots, k$

s_y and s_j are input to this subroutine.

The intercept is found by the following equation:

$$b_0 = \bar{Y} - \sum_{j=1}^k b_j \cdot \bar{X}_j \quad (3)$$

where \bar{Y} = mean of dependent variable

\bar{X}_j = mean of j^{th} independent variable

\bar{Y} and \bar{X}_j are input to this subroutine.

Multiple correlation coefficient, R , is found first by calculating the coefficient of determination by the following equation:

$$R^2 = \sum_{i=1}^k \beta_i r_{iy} \quad (4)$$

and taking the square root of R^2 :

$$R = \sqrt{R^2} \quad (5)$$

The sum of squares attributable to the regression is found by:

$$\text{SSAR} = R^2 \cdot D_{yy} \quad (6)$$

where D_{yy} = sum of squares of deviations from mean for dependent variable

D_{yy} is input to this subroutine.

The sum of squares of deviations from the regression is obtained by:

$$\text{SSDR} = D_{yy} - \text{SSAR} \quad (7)$$

Then, the F-value for the analysis of variance is calculated as follows:

$$F = \frac{\text{SSAR}/k}{\text{SSDR}/(n-k-1)} = \frac{\text{SSAR}(n-k-1)}{\text{SSDR}(k)} \quad (8)$$

Certain other statistics are calculated as follows:

Variance and standard error of estimate:

$$S_{y.12\dots k}^2 = \frac{\text{SSDR}}{n-k-1} \quad (9)$$

where n = number of observations

$$S_{y.12\dots k} = \sqrt{S_{y.12\dots k}^2} \quad (10)$$

Standard deviations of regression coefficients:

$$S_{b_j} = \sqrt{\frac{r_{jj}^{-1}}{D_{jj}} \cdot S_{y.12\dots k}^2} \quad (11)$$

where D_{jj} = sum of squares of deviations from mean for j^{th} independent variable.

D_{jj} is input to this subroutine.

$j = 1, 2, \dots, k$

Computed t :

$$t_j = \frac{b_j}{S_{b_j}} \quad (12)$$

$j = 1, 2, \dots, k$

Polynomial Regression

In the Scientific Subroutine Package, polynomial regression is normally performed by calling the following four subroutines in sequence:

1. GDATA - to generate the powers of the independent variable and find means, standard deviations, and correlation matrix
2. ORDER - to choose a dependent variable and subset of independent variables from a larger set of variables
3. MINV - to invert the correlation coefficient matrix
4. MULTR - to compute the regression coefficients $b_0, b_1, b_2, \dots, b_m$, and various confidence measures

Subroutine GDATA

This subroutine generates independent variables up to the m^{th} power (the highest degree polynomial specified) and calculates means, standard deviations, sums of cross-products of deviations from means, and product moment correlation coefficients.

X_{i1} denotes the i^{th} case of the independent variable;
 X_{ip} denotes the i^{th} case of the dependent variable,
 where $i = 1, 2, \dots, n$

n = number of cases (observations)
 $p = m + 1$
 m = highest degree polynomial specified

The subroutine GDATA generates powers of the independent variable as follows:

$$\begin{aligned} X_{i2} &= X_{i1} \cdot X_{i1} \\ X_{i3} &= X_{i2} \cdot X_{i1} \\ X_{i4} &= X_{i3} \cdot X_{i1} \\ &\cdot \\ &\cdot \\ X_{im} &= X_{i,m-1} \cdot X_{i1} \end{aligned} \quad (1)$$

where i and m are as defined as above.

Then, the following are calculated.

Means:

$$\bar{X}_j = \frac{\sum_{i=1}^n X_{ij}}{n} \quad (2)$$

where $j = 1, 2, \dots, p$

Sums of cross-products of deviations from means:

$$D_{jk} = \sum_{i=1}^n (X_{ij} - \bar{X}_j)(X_{ik} - \bar{X}_k) - \frac{\sum_{i=1}^n (X_{ij} - \bar{X}_j) \sum_{i=1}^n (X_{ik} - \bar{X}_k)}{n} \quad (3)$$

where $j = 1, 2, \dots, p$; $k = 1, 2, \dots, p$.

Correlation coefficients:

$$r_{ij} = \frac{D_{ij}}{\sqrt{D_{ii}} \sqrt{D_{jj}}} \quad (4)$$

where $i = 1, 2, \dots, p$; $j = 1, 2, \dots, p$.

Standard deviations:

$$s_j = \frac{\sqrt{D_{jj}}}{\sqrt{n-1}} \quad (5)$$

where $j = 1, 2, \dots, p$

```

C          GOAT 10
C          .....
C          SUBROUTINE GDATA                        GOAT 20
C                                                  GOAT 30
C          PURPOSE                                GOAT 40
C          GENERATE INDEPENDENT VARIABLES UP TO THE M-TH POWER (THE      GOAT 60
C          HIGHEST DEGREE POLYNOMIAL SPECIFIED) AND COMPUTE MEANS,      GOAT 80
C          STANDARD DEVIATIONS, AND CORRELATION COEFFICIENTS. THIS      GOAT 90
C          SUBROUTINE IS NORMALLY CALLED BEFORE SUBROUTINES ORDER,      GOAT 100
C          MINV AND MULTR IN THE PERFORMANCE OF A POLYNOMIAL            GOAT 110
C          REGRESSION.                                                  GOAT 120
C          USAGE                                                        GOAT 130
C          CALL GDATA (N,M,X,XBAR,STD,D,SUMSQ)                          GOAT 140
C          GOAT 150
C          GOAT 160
C          DESCRIPTION OF PARAMETERS                                    GOAT 170
C          N - NUMBER OF OBSERVATIONS.                                GOAT 180
C          M - THE HIGHEST DEGREE POLYNOMIAL TO BE FITTED.           GOAT 190
C          X - INPUT MATRIX (N BY M+1). WHEN THE SUBROUTINE IS          GOAT 200
C          CALLED, DATA FOR THE INDEPENDENT VARIABLE ARE              GOAT 210
C          STORED IN THE FIRST COLUMN OF MATRIX X, AND DATA FOR        GOAT 220
C          THE DEPENDENT VARIABLE ARE STORED IN THE LAST                GOAT 230
C          COLUMN OF THE MATRIX. UPON RETURNING TO THE CALLING          GOAT 240
C          ROUTINE, GENERATED POWERS OF THE INDEPENDENT                GOAT 250
C          VARIABLE ARE STORED IN COLUMNS 2 THROUGH M.                 GOAT 260
C          XBAR - OUTPUT VECTOR OF LENGTH M+1 CONTAINING MEANS OF       GOAT 270
C          INDEPENDENT AND DEPENDENT VARIABLES.                        GOAT 280
C          STD - OUTPUT VECTOR OF LENGTH M+1 CONTAINING STANDARD        GOAT 290
C          DEVIATIONS OF INDEPENDENT AND DEPENDENT VARIABLES.         GOAT 300
C          U - OUTPUT MATRIX (ONLY UPPER TRIANGULAR PORTION OF THE     GOAT 310
C          SYMMETRIC MATRIX OF M+1 BY M+1) CONTAINING CORRELA-        GOAT 320
C          TION COEFFICIENTS. (STORAGE MODE OF 1)                     GOAT 330
C          SUMSQ - OUTPUT VECTOR OF LENGTH M+1 CONTAINING SUMS OF      GOAT 340
C          PRODUCTS OF DEVIATIONS FROM MEANS OF INDEPENDENT           GOAT 350
C          AND DEPENDENT VARIABLES.                                   GOAT 360
C          REMARKS                                                    GOAT 370
C          N MUST BE GREATER THAN M+1.                                GOAT 380
C          IF M IS EQUAL TO 5 OR GREATER, SINGLE PRECISION MAY NOT BE GOAT 390
C          SUFFICIENT TO GIVE SATISFACTORY COMPUTATIONAL RESULTS.     GOAT 400
C          GOAT 410
  
```

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C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED          GDAT 420
C          NONE                                                  GDAT 430
C          METHOD                                                 GDAT 440
C          REFER TO B. OSTLE, 'STATISTICS IN RESEARCH', THE IOWA STATE GDAT 450
C          COLLEGE PRESS, 1954, CHAPTER 9.                      GDAT 460
C          .....                                              GDAT 470
C          .....                                              GDAT 480
C          .....                                              GDAT 490
C          .....                                              GDAT 500
C          SUBROUTINE GOATA (N,M,K,XBAR,STO,J,SUMSQ)              GDAT 510
C          DIMENSION X(1),XBAR(1),STO(1),D(1),SUMSQ(1)          GDAT 520
C          .....                                              GDAT 530
C          .....                                              GDAT 540
C          .....                                              GDAT 550
C          IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE GDAT 560
C          C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION GDAT 570
C          STATEMENT WHICH FOLLOWS.                             GDAT 580
C          .....                                              GDAT 590
C          DOUBLE PRECISION X,XBAR,STO,J,SUMSQ,FL,FZ            GDAT 600
C          .....                                              GDAT 610
C          THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS GDAT 620
C          APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS GDAT 630
C          ROUTINE.                                             GDAT 640
C          .....                                              GDAT 650
C          THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO GDAT 660
C          CONTAIN DOUBLE PRECISION FORTRAN FUNCTIONS.  SQRT AND ABS IN GDAT 670
C          STATEMENT 180 MUST BE CHANGED TO DSQRT AND DABS.     GDAT 680
C          .....                                              GDAT 690
C          .....                                              GDAT 700
C          .....                                              GDAT 710
C          GENERATE INDEPENDENT VARIABLES                       GDAT 720
C          .....                                              GDAT 730
C          IF (A=1) GO 105, 105, 90                             GDAT 740
C          90  L1=0                                             GDAT 750
C          DO 100 I=2,M                                         GDAT 760
C          L1=L1+N                                             GDAT 770
C          DO 100 J=1,N                                         GDAT 780
C          L=L1+J                                             GDAT 790
C          K=L-N                                             GDAT 800
C          100  X(L)=X(K)*X(J)                                  GDAT 810
C          .....                                              GDAT 820
C          CALCULATE MEANS                                     GDAT 830
C          .....                                              GDAT 840
C          105  MM=M+1                                          GDAT 850
C          OPEN                                             GDAT 860
C          L=0                                               GDAT 870
C          DO 110 I=1,MM                                       GDAT 880
C          XBAR(I)=0.0                                         GDAT 890
C          DO 110 J=1,N                                         GDAT 900
C          L=L+1                                             GDAT 910
C          110  XBAR(I)=XBAR(I)+X(L)                            GDAT 920
C          115  XBAR(I)=XBAR(I)/J                               GDAT 930
C          .....                                              GDAT 940
C          DO 130 I=1,MM                                       GDAT 950
C          130  STO(I)=0.0                                       GDAT 960
C          .....                                              GDAT 970
C          CALCULATE SUMS OF CROSS-PRODUCTS OF DEVIATIONS    GDAT 980
C          .....                                              GDAT 990
C          L=(MM+1)*MM/2                                       GDAT1000
C          DO 150 I=1,L                                         GDAT1010
C          150  D(I)=L.C                                         GDAT1020
C          DO 170 K=1,N                                         GDAT1030
C          L=0                                               GDAT1040
C          DO 170 J=1,MM                                       GDAT1050
C          L2=N*(J-1)+K                                       GDAT1060
C          T2=X(L2)-XBAR(J)                                       GDAT1070
C          STO(J)=STO(J)+T2                                       GDAT1080
C          DO 170 I=1,J                                       GDAT1090
C          L1=N*(I-1)+K                                       GDAT1100
C          T1=X(L1)-XBAR(I)                                       GDAT1110
C          L=L+1                                             GDAT1120
C          170  D(I)=D(I)+T1*T2                                       GDAT1130
C          .....                                              GDAT1140
C          DO 175 J=1,MM                                       GDAT1150
C          DO 175 I=1,J                                       GDAT1160
C          L=L+1                                             GDAT1170
C          175  D(I)=D(I)-STO(I)+STO(J)/DF                                       GDAT1180
C          .....                                              GDAT1190
C          DO 180 I=1,MM                                       GDAT1200
C          L=L+1                                             GDAT1210
C          SUMSQ(I)=D(I)                                       GDAT1220
C          180  STO(I)=SQRT(ASS(D(I)))                                       GDAT1230
C          .....                                              GDAT1240
C          CALCULATE CORRELATION COEFFICIENTS                GDAT1250
C          .....                                              GDAT1260
C          L=0                                               GDAT1270
C          DO 190 J=1,MM                                       GDAT1280
C          DO 190 I=1,J                                       GDAT1290
C          L=L+1                                             GDAT1300
C          190  D(I)=D(I)/(STO(I)+STO(J))                                       GDAT1310
C          .....                                              GDAT1320
C          CALCULATE STANDARD DEVIATIONS                      GDAT1330
C          .....                                              GDAT1340
C          DF=SQRT(DF-1.0)                                       GDAT1350
C          DO 200 I=1,MM                                       GDAT1360
C          200  STO(I)=STO(I)/DF                                       GDAT1370
C          RETURN                                             GDAT1380
C          END                                               GDAT1390
C          .....                                              GDAT1400

```

Stepwise Multiple Regression

In the Scientific Subroutine Package, stepwise multiple regression is normally performed by calling the following subroutines:

1. CORRE - to find means, standard deviations, sums of cross-products of deviation matrix, and correlation matrix
2. MSTR - to save the matrix of sums of cross-products of deviations and to copy it to a working matrix for the purpose of using the same data repeatedly
3. LOC - to compute a vector subscript for an element in general and symmetric matrices. This subroutine is called by the subroutine MSTR
4. STPRG - to compute regression coefficients and other statistics for each step of regression

The subroutine CORRE works in either of two ways: (1) it expects all observations in core, or (2) it triggers a user-provided input subroutine, DATA, to read one observation at a time into a work area. In either case, the user must provide a subroutine named DATA (see "Subroutines and Function Subprograms Required" in the comment cards description of the subroutine CORRE).

The subroutine STPRG calls an output subroutine, STOUT, in order to print various statistics computed for each step of regression. The subroutine STOUT must also be provided by the user.

Subroutine STPRG

This subroutine performs a stepwise multiple regression analysis for a dependent variable and a set of independent variables. In each step of the regression $i=1,2,\dots,q$, where q is the number of independent variables, the abbreviated Doolittle method is used to calculate the following statistics:

The independent variable entering in the regression is selected, first, by computing the amount of reduction of sum of squares for each variable:

$$C_j = \frac{a_{jy}^2}{a_{jj}} \quad (1)$$

where a_{jj} is initially an element in the sums of cross-products of deviations matrix which will be modified in successive steps.

$j = 1, 2, \dots, q$ are independent variables ($j \neq$ variables deleted and variables entered before the i^{th} step)

$y =$ dependent variable

and, second, by finding the maximum (over j) of C_j .

Set $S_i = C_j$ to indicate the sum of squares that will be reduced in the i^{th} step.

The proportion of S_i to the total is obtained by:

$$p = \frac{S_i}{D} \quad (2)$$

where $D = \sum_{j=1}^n (y_j - \bar{y})^2$

$n =$ number of observations

If p is less than the constant specified by the user to limit independent variables, the analysis will be terminated without entering the last variable selected; otherwise, the following calculations are continued:

The cumulative sum of squares reduced is obtained by

$$S_{cum} = S_{cum} + S_i \quad (3)$$

and the cumulative proportion reduced by

$$P_{cum} = P_{cum} + p \quad (4)$$

The multiple correlation coefficient is computed by

$$R = \sqrt{P_{cum}} \quad (5)$$

and adjusted for degrees of freedom by

$$R_c = \sqrt{1 - (1-R^2) \frac{(n-1)}{(n-k)}}$$

where there are k independent variables in the regression.

The F-value for analysis of variance is given by

$$F = \frac{S_{cum} / k}{(D - S_{cum}) / (n-k-1)} \quad (6)$$

The standard error of the estimated y is obtained by the use of the formula

$$s_{y.12\dots i} = \sqrt{\frac{D - S_{cum}}{n - k - 1}} \quad (7)$$

and adjusted by

$$s_c = s \sqrt{(n-1) / (n-k)}$$

Then, the following is computed:

$$a_{jj} = a_{jj} + \frac{a_{ij}^2}{a_{ii}} \quad (8)$$

where $i =$ variable entered in the i^{th} step

$j = v_1, v_2, \dots, v_{i-1}$ are the variables entered in the regression before the i^{th} step, and

$$g_{ik} = \frac{a_{ik}}{a_{ii}} \quad (9)$$

where $k = 1, 2, \dots, m$ are variables including y ($k \neq$ variables deleted and the variable entered in the i^{th} step).

Regression coefficients are computed by:

$$b_i = g_{iy} \quad (10)$$

$$b_{i-1} = g_{(i-1)y} - b_i g_{(i-1)i}$$

$$b_{i-2} = g_{(i-2)y} - b_i g_{(i-2)i} - b_{i-1} g_{(i-2)(i-1)}$$

etc. ,

and the value of the intercept as

$$b_0 = \bar{y} - \sum_{j=1}^k b_j \bar{x}_j \quad (11)$$

where k = number of independent variables in the regression.

Standard errors of regression coefficients are given by

$$s_{b_j} = \sqrt{a_{jj}} s_{y.12\dots i} \quad (12)$$

where $j = v_1, v_2, \dots, v_i$ are variables in the regression, and t-values as

$$t_j = \frac{b_j}{s_{b_j}} \quad (13)$$

Perform the reduction to eliminate the variable entered in the ith step:

$$a_{jk} = a_{jk} - a_{ji}g_{ik} \quad (14)$$

where i = variable entered in the ith step

$j = 1, 2, \dots, m$ (j ≠ variables deleted or variables in the regression)

$k = 1, 2, \dots, m$ (k ≠ variables deleted and the variable entered in the ith step)

$$a_{ji} = \frac{a_{ji}}{-a_{ii}} \quad (15)$$

$$a_{ii} = \frac{1}{a_{ii}} \quad (16)$$

For reference see C. A. Bennett and N. L. Franklin, *Statistical Analysis in Chemistry and the Chemical Industry*. John Wiley and Sons, 1954, Appendix 6A.

```

C
C
C
C-----STPR 10
C-----STPR 20
C
C SUBROUTINE STPRC
C
C STPR 30
C
C PURPOSE
C STPR 40
C TO PERFORM A STEPWISE MULTIPLE REGRESSION ANALYSIS FOR A
C STPR 50
C DEPENDENT VARIABLE AND A SET OF INDEPENDENT VARIABLES. AT
C STPR 60
C EACH STEP, THE VARIABLE ENTERED INTO THE REGRESSION EQUATION
C STPR 70
C IS THAT WHICH EXPLAINS THE GREATEST AMOUNT OF VARIANCE
C STPR 100
C BETWEEN IT AND THE DEPENDENT VARIABLE (I.E. THE VARIABLE
C STPR 110
C WITH THE HIGHEST PARTIAL CORRELATION WITH THE DEPENDENT
C STPR 120
C VARIABLE). ANY VARIABLE CAN BE DESIGNATED AS THE DEPENDENT
C STPR 130
C VARIABLE. ANY INDEPENDENT VARIABLE CAN BE FORCED INTO OR
C STPR 140
C DELETED FROM THE REGRESSION EQUATION, IRRESPECTIVE OF ITS
C STPR 150
C CONTRIBUTION TO THE EQUATION.
C STPR 160
C
C USAGE
C STPR 170
C CALL STPRC (M,N,C,XBAR,ICX,PCT,ASTEP,ANS,L,B,S,T,LL,IER)
C STPR 180
C STPR 190
C STPR 200
C
C DESCRIPTION OF PARAMETERS
C STPR 210
C M - TOTAL NUMBER OF VARIABLES IN DATA MATRIX
C STPR 220
C N - NUMBER OF OBSERVATIONS
C STPR 230
C C - INPUT MATRIX (M X N) OF SUMS OF CROSS-PRODUCTS OF
C STPR 240
C DEVIATIONS FROM MEAN. THIS MATRIX WILL BE DESTROYED.
C STPR 250
C XBAR - INPUT VECTOR OF LENGTH P OF MEANS
C STPR 260
C ICX - INPUT VECTOR OF LENGTH P HAVING ONE OF THE FOLLOWING
C STPR 270
C VALUES FOR EACH VARIABLE:
C STPR 280
C 0 - INDEPENDENT VARIABLE AVAILABLE FOR SELECTION
C STPR 290
C 1 - INDEPENDENT VARIABLE TO BE FORCED INTO THE
C STPR 300
C REGRESSION EQUATION
C STPR 310
C 2 - VARIABLE NOT TO BE CONSIDERED IN THE EQUATION
C STPR 320
C 3 - DEPENDENT VARIABLE
C STPR 330
C THIS VECTOR WILL BE DESTROYED
C STPR 340
C PCT - A CONSTANT VALUE INDICATING THE PROPORTION OF THE
C STPR 350
C TOTAL VARIANCE TO BE EXPLAINED BY ANY INDEPENDENT
C STPR 360
C VARIABLE. THOSE INDEPENDENT VARIABLES WHICH FALL
C STPR 370

```

```

C
C
C
C-----STPR 380
C-----STPR 390
C
C BELLN THIS PROGRAM WILL NOT ENTER THE REGRESSION
C STPR 400
C EQUATION. TO ENSURE THAT ALL VARIABLES ENTER THE
C STPR 410
C EQUATION, SET PCT = 0.0.
C STPR 420
C
C ASTEP= OUTPUT VECTOR OF LENGTH 5 CONTAINING THE FOLLOWING
C STPR 430
C INFORMATION
C STPR 440
C ASTEP(1) - THE NUMBER OF THE DEPENDENT VARIABLE
C STPR 450
C ASTEP(2) - NUMBER OF VARIABLES FORCED INTO THE
C STPR 460
C REGRESSION EQUATION
C STPR 470
C ASTEP(3) - NUMBER OF VARIABLE DELETED FROM THE
C STPR 480
C EQUATION
C STPR 490
C ASTEP(4) - THE NUMBER OF THE LAST STEP
C STPR 500
C ASTEP(5) - THE NUMBER OF THE LAST VARIABLE ENTERED
C STPR 510
C
C ANS - OUTPUT VECTOR OF LENGTH 11 CONTAINING THE FOLLOWING
C STPR 520
C INFORMATION FOR THE LAST STEP
C STPR 530
C ANS(1) - SUM OF SQUARES REDUCED BY THIS STEP
C STPR 540
C ANS(2) - PROPORTION OF TOTAL SUM OF SQUARES REDUCED
C STPR 550
C THIS STEP
C STPR 560
C ANS(3) - CUMULATIVE SUM OF SQUARES REDUCED UP TO
C STPR 570
C THIS STEP
C STPR 580
C ANS(4) - CUMULATIVE PROPORTION OF TOTAL SUM OF
C STPR 590
C SQUARES REDUCED
C STPR 600
C ANS(5) - SUM OF SQUARES OF THE DEPENDENT VARIABLE
C STPR 610
C ANS(6) - MULTIPLE CORRELATION COEFFICIENT
C STPR 620
C ANS(7) - F RATIO FOR SUM OF SQUARES DUE TO
C STPR 630
C REGRESSION
C STPR 640
C ANS(8) - STANDARD ERROR OF THE ESTIMATE (RESIDUAL
C STPR 650
C MEAN SQUARE)
C STPR 660
C ANS(9) - INTERCEPT CONSTANT
C STPR 670
C ANS(10) - MULTIPLE CORRELATION COEFFICIENT ADJUSTED
C STPR 680
C FOR DEGREES OF FREEDOM.
C STPR 690
C ANS(11) - STANDARD ERROR OF THE ESTIMATE ADJUSTED
C STPR 700
C FOR DEGREES OF FREEDOM.
C STPR 710
C
C L - OUTPUT VECTOR OF LENGTH K, WHERE K IS THE NUMBER OF
C STPR 720
C INDEPENDENT VARIABLES IN THE REGRESSION EQUATION.
C STPR 730
C THIS VECTOR CONTAINS THE NUMBERS OF THE INDEPENDENT
C STPR 740
C VARIABLES IN THE EQUATION.
C STPR 750
C
C E - OUTPUT VECTOR OF LENGTH K, CONTAINING THE PARTIAL
C STPR 760
C REGRESSION COEFFICIENTS CORRESPONDING TO THE
C STPR 770
C VARIABLES IN VECTOR L.
C STPR 780
C
C S - OUTPUT VECTOR OF LENGTH K, CONTAINING THE STANDARD
C STPR 790
C DEVIATIONS OF THE PARTIAL REGRESSION COEFFICIENTS,
C STPR 800
C CORRESPONDING TO THE VARIABLES IN VECTOR L.
C STPR 810
C
C T - OUTPUT VECTOR OF LENGTH K, CONTAINING THE COMPUTED
C STPR 820
C T-VALUES CORRESPONDING TO THE VARIABLES IN VECTOR L.
C STPR 830
C
C LL - WORKING VECTOR OF LENGTH M
C STPR 840
C IER = C, IF THERE IS NO ERROR.
C STPR 850
C 1, IF RESIDUAL SUM OF SQUARES IS NEGATIVE OR IF THE
C STPR 860
C PIVOTAL ELEMENT IN THE STEWISE INVERSION PROCESS IS
C STPR 870
C ZERO. IN THIS CASE, THE VARIABLE WHICH CAUSES THIS
C STPR 880
C ERROR IS NOT ENTERED IN THE REGRESSION, THE RESULT
C STPR 890
C PRIOR TO THIS STEP IS RETAINED, AND THE CURRENT
C STPR 900
C SELECTION IS TERMINATED.
C STPR 910
C
C REPARKS
C STPR 920
C THE NUMBER OF DATA POINTS MUST BE AT LEAST GREATER THAN THE
C STPR 930
C NUMBER OF INDEPENDENT VARIABLES PLUS ONE. FORCED VARIABLES
C STPR 940
C ARE ENTERED INTO THE REGRESSION EQUATION BEFORE ALL OTHER
C STPR 950
C INDEPENDENT VARIABLES. WITHIN THE SET OF FORCED VARIABLES,
C STPR 960
C ONE MUST BE CHOSEN FIRST WILL BE THAT ONE WHICH EXPLAINS
C STPR 970
C THE GREATEST AMOUNT OF VARIANCE.
C STPR 980
C INSTEAD OF USING, AS A STOPPING CRITERION, A PROPORTION OF
C STPR 990
C THE TOTAL VARIANCE, SOME OTHER CRITERION MAY BE ADDED TO
C STPR 1000
C SUBROUTINE STPRC.
C STPR 1010
C
C SUBROUTINE STPRC (M,N,C,XBAR,ICX,PCT,ASTEP,ANS,L,B,S,T,LL,IER)
C STPR 1020
C
C THIS SUBROUTINE MUST BE PROVIDED BY THE USER. IT IS AN
C STPR 1030
C OPTION WHICH WILL PRINT THE RESULTS OF EACH STEP OF
C STPR 1040
C THE REGRESSION ANALYSIS. ASTEP IS AN OPTION CODE WHICH IS
C STPR 1050
C ONE IF THE STEPWISE REGRESSION IS TO BE TERMINATED, AND IS
C STPR 1060
C ZERO IF IT IS TO CONTINUE. THE USER MUST CONSIDER THIS IF
C STPR 1070
C SOME OTHER STOPPING CRITERION THAN VARIANCE PROPORTION IS
C STPR 1080
C USED.
C STPR 1090
C
C METHCC
C STPR 1100
C THE ABBREVIATED DOUBLE METHCC IS USED TO (1) DECIDE VARI-
C STPR 1110
C ABLES ENTERING IN THE REGRESSION AND (2) COMPUTE REGRESSION
C STPR 1120
C COEFFICIENTS. REFER TO C. A. BENNETT AND N. L. FRANKLIN,
C STPR 1130
C "STATISTICAL ANALYSIS IN CHEMISTRY AND THE CHEMICAL INDUS-
C STPR 1140
C TRY", JOHN WILEY AND SONS, 1954, APPENDIX 6A.
C STPR 1150
C STPR 1160
C STPR 1170
C STPR 1180
C STPR 1190
C STPR 1200
C
C SUBROUTINE STPRC (M,N,C,XBAR,ICX,PCT,ASTEP,ANS,L,B,S,T,LL,IER)
C STPR 1210
C
C DEPENDENT VARIABLE, NUMBER OF VARIABLES TO BE FORCED TO
C STPR 1220
C ENTER IN THE REGRESSION, AND NUMBER OF VARIABLES TO BE DELETED
C STPR 1230
C
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE
C STPR 1240
C STATEMENT W/ICP FOLLOWS.
C STPR 1250
C
C DOUBLE PRECISION D,XBAR,ANS,B,S,T,D,R,E
C STPR 1260
C
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS
C STPR 1270
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS
C STPR 1280
C ROUTINE.
C STPR 1290
C
C THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO
C STPR 1300
C CONTAIN DOUBLE PRECISION FORTRAN STATEMENTS. SORT IN STATEMENTS
C STPR 1310
C 05,06,11,12,AND 13, MUST BE CHANGED TO DSGRT.
C STPR 1320
C STPR 1330
C STPR 1340
C STPR 1350
C STPR 1360
C STPR 1370
C STPR 1380
C STPR 1390
C STPR 1400
C STPR 1410
C STPR 1420
C STPR 1430
C STPR 1440
C STPR 1450
C STPR 1460
C STPR 1470
C STPR 1480
C STPR 1490
C STPR 1500
C STPR 1510
C STPR 1520
C STPR 1530
C STPR 1540
C STPR 1550
C STPR 1560
C STPR 1570
C STPR 1580
C STPR 1590
C STPR 1600
C STPR 1610
C STPR 1620
C STPR 1630
C STPR 1640
C STPR 1650
C STPR 1660

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```

ASTEF(1)=PY
LY=PY-PY-1
LYF=LY+PY
ANS(1)=C(LYF)
3C CCNTINLE
  ASTEF(2)=AFC
C
  FINE THE MAXIMUM NUMBER OF STEPS
C
  PR=P-ASTEF(2)-1
C
  START SELECTION OF VARIABLES
C
  CC 14C AL=1,PX
  RC=C
  IF(AL-AFC) 35, 35, 55
C
  SELECT NEXT VARIABLE TO ENTER AMONG FORCED VARIABLES
C
  35 CC 5C I=1,NFC
  K=IC(I)
  IF(LL(I)) 5C, 5C, 4C
  4C LYF=LY+K
  IF(P=I)-1+K
  RE=C(LYF+IC(LYF)/G(I))
  IF(RE-RE) 45, 5C, 5C
  45 RC=RE
  NEN=K
  5C CCNTINLE
  CC 1C 75
C
  SELECT NEXT VARIABLE TO ENTER AMONG NON-FORCED VARIABLES
C
  55 CC 7C I=1,P
  IF(I-PY) 6C, 7C, 6C
  6C IF(LL(I)) 7C, 7C, 6C
  62 LYF=LY+I
  IF(P=I)-1+I
  RE=C(LYF+IC(LYF)/G(I))
  IF(RE-RE) 64, 7C, 7C
  64 RC=RE
  NEN=I
  7C CCNTINLE
C
  TEST WHETHER THE PROPORTION OF THE SUM OF SQUARES REDUCED BY
  THE LAST VARIABLE ENTERED IS GREATER THAN OR EQUAL TO THE
  SPECIFIC PROPORTION
C
  75 IF(RE) 77,77,76
  76 IF(AAS(5)-AAS(3)+RC)/77,77,76
  77 IER=1
  CC 1C 15C
  78 RE=RC/AAS(5)
  IF(RE-IER) 15C, 8C, 8C
C
  IT IS GREATER THAN OR EQUAL
C
  EC LL(NEN)=C
  C(L1)=NEN
  ANS(1)=RE
  ANS(2)=RE
  ANS(3)=ANS(3)+RC
  ANS(4)=ANS(4)+RE
  NSTEP(4)=NL
  NSTEP(5)=NEN
C
  COMPLETE MULTIPLE CORRELATION, F-VALUE FOR ANALYSIS OF
  VARIANCE, AND STANDARD ERROR OF ESTIMATE
C
  85 ANS(4)=SQRT(ANS(4))
  RC=NL
  RE=CAP-RC
  RE=(ANS(5)-ANS(3))/RE
  ANS(7)=(ANS(3)/RC)/RE
  9C ANS(8)=SQRT(8E)
C
  DIVIDE BY THE PIVOTAL ELEMENT
C
  IF=P+(NEN-1)*NEN
  RC=C(I)
  LYF=NEN-P
  CC 1CC J=1,P
  LYF=LYF+P
  IF(LL(J)) 1CC, 54, 57
  94 IF(J=NEN) 5C, 5C, 5C
  96 IJ=P+(J-1)*P
  C(L1)=C(IJ)+C(LYF)+C(LYF)/RD
  97 C(LYF)=C(LYF)/RC
  CC 1C 1CC
  98 C(I)F=I.C/RC
  1CC CCNTINLE
C
  COMPLETE REGRESSION COEFFICIENTS
C
  LYF=LY+NEN
  E(NL)=C(LYF)
  IF(AL-1) 112, 112, 1C5
  1C5 IC=AL-1
  CC 11C J=1,IC
  IJ=NL-J
  K=C(IJ)
  LYF=LY+K
  E(IJ)=C(LYF)
  CC 11C K=1,J
  K=NL-K+1
  PK=L(IK)
  LYF=P+(PK-1)+K
  11C E(IJ)=E(IJ)-C(LYF)*K(IK)
C
  COMPLETE INTERCEPT
C
  112 ANS(5)=RE/P(Y)
  CC 115 I=1,NL
  KK=L(I)
  ANS(5)=ANS(5)-E(I)*XBAR(KK)
  IJ=P+(K-1)+K
  114 S(I)=ANS(5)*SQRT(C(L1))
  115 T(I)=E(I)/S(I)
C
  PERFORM A REDUCTION TO ELIMINATE THE LAST VARIABLE ENTERED
C
  IF=P+(NEN-1)
  CC 13C I=1,P
  IJ=I-P
  IR=NEN-P
  IF=IP+1
  IF(LL(I)) 13C, 13C, 12C
  12C CC 12C J=1,P
  IJ=IJ+P
```

```

STPR1670
STPR1680
STPR1690
STPR1700
STPR1710
STPR1720
STPR1730
STPR1740
STPR1750
STPR1760
STPR1770
STPR1780
STPR1790
STPR1800
STPR1810
STPR1820
STPR1830
STPR1840
STPR1850
STPR1860
STPR1870
STPR1880
STPR1890
STPR1900
STPR1910
STPR1920
STPR1930
STPR1940
STPR1950
STPR1960
STPR1970
STPR1980
STPR1990
STPR2000
STPR2010
STPR2020
STPR2030
STPR2040
STPR2050
STPR2060
STPR2070
STPR2080
STPR2090
STPR2100
STPR2110
STPR2120
STPR2130
STPR2140
STPR2150
STPR2160
STPR2170
STPR2180
STPR2190
STPR2200
STPR2210
STPR2220
STPR2230
STPR2240
STPR2250
STPR2260
STPR2270
STPR2280
STPR2290
STPR2300
STPR2310
STPR2320
STPR2330
STPR2340
STPR2350
STPR2360
STPR2370
STPR2380
STPR2390
STPR2400
STPR2410
STPR2420
STPR2430
STPR2440
STPR2450
STPR2460
STPR2470
STPR2480
STPR2490
STPR2500
STPR2510
STPR2520
STPR2530
STPR2540
STPR2550
STPR2560
STPR2570
STPR2580
STPR2590
STPR2600
STPR2610
STPR2620
STPR2630
STPR2640
STPR2650
STPR2660
STPR2670
STPR2680
STPR2690
STPR2700
STPR2710
STPR2720
STPR2730
STPR2740
STPR2750
STPR2760
STPR2770
STPR2780
STPR2790
STPR2800
STPR2810
STPR2820
STPR2830
STPR2840
STPR2850
STPR2860
STPR2870
STPR2880
STPR2890
STPR2900
STPR2910
STPR2920
STPR2930
STPR2940
STPR2950
```

```

I=IK+P
IF(LL(J)) 126, 126, 122
122 IF(J=NEN) 124, 126, 124
124 C(L1)=C(IJ)-C(I)*C(IK)
126 CCNTINLE
  C(I)F=C(I)F/(1-RC)
  13C CCNTINLE
C
  ADJUST STANDARD ENCR OF THE ESTIMATE AND MULTIPLE CORRELATION
  COEFFICIENT
C
  RC=P-ASTEF(4)
  RE=CAW/RC
  132 ANS(1C)=SQRT(1.C-(1.C-ANS(1C))*ANS(1C))*RC)
  134 ANS(11)=ANS(1)*SQRT(8C)
C
  CALL THE CLPTL SLERCLINE
  CALL STCLT (NSTEP,ANS,L,B,S,Y,ASTCP)
C
  TEST WHETHER THE STEP-WISE REGRESSION WAS TERMINATED IN
  SUBROUTINE STCLT
  IF(ASTCF) 14C, 14C, 150
  14C CCNTINLE
  15C RETURN
  END
```

```

STPR2960
STPR2970
STPR2980
STPR2990
STPR3000
STPR3010
STPR3020
STPR3030
STPR3040
STPR3050
STPR3060
STPR3070
STPR3080
STPR3090
STPR3100
STPR3110
STPR3120
STPR3130
STPR3140
STPR3150
STPR3160
STPR3170
STPR3180
STPR3190
STPR3200
STPR3210
STPR3220
STPR3230
```

Subroutine PROBT

This subroutine obtains maximum likelihood estimates of a and b for the probit equation $Y = a + bX$. An iterative scheme is used. The input to the subroutine consists of k different levels X_1, X_2, \dots, X_k of a stimulus applied to N_1, N_2, \dots, N_k objects with R_1, R_2, \dots, R_k responses respectively. The procedures described here assume that the distribution of critical values is normal. The computational steps are as follows:

1. Compute the proportions of objects responding to various levels of a stimulus:

$$p_i = \frac{R_i}{N_i} \quad (1)$$

where $i = 1, 2, \dots, k$ are levels of a stimulus.

2. Compute the initial estimates of a and b for the probit equation, $Y = a + bX$, as follows:

$$b = \frac{\sum_{i=1}^m X_i Z_i - \frac{\left(\sum_{i=1}^m X_i\right)\left(\sum_{i=1}^m Z_i\right)}{m}}{\sum_{i=1}^m X_i^2 - \frac{\left(\sum_{i=1}^m X_i\right)^2}{m}} \quad (2)$$

$$a = \bar{Z} - b\bar{X} \quad (3)$$

where X_i = ith level of a stimulus

Z_i = 5 plus the standard normal variable corresponding to p_i

m = number of p values which are not equal to 0.0 and 1.0

3. Compute values of expected probit using the initial estimates of a and b:

$$Y_i = a + bX_i \quad (4)$$

where $i = 1, 2, \dots, k$

4. Corresponding to each value of Y, compute the following:

a. Weighting coefficient for probit analysis:

$$W_i = \frac{D_i^2}{P_i Q_i} \quad (5)$$

where D_i = density of the normal curve corresponding to the standard normal variable $Y_i - 5$

P_i = cumulative normal distribution value corresponding to $Y_i - 5$

$$Q_i = 1 - P_i$$

b. Working probit:

For $Y_i \leq 5.0$

$$y_i = Y_i - \frac{P_i}{D_i} + p_i \frac{1}{D_i} \quad (6)$$

For $Y_i > 5.0$

$$y_i = Y_i + \frac{Q_i}{D_i} - (1-p_i) \frac{1}{D_i} \quad (7)$$

5. Compute:

$$S_1 = \sum_{i=1}^k N_i W_i X_i^2 - \frac{\left(\sum_{i=1}^k N_i W_i X_i\right)^2}{\sum_{i=1}^k N_i W_i} \quad (8)$$

$$S_2 = \sum_{i=1}^k N_i W_i X_i y_i - \frac{\left(\sum_{i=1}^k N_i W_i X_i\right)\left(\sum_{i=1}^k N_i W_i y_i\right)}{\sum_{i=1}^k N_i W_i} \quad (9)$$

$$S_3 = \sum_{i=1}^k N_i W_i y_i^2 - \frac{\left(\sum_{i=1}^k N_i W_i y_i\right)^2}{\sum_{i=1}^k N_i W_i} \quad (10)$$

6. Compute new estimates of a and b for the probit equation:

$$b = \frac{S_2}{S_1} \quad (11)$$

$$a = \frac{\sum_{i=1}^k N_i W_i y_i}{\sum_{i=1}^k N_i W_i} - b \cdot \frac{\sum_{i=1}^k N_i W_i X_i}{\sum_{i=1}^k N_i W_i} \quad (12)$$

C		PROB 880	C	COMPUTE WORKING PROBIT	PROB1550
C	COMPUTE PROPORTIONS OF OBJECTS RESPONDING	PROB 890	C		PROB1560
C		PROB 900	C	IF(Y=5.0) 35, 35, 40	PROB1570
16	DO 18 I=1,K	PROB 910	35	WP=(Y-P/Z)+W(I)/Z	PROB1580
	IF(S(I)-R(I)) 17,18,18	PROB 920	GO TO 45		PROB1590
17	IER=4	PROB 930	40	WP=(Y+Q/Z)-(1.0-W(I))/Z	PROB1600
	GO TO 90	PROB 940	C		PROB1610
18	CONTINUE	PROB 950	C	SUM INTERMEDIATE RESULTS	PROB1620
20	DO 23 I=1,K	PROB 960	C		PROB1630
	IF(S(I))21,21,22	PROB 970	45	WN=W*(S(I))	PROB1640
21	IER=3	PROB 980	SNW=SNW+WN		PROB1650
	GO TO 90	PROB 990	SNW=SNW+WN*X(I)		PROB1660
22	W(I)=R(I)/S(I)	PROB1000	SNWY=SNWY+WN*W		PROB1670
23	CONTINUE	PROB1010	SNWXX=SNWXX+WN*X(I)**2		PROB1680
C		PROB1020	50	SNWXY=SNWXY+WN*X(I)*W	PROB1690
C	COMPUTE INITIAL ESTIMATES OF INTERCEPT AND PROBIT REGRESSION	PROB1030	C		PROB1700
C	COEFFICIENT	PROB1040	C	COMPUTE NEW ESTIMATES OF INTERCEPT AND COEFFICIENT	PROB1710
C		PROB1050	C		PROB1720
	WN=0.0	PROB1060	C	XBAR=SNW/SNW	PROB1730
	XBAR=XBAR/WN	PROB1070	C		PROB1740
	SNWY=0.0	PROB1080	C	SXX=SNWXX-(SNW**2)/SNW	PROB1750
	SXX=0.0	PROB1090	C	SXY=SNWXY-(SNW*XBAR)	PROB1760
	SXY=0.0	PROB1100	C	B=SXY/SXX	PROB1770
C		PROB1110	C	A=SNWY/SNW-B*XBAR	PROB1780
DD	DO 30 I=1,K	PROB1120	C		PROB1790
	P=W(I)	PROB1130	C	EXAMINE THE CHANGES IN Y	PROB1800
	IF(P) 30, 30, 24	PROB1140	C		PROB1810
24	IF(P-1.0) 25, 30, 30	PROB1150	C		PROB1820
25	WN=WN+1.0	PROB1160	C	SXX=0.0	PROB1830
C		PROB1170	DO	DO 60 I=1,K	PROB1840
C	CALL NDTRI (P,Z,D,IER)	PROB1180	Y	Y=A+B*X(I)	PROB1850
	Z=Z*5.0	PROB1190	D	D=WZ(I)-Y	PROB1860
	XBAR=XBAR+X(I)	PROB1200	SXX	SXX=SXX+D*D	PROB1870
	SNWY=SNWY+Z	PROB1210	60	WZ(I)=Y	PROB1880
	SXX=SXX+X(I)**2	PROB1220	IF	IF(ABS(DO-SXX)-(1.0E-7)) 65, 65, 63	PROB1890
	SXY=SXY+X(I)*Z	PROB1230	63	DO=SXX	PROB1900
30	CONTINUE	PROB1240	GO	GO TO 33	PROB1910
C		PROB1250	C		PROB1920
C	B=(SXY-(XBAR*SNWY)/WN)/(SXX-(XBAR*XBAR)/WN)	PROB1260	C	STORE INTERCEPT AND COEFFICIENT	PROB1930
	XBAR=XBAR/WN	PROB1270	C		PROB1940
	SNWY=SNWY/WN	PROB1280	65	ANS(1)=A	PROB1950
	A=SNWY-B*XBAR	PROB1300	C	ANS(2)=B	PROB1960
	DO=0.0	PROB1310	C	COMPUTE CHI-SQUARE	PROB1970
C		PROB1320	C		PROB1980
C	COMPUTE EXPECTED PROBIT	PROB1330	C	ANS(3)=0.0	PROB1990
C		PROB1340	DO	DO TO I=1,K	PROB2000
DD	DO 31 I=1,K	PROB1350	Y	Y=WZ(I)-5.0	PROB2010
31	WZ(I)=A+B*X(I)	PROB1360	C		PROB2020
C		PROB1370	C	CALL NDTR (Y,P,0)	PROB2030
33	SNW=0.0	PROB1380	C		PROB2040
	SNWXX=0.0	PROB1390	AA	AA=P(I)-S(I)**P	PROB2050
	SNWY=0.0	PROB1400	DD	DD=S(I)**P*(1.0-P)	PROB2060
	SNWXX=0.0	PROB1410	70	ANS(3)=ANS(3)+AA*AA/DD	PROB2070
	SNWXY=0.0	PROB1420	C		PROB2080
	DO 50 I=1,K	PROB1430	C	DEGREES OF FREEDOM FOR CHI-SQUARE	PROB2090
	Y=WZ(I)	PROB1440	C		PROB2100
		PROB1450	C	ANS(4)=K-2	PROB2110
C		PROB1460	C		PROB2120
C	FIND A WEIGHTING COEFFICIENT FOR PROBIT ANALYSIS	PROB1470	80	RETURN	PROB2130
C		PROB1480	90	DO 100 I=1,K	PROB2140
C	D=Y-5.0	PROB1490	W	W(I)=0.0	PROB2150
C	CALL NDTF (D,P,Z)	PROB1500	100	WZ(I)=0.0	PROB2160
C		PROB1510	DO	DO 110 I=1,4	PROB2170
C	Q=1.0-P	PROB1520	ANS	ANS(I)=0.0	PROB2180
C	W=(Z*Z)/(P*Q)	PROB1530	GO	GO TO 80	PROB2190
C		PROB1540	END		PROB2200
					PROB2210

Canonical Correlation

In the Scientific Subroutine Package, canonical correlation analysis is normally performed by calling the following five subroutines:

1. CORRE - to compute means, standard deviations, and correlation matrix
2. MINV - to invert a part of the correlation matrix
3. EIGEN - to compute eigenvalues and eigenvectors
4. NROOT - to compute eigenvalues and eigenvectors of real nonsymmetric matrix of the form $B^{-1}A$
5. CANOR - to compute canonical correlations and coefficients

The subroutine CORRE works in either of two ways: (1) it expects all observations in core, or (2) it triggers a user-provided input subroutine, DATA, to read one observation at a time into a work area. In either case, the user must provide a subroutine named DATA (see "Subroutines Required" in the comment cards description of subroutine CORRE).

Subroutine CANOR

This subroutine performs a canonical correlation analysis between two sets of variables.

The matrix of intercorrelations, R , is partitioned into four submatrices:

$$R = \begin{bmatrix} R_{11} & R_{12} \\ R_{21} & R_{22} \end{bmatrix} \quad (1)$$

- R_{11} = intercorrelations among p variables in the first set (that is, left-hand variables)
- R_{12} = intercorrelations between the variables in the first and second sets
- R_{21} = the transpose of R_{12}
- R_{22} = intercorrelations among q variables in the second set (that is, right-hand variables)

The equation:

$$\begin{vmatrix} R_{22}^{-1} & R_{21}^{-1} & R_{12} & -\lambda I \end{vmatrix} = 0 \quad (2)$$

is then solved for all values of λ , eigenvalues, in the following matrix operation:

$$T = R_{11}^{-1} R_{12} \quad (3)$$

$$A = R_{21} T \quad (4)$$

The subroutine NROOT calculates eigenvalues (λ_i), with associated eigenvectors, of $R_{22}^{-1}A$, where $i = 1, 2, \dots, q$.

For each subscript $i = 1, 2, \dots, q$, the following statistics are calculated:

Canonical correlation:

$$\text{CANR} = \sqrt{\lambda_i} \quad (5)$$

where λ_i = i^{th} eigenvalue

Chi-square:

$$\chi^2 = - \left[n - 0.5(p + q + 1) \right] \log_e \Lambda \quad (6)$$

where n = number of observations

$$\Lambda = \prod_{j=1}^q (1 - \lambda_j)$$

Degrees of freedom for χ^2 :

$$\text{DF} = [p - (i - 1)] [q - (i - 1)] \quad (7)$$

i^{th} set of right-hand coefficients:

$$b_k = v_{ki} \quad (8)$$

where v_{ki} = eigenvector associated with λ_i

$$k = 1, 2, \dots, q;$$

i^{th} set of left-hand coefficients:

$$a_j = \frac{\sum_{k=1}^q t_{jk} b_k}{\text{CANR}} \quad (9)$$

where $\{t_{jk}\} = T = R_{11}^{-1} R_{12}$
 $j = 1, 2, \dots, p$

Design Analysis (see Smoothing, Regression, Factorization)

In the Scientific Subroutine Package, analysis of variance is normally performed by calling the following three subroutines in sequence:

1. AVDAT - to place data in properly distributed positions of storage
2. AVCAL - to apply the operators sigma and delta in order to compute deviates for analysis of variance
3. MEANQ - to pool the deviates and compute sums of squares, degrees of freedom, and mean squares

Subroutine AVDAT

This subroutine places data for analysis of variance in properly distributed positions of storage.

The size of data array X required for an analysis-of-variance problem is calculated as follows:

$$n = \prod_{i=1}^k (L_i + 1) \quad (1)$$

where L_i = number of levels of i^{th} factor

k = number of factors

The input data placed in the lower part of the array X are moved temporarily to the upper part of the array. From there, the data are redistributed according to the equation (4) below. Prior to that, multipliers, s_j , to be used in finding proper positions of storage, are calculated as follows:

$$s_1 = 1 \quad (2)$$

$$s_j = \prod_{i=1}^{j-1} (L_i + 1) \quad (3)$$

where $j = 2, 3, \dots, k$

Then a position for each data point is calculated by the following equation:

$$S = KOUNT_1 + \sum_{j=2}^k s_j \cdot (KOUNT_j - 1) \quad (4)$$

where $KOUNT_j$ = value of j^{th} subscript of the data to be stored.

The subroutine increments the value(s) of subscript(s) after each data point is stored.

```

C .....AVDA 10
C .....AVDA 20
C .....AVDA 30
C .....SUBROUTINE AVDAT .....AVDA 40
C .....PURPOSE .....AVDA 50
C .....AVDA 60
C .....PLACE DATA FOR ANALYSIS OF VARIANCE IN PROPERLY DISTRIBUTED .....AVDA 70
C .....POSITIONS OF STORAGE. THIS SUBROUTINE IS NORMALLY FOLLOWED .....AVDA 80
C .....BY CALLS TO AVCAL AND MEANQ SUBROUTINES IN THE PERFORMANCE .....AVDA 90
C .....OF ANALYSIS OF VARIANCE FOR A COMPLETE FACTORIAL DESIGN. .....AVDA 100
C .....AVDA 110
C .....USAGE .....AVDA 120
C .....CALL AVDAT (K,LEVEL,N,X,L,ISTEP,KOUNT) .....AVDA 130
C .....AVDA 140
C .....DESCRIPTION OF PARAMETERS .....AVDA 150
C .....K - NUMBER OF VARIABLES (FACTORS). K MUST BE .GT. ONE. .....AVDA 160
C .....LEVEL - INPUT VECTOR OF LENGTH K CONTAINING LEVELS (CATE- .....AVDA 170
C .....GORIES) WITHIN EACH VARIABLE. .....AVDA 180
C .....N - TOTAL NUMBER OF DATA POINTS READ IN. .....AVDA 190
C .....X - WHEN THE SUBROUTINE IS CALLED, THIS VECTOR CONTAINS .....AVDA 200
C .....DATA IN LOCATIONS X(1) THROUGH X(N). UPON RETURNING .....AVDA 210
C .....TO THE CALLING ROUTINE, THE VECTOR CONTAINS THE DATA .....AVDA 220
C .....IN PROPERLY REDISTRIBUTED LOCATIONS OF VECTOR X. .....AVDA 230
C .....THE LENGTH OF VECTOR X IS CALCULATED BY (1) ADDING .....AVDA 240
C .....ONE TO EACH LEVEL OF VARIABLE AND (2) OBTAINING THE .....AVDA 250
C .....CUMULATIVE PRODUCT OF ALL LEVELS. (THE LENGTH OF .....AVDA 260
C .....X = (LEVEL(1)+1)*(LEVEL(2)+1)*...*(LEVEL(K)+1).) .....AVDA 270
C .....L - OUTPUT VARIABLE CONTAINING THE POSITION IN VECTOR X .....AVDA 280
C .....WHERE THE LAST INPUT DATA IS STORED. .....AVDA 290
C .....ISTEP - OUTPUT VECTOR OF LENGTH K CONTAINING CONTROL STEPS .....AVDA 300
C .....WHICH ARE USED TO LOCATE DATA IN PROPER POSITIONS .....AVDA 310
C .....OF VECTOR X. .....AVDA 320
C .....KOUNT - WORKING VECTOR OF LENGTH K. .....AVDA 330
C .....AVDA 340
C .....REMARKS .....AVDA 350
C .....INPUT DATA MUST BE ARRANGED IN THE FOLLOWING MANNER. .....AVDA 360
C .....CONSIDER THE J-VARIABLE ANALYSIS OF VARIANCE DESIGN, WHERE .....AVDA 370
C .....ONE VARIABLE HAS 3 LEVELS AND THE OTHER TWO VARIABLES HAVE .....AVDA 380
C .....2 LEVELS. THE DATA MAY BE REPRESENTED IN THE FORM X(I,J,K) .....AVDA 390
C .....I=1,2,3 J=1,2 K=1,2. IN ARRANGING DATA, THE INNER .....AVDA 400
C .....SUBSCRIPT, NAMELY I, CHANGES FIRST. WHEN I=3, THE NEXT .....AVDA 410
C .....INNER SUBSCRIPT, J, CHANGES AND SO ON UNTIL I=3, J=2, AND .....AVDA 420
C .....K=2. .....AVDA 430
C .....AVDA 440
C .....SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED .....AVDA 450
C .....NONE .....AVDA 460
C .....AVDA 470
C .....METHOD .....AVDA 480
C .....THE METHOD IS BASED ON THE TECHNIQUE DISCUSSED BY H. G. .....AVDA 490
C .....HARTLEY IN "MATHEMATICAL METHODS FOR DIGITAL COMPUTERS", .....AVDA 500
C .....EDITED BY A. RALSTON AND H. WILF, JOHN WILEY AND SONS, .....AVDA 510
C .....1962, CHAPTER 20. .....AVDA 520
C .....AVDA 530
C .....AVDA 540
C .....SUBROUTINE AVDAT (K,LEVEL,N,X,L,ISTEP,KOUNT) .....AVDA 550
C .....DIMENSION LEVEL(1),X(1),ISTEP(1),KOUNT(1) .....AVDA 560
C .....AVDA 570
C .....AVDA 580
C .....AVDA 590
C .....AVDA 600
C .....IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE .....AVDA 610
C .....C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION .....AVDA 620
C .....STATEMENT WHICH FOLLOWS. .....AVDA 630
C .....AVDA 640
C .....DOUBLE PRECISION X .....AVDA 650
C .....AVDA 660
C .....THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS .....AVDA 670
C .....APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS .....AVDA 680
C .....ROUTINE. .....AVDA 690
C .....AVDA 700
C .....AVDA 710
C .....AVDA 720
C .....CALCULATE TOTAL DATA AREA REQUIRED .....AVDA 730
C .....AVDA 740
C .....M=LEVEL(1)+1 .....AVDA 750
C .....DO 105 I=2,K .....AVDA 760
C 105 M=M*(LEVEL(I)+1) .....AVDA 770
C .....AVDA 780
C .....MOVE DATA TO THE UPPER PART OF THE ARRAY X .....AVDA 790
C .....FOR THE PURPOSE OF REARRANGEMENT .....AVDA 800
C .....AVDA 810
C .....N1=M+1 .....AVDA 820
C .....N2=N+1 .....AVDA 830
C .....DO 107 I=1,N .....AVDA 840
C .....N1=N1-1 .....AVDA 850
C .....N2=N2-1 .....AVDA 860
C 107 X(N1)=X(N2) .....AVDA 870
C .....AVDA 880
C .....CALCULATE MULTIPLIERS TO BE USED IN FINDING STORAGE LOCATIONS FOR .....AVDA 890
C .....INPUT DATA .....AVDA 900
C .....AVDA 910
C .....ISTEP(1)=1 .....AVDA 920
C .....DO 110 I=2,K .....AVDA 930
C 110 ISTEP(I)=ISTEP(I-1)*(LEVEL(I-1)+1) .....AVDA 940
C .....AVDA 950
C 115 KOUNT(1)=1 .....AVDA 960
C .....AVDA 970
C .....PLACE DATA IN PROPER LOCATIONS .....AVDA 980
C .....AVDA 990
C .....N1=N1-1 .....AVDA1000
C .....DO 125 I=1,N .....AVDA1010
C .....L=KOUNT(I) .....AVDA1020
C .....DO 123 J=2,K .....AVDA1030
C 120 L=L+ISTEP(J)*(KOUNT(J)-1) .....AVDA1040
C .....AVDA1050
C .....X(I)=X(N) .....AVDA1060
C .....DO 124 J=1,K .....AVDA1070
C .....IF (KOUNT(J)-LEVEL(J)) 124, 125, 124 .....AVDA1080
C 124 KOUNT(J)=KOUNT(J)+1 .....AVDA1090
C .....AVDA1100
C .....GO TO 125 .....AVDA1110
C 125 KOUNT(J)=1 .....AVDA1120
C 130 CONTINUE .....AVDA1130
C 135 CONTINUE .....AVDA1140
C .....RETURN .....AVDA1150
C .....END .....AVDA1150

```

Subroutine AVCAL

This subroutine performs the calculus for the general k -factor experiment: operator Σ and operator Δ . An example is presented in terms of $k=3$ to illustrate these operators.

Let x_{abc} denote the experimental reading from the a^{th} level of factor A, the b^{th} level of factor B, and the c^{th} level of factor C. The symbols A, B, and C will also denote the number of levels for each factor so that $a = 1, 2, \dots, A$; $b = 1, 2, \dots, B$; and $c = 1, 2, \dots, C$.

With regard to the first factor A:

operator $\sum_a \equiv$ sum over all levels $a = 1, 2, \dots, A$, holding the other subscripts at constant levels, and

operator $\Delta_a \equiv$ multiply all items by A and subtract the result of \sum_a from all items

In mathematical notation, these operators are defined as follows:

$$\sum_a x_{abc} \equiv X_{.bc} \equiv \sum_{a=1}^A x_{abc} \quad (1)$$

$$\Delta_a x_{abc} \equiv A x_{abc} - X_{.bc} \quad (2)$$

The operators Σ and Δ will be applied sequentially to all factors A, B, and C. Upon the completion of these operations, the storage array X contains deviates to be used for analysis-of-variance components in the subroutine MEANQ.

```

C ..... AVCA 10
C ..... AVCA 20
C ..... AVCA 30
C SUBROUTINE AVCAL AVCA 40
C ..... AVCA 50
C PURPOSE AVCA 60
C PERFORM THE CALCULUS OF A FACTORIAL EXPERIMENT USING AVCA 70
C OPERATOR SIGMA AND OPERATOR DELTA. THIS SUBROUTINE IS AVCA 80
C PRECEDED BY SUBROUTINE AVDAT AND FOLLOWED BY SUBROUTINE AVCA 90
C MEANQ IN THE PERFORMANCE OF ANALYSIS OF VARIANCE FOR A AVCA 100
C COMPLETE FACTORIAL DESIGN. AVCA 110
C ..... AVCA 120
C USAGE AVCA 130
C CALL AVCAL (K,LEVEL,X,L,ISTEP,LASTS) AVCA 140
C ..... AVCA 150
C DESCRIPTION OF PARAMETERS AVCA 160
C K - NUMBER OF VARIABLES (FACTORS). K MUST BE .GT. ONE. AVCA 170
C LEVEL - INPUT VECTOR OF LENGTH K CONTAINING LEVELS (CATE- AVCA 180
C GORIES) WITHIN EACH VARIABLE. AVCA 190
C X - INPUT VECTOR CONTAINING DATA. DATA HAVE BEEN PLACED AVCA 200
C IN VECTOR X BY SUBROUTINE AVDAT. THE LENGTH OF X AVCA 210
C IS (LEVEL(1)+1)*(LEVEL(2)+1)*...*(LEVEL(K)+1). AVCA 220
C L - THE POSITION IN VECTOR K WHERE THE LAST INPUT DATA AVCA 230
C IS LOCATED. L HAS BEEN CALCULATED BY SUBROUTINE AVCA 240
C AVDAT. AVCA 250
C ISTEP - INPUT VECTOR OF LENGTH K CONTAINING STORAGE CONTROL AVCA 260
C STEPS WHICH HAVE BEEN CALCULATED BY SUBROUTINE AVCA 270
C AVDAT. AVCA 280
C LASTS - WORKING VECTOR OF LENGTH K. AVCA 290
C ..... AVCA 300
C REMARKS AVCA 310
C THIS SUBROUTINE MUST FOLLOW SUBROUTINE AVDAT. AVCA 320
C ..... AVCA 330
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED AVCA 340
C NONE AVCA 350
C ..... AVCA 360
C METHOD AVCA 370
C THE METHOD IS BASED ON THE TECHNIQUE DISCUSSED BY H. O. AVCA 380
C HARTLEY IN "MATHEMATICAL METHODS FOR DIGITAL COMPUTERS", AVCA 390
C EDITED BY A. AALSTON AND H. WILF, JOHN WILEY AND SONS, AVCA 400
C 1962, CHAPTER 20. AVCA 410
C ..... AVCA 420
C ..... AVCA 430
C SUBROUTINE AVCAL (K,LEVEL,X,L,ISTEP,LASTS) AVCA 440
C DIMENSION LEVEL(1),X(1),ISTEP(1),LASTS(1) AVCA 450
C ..... AVCA 460
C ..... AVCA 470
C ..... AVCA 480
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE AVCA 500
C C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION AVCA 510
C STATEMENT WHICH FOLLOWS. AVCA 520
C ..... AVCA 530
C DOUBLE PRECISION X,SUM AVCA 540
C ..... AVCA 550
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS AVCA 560
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS AVCA 570
C ROUTINE. AVCA 580
C ..... AVCA 590
C ..... AVCA 600
C ..... AVCA 610
C CALCULATE THE LAST DATA POSITION OF EACH FACTOR AVCA 620
C ..... AVCA 630
C LASTS(1)=L+1 AVCA 640
C DO 145 I=2,K AVCA 650
C 145 LASTS(I)=LASTS(I-1)+ISTEP(I) AVCA 660
C ..... AVCA 670
C PERFORM CALCULUS OF OPERATION AVCA 680
C ..... AVCA 690
C 150 DO 175 I=1,K AVCA 700
C L=L AVCA 710
C LL=L AVCA 720
C SUM=0.0 AVCA 730
C NN=LEVEL(I) AVCA 740
C FN=NN AVCA 750
C INCN=ISTEP(I) AVCA 760
C LAST=LASTS(I) AVCA 770
C ..... AVCA 780
C SIGMA OPERATION AVCA 790
C ..... AVCA 800
C 155 DO 160 J=1,NN AVCA 810
C SUM=SUM+X(I) AVCA 820
C 160 L=L+INCR AVCA 830
C X(LL)=SUM AVCA 840
C ..... AVCA 850
C DELTA OPERATION AVCA 860
C ..... AVCA 870
C DO 165 J=1,NN AVCA 880
C X(LL)=FN*X(LL)-SUM AVCA 890
C 165 LL=LL+INCR AVCA 900
C SUM=0.0 AVCA 910
C IF(LL-LAST) 167, 175, 175 AVCA 920
C 167 IF(LL-LAST+INCR) 168, 166, 170 AVCA 930
C 168 L=L+INCR AVCA 940
C LL=LL+INCR AVCA 950
C 170 L=L+INCR+1-LAST AVCA 960
C LL=LL+INCR+1-LAST AVCA 970
C GO TO 155 AVCA 980
C 175 CONTINUE AVCA 990
C RETURN AVCA 1000
C END AVCA 1010

```

Subroutine MEANQ

This subroutine performs the mean square operation for the general k-factor experiment in the following two steps:

1. Square each value of deviates for analysis of variance stored in the array X (the result of the operators Σ and Δ applied in the subroutine AVCAL).

2. Add the squared value into summation storage. In a three-factor experiment, for example, the squared value is added into one of seven storages ($7 = 2^3 - 1$) as shown in the first column of Table 1. The symbols A, B, and C in the first column denote factor A, factor B, and factor C.

After the mean square operation is completed for all values in the storage array X, the subroutine forms sums of squares of analysis of variance by dividing the totals of squared values by proper divisors. These divisors for the three-factor experiment mentioned above are shown in the second column of Table 1. The symbols A, B, and C in the second column denote the number of levels for each factor.

The subroutine, then, forms mean squares by dividing sums of squares by degrees of freedom. The third column of the summary table shows the degrees of freedom. The symbols A, B, and C denote the number of levels for each factor.

Table 1. Table Showing Summation Storages, Divisors to Form Sum of Squares, and Degrees of Freedom (Subroutine MEANQ)

Designation of Store and of Quantity Contained in it	Divisor Required to Form Sum of Squares of Analysis of Variance	Degrees of Freedom Required to Form Mean Squares
(A) ²	ABC·A	(A-1)
(B) ²	ABC·B	(B-1)
(AB) ²	ABC·AB	(A-1)(B-1)
(C) ²	ABC·C	(C-1)
(AC) ²	ABC·AC	(A-1)(C-1)
(BC) ²	ABC·BC	(B-1)(C-1)
(ABC) ²	ABC·ABC	(A-1)(B-1)(C-1)

```

C ..... MEAN 10
C ..... MEAN 20
C ..... MEAN 30
C ..... MEAN 40
C ..... MEAN 50
C ..... MEAN 60
C ..... MEAN 70
C ..... MEAN 80
C ..... MEAN 90
C ..... MEAN 100
C ..... MEAN 110
C ..... MEAN 120
C ..... MEAN 130
C ..... MEAN 140
C ..... MEAN 150
C ..... MEAN 160
C ..... MEAN 170
C ..... MEAN 180
C ..... MEAN 190
C ..... MEAN 200
C ..... MEAN 210
C ..... MEAN 220
C ..... MEAN 230
C ..... MEAN 240
C ..... MEAN 250
C ..... MEAN 260
C ..... MEAN 270
C ..... MEAN 280
C ..... MEAN 290
C ..... MEAN 300
C ..... MEAN 310
C ..... MEAN 320
C ..... MEAN 330
C ..... MEAN 340
C ..... MEAN 350
C ..... MEAN 360
C ..... MEAN 370
C ..... MEAN 380
C ..... MEAN 390
C ..... MEAN 400
C ..... MEAN 410
C ..... MEAN 420
C ..... MEAN 430
C ..... MEAN 440
C ..... MEAN 450
C ..... MEAN 460
C ..... MEAN 470
C ..... MEAN 480
C ..... MEAN 490
C ..... MEAN 500
C ..... MEAN 510
C ..... MEAN 520
C ..... MEAN 530
C ..... MEAN 540
C ..... MEAN 550
C ..... MEAN 560
C ..... MEAN 570
C ..... MEAN 580
C ..... MEAN 590
C ..... MEAN 600
C ..... MEAN 610
C ..... MEAN 620
C ..... MEAN 630
C ..... MEAN 640
C ..... MEAN 650
C ..... MEAN 660
C ..... MEAN 670
C ..... MEAN 680
C ..... MEAN 690
C ..... MEAN 700
C ..... MEAN 710
C ..... MEAN 720
C ..... MEAN 730
C ..... MEAN 740
C ..... MEAN 750
C ..... MEAN 760
C ..... MEAN 770
C ..... MEAN 780
C ..... MEAN 790
C ..... MEAN 800
C ..... MEAN 810
C ..... MEAN 820
C ..... MEAN 830
C ..... MEAN 840
C ..... MEAN 850
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C ..... MEAN1000
C ..... MEAN1010
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C ..... MEAN1060
C ..... MEAN1070
C ..... MEAN1080
C ..... MEAN1090
C ..... MEAN1100
C ..... MEAN1110
C ..... MEAN1120
C ..... MEAN1130
C ..... MEAN1140
C ..... MEAN1150
C ..... MEAN1160
C ..... MEAN1170
C ..... MEAN1180
C ..... MEAN1190
C ..... MEAN1200
C ..... MEAN1210
C ..... MEAN1220
C ..... MEAN1230
C ..... MEAN1240
C ..... MEAN1250
C ..... MEAN1260
C ..... MEAN1270
C ..... MEAN1280
C ..... MEAN1290

```

```

330 N01=N01*LEVEL111
    N02=N02*LEVEL111-L1
340 CONTINUE
    FN1=N*N01
    FN2=N*N02
    NN=NN+1
    SUMSQ(MN)=SUMSQ(MN)/FN1
    NDF(MN)=N02
    S(MEAN(MN)=SUMSQ(MN)/FN2
    IF(MN=LL) 345, 370, 370
345 JJ=360 I=1,K
    IF(MSTEP11) 347, 350, 347
347 MSTEP11=0
    GO TO 340
350 MSTEP11=1
    GO TO 320
360 CONTINUE
370 RETURN
    END

```

```

MEAN1300
MEAN1310
MEAN1320
MEAN1330
MEAN1340
MEAN1350
MEAN1360
MEAN1370
MEAN1380
MEAN1390
MEAN1400
MEAN1410
MEAN1420
MEAN1430
MEAN1440
MEAN1450
MEAN1460
MEAN1470
MEAN1480

```

Discriminant Analysis

In the Scientific Subroutine Package, discriminant analysis is normally performed by calling the following three subroutines in sequence:

1. DMATX - to compute means of variables in each group and a pooled dispersion matrix
2. MINV - to invert the pooled dispersion matrix
3. DISCR - to compute coefficients of discriminant functions and evaluate the functions for each observation (individual)

Subroutine DMATX

This subroutine calculates means of variables in each group and a pooled dispersion matrix for the set of groups in a discriminant analysis.

For each group $k = 1, 2, \dots, g$, the subroutine calculates means and sums of cross-products of deviations from means as shown below.

Means:

$$\bar{x}_{jk} = \frac{\sum_{i=1}^{n_k} x_{ijk}}{n_k} \quad (1)$$

where n_k = sample size in the k^{th} group
 $j = 1, 2, \dots, m$ are variables

Sum of cross-products of deviations from means:

$$S_k = \left\{ \begin{matrix} s_{jk} \\ s_{\ell k} \end{matrix} \right\} = \sum (x_{ijk} - \bar{x}_{jk}) (x_{i\ell k} - \bar{x}_{\ell k}) \quad (2)$$

where $j = 1, 2, \dots, m$

$\ell = 1, 2, \dots, m$

The pooled dispersion matrix is calculated as follows:

$$D = \frac{\sum_{k=1}^g S_k}{\sum_{k=1}^g n_k - g} \quad (3)$$

where g = number of groups


```

C .....DMAT 10
C .....DMAT 20
C .....DMAT 30
C .....DMAT 40
C .....DMAT 50
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C .....DMAT 80
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C .....DMAT 140
C .....DMAT 150
C .....DMAT 160
C .....DMAT 170
C .....DMAT 180
C .....DMAT 190
C .....DMAT 200
C .....DMAT 210
C .....DMAT 220
C .....DMAT 230
C .....DMAT 240
C .....DMAT 250
C .....DMAT 260
C .....DMAT 270
C .....DMAT 280
C .....DMAT 290
C .....DMAT 300
C .....DMAT 310
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C .....DMAT 340
C .....DMAT 350
C .....DMAT 360
C .....DMAT 370
C .....DMAT 380
C .....DMAT 390
C .....DMAT 400
C .....DMAT 410
C .....DMAT 420
C .....DMAT 430
C .....DMAT 440
C .....DMAT 450
C .....DMAT 460
C .....DMAT 470
C .....DMAT 480
C .....DMAT 490
C .....DMAT 500
C .....DMAT 510
C .....DMAT 520
C .....DMAT 530
C .....DMAT 540
C .....DMAT 550
C .....DMAT 560
C .....DMAT 570
C .....DMAT 580
C .....DMAT 590
C .....DMAT 600
C .....DMAT 610
C .....DMAT 620
C .....DMAT 630
C .....DMAT 640
C .....DMAT 650
C .....DMAT 660
C .....DMAT 670
C .....DMAT 680
C .....DMAT 690
C .....DMAT 700
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C .....DMAT 770
C .....DMAT 780
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C .....DMAT 1120
C .....DMAT 1130
C .....DMAT 1140
C .....DMAT 1150
C .....DMAT 1160
C .....DMAT 1170
C .....DMAT 1180
C .....DMAT 1190
C .....DMAT 1200
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C .....DMAT 1870
C .....DMAT 1880
C .....DMAT 1890
C .....DMAT 1900
C .....DMAT 1910
C .....DMAT 1920
C .....DMAT 1930
C .....DMAT 1940
C .....DMAT 1950
C .....DMAT 1960
C .....DMAT 1970
C .....DMAT 1980
C .....DMAT 1990
C .....DMAT 2000

```

Subroutine DISCR

This subroutine performs a discriminant analysis by calculating a set of linear functions that serve as indices for classifying an individual into one of K groups.

For all groups combined, the following are obtained.

Common means:

$$\bar{x}_j = \frac{\sum_{k=1}^g n_k \bar{x}_{jk}}{\sum_{k=1}^g n_k} \tag{1}$$

- where g = number of groups
- j = 1, 2, ..., m are variables
- n_k = sample size in the kth group
- \bar{x}_{jk} = mean of jth variable in kth group

Generalized Mahalanobis D² statistics, V:

$$V = \sum_{i=1}^m \sum_{j=1}^m d_{ij} \sum_{k=1}^g n_k (\bar{x}_{ik} - \bar{x}_i) (\bar{x}_{jk} - \bar{x}_j) \tag{2}$$

where d_{ij} = the inverse element of the pooled dispersion matrix D

V can be used as chi-square (under assumption of normality) with m(g-1) degrees of freedom, to test the hypothesis that the mean values are the same in all the g groups for these m variables. For each discriminant function k* = 1, 2, ..., g, the following statistics are calculated.

Coefficients:

$$C_{ik*} = \sum_{j=1}^m d_{ij} \bar{x}_{jk} \tag{3}$$

where i = 1, 2, ..., m
k = k*

Constant:

$$C_{ok*} = -1/2 \sum_{j=1}^m \sum_{l=1}^m d_{jl} \bar{x}_{jk} \bar{x}_{lk} \tag{4}$$

For each i^{th} case in each k^{th} group, the following calculations are performed.

Discriminant functions:

$$f_{k*} = \sum_{j=1}^m C_{jk} x_{ijk} + C_{ok*} \quad (5)$$

where $k* = 1, 2, \dots, g$

Probability associated with largest discriminant function:

$$P_L = \frac{1}{\sum_{k*=1}^g e^{(f_{k*} - f_L)}} \quad (6)$$

where f_L = the value of the largest discriminant function

L = the subscript of the largest discriminant function

C	DISC 10
C	DISC 20
C	DISC 30
C	DISC 40
C	DISC 50
C	DISC 60
C	DISC 70
C	DISC 80
C	DISC 90
C	DISC 100
C	DISC 110
C	DISC 120
C	DISC 130
C	DISC 140
C	DISC 150
C	DISC 160
C	DISC 170
C	DISC 180
C	DISC 190
C	DISC 200
C	DISC 210
C	DISC 220
C	DISC 230
C	DISC 240
C	DISC 250
C	DISC 260
C	DISC 270
C	DISC 280
C	DISC 290
C	DISC 300
C	DISC 310
C	DISC 320
C	DISC 330
C	DISC 340
C	DISC 350
C	DISC 360
C	DISC 370
C	DISC 380
C	DISC 390
C	DISC 400
C	DISC 410
C	DISC 420
C	DISC 430
C	DISC 440
C	DISC 450
C	DISC 460
C	DISC 470
C	DISC 480
C	DISC 490
C	DISC 500
C	DISC 510
C	DISC 520
C	DISC 530
C	DISC 540
C	DISC 550
C	DISC 560
C	DISC 570
C	DISC 580
C	DISC 590
C	DISC 600
C	DISC 610
C	DISC 620
C	DISC 630

```

C .....DISC 640
C .....DISC 650
SUBROUTINE DISCR (K,M,N,X,KBAR,D,CMEAN,V,C,P,LG)
DIMENSION N(1),X(1),KBAR(1),D(1),CMEAN(1),C(1),P(1),LG(1)
C .....DISC 660
C .....DISC 670
C .....DISC 680
C .....DISC 690
C .....DISC 700
C .....DISC 710
C .....DISC 720
C .....DISC 730
C .....DISC 740
C .....DISC 750
C .....DISC 760
C .....DISC 770
C .....DISC 780
C .....DISC 790
C .....DISC 800
C .....DISC 810
C .....DISC 820
C .....DISC 830
C .....DISC 840
C .....DISC 850
C .....DISC 860
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C .....DISC 930
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C .....DISC 950
C .....DISC 960
C .....DISC 970
C .....DISC 980
C .....DISC 990
C .....DISC1000
C .....DISC1010
C .....DISC1020
C .....DISC1030
C .....DISC1040
C .....DISC1050
C .....DISC1060
C .....DISC1070
C .....DISC1080
C .....DISC1090
C .....DISC1100
C .....DISC1110
C .....DISC1120
C .....DISC1130
C .....DISC1140
C .....DISC1150
C .....DISC1160
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C .....DISC1180
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C .....DISC1600
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C .....DISC1680
C .....DISC1690
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C .....DISC1730
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C .....DISC1750
C .....DISC1760
C .....DISC1770
C .....DISC1780
C .....DISC1790
C .....DISC1800
C .....DISC1810
C .....DISC1820
C .....DISC1830
C .....DISC1840
C .....DISC1850
C .....DISC1860
C .....DISC1870
C .....DISC1880
C .....DISC1890
C .....DISC1900

```

Factor Analysis (see Eigenanalysis)

In the Scientific Subroutine Package, factor analysis is normally performed by calling the following five subroutines in sequence:

1. CORRE - to find means, standard deviations, and correlation matrix
2. EIGEN - to compute eigenvalues and associated eigenvectors of the correlation matrix
3. TRACE - to select the eigenvalues that are greater than or equal to the control value specified by the user
4. LOAD - to compute a factor matrix
5. VARMX - to perform varimax rotation of the factor matrix

The subroutine CORRE works in either of two ways: (1) it expects all observations in core, or (2) it triggers a user-provided input subroutine, DATA, to read one observation at a time into a work area. In either case, the user must provide a subroutine named DATA (see "Subroutines Required" in the comment cards designation of subroutine CORRE).

Subroutine TRACE

This subroutine finds k, the number of eigenvalues that are greater than or equal to the value of a specified constant. The given eigenvalues $\lambda_1, \lambda_2, \dots, \lambda_m$ must be arranged in descending order.

Cumulative percentages for these k eigenvalues are:

$$d_j = \sum_{i=1}^j \frac{\lambda_i}{m} \quad (1)$$

where $j = 1, 2, \dots, k$

$m =$ number of eigenvalues (or variables)

$k \leq m$

```

C
C
C -----
C SUBROUTINE TRACE
C
C PURPOSE
C   COMPUTE CUMULATIVE PERCENTAGE OF EIGENVALUES GREATER THAN
C   OR EQUAL TO A CONSTANT SPECIFIED BY THE USER. THIS SUB-
C   ROUTINE NORMALLY OCCURS IN A SEQUENCE OF CALLS TO SUB-
C   ROUTINES CORRE, EIGEN, TRACE, LCAID, AND VARMX IN THE PER-
C   FORMANCE OF A FACTOR ANALYSIS.
C
C USAGE
C   CALL TRACE (M,R,CCN,K,D)
C
C DESCRIPTION OF PARAMETERS
C   M - NUMBER OF VARIABLES. M MUST BE > OR = TO 1
C   R - INPUT MATRIX (SYMMETRIC AND STORED IN COMPRESSED
C   FORM WITH ONLY LOWER TRIANGLE BY COLUMN IN CORE)
C   CCN - CONSTANT USED TO DECIDE HOW MANY EIGENVALUES TO
C   RETAIN. CUMULATIVE PERCENTAGE OF EIGENVALUES
C   WHICH ARE GREATER THAN OR EQUAL TO THIS VALUE IS
C   CALCULATED.
C   K - CUTOFF VARIABLE CONTAINING THE NUMBER OF EIGENVALUES
C   GREATER THAN OR EQUAL TO CCN. (K IS THE NUMBER OF
C   FACTORS.)
C   D - CUTOFF VECTOR OF LENGTH M CONTAINING CUMULATIVE
C   PERCENTAGE OF EIGENVALUES WHICH ARE GREATER THAN
C   OR EQUAL TO CCN.
C
C REMARKS
C   NONE
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C   NONE
C
C METHOD
C   EACH EIGENVALUE GREATER THAN OR EQUAL TO CCN IS DIVIDED BY
C   AND THE RESULT IS ADDED TO THE PREVIOUS TOTAL TO OBTAIN
C   THE CUMULATIVE PERCENTAGE FOR EACH EIGENVALUE.
C
C -----
C
C SUBROUTINE TRACE (M,R,CCN,K,D)
C   DIMENSION R(1),D(1)
C
C   IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE
C   C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION
C   STATEMENT WHICH FOLLOWS.
C
C   DOUBLE PRECISION R,D
C
C   THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS
C   APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS
C   ROUTINE.
C
C -----
C
C   FM=1
C   LC=C
C   CC 100 I=1,M
C   L=L+1
C100 C(I)=R(I)
C   K=C
C
C   TEST WHETHER 1-TH EIGENVALUE IS GREATER
C   THAN OR EQUAL TO THE CONSTANT
C
C   CC 110 I=1,M
C   IF(C(I)-CCN) 120, 105, 105
C105 R=R+1
C110 C(I)=C(I)/FM
C
C   COMPUTE CUMULATIVE PERCENTAGE OF EIGENVALUES
C
C120 CC 120 I=2,M
C130 C(I)=C(I)+C(I-1)
C   RETURN
C   END
C
C TRAC 10
C TRAC 20
C TRAC 30
C TRAC 40
C TRAC 50
C TRAC 60
C TRAC 70
C TRAC 80
C TRAC 90
C TRAC 100
C TRAC 110
C TRAC 120
C TRAC 130
C TRAC 140
C TRAC 150
C TRAC 160
C TRAC 170
C TRAC 180
C TRAC 190
C TRAC 200
C TRAC 210
C TRAC 220
C TRAC 230
C TRAC 240
C TRAC 250
C TRAC 260
C TRAC 270
C TRAC 280
C TRAC 290
C TRAC 300
C TRAC 310
C TRAC 320
C TRAC 330
C TRAC 340
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C TRAC 360
C TRAC 370
C TRAC 380
C TRAC 390
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C TRAC 420
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C TRAC 630
C TRAC 640
C TRAC 650
C TRAC 660
C TRAC 670
C TRAC 680
C TRAC 690
C TRAC 700
C TRAC 710
C TRAC 720
C TRAC 730
C TRAC 740
C TRAC 750
C TRAC 760
C TRAC 770
C TRAC 780
C TRAC 790
C TRAC 800
C TRAC 810
C TRAC 820
C TRAC 830
C TRAC 840

```


Assuming that x and y are factors to be rotated, where x is the lower-numbered or left-hand factor, the following notation for rotating these two factors is used:

$$\begin{bmatrix} x_1 & y_1 \\ x_2 & y_2 \\ \cdot & \cdot \\ \cdot & \cdot \\ \cdot & \cdot \\ x_m & y_m \end{bmatrix} \cdot \begin{bmatrix} \cos\phi & -\sin\phi \\ \sin\phi & \cos\phi \end{bmatrix} = \begin{bmatrix} X_1 & Y_1 \\ X_2 & Y_2 \\ \cdot & \cdot \\ \cdot & \cdot \\ \cdot & \cdot \\ X_m & Y_m \end{bmatrix} \quad (6)$$

where x_i and y_i are presently available normalized loadings, and X_i and Y_i , the desired normalized loadings, are functions of ϕ , the angle of rotation. The computational steps are (a) through (e) below.

(a) Calculation of NUM and DEN:

$$A = \sum_i (x_i + y_i) (x_i - y_i)$$

$$B = 2 \sum_i x_i y_i$$

$$C = \sum_i \left[(x_i + y_i) (x_i - y_i) + 2x_i y_i \right] \\ \left[(x_i + y_i) (x_i - y_i) - 2x_i y_i \right]$$

$$D = 4 \sum_i (x_i + y_i) (x_i - y_i) x_i y_i \quad (7)$$

$$\text{NUM} = D - 2AB/m$$

$$\text{DEN} = C - [(A + B)(A - B)]/m$$

(b) Comparison of NUM and DEN:

The following four cases may arise.

NUM < DEN, go to (b1) below

NUM > DEN, go to (b2) below

(NUM + DEN) $\geq \epsilon^*$, go to (b3) below

(NUM + DEN) < ϵ , skip to the next rotation

* ϵ is a small tolerance factor.

$$(b1) \quad \tan 4\theta = |\text{NUM}|/|\text{DEN}| \quad (8)$$

If $\tan 4\theta < \epsilon$ and

(i) DEN is positive, skip to the next rotation.

(ii) DEN is negative, set $\cos\phi = \sin\phi = (\sqrt{2})/2$ and go to (e) below.

If $\tan 4\theta \geq \epsilon$, calculate:

$$\cos 4\theta = 1/\sqrt{1 + \tan^2 4\theta} \quad (9)$$

$$\sin 4\theta = \tan 4\theta \cdot \cos 4\theta \quad (10)$$

and go to (c) below.

$$(b2) \quad \text{ctn} 4\theta = |\text{NUM}|/|\text{DEN}| \quad (11)$$

If $\text{ctn} 4\theta < \epsilon$, set $\cos 4\theta = 0$ and $\sin 4\theta = 1$. Go to (c) below.

If $\text{ctn} 4\theta \geq \epsilon$, calculate:

$$\sin 4\theta = 1/\sqrt{1 + \text{ctn}^2 4\theta} \quad (12)$$

$$\cos 4\theta = \text{ctn} 4\theta \cdot \sin 4\theta \quad (13)$$

and go to (c) below.

(b3) Set $\cos 4\theta = \sin 4\theta = (\sqrt{2})/2$ and go to (c) below.

(c) Determining $\cos\theta$ and $\sin\theta$:

$$\cos 2\theta = \sqrt{(1 + \cos 4\theta)/2} \quad (14)$$

$$\sin 2\theta = \sin 4\theta / 2\cos 2\theta \quad (15)$$

$$\cos \theta = \sqrt{(1 + \cos 2\theta)/2} \quad (16)$$

$$\sin \theta = \sin 2\theta / 2\cos \theta \quad (17)$$

(d) Determining $\cos\phi$ and $\sin\phi$:

(d1) If DEN is positive, set

$$\cos \phi = \cos \theta \quad (18)$$

$$\sin \phi = \sin \theta \quad (19)$$

and go to (d2) below.

If DEN is negative, calculate

$$\cos \phi = \frac{\sqrt{2}}{2} \cos \theta + \frac{\sqrt{2}}{2} \sin \theta \quad (20)$$

$$\sin\phi = \left| \frac{\sqrt{2}}{2} \cos\theta - \frac{\sqrt{2}}{2} \sin\theta \right| \quad (21)$$

and go to (d2) below.

(d2) If NUM is positive, set

$$\cos\phi = |\cos\theta| \quad (22)$$

$$\sin\phi = |\sin\theta| \quad (23)$$

and go to (e) below.

If NUM is negative, set

$$\cos\phi = |\cos\theta| \quad (24)$$

$$\sin\phi = -|\sin\theta| \quad (25)$$

(e) Rotation:

$$X_i = x_i \cos\phi + y_i \sin\phi \quad (26)$$

$$Y_i = x_i \sin\phi + y_i \cos\phi \quad (27)$$

where $i = 1, 2, \dots, m$

After one cycle of $k(k-1)/2$ rotations is completed, the subroutine goes back to calculate the variance for the factor matrix by equation (4).

Denormalization:

$$a_{ij} = b_{ij} \cdot h_i \quad (28)$$

where $i = 1, 2, \dots, m$

$j = 1, 2, \dots, k$

Check on communalities:

$$\text{Final communalities } f_i^2 = \sum_{j=1}^k a_{ij}^2 \quad (29)$$

$$\text{Difference } d_i = h_i^2 - f_i^2 \quad (30)$$

where $i = 1, 2, \dots, m$

```

C
C .....
C VARM 10
C VARM 20
C SLEPCLINE VARPH VARM 30
C VARM 40
C PLRPFCE VARM 50
C PERFGRM CRTHEGICAL NOTATIONS OF A FACTOR MATRIX. THIS VARM 60
C SLEPCLINE NORMALLY OCCURS IN A SEQUENCE OF CALLS TO SUB- VARM 70
C ROUTINES CORR, EIGEN, THACK, LOGAC, VARPH IN THE PERFORMANCE VARM 80
C OF A FACTOR ANALYSIS. VARM 90
C VARM 100
C LSAE VARM 110
C CALL VARPH (P,R,A,NC,TV,F,F,D,IER) VARM 120
C VARM 130
C DESCRIPTIVE OF PARAMETERS VARM 140
C P - NUMBER OF VARIABLES AND NUMBER OF ROWS OF MATRIX A. VARM 150
C R - NUMBER OF FACTORS. VARM 160
C A - INFLT IS THE ORIGINAL FACTOR MATRIX, AND OUTPLT IS VARM 170
C THE ROTATED FACTOR MATRIX. THE ORDER OF MATRIX A VARM 180
C IS M X K. VARM 190
C NC - OUTPLT VARIABLE CONTAINING THE NUMBER OF ITERATION VARM 200
C CYCLES PERFORMED. VARM 210
C TV - OUTPLT VECTOR CONTAINING THE VARIANCE OF THE FACTOR VARM 220
C MATRIX FOR EACH ITERATION CYCLE. THE VARIANCE PRIOR VARM 230
C TO THE FIRST ITERATION CYCLE IS ALSO CALCULATED. VARM 240
C THIS MEANS THAT NC+1 VARIANCES ARE STORED IN VECTOR VARM 250
C TV. MAXIMUM NUMBER OF ITERATION CYCLES ALLOWED IN VARM 260
C THIS SLEPCLINE IS 50. THEREFORE, THE LENGTH OF VARM 270
C VECTOR TV IS 51. VARM 280
C F - OUTPLT VECTOR OF LENGTH P CONTAINING THE ORIGINAL VARM 290
C COMMUNALITIES. VARM 300
C F - OUTPLT VECTOR OF LENGTH P CONTAINING THE FINAL VARM 310
C COMMUNALITIES. VARM 320
C C - OUTPLT VECTOR OF LENGTH P CONTAINING THE DIFFERENCES VARM 330
C BETWEEN THE ORIGINAL AND FINAL COMMUNALITIES. VARM 340
C IER - IER=0 - NC ERRORS VARM 351
C IER=1 - CONVERGENCE WAS NOT ACHIEVED IN 50 CYCLES VARM 352
C OF ROTATION VARM 353
C VARM 354
C REMARKS VARM 360
C IF VARIANCE COMPUTED AFTER EACH ITERATION CYCLE DOES NOT VARM 370
C INCREASE FOR FOUR SUCCESSIVE TIMES, THE SLEPCLINE STOPS VARM 380
C ROTATION. VARM 390
C VARM 400
C SLEPCLINES AND FLATCHN SLEPPROGRAMS REQUIRED VARM 410
C ACSE VARM 420
C VARM 430
C METPCC VARM 440
C KAISEN'S VARIMAX ROTATION AS DESCRIBED IN 'COMPUTER PROGRAM VARM 450
C FOR VARIMAX ROTATION IN FACTOR ANALYSIS' BY THE SAME AUTHOR, VARM 460
C 'ELLIPTICAL AND PSYCHOLOGICAL MEASUREMENT', VOL XIX, NO. 3, VARM 470
C 1955. VARM 480
C VARM 490
C ..... VARM 500
C SLEPCLINE VARPH (P,R,A,NC,TV,F,F,D,IER) VARM 510
C DIMENSION A(1),TV(1),H(1),F(1),C(1) VARM 520
C VARM 530
C ..... VARM 540
C VARM 550
C ..... VARM 560
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE VARM 570
C C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION VARM 580
C STATEMENTS. VARM 590
C ..... VARM 600
C DOUBLE PRECISION A,TV,F,F,D,TVLT,CONS,AA,BB,CC,DD,U,F,B,COSAT, VARM 610
C SINAT,TANAT,SINP,COSP,CTNAT,COS2T,SIN2T,COST,SINTVARM 620
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS VARM 630
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS VARM 640
C ROUTINE. VARM 650
C ..... VARM 660
C THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO VARM 670
C CONTAIN DOUBLE PRECISION FORMAT FUNCTIONS. SORT IN STATEMENTS VARM 680
C 115, 290, 330, 390, AND 355 MUST BE CHANGED TO CSORT. ABS IN VARM 700
C STATEMENTS 260, 320, AND 375 MUST BE CHANGED TO CABS. VARM 710
C ..... VARM 720
C ..... VARM 730
C INITIALIZATION VARM 740
C VARM 750
C IER=0 VARM 760
C EPS=C.CC11E VARM 761
C TVLT=C.C VARM 770
C LL=1 VARM 780
C NV=1 VARM 790
C AC=C VARM 800
C FA=0 VARM 810
C FFA=FA*FA VARM 820
C CCAS=C.TC71C6E VARM 830
C ..... VARM 840
C CALCULATE ORIGINAL COMMUNALITIES VARM 850
C ..... VARM 860
C CC 110 I=1,P VARM 870
C F(1)=C.C VARM 880
C CC 110 J=1,K VARM 890
C L=0(J-I)+1 VARM 900
C 110 F(1)=F(1)+A(L)*A(L) VARM 910
C ..... VARM 920
C CALCULATE NORMALIZED FACTOR MATRIX VARM 930
C ..... VARM 940
C CC 120 I=1,P VARM 950
C 115 F(1)=SQRT(F(1)) VARM 960
C CC 120 J=1,K VARM 970
C L=0(J-I)+1 VARM 980
C 120 A(L)=A(L)/F(1) VARM 990
C CC 10 132 VARM 1000
C ..... VARM 1010
C CALCULATE VARIANCE FOR FACTOR MATRIX VARM 1020
C ..... VARM 1030
C 130 AV=AV+1 VARM 1040
C TVLT=TV(NV-1) VARM 1050
C 132 TV(NV)=C.C VARM 1060
C CC 150 J=1,K VARM 1070
C AA=C.C VARM 1080
C EB=C.C VARM 1090
C LB=0(J-1) VARM 1100
C CC 140 I=1,P VARM 1110
C L=LB+1 VARM 1120
C CC=A(L)*A(L) VARM 1130
C AA=AA+CC VARM 1140
C 140 EB=EB+CC VARM 1150
C 150 TV(NV)=TV(NV)+(FA*EE-AA*AA)/FFA VARM 1160
C IF(NV-5)1160,155,155 VARM 1170
C 155 IER=1 VARM 1180
C CC 10 430 VARM 1190
C ..... VARM 1200
C PERFGRM CONVERGENCE TEST VARM 1210

```

```

12C IF(17V(AV)-1VLTJ)-11.E-7) 17C, 17C, 150
17C NC=NC+1
IF(AC-3) 15C, 15C, 43C
C
C RECTANG OF THE FACTS CONTAINES UP TO
C THE STATEMENT 12C.
C
15C EC 42C J=1,LL
L1=J-1
L2=J
C
C CALCULATE NLP AND DEN
C
EC 42C K1=11,K
L2=K*(K1-1)
AA=C.C
BB=C.C
CC=C.C
DD=C.C
EE=C.C
EC 23C I=1,P
L3=L1+1
L4=L2+1
L=A(L3)+A(L4)+A(L3)-A(L4)
T=A(L3)+A(L4)
T=1+T
CC=CC+(L+1)*(L-1)
EE=EE+2.C*L+1
AA=AA+L
23C EP=EP+T
T=CC-2.C*AA*EE/FA
EE=CC-(2*AA*EP-EE*EP)/FA
C
C CORRELATION OF NLP AND DEN
C
IF(T-0) 26C, 24C, 32C
24C IF(17E)-EPS) 42C, 25C, 25C
C
C NLP & DEN IS GREATER THAN OR EQUAL TO THE
C TOLERANCE FACTOR
C
25C CCS4T=CCNS
SIN4T=CCNS
CC TC 25C
C
C NLP IS LESS THAN DEN
C
26C TAN4T=ABS(17E)/ABS(E)
IF(TAN4T-EPS) 30C, 29C, 29C
25C CCS4T=1.C/SQRT(1.C+TAN4T*TAN4T)
SIN4T=TAN4T*CCS4T
CC TC 25C
30C IF(E) 31C, 42C, 42C
31C SINP=CCNS
CCSP=CCNS
CC TC 42C
C
C NLP IS GREATER THAN DEN
C
32C CIN4T=ABS(17E)
IF(CIN4T-EPS) 34C, 23C, 33C
33C SIN4T=1.C/SQRT(1.C+CIN4T*CIN4T)
CCS4T=CIN4T*SIN4T
CC TC 23C
24C CCS4T=C.C
SIN4T=1.C
C
C DETERMINE COS THETA AND SIN THETA
C
25C CCS2T=SQRT(1.C+CCS4T)/2.C)
SIN2T=SIN4T/(2.C*CCS2T)
35C CLST=SQRT(1.C-CCS2T)/2.C)
SINT=SIN2T/(2.C*CCS2T)
C
C DETERMINE COS PHI AND SIN PHI
C
IF(P) 37C, 37C, 36C
36C CCSP=CCST
SINP=SINT
CC TC 26C
37C CCSP=CCNS*CCST+CCNS*SINT
37S SINP=ABS(CCNS*CCST-CCNS*SINT)
38C IF(1) 35C, 35C, 40C
35C SINP=-SINF
C
C PERFECT RECTANG
C
40C EC 41C I=1,P
L3=L1+1
L4=L2+1
AA=A(L3)*CCSP+A(L4)*SINP
B(L4)=A(L3)*SINP+A(L4)*CCSP
41C B(L3)=AA
42C CENTINLE
CC TC 13C
C
C ENCRPALIZE VARIMAX LOADINGS
C
43C EC 44C I=1,P
EC 44C J=1,K
L=J+K-1
44C A(L1)=A(L1)+A(L1)
C
C CHECK ON COLLINARITIES
C
NC=NC+1
EC 45C I=1,P
45C B(I1)=B(I1)+B(I1)
CC 47C I=1,P
F(I1)=C.C
EC 46C J=1,K
L=J+K-1
46C F(I1)=F(I1)+B(I1)*A(L1)
47C F(I1)=F(I1)-F(I1)
RETURN
ENC

```

```

VARM1220
VARM1230
VARM1240
VARM1250
VARM1260
VARM1270
VARM1280
VARM1290
VARM1300
VARM1310
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VARM2180
VARM2190
VARM2200
VARM2210
VARM2220
VARM2230
VARM2240
VARM2250
VARM2260
VARM2270
VARM2280
VARM2290
VARM2300
VARM2310
VARM2320
VARM2330
VARM2340
VARM2350
VARM2360

```

Time Series (see Smoothing)

Subroutine AUTO

This subroutine calculates the autocovariances for lags 0, 1, 2, ..., (L-1), given a time series of observations A_1, A_2, \dots, A_n and a number L.

$$R_j = \frac{1}{n-j+1} \sum_{i=1}^{n-j+1} (A_i - \text{AVER}) (A_{i+j-1} - \text{AVER}) \quad (1)$$

where $\text{AVER} = \frac{1}{n} \sum_{i=1}^n A_i$

n = number of observations in time series A

j = 1, 2, 3, ..., L represent time lags 0, 1, 2, ..., (L-1)

```

C ..... AUTO 10
C ..... AUTO 20
C ..... AUTO 30
C ..... AUTO 40
C ..... AUTO 50
C ..... AUTO 6C
C ..... AUTO 70
C ..... AUTO 80
C ..... AUTO 90
C ..... AUTO 100
C ..... AUTO 110
C ..... AUTO 120
C ..... AUTO 130
C ..... AUTO 140
C ..... AUTO 150
C ..... AUTO 160
C ..... AUTO 170
C ..... AUTO 180
C ..... AUTO 190
C ..... AUTO 200
C ..... AUTO 210
C ..... AUTO 220
C ..... AUTO 230
C ..... AUTO 240
C ..... AUTO 250
C ..... AUTO 260
C ..... AUTO 270
C ..... AUTO 280
C ..... AUTO 290
C ..... AUTO 300
C ..... AUTO 310
C ..... AUTO 320
C ..... AUTO 330
C ..... AUTO 340
C ..... AUTO 350
C ..... AUTO 360
C ..... AUTO 370
C ..... AUTO 380
C ..... AUTO 390
C ..... AUTO 400
C ..... AUTO 410
C ..... AUTO 420
C ..... AUTO 430
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C ..... AUTO 450
C ..... AUTO 460
C ..... AUTO 470
C ..... AUTO 480
C ..... AUTO 490
C ..... AUTO 500
C ..... AUTO 510
C ..... AUTO 520
C ..... AUTO 530
C ..... AUTO 540
C ..... AUTO 550
C ..... AUTO 560
C ..... AUTO 570
C ..... AUTO 580
C ..... AUTO 590
C ..... AUTO 600
C
SUBROUTINE AUTO
C
C PURPOSE
C TO FIND AUTOCOVARIANCES OF SERIES A FOR LAGS 0 TO L-1.
C
C USAGE
C CALL AUTJ (A,N,L,R)
C
C DESCRIPTION OF PARAMETERS
C A - INPUT VECTOR OF LENGTH N CONTAINING THE TIME SERIES
C WHOSE AUTOCOVARIANCE IS DESIRED.
C N - LENGTH OF THE VECTOR A.
C L - AUTOCOVARIANCE IS CALCULATED FOR LAGS OF 0, 1, 2, ...,
C L-1.
C R - OUTPUT VECTOR OF LENGTH L CONTAINING AUTOCOVARIANCES
C OF SERIES A.
C
C REMARKS
C THE LENGTH OF R IS DIFFERENT FROM THE LENGTH OF A. N MUST
C BE GREATER THAN L. IF NOT, R(1) IS SET TO ZERO AND RETURN
C IS MADE TO THE CALLING PROGRAM.
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C
C METHOD
C DESCRIBED IN R.B. BLACKMAN AND J.W. TUKEY, "THE MEASUREMENT
C OF POWER SPECTRA", DOVER PUBLICATIONS INC., NEW YORK, 1959.
C
C .....
C
SUBROUTINE AUTO (A,N,L,R)
DIMENSION A(1),R(1)
C
C CALCULATE AVERAGE OF TIME SERIES A
C
AVER=C.O
IF(N=1) 50,50,C,100
50 R(1)=D.C
RETURN
100 GO 110 I=1,N
110 AVER=AVER+A(I)
FN=N
AVER=AVER/FN
C
C CALCULATE AUTOCOVARIANCES
C
DO 130 J=1,L
NJ=N-J+1
SUM=C.O
DO 120 I=1,NJ
IJ=I+J-1
120 SUM=SUM+(A(IJ)-AVER)*(A(IJ)-AVER)
FNJ=NJ
130 R(J)=SUM/FNJ
RETURN
END

```

Subroutine CROSS

This subroutine calculates the cross covariances of series B lagging and leading A, given two time series A_1, A_2, \dots, A_n and B_1, B_2, \dots, B_n and given a number L.

(a) B lags A:

$$R_j = \frac{1}{n-j+1} \sum_{i=1}^{n-j+1} (A_i - AVERA) (B_{i+j-1} - AVERB) \quad (1)$$

(b) B leads A:

$$S_j = \frac{1}{n-j+1} \sum_{i=1}^{n-j+1} (A_{i+j-1} - AVERA) (B_i - AVERB) \quad (2)$$

where $AVERA = \frac{1}{n} \sum_{i=1}^n A_i$

$$AVERB = \frac{1}{n} \sum_{i=1}^n B_i$$

n = number of observations in each series

j = 1, 2, ..., L represent time lags (or leads) of 0, 1, 2, ..., (L-1)

```

C      CROSS 10
C      CROSS 20
C      CROSS 30
C      SUBROUTINE CROSS          CROSS 40
C      CROSS 50
C      PURPOSE                    CROSS 60
C      TO FIND THE CROSSCOVARIANCES OF SERIES A WITH SERIES B  CROSS 70
C      (WHICH LEADS AND LAGS A).  CROSS 80
C      CROSS 90
C      USAGE                      CROSS 100
C      CALL CROSS (A,B,N,L,R,S)   CROSS 110
C      CROSS 120
C      DESCRIPTION OF PARAMETERS  CROSS 130
C      A - INPUT VECTOR OF LENGTH N CONTAINING FIRST TIME  CROSS 140
C      SERIES.              CROSS 150
C      B - INPUT VECTOR OF LENGTH N CONTAINING SECOND TIME  CROSS 160
C      SERIES.              CROSS 170
C      N - LENGTH OF SERIES A AND B.             CROSS 180
C      L - CROSSCOVARIANCE IS CALCULATED FOR LAGS AND LEADS OF  CROSS 190
C      0, 1, 2, ..., L-1.             CROSS 200
C      K - OUTPUT VECTOR OF LENGTH L CONTAINING CROSSCOVARI-  CROSS 210
C      ANCES OF A WITH B, WHERE B LAGS A.  CROSS 220
C      S - OUTPUT VECTOR OF LENGTH L CONTAINING CROSSCOVARI-  CROSS 230
C      ANCES OF A WITH B, WHERE B LEADS A.  CROSS 240
C      CROSS 250
C      REMARKS                     CROSS 260
C      N MUST BE GREATER THAN L. IF NOT, R(1) AND S(1) ARE SET TO  CROSS 270
C      ZERO AND RETURN IS MADE TO THE CALLING PROGRAM.  CROSS 280
C      CROSS 290
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED  CROSS 300
C      NONE                                CROSS 310
C      CROSS 320
C      METHOD                          CROSS 330
C      DESCRIBED IN R.B. BLACKMAN AND J.W. TUKEY, "THE MEASUREMENT  CROSS 340
C      OF POWER SPECTRA", DOVER PUBLICATIONS INC., NEW YORK, 1959.  CROSS 350
C      CROSS 360
C      -----CROSS 370
C      SUBROUTINE CROSS (A,B,N,L,R,S)  CROSS 380
C      DIMENSION A(1),B(1),R(1),S(1)  CROSS 390
C      CROSS 400
C      CALCULATE AVERAGES OF SERIES A AND B  CROSS 410
C      CROSS 420
C      CROSS 430
C      FN=N                            CROSS 440
C      AVERA=A.O                         CROSS 450
C      AVERB=B.O                         CROSS 460
C      IF(N=1)50,50,50,100              CROSS 470
C      50 R(1)=A.O                        CROSS 480
C      S(1)=B.O                          CROSS 490
C      RETURN                             CROSS 500
C      100 DO 110 I=1,N                   CROSS 510
C      AVERA=AVERA+A(I)                  CROSS 520
C      110 AVERB=AVERB+B(I)               CROSS 530
C      AVERA=AVERA/FN                    CROSS 540
C      AVERB=AVERB/FN                    CROSS 550
C      CROSS 560
C      CALCULATE CROSSCOVARIANCES OF SERIES A AND B  CROSS 570
C      CROSS 580
C      DO 130 J=1,L                       CROSS 590
C      NJ=N-J+1                           CROSS 600
C      SUMR=O.O                            CROSS 610
C      SUMS=O.O                            CROSS 620
C      DO 120 I=1,NJ                       CROSS 630
C      IJ=I+J-1                            CROSS 640
C      SUMR=SUMR+(A(I)-AVERA)*(B(IJ)-AVERB)  CROSS 650
C      120 SUMS=SUMS+(A(IJ)-AVERA)*(B(I)-AVERB)  CROSS 660
C      FNJ=NJ                               CROSS 670
C      R(J)=SUMR/FNJ                       CROSS 680
C      130 S(J)=SUMS/FNJ                   CROSS 690
C      RETURN                             CROSS 700
C      END                                 CROSS 710

```


Subroutine SMO

This subroutine calculates the smoothed or filtered series, given a time series A_1, A_2, \dots, A_n , a selection integer L , and a weighting series W_1, W_2, \dots, W_m .

$$R_i = \sum_{j=1}^m A_p \cdot W_j \quad (1)$$

where $p = j \cdot L - L + k$

$$k = i - IL + 1$$

$$i = IL \text{ to } IH$$

$$IL = \frac{L(m-1)}{2} + 1 \quad (2)$$

$$IH = n - \frac{L(m-1)}{2} \quad (3)$$

L = a given selection integer. For example, $L = 4$ applies weights to every 4th item of the time series.

m = number of weights. Must be an odd integer. (If m is an even integer, any fraction resulting from the calculation of $\frac{L(m-1)}{2}$ in (2) and (3) above will be truncated.)

n = number of items in the time series

From IL to IH elements of the vector R are filled with the smoothed series, and other elements with zeros.

```

C .....SMO 10
C .....SMO 20
C .....SMO 30
C .....SMO 40
C .....SMO 50
C .....SMO 60
C .....SMO 70
C .....SMO 80
C .....SMO 90
C .....SMO 100
C .....SMO 110
C .....SMO 120
C .....SMO 130
C .....SMO 140
C .....SMO 150
C .....SMO 160
C .....SMO 170
C .....SMO 180
C .....SMO 190
C .....SMO 200
C .....SMO 210
C .....SMO 220
C .....SMO 230
C .....SMO 240
C .....SMO 250
C .....SMO 260
C .....SMO 270
C .....SMO 280
C .....SMO 290
C .....SMO 300
C .....SMO 310
C .....SMO 320
C .....SMO 330
C .....SMO 340
C .....SMO 350
C .....SMO 360
C .....SMO 370
C .....SMO 380
C .....SMO 390
C .....SMO 400
C .....SMO 410
C .....SMO 420
C .....SMO 430
C .....SMO 440
C .....SMO 450
C .....SMO 460
C .....SMO 470
C .....SMO 480
C .....SMO 490
C .....SMO 500
C .....SMO 510
C .....SMO 520
C .....SMO 530
C .....SMO 540
C .....SMO 550
C .....SMO 560
C .....SMO 570
C .....SMO 580
C .....SMO 590
C .....SMO 600
C .....SMO 610
C .....SMO 620

C .....SMO 10
C .....SMO 20
C .....SMO 30
C .....SMO 40
C .....SMO 50
C .....SMO 60
C .....SMO 70
C .....SMO 80
C .....SMO 90
C .....SMO 100
C .....SMO 110
C .....SMO 120
C .....SMO 130
C .....SMO 140
C .....SMO 150
C .....SMO 160
C .....SMO 170
C .....SMO 180
C .....SMO 190
C .....SMO 200
C .....SMO 210
C .....SMO 220
C .....SMO 230
C .....SMO 240
C .....SMO 250
C .....SMO 260
C .....SMO 270
C .....SMO 280
C .....SMO 290
C .....SMO 300
C .....SMO 310
C .....SMO 320
C .....SMO 330
C .....SMO 340
C .....SMO 350
C .....SMO 360
C .....SMO 370
C .....SMO 380
C .....SMO 390
C .....SMO 400
C .....SMO 410
C .....SMO 420
C .....SMO 430
C .....SMO 440
C .....SMO 450
C .....SMO 460
C .....SMO 470
C .....SMO 480
C .....SMO 490
C .....SMO 500
C .....SMO 510
C .....SMO 520
C .....SMO 530
C .....SMO 540
C .....SMO 550
C .....SMO 560
C .....SMO 570
C .....SMO 580
C .....SMO 590
C .....SMO 600
C .....SMO 610
C .....SMO 620

SUBROUTINE SMO
PURPOSE
    TO SMOOTH JK FILTER SERIES A BY WEIGHTS W.
USAGE
    CALL SMO (A,N,W,M,L,R)
DESCRIPTION OF PARAMETERS
    A - INPUT VECTOR OF LENGTH N CONTAINING TIME SERIES DATA.
    N - LENGTH OF SERIES A.
    W - INPUT VECTOR OF LENGTH M CONTAINING WEIGHTS.
    M - NUMBER OF ITEMS IN WEIGHT VECTOR. M MUST BE AN ODD
        INTEGER. IF M IS AN EVEN INTEGER, ANY FRACTION
        RESULTING FROM THE CALCULATION OF (L*(M-1))/2 IN (1)
        AND (2) BELOW WILL BE TRUNCATED.
    L - SELECTION INTEGER. FOR EXAMPLE, L=12 MEANS THAT WEIGHTS
        ARE APPLIED TO EVERY 12-TH ITEM OF A. L=1 APPLIES
        WEIGHTS TO SUCCESSIVE ITEMS OF A. FOR MONTHLY DATA,
        L=12 GIVES YEAR-TO-YEAR AVERAGES AND L=1 GIVES MONTH-TO-
        MONTH AVERAGES.
    R - OUTPUT VECTOR OF LENGTH N. FROM IL TO IH ELEMENTS OF
        THE VECTOR R ARE FILLED WITH THE SMOOTHED SERIES AND
        OTHER ELEMENTS WITH ZERO, WHERE
        IL=(L*(M-1))/2+1 ..... (1)
        IH=N-(L*(M-1))/2 ..... (2)
REMARKS
    N MUST BE GREATER THAN OR EQUAL TO THE PRODUCT OF L*M.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
    NONE
METHOD
    REFER TO THE ARTICLE 'FORTRAN SUBROUTINES FOR TIME SERIES
    ANALYSIS', BY J. R. HEALY AND B. P. BOGERT, COMMUNICATIONS
    OF ACM, V.6, NO.1, JANUARY, 1963.
.....
SUBROUTINE SMO (A,N,W,M,L,R)
DIMENSION A(1),W(1),R(1)
INITIALIZATION
DO 110 I=1,N
R(I)=0.C
110 R(I)=0.C
IL=(L*(M-1))/2+1
IH=N-(L*(M-1))/2
SMOOTH SERIES A BY WEIGHTS W
DO 120 I=IL,IH
K=I-IL+1
DO 120 J=1,M
IP=(J*L)-L+K
120 R(I)=R(I)+A(IP)*W(J)
RETURN
END

```

Subroutine EXSMO

This subroutine calculates a smoothed series S_1, S_2, \dots, S_{NX} , given time series X_1, X_2, \dots, X_{NX} and a smoothing constant α . Also, at the end of the computation, the coefficients $A, B,$ and C are given for the expression $A + B(T) + C(T)^2/2$. This expression can be used to find estimates of the smoothed series for a given number of time periods, T , ahead.

The subroutine has the following two stages for $i = 1, 2, \dots, NX$, starting with $A, B,$ and C either given by the user or provided automatically by the subroutine (see below).

- (a) Find S_i for one period ahead:

$$S_i = A + B + 0.5C \quad (1)$$

- (b) Update coefficients $A, B,$ and C :

$$A = X_i + (1 - \alpha)^3 (S_i - X_i) \quad (2)$$

$$B = B + C - 1.5 (\alpha^2) (2 - \alpha) (S_i - X_i) \quad (3)$$

$$C = C - (\alpha^3) (S_i - X_i) \quad (4)$$

where $\alpha =$ smoothing constant specified by the user

$$(0.0 < \alpha < 1.0)$$

If coefficients $A, B,$ and C are not all zero (0.0), take given values as initial values. However, if $A = B = C = 0.0$, generate initial values of $A, B,$ and C as follows:

$$C = X_1 - 2X_2 + X_3 \quad (5)$$

$$B = X_2 - X_1 - 1.5C \quad (6)$$

$$A = X_1 - B - 0.5C \quad (7)$$

```

C ..... EXSM 10
C ..... EXSM 20
C ..... EXSM 30
C SUBROUTINE EXSMO EXSM 40
C ..... EXSM 50
C ..... EXSM 60
C PURPOSE TO FIND THE TRIPLE EXPONENTIAL SMOOTHED SERIES S OF THE EXSM 70
C ..... EXSM 80
C ..... EXSM 90
C USAGE CALL EXSMO (K,NX,AL,A,B,C,S) EXSM 100
C ..... EXSM 110
C ..... EXSM 120
C DESCRIPTION OF PARAMETERS EXSM 130
C X - INPUT VECTOR OF LENGTH NX CONTAINING TIME SERIES EXSM 140
C DATA WHICH IS TO BE EXPONENTIALLY SMOOTHED. EXSM 150
C NX - THE NUMBER OF ELEMENTS IN X. EXSM 160
C AL - SMOOTHING CONSTANT, ALPHA. AL MUST BE GREATER THAN EXSM 170
C ZERO AND LESS THAN ONE. EXSM 180
C A,B,C - COEFFICIENTS OF THE PREDICTION EQUATION WHERE S IS EXSM 190
C PREDICTED T PERIODS HENCE BY EXSM 200
C A + B*T + C*T**2. EXSM 210
C AS INPUT-- IF A=B=C=0, PROGRAM WILL PROVIDE INITIAL EXSM 220
C VALUES. IF AT LEAST ONE OF A,B,C IS NOT ZERO, EXSM 230
C PROGRAM WILL TAKE GIVEN VALUES AS INITIAL VALUES. EXSM 240
C AS OUTPUT-- A+B+C CONTAIN LATEST, UPDATED COEFFI- EXSM 250
C CIENTS OF PREDICTION. EXSM 260
C S - OUTPUT VECTOR OF LENGTH NX CONTAINING TRIPLE EXSM 270
C EXPONENTIALLY SMOOTHED TIME SERIES. EXSM 280
C ..... EXSM 290
C REMARKS EXSM 300
C NONE EXSM 310
C ..... EXSM 320
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED EXSM 330
C NONE EXSM 340
C ..... EXSM 350
C METHOD EXSM 360
C REFER TO H. G. BROWN, "SMOOTHING, FORECASTING AND PREDICTION EXSM 370
C OF DISCRETE TIME SERIES", PRENTICE-HALL, N.J., 1963, EXSM 380
C PP. 140 TO 144. EXSM 390
C ..... EXSM 400
C ..... EXSM 410
C SUBROUTINE EXSMO (K,NX,AL,A,B,C,S) EXSM 420
C DIMENSION X(1),S(1) EXSM 430
C ..... EXSM 440
C IF A=B=C=0, GENERATE INITIAL VALUES OF A, B, AND C EXSM 450
C ..... EXSM 460
C IF(A) 140, 110, 140 EXSM 470
C IF(B) 140, 120, 140 EXSM 480
C IF(C) 140, 130, 140 EXSM 490
C C=X(1)-2.0*X(2)+X(3) EXSM 500
C B=X(2)-X(1)-1.5*C EXSM 510
C A=X(1)-B-0.5*C EXSM 520
C ..... EXSM 530
C 140 BE=1.0-AL EXSM 540
C BECUB=BE*BE*BE EXSM 550
C ALCUB=AL*AL*AL EXSM 560
C ..... EXSM 570
C DO THE FOLLOWING FOR I=1 TO NX EXSM 580
C ..... EXSM 590
C DO 150 I=1,NX EXSM 600
C ..... EXSM 610
C FIND S(I) FOR ONE PERIOD AHEAD EXSM 620
C ..... EXSM 630
C S(I)=A+B+0.5*C EXSM 640
C ..... EXSM 650
C UPDATE COEFFICIENTS A, B, AND C EXSM 660
C ..... EXSM 670
C DIF=S(I)-X(I) EXSM 680
C A=X(I)+BECUB*DIF EXSM 690
C B=B-C-1.5*AL*AL*(2.0-AL)*DIF EXSM 700
C 150 C=C-ALCUB*DIF EXSM 710
C RETURN EXSM 720
C END EXSM 730
C ..... EXSM 740

```

Nonparametric Statistics

Subroutine KOLMO

Given a sample of n independent and identically distributed random variables X_1, X_2, \dots, X_n with continuous cumulative distribution function $F(x)$, this subroutine tests the difference in absolute value between the empirical distribution $F_n(x)$ and theoretical distribution $F(x)$, using Kolmogorov-Smirnov's limiting distribution.

For this purpose:

1. The order statistics $\{x_{(i)}\}$ are determined from the set $\{x_i\}$ by sorting $\{x_i\}$ into a nondecreasing sequence.

2. The empirical cumulative distribution function $F_n(x)$ is computed. This is the following step-function:

$$F_n(x) = \begin{cases} 0 & x < x_{(1)} \\ k/n & x_{(k)} \leq x < x_{(k+1)}; k=1, \dots, n-1 \\ 1 & x_{(n)} \leq x \end{cases}$$

3. The maximum deviation D_n in absolute value between the empirical and theoretical distribution is computed:

$$D_n = \max_{-\infty < x < \infty} |F_n(x) - F(x)|$$

Since $F_n(x)$ and $F(x)$ are nondecreasing functions, the result is:

$$D_n = \max_{1 \leq k \leq n} |F_n[x_{(k)}] - F[x_{(k)}]|$$

D_n is a random variable, and $L(z)$ is the limiting cumulative distribution function of $n^{1/2} D_n$:

$$\lim_{n \rightarrow \infty} \text{Prob} \{n^{1/2} D_n < z\} = L(z)$$

4. Finally,

$$z = n^{1/2} D_n$$

and the probability of being greater than or equal to the computed value of $n^{1/2} D_n$

$$P = 1 - L(z)$$

are computed.

Generally, theoretical distribution functions are to be included by the user, as specified in the program. However, four functions are evaluated in KOLMO, as follows:

$$\int_{-\infty}^x dF(t) = F(x) \quad (1)$$

is evaluated at the points of the set $\{X_{(i)}\}$, where $F(x)$ is one of the following:

- The normal pdf with mean u and variance s^2
- The exponential pdf with mean u and variance s^2
- The Cauchy pdf with median u , and first quartile $s - u$
- The uniform pdf with endpoints u and s

Any user-written pdf should evaluate (1) above, using the parameters u and s at his convenience. Instructions given in the program KOLMO should be followed.

Lilliefors (1967) notes that critical values determined by this test are not correct when one or more parameters are estimated from the sample. The user should refer to his article for notes on approximations which may be considered if such estimates are used.

For references see:

- (1) W. Feller, "On the Kolmogorov - Smirnov limit theorems for empirical distributions", Annals of Math. Stat., 19, pp. 177-189.
- (2) N. Smirnov, "Table for estimating the goodness of fit of empirical distributions", Annals of Math. Stat., 19, pp. 279-281.
- (3) R. Von Mises, Mathematical Theory of Probability and Statistics. Academic Press, New York, 1964, pp. 490-493.
- (4) B. V. Gnedenko, The Theory of Probability. Chelsea Publishing Co., New York, 1962, pp. 384-401.
- (5) H. W. Lilliefors, "On the Kolmogorov-Smirnov test for normality with mean and variance unknown", J. A. S. A., 62 (1967), pp. 399-402.

```

C
C ..... KLMO 10
C KLMO 20 7 CONTINUE
C KLMO 30 8 J=N KLMO1300
C SUBROUTINE KOLMO KLMO 40 9 IL=J+1 KLMO1310
C KLMO 50 F1=FS KLMO1320
C PURPOSE FS=FLOAT(J)/XN KLMO1330
C TESTS THE DIFFERENCE BETWEEN EMPIRICAL AND THEORETICAL KLMO 60 IF(IFCOD=2)10,13,17 KLMO1340
C DISTRIBUTIONS USING THE KOLMOGOROV-SMIRNOV TEST KLMO 70 10 IF(S11,11,12 KLMO1350
C KLMO 80 11 IER=1 KLMO1360
C USAGE GO TO 29 KLMO 90 KLMO1370
C CALL KOLMO(X,N,Z,PROB,IFCOD,U,S,IER) KLMO 100 12 Z=(X(J)-U)/S KLMO1380
C KLMO 110 CALL NQTR(Z,Y,D) KLMO1390
C KLMO 120 GO TO 27 KLMO1400
C DESCRIPTION OF PARAMETERS KLMO 130 KLMO1410
C X - INPUT VECTOR OF N INDEPENDENT OBSERVATIONS. ON KLMO 140 13 IF(S11,11,14 KLMO1420
C RETURN FROM KOLMO, X HAS BEEN SORTED INTO A KLMO 150 14 Z=(X(J)-U)/S+1.0 KLMO1430
C MONOTONIC NON-DECREASING SEQUENCE. KLMO 160 15 Y=0.0 KLMO1440
C N - NUMBER OF OBSERVATIONS IN X. KLMO 170 GO TO 27 KLMO1450
C Z - OUTPUT VARIABLE CONTAINING THE GREATEST VALUE WITH KLMO 180 16 Y=1-EXP(-Z) KLMO1460
C RESPECT TO X OF SORT(N)*FS(FN(X)-F(X)) WHERE KLMO 190 17 IF(IFCOD=4)18,20,26 KLMO1470
C F(X) IS A THEORETICAL DISTRIBUTION FUNCTION AND KLMO 200 18 IF(S)19,11,19 KLMO1480
C FN(X) AN EMPIRICAL DISTRIBUTION FUNCTION. KLMO 210 19 Y=ATAN(X(J)-U)/S)*0.3183099+0.5 KLMO1490
C PROB - OUTPUT VARIABLE CONTAINING THE PROBABILITY OF KLMO 220 GO TO 27 KLMO1500
C THE STATISTIC BEING GREATER THAN OR EQUAL TO Z IF KLMO 230 20 IF(S=U)11,11,21 KLMO1510
C THE HYPOTHESIS THAT X IS FROM THE DENSITY UNDER KLMO 240 21 IF(X(J)-U)7,22,23 KLMO1520
C CONSIDERATION IS TRUE. E.G., PROB = 0.05 IMPLIES KLMO 250 22 Y=0.0 KLMO1530
C THAT ONE CAN REJECT THE NULL HYPOTHESIS THAT THE SET KLMO 260 GO TO 27 KLMO1540
C X IS FROM THE DENSITY UNDER CONSIDERATION WITH 5 PER KLMO 270 23 IF(X(J)-S)7,25,24 KLMO1550
C CENT PROBABILITY OF BEING INCORRECT. PROB = 1. - KLMO 280 24 Y=1.0 KLMO1560
C SMIRN(Z). KLMO 290 GO TO 27 KLMO1570
C IFCOD - A CODE DENOTING THE PARTICULAR THEORETICAL KLMO 300 25 Y=(X(J)-U)/(S-U) KLMO1580
C PROBABILITY DISTRIBUTION FUNCTION BEING CONSIDERED. KLMO 310 GO TO 27 KLMO1590
C = 1---F(X) IS THE NORMAL PDF. KLMO 320 26 IER=1 KLMO1600
C = 2---F(X) IS THE EXPONENTIAL PDF. KLMO 330 GO TO 29 KLMO1610
C = 3---F(X) IS THE CAUCHY PDF. KLMO 340 27 E1=ABS(Y-F1) KLMO1620
C = 4---F(X) IS THE UNIFORM PDF. KLMO 350 FS=ABS(Y-FS) KLMO1630
C = 5---F(X) IS USER SUPPLIED. KLMO 360 DN=MAX(ION,E1,ES) KLMO1640
C U - WHEN IFCOD IS 1 OR 2, U IS THE MEAN OF THE DENSITY KLMO 370 IF(LL=N)6,8,28 KLMO1650
C GIVEN ABOVE. KLMO 380 KLMO1660
C WHEN IFCOD IS 3, U IS THE MEDIAN OF THE CAUCHY KLMO 390 KLMO1670
C DENSITY. KLMO 400 KLMO1680
C WHEN IFCOD IS 4, U IS THE LEFT ENDPOINT OF THE KLMO 410 KLMO1690
C UNIFORM DENSITY. KLMO 420 28 Z=DN*SQRT(XN) KLMO1700
C WHEN IFCOD IS 5, U IS USER SPECIFIED. KLMO 430 CALL SMIRN(Z,PROB) KLMO1710
C S - WHEN IFCOD IS 1 OR 2, S IS THE STANDARD DEVIATION OF KLMO 440 PROB=1.0-PROB KLMO1720
C DENSITY GIVEN ABOVE, AND SHOULD BE POSITIVE. KLMO 450 29 RETURN KLMO1730
C WHEN IFCOD IS 3, U - S SPECIFIES THE FIRST QUANTILE KLMO 460 END KLMO1740
C OF THE CAUCHY DENSITY. S SHOULD BE NON-ZERO. KLMO 470 KLMO1750
C IF IFCOD IS 4, S IS THE RIGHT ENDPOINT OF THE UNIFORM KLMO 480
C DENSITY. S SHOULD BE GREATER THAN U. KLMO 490
C IF IFCOD IS 5, S IS USER SPECIFIED. KLMO 500
C IER - ERROR INDICATOR WHICH IS NON-ZERO IF S VIOLATES ABOVE KLMO 510
C CONVENTIONS. ON RETURN NO TEST HAS BEEN MADE, AND X KLMO 520
C AND Y HAVE BEEN SORTED INTO MONOTONIC NON-DECREASING KLMO 530
C SEQUENCES. IER IS SET TO ZERO ON ENTRY TO KOLMO. KLMO 540
C IER IS CURRENTLY SET TO ONE IF THE USER-SUPPLIED PDF KLMO 550
C IS REQUESTED FOR TESTING. THIS SHOULD BE CHANGED KLMO 560
C (SEE REMARKS) WHEN SOME PDF IS SUPPLIED BY THE USER. KLMO 570
C KLMO 580
C REMARKS KLMO 590
C N SHOULD BE GREATER THAN OR EQUAL TO 100. (SEE THE KLMO 600
C MATHEMATICAL DESCRIPTION GIVEN FOR THE PROGRAM SMIRN. KLMO 610
C CONCERNING ASYMPTOTIC FORMULAE) ALSO, PROBABILITY LEVELS KLMO 620
C DETERMINED BY THIS PROGRAM WILL NOT BE CORRECT IF THE KLMO 630
C SAME SAMPLES ARE USED TO ESTIMATE PARAMETERS FOR THE KLMO 640
C CONTINUOUS DISTRIBUTIONS WHICH ARE USED IN THIS TEST. KLMO 650
C (SEE THE MATHEMATICAL DESCRIPTION FOR THIS PROGRAM) KLMO 660
C F(X) SHOULD BE A CONTINUOUS FUNCTION. KLMO 670
C ANY USER SUPPLIED CUMULATIVE PROBABILITY DISTRIBUTION KLMO 680
C FUNCTION SHOULD BE CODED BEGINNING WITH STATEMENT 26 BELOW, KLMO 690
C AND SHOULD RETURN TO STATEMENT 27. KLMO 700
C KLMO 710
C DOUBLE PRECISION USAGE---IT IS DOUBTFUL THAT THE USER WILL KLMO 720
C WISH TO PERFORM THIS TEST USING DOUBLE PRECISION ACCURACY. KLMO 730
C IF ONE WISHES TO COMMUNICATE WITH KOLMO IN A DOUBLE KLMO 740
C PRECISION PROGRAM, HE SHOULD CALL THE FORTRAN SUPPLIED KLMO 750
C PROGRAM SNGL(X) PRIOR TO CALLING KOLMO, AND CALL THE KLMO 760
C FORTRAN SUPPLIED PROGRAM DBL(X) AFTER EXITING FROM KOLMO. KLMO 770
C (NOTE THAT SUBROUTINE SMIRN DOES HAVE DOUBLE PRECISION KLMO 780
C CAPABILITY AS SUPPLIED BY THIS PACKAGE.) KLMO 790
C KLMO 800
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED KLMO 810
C SMIRN, NQTR, AND ANY USER SUPPLIED SUBROUTINES REQUIRED. KLMO 820
C KLMO 830
C METHOD KLMO 840
C FOR REFERENCE, SEE (1) W. FELLER--ON THE KOLMOGOROV-SMIRNOV KLMO 850
C LIMIT THEOREMS FOR EMPIRICAL DISTRIBUTIONS-- KLMO 860
C ANNALS OF MATH. STAT., 19, 1948. 177-189, KLMO 870
C (2) N. SMIRNOV--TABLE FOR ESTIMATING THE GOODNESS OF FIT KLMO 880
C OF EMPIRICAL DISTRIBUTIONS--ANNALS OF MATH. STAT., 19, KLMO 890
C 1946. 279-281. KLMO 900
C (3) R. VON MISES--MATHEMATICAL THEORY OF PROBABILITY AND KLMO 910
C STATISTICS--ACADEMIC PRESS, NEW YORK, 1964. 490-493, KLMO 920
C (4) B.V. GNEDENKO--THE THEORY OF PROBABILITY--CHELSEA KLMO 930
C PUBLISHING COMPANY, NEW YORK, 1962. 384-401. KLMO 940
C KLMO 950
C ..... KLMO 960
C SUBROUTINE KOLMO(X,N,Z,PROB,IFCOD,U,S,IER) KLMO 970
C DIMENSION X(1) KLMO 980
C NON DECREASING ORDERING OF X(I)'S (DUBY METHOD) KLMO 990
C KLMO1000
C IER=0 KLMO1010
C DO 5 I=2,N KLMO1020
C IF(X(I)-X(I-1))1,5,5 KLMO1030
C 1 TEMP=X(I) KLMO1040
C IM=I-1 KLMO1050
C DO 3 J=1,IM KLMO1060
C LS=J KLMO1070
C IF(TEMP-X(L))2,4,4 KLMO1080
C 2 X(L+1)=X(L) KLMO1090
C 3 CONTINUE KLMO1100
C X(I)=TEMP KLMO1110
C GO TO 5 KLMO1120
C 4 X(L+1)=TEMP KLMO1130
C 5 CONTINUE KLMO1140
C KLMO1150
C KLMO1160
C KLMO1170
C COMPUTES MAXIMUM DEVIATION DN IN ABSOLUTE VALUE BETWEEN KLMO1180
C EMPIRICAL AND THEORETICAL DISTRIBUTIONS KLMO1190
C KLMO1200
C KLMO1210
C NM1=N-1 KLMO1220
C XN=N KLMO1230
C DN=0.0 KLMO1240
C FS=0.0 KLMO1250
C IL=1 KLMO1260
C DD 7 I=IL,NM1 KLMO1270
C J=I KLMO1280
C IF(X(J)-X(J+1))9,7,9 KLMO1290

```

Subroutine KOLM2

Given a sample of n i. i. d. (independent and identically distributed) random variables X , and a sample of m i. i. d. random variables Y , this subroutine tests the difference between the two empirical distribution functions $F_n(x)$ and $G_m(y)$ using Kolmogorov-Smirnov's limiting distribution. For this purpose:

1. The sets X and Y are sorted into the ordered sets $\{X_{(i)}\}$ and $\{Y_{(j)}\}$, which are nondecreasing sequences.

2. The empirical cumulative distribution functions $F_n(x)$ for the set X , and $G_m(y)$ for the set Y are computed. For example,

$$F_n(x) = \begin{cases} 0 & x < x_{(1)} \\ k/n & x_{(k)} \leq x < x_{(k+1)}; k=1, \dots, n-1 \\ 1 & x_{(n)} \leq x \end{cases}$$

3. The maximum difference in absolute value between the two sample distribution functions is computed:

$$D_{m,n} = \max_{x,y} |F_n(x) - G_m(y)|$$

The statistic $\sqrt{\frac{mn}{m+n}} D_{m,n}$ is a random variable with limiting cumulative distribution function $L(z)$, which is described under "Subroutine SMIRN" in this manual. That is,

$$\lim_{m,n \rightarrow \infty} \text{Prob} \left\{ \sqrt{\frac{mn}{m+n}} D_{m,n} < z \right\} = L(z)$$

$$m, n \rightarrow \infty, \infty$$

4. Finally, the probability (asymptotic) of the statistic $\sqrt{\frac{mn}{m+n}} D_{m,n}$ being not less than its computed value, under the assumption of equality of the two theoretical distribution functions from which X and Y were taken, is computed:

$$P = 1 - L(z)$$

For reference see:

(1) W. Feller, "On the Kolmogorov-Smirnov limit theorems for empirical distributions", Annals of Math. Stat., 19, pp. 177-189.

(2) N. Smirnov, "Table for estimating the goodness of fit of empirical distributions", Annals of Math. Stat., 19, pp. 279-281.

(3) B. V. Gnedenko, The Theory of Probability. Chelsea Publishing Co. New York, 1962, pp. 384-401.

```

C ..... KLM2 10
C SUBROUTINE KOLM2 KLM2 20
C KLM2 30
C KLM2 40
C PURPOSE KLM2 50
C KLM2 60
C TESTS THE DIFFERENCE BETWEEN TWO SAMPLE DISTRIBUTION KLM2 80
C FUNCTIONS USING THE KOLMGOROV-SMIRNOV TEST KLM2 90
C KLM2 100
C USAGE KLM2 110
C CALL KOLM2(X,Y,N,M,Z,PROB) KLM2 120
C KLM2 130
C DESCRIPTION OF PARAMETERS KLM2 140
C X - INPUT VECTOR OF N INDEPENDENT OBSERVATIONS. ON KLM2 150
C RETURN FROM KOLM2, X HAS BEEN SORTED INTO A KLM2 160
C MONOTONIC NON-DECREASING SEQUENCE. KLM2 170
C Y - INPUT VECTOR OF M INDEPENDENT OBSERVATIONS. ON KLM2 180
C RETURN FROM KOLM2, Y HAS BEEN SORTED INTO A KLM2 190
C MONOTONIC NON-DECREASING SEQUENCE. KLM2 200
C N - NUMBER OF OBSERVATIONS IN X KLM2 210
C M - NUMBER OF OBSERVATIONS IN Y KLM2 220
C Z - OUTPUT VARIABLE CONTAINING THE GREATEST VALUE WITH KLM2 230
C RESPECT TO THE SPECTRUM OF X AND Y OF KLM2 240
C SORT((M*N)/(M+N))*ABS(FN(X)-GM(Y)) WHERE KLM2 250
C FN(X) IS THE EMPIRICAL DISTRIBUTION FUNCTION OF THE KLM2 260
C SET (X) AND GM(Y) IS THE EMPIRICAL DISTRIBUTION KLM2 270
C FUNCTION OF THE SET (Y). KLM2 280
C PROB - OUTPUT VARIABLE CONTAINING THE PROBABILITY OF KLM2 290
C THE STATISTIC BEING GREATER THAN OR EQUAL TO Z IF KLM2 300
C THE HYPOTHESIS THAT X AND Y ARE FROM THE SAME PDF IS KLM2 310
C TRUE. E.G., PROB = 0.05 IMPLIES THAT ONE CAN REJECT KLM2 320
C THE NULL HYPOTHESIS THAT THE SETS X AND Y ARE FROM KLM2 330
C THE SAME DENSITY WITH 5 PER CENT PROBABILITY OF BEING KLM2 340
C INCORRECT. PROB = 1. - SMIRN(Z). KLM2 350
C KLM2 360
C REMARKS KLM2 370
C N AND M SHOULD BE GREATER THAN OR EQUAL TO 100. (SEE THE KLM2 380
C MATHEMATICAL DESCRIPTION FOR THIS SUBROUTINE AND FOR THE KLM2 390
C SUBROUTINE SMIRN, CONCERNING ASYMPTOTIC FORMULAE). KLM2 400
C KLM2 410
C DOUBLE PRECISION USAGE---IT IS DOUBTFUL THAT THE USER WILL KLM2 420
C WISH TO PERFORM THIS TEST USING DOUBLE PRECISION ACCURACY. KLM2 430
C IF ONE WISHES TO COMMUNICATE WITH KOLM2 IN A DOUBLE KLM2 440
C PRECISION PROGRAM, HE SHOULD CALL THE FORTRAN SUPPLIED KLM2 450
C PROGRAM SNGLEX) PRIOR TO CALLING KOLM2, AND CALL THE KLM2 460
C FORTRAN SUPPLIED PROGRAM DBLEX) AFTER EXITING FROM KOLM2. KLM2 470
C (NOTE THAT SUBROUTINE SMIRN DOES HAVE DOUBLE PRECISION KLM2 480
C CAPABILITY AS SUPPLIED BY THIS PACKAGE.) KLM2 490
C KLM2 500
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED KLM2 510
C SMIRN KLM2 520
C KLM2 530
C KLM2 540
C KLM2 550
C METHOD KLM2 560
C FOR REFERENCE, SEE (1) W. FELLER--ON THE KOLMGOROV-SMIRNOV KLM2 570
C LIMIT THEOREMS FOR EMPIRICAL DISTRIBUTIONS-- KLM2 580
C ANNALS OF MATH. STAT., 19, 1948. 177-189, KLM2 590
C (2) N. SMIRNOV--TABLE FOR ESTIMATING THE GOODNESS OF FIT KLM2 600
C OF EMPIRICAL DISTRIBUTIONS--ANNALS OF MATH. STAT., 19, KLM2 610
C 1948. 279-281. KLM2 620
C (3) R. VON MISES--MATHEMATICAL THEORY OF PROBABILITY AND KLM2 630
C STATISTICS--ACADEMIC PRESS, NEW YORK, 1964. 490-493, KLM2 640
C (4) B.V. GNEDENKO--THE THEORY OF PROBABILITY--CHELSEA KLM2 650
C PUBLISHING COMPANY, NEW YORK, 1962. 384-401. KLM2 660
C KLM2 670
C ..... KLM2 680
C SUBROUTINE KOLM2(X,Y,N,M,Z,PROB) KLM2 690
C DIMENSION X(1),Y(1) KLM2 700
C KLM2 710
C SORT X INTO ASCENDING SEQUENCE KLM2 720
C KLM2 730
C KLM2 740
C DO 5 I=2,N KLM2 750
C IF(X(I)-X(I-1))1,5,5 KLM2 760
C 1 TEMP=X(I) KLM2 770
C IM=I-1 KLM2 780
C DO 3 J=1,IM KLM2 790
C L=I-J KLM2 800
C IF(TEMP-X(L))2,4,4 KLM2 810
C 2 X(L+1)=X(L) KLM2 820
C 3 CONTINUE KLM2 830
C X(L)=TEMP KLM2 840
C GO TO 5 KLM2 850
C 4 X(L+1)=TEMP KLM2 860
C 5 CONTINUE KLM2 870
C KLM2 880
C SORT Y INTO ASCENDING SEQUENCE KLM2 890
C KLM2 900
C DO 10 I=2,M KLM2 910
C IF(Y(I)-Y(I-1))6,10,10 KLM2 920
C 6 TEMP=Y(I) KLM2 930
C IM=I-1 KLM2 940
C DO 8 J=1,IM KLM2 950
C L=I-J KLM2 960
C IF(TEMP-Y(L))7,9,9 KLM2 970
C 7 Y(L+1)=Y(L) KLM2 980
C 8 CONTINUE KLM2 990
C Y(L)=TEMP KLM2 1000
C GO TO 10 KLM2 1010
C 9 Y(L+1)=TEMP KLM2 1020
C 10 CONTINUE KLM2 1030
C KLM2 1040
C CALCULATE D = ABS(FN-GM) OVER THE SPECTRUM OF X AND Y KLM2 1050
C KLM2 1060
C XN=FLOAT(N) KLM2 1070
C XN1=1./XN KLM2 1080
C XM=FLOAT(M) KLM2 1090
C XM1=1./XM KLM2 1100
C D=0.0 KLM2 1110
C I=0 KLM2 1120

```

```

J=0
K=0
I=0
11 IF(X(I+1)-Y(J+1))17,13,18
12 K=1
GO TO 14
13 K=0
14 I=I+1
IF(I-N)15,21,21
15 IF(X(I+1)-X(J))14,14,16
16 IF(K)17,18,17
C
C      CHOOSE THE MAXIMUM DIFFERENCE, D
C
17 D=AMAX1(0,ABS(FLOAT(I)*XN1-FLOAT(J)*XM1))
IF(L)22,11,22
18 J=J+1
IF(I-N)19,20,20
19 IF(Y(J+1)-Y(I))19,18,17
20 L=L+1
GO TO 17
21 L=L-1
GO TO 16
C
C      CALCULATE THE STATISTIC Z
C
22 Z=D*SQRT((XN*XM)/(XN+XM))
C
C      CALCULATE THE PROBABILITY ASSOCIATED WITH Z
C
CALL SMIRN(Z,PROB)
PROB=1.0-PROB
RETURN
END

```

```

KLM21120
KLM21130
KLM21140
KLM21150
KLM21160
KLM21170
KLM21180
KLM21190
KLM21200
KLM21210
KLM21220
KLM21230
KLM21240
KLM21250
KLM21260
KLM21270
KLM21280
KLM21290
KLM21300
KLM21310
KLM21320
KLM21330
KLM21340
KLM21350
KLM21360
KLM21370
KLM21380
KLM21390
KLM21400
KLM21410
KLM21420
KLM21430
KLM21440
KLM21450

```

Subroutine SMIRN

This subroutine computes the values of Kolmogorov-Smirnov's limiting distribution for a given argument x .

$$L(x) = \begin{cases} 0 & x \leq 0 \\ 1 - 2 \sum_{k=1}^{\infty} (-1)^{k-1} \exp(-2k^2 x^2) & x > 0 \end{cases} \quad (1)$$

$L(x)$ is the limit (Kolmogorov) of the cumulative distribution function of $\sqrt{n} D_n$, and of (Smirnov) $[mn/(m+n)]^{1/2} D_{m,n}$ where:

D_n is the maximum, over all x , of the difference $|F_n(x) - F(x)|$ between the sample distribution function $F_n(x)$ and the continuous theoretical distribution function $F(x)$, and

$D_{m,n}$ is the maximum, over all x , of the difference between the two sample distribution functions $F_m(x)$ and $G_n(x)$, from two independent samples of sizes m and n .

When x is very small, the series (1) converges slowly, but, using Jacobi's Theta-functions $\theta_2(u, t)$ and $\theta_4(u, t)$:

$$\theta_2(u, t) = 2 \sum_{k=0}^{\infty} \exp [i \pi (k+1/2)^2 t] \cos [(2k+1)u]$$

$$\theta_4(u, t) = 1 - 2 \sum_{k=0}^{\infty} (-1)^{k-1} \exp (i \pi k^2 t) \cos (2ku)$$

and using the Jacobi imaginary transformation

$$\theta_4(0, t) = (-it)^{-1/2} \theta_2(0, -1/t)$$

it follows that:

$$\begin{aligned} L(x) &= \theta_4(0, 2ix^2/\pi) \\ &= (\sqrt{2\pi}/x) \sum_{k=1}^{\infty} \exp [-(2k-1)^2 \pi^2 / 8x^2] \end{aligned}$$

which converges quickly when x is small. The computation here uses, with errors $E_i(x)$, $i=1, 2$:

$$L(x) = \begin{cases} 0 & x \leq 0.27 \\ (\sqrt{2\pi}/x) \sum_{k=1}^3 \exp[-(2k-1)^2 \pi^2 / 8x^2] + E_1(x); & 0.27 < x < 1.0 \\ 1 - 2 \sum_{k=1}^4 (-1)^{k-1} \exp(-2k^2 x^2) + E_2(x) & 1.0 \leq x < 3.1 \\ 1 & 3.1 \leq x < \infty \end{cases}$$

where:

$$E_1(x) \leq 6 \cdot 10^{-15} \text{ when } x < 1$$

$$E_2(x) < 10^{-20} \text{ when } x \geq 1$$

For reference see:

- (1) E. T. Whittaker and G. N. Watson, A Course of Modern Analysis. Cambridge University Press, Cambridge, England, 1952, pp. 462-476.
- (2) W. Feller, "On the Kolmogorov-Smirnov limit theorems for empirical distributions", Annals of Math. Stat. 19, pp. 177-189.
- (3) N. Smirnov, "Table for estimating the goodness of fit of empirical distributions", Annals of Math. Stat. 19, pp. 279-281.

```

C ..... SMIR 10
C ..... SMIR 20
C ..... SMIR 30
C ..... SMIR 40
C ..... SMIR 50
C ..... SMIR 60
C ..... SMIR 70
C ..... SMIR 80
C ..... SMIR 90
C ..... SMIR 100
C ..... SMIR 110
C ..... SMIR 120
C ..... SMIR 130
C ..... SMIR 140
C ..... SMIR 150
C ..... SMIR 160
C ..... SMIR 170
C ..... SMIR 180
C ..... SMIR 190
C ..... SMIR 200
C ..... SMIR 210
C ..... SMIR 220
C ..... SMIR 230
C ..... SMIR 240
C ..... SMIR 250
C ..... SMIR 260
C ..... SMIR 270
C ..... SMIR 280
C ..... SMIR 290
C ..... SMIR 300
C ..... SMIR 310
C ..... SMIR 320
C ..... SMIR 330
C ..... SMIR 340
C ..... SMIR 350
C ..... SMIR 360
C ..... SMIR 370
C ..... SMIR 380
C ..... SMIR 390
C ..... SMIR 400
C ..... SMIR 410
C ..... SMIR 420
C ..... SMIR 430
C ..... SMIR 440
C ..... SMIR 450
C ..... SMIR 460
C ..... SMIR 470
C ..... SMIR 480
C ..... SMIR 490
C ..... SMIR 500
C ..... SMIR 510
C ..... SMIR 520
C ..... SMIR 530
C ..... SMIR 540
C ..... SMIR 550
C ..... SMIR 560
C ..... SMIR 570
C ..... SMIR 580
C ..... SMIR 590
C ..... SMIR 600
C ..... SMIR 610
C ..... SMIR 620
C ..... SMIR 630
C ..... SMIR 640
C ..... SMIR 650
C ..... SMIR 660
C ..... SMIR 670
C ..... SMIR 680
C ..... SMIR 690
C ..... SMIR 700
C ..... SMIR 710
C ..... SMIR 720
C ..... SMIR 730
C ..... SMIR 740
C ..... SMIR 750
C ..... SMIR 760
C ..... SMIR 770
C ..... SMIR 780
C ..... SMIR 790
C ..... SMIR 800
C ..... SMIR 810
C ..... SMIR 820
C ..... SMIR 830
C ..... SMIR 840
C ..... SMIR 850

```

Subroutine CHISQ

This subroutine calculates degrees of freedom and chi-square for a given contingency table A of observed frequencies with n rows (conditions) and m columns (groups). The degrees of freedom are:

$$\text{d.f.} = (n - 1) (m - 1) \quad (1)$$

If one or more cells contain an expected value less than 1.0, chi-square will be computed, but the error code will be set to one.

The following totals are computed:

$$T_i = \sum_{j=1}^m A_{ij}; \quad i = 1, 2, \dots, n \text{ (row totals)} \quad (2)$$

$$T_j = \sum_{i=1}^n A_{ij}; \quad j = 1, 2, \dots, m \text{ (column totals)} \quad (3)$$

$$GT = \sum_{i=1}^n T_i \quad \text{(grand total)} \quad (4)$$

Chi-square is obtained for two cases.

(a) For 2 x 2 table:

$$\chi^2 = \frac{GT \left(\left| \begin{matrix} A_{11} & A_{22} \\ A_{12} & A_{21} \end{matrix} \right| - \frac{GT}{2} \right)^2}{(A_{11} + A_{12})(A_{21} + A_{22})(A_{11} + A_{21})(A_{12} + A_{22})} \quad (5)$$

(b) For other contingency tables:

$$\chi^2 = \sum_{i=1}^n \sum_{j=1}^m \frac{(A_{ij} - E_{ij})^2}{E_{ij}} \quad (6)$$

where $E_{ij} = \frac{T_i T_j}{GT}$
 $i = 1, 2, \dots, n$
 $j = 1, 2, \dots, m$

```
C
C
C
C-----CHIS 10
C                                     CHIS 20
C SUBROUTINE CHISQ
C                                     CHIS 30
C PURPOSE
C   COMPUTE CHI-SQUARE FROM A CONTINGENCY TABLE
C                                     CHIS 40
C                                     CHIS 50
C                                     CHIS 60
C USAGE
C   CALL CHISQ(A,N,M,CS,NDF,IERR,TR,TC)
C                                     CHIS 70
C                                     CHIS 80
C DESCRIPTION OF PARAMETERS
C   A - INPUT MATRIX, N BY M, CONTAINING CONTINGENCY TABLE
C                                     CHIS 90
C   N - NUMBER OF ROWS IN A
C   M - NUMBER OF COLUMNS IN A
C                                     CHIS 100
C   CS - CHI-SQUARE (OUTPUT)
C                                     CHIS 110
C   NDF - NUMBER OF DEGREES OF FREEDOM (OUTPUT)
C                                     CHIS 120
C   IERR - ERROR CODE (OUTPUT)
C   0 - NORMAL CASE
C   1 - EXPECTED VALUE IS LESS THAN 1.0 IN ONE OR
C   3 - NUMBER OF DEGREES OF FREEDOM IS ZERO
C                                     CHIS 130
C   TR - WORK VECTOR OF LENGTH N
C                                     CHIS 140
C   TC - WORK VECTOR OF LENGTH M
C                                     CHIS 150
C
C REMARKS
C   IF ONE OR MORE CELLS CONTAIN AN EXPECTED VALUE (I.E.,
C   THEORETICAL VALUE) LESS THAN 1.0, CHI-SQUARE WILL BE
C   COMPUTED, BUT ERROR CODE WILL BE SET TO 1.
C   SEE REFERENCE GIVEN BELOW.
C   CHI-SQUARE IS SET TO ZERO IF EITHER N OR M IS ONE (ERROR
C   CODE 3).
C                                     CHIS 160
C                                     CHIS 170
C                                     CHIS 180
C                                     CHIS 190
C                                     CHIS 200
C                                     CHIS 210
C                                     CHIS 220
C                                     CHIS 230
C                                     CHIS 240
C                                     CHIS 250
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C   NONE
C                                     CHIS 260
C
C METHOD
C   DESCRIBED IN S. SIEGEL, "NONPARAMETRIC STATISTICS FOR THE
C   BEHAVIORAL SCIENCES", MCGRAW-HILL, NEW YORK, 1956,
C   CHAPTER 6 AND CHAPTER 8.
C                                     CHIS 270
C                                     CHIS 280
C                                     CHIS 290
C                                     CHIS 300
C                                     CHIS 310
C                                     CHIS 320
C-----CHIS 330
C
C SUBROUTINE CHISQ(A,N,M,CS,NDF,IERR,TR,TC)
C   DIMENSION A(1),TR(1),TC(1)
C                                     CHIS 340
C                                     CHIS 350
C
C   NM=N*M
C   IERR=0
C   CS=0.0
C                                     CHIS 360
C                                     CHIS 370
C
C   FIND DEGREES OF FREEDOM
C   NDF=(N-1)*(M-1)
C   IF(NDF) 5,5,10
C   5 IERR=3
C   RETURN
C                                     CHIS 380
C                                     CHIS 390
C
C   COMPUTE TOTALS OF ROWS
C   10 DO 90 I=1,N
C     TR(I)=0.0
C     IJ=I-N
C     DO 90 J=1,M
C       IJ=J+N
C       TR(I)=TR(I)+A(IJ)
C                                     CHIS 400
C                                     CHIS 410
C                                     CHIS 420
C                                     CHIS 430
C                                     CHIS 440
C                                     CHIS 450
C                                     CHIS 460
C                                     CHIS 470
C                                     CHIS 480
C                                     CHIS 490
C                                     CHIS 500
C                                     CHIS 510
C                                     CHIS 520
C                                     CHIS 530
C                                     CHIS 540
C                                     CHIS 550
C                                     CHIS 560
C                                     CHIS 570
C                                     CHIS 580
C                                     CHIS 590
C                                     CHIS 600
C                                     CHIS 610
C                                     CHIS 620
C                                     CHIS 630
C                                     CHIS 640
C                                     CHIS 650
C
C   COMPUTE TOTALS OF COLUMNS
C   IJ=0
C   DO 100 J=1,M
C     TC(J)=0.0
C     DO 100 I=1,N
C       IJ=IJ+1
C       TC(J)=TC(J)+A(IJ)
C                                     CHIS 660
C                                     CHIS 670
C                                     CHIS 680
C                                     CHIS 690
C                                     CHIS 700
C                                     CHIS 710
C                                     CHIS 720
C                                     CHIS 730
C                                     CHIS 740
C                                     CHIS 750
C
C   COMPUTE GRAND TOTAL
C   GT=0.0
C   DO 110 I=1,N
C     110 GT=GT+TR(I)
C                                     CHIS 760
C                                     CHIS 770
C                                     CHIS 780
C                                     CHIS 790
C                                     CHIS 800
C                                     CHIS 810
C
C   COMPUTE CHI SQUARE FOR 2 BY 2 TABLE (SPECIAL CASE)
C   IF(NM=4) 130,120,130
C   120 CS=GT*(ABS(A(1)*A(4)-A(2)*A(3))-GT/2.0)**2 / (TC(1)*TC(2)*TR(1)
C   1*TR(2))
C   RETURN
C                                     CHIS 820
C                                     CHIS 830
C                                     CHIS 840
C                                     CHIS 850
C                                     CHIS 860
C                                     CHIS 870
C                                     CHIS 880
C
C   COMPUTE CHI SQUARE FOR OTHER CONTINGENCY TABLES
C   130 IJ=0
C   DO 140 J=1,M
C     DO 140 I=1,N
C       IJ=IJ+1
C       E=TR(I)*TC(J)/GT
C       IF(E=1.0) 135, 140, 140
C   135 IERR=1
C   140 CS=CS+(A(IJ)-E)*(A(IJ)-E)/E
C   RETURN
C   END
C                                     CHIS 890
C                                     CHIS 900
C                                     CHIS 910
C                                     CHIS 920
C                                     CHIS 930
C                                     CHIS 940
C                                     CHIS 950
C                                     CHIS 960
C                                     CHIS 970
C                                     CHIS 980
C                                     CHIS 990
C                                     CHIS1000
```


Subroutine KRANK

The subroutine computes the Kendall rank correlation coefficient, given two vectors of n observations for two variables, A and B. The observations on each variable are ranked from 1 to n . Tied observations are assigned the average of the tied ranks. Ranks are sorted in sequence of variable A.

A correction factor for ties is obtained:

$$T_a = \sum \frac{t(t-1)}{2} \text{ for variable A} \quad (1)$$

$$T_b = \sum \frac{t(t-1)}{2} \text{ for variable B}$$

where t = number of observations tied for a given rank

The Kendall rank correlation coefficient is then computed for the following two cases:

(a) if T_a and T_b are zero,

$$\tau = \frac{S}{\frac{1}{2} n (n-1)} \quad (2)$$

where n = number of ranks

S = total score calculated for ranks in variable B by selecting each rank in turn, adding 1 for each larger rank to its right, subtracting 1 for each smaller rank to its right

(b) if T_a and/or T_b are not zero,

$$\tau = \frac{S}{\sqrt{\frac{1}{2} n (n-1) - T_a} \sqrt{\frac{1}{2} n (n-1) - T_b}} \quad (3)$$

The standard deviation is calculated:

$$s = \sqrt{\frac{2(2n+5)}{9n(n-1)}} \quad (4)$$

The significance of τ can be measured by

$$z = \frac{T}{s} \quad (5)$$

```

C .....
C KRANK 10
C KRANK 20
C KRANK 30
C SUBROUTINE KRANK KRANK 40
C KRANK 50
C KRANK 60
C PURPOSE KRANK 70
C TEST CORRELATION BETWEEN TWO VARIABLES BY MEANS OF KENDALL KRANK 80
C RANK CORRELATION COEFFICIENT KRANK 90
C KRANK 100
C USAGE KRANK 110
C CALL KRANK(A,B,R,N,TAU,SD,Z,NR) KRANK 120
C KRANK 130
C DESCRIPTION OF PARAMETERS KRANK 140
C A - INPUT VECTOR OF N OBSERVATIONS FOR FIRST VARIABLE KRANK 150
C B - INPUT VECTOR OF N OBSERVATIONS FOR SECOND VARIABLE KRANK 160
C R - OUTPUT VECTOR OF RANKED DATA OF LENGTH 2*N. SMALLEST KRANK 170
C OBSERVATION IS RANKED 1, LARGEST IS RANKED N. TIES KRANK 180
C ARE ASSIGNED AVERAGE OF TIED RANKS. KRANK 190
C N - NUMBER OF OBSERVATIONS KRANK 200
C TAU - KENDALL RANK CORRELATION COEFFICIENT (OUTPUT) KRANK 210
C SD - STANDARD DEVIATION (OUTPUT) KRANK 220
C Z - TEST OF SIGNIFICANCE OF TAU IN TERMS OF NORMAL KRANK 230
C DISTRIBUTION (OUTPUT) KRANK 240
C NR - CODE, 0 FOR UNRANKED DATA IN A AND B, 1 FOR RANKED KRANK 250
C DATA IN A AND B (INPUT) KRANK 260
C KRANK 270
C REMARKS KRANK 280
C SD AND Z ARE SET TO ZERO IF N IS LESS THAN TEN KRANK 290
C KRANK 300
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED KRANK 310
C RANK KRANK 320
C TIE KRANK 330
C KRANK 340
C METHOD KRANK 350
C DESCRIBED IN S. SIEGEL, "NONPARAMETRIC STATISTICS FOR THE KRANK 360
C BEHAVIORAL SCIENCES", MCGRAW-HILL, NEW YORK, 1956, KRANK 370
C CHAPTER 9 KRANK 380
C KRANK 390
C .....
C SUBROUTINE KRANK(A,B,R,N,TAU,SD,Z,NR) KRANK 400
C DIMENSION A(1),B(1),R(1) KRANK 410
C KRANK 420
C SD=0.0 KRANK 430
C Z=0.0 KRANK 440
C FN=N KRANK 450
C FN1=N*(N-1) KRANK 460
C DETERMINE WHETHER DATA IS RANKED KRANK 470
C KRANK 480
C IF(NR-1) 5, 10, 5 KRANK 490
C KRANK 500
C RANK DATA IN A AND B VECTORS AND ASSIGN TIED OBSERVATIONS KRANK 510
C AVERAGE OF TIED RANKS KRANK 520
C KRANK 530
C 5 CALL RANK (A,R,N) KRANK 540
C CALL RANK (B,R(N+1),N) KRANK 550
C GO TO 40 KRANK 560
C KRANK 570
C MOVE RANKED DATA TO R VECTOR KRANK 580
C KRANK 590
C KRANK 600
C 10 DO 20 I=1,N KRANK 610
C 20 R(I)=A(I) KRANK 620
C DO 30 I=1+N KRANK 630
C J=I+N KRANK 640
C 30 R(J)=B(I) KRANK 650
C KRANK 660
C KRANK 670
C SORT RANK VECTOR R IN SEQUENCE OF VARIABLE A KRANK 680
C KRANK 690
C KRANK 700
C 40 ISORT=0 KRANK 710
C DO 50 I=2,N KRANK 720
C IF(R(I)-R(I-1)) 45,50,50 KRANK 730
C 45 ISORT=ISORT+1 KRANK 740
C RSAVE=R(I) KRANK 750
C R(I)=R(I-1) KRANK 760
C R(I-1)=RSAVE KRANK 770
C I2=I+N KRANK 780
C SAVER=R(I2) KRANK 790
C R(I2)=R(I2-1) KRANK 800
C R(I2-1)=SAVER KRANK 810
C 50 CONTINUE KRANK 820
C IF(ISORT) 40,55,40 KRANK 830
C KRANK 840
C COMPUTE S ON VARIABLE B. STARTING WITH THE FIRST RANK, ADD 1 KRANK 850
C TO S FOR EACH LARGER RANK TO ITS RIGHT AND SUBTRACT 1 FOR EACH KRANK 860
C SMALLER RANK. REPEAT FOR ALL RANKS. KRANK 870
C KRANK 880
C 55 S=0.0 KRANK 890
C NM=N-1 KRANK 900
C DO 60 I=1,NM KRANK 910
C J=N+I KRANK 920
C DO 60 L=I,N KRANK 930
C K=N+L KRANK 940
C IF(R(K)-R(J)) >0,60,57 KRANK 950
C 60 S=S-1.0 KRANK 960
C GO TO 60 KRANK 970
C 57 S=S+1.0 KRANK 980
C 60 CONTINUE KRANK 990
C KRANK 1000
C COMPUTE TIED SCORE INDEX FOR BOTH VARIABLES KRANK 1010
C KRANK 1020
C KT=2 KRANK 1030
C CALL TIE(R,N,KT,TA) KRANK 1040
C CALL TIE(R(N+1),N,KT,TB) KRANK 1050
C KRANK 1060
C COMPUTE TAU KRANK 1070
C KRANK 1080
C IF(TA) 70,65,70 KRANK 1090
C 65 IF(TB) 70,67,70 KRANK 1100
C 67 TAU=S/(0.5*FN1) KRANK 1110
C GO TO 80 KRANK 1120
C 70 TAU=S/((ISORT*0.5*FN1-TA))*((ISORT*0.5*FN1-TB)) KRANK 1130
C KRANK 1140
C COMPUTE STANDARD DEVIATION AND Z IF N IS 10 OR LARGER KRANK 1150
C KRANK 1160
C 80 IF(N-1) 90,85,85 KRANK 1170
C 85 SD=(S*RT((12.0*(FN*FN+S.C))/(9.0*FN1))) KRANK 1180
C Z=TAU/SD KRANK 1190
C RETURN KRANK 1200
C END

```


Subroutine QTEST

This subroutine determines the Cochran Q-test statistic, given a matrix A of dichotomous data with n rows (sets) and m columns (groups).

Row and column totals are calculated:

$$L_i = \sum_{j=1}^m A_{ij} \quad (\text{row totals}) \quad (1)$$

where $i = 1, 2, \dots, n$

$$G_j = \sum_{i=1}^n A_{ij} \quad (\text{column totals}) \quad (2)$$

where $j = 1, 2, \dots, m$

The Cochran Q statistic is computed:

$$Q = \frac{(m-1) \left[m \sum_{j=1}^m G_j^2 - \left(\sum_{j=1}^m G_j \right)^2 \right]}{m \sum_{i=1}^n L_i - \sum_{i=1}^n L_i^2} \quad (3)$$

The degrees of freedom are:

$$d.f. = m - 1 \quad (4)$$

```

C .....
C SUBROUTINE QTEST
C .....
C PURPOSE
C TEST WHETHER THREE OR MORE MATCHED GROUPS OF DICOTOMOUS
C DATA DIFFER SIGNIFICANTLY BY THE COCHRAN Q-TEST
C .....
C USAGE
C CALL QTEST(A,N,M,Q,NDF)
C .....
C DESCRIPTION OF PARAMETERS
C A - INPUT MATRIX, N BY M, OF DICOTOMOUS DATA (0 AND 1)
C N - NUMBER OF SETS IN EACH GROUP
C M - NUMBER OF GROUPS
C Q - COCHRAN Q STATISTIC (OUTPUT)
C NDF - NUMBER OF DEGREES OF FREEDOM (OUTPUT)
C .....
C REMARKS
C M MUST BE THREE OR GREATER
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C .....
C METHOD
C DESCRIBED IN S. SIEGEL, "NONPARAMETRIC STATISTICS FOR THE
C BEHAVIORAL SCIENCES", MCGRAW-HILL, NEW YORK, 1956,
C CHAPTER 7
C .....
C SUBROUTINE QTEST(A,N,M,Q,NDF)
C DIMENSION A(1)
C .....
C COMPUTE SUM OF SQUARES OF ROW TOTALS, RSQ, AND GRAND TOTAL OF
C ALL ELEMENTS, GD
C .....
C RSQ=0.0
C GD=0.0
C DO 20 I=1,N
C TR=0.0
C IJ=1-M
C DO 10 J=1,M
C IJ=IJ+N
C 10 TR=TR+A(IJ)
C GD=GD+TR
C 20 RSQ=RSQ+TR*TR
C .....
C COMPUTE SUM OF SQUARES OF COLUMN TOTALS, CSQ
C .....
C CSQ=0.0
C IJ=0
C DO 40 J=1,M
C TC=0.0
C DO 30 I=1,N
C IJ=IJ+1
C 30 TC=TC+A(IJ)
C 40 CSQ=CSQ+TC*TC
C .....
C COMPUTE COCHRAN Q TEST VALUE
C .....
C FM=M
C Q=(FM-1.0)*(FM*CSQ-GD*GD)/(FM*GD-RSQ)
C .....
C FIND DEGREES OF FREEDOM
C .....
C NDF=M-1
C RETURN
C END

```

Subroutine RANK

```

C .....
C .....
C .....
C SUBROUTINE RANK
C .....
C PURPOSE
C RANK A VECTOR OF VALUES
C .....
C USAGE
C CALL RANK(A,R,N)
C .....
C DESCRIPTION OF PARAMETERS
C A - INPUT VECTOR OF N VALUES
C R - OUTPUT VECTOR OF LENGTH N. SMALLEST VALUE IS RANKED 1,
C LARGEST IS RANKED N. TIES ARE ASSIGNED AVERAGE OF TIED
C RANKS
C N - NUMBER OF VALUES
C .....
C REMARKS
C NONE
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C .....
C METHOD
C VECTOR IS SEARCHED FOR SUCCESSIVELY LARGER ELEMENTS. IF TIES
C OCCUR, THEY ARE LOCATED AND THEIR RANK VALUE COMPUTED.
C FOR EXAMPLE, IF 2 VALUES ARE TIED FOR SIXTH RANK, THEY ARE
C ASSIGNED A RANK OF 6.5 ((6+7)/2)
C .....
C .....
C SUBROUTINE RANK(A,R,N)
C DIMENSION A(1),R(1)
C .....
C INITIALIZATION
C .....
C DO 10 I=1,N
C 10 R(I)=0.0
C .....
C FIND RANK OF DATA
C .....
C DO 100 I=1,N
C .....
C TEST WHETHER DATA POINT IS ALREADY RANKED
C .....
C IF(R(I)) 20, 20, 100
C .....
C DATA POINT TO BE RANKED
C .....
C 20 SMALL=0.0
C EQUAL=0.0
C X=A(I)
C DO 50 J=1,N
C IF(A(J)-X) 30, 40, 50
C COUNT NUMBER OF DATA POINTS WHICH ARE SMALLER
C .....
C 30 SMALL=SMALL+1.0
C GO TO 50
C .....
C COUNT NUMBER OF DATA POINTS WHICH ARE EQUAL
C .....
C 40 EQUAL=EQUAL+1.0
C R(I)=1.0
C 50 CONTINUE
C .....
C TEST FOR TIE
C .....
C IF(EQUAL-1.0) 60, 60, 70
C .....
C STORE RANK OF DATA POINT WHERE NO TIE
C .....
C 60 R(I)=SMALL+1.0
C GO TO 100
C .....
C CALCULATE RANK OF TIED DATA POINTS
C .....
C 70 P=SMALL + (EQUAL + 1.0)*0.5
C DO 90 J=1,N
C IF(R(J)+1.0) 90, 90, 90
C 80 R(J)=P
C 90 CONTINUE
C 100 CONTINUE
C RETURN
C END

```

Subroutine SIGNT

This subroutine performs a sign test, given two vectors of n observations of two matched samples. The computational steps are as follows:

1. Find the sign of the difference between the two numbers of each pair.
2. Find K = the number of pairs whose differences are not zero (0). Disregard those pairs whose differences are zero (0).
3. Find M = the number of (+) differences or the number of (-) differences, whichever is fewer.
4. If K is less than or equal to 25, the probability associated with a value as small as the observed value of M is given by the binomial distribution as:

$$p = \sum_{i=0}^M \binom{K}{i} P^i Q^{K-i} \quad (1)$$

where $P = Q = 0.5$

$$\binom{K}{i} = \frac{K!}{i! (K-i)!}$$

The equation (1) is rewritten to simplify the calculation as follows:

$$p = \frac{\sum_{i=0}^M \binom{K}{i}}{2^K} \quad (2)$$

If K is greater than 25, the probability is calculated by the normal approximation to the binomial distribution as follows:

$$\text{Mean: } \mu = KP = \frac{1}{2} K \quad (3)$$

$$\text{Standard deviation: } \sigma = \sqrt{KPQ} = \frac{1}{2} \sqrt{K} \quad (4)$$

$$\text{Value of } Z: Z = \frac{(M+0.5) - \mu}{\sigma} \quad (5)$$

Then the probability, p , associated with the value as extreme as Z is obtained by the subroutine NDTR.

Note: p computed by this subroutine is the probability for a one-tailed test; thus for a two-tailed test, the user should double the value of p .

For reference see S. Siegel, Nonparametric Statistics for the Behavioral Sciences, McGraw-Hill, New York, 1956, chapter 5.

```

C
C ..... SIGN 10
C ..... SIGN 20
C ..... SIGN 30
SUBROUTINE SIGNT SIGN 40
C ..... SIGN 40
C ..... SIGN 50
PURPOSE SIGN 60
C TO PERFORM A NON-PARAMETRIC SIGN TEST, GIVEN TWO SETS OF SIGN 70
C MATCHED OBSERVATIONS. IT TESTS THE NULL HYPOTHESIS THAT THE SIGN 80
C DIFFERENCES BETWEEN EACH PAIR OF MATCHED OBSERVATIONS HAS A SIGN 90
C MEDIAN EQUAL TO ZERO. SIGN 100
C ..... SIGN 110
USAGE SIGN 120
C CALL SIGNT (N,A,B,K,M,P,IE) SIGN 130
C ..... SIGN 140
DESCRIPTION OF PARAMETERS SIGN 150
C N - NUMBER OF OBSERVATIONS IN SETS A AND B SIGN 160
C A - INPUT VECTOR OF LENGTH N CONTAINING DATA FROM THE FIRST SIGN 170
C SAMPLE, A SIGN 180
C B - INPUT VECTOR OF LENGTH N CONTAINING DATA FROM THE SECOND SIGN 190
C SAMPLE, B SIGN 200
C K - OUTPUT VARIABLE CONTAINING THE NUMBER OF PAIRS OF SIGN 210
C OBSERVATIONS FROM THE TWO SAMPLES WHOSE DIFFERENCES ARE SIGN 220
C NON-ZERO SIGN 230
C M - OUTPUT VARIABLE CONTAINING THE NUMBER OF PLUS OR MINUS SIGN 240
C DIFFERENCES, WHICHEVER IS FEWER. SIGN 250
C P - COMPUTED PROBABILITY OF AS FEW AS M NUMBER OF PAIRS SIGN 260
C HAVING THE SAME SIGN, ASSUMING THAT THE SAMPLES CAME SIGN 270
C FROM THE SAME POPULATION. SIGN 280
C IE= 0, IF THERE IS NO ERROR. SIGN 290
C 1, IF K IS ZERO. IN THIS CASE, P IS SET TO 1.0 AND SIGN 300
C M TO 0. SIGN 310
C ..... SIGN 320
REMARKS SIGN 330
C IF K IS LESS THAN OR EQUAL TO 25, THE PROBABILITY WILL BE SIGN 340
C COMPUTED USING THE BINOMIAL DISTRIBUTION. IF K IS GREATER SIGN 350
C THAN 25, THE PROBABILITY WILL BE COMPUTED USING THE NORMAL SIGN 360
C APPROXIMATION TO THE BINOMIAL DISTRIBUTION. SIGN 370
C P COMPUTED IS THE PROBABILITY FOR A ONE-TAILED TEST. THUS, SIGN 380
C FOR A TWO TAILED TEST, DOUBLE THE VALUE FOR P. SIGN 390
C ..... SIGN 400
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SIGN 410
C NDTR SIGN 420
C ..... SIGN 430
METHOD SIGN 440
C REFER TO DIXON AND MASSEY, INTRODUCTION TO STATISTICAL SIGN 450
C ANALYSIS (MCGRAW-HILL, 1957). SIGN 460
C ..... SIGN 470
SUBROUTINE SIGNT (N,A,B,K,M,P,IE) SIGN 480
C ..... SIGN 490
C DIMENSION A(1),B(1) SIGN 500
C DOUBLE PRECISION FN,FD SIGN 510
C ..... SIGN 520
INITIALIZATION SIGN 530
C ..... SIGN 540
C IE=0 SIGN 550
C K=0 SIGN 560
C MPLUS=0 SIGN 570
C MMIN=0 SIGN 580
C ..... SIGN 590
FIND (+) OR (-) DIFFERENCE SIGN 600
C ..... SIGN 610
DO 40 I=1,N SIGN 620
D=A(I)-B(I) SIGN 630
IF(D) 20, 40, 30 SIGN 640
C ..... SIGN 650
(-) DIFFERENCE SIGN 660
C ..... SIGN 670
20 K=K+1 SIGN 680
MMIN=MMIN+1 SIGN 690
GO TO 40 SIGN 700
C ..... SIGN 710
(+) DIFFERENCE SIGN 720
C ..... SIGN 730
30 K=K+1 SIGN 740
MPLUS=MPLUS+1 SIGN 750
C ..... SIGN 760
40 CONTINUE SIGN 770
IF(K) 41,41,42 SIGN 780
41 IE=1 SIGN 790
P=1.0 SIGN 800
M=0 SIGN 810
GO TO 95 SIGN 820
42 FK=K SIGN 830
C ..... SIGN 840
FIND THE NUMBER OF FEWER SIGNS SIGN 850
C ..... SIGN 860
IF(MPLUS-MMIN) 45, 45, 50 SIGN 870
45 M=MPLUS SIGN 880
GO TO 55 SIGN 890
50 M=MMIN SIGN 900
C ..... SIGN 910
TEST WHETHER K IS GREATER THAN 25 SIGN 920
C ..... SIGN 930
55 IF(K-25) 60, 40, 77 SIGN 940
C ..... SIGN 950
K IS LESS THAN OR EQUAL TO 25 SIGN 960
C ..... SIGN 970
60 P=1.0 SIGN 980
IF(M) 75, 75, 65 SIGN 990
65 FN=1.0 SIGN 1000
FD=1.0 SIGN 1010
DO 70 I=1,M SIGN 1020
FI=I SIGN 1030
FN=FN*(FK-(FI-1.0)) SIGN 1040
FD=FD*FI SIGN 1050
70 P=FN/FD SIGN 1060
C ..... SIGN 1070
75 P=P/(2.0**K) SIGN 1080
GO TO 95 SIGN 1090
C ..... SIGN 1100
K IS GREATER THAN 25. COMPUTE MEAN, STANDARD DEVIATION, AND Z SIGN 1110
C ..... SIGN 1120
77 U=0.5*FK SIGN 1130
S=0.5*SQRT(FK) SIGN 1140
FM=M SIGN 1150
IF(FM-U) 80, 85, 85 SIGN 1160
80 CON=0.5 SIGN 1170
GO TO 90 SIGN 1180
85 CON=0.0 SIGN 1190
90 Z=(FM+CON-U)/S SIGN 1200
C ..... SIGN 1210
COMPUTE P ASSOCIATED WITH THE VALUE AS EXTREME AS Z SIGN 1220
C ..... SIGN 1230
CALL NDTR (Z,P,D) SIGN 1240
C ..... SIGN 1250
95 RETURN SIGN 1260
END SIGN 1270
C ..... SIGN 1280
C ..... SIGN 1290

```

Subroutine SRANK

This subroutine measures the correlation between two variables by means of the Spearman rank correlation coefficient, given two vectors of n observations for the variables.

The observations on each variable are ranked from 1 to n. Tied observations are assigned the average of the tied ranks.

The sum of squares of rank differences is calculated:

$$D = \sum_{i=1}^n (A_i - B_i)^2 \quad (1)$$

where A_i = first ranked vector

B_i = second ranked vector

n = number of ranks

A correction factor for ties is obtained:

$$T_a = \sum \frac{t^3 - t}{12} \text{ over variable A} \quad (2)$$

$$T_b = \sum \frac{t^3 - t}{12} \text{ over variable B}$$

where t = number of observations tied for a given rank

The Spearman rank correlation coefficient is then computed for the following two cases:

(a) if T_a and T_b are zero,

$$r_s = 1 - \frac{6D}{n^3 - n} \quad (3)$$

(b) if T_a and/or T_b are not zero,

$$r_s = \frac{X + Y - D}{2 \sqrt{XY}} \quad (4)$$

where $X = \frac{n^3 - n}{12} - T_a$ (5)

$$Y = \frac{n^3 - n}{12} - T_b \quad (6)$$

The statistic used to measure the significance of r_s is:

$$t = r_s \sqrt{\frac{n-2}{1-r_s^2}} \quad (7)$$

The degrees of freedom are:

$$d.f. = n - 2 \quad (8)$$

```

C
C
C ..... SRAN 10
C SUBROUTINE SRANK SRAN 20
C SRAN 30
C SRAN 40
C SRAN 50
C SRAN 60
C SRAN 70
C SRAN 80
C SRAN 90
C SRAN 100
C USAGE SRAN 110
C CALL SRANK(A,B,R,N,RS,T,NDF,NR) SRAN 120
C SRAN 130
C DESCRIPTION OF PARAMETERS SRAN 140
C A - INPUT VECTOR OF N OBSERVATIONS FOR FIRST VARIABLE SRAN 150
C B - INPUT VECTOR OF N OBSERVATIONS FOR SECOND VARIABLE SRAN 160
C R - OUTPUT VECTOR FOR RANKED DATA, LENGTH IS 2*N, SMALLEST SRAN 170
C OBSERVATION IS RANKED 1, LARGEST IS RANKED N. TIES SRAN 180
C ARE ASSIGNED AVERAGE OF TIED RANKS. SRAN 190
C N - NUMBER OF OBSERVATIONS SRAN 200
C RS - SPEARMAN RANK CORRELATION COEFFICIENT (OUTPUT) SRAN 210
C T - TEST OF SIGNIFICANCE OF RS (OUTPUT) SRAN 220
C NDF - NUMBER OF DEGREES OF FREEDOM (OUTPUT) SRAN 230
C NR - CODE, 0 FOR UNRANKED DATA IN A AND B, 1 FOR RANKED SRAN 240
C DATA IN A AND B (INPUT) SRAN 250
C SRAN 260
C REMARKS SRAN 270
C T IS SET TO ZERO IF N IS LESS THAN TEN SRAN 280
C SRAN 290
C SUBROUTINES AND FUNCTION SUBPROGAMS REQUIRED SRAN 300
C RANK SRAN 310
C TIE SRAN 320
C SRAN 330
C METHOD SRAN 340
C DESCRIBED IN S. SIEGEL, 'NONPARAMETRIC STATISTICS FOR THE SRAN 350
C BEHAVIORAL SCIENCES', MCGRAW-HILL, NEW YORK, 1956, SRAN 360
C CHAPTER 9 SRAN 370
C ..... SRAN 380
C SUBROUTINE SRANK(A,B,R,N,RS,T,NDF,NR) SRAN 390
C DIMENSION A(1),B(1),R(1) SRAN 400
C SRAN 410
C SRAN 420
C FNNN=N*N*N-N SRAN 430
C SRAN 440
C DETERMINE WHETHER DATA IS RANKED SRAN 450
C SRAN 460
C IF(NR-1) 5, 10, 5 SRAN 470
C SRAN 480
C RANK DATA IN A AND B VECTORS AND ASSIGN TIED OBSERVATIONS SRAN 490
C AVERAGE OF TIED RANKS SRAN 500
C SRAN 510
C 5 CALL RANK (A,R,N) SRAN 520
C CALL RANK (B,R(N+1),N) SRAN 530
C GO TO 40 SRAN 540
C SRAN 550
C SRAN 560
C MOVE RANKED DATA TO R VECTOR SRAN 570
C SRAN 580
C 10 DO 20 I=1,N SRAN 590
C 20 R(I)=A(I) SRAN 600
C DO 30 I=1,N SRAN 610
C J=I+N SRAN 620
C 30 R(J)=B(I) SRAN 630
C SRAN 640
C COMPUTE SUM OF SQUARES OF RANK DIFFERENCES SRAN 650
C SRAN 660
C 40 D=0.0 SRAN 670
C DO 50 I=1,N SRAN 680
C J=I+N SRAN 690
C 50 D=D+(R(I)-R(J))*(R(I)-R(J)) SRAN 700
C SRAN 710
C COMPUTE TIED SCORE INDEX SRAN 720
C SRAN 730
C KI=1 SRAN 740
C CALL TIE (R,N,KI,TSA) SRAN 750
C CALL TIE (R(N+1),N,KI,TSB) SRAN 760
C SRAN 770
C COMPUTE SPEARMAN RANK CORRELATIUN COEFFICIENT SRAN 780
C SRAN 790
C IF(TSA) 60,55,60 SRAN 800
C 55 IF(TSB) 60,57,60 SRAN 810
C 57 RS=1.0-6.0*D/FNNN SRAN 820
C GO TO 70 SRAN 830
C 60 X=FNNN/12.0-TSA SRAN 840
C Y=X+TSB-TSB SRAN 850
C RS=(X+Y-D)/(2.0*(SQRT(X*Y))) SRAN 860
C SRAN 870
C COMPUTE T AND DEGREES OF FREEDOM IF N IS 10 OR LARGER SRAN 880
C SRAN 890
C T=0.0 SRAN 900
C 70 IF(N-10) 80,75,75 SRAN 910
C 75 T=RS*SQRT(FL0AT(N-2)/(1.0-RS*RS)) SRAN 920
C 80 NDF=N-2 SRAN 930
C RETURN SRAN 940
C END

```

Subroutine TIE

```

C .....
C SUBROUTINE TIE
C .....
C PURPOSE
C CALCULATE CORRECTION FACTOR DUE TO TIES
C .....
C USAGE
C CALL TIE(R,N,KT,I)
C .....
C DESCRIPTION OF PARAMETERS
C R - INPUT VECTOR OF RANKS OF LENGTH N CONTAINING VALUES
C 1 TO N
C N - NUMBER OF RANKED VALUES
C KT - INPUT CODE FOR CALCULATION OF CORRECTION FACTOR
C 1 SOLVE EQUATION 1
C 2 SOLVE EQUATION 2
C T - CORRECTION FACTOR (OUTPUT)
C EQUATION 1 T=SUM(CT**3-CT)/12
C EQUATION 2 T=SUM(CT*(CT-1)/2)
C WHERE CT IS THE NUMBER OF OBSERVATIONS TIED FOR A
C GIVEN RANK
C .....
C REMARKS
C NONE
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C .....
C METHOD
C VECTOR IS SEARCHED FOR SUCCESSIVELY LARGER RANKS. TIES ARE
C COUNTED AND CORRECTION FACTOR 1 OR 2 SUMMED.
C .....
C SUBROUTINE TIE(R,N,KT,I)
C DIMENSION R(1)
C .....
C INITIALIZATION
C .....
C T=0.0
C Y=0.0
C 5 X=1.0E38
C IND=0
C .....
C FIND NEXT LARGEST RANK
C .....
C DO 30 I=1,N
C IF(R(I)-Y) 30,30,10
C 10 IF(R(I)-X) 20,30,30
C 20 X=R(I)
C IND=IND+1
C 30 CONTINUE
C .....
C IF ALL RANKS HAVE BEEN TESTED, RETURN
C .....
C IF(IND) 90,90,40
C 40 Y=X
C CT=0.0
C .....
C COUNT TIES
C .....
C DO 60 I=1,N
C IF(R(I)-X) 60,50,60
C 50 CT=CT+1.0
C 60 CONTINUE
C .....
C CALCULATE CORRECTION FACTOR
C .....
C IF(CT) 70,5,70
C 70 IF(KT=1) 75,80,75
C 75 T=T+CT*(CT-1)/2.0
C GO TO 5
C 80 T=T+(CT*CT*CT-CT)/12.0
C GO TO 5
C 90 RETURN
C END

```

Subroutine TWOAV

This subroutine determines the Friedman two-way analysis of variance statistic, given a matrix A with n rows (groups) and m columns (cases). Data in each group is ranked from 1 to m. Tied observations are assigned the average of the tied ranks.

The sum of ranks is calculated:

$$R_j = \sum_{i=1}^n A_{ij} \quad (1)$$

Friedman's statistic is then computed:

$$\chi_r^2 = \frac{12}{nm(m+1)} \sum_{j=1}^m (R_j)^2 - 3n(m+1) \quad (2)$$

The degrees of freedom are:

$$d.f. = m - 1 \quad (3)$$

```

C .....
C SUBROUTINE TWOAV
C .....
C PURPOSE
C TEST WHETHER A NUMBER OF SAMPLES ARE FROM THE SAME
C POPULATION BY THE FRIEDMAN TWO-WAY ANALYSIS OF VARIANCE TEST
C .....
C USAGE
C CALL TWOAV(A,R,N,M,W,XR,NDF,NR)
C .....
C DESCRIPTION OF PARAMETERS
C A - INPUT MATRIX, N BY M, OF ORIGINAL DATA
C R - OUTPUT MATRIX, N BY M, OF RANKED DATA
C N - NUMBER OF GROUPS
C M - NUMBER OF CASES IN EACH GROUP
C W - WORK AREA OF LENGTH 2*M
C XR - FRIEDMAN STATISTIC (OUTPUT)
C NDF - NUMBER OF DEGREES OF FREEDOM (OUTPUT)
C NR - CODE, 0 FOR UNRANKED DATA IN A, 1 FOR RANKED DATA
C IN A (INPUT)
C .....
C REMARKS
C NONE
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C RANK
C .....
C METHOD
C DESCRIBED IN S. SIEGEL, "NONPARAMETRIC STATISTICS FOR THE
C BEHAVIORAL SCIENCES", MCGRAW-HILL, NEW YORK, 1956,
C CHAPTER 7
C .....
C SUBROUTINE TWOAV (A,R,N,M,W,XR,NDF,NR)
C DIMENSION A(1),R(1),W(1)
C .....
C DETERMINE WHETHER DATA IS RANKED
C .....
C IF(NR=1) 10, 30, 10
C .....
C RANK DATA IN EACH GROUP AND ASSIGN TIED OBSERVATIONS AVERAGE
C OF TIED RANK
C .....
C 10 DO 20 I=1,N
C IJ=1-N
C IK=IJ
C DO 15 J=1,M
C IJ=IJ+N
C 15 W(J)=A(IJ)
C CALL RANK (W,W(M*1),M)
C DO 20 J=1,M
C IK=IK+N
C IW=M+J
C 20 R(IK)=W(IW)
C GO TO 35
C 30 NM=N*M
C DO 32 I=1,NM
C 32 R(I)=A(I)
C .....
C CALCULATE SUM OF SQUARES OF SUMS OF RANKS
C .....
C 35 RTSQ=0.0
C IR=0
C DO 50 J=1,M
C RT=0.0
C DO 40 I=1,N
C IR=IR+1
C 40 RT=RT+A(IK)
C 50 RTSQ=RTSQ+RT*RT
C .....
C CALCULATE FRIEDMAN TEST VALUE, XR
C .....
C FNM=N*(M+1)
C F=M*M
C XR=(12.0/(F*M*FNM))*RTSQ-3.0*FNM
C .....
C FIND DEGREES OF FREEDOM
C .....
C NDF=M-1
C RETURN
C END

```

Subroutine UTEST

This subroutine tests whether two independent groups are from the same population by means of the Mann-Whitney U-test, given an input vector A with the smaller group preceding the larger group. The scores for both groups are ranked together in ascending order. Tied observations are assigned the average of the tied ranks.

The sum of ranks in the larger group, R2, is calculated. The U statistic is then computed as follows:

$$U' = n_1 n_2 + \frac{n_2 (n_2 + 1)}{2} - R_2 \quad (1)$$

where n_1 = number of cases in smaller group

n_2 = number of cases in larger group

$$U = n_1 n_2 - U'$$

if $U' < U$, set $U = U'$ (2)

A correction factor for ties is obtained:

$$T = \sum \frac{t^3 - t}{12} \quad (3)$$

where t = number of observations tied for a given rank

The standard deviation is computed for two cases:

(a) if $T = 0$

$$s = \sqrt{\frac{n_1 n_2 (n_1 + n_2 + 1)}{12}} \quad (4)$$

(b) if $T > 0$

$$s = \sqrt{\left(\frac{n_1 n_2}{N(N-1)}\right) \left(\frac{N^3 - N}{12} - T\right)} \quad (5)$$

where N = total number of cases ($n_1 + n_2$)

The significance of U can be measured by

$$Z = \frac{U - \bar{X}}{s} \quad (6)$$

where $\bar{X} = \text{mean} = \frac{n_1 n_2}{2}$

Z is set to zero if n_2 is less than 20.

```

C          UTEST 10
C          ..... UTEST 20
C          ..... UTEST 30
C          ..... UTEST 40
C          ..... UTEST 50
C          ..... UTEST 60
C          ..... UTEST 70
C          ..... UTEST 80
C          ..... UTEST 90
C          ..... UTEST 100
C          ..... UTEST 110
C          ..... UTEST 120
C          ..... UTEST 130
C          ..... UTEST 140
C          ..... UTEST 150
C          ..... UTEST 160
C          ..... UTEST 170
C          ..... UTEST 180
C          ..... UTEST 190
C          ..... UTEST 200
C          ..... UTEST 210
C          ..... UTEST 220
C          ..... UTEST 230
C          ..... UTEST 240
C          ..... UTEST 250
C          ..... UTEST 251
C          ..... UTEST 252
C          ..... UTEST 260
C          ..... UTEST 270
C          ..... UTEST 280
C          ..... UTEST 290
C          ..... UTEST 300
C          ..... UTEST 310
C          ..... UTEST 320
C          ..... UTEST 330
C          ..... UTEST 340
C          ..... UTEST 350
C          ..... UTEST 360
C          ..... UTEST 370
C          ..... UTEST 380
C          ..... UTEST 390
C          ..... UTEST 400
C          ..... UTEST 410
C          ..... UTEST 420
C          ..... UTEST 430
C          ..... UTEST 440
C          ..... UTEST 450
C          ..... UTEST 460
C          ..... UTEST 470
C          ..... UTEST 480
C          ..... UTEST 490
C          ..... UTEST 500
C          ..... UTEST 510
C          ..... UTEST 520
C          ..... UTEST 530
C          ..... UTEST 540
C          ..... UTEST 550
C          ..... UTEST 560
C          ..... UTEST 570
C          ..... UTEST 580
C          ..... UTEST 590
C          ..... UTEST 600
C          ..... UTEST 610
C          ..... UTEST 620
C          ..... UTEST 630
C          ..... UTEST 640
C          ..... UTEST 650
C          ..... UTEST 660
C          ..... UTEST 670
C          ..... UTEST 680
C          ..... UTEST 690
C          ..... UTEST 700
C          ..... UTEST 710
C          ..... UTEST 720
C          ..... UTEST 730
C          ..... UTEST 740
C          ..... UTEST 750
C          ..... UTEST 760
C          ..... UTEST 761
C          ..... UTEST 762
C          ..... UTEST 763
C          ..... UTEST 770
C          ..... UTEST 780
C          ..... UTEST 790
C          ..... UTEST 800
C          ..... UTEST 810
C          ..... UTEST 820
C          ..... UTEST 830
C          ..... UTEST 840
C          ..... UTEST 850

C          SUBROUTINE UTEST
C          PLUPCASE
C          TEST WHETHER TWO INDEPENDENT GROUPS ARE FROM THE SAME
C          POPULATION BY MEANS OF MANN-WHITNEY U-TEST
C          LSPACE
C          CALL UTEST(A,R,N1,N2,L,Z,IER)
C          DESCRIBTION OF PARAMETERS
C          A - INPUT VECTOR OF CASES CONSISTING OF TWO INDEPENDENT
C          GROUPS - SMALLER GROUP PRECEDES LARGER GROUP. LENGTH
C          IS N1+N2.
C          R - UTEST VECTOR OF RANKS. SMALLEST VALUE IS RANKED 1.
C          LARGEST IS RANKED N. TIES ARE ASSIGNED AVERAGE OF TIED
C          RANKS. LENGTH IS N1+N2.
C          N1 - NUMBER OF CASES IN SMALLER GROUP
C          N2 - NUMBER OF CASES IN LARGER GROUP
C          L - STATISTIC USED TO TEST HOMOGENEITY OF THE TWO
C          GROUPS (UPLT)
C          Z - MEASURE OF SIGNIFICANCE OF U IN TERMS OF NORMAL
C          DISTRIBUTION (UPLT)
C          IER- 0, IF NO ERROR
C          - 1, IF ALL VALUES OF ONE GROUP ARE TIED.
C          REPAIRS
C          Z IS SET TO ZERO IF N2 IS LESS THAN 20
C          SUBROUTINES AND FUNCTIONAL PROGRAMS REQUIRED
C          RANK
C          TIE
C          METHC
C          DESCRIBED IN S. SIEGEL, 'NONPARAMETRIC STATISTICS FOR THE
C          BEHAVIORAL SCIENCES', MCCRAW-HILL, NEW YORK, 1956,
C          CHAPTER 6
C          ..... UTEST 390
C          ..... UTEST 400
C          ..... UTEST 410
C          ..... UTEST 420
C          ..... UTEST 430
C          ..... UTEST 440
C          ..... UTEST 450
C          ..... UTEST 460
C          ..... UTEST 470
C          ..... UTEST 480
C          ..... UTEST 490
C          ..... UTEST 500
C          ..... UTEST 510
C          ..... UTEST 520
C          ..... UTEST 530
C          ..... UTEST 540
C          ..... UTEST 550
C          ..... UTEST 560
C          ..... UTEST 570
C          ..... UTEST 580
C          ..... UTEST 590
C          ..... UTEST 600
C          ..... UTEST 610
C          ..... UTEST 620
C          ..... UTEST 630
C          ..... UTEST 640
C          ..... UTEST 650
C          ..... UTEST 660
C          ..... UTEST 670
C          ..... UTEST 680
C          ..... UTEST 690
C          ..... UTEST 700
C          ..... UTEST 710
C          ..... UTEST 720
C          ..... UTEST 730
C          ..... UTEST 740
C          ..... UTEST 750
C          ..... UTEST 760
C          ..... UTEST 761
C          ..... UTEST 762
C          ..... UTEST 763
C          ..... UTEST 770
C          ..... UTEST 780
C          ..... UTEST 790
C          ..... UTEST 800
C          ..... UTEST 810
C          ..... UTEST 820
C          ..... UTEST 830
C          ..... UTEST 840
C          ..... UTEST 850
          
```

Subroutine WTEST

This subroutine computes the Kendall coefficient of concordance, given a matrix A of n rows (variables) and m columns (cases). The observations on all variables are ranked from 1 to m. Tied observations are assigned the average of the tied ranks.

A correction factor for ties is obtained:

$$T = \sum_{i=1}^n \frac{t^3 - t}{12} \quad (1)$$

where t = number of observations tied for a given rank

Sums of ranks are calculated:

$$Y_j = \sum_{i=1}^n R_{ij} \quad (2)$$

where j = 1, 2, ..., m

From these, the mean of sums of ranks is found:

$$\bar{R} = \frac{\sum_{j=1}^m Y_j}{m} \quad (3)$$

The sum of squares of deviations is derived:

$$s = \sum_{j=1}^m (Y_j - \bar{R})^2 \quad (4)$$

The Kendall coefficient of concordance is then computed:

$$W = \frac{s}{\frac{1}{12} n^2 (m^3 - m) - nT} \quad (5)$$

For m larger than 7, chi-square is:

$$\chi^2 = n(m-1)W \quad (6)$$

The degrees of freedom are:

$$d.f. = n-1 \quad (7)$$

```

C ..... WTES 10
C ..... WTES 20
C ..... WTES 30
SUBROUTINE WTEST
C ..... WTES 40
C ..... WTES 50
PURPOSE
C ..... WTES 60
TEST DEGREE OF ASSOCIATION AMONG A NUMBER OF VARIABLES BY
C ..... WTES 70
THE KENDALL COEFFICIENT OF CONCORDANCE
C ..... WTES 80
C ..... WTES 90
USAGE
CALL WTEST(A,N,M,WA,W,CS,NDF,NR)
C ..... WTES 100
C ..... WTES 110
DESCRIPTION OF PARAMETERS
A - INPUT MATRIX, N BY M, OF ORIGINAL DATA
C ..... WTES 120
K - OUTPUT MATRIX, N BY M, OF RANKED DATA, SMALLEST VALUE
C ..... WTES 130
IS RANKED 1, LARGEST IS RANKED N. TIES ARE ASSIGNED
C ..... WTES 140
AVERAGE OF TIED RANKS
N - NUMBER OF VARIABLES
C ..... WTES 150
M - NUMBER OF CASES
C ..... WTES 160
WA - WORK AREA VECTOR OF LENGTH 2*M
C ..... WTES 170
W - KENDALL COEFFICIENT OF CONCORDANCE (OUTPUT)
C ..... WTES 180
CS - CHI-SQUARE (OUTPUT)
C ..... WTES 190
NDF - NUMBER OF DEGREES OF FREEDOM (OUTPUT)
C ..... WTES 200
NR - CORRECTION FOR UNRANKED DATA IN A, 1 FOR RANKED DATA
C ..... WTES 210
IN A (INPUT)
C ..... WTES 220
C ..... WTES 230
REMARKS
C ..... WTES 240
CHI-SQUARE IS SET TO ZERO IF M IS 7 OR SMALLER
C ..... WTES 250
C ..... WTES 260
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C ..... WTES 270
NONE
C ..... WTES 280
C ..... WTES 290
METHOD
C ..... WTES 300
DESCRIBED IN S. SIEGEL, "NONPARAMETRIC STATISTICS FOR THE
C ..... WTES 310
BEHAVIORAL SCIENCES", ALDRIN-HILL, NEW YORK, 1956,
C ..... WTES 320
CHAPTER 9
C ..... WTES 330
C ..... WTES 340
C ..... WTES 350
SUBROUTINE WTEST (A,N,M,WA,W,CS,NDF,NR)
C ..... WTES 360
DIMENSION A(1),R(1),WA(1)
C ..... WTES 370
C ..... WTES 380
C ..... WTES 390
C ..... WTES 400
C ..... WTES 410
C ..... WTES 420
C ..... WTES 430
C ..... WTES 440
C ..... WTES 450
C ..... WTES 460
C ..... WTES 470
C ..... WTES 480
C ..... WTES 490
C ..... WTES 500
C ..... WTES 510
C ..... WTES 520
C ..... WTES 530
C ..... WTES 540
C ..... WTES 550
C ..... WTES 560
C ..... WTES 570
C ..... WTES 580
C ..... WTES 590
C ..... WTES 600
C ..... WTES 610
C ..... WTES 620
C ..... WTES 630
C ..... WTES 640
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C ..... WTES 660
C ..... WTES 670
C ..... WTES 680
C ..... WTES 690
C ..... WTES 700
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C ..... WTES 750
C ..... WTES 760
C ..... WTES 770
C ..... WTES 780
C ..... WTES 790
C ..... WTES 800
C ..... WTES 810
C ..... WTES 820
C ..... WTES 830
C ..... WTES 840
C ..... WTES 850
C ..... WTES 860
C ..... WTES 870
C ..... WTES 880
C ..... WTES 890
C ..... WTES 900
C ..... WTES 910
C ..... WTES 920
C ..... WTES 930
C ..... WTES 940
C ..... WTES 950
C ..... WTES 960
C ..... WTES 970
C ..... WTES 980
C ..... WTES 990
C ..... WTES 1000

```


Generation of Random Variates; Distribution Functions

Generators

Subroutine RANDU

```

C RAND 10
C ..... RAND 20
C SUBROUTINE RANDU RAND 30
C PURPOSE RAND 40
C COMPUTES UNIFORMLY DISTRIBUTED RANDOM REAL NUMBERS BETWEEN RAND 50
C 0 AND 1.0 AND RANDOM INTEGERS BETWEEN ZERO AND RAND 60
C 2**31. EACH ENTRY USES AS INPUT AN INTEGER RANDOM NUMBER RAND 70
C AND PRODUCES A NEW INTEGER AND REAL RANDOM NUMBER. RAND 80
C USAGE RAND 90
C CALL RANDU(IK,IY,YFL) RAND 100
C DESCRIPTION OF PARAMETERS RAND 110
C IK - FOR THE FIRST ENTRY THIS MUST CONTAIN ANY ODD INTEGER RAND 120
C NUMBER WITH NINE OR LESS DIGITS. AFTER THE FIRST ENTRY, RAND 130
C IK SHOULD BE THE PREVIOUS VALUE OF IK COMPUTED BY THIS RAND 140
C SUBROUTINE. RAND 150
C IY - A RESULTANT INTEGER RANDOM NUMBER REQUIRED FOR THE NEXT RAND 160
C ENTRY TO THIS SUBROUTINE. THE RANGE OF THIS NUMBER IS RAND 170
C BETWEEN ZERO AND 2**31. RAND 180
C YFL - THE RESULTANT UNIFORMLY DISTRIBUTED, FLOATING POINT, RAND 190
C RANDOM NUMBER IN THE RANGE 0 TO 1.0. RAND 200
C REMARKS RAND 210
C THIS SUBROUTINE IS SPECIFIC TO SYSTEM/360 AND WILL PRODUCE RAND 220
C 2**29 TERMS BEFORE REPEATING. THE REFERENCE BELOW DISCUSSES RAND 230
C SEEDS (65539 HERE), RUN PROBLEMS, AND PROBLEMS CONCERNING RAND 240
C RANDOM DIGITS USING THIS GENERATION SCHEME. MACLAREN AND RAND 250
C MARGAULTA, JACR 12, P. 38-39, DISCUSS CONVENTIONAL RAND 260
C GENERATION METHODS AND TESTS. THE USE OF THE GENERATORS OF RAND 270
C THE RANDU TYPE, ONE FILLING A TABLE AND ONE PICKING FROM THE RAND 280
C TABLE, IS OF BENEFIT IN SOME CASES. 65549 HAS BEEN RAND 290
C SUGGESTED AS A SEED WHICH HAS BETTER STATISTICAL PROPERTIES RAND 300
C FOR HIGH ORDER BITS OF THE GENERATED DEVIATE. RAND 310
C SEEDS SHOULD BE CHOSEN IN ACCORDANCE WITH THE DISCUSSION RAND 320
C GIVEN IN THE REFERENCE BELOW. ALSO, IT SHOULD BE NOTED THAT RAND 330
C IF FLOATING POINT RANDOM NUMBERS ARE DESIRED, AS ARE RAND 340
C AVAILABLE FROM RANDU, THE RANDOM CHARACTERISTICS OF THE RAND 350
C FLOATING POINT DEVIATES ARE MODIFIED AND IN FACT THESE RAND 360
C DEVIATES HAVE HIGH PROBABILITY OF HAVING A TRAILING LOW RAND 370
C ORDER ZERO BIT IN THEIR FRACTIONAL PART. RAND 380
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED RAND 390
C NAME RAND 400
C METHOD RAND 410
C POWER RESIDUE METHOD DISCUSSED IN IBM MANUAL C20-3011, RAND 420
C RANDOM NUMBER GENERATION AND TESTING. RAND 430
C ..... RAND 440
C SUBROUTINE RANDU(IK,IY,YFL) RAND 450
C IY=IK*65539 RAND 460
C IF(IY).GT.0 RAND 470
C IY=IY*2147483647+1 RAND 480
C YFL=IY RAND 490
C YFL=YFL*.46069138-9 RAND 500
C RETURN RAND 510
C END

```

65539

Subroutine GAUSS

This subroutine computes a normally distributed random number with a given mean and standard deviation.

An approximation to normally distributed random numbers Y can be found from a sequence of uniform random numbers† using the formula:

$$Y = \frac{\sum_{i=1}^K X_i - \frac{K}{2}}{\sqrt{K/12}} \quad (1)$$

where X_i is a uniformly distributed random number, $0 < X_i < 1$

K is the number of values X_i to be used

Y approaches a true normal distribution asymptotically as K approaches infinity. For this subroutine, K was chosen as 12 to reduce execution time.

Equation (1) thus becomes:

$$Y = \sum_{i=1}^{12} X_i - 6.0$$

The adjustment for the required mean and standard deviation is then:

$$Y' = Y * S + AM \quad (2)$$

where Y' is the required normally distributed random number

S is the required standard deviation

AM is the required mean

```

C ..... GAUS 10
C SUBROUTINE GAUSS GAUS 20
C PURPOSE GAUS 30
C COMPUTES A NORMALLY DISTRIBUTED RANDOM NUMBER WITH A GIVEN GAUS 40
C MEAN AND STANDARD DEVIATION GAUS 50
C USAGE GAUS 60
C CALL GAUSS(IK,S,AM,V) GAUS 70
C DESCRIPTION OF PARAMETERS GAUS 80
C IK - IK MUST CONTAIN AN ODD INTEGER NUMBER WITH NINE OR GAUS 90
C LESS DIGITS ON THE FIRST ENTRY TO GAUSS. THEREAFTER GAUS 100
C IT WILL CONTAIN A UNIFORMLY DISTRIBUTED INTEGER RANDOM GAUS 110
C NUMBER GENERATED BY THE SUBROUTINE FOR USE ON THE NEXT GAUS 120
C ENTRY TO THE SUBROUTINE. GAUS 130
C S - THE DESIRED STANDARD DEVIATION OF THE NORMAL GAUS 140
C DISTRIBUTION. GAUS 150
C AM - THE DESIRED MEAN OF THE NORMAL DISTRIBUTION GAUS 160
C V - THE VALUE OF THE COMPUTED NORMAL RANDOM VARIABLE GAUS 170
C REMARKS GAUS 180
C THIS SUBROUTINE USES RANDU WHICH IS MACHINE SPECIFIC GAUS 190
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED GAUS 200
C NAME GAUS 210
C METHOD GAUS 220
C USES 12 UNIFORM RANDOM NUMBERS TO COMPUTE NORMAL RANDOM GAUS 230
C NUMBERS BY CENTRAL LIMIT THEOREM. THE RESULT IS THEN GAUS 240
C ADJUSTED TO MATCH THE GIVEN MEAN AND STANDARD DEVIATION. GAUS 250
C THE UNIFORM RANDOM NUMBERS COMPUTED WITHIN THE SUBROUTINE GAUS 260
C ARE FOUND BY THE POWER RESIDUE METHOD. GAUS 270
C ..... GAUS 280
C SUBROUTINE GAUSS(IK,S,AM,V) GAUS 290
C A=0.0 GAUS 300
C DU 50 I=1,12 GAUS 310
C CALL RANDU(IK,IY,Y) GAUS 320
C IX=IY GAUS 330
C 50 A=A+Y GAUS 340
C V=(A-6.0)/S*AM GAUS 350
C RETURN GAUS 360
C END GAUS 370

```

† R. W. Hamming, Numerical Methods for Scientists and Engineers, McGraw-Hill, N. Y., 1962, pages 34 and 389.

Distribution Functions

Subroutine NDTR

This subroutine computes $y = P(x) = \text{Prob}(X \leq x)$, where X is a random variable distributed normally with mean zero and variance one.

$$P(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^x \exp(-u^2/2) du$$

The following approximation[†] is used:

$$P(x) = 1 - f(x) \sum_{i=1}^5 a_i w^i; x \geq 0$$

where:

- $w = 1/(1 + px)$
- $f(x) = \exp(-x^2/2) / \sqrt{2\pi}$
- $P = 0.2316419$
- $a_1 = 0.3193815$
- $a_2 = -0.3565638$
- $a_3 = 1.781478$
- $a_4 = -1.821256$
- $a_5 = 1.330274$

The maximum error is $7(10^{-7})$; $f(x)$ is also presented in output.

[†]C. Hastings, Approximations for Digital Computers. Princeton University Press, Princeton, N. J., 1955.

M. Abramowitz and I. A. Stegun, Handbook of Mathematical Functions. Dover Publications, Inc., N. Y., equation 26.2.17.

Subroutine BDTR

This subroutine computes $P=I_x(m,n)=\text{Prob}(X \leq x)$ where X is a random variable following the beta distribution with degrees of freedom (continuous parameters) m and n . For computation to take place, $0 \leq x \leq 1$, $0.5 \leq m \leq 10^{+5}$, and $0.5 \leq n \leq 10^{+5}$. D , the ordinate of the beta density at x , is also presented in the output.

For $0 \leq x \leq 1$, $I_x(m,n)$ may be written as:

$$I_x(m,n) = \int_0^x f(m,n,y) dy$$

where:

$$f(m,n,y) = \frac{1}{B(m,n)} y^{m-1} (1-y)^{n-1} \tag{1}$$

$$B(m,n) = \frac{\Gamma(m)\Gamma(n)}{\Gamma(m+n)}; D = f(m,n,x)$$

$I_x(m,n)$ can be reduced to a binomial partial sum which can be evaluated by means of a continued fraction expansion.

Let $N = m+n-1$ and $r = m-1$. Then:

$$I_x(m,n) = I_x(r+1, N-r)$$

$$I_x(r+1, N-r) = \sum_{s=r+1}^N \binom{N}{s} x^s (1-x)^{N-s} \tag{2}$$

$$= \binom{N}{r+1} x^{r+1} (1-x)^{N-r-1} S$$

where $0 \leq s \leq N$

S is a continued fraction, with 80 terms being sufficient for the desired accuracy.

$$S = \frac{1}{1-} \frac{c_1}{1+} \frac{d_1}{1-} \frac{c_2}{1+} \frac{d_2}{1-} \dots \frac{c_{80}}{1+} \frac{d_{80}}{1} \tag{3}$$

$$c_i = \frac{(N-i-r)(r+i)}{(r+2i-1)(r+2i)} \frac{x}{1-x} \tag{4}$$

$$d_i = \frac{i(N+i)}{(r+2i+1)(r+2i)} \frac{x}{1-x} \tag{5}$$

```

C-----NDTR 10
C-----NDTR 20
C-----NDTR 30
C-----NDTR 40
C-----NDTR 50
C-----NDTR 60
C-----NDTR 70
C-----NDTR 80
C-----NDTR 90
C-----NDTR 100
C-----NDTR 110
C-----NDTR 120
C-----NDTR 130
C-----NDTR 140
C-----NDTR 150
C-----NDTR 160
C-----NDTR 170
C-----NDTR 180
C-----NDTR 190
C-----NDTR 200
C-----NDTR 210
C-----NDTR 220
C-----NDTR 230
C-----NDTR 240
C-----NDTR 250
C-----NDTR 260
C-----NDTR 270
C-----NDTR 280
C-----NDTR 290
C-----NDTR 300
C-----NDTR 310
C-----NDTR 320
C-----NDTR 330
C-----NDTR 340
C-----NDTR 350
C-----NDTR 360
C-----NDTR 370
C-----NDTR 380
C-----NDTR 390
C-----NDTR 400
C-----NDTR 410
C-----NDTR 420
C-----NDTR 430
C-----NDTR 440
C-----NDTR 450
SUBROUTINE NDTR(X,P,D)
AX=ARS(X)
T=1.0/((1.0+.2216419*AX)
D=0.765765238EAP1-XXX/2.0)
P=1.0-D*TE((111.310274*T-1.821256)*T+1.781478)*T-
1 G.3565638)*T+0.3193815)
IF(X)1,2,2
1 P=1.C-P
2 RETURN
END

```

The above continued fraction expansion of $I_x(m, n)$ holds for positive m and n (integers or nonintegers), $N \geq 0$ ($m+n \geq 1$), and $r \geq 0$ ($m \geq 1$). In order to fulfill these last two conditions, if $m < 1$, the following transformation must be made before computation of $I_x(m, n)$ can take place:

$$I_x(m, n) = \frac{\Gamma(m+n)}{\Gamma(m+1)\Gamma(n)} x^m(1-x)^n + I_x(m+1, n) \quad (6)$$

The quantities on the right-hand side of equation (6) are those which are computed.

It is known that $I_x(m, n) = I_{1-x}(n, m)$. Thus, either of the two parameter sets indicated by this equation may be used in computing the beta integral. The parameter set selection is made by applying the following empirically derived rule:

Let p and q be the degrees of freedom corresponding to z , where $z = x$ if $x \leq .5$ or $(1-x)$ otherwise. If the quantity $[(p-1) - (p+q-1)z^{6/5} + 2]$ is positive, use the parameter set corresponding to z . Otherwise, use the parameter set corresponding to $(1-z)$.

If $0 \leq x \leq 10^{-8}$ or $0 \leq 1-x \leq 10^{-8}$, the approximation is made that $x = 0$ or 1 respectively. P and D are then set according to the following table:

$0 \leq x \leq 10^{-8}$	$0 \leq 1-x \leq 10^{-8}$
$P = 0$	$P = 1$
If: $A < 1$ then: $D = 10^{75}$	If: $B < 1$ then: $D = 10^{75}$
$A = 1$ then: $D = 1/B(m, n)$	$B = 1$ then: $D = 1/B(m, n)$
$A > 1$ then: $D = 0$	$B > 1$ then: $D = 0$

If either or both m and n are within 10^{-8} of 1 , the beta integral is solved explicitly for $m = 1$, $n = 1$, or $m = n = 1$:

If: $A = 1, B = 1$	then: $P = x$
$A = 1, B \neq 1$	$P = 1 - (1-x)^n$
$A \neq 1, B = 1$	$P = x^m$

If m or n is greater than 1000 , the chi-square approximation is used:

$z_1 = 2m(1-x)/x$ is distributed as χ^2 with $2n$ degrees of freedom and $P = 1 - P_{\chi^2}(z_1)$ for $m > 1000$.

$z_2 = 2nx/(1-x)$ is distributed as χ^2 with $2m$ degrees of freedom and $P = P_{\chi^2}(z_2)$ for $n > 1000$.

If both m and n are greater than 1000 , the approximation corresponding to z_1 is used.

The values of P very near zero or one may be somewhat imprecise. To eliminate possible misinterpretation of results, if $0 \leq P \leq 10^{-8}$ or $1 - P \leq 10^{-8}$, P is set to 0 or 1 respectively.

For reference see:

- R. E. Bargmann and S. P. Ghosh, Statistical Description Programs For a Computer Language. IBM Research Report RC-1094, 1963.
- M. Abramowitz and I. A. Stegun, Handbook of Mathematical Functions. U. S. Department of Commerce, National Bureau of Standards Applied Mathematics Series, 1966.

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C .....
C BDFR 10
C BDFR 20
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C BDFR 420
C BDFR 430
C BDFR 440
C BDFR 450
C BDFR 460
C BDFR 470
C BDFR 480
C BDFR 490
C BDFR 500
C BDFR 510
C BDFR 520
C BDFR 530
C BDFR 540
C BDFR 550
C BDFR 560
C BDFR 570
C BDFR 580
C BDFR 590

```

```

C      COMPUTE LOG(BETA(A,B))
C
60 AA=DBLE(A)
   BB=DBLE(B)
   CALL DLGAM(AA,G1,IOK)
   CALL DLGAM(BB,G2,IOK)
   CALL DLGAM(AA+BB,G3,IOK)
   DLBETA=G1+G2-G3
C
C      TEST FOR X NEAR 0.0 OR 1.0
C
   IF(X-1.E-8) 80,80,70
70 IF((1.-X)-1.E-8) 130,130,140
80 P=0.0
   IF(A-1.) 90,100,120
90 D=1.E+75
   GO TO 660
100 DD=DLBETA
   IF(DD+1.68002) 120,120,110
110 DD=DEXP(DD)
   D=SNGL(DD)
   GO TO 660
120 D=0.0
   GO TO 660
130 P=1.0
   IF(B-1.) 90,100,120
C
C      SET PROGRAM PARAMETERS
C
140 XX=DBLE(X)
   DLXX=DLG(XX)
   DLIX=DLG(1.00-XX)
   XO=XX/(1.00-XX)
   ID=0
C
C      COMPUTE ORDINATE
C
   DD=(A-1.00)*DLXX+(BB-1.00)*DLIX-DLBETA
   IF(DD-1.68002) 150,150,160
150 IF(DD+1.68002) 170,170,180
160 D=1.E75
   GO TO 190
170 D=0.0
   GO TO 190
180 DD=DEXP(DD)
   D=SNGL(DD)
C
C      A OR B OR BOTH WITHIN 1.E-8 OF 1.0
C
190 IF(ABS(A-1.)-1.E-8) 200,200,210
200 IF(ABS(B-1.)-1.E-8) 220,220,230
210 IF(ABS(B-1.)-1.E-8) 260,260,290
220 P=X
   GO TO 660
230 PP=BB*DLIX
   IF(PP+1.68002) 240,240,250
240 P=1.0
   GO TO 660
250 PP=DEXP(PP)
   PP=1.00-PP
   P=SNGL(PP)
   GO TO 660
260 PP=AA*DLXX
   IF(PP+1.68002) 270,270,280
270 P=0.0
   GO TO 660
280 PP=DEXP(PP)
   P=SNGL(PP)
   GO TO 660
C
C      TEST FOR A OR B GREATER THAN 1000.0
C
290 IF(A-1000.) 300,300,310
300 IF(B-1000.) 330,330,320
310 XX=2.00*AA/XO
   XS=SNGL(XX)
   AA=2.00*BB
   DF=SNGL(AA)
   CALL CDTR(XS,DF,P,DUMMY,IER)
   P=1.0-P
   GO TO 670
320 XX=2.00*BB*XD
   XS=SNGL(XX)
   AA=2.00*AA
   DF=SNGL(AA)
   CALL CDTR(XS,DF,P,DUMMY,IER)
   GO TO 670
C
C      SELECT PARAMETERS FOR CONTINUED FRACTION COMPUTATION
C
330 IF(X-.5) 340,340,380
340 IF(AA-1.00) 350,350,360
      BDTR 600
      BDTR 610
      BDTR 620
      BDTR 630
      BDTR 640
      BDTR 650
      BDTR 660
      BDTR 670
      BDTR 680
      BDTR 690
      BDTR 700
      BDTR 710
      BDTR 720
      BDTR 730
      BDTR 740
      BDTR 750
      BDTR 760
      BDTR 770
      BDTR 780
      BDTR 790
      BDTR 800
      BDTR 810
      BDTR 820
      BDTR 830
      BDTR 840
      BDTR 850
      BDTR 860
      BDTR 870
      BDTR 880
      BDTR 890
      BDTR 900
      BDTR 910
      BDTR 920
      BDTR 930
      BDTR 940
      BDTR 950
      BDTR 960
      BDTR 970
      BDTR 980
      BDTR 990
      BDTR1000
      BDTR1010
      BDTR1020
      BDTR1030
      BDTR1040
      BDTR1050
      BDTR1060
      BDTR1070
      BDTR1080
      BDTR1090
      BDTR1100
      BDTR1110
      BDTR1120
      BDTR1130
      BDTR1140
      BDTR1150
      BDTR1160
      BDTR1170
      BDTR1180
      BDTR1190
      BDTR1200
      BDTR1210
      BDTR1220
      BDTR1230
      BDTR1240
      BDTR1250
      BDTR1260
      BDTR1270
      BDTR1280
      BDTR1290
      BDTR1300
      BDTR1310
      BDTR1320
      BDTR1330
      BDTR1340
      BDTR1350
      BDTR1360
      BDTR1370
      BDTR1380
      BDTR1390
      BDTR1400
      BDTR1410
      BDTR1420
      BDTR1430
      BDTR1440
      BDTR1450
      BDTR1460
      BDTR1470
      BDTR1480
      BDTR1490
      BDTR1500
      BDTR1510
350 RR=AA+1.00
   GO TO 370
360 RR=AA
370 DD=DLXX/5.00
   DD=DEXP(DD)
   DD=(RR-1.00)-(RR+BB-1.00)*XX*DD +2.00
   IF(DD) 420,420,430
380 IF(BB-1.00) 390,390,400
390 RR=BB+1.00
   GO TO 410
400 RR=BB
410 DD=DLIX/5.00
   DD=DEXP(DD)
   DD=(RR-1.00)-(AA+RR-1.00)*(1.00-XX)*DD +2.00
   IF(DD) 430,430,420
420 ID=1
   FF=DLIX
   DLIX=DLXX
   DLXX=FF
   XO=1.00/XO
   FF=AA
   AA=BB
   BB=FF
   G2=G1
C
C      TEST FOR A LESS THAN 1.0
C
430 FF=0.00
   IF(AA-1.00) 440,440,470
440 CALL DLGAM(AA+1.00,G4,IOK)
   DD=AA*DLXX+BB*DLIX+G3-G2-G4
   IF(DD+1.68002) 460,460,450
450 FF=FF+DEXP(DD)
460 AA=AA+1.00
C
C      COMPUTE P USING CONTINUED FRACTION EXPANSION
C
470 FN=AA+BB-1.00
   RR=AA-1.00
   II=80
   XI=DFLOAT(II)
   SS=(BB-XI)*(RR+XI)/((RR+2.00*XI-1.00)*(RR+2.00*XI))
   SS=SS*XO
   DD 480 I=1,79
   II=80-I
   XI=DFLOAT(II)
   DD=(XI*(FN+XI))/((RR+2.00*XI+1.00)*(RR+2.00*XI))
   DD=DD*XO
   CC=((BB-XI)*(RR+XI)/((RR+2.00*XI-1.00)*(RR+2.00*XI))
   CC=CC*XO
   SS=CC/(1.00+DD/(1.00-SS))
480 CONTINUE
   SS=1.00/(1.00-SS)
   IF(SS) 650,650,490
490 CALL DLGAM(AA+BB,G1,IOK)
   CALL DLGAM(AA+1.00,G4,IOK)
   CC=G1-G2-G4+AA*DLXX+(BB-1.00)*DLIX
   PP=CC+DLG(SS)
   IF(PP+1.68002) 500,500,510
500 PP=FF
   GO TO 520
510 PP=DEXP(PP)+FF
520 IF(ID) 540,540,530
530 PP=1.00-PP
540 P=SNGL(PP)
C
C      SET ERROR INDICATOR
C
   IF(P) 550,570,570
550 IF(ABS(P)-1.E-7) 560,560,650
560 P=0.0
   GO TO 660
570 IF(1.-P) 580,600,600
580 IF(ABS(1.-P)-1.E-7) 590,590,650
590 P=1.0
   GO TO 660
600 IF(P-1.E-6) 610,610,620
610 P=0.0
   GO TO 660
620 IF((1.0-P)-1.E-8) 630,630,660
630 P=1.0
   GO TO 660
640 IER=-2
   D=-1.E75
   P=-1.E75
   GO TO 670
650 IEP=+2
   P=1.E75
   GO TO 670
660 IER=0
670 RETURN
   END
      BDTR1520
      BDTR1530
      BDTR1540
      BDTR1550
      BDTR1560
      BDTR1570
      BDTR1580
      BDTR1590
      BDTR1600
      BDTR1610
      BDTR1620
      BDTR1630
      BDTR1640
      BDTR1650
      BDTR1660
      BDTR1670
      BDTR1680
      BDTR1690
      BDTR1700
      BDTR1710
      BDTR1720
      BDTR1730
      BDTR1740
      BDTR1750
      BDTR1760
      BDTR1770
      BDTR1780
      BDTR1790
      BDTR1800
      BDTR1810
      BDTR1820
      BDTR1830
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      BDTR1860
      BDTR1870
      BDTR1880
      BDTR1890
      BDTR1900
      BDTR1910
      BDTR1920
      BDTR1930
      BDTR1940
      BDTR1950
      BDTR1960
      BDTR1970
      BDTR1980
      BDTR1990
      BDTR2000
      BDTR2010
      BDTR2020
      BDTR2030
      BDTR2040
      BDTR2050
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      BDTR2110
      BDTR2120
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      BDTR2140
      BDTR2150
      BDTR2160
      BDTR2170
      BDTR2180
      BDTR2190
      BDTR2200
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      BDTR2340
      BDTR2350
      BDTR2360
      BDTR2370
      BDTR2380
      BDTR2390
      BDTR2400
      BDTR2410
      BDTR2420
      BDTR2430

```

Subroutine CDTR

This subroutine computes $P = P(x) = \text{Prob.}(X \leq x)$, where X is a random variable following the χ^2 distribution with continuous parameter m . The value of x must be greater than or equal to zero and $0.5 \leq m \leq 2 (10^5)$ for computation to take place. D , the ordinate of the χ^2 density at x , is also presented in the output.

For $x \geq 0$, $P(x)$ may be written as:

$$P(x) = \int_0^x f(m, y) dy \tag{1}$$

where $f(m, y) = y^{(m-2)/2} e^{-y/2} / (2^{m/2} \Gamma(\frac{m}{2}))$

and $D = f(m, x)$

To evaluate the integral, $\theta = \frac{m}{2} - [\frac{m}{2}]$ is first defined where $[\frac{m}{2}]$ denotes the largest integer less than or equal to $\frac{m}{2}$. θ is thus the fractional part of $\frac{m}{2}$.

Substituting this expression into the integral and performing the proper reductions, the following results are obtained.

If:	then:
$0 < m < 2$	$P(x) = T1 + T2$
$2 \leq m < 4$	$P(x) = T1$
$m \geq 4$	$P(x) = T1 - 2T3$

where:

$$T1 = \int_0^x \frac{y^\theta e^{-y/2} dy}{2^{1+\theta} \Gamma(1+\theta)}$$

$$T2 = f(2+2\theta, x)$$

$$T3 = \sum_{i=2}^{[\frac{m}{2}]} f(2i+2\theta, x)$$

$T2$ and $T3$ may be evaluated directly using logs and antilogs.

If $\theta = 0$ ($\frac{m}{2}$ is an integer), $T1$ is easily evaluated as:

$$T1 = 1 - e^{-x/2}$$

If $\theta > 0$, $T1$ can be expanded in the following infinite series:

$$T1 = \frac{Z^\theta}{\Gamma(1+\theta)} \left(\frac{Z}{1+\theta} - \frac{Z^2}{2+\theta} + \frac{Z^3}{2!(3+\theta)} - \frac{Z^4}{3!(4+\theta)} \dots \right) \tag{2}$$

where $Z = \frac{x}{2}$

This series is used in the range $10^{-8} < x \leq 10$, and not more than 30 terms are necessary to ensure convergence within error bounds of 10^{-9} .

For $x > 10$, $1-T1$ is evaluated by the Euler-McLaurin formula up to third-derivative terms (see reference (2), equation 23.1.30). One finds:

$$1 - T1 = \int_0^N h(u) du \tag{3}$$

where $h(u) = \frac{1}{\Gamma(1+\theta)} \left(\frac{2u}{Nx}\right)^{-(1+\theta)} u^{-1} e^{-Nx/2u}$

$$\begin{aligned} \text{and } \int_0^N h(u) du &= \sum_{u=0}^{N-1} h(u) + \frac{1}{2} h(N) - \frac{1}{12} h'(N) \\ &+ \frac{1}{720} h'''(N) \quad (\text{Note: } h' = h''') \\ &= 0 \text{ at } 0 \end{aligned}$$

In order to achieve accuracy consistent with that obtained by the method of equation (2), $N = 26$ is used in equation (3).

If $0 \leq x \leq 10^{-8}$, the approximation $x = 0$ is made. P is set to 0; and D is set to 10^{75} , 0.5, or 0, corresponding to m less than 2, equal to 2, or greater than 2 respectively.

If $m > 1000$, Wilson and Hilferty's approximation is used. $(\chi^2/m)^{1/3}$ is approximately normally distributed with mean $1 - 2/9m$ and variance $2/9m$ (see reference (2), equation 26.4.14). If $m \leq 1000$ and $x > 2000$, or $m > 1000$ and $x > 10^6$, P is set to 1.

Since $T1$ may have an error of about 10^{-9} , values of $P(x)$ very near zero or one may be somewhat imprecise. To eliminate possible misinterpretation of results, if $0 \leq P(x) \leq 10^{-8}$ or $0 \leq 1-P(x) \leq 10^{-8}$, $P(x)$ is set to 0 or 1 respectively.

The χ^2 distribution is a member of the gamma family of probability distributions. The general form for distributions of this class is:

$$P_G(x) = \int_0^x G(n, A, \psi; u) du$$

where $G(n, a, \psi; u) = (u-a)^{n-1} e^{-(u-a)/\psi} / (\psi^n \Gamma(n))$

This subroutine may, therefore, also be used to compute the probability integral from zero to x and the corresponding ordinate at x for any member of this gamma family by setting:

$$x = 2(u-a) / \psi \text{ and } m = 2n$$

Then $P(x)$ will be the desired probability and $2f(m, x)/\psi$ will be the desired ordinate.

For reference see:

- (1) R. E. Bargmann and S. P. Ghosh, Statistical Distribution Programs For a Computer Language, IBM Research Report RC-1094, 1963
- (2) M. Abramowitz and I. A. Stegun, Handbook of Mathematical Functions, U. S. Department of Commerce, National Bureau of Standards Applied Mathematics Series, 1966.

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C
C                                     CDF 10
C-----C-----C-----C-----C-----C-----C-----C-----
C                                     CDF 20
C                                     CDF 30
C     SUBROUTINE CDF      CDF 40
C                                     CDF 50
C     PURPOSE              CDF 60
C     COMPUTES P(X) = PROBABILITY THAT THE RANDOM VARIABLE U,
C     DISTRIBUTED ACCORDING TO THE CHI-SQUARE DISTRIBUTION WITH G
C     DEGREES OF FREEDOM, IS LESS THAN OR EQUAL TO X. F(G,X), THE
C     ORDINATE OF THE CHI-SQUARE DENSITY AT X, IS ALSO COMPUTED.
C                                     CDF 100
C     USAGE                CDF 110
C     CALL CDF(X,G,P,D,IER) CDF 120
C     DESCRIPTION OF PARAMETERS
C     X - INPUT SCALAR FOR WHICH P(X) IS COMPUTED.    CDF 160
C     G - NUMBER OF DEGREES OF FREEDOM OF THE CHI-SQUARE
C     DISTRIBUTION. G IS A CONTINUOUS PARAMETER.      CDF 180
C     P - OUTPUT PROBABILITY.                          CDF 190
C     D - OUTPUT DENSITY.                             CDF 200
C     IER - RESULTANT ERROR CODE WHERE
C     IER= 0 --- NO ERROR                             CDF 220
C     IER=-1 --- AN INPUT PARAMETER IS INVALID. X IS LESS
C     THAN 0.0, OR G IS LESS THAN 0.5 OR GREATER
C     THAN 2*10**(45). P AND D ARE SET TO -1.E75.    CDF 250
C     IER=+1 --- INVALID OUTPUT. P IS LESS THAN ZERO OR
C     GREATER THAN ONE, OR SERIES FOR T1 (SEE
C     MATHEMATICAL DESCRIPTION) HAS FAILED TO
C     CONVERGE. P IS SET TO 1.E75.
C                                     CDF 290
C     REMARKS              CDF 300
C     SEE MATHEMATICAL DESCRIPTION.
C     SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C     DLGAM                    CDF 340
C     NOTR                      CDF 350
C     METHOD                 CDF 360
C     REFER TO R.E. BARGMANN AND S.P. GHOSH, STATISTICAL
C     DISTRIBUTION PROGRAMS FOR A COMPUTER LANGUAGE,
C     IBM RESEARCH REPORT RC-1094, 1963.
C-----C-----C-----C-----C-----C-----C-----C-----
C     SUBROUTINE CDF(X,G,P,D,IER) CDF 450
C     DOUBLE PRECISION XX,DLXX,X2,DLX2,GG,GG2,DLT3,THETA,THP1,
C     IGLG2,DD,T1,SER,CC,XI,FAC,TLGG,TERM,GTH,A2,A,B,C,DT2,DT3,THP1
C     TEST FOR VALID INPUT DATA
C     IF(G-.5-1.E-5) 590,10,10
C     IF(G-2.E+5) 20,20,590
C     IF(X) 590,30,30
C     TEST FOR X NEAR 0.0
C     IF(X-1.E-8) 40,40,80
C     P=0.0
C     IF(G-2.) 50,60,70
C     D=1.E75
C     GG TO 610
C     D=0.5
C     GG TO 610
C     D=0.0
C     GG TO 610
C     CDF 510
C     CDF 520
C     CDF 530
C     CDF 540
C     CDF 550
C     CDF 560
C     CDF 570
C     CDF 580
C     CDF 590
C     CDF 600
C     CDF 610
C     CDF 620
C     CDF 630
C     CDF 640
C     CDF 650
C     CDF 660
```

```
C     TEST FOR X GREATER THAN 1.E+6
C     CDF 680
C     CDF 690
C     CDF 700
C     CDF 710
C     CDF 720
C     CDF 730
C     CDF 740
C     CDF 750
C     CDF 760
C     CDF 770
C     CDF 780
C     CDF 790
C     CDF 800
C     CDF 810
C     CDF 820
C     CDF 830
C     CDF 840
C     CDF 850
C     CDF 860
C     CDF 870
C     CDF 880
C     CDF 890
C     CDF 900
C     CDF 910
C     CDF 920
C     CDF 930
C     CDF 940
C     CDF 950
C     CDF 960
C     CDF 970
C     CDF 980
C     CDF 990
C     CDF 1000
C     CDF 1010
C     CDF 1020
C     CDF 1030
C     CDF 1040
C     CDF 1050
C     CDF 1060
C     CDF 1070
C     CDF 1080
C     CDF 1090
C     CDF 1100
C     CDF 1110
C     CDF 1120
C     CDF 1130
C     CDF 1140
C     CDF 1150
C     CDF 1160
C     CDF 1170
C     CDF 1180
C     CDF 1190
C     CDF 1200
C     CDF 1210
C     CDF 1220
C     CDF 1230
C     CDF 1240
C     CDF 1250
C     CDF 1260
C     CDF 1270
C     CDF 1280
C     CDF 1290
C     CDF 1300
C     CDF 1310
C     CDF 1320
C     CDF 1330
C     CDF 1340
C     CDF 1350
C     CDF 1360
C     CDF 1370
C     CDF 1380
C     CDF 1390
C     CDF 1400
C     CDF 1410
C     CDF 1420
C     CDF 1430
C     CDF 1440
C     CDF 1450
C     CDF 1460
C     CDF 1470
C     CDF 1480
C     CDF 1490
C     CDF 1500
C     CDF 1510
C     CDF 1520
C     CDF 1530
C     CDF 1540
C     CDF 1550
C     CDF 1560
C     CDF 1570
C     CDF 1580
C     CDF 1590
C     CDF 1600
C     CDF 1610
C     CDF 1620
C     CDF 1630
C     CDF 1640
C     CDF 1650
C     CDF 1660
C     CDF 1670
C     CDF 1680
C     CDF 1690
C     CDF 1700
C     CDF 1710
C     CDF 1720
C     CDF 1730
C     CDF 1740
C     CDF 1750
C     CDF 1760
C     CDF 1770
C     CDF 1780
C     CDF 1790
C     CDF 1800
C     CDF 1810
C     CDF 1820
C     CDF 1830
C     CDF 1840
C     CDF 1850
C     CDF 1860
C     CDF 1870
C     CDF 1880
C     CDF 1890
C     CDF 1900
C     CDF 1910
C     CDF 1920
C     CDF 1930
C     CDF 1940
```

```

      IF(DT2+1.68002) 430,430,440
430 P=T1
      GG TO 490
440 DT2=DEXP(DT2)
      T2=SNGL(DT2)
      P=T1+T2+T2
      GO TO 490
C
C      COMPUTE P FOR G GREATER THAN OR EQUAL TO 2.0
C      AND LESS THAN 4.0
C
450 P=T1
      GO TO 490
C
C      COMPUTE P FOR G GREATER THAN OR EQUAL TO 4.0
C      AND LESS THAN OR EQUAL TO 1000.0
C
460 DT3=0.00
      DO 480 I3=2,K
      THPI=DFLGAT(I3)+THETA
      CALL DLGAM(THPI,GTH,IOK)
      DLT3=THPI*DLX2-OLXX-X2-GTH
      IF(DLT3+1.68002) 480,480,470
470 DT3=DT3+DEXP(DLT3)
480 CONTINUE
      T3=SNGL(DT3)
      P=T1-T3-T3
C
C      SET ERROR INDICATOR
C
490 IF(P) 500,520,520
500 IF(ABS(P)-1.E-7) 510,510,600
510 P=0.0
      GO TO 610
520 IF(1.-P) 530,550,550
530 IF(ABS(1.-P)-1.E-7) 540,540,600
540 P=1.0
      GO TO 610
550 IF(P-1.E-8) 560,560,570
560 P=0.0
      GO TO 610
570 IF((1.0-P)-1.E-8) 580,580,610
580 P=1.0
      GO TO 610
590 IER=-1
      O=-1.E75
      P=-1.E75
      GO TO 620
600 IEP=+1
      P= 1.E75
      GO TO 620
610 IER=0
620 RETURN
      END

```

```

CDTR1950
CDTR1960
CDTR1970
CDTR1980
CDTR1990
CDTR2000
CDTR2010
CDTR2020
CDTR2030
CDTR2040
CDTR2050
CDTR2060
CDTR2070
CDTR2080
CDTR2090
CDTR2100
CDTR2110
CDTR2120
CDTR2130
CDTR2140
CDTR2150
CDTR2160
CDTR2170
CDTR2180
CDTR2190
CDTR2200
CDTR2210
CDTR2220
CDTR2230
CDTR2240
CDTR2250
CDTR2260
CDTR2270
CDTR2280
CDTR2290
CDTR2300
CDTR2310
CDTR2320
CDTR2330
CDTR2340
CDTR2350
CDTR2360
CDTR2370
CDTR2380
CDTR2390
CDTR2400
CDTR2410
CDTR2420
CDTR2430
CDTR2440
CDTR2450
CDTR2460
CDTR2470
CDTR2480

```

Subroutine NDTRI

This subroutine computes $x = p^{-1}(y)$ such that $y = P(x) = \text{Prob}(X \leq x)$ where X is a random variable distributed normally with mean zero and variance one.

That is, given $P(x)$, the following is solved for x :

$$P(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^x \exp(-u^2/2) du$$

The following approximation[†] is used:

$$x = w - \sum_{i=0}^2 a_i w^i / \sum_{i=0}^3 b_i w^i \quad (1)$$

where:

$$w = \sqrt{\ln(1/p^2)} \quad (0 < p \leq .5) \quad (2)$$

$$a_0 = 2.515517$$

$$a_1 = 0.802853$$

$$a_2 = 0.010328$$

$$b_1 = 1.432788$$

$$b_2 = 0.189269$$

$$b_3 = 0.001308$$

If $P(x)$ is greater than 0.5, $1 - P(x)$ is used as p in (2) above, and the result of (1), x , is negated. The maximum error is 0.00045; $f(x)$ is also calculated.

[†]C. Hastings, Approximations for Digital Computers. Princeton University Press, Princeton, N. J., 1955

M. Abramowitz and I. A. Stegun, Handbook of Mathematical Functions. Dover Publications, Inc., N. Y., equation 26.2.23.

```

C
C ..... NTRI 10
C ..... NTRI 20
C ..... NTRI 30
C ..... NTRI 40
C ..... NTRI 50
C ..... NTRI 60
C ..... NTRI 70
C ..... NTRI 80
C ..... NTRI 90
C ..... NTRI 100
C ..... NTRI 110
C ..... NTRI 120
C ..... NTRI 130
C ..... NTRI 140
C ..... NTRI 150
C ..... NTRI 160
C ..... NTRI 170
C ..... NTRI 180
C ..... NTRI 190
C ..... NTRI 200
C ..... NTRI 210
C ..... NTRI 211
C ..... NTRI 220
C ..... NTRI 230
C ..... NTRI 240
C ..... NTRI 250
C ..... NTRI 260
C ..... NTRI 270
C ..... NTRI 280
C ..... NTRI 290
C ..... NTRI 300
C ..... NTRI 310
C ..... NTRI 320
C ..... NTRI 330
C ..... NTRI 340
C ..... NTRI 350
C ..... NTRI 360
C ..... NTRI 370
C ..... NTRI 380
C ..... NTRI 390
C ..... NTRI 400
C ..... NTRI 410
C ..... NTRI 420
C ..... NTRI 430
C ..... NTRI 431
C ..... NTRI 432
C ..... NTRI 440
C ..... NTRI 450
C ..... NTRI 460
C ..... NTRI 470
C ..... NTRI 480
C ..... NTRI 490
C ..... NTRI 500
C ..... NTRI 510
C ..... NTRI 520
C ..... NTRI 530
C ..... NTRI 540
C ..... NTRI 550
C ..... NTRI 560
C ..... NTRI 570
C ..... NTRI 580
C ..... NTRI 590
C ..... NTRI 600
C ..... NTRI 610
C ..... NTRI 620
C ..... NTRI 630
C ..... NTRI 640
C ..... NTRI 640

```


Elementary Statistics and Miscellany

Subroutine MOMEN

This subroutine computes four moments for grouped data F_1, F_2, \dots, F_n on equal class intervals. The number of class intervals is computed as follows:

$$n = (UBO_3 - UBO_1) / UBO_2 \quad (1)$$

where UBO_1 = given lower bound
 UBO_2 = given class interval
 UBO_3 = given upper bound

and the total frequency as follows:

$$T = \sum_{i=1}^n F_i \quad (2)$$

where F_i = frequency count in i^{th} interval.

Then, the following are computed.

First moment (mean):

$$ANS_1 = \frac{\sum_{i=1}^n F_i [UBO_1 + (i-0.5) UBO_2]}{T} \quad (3)$$

j^{th} moment:

$$ANS_j = \frac{\sum_{i=1}^n F_i [UBO_1 + (i-0.5) UBO_2 - ANS_1]^j}{T} \quad (4)$$

$j = 2, 3, 4$

These moments are biased and not corrected for grouping.

```

C ..... MCME 10
C ..... MCME 20
C ..... MCME 30
C ..... MCME 40
C ..... MCME 50
C ..... MCME 60
C ..... MCME 70
C ..... MCME 80
C ..... MCME 90
C ..... MCME 100
C ..... MCME 110
C ..... MCME 120
C ..... MCME 130
C ..... MCME 140
C ..... MCME 150
C ..... MCME 160
C ..... MCME 170
C ..... MCME 180
C ..... MCME 190
C ..... MCME 200
C ..... MCME 210
C ..... MCME 220
C ..... MCME 230
C ..... MCME 240
C ..... MCME 250
C ..... MCME 260
C ..... MCME 270
C ..... MCME 280
C ..... MCME 290
C ..... MCME 300
C ..... MCME 310
C ..... MCME 320
C ..... MCME 330
C ..... MCME 340
C ..... MCME 350
C ..... MCME 360
C ..... MCME 370
C ..... MCME 380
C ..... MCME 390
C ..... MCME 400
C ..... MCME 410
C ..... MCME 420
C ..... MCME 430
C ..... MCME 440
C ..... MCME 450
C ..... MCME 460
C ..... MCME 470
C ..... MCME 480
C ..... MCME 490
C ..... MCME 500
C ..... MCME 510
C ..... MCME 520
C ..... MCME 530
C ..... MCME 540
C ..... MCME 550
C ..... MCME 560
C ..... MCME 570
C ..... MCME 580
C ..... MCME 590
C ..... MCME 600
C ..... MCME 610
C ..... MCME 620
C ..... MCME 630
C ..... MCME 640
C ..... MCME 650
C ..... MCME 660
C ..... MCME 670
C ..... MCME 680
C ..... MCME 690
C ..... MCME 700
C ..... MCME 710
C ..... MCME 720
C ..... MCME 730
C ..... MCME 740
C ..... MCME 750
C ..... MCME 760
C ..... MCME 770
C ..... MCME 780
C ..... MCME 790
C ..... MCME 800
C ..... MCME 810
C ..... MCME 820
C ..... MCME 830
C ..... MCME 840
C ..... MCME 850
C ..... MCME 860
C ..... MCME 870
C ..... MCME 880
C ..... MCME 890
C ..... MCME 900
C ..... MCME 910
C ..... MCME 920
C ..... MCME 930

```

Subroutine TTEST

This subroutine computes certain t-statistics on the means of populations under various hypotheses.

The sample means of A_1, A_2, \dots, A_{NA} , and B_1, B_2, \dots, B_{NB} are normally found by the following formulas:

$$\bar{A} = \frac{\sum_{i=1}^{NA} A_i}{NA}; \quad \bar{B} = \frac{\sum_{i=1}^{NB} B_i}{NB} \quad (1)$$

and the corresponding sample variances by:

$$SA^2 = \frac{\sum_{i=1}^{NA} (A_i - \bar{A})^2}{NA - 1}; \quad SB^2 = \frac{\sum_{i=1}^{NB} (B_i - \bar{B})^2}{NB - 1} \quad (2)$$

The quantities μ and σ^2 stand respectively for population mean and variance in the following hypotheses.

Hypothesis: $\mu_B = A$; $A =$ a given value (Option 1)

Let \bar{B} = estimate of μ_B and set $NA = 1$. (A is stored in location A_1).

The subroutine computes:

$$ANS = \frac{\bar{B} - A}{SB} \cdot \sqrt{NB} \quad (\text{t-statistics}) \quad (3)$$

$$NDF = NB - 1 \quad (\text{degrees of freedom}) \quad (4)$$

Hypothesis: $\mu_A = \mu_B$ ($\sigma_A^2 = \sigma_B^2$) (Option 2)

The subroutine computes:

$$ANS = \frac{\bar{B} - \bar{A}}{S} \cdot \frac{1}{\sqrt{\frac{1}{NA} + \frac{1}{NB}}} \quad (\text{t-statistics}) \quad (5)$$

$$NDF = NA + NB - 2 \quad (\text{degrees of freedom}) \quad (6)$$

$$\text{where } S = \sqrt{\frac{(NA - 1) SA^2 + (NB - 1) SB^2}{NA + NB - 2}} \quad (7)$$

Hypothesis: $\mu_A = \mu_B$ ($\sigma_A^2 \neq \sigma_B^2$) (Option 3)

The subroutine computes:

$$ANS = \frac{\bar{B} - \bar{A}}{\sqrt{\frac{SA^2}{NA} + \frac{SB^2}{NB}}} \quad (\text{t-statistics}) \quad (8)$$

$$NDF = \frac{\left(\frac{SA^2}{NA} + \frac{SB^2}{NB} \right)^2}{\left(\frac{SA^2}{NA} \right)^2 / (NA + 1) + \left(\frac{SB^2}{NB} \right)^2 / (NB + 1)} - 2$$

(degrees of freedom)

Note: The program returns a rounded NDF, not a truncated NDF.

Hypothesis: $\mu_A = \mu_B$ (no assumption on σ^2) (Option 4)

The subroutine computes:

$$ANS = \frac{\bar{D}}{SD} \cdot \sqrt{NB} \quad (\text{t-statistics}) \quad (10)$$

$$NDF = NB - 1 \quad (\text{degrees of freedom}) \quad (11)$$

where $\bar{D} = \bar{B} - \bar{A}$ (12)

$$SD = \sqrt{\frac{\sum_{i=1}^{NB} (B_i - A_i - \bar{D})^2}{NB - 1}} \quad (13)$$

NA = NB

```

C ..... TTES 10
C ..... TTES 20
C ..... TTES 30
C SUBROUTINE TTEST TTES 40
C ..... TTES 50
C ..... TTES 60
C PURPOSE TTES 70
C TO FIND CERTAIN T-STATISTICS ON THE MEANS OF POPULATIONS. TTES 70
C ..... TTES 80
C USAGE TTES 90
C CALL TTEST (A,NA,B,NB,NOP,NDF,ANS) TTES 100
C ..... TTES 110
C DESCRIPTION OF PARAMETERS TTES 120
C A - INPUT VECTOR OF LENGTH NA CONTAINING DATA. TTES 130
C NA - NUMBER OF OBSERVATIONS IN A. TTES 140
C B - INPUT VECTOR OF LENGTH NB CONTAINING DATA. TTES 150
C NB - NUMBER OF OBSERVATIONS IN B. TTES 160
C NOP - OPTIONS FOR VARIOUS HYPOTHESES... TTES 170
C NOP=1--- THAT POPULATION MEAN OF B = GIVEN VALUE A. TTES 180
C (SET NA=1) TTES 190
C NOP=2--- THAT POPULATION MEAN OF B = POPULATION MEAN TTES 200
C OF A, GIVEN THAT THE VARIANCE OF B = THE TTES 210
C VARIANCE OF A. TTES 220
C NOP=3--- THAT POPULATION MEAN OF B = POPULATION MEAN TTES 230
C OF A, GIVEN THAT THE VARIANCE OF B IS NOT TTES 240
C EQUAL TO THE VARIANCE OF A. TTES 250
C NOP=4--- THAT POPULATION MEAN OF B = POPULATION MEAN TTES 260
C OF A, GIVEN NO INFORMATION ABOUT VARIANCES OF TTES 270
C A AND B. (SET NA=NB) TTES 280
C NOP - OUTPUT VARIABLE CONTAINING DEGREES OF FREEDOM ASSOCI- TTES 290
C ATED WITH T-STATISTIC CALCULATED. TTES 300
C ANS - T-STATISTIC FOR GIVEN HYPOTHESES. TTES 310
C ..... TTES 320
C REMARKS TTES 330
C NA AND NB MUST BE GREATER THAN 1, EXCEPT THAT NA=1 IN TTES 340
C OPTION 1. NA AND NB MUST BE THE SAME IN OPTION 4. TTES 350
C IF NOP IS OTHER THAN 1, 2, 3 OR 4, DEGREES OF FREEDOM AND TTES 360
C T-STATISTIC WILL NOT BE CALCULATED. NOP AND ANS WILL BE TTES 370
C SET TO ZERO. TTES 380
C ..... TTES 390
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED TTES 400
C NONE TTES 410
C ..... TTES 420
C METHOD TTES 430
C REFER TO OSTLE, BERNARD, "STATISTICS IN RESEARCH", IOWA TTES 440
C STATE COLLEGE PRESS, 1954, CHAPTER 5. TTES 450
C ..... TTES 460
C ..... TTES 470
C SUBROUTINE TTEST (A,NA,B,NB,NOP,NDF,ANS) TTES 480
C DIMENSION A(1),B(1) TTES 490
C ..... TTES 500
C ..... TTES 510
C INITIALIZATION TTES 520
C ..... TTES 530
C NDF=0 TTES 540
C ANS=0.0 TTES 550
C ..... TTES 560
C CALCULATE THE MEAN OF A TTES 570
C AMEAN=0.0 TTES 580
C WJ LCL 1=1,NA TTES 590
C ..... TTES 600

```

```

111 AMLAN=BMEAN+0.11
    FNA=FNA
    AMEAN=AMEAN/FNA
C
C   CALCULATE THE MEAN OF B
C
C   115 BMEAN=0.C
    DO 120 I=1,NB
120 BMLAN=BMEAN+0.11
    FNB=Nb
    BMEAN=BMLAN/FNB
C
C   IF(NOP=4) 122, 180, 200
122 IF(NOP=1) 200, 130, 125
C
C   CALCULATE THE VARIANCE OF A
C
C   125 SAZ=0.J
    DO 130 I=1,NA
130 SAZ=SAZ+(A(I)-AMEAN)**2
    SAZ=SAZ/(FNA-1.0)
C
C   CALCULATE THE VARIANCE OF B
C
C   135 SBZ=0.0
    DO 140 I=1,NB
140 SBZ=SBZ+(B(I)-BMEAN)**2
    SBZ=SBZ/(FNB-1.0)
C
C   GO TO (150,160,170), NOP
C
C   OPTION 1
C
C   150 ANS=((BMEAN-AMEAN)/SQRT(SBZ))*SQRT(FNB)
    NDF=Nb-1
    GO TO 200
C
C   OPTION 2
C
C   160 NDF=NA+NB-2
    FNDF=NDF
    S=SQRT(((FNA-1.0)*SAZ+(FNB-1.0)*SBZ)/FNDF)
    ANS=((BMEAN-AMEAN)/S)*(1.C/SQRT(1.C/FNA+1.0/FNB))
    GO TO 200
C
C   OPTION 3
C
C   170 ANS=(BMEAN-AMEAN)/SQRT(SAZ/FNA+SBZ/FNB)
    A1=(SAZ/FNA+SBZ/FNB)**2
    A2=(SAZ/FNA)**2/(FNA+1.C)+(SBZ/FNB)**2/(FNB+1.0)
    NDF=A1/A2-2.C*0.5
    GO TO 200
C
C   OPTION 4
C
C   180 SD=0.0
    D=BMEAN-AMEAN
    DO 190 I=1,NB
190 SD=SD+(B(I)-A(I)-D)**2
    SD=SQRT(SD/(FNB-1.0))
    ANS=(D/SD)*SQRT(FNB)
    NDF=Nb-1
C
200 RETURN
    END

```

Subroutine BISER

This subroutine computes a biserial coefficient of correlation between two continuous variables when one has been artificially dichotomized. The computational steps are as follows:

1. Compute the mean of the continuously measured variable, A:

$$\bar{A} = \frac{\sum_{i=1}^N A_i}{N} \quad (1)$$

where N = number of observations in the sample.

2. Compute the standard deviation of the continuously measured variable, A:

$$s = \sqrt{\frac{\sum_{i=1}^N A_i^2 - \frac{\left(\sum_{i=1}^N A_i\right)^2}{N}}{N - 1}} \quad (2)$$

3. Obtain the following information for the dichotomous variable, B:

p = proportion of the cases in the higher group
q = proportion of the cases in the lower group
y = ordinate of the normal distribution curve at the point of division between p and q proportions

4. Obtain \bar{A}_p = mean of A values whose corresponding B values are in the higher group.

5. Then, compute the biserial coefficient of correlation, r_b , by the use of the following formula:

$$r_b = \frac{\bar{A}_p - \bar{A}}{s} \cdot \frac{p}{y} \quad (3)$$

6. The standard error of r_b is estimated by the formula:

$$s_{r_b} = \frac{\sqrt{\frac{pq}{y} - r_b^2}}{\sqrt{N}} \quad (4)$$

For reference see:

(1) J. P. Guilford, Fundamental Statistics in Psychology and Education. McGraw-Hill, New York, 1956, chapter 13.

(2) J. W. Dunlop, "Note on Computation of Biserial Correlations in Item Evaluation", Psychometrika, 1936, I, pp. 51-60.

```

C ..... BISE 10
C ..... BISE 20
C ..... BISE 30
C ..... BISE 40
C ..... BISE 50
C ..... BISE 60
C ..... BISE 70
C ..... BISE 80
C ..... BISE 90
C ..... BISE 100
C ..... BISE 110
C ..... BISE 120
C ..... BISE 130
C ..... BISE 140
C ..... BISE 150
C ..... BISE 160
C ..... BISE 170
C ..... BISE 180
C ..... BISE 190
C ..... BISE 200
C ..... BISE 210
C ..... BISE 220
C ..... BISE 230
C ..... BISE 240
C ..... BISE 250
C ..... BISE 260
C ..... BISE 270
C ..... BISE 280
C ..... BISE 290
C ..... BISE 300
C ..... BISE 310
C ..... BISE 320
C ..... BISE 330
C ..... BISE 340
C ..... BISE 350
C ..... BISE 360
C ..... BISE 370
C ..... BISE 380
C ..... BISE 390
C ..... BISE 400
C ..... BISE 410
C ..... BISE 420
C ..... BISE 430
C ..... BISE 440
C ..... BISE 450
C ..... BISE 460
C ..... BISE 470
C ..... BISE 480
C ..... BISE 490
C ..... BISE 500
C ..... BISE 510
C ..... BISE 520
C ..... BISE 530
C ..... BISE 540
C ..... BISE 550
C ..... BISE 560
C ..... BISE 570
C ..... BISE 580
C ..... BISE 590
C ..... BISE 600
C ..... BISE 610
C ..... BISE 620
C ..... BISE 630
C ..... BISE 640
C ..... BISE 650
C ..... BISE 660
C ..... BISE 670
C ..... BISE 680
C ..... BISE 690
C ..... BISE 700
C ..... BISE 710
C ..... BISE 720
C ..... BISE 730
C ..... BISE 740
C ..... BISE 750
C ..... BISE 760
C ..... BISE 770
C ..... BISE 780
C ..... BISE 790
C ..... BISE 800
C ..... BISE 810
C ..... BISE 820
C ..... BISE 830
C ..... BISE 840
C ..... BISE 850
C ..... BISE 860
C ..... BISE 870
C ..... BISE 880
C ..... BISE 890
C ..... BISE 900
C ..... BISE 910
C ..... BISE 920
C ..... BISE 930
C ..... BISE 940
C ..... BISE 950
C ..... BISE 960
C ..... BISE 970
C ..... BISE 980
C ..... BISE 990
C ..... BISE 1000
C ..... BISE 1010
C ..... BISE 1020
C ..... BISE 1030
C ..... BISE 1040
C ..... BISE 1050
C ..... BISE 1060
C ..... BISE 1070
C ..... BISE 1080
C ..... BISE 1090
C ..... BISE 1100
C ..... BISE 1110
C ..... BISE 1120
C ..... BISE 1130
C ..... BISE 1140
C ..... BISE 1150
C ..... BISE 1160
C ..... BISE 1170
C ..... BISE 1180
C ..... BISE 1190
C ..... BISE 1200
C ..... BISE 1210
C ..... BISE 1220
C ..... BISE 1230
C ..... BISE 1240
C ..... BISE 1250
C ..... BISE 1260

```

Subroutine PHI

This subroutine computes a phi coefficient between two variables which are dichotomous. The computational steps are as follows:

1. Two dichotomous variables are summarized in a 2 x 2 table as shown below:

		Variable 1	
		High	Low
Variable 2	High	A	B
	Low	C	D

A, B, C, and D stand for frequencies.

2. Compute the phi coefficient by the formula:

$$\phi = \frac{AD - BC}{\sqrt{(A+B)(C+D)(A+C)(B+D)}} \quad (1)$$

3. Compute χ^2 as a function of phi coefficient as follows:

$$\chi^2 = N \phi^2 \quad (2)$$

where N = number of observations.

χ^2 , with one degree of freedom, may be tested at a required level of significance. If it is significant, the obtained phi coefficient is also significant.

4. Compute the maximal phi coefficient that can be attainable in a given problem by the formula:

$$\phi_{\max} = \sqrt{\left(\frac{p_j}{q_j}\right) \left(\frac{q_i}{p_i}\right)} \quad (3)$$

where p_j is the largest marginal proportion in a 2 x 2 contingency table, and p_j is the corresponding marginal proportion in the other variable.

For reference see:

(1) J. P. Guilford, Fundamental Statistics in Psychology and Education. McGraw-Hill, New York, 1956, chapter 13.

(2) G. U. Yule, "On the Methods of Measuring the Association Between Two Attributes", Journal of Royal Statistical Association, 1912, 75, pp. 576-642.

```

C ..... PHI 110
C ..... PHI 120
C ..... PHI 130
C ..... PHI 140
C ..... PHI 150
C ..... PHI 160
C ..... PHI 170
C ..... PHI 180
C ..... PHI 190
C ..... PHI 200
C ..... PHI 210
C ..... PHI 220
C ..... PHI 230
C ..... PHI 240
C ..... PHI 250
C ..... PHI 260
C ..... PHI 270
C ..... PHI 280
C ..... PHI 290
C ..... PHI 300
C ..... PHI 310
C ..... PHI 320
C ..... PHI 330
C ..... PHI 340
C ..... PHI 350
C ..... PHI 360
C ..... PHI 370
C ..... PHI 380
C ..... PHI 390
C ..... PHI 400
C ..... PHI 410
C ..... PHI 420
C ..... PHI 430
C ..... PHI 440
C ..... PHI 450
C ..... PHI 460
C ..... PHI 470
C ..... PHI 480
C ..... PHI 490
C ..... PHI 500
C ..... PHI 510
C ..... PHI 520
C ..... PHI 530
C ..... PHI 540
C ..... PHI 550
C ..... PHI 560
C ..... PHI 570
C ..... PHI 580
C ..... PHI 590
C ..... PHI 600
C ..... PHI 610
C ..... PHI 620
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C ..... PHI 750
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C ..... PHI 1080
C ..... PHI 1090
C ..... PHI 1100
C ..... PHI 1110
C ..... PHI 1120
C ..... PHI 1130

SUBROUTINE PHI
    PH I 110
    PH I 120
    PH I 130
    PH I 140
    PH I 150
    PH I 160
    PH I 170
    PH I 180
    PH I 190
    PH I 200
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    PH I 1060
    PH I 1070
    PH I 1080
    PH I 1090
    PH I 1100
    PH I 1110
    PH I 1120
    PH I 1130

PURPOSE
    TO COMPUTE THE PHI COEFFICIENT BETWEEN TWO VARIABLES WHICH
    ARE DICHOTOMOUS.

USAGE
    CALL PHI (N,U,V,HU,HV,P,CH,XP,IE)

DESCRIPTION OF PARAMETERS
    N - NUMBER OF OBSERVATIONS
    U - INPUT VECTOR OF LENGTH N CONTAINING THE FIRST DICHOTO-
        MOUS VARIABLE
    V - INPUT VECTOR OF LENGTH N CONTAINING THE SECOND DICHOTO-
        MOUS VARIABLE
    HU - INPUT NUMERICAL CODE WHICH INDICATES THE HIGHER
        CATEGORY OF THE FIRST VARIABLE. ANY OBSERVATION IN
        VECTOR U WHICH HAS A VALUE EQUAL TO OR GREATER THAN HU
        WILL BE CLASSIFIED IN THE HIGHER CATEGORY.
    HV - INPUT NUMERICAL CODE FOR VECTOR V, SIMILAR TO HU
    P - PHI COEFFICIENT COMPUTED
    CH - CHI-SQUARE COMPUTED AS A FUNCTION OF PHI COEFFICIENT
        (DEGREES OF FREEDOM FOR CHI-SQUARE = 1)
    XP - COMPUTED VALUE OF THE MAXIMAL PHI COEFFICIENT THAT
        CAN BE ATTAINED IN THE PROBLEM
    IE - IF IE IS NON-ZERO, SOME CELL IN THE 2 BY 2 TABLE IS
        NULL. IF SO, P, CH, AND XP ARE SET TO 10**75.

REMARKS
    VARIABLES U AND V MUST BE SPECIFIED NUMERIC.
    THE PHI COEFFICIENT IS A SPECIAL CASE OF THE
    PEARSON PRODUCT-MOMENT CORRELATION WHEN BOTH VARIABLES ARE
    BINARY.

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
    NONE

METHOD
    REFER TO P. HORST, 'PSYCHOLOGICAL MEASUREMENT AND
    PREDICTION', P. 94 (WADSWORTH, 1966).

SUBROUTINE PHI (N,U,V,HU,HV,P,CH,XP,IE)
    DIMENSION U(1),V(1)
    CONSTRUCT A 2X2 CONTINGENCY TABLE

    IE=0
    A=0.0
    R=0.0
    C=0.0
    D=0.0

    DO 40 I=1,N
        IF(U(I)-HU) 10,25,25
    10 IF(V(I)-HV) 15,20,20
    15 D=D+1.0
        GO TO 40
    20 B=B+1.0
        GO TO 40
    25 IF(V(I)-HV) 30,35,35
    30 C=C+1.0
        GO TO 40
    35 A=A+1.0
    40 CONTINUE
        IF(A) 100,100,41
    41 IF(B) 100,100,42
    42 IF(C) 100,100,43
    43 IF(D) 100,100,44

    COMPUTE THE PHI COEFFICIENT
    44 P=(A*D-B*C)/SQRT((A+B)*(C+D)*(A+C)*(B+D))

    COMPUTE CHI-SQUARE

    T=N
    CH=T*P*P

    COMPUTE THE MAXIMAL PHI COEFFICIENT

    P1=(A+C)/T
    P2=(B+D)/T
    P3=(A+B)/T
    P4=(C+D)/T
    IF(P1-P2) 75,45,45
    45 IF(P3-P4) 65,50,50
    50 IF(P1-P3) 60,55,55
    55 XP=SQRT((P3/P4)*(P2/P1))
        GO TO 95
    60 XP=SQRT((P1/P2)*(P4/P3))
        GO TO 95
    65 IF(P1-P4) 70,55,55
    70 XP=SQRT((P2/P1)*(P3/P4))
        GO TO 95
    75 IF(P3-P4) 90,80,80
    80 IF(P2-P3) 60,85,85
    85 XP=SQRT((P4/P3)*(P1/P2))
        GO TO 95
    90 IF(P2-P4) 70,85,85

    95 RETURN
    100 IE=1
        P=1.E75
        CH=1.E75
        XP=1.E75
        GO TO 95
    END

```

Subroutine POINT

This subroutine computes a point-biserial correlation coefficient between two variables, one binary (dichotomized) and one continuous. The computational steps are as follows:

1. Compute the mean of the continuously measured variable, \bar{A} :

$$\bar{A} = \frac{\sum_{i=1}^N A_i}{N} \quad (1)$$

where N = number of observations in the sample.

2. Compute the standard deviation of the continuously measured variable, s :

$$s = \sqrt{\frac{\sum_{i=1}^N A_i^2 - \frac{\left(\sum_{i=1}^N A_i\right)^2}{N}}{N-1}} \quad (2)$$

3. Obtain the following information for the dichotomous variable, B :

N_p = number of cases in the higher group

N_q = number of cases in the lower group

4. Obtain \bar{A}_p = mean of A values whose corresponding B values are in the higher group.

5. Then, compute the point-biserial correlation, r_{pb} :

$$r_{pb} = \frac{\bar{A}_p - \bar{A}}{s} \sqrt{\frac{N_p}{N_q}} \quad (3)$$

6. Compute the t ratio used to test the hypothesis of zero correlation:

$$t = r_{pb} \sqrt{\frac{N-2}{1-r_{pb}^2}} \quad (4)$$

7. The degrees of freedom for the t ratio are obtained by:

$$d.f. = N-2 \quad (5)$$

For reference see:

(1) J. P. Guilford, *Fundamental Statistics in Psychology and Education*. McGraw-Hill, New York, 1956, chapter 13.

(2) N. C. Perry and W. B. Michael, "The Reliability of a Point-Biserial Coefficient of Correlation". *Psychometrika*, 1954, 16, pp. 313-325.

Subroutine TETRA

This subroutine computes a tetrachoric correlation coefficient between two variables where both of the variables have been reduced artificially to two categories. The computational steps are as follows:

1. Two dichotomous variables are summarized in a 2 x 2 table such as the one shown below.

Variable 1
High Low

	High	Low
High	A	B
Low	C	D

Variable 2
High
Low

A, B, C, and D stand for frequencies. If any frequency is zero (0), the tetrachoric correlation will not be computed.

2. Obtain the proportions of marginal totals:

$$p_1 = (A+C)/N \quad (1)$$

$$q_1 = (B+D)/N \quad (2)$$

$$p_2 = (A+B)/N \quad (3)$$

$$q_2 = (C+D)/N \quad (4)$$

where N = number of observations.

3. Obtain:

y_1 = ordinate of the normal distribution curve at the point of division between p_1 and q_1 proportions

y_2 = same as y_1 using p_2 and q_2 proportions

z_1 = standard normal variable corresponding to y_1

z_2 = standard normal variable corresponding to y_2

4. Then, compute the tetrachoric correlation coefficient by the use of the following formula:

$$\frac{AD - BC}{y_1 y_2 N^2} = r_t + \frac{1}{2} z_1 z_2 r_t^2 + \frac{1}{6} (z_1^2 - 1)(z_2^2 - 1) r_t^3 + \frac{1}{24} z_1 (z_1^2 - 3) z_2 (z_2^2 - 3) r_t^4 + \frac{1}{120} (z_1^4 - 6z_1^2 + 3)(z_2^4 - 6z_2^2 + 3) r_t^5 + \frac{1}{720} z_1 (z_1^4 - 10z_1^2 + 15) z_2 (z_2^4 - 10z_2^2 + 15) r_t^6 + \frac{1}{5040} (z_1^6 - 15z_1^4 + 45z_1^2 - 15) (z_2^6 - 15z_2^4 + 45z_2^2 - 15) r_t^7 \quad (5)$$

```

C ..... POIN 10
C SUBROUTINE POINT POIN 20
C POIN 30
C POIN 40
C POIN 50
C POIN 60
C POIN 70
C POIN 80
C POIN 90
C POIN 100
C POIN 110
C POIN 120
C POIN 130
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C POIN1120
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C POIN1140
C POIN1150
C POIN1160
C POIN1170
C POIN1180
C POIN1190
C POIN1200
C POIN1210
C POIN1220
C POIN1230
C POIN1240
.....
SUBROUTINE POINT
  PURPOSE
  TO COMPUTE THE POINT-BISERIAL CORRELATION COEFFICIENT
  BETWEEN TWO VARIABLES, WHEN ONE OF THE VARIABLES IS A BINARY
  VARIABLE AND ONE IS CONTINUOUS. THIS IS A SPECIAL CASE OF
  THE PEARSON PRODUCT-MOMENT CORRELATION COEFFICIENT.
  USAGE
  CALL POINT (N,A,B,HI,ANS,IER)
  DESCRIPTION OF PARAMETERS
  N - NUMBER OF OBSERVATIONS
  A - INPUT VECTOR OF LENGTH N CONTAINING THE CONTINUOUS
  VARIABLE
  B - INPUT VECTOR OF LENGTH N CONTAINING THE DICHOTOMOUS
  (BINARY) VARIABLE
  HI - INPUT NUMERICAL CODE TO INDICATE THE HIGHER CATEGORY.
  ANY VALUE OF THE BINARY VARIABLE NOT LESS THAN HI WILL
  BE CLASSIFIED IN THE HIGHER OF THE TWO CATEGORIES.
  ANS - OUTPUT VECTOR OF LENGTH 9 CONTAINING THE FOLLOWING
  RESULTS
  ANS(1)- MEAN OF VARIABLE A
  ANS(2)- STANDARD DEVIATION OF VARIABLE A
  ANS(3)- NUMBER OF OBSERVATIONS IN THE HIGHER
  CATEGORY OF VARIABLE B
  ANS(4)- NUMBER OF OBSERVATIONS IN THE LOWER
  CATEGORY OF VARIABLE B
  ANS(5)- MEAN OF VARIABLE A FOR ONLY THOSE
  OBSERVATIONS IN THE HIGHER CATEGORY OF
  VARIABLE B
  ANS(6)- MEAN OF VARIABLE A FOR ONLY THOSE
  OBSERVATIONS IN THE LOWER CATEGORY OF
  VARIABLE B
  ANS(7)- POINT-BISERIAL CORRELATION COEFFICIENT
  ANS(8)- T-TEST FOR THE SIGNIFICANCE OF THE
  DIFFERENCE BETWEEN THE MEANS OF VARIABLE A
  FOR THE HIGHER AND LOWER CATEGORIES
  RESPECTIVELY.
  ANS(9)- DEGREES OF FREEDOM FOR THE T-TEST
  IER- 1, IF ALL ELEMENTS OF B ARE NOT LESS THAN HI.
  -1, IF ALL ELEMENTS OF B ARE LESS THAN HI.
  0, OTHERWISE. IF IER IS NON-ZERO, ANS(1), I=5,....,9,
  IS SET TO 10**75.
  REMARKS
  THE SYMBOLS USED TO IDENTIFY THE VALUES OF THE TWO CATEGORIES
  OF VARIABLE B MUST BE NUMERIC. ALPHABETIC OR SPECIAL
  CHARACTERS CANNOT BE USED.
  THE T-TEST(ANS(8)) IS A TEST OF WHETHER THE POINT-BISERIAL
  COEFFICIENT DIFFERS SIGNIFICANTLY FROM ZERO.
  SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
  METHOD
  REFER TO P. HORST, 'PSYCHOLOGICAL MEASUREMENT AND
  PREDICTION', P. 91 (WADSWORTH, 1966).
  SUBROUTINE POINT (N,A,B,HI,ANS,IER)
  DIMENSION A(1),B(1),ANS(1)
  COMPUTE MEAN AND STANDARD DEVIATION OF VARIABLE A
  IER=0
  SUM=0.0
  SUM2=0.0
  DO 10 I=1,N
  SUM=SUM+A(I)
  10 SUM2=SUM2+A(I)*A(I)
  FN=N
  ANS(1)=SUM/FN
  ANS(2)=(SUM2-ANS(1)*SUM)/(FN-1.0)
  ANS(2)= SQRT(ANS(2))
  FIND NUMBERS OF CASES IN THE HIGHER AND LOWER CATEGORIES
  P=0.0
  SUM=0.0
  SUM2=0.0
  DO 30 I=1,N
  IF(B(I)-HI) 20, 25, 25
  20 SUM2=SUM2+A(I)
  GO TO 30
  25 P=P+1.0
  SUM=SUM+A(I)
  30 CONTINUE
  Q=FN-P
  ANS(3)=P
  ANS(4)=0
  IF (P) 35,35,40
  35 IER=-1
  GO TO 50
  40 ANS(5)=SUM/P
  IF (Q) 45,45,60
  45 IER=1
  50 DO 55 I=5,9
  55 ANS(I)=1.E75
  GO TO 65
  60 ANS(6)=SUM2/Q
  COMPUTE THE POINT-BISERIAL CORRELATION
  R=((ANS(5)-ANS(1))/ANS(2))* SQRT(P/Q)
  ANS(7)=R
  COMPUTE T RATIO USED TO TEST THE HYPOTHESIS OF ZERO CORRELATION
  T=R* SQRT((FN-2.0)/(1.0-R**2))
  ANS(8)=T
  COMPUTE DEGREES OF FREEDOM
  ANS(9)=FN-2
  65 RETURN
  END

```

Note: r_t is found by the subroutine POLRT -- Newton-Raphson method of approximation to the root of the above equation.

5. For the purpose of testing $r_t = 0.0$, the standard error is estimated by the formula:

$$s_{r_t} = \frac{\sqrt{p_1 p_2 q_1 q_2}}{y_1 y_2 \sqrt{N}} \quad (6)$$

6. In selecting the real root in $[-1, 1]$, if $r_t = a + bi$, and

$$|b| \leq .5(10^{-6}) |a|$$

r_t is considered to be a real root.

For reference see:

(1) J. P. Guilford, Fundamental Statistics in Psychology and Education. McGraw-Hill, New York, 1956, chapter 13.

(2) W. P. Elderton, Frequency Curves and Correlation, 4th Edition. Cambridge University Press, 1953, chapter 9.

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C-----TETR 10
C-----TETR 20
C-----TETR 30
C-----TETR 40
C-----TETR 50
C-----TETR 60
C-----TETR 70
C-----TETR 80
C-----TETR 90
C-----TETR 100
C-----TETR 110
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C-----TETR 410
C-----TETR 420
C-----TETR 430
C-----TETR 440
C-----TETR 450
C-----TETR 460
C-----TETR 470
C-----TETR 480
C-----TETR 490
C-----TETR 500
C-----TETR 510
C-----TETR 520
C-----TETR 530
C-----TETR 540
C-----TETR 550

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SUBROUTINE TETRA (N,U,V,HU,HV,R,RS,IE)

PURPOSE
COMPUTE A TETRACHORIC CORRELATION COEFFICIENT BETWEEN TWO VARIABLES WHERE DATA IN BOTH VARIABLES HAVE BEEN REDUCED ARTIFICIALLY TO TWO CATEGORIES.

USAGE
CALL TETRA (N,U,V,HU,HV,R,RS,IE)

DESCRIPTION OF PARAMETERS
N - NUMBER OF OBSERVATIONS
U - INPUT VECTOR OF LENGTH N CONTAINING THE FIRST VARIABLE REDUCED TO TWO CATEGORIES
V - INPUT VECTOR OF LENGTH N CONTAINING THE SECOND VARIABLE REDUCED TO TWO CATEGORIES
HU - INPUT NUMERICAL CODE INDICATING THE HIGHER CATEGORY OF THE FIRST VARIABLE. IF ANY VALUE OF VARIABLE U IS EQUAL TO OR GREATER THAN HU, IT WILL BE CLASSIFIED AS THE HIGHER CATEGORY, OTHERWISE AS THE LOWER CATEGORY.
HV - SAME AS HU EXCEPT THAT HV IS FOR THE SECOND VARIABLE.
R - TETRACHORIC CORRELATION COMPUTED
RS - STANDARD ERROR OF TETRACHORIC CORRELATION COMPUTED
IE - ERROR CODE
0 - NO ERROR
1 - UNABLE TO COMPUTE A TETRACHORIC CORRELATION DUE TO THE FACT THAT AT LEAST ONE CELL SHOWS ZERO FREQUENCY IN THE 2X2 CONTINGENCY TABLE CONSTRUCTED FROM INPUT DATA. IN THIS CASE, R AND RS ARE SET TO 10**75. (SEE GUILFORD, 1956)
2 - THE ROOT SOLVER GIVES MULTIPLE ROOTS, OR NO ROOTS, R, IN THE INTERVAL (-1,1) INCLUSIVE. R AND RS ARE SET TO 10**75.
3 - UNABLE TO COMPUTE A SATISFACTORY VALUE OF TETRACHORIC CORRELATION USING NEWTON-RAPHSON METHOD OF APPROXIMATION TO THE ROOT OF THE EQUATION. R AND RS ARE SET TO 10**75. SEE SUBROUTINE POLRT ERROR INDICATORS.
4 - HIGH ORDER COEFFICIENT OF THE POLYNOMIAL IS ZERO. SEE SUBROUTINE POLRT ERROR INDICATORS.

REMARKS
VALUES OF VARIABLES U AND V MUST BE NUMERICAL, AND ALPHABETIC AND SPECIAL CHARACTERS MUST NOT BE USED. FOR A DEPENDABLE RESULT FOR TETRACHORIC CORRELATION, IT IS RECOMMENDED THAT N BE AT LEAST 200 OR GREATER.

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NDTRI
POLRT--THIS POLYNOMIAL ROOT ROUTINE WAS SELECTED BECAUSE OF ITS SMALL STORAGE REQUIREMENT. OTHER SSP ROUTINES

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C-----TETR 550
C-----TETR 560
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C-----TETR 620
C-----TETR 630
C-----TETR 640
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C-----TETR1110
C-----TETR1120
C-----TETR1130
C-----TETR1140
C-----TETR1150
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C-----TETR1180
C-----TETR1190
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C-----TETR1370
C-----TETR1380
C-----TETR1390
C-----TETR1400
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C-----TETR1420
C-----TETR1430
C-----TETR1440
C-----TETR1450
C-----TETR1460
C-----TETR1470
C-----TETR1480
C-----TETR1490
C-----TETR1500
C-----TETR1510
C-----TETR1520
C-----TETR1530
C-----TETR1540
C-----TETR1550
C-----TETR1560
C-----TETR1570
C-----TETR1580
C-----TETR1590
C-----TETR1600
C-----TETR1610
C-----TETR1620
C-----TETR1630
C-----TETR1640
C-----TETR1650
C-----TETR1660
C-----TETR1670

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WHICH COULD REPLACE POLRT ARE PROG AND PRGM. THEIR USE WOULD REQUIRE MODIFICATION OF TETRA.

METHOD
REFER TO J. P. GUILFORD, 'FUNDAMENTAL STATISTICS IN PSYCHOLOGY AND EDUCATION', MCGRAW-HILL, NEW YORK, 1956, CHAPTER 13 AND W. P. ELDERTON, 'FREQUENCY CURVES AND CORRELATION' 4-TH ED., 'CAMBRIDGE UNIVERSITY PRESS, 1953, CHAPTER 9.

SUBROUTINE TETRA (N,U,V,HU,HV,R,RS,IE)

DIMENSION XCOF(8),COF(8),ROOTR(7),ROOTI(7)
DIMENSION U(1),V(1)
DOUBLE PRECISION X31,X32,X312,X322

CONSTRUCT A 2X2 CONTINGENCY TABLE

A=0.0
B=0.0
C=0.0
D=0.0
DO 40 I=1,N
IF(U(I)-HU) 10, 25, 25
10 IF(V(I)-HV) 15, 20, 20
15 D=D+1.0
GO TO 40
20 B=B+1.0
GO TO 40
25 IF(V(I)-HV) 30, 35, 35
30 C=C+1.0
GO TO 40
35 A=A+1.0
40 CONTINUE

TEST WHETHER ANY CELL IN THE CONTINGENCY TABLE IS ZERO.
IF SO, RETURN TO THE CALLING ROUTINE WITH R=0.0 AND IE=1.

IE=0
IF(A) 60, 60, 45
45 IF(B) 60, 60, 50
50 IF(C) 60, 60, 55
55 IF(D) 60, 60, 70
60 IE=1
GO TO 86

COMPUTE P1, Q1, P2, AND Q2

FN=N
P1=(A+C)/FN
Q1=(B+D)/FN
P2=(A+B)/FN
Q2=(C+D)/FN

FIND THE STANDARD NORMAL DEVIATES AT Q1 AND Q2, AND THE ORDINATES AT THOSE POINTS

CALL NDTRI (Q1,X1,Y1,FR)
CALL NDTRI (Q2,X2,Y2,ER)

COMPUTE THE TETRACHORIC CORRELATION COEFFICIENT

IF(X1) 76, 72, 76
72 IF(X2) 76, 74, 76
74 F=0.0
GO TO 99
76 XCOF(1)=-((A*D-B*C)/(Y1*Y2+F*FN))
XCOF(2)=1.0
XCOF(3)=X1*X2/2.0
XCOF(4)=(X1*X1-1.0)*(X2*X2-1.0)/6.0
X31=DBLE(X1)
X32=DBLE(X2)
X312=X31**2
X322=X32**2
XCOF(5)=SNGL(X31*(X312-3.000)*X32*(X322-3.000)/24.000)
XCOF(6)=SNGL((X312*(X312-6.000)+3.000)*(X322*(X322-6.000)+3.000)/120.000)
1 XCOF(7)=SNGL(X31*(X312*(X312-10.000)+15.000)*X32*(X322*(X322-10.000)+15.000)/720.000)
1 XCOF(8)=SNGL(((X312-15.000)*X312+45.000)*X312*(X312-15.000))*((X322-15.000)*X322+45.000)*X322*(X322-15.000)/5040.000)

CALL POLRT (XCOF,COF,7,ROOTR,ROOTI,IER)

J=0
IF(IER) 78, 78, 84
78 DO 82 I=1,7
IF(ABS(ROOTI(I))-5*ABS(ROOTR(I))*1.0E-6)79,79,82
79 R=ROOTR(I)
IF(ABS(R)-1.C181.81.80
80 R=1.E75
GO TO 82
81 J=J+1
82 CONTINUE
IF(J-1)83,88,83
83 IE=2
GO TO 86

UNABLE TO COMPUTE R

84 IE=IER
86 P=1.0E75
RS=R
GO TO 100
88 IF(R-1.0E75)90,83,83

STANDARD ERROR OF R=0.0

90 RS=SQRT(P1*P2*Q1*Q2)/(Y1*Y2*SQRT(FN))

100 RETURN
END


```

C ..... SRAT 610
C ..... SRAT 620
C ..... SRAT 630
SUBROUTINE SRATE (N,K,X,IE) SRAT 640
C ..... SRAT 650
DIMENSION X(1) SRAT 660
C ..... SRAT 670
C ..... SRAT 680
C ..... SRAT 690
C ..... SRAT 700
C ..... SRAT 710
C ..... SRAT 720
C ..... SRAT 730
C ..... SRAT 740
C ..... SRAT 750
C ..... SRAT 760
C ..... SRAT 770
C ..... SRAT 780
C ..... SRAT 790
C ..... SRAT 800
C ..... SRAT 810
C ..... SRAT 820
C ..... SRAT 830
C ..... SRAT 840
C ..... SRAT 850
C ..... SRAT 860
C ..... SRAT 870
C ..... SRAT 880
C ..... SRAT 890
C ..... SRAT 900
C ..... SRAT 910
C ..... SRAT 920
C ..... SRAT 930
C ..... SRAT 940
C ..... SRAT 950
C ..... SRAT 960
C ..... SRAT 970
C ..... SRAT 980
C ..... SRAT 990
C ..... SRAT1000
C ..... SRAT1010
C ..... SRAT1020
C ..... SRAT1030

```

```

C DD 40 I=1,K SRAT1040
C ..... SRAT1050
C ..... SRAT1060
C ..... SRAT1070
C ..... SRAT1080
C ..... SRAT1090
C ..... SRAT1100
C ..... SRAT1110
C ..... SRAT1120
C ..... SRAT1130
C ..... SRAT1140
C ..... SRAT1150
C ..... SRAT1160
C ..... SRAT1170
C ..... SRAT1180
C ..... SRAT1190
C ..... SRAT1200
C ..... SRAT1210
C ..... SRAT1220
C ..... SRAT1230
C ..... SRAT1240
C ..... SRAT1250
C ..... SRAT1260
C ..... SRAT1270
C ..... SRAT1280
C ..... SRAT1290
C ..... SRAT1300
C ..... SRAT1310
C ..... SRAT1320
C ..... SRAT1330
C ..... SRAT1340
C ..... SRAT1350
C ..... SRAT1360
C ..... SRAT1370
C ..... SRAT1380
C ..... SRAT1390
C ..... SRAT1400
C ..... SRAT1410

```

MATHEMATICS

Matrices: Storage

Subroutine MCPY

```

C
C
C ..... MCPY 10
C ..... MCPY 20
C ..... MCPY 30
C ..... MCPY 40
C ..... MCPY 50
C ..... MCPY 60
C ..... MCPY 70
C ..... MCPY 80
C ..... MCPY 90
C ..... MCPY 100
C ..... MCPY 110
C ..... MCPY 120
C ..... MCPY 130
C ..... MCPY 140
C ..... MCPY 150
C ..... MCPY 160
C ..... MCPY 170
C ..... MCPY 180
C ..... MCPY 190
C ..... MCPY 200
C ..... MCPY 210
C ..... MCPY 220
C ..... MCPY 230
C ..... MCPY 240
C ..... MCPY 250
C ..... MCPY 260
C ..... MCPY 270
C ..... MCPY 280
C ..... MCPY 290
C ..... MCPY 300
C ..... MCPY 310
C ..... MCPY 320
C ..... MCPY 330
C ..... MCPY 340
C ..... MCPY 350
C ..... MCPY 360
C ..... MCPY 370
C ..... MCPY 380
C ..... MCPY 390
C ..... MCPY 400
C ..... MCPY 410
C ..... MCPY 420
C ..... MCPY 430
C ..... MCPY 440
C ..... MCPY 450
C ..... MCPY 460
C
SUBROUTINE MCPY
COPY ENTIRE MATRIX
USAGE
CALL MCPY (A,R,N,M,MS)
DESCRIPTION OF PARAMETERS
A - NAME OF INPUT MATRIX
R - NAME OF OUTPUT MATRIX
N - NUMBER OF ROWS IN A OR R
M - NUMBER OF COLUMNS IN A OR R
MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A (AND R)
      0 - GENERAL
      1 - SYMMETRIC
      2 - DIAGONAL
REMARKS
NONE
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
LOC
METHOD
EACH ELEMENT OF MATRIX A IS MOVED TO THE CORRESPONDING
ELEMENT OF MATRIX R
.....
SUBROUTINE MCPY(A,R,N,M,MS)
DIMENSION A(1),R(1)
      COMPUTE VECTOR LENGTH, IT
      CALL LOC(N,M,IT,N,M,MS)
      COPY MATRIX
      DO 1 I=1,IT
      R(I)=A(I)
      RETURN
      END

```

Subroutine RCPY

```

C
C ..... RCPY 10
C ..... RCPY 20
C ..... RCPY 30
C ..... RCPY 40
C ..... RCPY 50
C ..... RCPY 60
C ..... RCPY 70
C ..... RCPY 80
C ..... RCPY 90
C ..... RCPY 100
C ..... RCPY 110
C ..... RCPY 120
C ..... RCPY 130
C ..... RCPY 140
C ..... RCPY 150
C ..... RCPY 160
C ..... RCPY 170
C ..... RCPY 180
C ..... RCPY 190
C ..... RCPY 200
C ..... RCPY 210
C ..... RCPY 220
C ..... RCPY 230
C ..... RCPY 240
C ..... RCPY 250
C ..... RCPY 260
C ..... RCPY 270
C ..... RCPY 280
C ..... RCPY 290
C ..... RCPY 300
C ..... RCPY 310
C ..... RCPY 320
C ..... RCPY 330
C ..... RCPY 340
C ..... RCPY 350
C ..... RCPY 360
C ..... RCPY 370
C ..... RCPY 380
C ..... RCPY 390
C ..... RCPY 400
C ..... RCPY 410
C ..... RCPY 420
C ..... RCPY 430
C ..... RCPY 440
C ..... RCPY 450
C ..... RCPY 460
C ..... RCPY 470
C ..... RCPY 480
C ..... RCPY 490
C ..... RCPY 500
C ..... RCPY 510
C ..... RCPY 520
C ..... RCPY 530
C ..... RCPY 540
C ..... RCPY 550
C
SUBROUTINE RCPY
PURPOSE
COPY SPECIFIED ROW OF A MATRIX INTO A VECTOR
USAGE
CALL RCPY (A,L,R,N,M,MS)
DESCRIPTION OF PARAMETERS
A - NAME OF INPUT MATRIX
L - ROW OF A TO BE MOVED TO R
N - NAME OF OUTPUT VECTOR OF LENGTH M
M - NUMBER OF ROWS IN A
MS - NUMBER OF COLUMNS IN A
MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
      0 - GENERAL
      1 - SYMMETRIC
      2 - DIAGONAL
REMARKS
NONE
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
LOC
METHOD
ELEMENTS OF ROW L ARE MOVED TO CORRESPONDING POSITIONS
OF VECTOR R
.....
SUBROUTINE RCPY(A,L,R,N,M,MS)
DIMENSION A(1),R(1)
      DO 3 J=1,M
      LOCATE ELEMENT FOR ANY MATRIX STORAGE MODE
      CALL LOC(L,J,L,N,M,MS)
      TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
      IF(L) 1,2,1
      MOVE ELEMENT TO R
      1 R(J)=A(L)
      GO TO 3
      2 R(J)=0
      3 CONTINUE
      RETURN
      END

```


Subroutine XCPY

```

C ..... XCPY 13
C ..... XCPY 20
C ..... XCPY 30
C ..... XCPY 40
SUBROUTINE XCPY XCPY 40
C ..... XCPY 50
C ..... XCPY 53
PURPOSE XCPY 53
C ..... XCPY 60
C ..... XCPY 70
C ..... XCPY 80
C ..... XCPY 90
C ..... XCPY 90
C ..... XCPY 100
C ..... XCPY 110
C ..... XCPY 120
C ..... XCPY 130
C ..... XCPY 140
C ..... XCPY 150
C ..... XCPY 160
C ..... XCPY 170
C ..... XCPY 180
C ..... XCPY 190
C ..... XCPY 200
C ..... XCPY 210
C ..... XCPY 220
C ..... XCPY 230
C ..... XCPY 240
C ..... XCPY 250
C ..... XCPY 260
C ..... XCPY 270
C ..... XCPY 280
C ..... XCPY 290
C ..... XCPY 300
C ..... XCPY 310
C ..... XCPY 320
C ..... XCPY 330
C ..... XCPY 340
C ..... XCPY 350
C ..... XCPY 360
C ..... XCPY 370
C ..... XCPY 380
C ..... XCPY 390
C ..... XCPY 400
C ..... XCPY 410
C ..... XCPY 420
C ..... XCPY 430
C ..... XCPY 440
C ..... XCPY 450
C ..... XCPY 460
C ..... XCPY 470
C ..... XCPY 480
C ..... XCPY 490
C ..... XCPY 500
C ..... XCPY 510
C ..... XCPY 520
C ..... XCPY 530
C ..... XCPY 540
C ..... XCPY 550
C ..... XCPY 560
C ..... XCPY 570
C ..... XCPY 580
C ..... XCPY 590
C ..... XCPY 500
C ..... XCPY 610
C ..... XCPY 620
C ..... XCPY 630
C ..... XCPY 640
C ..... XCPY 640

SUBROUTINE XCPY(A,R,L,K,NR,NA,MA,MS)
DIMENSION A(L),R(1)

INITIALIZE
IR=0
L2=L+NR-1
K2=K+NR-1

DO 5 J=K,K2
DO 5 I=L,L2
IR=IR+1
R(IR)=C.0

LOCATE ELEMENT FOR ANY MATRIX STORAGE MODE
CALL LOC(I,J,IA,NA,MA,MS)

TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
IF(IA) 4,5,4
4 R(IR)=A(IA)
5 CONTINUE
RETURN
END

```

Subroutine MSTR

```

C ..... MSTR 10
C ..... MSTR 20
C ..... MSTR 30
C ..... MSTR 40
SUBROUTINE MSTR MSTR 40
C ..... MSTR 50
C ..... MSTR 60
PURPOSE MSTR 60
C ..... MSTR 70
C ..... MSTR 80
C ..... MSTR 90
C ..... MSTR 100
C ..... MSTR 110
C ..... MSTR 120
C ..... MSTR 130
C ..... MSTR 140
C ..... MSTR 150
C ..... MSTR 160
C ..... MSTR 170
C ..... MSTR 180
C ..... MSTR 190
C ..... MSTR 200
C ..... MSTR 210
C ..... MSTR 220
C ..... MSTR 230
C ..... MSTR 240
C ..... MSTR 250
C ..... MSTR 260
C ..... MSTR 270
C ..... MSTR 280
C ..... MSTR 290
C ..... MSTR 300
C ..... MSTR 310
C ..... MSTR 320
C ..... MSTR 330
C ..... MSTR 340
C ..... MSTR 350
C ..... MSTR 360
C ..... MSTR 370
C ..... MSTR 380
C ..... MSTR 390
C ..... MSTR 400
C ..... MSTR 410
C ..... MSTR 420
C ..... MSTR 430
C ..... MSTR 440
C ..... MSTR 450
C ..... MSTR 460
C ..... MSTR 470
C ..... MSTR 480
C ..... MSTR 490
C ..... MSTR 500
C ..... MSTR 510
C ..... MSTR 520
C ..... MSTR 530
C ..... MSTR 540
C ..... MSTR 550
C ..... MSTR 560
C ..... MSTR 570
C ..... MSTR 580
C ..... MSTR 590
C ..... MSTR 600
C ..... MSTR 610
C ..... MSTR 620
C ..... MSTR 630
C ..... MSTR 640
C ..... MSTR 650
C ..... MSTR 660
C ..... MSTR 670
C ..... MSTR 680
C ..... MSTR 690
C ..... MSTR 700
C ..... MSTR 710
C ..... MSTR 720
C ..... MSTR 730
C ..... MSTR 740
C ..... MSTR 750
C ..... MSTR 760
C ..... MSTR 770
C ..... MSTR 780
C ..... MSTR 790
C ..... MSTR 800

SUBROUTINE MSTR(A,R,N,MSA,MSR)
CHANGE STORAGE MODE OF A MATRIX
PURPOSE MSTR 70
C ..... MSTR 80
C ..... MSTR 90
C ..... MSTR 100
C ..... MSTR 110
C ..... MSTR 120
C ..... MSTR 130
C ..... MSTR 140
C ..... MSTR 150
C ..... MSTR 160
C ..... MSTR 170
C ..... MSTR 180
C ..... MSTR 190
C ..... MSTR 200
C ..... MSTR 210
C ..... MSTR 220
C ..... MSTR 230
C ..... MSTR 240
C ..... MSTR 250
C ..... MSTR 260
C ..... MSTR 270
C ..... MSTR 280
C ..... MSTR 290
C ..... MSTR 300
C ..... MSTR 310
C ..... MSTR 320
C ..... MSTR 330
C ..... MSTR 340
C ..... MSTR 350
C ..... MSTR 360
C ..... MSTR 370
C ..... MSTR 380
C ..... MSTR 390
C ..... MSTR 400
C ..... MSTR 410
C ..... MSTR 420
C ..... MSTR 430
C ..... MSTR 440
C ..... MSTR 450
C ..... MSTR 460
C ..... MSTR 470
C ..... MSTR 480
C ..... MSTR 490
C ..... MSTR 500
C ..... MSTR 510
C ..... MSTR 520
C ..... MSTR 530
C ..... MSTR 540
C ..... MSTR 550
C ..... MSTR 560
C ..... MSTR 570
C ..... MSTR 580
C ..... MSTR 590
C ..... MSTR 600
C ..... MSTR 610
C ..... MSTR 620
C ..... MSTR 630
C ..... MSTR 640
C ..... MSTR 650
C ..... MSTR 660
C ..... MSTR 670
C ..... MSTR 680
C ..... MSTR 690
C ..... MSTR 700
C ..... MSTR 710
C ..... MSTR 720
C ..... MSTR 730
C ..... MSTR 740
C ..... MSTR 750
C ..... MSTR 760
C ..... MSTR 770
C ..... MSTR 780
C ..... MSTR 790
C ..... MSTR 800

DESCRIPTION OF PARAMETERS
A - NAME OF INPUT MATRIX
R - NAME OF OUTPUT MATRIX
N - NUMBER OF ROWS AND COLUMNS IN A AND R
MSA - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
0 - GENERAL
1 - SYMMETRIC
2 - DIAGONAL
MSR - SAME AS MSA EXCEPT FOR MATRIX R

REMARKS
MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRIX A
MATRIX A MUST BE A SQUARE MATRIX

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
LOC

METHOD
MATRIX A IS RESTRUCTURED TO FORM MATRIX R.
MSA MSR
0 0 MATRIX A IS MOVED TO MATRIX R
0 1 THE UPPER TRIANGLE ELEMENTS OF A GENERAL MATRIX
ARE USED TO FORM A SYMMETRIC MATRIX
0 2 THE DIAGONAL ELEMENTS OF A GENERAL MATRIX ARE USED
TO FORM A DIAGONAL MATRIX
1 0 A SYMMETRIC MATRIX IS EXPANDED TO FORM A GENERAL
MATRIX
1 1 MATRIX A IS MOVED TO MATRIX R
1 2 THE DIAGONAL ELEMENTS OF A SYMMETRIC MATRIX ARE
USED TO FORM A DIAGONAL MATRIX
2 0 A DIAGONAL MATRIX IS EXPANDED BY INSERTING MISSING
ZERO ELEMENTS TO FORM A GENERAL MATRIX
2 1 A DIAGONAL MATRIX IS EXPANDED BY INSERTING MISSING
ZERO ELEMENTS TO FORM A SYMMETRIC MATRIX
2 2 MATRIX A IS MOVED TO MATRIX R

```

Subroutine LOC

```

C
C
C ..... LOC 10
C
C SUBROUTINE LOC LOC 20
C
C PURPOSE LOC 30
C COMPUTE A VECTOR SUBSCRIPT FOR AN ELEMENT IN A MATRIX OF LOC 40
C SPECIFIED STORAGE MODE LOC 50
C LOC 60
C USAGE LOC 70
C CALL LOC (I,J,IR,N,M,MS) LOC 80
C LOC 90
C DESCRIPTION OF PARAMETERS LOC 100
C I - ROW NUMBER OF ELEMENT LOC 110
C J - COLUMN NUMBER OF ELEMENT LOC 120
C IR - RESULTANT VECTOR SUBSCRIPT LOC 130
C N - NUMBER OF ROWS IN MATRIX LOC 140
C M - NUMBER OF COLUMNS IN MATRIX LOC 150
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX LOC 160
C 0 - GENERAL LOC 170
C 1 - SYMMETRIC LOC 180
C 2 - DIAGONAL LOC 190
C
C REMARKS LOC 200
C NONE LOC 210
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED LOC 220
C NONE LOC 230
C
C METHOD LOC 240
C MS=0 SUBSCRIPT IS COMPUTED FOR A MATRIX WITH N*M ELEMENTS LOC 250
C IN STORAGE (GENERAL MATRIX) LOC 260
C MS=1 SUBSCRIPT IS COMPUTED FOR A MATRIX WITH N*(N+1)/2 IN LOC 270
C STORAGE (UPPER TRIANGLE OF SYMMETRIC MATRIX). IF LOC 280
C ELEMENT IS IN LOWER TRIANGULAR PORTION, SUBSCRIPT IS LOC 290
C CORRESPONDING ELEMENT IN UPPER TRIANGLE. LOC 300
C MS=2 SUBSCRIPT IS COMPUTED FOR A MATRIX WITH N ELEMENTS LOC 310
C IN STORAGE (DIAGONAL ELEMENTS OF DIAGONAL MATRIX). LOC 320
C IF ELEMENT IS NOT ON DIAGONAL (AND THEREFORE NOT IN LOC 330
C STORAGE), IR IS SET TO ZERO. LOC 340
C
C ..... LOC 410
C
C SUBROUTINE LOC(I,J,IR,N,M,MS) LOC 420
C LOC 430
C LOC 440
C LOC 450
C IX=I LOC 460
C JX=J LOC 470
C IF(MS=1) 10,20,30 LOC 480
C IRX=N*(JX-1)+IX LOC 490
C GO TO 36 LOC 500
C 10 IF(I-X) 22,24+24 LOC 510
C 22 IRX=IX+(JX-JX-JX)/2 LOC 520
C GO TO 36 LOC 530
C 24 IRX=JX+(IX-I-X)/2 LOC 540
C GO TO 36 LOC 550
C 30 IRX=0 LOC 560
C IF(I-X) 36,32,36 LOC 570
C 32 IRX=IX LOC 580
C 36 IR=IRX LOC 590
C RETURN LOC 600
C END LOC 610

```

Subroutine CONV T

```

C
C ..... CONV 10
C
C SUBROUTINE CONV T CONV 20
C
C PURPOSE CONV 30
C CONVERT NUMBERS FROM SINGLE PRECISION TO DOUBLE PRECISION CONV 40
C OR FROM DOUBLE PRECISION TO SINGLE PRECISION. CONV 50
C USAGE CONV 60
C CALL CONV T (N,M,MODE,S,D,MS) CONV 70
C CONV 80
C CONV 90
C DESCRIPTION OF PARAMETERS CONV 100
C N - NUMBER OF ROWS IN MATRICES S AND D. CONV 110
C M - NUMBER OF COLUMNS IN MATRICES S AND D. CONV 120
C MODE - CODE INDICATING TYPE OF CONVERSION CONV 130
C 1 - FROM SINGLE PRECISION TO DOUBLE PRECISION CONV 140
C 2 - FROM DOUBLE PRECISION TO SINGLE PRECISION CONV 150
C S - IF MODE=1, THIS MATRIX CONTAINS SINGLE PRECISION CONV 160
C NUMBERS AS INPUT. IF MODE=2, IT CONTAINS SINGLE CONV 170
C PRECISION NUMBERS AS OUTPUT. THE SIZE OF MATRIX S CONV 180
C IS N BY M. CONV 190
C D - IF MODE=1, THIS MATRIX CONTAINS DOUBLE PRECISION CONV 200
C NUMBERS AS OUTPUT. IF MODE=2, IT CONTAINS DOUBLE CONV 210
C PRECISION NUMBERS AS INPUT. THE SIZE OF MATRIX D IS CONV 220
C N BY M. CONV 230
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX CONV 240
C 0 - GENERAL CONV 250
C 1 - SYMMETRIC CONV 260
C 2 - DIAGONAL CONV 270
C
C REMARKS CONV 280
C MATRIX D CANNOT BE IN THE SAME LOCATION AS MATRIX S. CONV 290
C MATRIX D MUST BE DEFINED BY A DOUBLE PRECISION STATEMENT IN CONV 300
C THE CALLING PROGRAM. CONV 310
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED CONV 320
C NONE CONV 330
C
C METHOD CONV 340
C ACCORDING TO THE TYPE OF CONVERSION INDICATED IN MODE, THIS CONV 350
C SUBROUTINE COPIES NUMBERS FROM MATRIX S TO MATRIX D OR FROM CONV 360
C MATRIX D TO MATRIX S. CONV 370
C
C ..... CONV 400
C
C SUBROUTINE CONV T (N,M,MODE,S,D,MS) CONV 410
C DIMENSION S(L),D(L) CONV 420
C DOUBLE PRECISION D CONV 430
C
C FIND STORAGE MODE OF MATRIX AND NUMBER OF DATA POINTS CONV 440
C
C IF(MS=1) 2, 4, 6 CONV 450
C 2 NM=N*M CONV 460
C GO TO 8 CONV 470
C 4 NM=((N+1)*N)/2 CONV 480
C GO TO 8 CONV 490
C 6 NM=N CONV 500
C
C TEST TYPE OF CONVERSION CONV 510
C
C 8 IF(MODE=1) 10, 10, 20 CONV 520
C
C SINGLE PRECISION TO DOUBLE PRECISION CONV 530
C
C 10 DO 15 L=1,NM CONV 540
C 15 D(L)=S(L) CONV 550
C GO TO 30 CONV 560
C
C DOUBLE PRECISION TO SINGLE PRECISION CONV 570
C
C 20 DO 25 L=1,NM CONV 580
C 25 S(L)=D(L) CONV 590
C
C 30 RETURN CONV 600
C END CONV 610

```

Subroutine ARRAY

```

C .....
C SUBROUTINE ARRAY
C PURPOSE
C CONVERT DATA ARRAY FROM SINGLE TO DOUBLE DIMENSION OR VICE
C VERSA. THIS SUBROUTINE IS USED TO LINK THE USER PROGRAM
C WHICH HAS DOUBLE DIMENSION ARRAYS AND THE SSP SUBROUTINES
C WHICH OPERATE ON ARRAYS OF DATA IN A VECTOR FASHION.
C USAGE
C CALL ARRAY (MODE,I,J,N,M,S,D)
C DESCRIPTION OF PARAMETERS
C MODE - CODE INDICATING TYPE OF CONVERSION
C 1 - FROM SINGLE TO DOUBLE DIMENSION
C 2 - FROM DOUBLE TO SINGLE DIMENSION
C I - NUMBER OF ROWS IN ACTUAL DATA MATRIX
C J - NUMBER OF COLUMNS IN ACTUAL DATA MATRIX
C N - NUMBER OF ROWS SPECIFIED FOR THE MATRIX D IN
C DIMENSION STATEMENT
C M - NUMBER OF COLUMNS SPECIFIED FOR THE MATRIX D IN
C DIMENSION STATEMENT
C S - IF MODE=1, THIS VECTOR IS INPUT WHICH CONTAINS THE
C ELEMENTS OF A DATA MATRIX OF SIZE I BY J. COLUMN I+1
C OF DATA MATRIX FOLLOWS COLUMN I, ETC. IF MODE=2,
C THIS VECTOR IS OUTPUT REPRESENTING A DATA MATRIX OF
C SIZE I BY J CONTAINING ITS COLUMNS CONSECUTIVELY.
C THE LENGTH OF S IS IJ, WHERE IJ=I*J.
C J - IF MODE=1, THIS MATRIX OF SIZE N BY M IS OUTPUT,
C CONTAINING A DATA MATRIX OF SIZE I BY J IN THE FIRST
C I ROWS AND J COLUMNS. IF MODE=2, THIS N BY M MATRIX
C IS INPUT CONTAINING A DATA MATRIX OF SIZE I BY J IN
C THE FIRST I ROWS AND J COLUMNS.
C REMARKS
C VECTOR S CAN BE IN THE SAME LOCATION AS MATRIX J. VECTOR S
C IS REFERRED AS A MATRIX IN OTHER SSP ROUTINES, SINCE IT
C CONTAINS A DATA MATRIX.
C THIS SUBROUTINE CONVERTS ONLY GENERAL DATA MATRICES (STORAGE
C MODE OF 0).
C SUBROUTINES AND FUNCTION SUBROUTINES REQUIRED
C NONE
C METHOD
C REFER TO THE DISCUSSION ON VARIABLE DATA SIZE IN THE SECTION
C DESCRIBING OVERALL RULES FOR USAGE IN THIS MANUAL.
C .....
C SUBROUTINE ARRAY (MODE,I,J,N,M,S,D)
C DIMENSION S(I),D(I)
C NI=N-I
C TEST TYPE OF CONVERSION
C IF(MODE-1) 100, 100, 120
C CONVERT FROM SINGLE TO DOUBLE DIMENSION
100 IJ=I*J+1
NM=N*M+1
DO 110 K=1,J
NM=NM-NI
DO 110 L=1,I
IJ=IJ-1
NM=NM-1
110 D(NM)=S(IJ)
GO TO 140
C CONVERT FROM DOUBLE TO SINGLE DIMENSION
120 IJ=0
NM=0
DO 130 K=1,J
DO 125 L=1,I
IJ=IJ+1
NM=NM+1
125 S(IJ)=D(NM)
130 NM=NM+1
140 RETURN
END

```

Matrices: Operations

Subroutine GMADD

```

C .....
C SUBROUTINE GMADD
C PURPOSE
C ADD TWO GENERAL MATRICES TO FORM RESULTANT GENERAL MATRIX
C USAGE
C CALL GMADD(A,B,R,N,M)
C DESCRIPTION OF PARAMETERS
C A - NAME OF FIRST INPUT MATRIX
C B - NAME OF SECOND INPUT MATRIX
C R - NAME OF OUTPUT MATRIX
C N - NUMBER OF ROWS IN A+B,R
C M - NUMBER OF COLUMNS IN A+B,R
C REMARKS
C ALL MATRICES MUST BE STORED AS GENERAL MATRICES
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C METHOD
C ADDITION IS PERFORMED ELEMENT BY ELEMENT
C .....
C SUBROUTINE GMADD(A,B,R,N,M)
C DIMENSION A(I),B(I),R(I)
C CALCULATE NUMBER OF ELEMENTS
NM=N*M
C ADD MATRICES
DO 10 I=1,NM
10 R(I)=A(I)+B(I)
RETURN
END

```

Subroutine GMSUB

```

C ..... GMSU 10
C ..... GMSU 20
C ..... GMSU 30
C SUBROUTINE GMSUB GMSU 40
C ..... GMSU 50
C PURPOSE GMSU 60
C SUBTRACT ONE GENERAL MATRIX FROM ANOTHER TO FORM RESULTANT GMSU 70
C MATRIX GMSU 85
C ..... GMSU 90
C USAGE GMSU 100
C CALL GMSUB(A,B,R,N,M) GMSU 110
C ..... GMSU 120
C DESCRIPTION OF PARAMETERS GMSU 130
C A - NAME OF FIRST INPUT MATRIX GMSU 140
C B - NAME OF SECOND INPUT MATRIX GMSU 150
C R - NAME OF OUTPUT MATRIX GMSU 160
C N - NUMBER OF ROWS IN A,B,R GMSU 170
C M - NUMBER OF COLUMNS IN A,B,R GMSU 180
C ..... GMSU 190
C REMARKS GMSU 200
C ALL MATRICES MUST BE STORED AS GENERAL MATRICES GMSU 210
C ..... GMSU 220
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED GMSU 230
C NONE GMSU 240
C ..... GMSU 250
C METHOD GMSU 260
C MATRIX B ELEMENTS ARE SUBTRACTED FROM CORRESPONDING MATRIX GMSU 270
C ELEMENTS GMSU 280
C ..... GMSU 290
C ..... GMSU 300
C ..... GMSU 310
C SUBROUTINE GMSUB(A,B,R,N,M) GMSU 320
C DIMENSION A(1),B(1),R(1) GMSU 330
C ..... GMSU 340
C CALCULATE NUMBER OF ELEMENTS GMSU 350
C ..... GMSU 360
C NM=N*M GMSU 370
C ..... GMSU 380
C SUBTRACT MATRICES GMSU 390
C ..... GMSU 400
C DO 10 I=1,NM GMSU 410
C R(I)=A(I)-B(I) GMSU 420
C RETURN GMSU 430
C END GMSU 440

```

Subroutine GMPRD

```

C ..... GMPR 10
C ..... GMPR 20
C ..... GMPR 30
C SUBROUTINE GMPRD GMPR 40
C ..... GMPR 50
C PURPOSE GMPR 60
C MULTIPLY TWO GENERAL MATRICES TO FORM A RESULTANT GENERAL GMPR 70
C MATRIX GMPR 80
C ..... GMPR 90
C USAGE GMPR 100
C CALL GMPRD(A,B,R,N,M,L) GMPR 110
C ..... GMPR 120
C DESCRIPTION OF PARAMETERS GMPR 130
C A - NAME OF FIRST INPUT MATRIX GMPR 140
C B - NAME OF SECOND INPUT MATRIX GMPR 150
C R - NAME OF OUTPUT MATRIX GMPR 160
C N - NUMBER OF ROWS IN A GMPR 170
C M - NUMBER OF COLUMNS IN A AND ROWS IN B GMPR 180
C L - NUMBER OF COLUMNS IN B GMPR 190
C ..... GMPR 200
C REMARKS GMPR 210
C ALL MATRICES MUST BE STORED AS GENERAL MATRICES GMPR 220
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRIX A GMPR 230
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRIX B GMPR 240
C NUMBER OF COLUMNS OF MATRIX A MUST BE EQUAL TO NUMBER OF ROWS GMPR 250
C OF MATRIX B GMPR 260
C ..... GMPR 270
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED GMPR 280
C NONE GMPR 290
C ..... GMPR 300
C METHOD GMPR 310
C THE M BY L MATRIX B IS PREMULTIPLIED BY THE N BY M MATRIX A GMPR 320
C AND THE RESULT IS STORED IN THE N BY L MATRIX R. GMPR 330
C ..... GMPR 340
C ..... GMPR 350
C SUBROUTINE GMPRD(A,B,R,N,M,L) GMPR 360
C DIMENSION A(1),B(1),R(1) GMPR 370
C ..... GMPR 380
C ..... GMPR 390
C IR=0 GMPR 400
C IK=-M GMPR 410
C DO 10 K=1,L GMPR 420
C IK=IK+M GMPR 430
C DO 10 J=1,N GMPR 440
C IR=IR+1 GMPR 450
C JI=J-N GMPR 460
C IB=IK GMPR 470
C R(IR)=0 GMPR 480
C DO 10 I=1,M GMPR 490
C JI=JI+N GMPR 500
C IB=IB+1 GMPR 510
C 10 R(IR)=R(IR)+A(JI)*B(IB) GMPR 520
C RETURN GMPR 530
C END GMPR 540

```


Subroutine MADD

```

C ..... MADD 10
C ..... MADD 20
C ..... MADD 30
C ..... MADD 40
C ..... MADD 50
C ..... MADD 60
C ..... MADD 70
C ..... MADD 80
C ..... MADD 90
C ..... MADD 100
C ..... MADD 110
C ..... MADD 120
C ..... MADD 130
C ..... MADD 140
C ..... MADD 150
C ..... MADD 160
C ..... MADD 170
C ..... MADD 180
C ..... MADD 190
C ..... MADD 200
C ..... MADD 210
C ..... MADD 220
C ..... MADD 230
C ..... MADD 240
C ..... MADD 250
C ..... MADD 260
C ..... MADD 270
C ..... MADD 280
C ..... MADD 290
C ..... MADD 300
C ..... MADD 310
C ..... MADD 320
C ..... MADD 330
C ..... MADD 340
C ..... MADD 350
C ..... MADD 360
C ..... MADD 370
C ..... MADD 380
C ..... MADD 390
C ..... MADD 400
C ..... MADD 410
C ..... MADD 420
C ..... MADD 430
C ..... MADD 440
C ..... MADD 450
C ..... MADD 460
C ..... MADD 470
C ..... MADD 480
C ..... MADD 490
C ..... MADD 500
C ..... MADD 510
C ..... MADD 520
C ..... MADD 530
C ..... MADD 540
C ..... MADD 550
C ..... MADD 560
C ..... MADD 570
C ..... MADD 580
C ..... MADD 590
C ..... MADD 600
C ..... MADD 610
C ..... MADD 620
C ..... MADD 630
C ..... MADD 640
C ..... MADD 650
C ..... MADD 660
C ..... MADD 670
C ..... MADD 680
C ..... MADD 690
C ..... MADD 700
C ..... MADD 710
C ..... MADD 720
C ..... MADD 730
C ..... MADD 740
C ..... MADD 750
C ..... MADD 760
C ..... MADD 770
C ..... MADD 780
C ..... MADD 790
C ..... MADD 800
C ..... MADD 810
C ..... MADD 820
C ..... MADD 830
C ..... MADD 840
C ..... MADD 850
C ..... MADD 860
C ..... MADD 870
C ..... MADD 880
C ..... MADD 890
C ..... MADD 900
C ..... MADD 910
C ..... MADD 920
C ..... MADD 930
C ..... MADD 940
C ..... MADD 950
C ..... MADD 960
C ..... MADD 970
C ..... MADD 980
C ..... MADD 990
C ..... MADD 1000

```

Subroutine MSUB

```

C ..... MSUB 10
C ..... MSUB 20
C ..... MSUB 30
C ..... MSUB 40
C ..... MSUB 50
C ..... MSUB 60
C ..... MSUB 70
C ..... MSUB 80
C ..... MSUB 90
C ..... MSUB 100
C ..... MSUB 110
C ..... MSUB 120
C ..... MSUB 130
C ..... MSUB 140
C ..... MSUB 150
C ..... MSUB 160
C ..... MSUB 170
C ..... MSUB 180
C ..... MSUB 190
C ..... MSUB 200
C ..... MSUB 210
C ..... MSUB 220
C ..... MSUB 230
C ..... MSUB 240
C ..... MSUB 250
C ..... MSUB 260
C ..... MSUB 270
C ..... MSUB 280
C ..... MSUB 290
C ..... MSUB 300
C ..... MSUB 310
C ..... MSUB 320
C ..... MSUB 330
C ..... MSUB 340
C ..... MSUB 350
C ..... MSUB 360
C ..... MSUB 370
C ..... MSUB 380
C ..... MSUB 390
C ..... MSUB 400
C ..... MSUB 410
C ..... MSUB 420
C ..... MSUB 430
C ..... MSUB 440
C ..... MSUB 450
C ..... MSUB 460
C ..... MSUB 470
C ..... MSUB 480
C ..... MSUB 490
C ..... MSUB 500
C ..... MSUB 510
C ..... MSUB 520
C ..... MSUB 530
C ..... MSUB 540
C ..... MSUB 550
C ..... MSUB 560
C ..... MSUB 570
C ..... MSUB 580
C ..... MSUB 590
C ..... MSUB 600
C ..... MSUB 610
C ..... MSUB 620
C ..... MSUB 630
C ..... MSUB 640
C ..... MSUB 650
C ..... MSUB 660
C ..... MSUB 670
C ..... MSUB 680
C ..... MSUB 690
C ..... MSUB 700
C ..... MSUB 710
C ..... MSUB 720
C ..... MSUB 730
C ..... MSUB 740
C ..... MSUB 750
C ..... MSUB 760
C ..... MSUB 770
C ..... MSUB 780
C ..... MSUB 790
C ..... MSUB 800
C ..... MSUB 810
C ..... MSUB 820
C ..... MSUB 830
C ..... MSUB 840
C ..... MSUB 850
C ..... MSUB 860
C ..... MSUB 870
C ..... MSUB 880
C ..... MSUB 890
C ..... MSUB 900
C ..... MSUB 910
C ..... MSUB 920
C ..... MSUB 930
C ..... MSUB 940
C ..... MSUB 950
C ..... MSUB 960
C ..... MSUB 970
C ..... MSUB 980
C ..... MSUB 990
C ..... MSUB 1000

```

Subroutine MPRD

```

C ..... MPRD 10
C ..... MPRD 20
C ..... MPRD 30
C ..... MPRD 40
C ..... MPRD 50
C ..... MPRD 60
C ..... MPRD 70
C ..... MPRD 80
C ..... MPRD 90
C ..... MPRD 100
C ..... MPRD 110
C ..... MPRD 120
C ..... MPRD 130
C ..... MPRD 140
C ..... MPRD 150
C ..... MPRD 160
C ..... MPRD 170
C ..... MPRD 180
C ..... MPRD 190
C ..... MPRD 200
C ..... MPRD 210
C ..... MPRD 220
C ..... MPRD 230
C ..... MPRD 240
C ..... MPRD 250
C ..... MPRD 260
C ..... MPRD 270
C ..... MPRD 280
C ..... MPRD 290
C ..... MPRD 300
C ..... MPRD 310
C ..... MPRD 320
C ..... MPRD 330
C ..... MPRD 340
C ..... MPRD 350
C ..... MPRD 360
C ..... MPRD 370
C ..... MPRD 380
C ..... MPRD 390
C ..... MPRD 400
C ..... MPRD 410
C ..... MPRD 420
C ..... MPRD 430
C ..... MPRD 440
C ..... MPRD 450
C ..... MPRD 460
C ..... MPRD 470
C ..... MPRD 480
C ..... MPRD 490
C ..... MPRD 500
C ..... MPRD 510
C ..... MPRD 520
C ..... MPRD 530
C ..... MPRD 540
C ..... MPRD 550
C ..... MPRD 560
C ..... MPRD 570
C ..... MPRD 580
C ..... MPRD 590
C ..... MPRD 600
C ..... MPRD 610
C ..... MPRD 620
C ..... MPRD 630
C ..... MPRD 640
C ..... MPRD 650
C ..... MPRD 660
C ..... MPRD 670
C ..... MPRD 680
C ..... MPRD 690
C ..... MPRD 700
C ..... MPRD 710
C ..... MPRD 720
C ..... MPRD 730
C ..... MPRD 740
C ..... MPRD 750
C ..... MPRD 760
C ..... MPRD 770
C ..... MPRD 780
C ..... MPRD 790
C ..... MPRD 800
C ..... MPRD 810

SUBROUTINE MPRD
PURPOSE
MULTIPLY TWO MATRICES TO FORM A RESULTANT MATRIX

USAGE
CALL MPRD(A,B,R,N,M,MSA,MSB,L)

DESCRIPTION OF PARAMETERS
A - NAME OF FIRST INPUT MATRIX
B - NAME OF SECOND INPUT MATRIX
R - NAME OF OUTPUT MATRIX
N - NUMBER OF ROWS IN A AND R
M - NUMBER OF COLUMNS IN A AND ROWS IN B
MSA - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
      0 - GENERAL
      1 - SYMMETRIC
      2 - DIAGONAL
MSB - SAME AS MSA EXCEPT FOR MATRIX B
L - NUMBER OF COLUMNS IN B AND R

REMARKS
MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRICES A OR B
NUMBER OF COLUMNS OF MATRIX A MUST BE EQUAL TO NUMBER OF ROWS
OF MATRIX B

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
LOC

METHOD
THE M BY L MATRIX B IS PREMULTIPLIED BY THE N BY M MATRIX A
AND THE RESULT IS STORED IN THE N BY L MATRIX R. THIS IS A
ROW INTO COLUMN PRODUCT.
THE FOLLOWING TABLE SHOWS THE STORAGE MODE OF THE OUTPUT
MATRIX FOR ALL COMBINATIONS OF INPUT MATRICES
      A           B           R
      GENERAL     GENERAL     GENERAL
      GENERAL     SYMMETRIC    GENERAL
      GENERAL     DIAGONAL     GENERAL
      SYMMETRIC   GENERAL      GENERAL
      SYMMETRIC   SYMMETRIC    GENERAL
      SYMMETRIC   DIAGONAL     GENERAL
      DIAGONAL    GENERAL      GENERAL
      DIAGONAL    SYMMETRIC    GENERAL
      DIAGONAL    DIAGONAL     DIAGONAL
.....
SUBROUTINE MPRD(A,B,R,N,M,MSA,MSB,L)
DIMENSION A(1),B(1),R(1)

SPECIAL CASE FOR DIAGONAL BY DIAGONAL
MS=MSA*10+MSB
IF(MS-22) 30,10,30
10 DO 20 I=1,N
20 R(I)=A(I)*B(I)
RETURN

ALL OTHER CASES
30 IR=1
DO 90 K=1,L
DO 90 J=1,N
R(IR)=0
DO 80 I=1,M
IF(MS) 40,60,40
40 CALL LOC(J,I,A,N,M,MSA)
CALL LOC(I,K,B,M,L,MSB)
IF(IA) 50,80,50
50 IF(IB) 70,80,70
60 IA=M-(I-1)+J
IB=M-(I-1)+I
70 R(IR)=R(IR)+A(IA)*B(IB)
80 CONTINUE
90 IR=IR+1
RETURN
END

```

Subroutine MTRA

```

C ..... MTRA 10
C ..... MTRA 20
C ..... MTRA 30
C ..... MTRA 40
C ..... MTRA 50
C ..... MTRA 60
C ..... MTRA 70
C ..... MTRA 80
C ..... MTRA 90
C ..... MTRA 100
C ..... MTRA 110
C ..... MTRA 120
C ..... MTRA 130
C ..... MTRA 140
C ..... MTRA 150
C ..... MTRA 160
C ..... MTRA 170
C ..... MTRA 180
C ..... MTRA 190
C ..... MTRA 200
C ..... MTRA 210
C ..... MTRA 220
C ..... MTRA 230
C ..... MTRA 240
C ..... MTRA 250
C ..... MTRA 260
C ..... MTRA 270
C ..... MTRA 280
C ..... MTRA 290
C ..... MTRA 300
C ..... MTRA 310
C ..... MTRA 320
C ..... MTRA 330
C ..... MTRA 340
C ..... MTRA 350
C ..... MTRA 360
C ..... MTRA 370
C ..... MTRA 380
C ..... MTRA 390
C ..... MTRA 400
C ..... MTRA 410
C ..... MTRA 420
C ..... MTRA 430
C ..... MTRA 440
C ..... MTRA 450
C ..... MTRA 460
C ..... MTRA 470
C ..... MTRA 480
C ..... MTRA 490
C ..... MTRA 500
C ..... MTRA 510
C ..... MTRA 520
C ..... MTRA 530
C ..... MTRA 540

SUBROUTINE MTRA
PURPOSE
TRANSPOSE A MATRIX

USAGE
CALL MTRA(A,R,N,M,MS)

DESCRIPTION OF PARAMETERS
A - NAME OF MATRIX TO BE TRANSPOSED
R - NAME OF OUTPUT MATRIX
N - NUMBER OF ROWS OF A AND COLUMNS OF R
M - NUMBER OF COLUMNS OF A AND ROWS OF R
MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A (AND R)
      0 - GENERAL
      1 - SYMMETRIC
      2 - DIAGONAL

REMARKS
MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRIX A

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
MCPY

METHOD
TRANSPOSE N BY M MATRIX A TO FORM M BY N MATRIX R BY MOVING
EACH ROW OF A INTO THE CORRESPONDING COLUMN OF R. IF MATRIX
A IS SYMMETRIC OR DIAGONAL, MATRIX R IS THE SAME AS A.
.....
SUBROUTINE MTRA(A,R,N,M,MS)
DIMENSION A(1),R(1)

IF(MS) 10,20,10
IF(MS) 10,20,10
10 CALL MCPY(A,R,N,N,MS)
RETURN

TRANSPOSE GENERAL MATRIX
20 IR=0
DO 30 I=1,N
IJ=I-N
DO 30 J=1,M
IJ=IJ+N
IR=IR+1
30 R(IR)=A(IJ)
RETURN
END

```

Subroutine TPRD

```

C .....
C TPRD 10
C TPRD 20
C TPRD 30
C SUBROUTINE TPRD TPRD 40
C TPRD 50
C PURPOSE TPRD 60
C TRANSPOSE A MATRIX AND POSTMULTIPLY BY ANOTHER TO FORM TPRD 70
C A RESULTANT MATRIX TPRD 80
C TPRD 90
C USAGE TPRD 100
C CALL TPRD(A,B,R,N,M,MSA,MSB,L) TPRD 110
C TPRD 120
C DESCRIPTION OF PARAMETERS TPRD 130
C A - NAME OF FIRST INPUT MATRIX TPRD 140
C B - NAME OF SECOND INPUT MATRIX TPRD 150
C R - NAME OF OUTPUT MATRIX TPRD 160
C N - NUMBER OF ROWS IN A AND B TPRD 170
C M - NUMBER OF COLUMNS IN A AND ROWS IN R TPRD 180
C MSA - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A TPRD 190
C 0 - GENERAL TPRD 200
C 1 - SYMMETRIC TPRD 210
C 2 - DIAGONAL TPRD 220
C MSB - SAME AS MSA EXCEPT FOR MATRIX B TPRD 230
C L - NUMBER OF COLUMNS IN B AND R TPRD 240
C TPRD 250
C REMARKS TPRD 260
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRICES A OR B TPRD 270
C TPRD 280
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED TPRD 290
C LOC TPRD 300
C TPRD 310
C METHOD TPRD 320
C MATRIX TRANSPOSE OF A IS NOT ACTUALLY CALCULATED. INSTEAD, TPRD 330
C ELEMENTS IN MATRIX A ARE TAKEN COLUMNWISE RATHER THAN TPRD 340
C ROWWISE FOR MULTIPLICATION BY MATRIX B. TPRD 350
C THE FOLLOWING TABLE SHOWS THE STORAGE MODE OF THE OUTPUT TPRD 360
C MATRIX FOR ALL COMBINATIONS OF INPUT MATRICES TPRD 370
C
C A B R TPRD 380
C GENERAL GENERAL GENERAL TPRD 390
C GENERAL SYMMETRIC GENERAL TPRD 400
C GENERAL DIAGONAL GENERAL TPRD 410
C SYMMETRIC GENERAL GENERAL TPRD 420
C SYMMETRIC SYMMETRIC GENERAL TPRD 430
C DIAGONAL DIAGONAL GENERAL TPRD 440
C DIAGONAL GENERAL GENERAL TPRD 450
C DIAGONAL SYMMETRIC GENERAL TPRD 460
C DIAGONAL DIAGONAL DIAGONAL TPRD 470
C TPRD 480
C .....
C SUBROUTINE TPRD(A,B,R,N,M,MSA,MSB,L) TPRD 510
C DIMENSION A(1),B(1),R(1) TPRD 520
C
C SPECIAL CASE FOR DIAGONAL BY DIAGONAL TPRD 530
C TPRD 540
C MS=MSA*10+MSB TPRD 550
C IF(MS-22) 30,10,30 TPRD 560
C 10 DO 20 I=1,M TPRD 570
C 20 R(I)=A(I)*B(I) TPRD 580
C RETURN TPRD 590
C TPRD 600
C MULTIPLY TRANSPOSE OF A BY B TPRD 610
C TPRD 620
C TPRD 630
C 30 IR=1 TPRD 640
C DO 90 K=1,L TPRD 650
C DO 90 J=1,M TPRD 660
C R(IR)=0.0 TPRD 670
C DO 80 I=1,N TPRD 680
C IF(MS) 40,60,40 TPRD 690
C 40 CALL LOC(I,J,IA,N,M,MSA) TPRD 700
C CALL LOC(I,K,IB,N,L,MSB) TPRD 710
C IF(IA) 50,80,50 TPRD 720
C 50 IF(IB) 70,80,70 TPRD 730
C 60 IA=N*(J-1)+I TPRD 740
C IB=N*(K-1)+I TPRD 750
C 70 R(IR)=R(IR)+A(IA)*B(IB) TPRD 760
C 80 CONTINUE TPRD 770
C 90 IR=IR+1 TPRD 780
C RETURN TPRD 790
C END TPRD 800

```

Subroutine MATA

```

C .....
C MATA 10
C MATA 20
C MATA 30
C SUBROUTINE MATA MATA 40
C MATA 50
C PURPOSE MATA 60
C PREMULTIPLY A MATRIX BY ITS TRANSPOSE TO FORM A MATA 70
C SYMMETRIC MATRIX MATA 80
C MATA 90
C USAGE MATA 100
C CALL MATA(A,R,N,M,MS) MATA 110
C MATA 120
C DESCRIPTION OF PARAMETERS MATA 130
C A - NAME OF INPUT MATRIX MATA 140
C R - NAME OF OUTPUT MATRIX MATA 150
C N - NUMBER OF ROWS IN A MATA 160
C M - NUMBER OF COLUMNS IN A. ALSO NUMBER OF ROWS AND MATA 170
C NUMBER OF COLUMNS OF R. MATA 180
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A MATA 190
C 0 - GENERAL MATA 200
C 1 - SYMMETRIC MATA 210
C 2 - DIAGONAL MATA 220
C MATA 230
C REMARKS MATA 240
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRIX A MATA 250
C MATRIX R IS ALWAYS A SYMMETRIC MATRIX WITH A STORAGE MODE=1 MATA 260
C MATA 270
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED MATA 280
C LOC MATA 290
C MATA 300
C METHOD MATA 310
C CALCULATION OF (A TRANSPOSE A) RESULTS IN A SYMMETRIC MATRIX MATA 320
C REGARDLESS OF THE STORAGE MODE OF THE INPUT MATRIX. THE MATA 330
C ELEMENTS OF MATRIX A ARE NOT CHANGED. MATA 340
C MATA 350
C .....
C SUBROUTINE MATA(A,R,N,M,MS) MATA 360
C DIMENSION A(1),R(1) MATA 370
C MATA 380
C DO 60 K=1,M MATA 390
C KX=(K*K-1)/2 MATA 400
C DO 60 J=1,M MATA 410
C IF(J-K) 10,10,60 MATA 420
C 10 IR=J+KX MATA 430
C R(IR)=0 MATA 440
C DO 60 I=1,N MATA 450
C IF(MS) 20,40,20 MATA 460
C 20 CALL LOC(I,J,IA,N,M,MS) MATA 470
C CALL LOC(I,K,IB,N,M,MS) MATA 480
C IF(IA) 30,60,30 MATA 490
C 30 IF(IB) 50,60,50 MATA 500
C 40 IA=N*(J-1)+I MATA 510
C IB=N*(K-1)+I MATA 520
C 50 R(IR)=R(IR)+A(IA)*A(IB) MATA 530
C 60 CONTINUE MATA 540
C RETURN MATA 550
C END MATA 560
C MATA 570
C MATA 580

```

Subroutine SADD

```

C ..... SADD 10
C ..... SADD 20
C ..... SADD 30
C SUBROUTINE SADD SADD 40
C ..... SADD 50
C PURPOSE SADD 60
C ADD A SCALAR TO EACH ELEMENT OF A MATRIX TO FORM A RESULTANT SADD 70
C MATRIX SADD 80
C ..... SADD 90
C USAGE SADD 100
C CALL SADD(A,C,R,N,M,MS) SADD 110
C ..... SADD 120
C DESCRIPTION OF PARAMETERS SADD 130
C A - NAME OF INPUT MATRIX SADD 140
C C - SCALAR SADD 150
C R - NAME OF OUTPUT MATRIX SADD 160
C N - NUMBER OF ROWS IN MATRIX A AND R SADD 170
C M - NUMBER OF COLUMNS IN MATRIX A AND R SADD 180
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A (AND R) SADD 190
C 0 - GENERAL SADD 200
C 1 - SYMMETRIC SADD 210
C 2 - DIAGONAL SADD 220
C ..... SADD 230
C REMARKS SADD 240
C NONE SADD 250
C ..... SADD 260
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SADD 270
C LOC SADD 280
C ..... SADD 290
C METHOD SADD 300
C SCALAR IS ADDED TO EACH ELEMENT OF MATRIX SADD 310
C ..... SADD 320
C ..... SADD 330
C ..... SADD 340
C SUBROUTINE SADD(A,C,R,N,M,MS) SADD 350
C DIMENSION A(1),R(1) SADD 360
C ..... SADD 370
C COMPUTE VECTOR LENGTH, IT SADD 380
C ..... SADD 390
C CALL LOC(N,M,IT,N,M,MS) SADD 400
C ..... SADD 410
C ADD SCALAR SADD 420
C ..... SADD 430
C DO 1 I=1,IT SADD 440
1 R(I)=A(I)+C SADD 450
RETURN SADD 460
END SADD 470

```

Subroutine SSUB

```

C ..... SSUB 10
C ..... SSUB 20
C ..... SSUB 30
C SUBROUTINE SSUB SSUB 40
C ..... SSUB 50
C PURPOSE SSUB 60
C SUBTRACT A SCALAR FROM EACH ELEMENT OF A MATRIX TO FORM A SSUB 70
C RESULTANT MATRIX SSUB 80
C ..... SSUB 90
C USAGE SSUB 100
C CALL SSUB(A,C,R,N,M,MS) SSUB 110
C ..... SSUB 120
C DESCRIPTION OF PARAMETERS SSUB 130
C A - NAME OF INPUT MATRIX SSUB 140
C C - SCALAR SSUB 150
C R - NAME OF OUTPUT MATRIX SSUB 160
C N - NUMBER OF ROWS IN MATRIX A AND R SSUB 170
C M - NUMBER OF COLUMNS IN MATRIX A AND R SSUB 180
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A (AND R) SSUB 190
C 0 - GENERAL SSUB 200
C 1 - SYMMETRIC SSUB 210
C 2 - DIAGONAL SSUB 220
C ..... SSUB 230
C REMARKS SSUB 240
C NONE SSUB 250
C ..... SSUB 260
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SSUB 270
C LOC SSUB 280
C ..... SSUB 290
C METHOD SSUB 300
C SCALAR IS SUBTRACTED FROM EACH EACH ELEMENT OF MATRIX SSUB 310
C ..... SSUB 320
C ..... SSUB 330
C ..... SSUB 340
C SUBROUTINE SSUB(A,C,R,N,M,MS) SSUB 350
C DIMENSION A(1),R(1) SSUB 360
C ..... SSUB 370
C COMPUTE VECTOR LENGTH, IT SSUB 380
C ..... SSUB 390
C CALL LOC(N,M,IT,N,M,MS) SSUB 400
C ..... SSUB 410
C SUBTRACT SCALAR SSUB 420
C ..... SSUB 430
C DO 1 I=1,IT SSUB 440
1 R(I)=A(I)-C SSUB 450
RETURN SSUB 460
END SSUB 470

```

Subroutine SMPY

```

C ..... SMPY 10
C ..... SMPY 20
C ..... SMPY 30
C SUBROUTINE SMPY SMPY 40
C ..... SMPY 50
C ..... SMPY 60
C PURPOSE SMPY 70
C MULTIPLY EACH ELEMENT OF A MATRIX BY A SCALAR TO FORM A
C RESULTANT MATRIX SMPY 80
C ..... SMPY 90
C USAGE SMPY 100
C CALL SMPY(A,C,R,N,M,MS) SMPY 110
C ..... SMPY 120
C DESCRIPTION OF PARAMETERS SMPY 130
C A - NAME OF INPUT MATRIX SMPY 140
C C - SCALAR SMPY 150
C R - NAME OF OUTPUT MATRIX SMPY 160
C N - NUMBER OF ROWS IN MATRIX A AND R SMPY 170
C M - NUMBER OF COLUMNS IN MATRIX A AND R SMPY 180
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A (AND R) SMPY 190
C 0 - GENERAL SMPY 200
C 1 - SYMMETRIC SMPY 210
C 2 - DIAGONAL SMPY 220
C ..... SMPY 230
C REMARKS SMPY 240
C NONE SMPY 250
C ..... SMPY 260
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SMPY 270
C LOC SMPY 280
C ..... SMPY 290
C METHOD SMPY 300
C SCALAR IS MULTIPLIED BY EACH ELEMENT OF MATRIX SMPY 310
C ..... SMPY 320
C ..... SMPY 330
C ..... SMPY 340
C SUBROUTINE SMPY(A,C,R,N,M,MS) SMPY 350
C DIMENSION A(1),R(1) SMPY 360
C ..... SMPY 370
C COMPUTE VECTOR LENGTH, IT SMPY 380
C ..... SMPY 390
C CALL LOC(N,M,IT,N,M,MS) SMPY 400
C ..... SMPY 410
C MULTIPLY BY SCALAR SMPY 420
C ..... SMPY 430
C ..... SMPY 440
C ..... SMPY 450
C ..... SMPY 460
C ..... SMPY 470
C ..... SMPY 480
C ..... SMPY 490
C ..... SMPY 500
C ..... SMPY 510
C ..... SMPY 520
C ..... SMPY 530
C ..... SMPY 540
C ..... SMPY 550
C ..... SMPY 560
C ..... SMPY 570
C ..... SMPY 580
C ..... SMPY 590
C ..... SMPY 600
C ..... SMPY 610
C ..... SMPY 620
C ..... SMPY 630
C ..... SMPY 640
C ..... SMPY 650
C ..... SMPY 660
C ..... SMPY 670
C ..... SMPY 680
C ..... SMPY 690
C ..... SMPY 700
C ..... SMPY 710
C ..... SMPY 720
C ..... SMPY 730
C ..... SMPY 740
C ..... SMPY 750
C ..... SMPY 760
C ..... SMPY 770
C ..... SMPY 780
C ..... SMPY 790
C ..... SMPY 800
C ..... SMPY 810
C ..... SMPY 820
C ..... SMPY 830
C ..... SMPY 840
C ..... SMPY 850
C ..... SMPY 860
C ..... SMPY 870
C ..... SMPY 880
C ..... SMPY 890
C ..... SMPY 900
C ..... SMPY 910
C ..... SMPY 920
C ..... SMPY 930
C ..... SMPY 940
C ..... SMPY 950
C ..... SMPY 960
C ..... SMPY 970
C ..... SMPY 980
C ..... SMPY 990
C ..... SMPY 1000

```

Subroutine SDIV

```

C ..... SDIV 10
C ..... SDIV 20
C ..... SDIV 30
C SUBROUTINE SDIV SDIV 40
C ..... SDIV 50
C ..... SDIV 60
C PURPOSE SDIV 70
C DIVIDE EACH ELEMENT OF A MATRIX BY A SCALAR TO FORM A
C RESULTANT MATRIX SDIV 80
C ..... SDIV 90
C USAGE SDIV 100
C CALL SDIV(A,C,R,N,M,MS) SDIV 110
C ..... SDIV 120
C DESCRIPTION OF PARAMETERS SDIV 130
C A - NAME OF INPUT MATRIX SDIV 140
C C - SCALAR SDIV 150
C R - NAME OF OUTPUT MATRIX SDIV 160
C N - NUMBER OF ROWS IN MATRIX A AND R SDIV 170
C M - NUMBER OF COLUMNS IN MATRIX A AND R SDIV 180
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A (AND R) SDIV 190
C 0 - GENERAL SDIV 200
C 1 - SYMMETRIC SDIV 210
C 2 - DIAGONAL SDIV 220
C ..... SDIV 230
C REMARKS SDIV 240
C IF SCALAR IS ZERO, DIVISION IS PERFORMED ONLY ONCE TO CAUSE
C FLOATING POINT OVERFLOW CONDITION SDIV 250
C ..... SDIV 260
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SDIV 270
C LOC SDIV 280
C ..... SDIV 290
C METHOD SDIV 300
C EACH ELEMENT OF MATRIX IS DIVIDED BY SCALAR SDIV 310
C ..... SDIV 320
C ..... SDIV 330
C ..... SDIV 340
C SUBROUTINE SDIV(A,C,R,N,M,MS) SDIV 350
C DIMENSION A(1),R(1) SDIV 360
C ..... SDIV 370
C COMPUTE VECTOR LENGTH, IT SDIV 380
C ..... SDIV 390
C CALL LOC(N,M,IT,N,M,MS) SDIV 400
C ..... SDIV 410
C DIVIDE BY SCALAR (IF SCALAR IS ZERO, DIVIDE ONLY ONCE) SDIV 420
C ..... SDIV 430
C ..... SDIV 440
C ..... SDIV 450
C ..... SDIV 460
C ..... SDIV 470
C ..... SDIV 480
C ..... SDIV 490
C ..... SDIV 500
C ..... SDIV 510
C ..... SDIV 520
C ..... SDIV 530
C ..... SDIV 540
C ..... SDIV 550
C ..... SDIV 560
C ..... SDIV 570
C ..... SDIV 580
C ..... SDIV 590
C ..... SDIV 600
C ..... SDIV 610
C ..... SDIV 620
C ..... SDIV 630
C ..... SDIV 640
C ..... SDIV 650
C ..... SDIV 660
C ..... SDIV 670
C ..... SDIV 680
C ..... SDIV 690
C ..... SDIV 700
C ..... SDIV 710
C ..... SDIV 720
C ..... SDIV 730
C ..... SDIV 740
C ..... SDIV 750
C ..... SDIV 760
C ..... SDIV 770
C ..... SDIV 780
C ..... SDIV 790
C ..... SDIV 800
C ..... SDIV 810
C ..... SDIV 820
C ..... SDIV 830
C ..... SDIV 840
C ..... SDIV 850
C ..... SDIV 860
C ..... SDIV 870
C ..... SDIV 880
C ..... SDIV 890
C ..... SDIV 900
C ..... SDIV 910
C ..... SDIV 920
C ..... SDIV 930
C ..... SDIV 940
C ..... SDIV 950
C ..... SDIV 960
C ..... SDIV 970
C ..... SDIV 980
C ..... SDIV 990
C ..... SDIV 1000

```

Subroutine SCLA

```

C ..... SCLA 10
C ..... SCLA 20
C ..... SCLA 30
C SUBROUTINE SCLA SCLA 40
C ..... SCLA 50
C PURPOSE SCLA 60
C SET EACH ELEMENT OF A MATRIX EQUAL TO A GIVEN SCALAR SCLA 70
C ..... SCLA 80
C USAGE SCLA 90
C CALL SCLA (A,C,N,M,MS) SCLA 100
C ..... SCLA 110
C DESCRIPTION OF PARAMETERS SCLA 120
C A - NAME OF INPUT MATRIX SCLA 130
C C - SCALAR SCLA 140
C N - NUMBER OF ROWS IN MATRIX A SCLA 150
C M - NUMBER OF COLUMNS IN MATRIX A SCLA 160
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A SCLA 170
C 0 - GENERAL SCLA 180
C 1 - SYMMETRIC SCLA 190
C 2 - DIAGONAL SCLA 200
C ..... SCLA 210
C REMARKS SCLA 220
C NONE SCLA 230
C ..... SCLA 240
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SCLA 250
C LUC SCLA 260
C ..... SCLA 270
C METHOD SCLA 280
C EACH ELEMENT OF MATRIX A IS REPLACED BY SCALAR C SCLA 290
C ..... SCLA 300
C ..... SCLA 310
C SUBROUTINE SCLA(A,C,N,M,MS) SCLA 320
C DIMENSION A(1) SCLA 330
C ..... SCLA 340
C COMPUTE VECTOR LENGTH, IT SCLA 350
C ..... SCLA 360
C CALL LUC(N,M,IT,N,M,MS) SCLA 370
C ..... SCLA 380
C REPLACE BY SCALAR SCLA 390
C ..... SCLA 400
C DO 1 I=1,IT SCLA 410
C 1 A(I)=C SCLA 420
C RETURN SCLA 430
C END SCLA 440
C ..... SCLA 450

```

Subroutine DCLA

```

C ..... DCLA 10
C ..... DCLA 20
C ..... DCLA 30
C SUBROUTINE DCLA DCLA 40
C ..... DCLA 50
C PURPOSE DCLA 60
C SET EACH DIAGONAL ELEMENT OF A MATRIX EQUAL TO A SCALAR DCLA 70
C ..... DCLA 80
C USAGE DCLA 90
C CALL DCLA (A,C,N,MS) DCLA 100
C ..... DCLA 110
C DESCRIPTION OF PARAMETERS DCLA 120
C A - NAME OF INPUT MATRIX DCLA 130
C C - SCALAR DCLA 140
C N - NUMBER OF ROWS AND COLUMNS IN MATRIX A DCLA 150
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A DCLA 160
C 0 - GENERAL DCLA 170
C 1 - SYMMETRIC DCLA 180
C 2 - DIAGONAL DCLA 190
C ..... DCLA 200
C REMARKS DCLA 210
C INPUT MATRIX MUST BE A SQUARE MATRIX DCLA 220
C ..... DCLA 230
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DCLA 240
C LUC DCLA 250
C ..... DCLA 260
C METHOD DCLA 270
C EACH ELEMENT ON DIAGONAL OF MATRIX IS REPLACED BY SCALAR C DCLA 280
C ..... DCLA 290
C ..... DCLA 300
C ..... DCLA 310
C SUBROUTINE DCLA(A,C,N,MS) DCLA 320
C DIMENSION A(1) DCLA 330
C ..... DCLA 340
C DO 3 I=1,N DCLA 350
C ..... DCLA 360
C LOCATE DIAGONAL ELEMENT FOR ANY MATRIX STORAGE MODE DCLA 370
C ..... DCLA 380
C CALL LUC(I,I,10,N,N,MS) DCLA 390
C ..... DCLA 400
C REPLACE DIAGONAL ELEMENTS DCLA 410
C ..... DCLA 420
C 3 A(I)=C DCLA 430
C RETURN DCLA 440
C END DCLA 450

```

Subroutine RADD

```

C
C .....
C
C SUBROUTINE RADD
C
C PURPOSE
C ADD ROW OF ONE MATRIX TO ROW OF ANOTHER MATRIX
C
C USAGE
C CALL RADD(A,IRA,R,IRR,N,M,MS,L)
C
C DESCRIPTION OF PARAMETERS
C A - NAME OF INPUT MATRIX
C IRA - ROW IN MATRIX A TO BE ADDED TO ROW IRR OF MATRIX R
C R - NAME OF OUTPUT MATRIX
C IRR - ROW IN MATRIX R WHERE SUMMATION IS DEVELOPED
C N - NUMBER OF ROWS IN A
C M - NUMBER OF COLUMNS IN A AND R
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C L - NUMBER OF ROWS IN R
C
C REMARKS
C MATRIX R MUST BE A GENERAL MATRIX
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRIX A UNLESS
C A IS GENERAL
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C
C METHOD
C EACH ELEMENT OF ROW IRA OF MATRIX A IS ADDED TO
C CORRESPONDING ELEMENT OF ROW IRR OF MATRIX R
C .....
C SUBROUTINE RADD(A,IRA,R,IRR,N,M,MS,L)
C DIMENSION A(1),R(1)
C
C IR=IRR-L
C DO 2 J=1,M
C IR=IR+L
C
C LOCATE INPUT ELEMENT FOR ANY MATRIX STORAGE MODE
C
C CALL LOC(IRA,J,IA,N,M,MS)
C
C TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
C
C IF(IA) 1,2,1
C
C ADD ELEMENTS
C
C 1 R(IR)=R(IR)+A(IA)
C 2 CONTINUE
C RETURN
C END
RADD 10
RADD 20
RADD 30
RADD 40
RADD 50
RADD 60
RADD 70
RADD 80
RADD 90
RADD 100
RADD 110
RADD 120
RADD 130
RADD 140
RADD 150
RADD 160
RADD 170
RADD 180
RADD 190
RADD 200
RADD 210
RADD 220
RADD 230
RADD 240
RADD 250
RADD 260
RADD 270
RADD 280
RADD 290
RADD 300
RADD 310
RADD 320
RADD 330
RADD 340
RADD 350
RADD 360
RADD 370
RADD 380
RADD 390
RADD 400
RADD 410
RADD 420
RADD 430
RADD 440
RADD 450
RADD 460
RADD 470
RADD 480
RADD 490
RADD 500
RADD 510
RADD 520
RADD 530
RADD 540
RADD 550
RADD 560
RADD 570
RADD 580
RADD 590

```

Subroutine CADD

```

C .....
C
C SUBROUTINE CADD
C
C PURPOSE
C ADD COLUMN OF ONE MATRIX TO COLUMN OF ANOTHER MATRIX
C
C USAGE
C CALL CADD(A,ICA,R,ICR,N,M,MS,L)
C
C DESCRIPTION OF PARAMETERS
C A - NAME OF INPUT MATRIX
C ICA - COLUMN IN MATRIX A TO BE ADDED TO COLUMN ICR OF R
C R - NAME OF OUTPUT MATRIX
C ICR - COLUMN IN MATRIX R WHERE SUMMATION IS DEVELOPED
C N - NUMBER OF ROWS IN A AND R
C M - NUMBER OF COLUMNS IN A
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C L - NUMBER OF COLUMNS IN R
C
C REMARKS
C MATRIX R MUST BE A GENERAL MATRIX
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRIX A UNLESS
C A IS GENERAL
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C
C METHOD
C EACH ELEMENT OF COLUMN ICA OF MATRIX A IS ADDED TO
C CORRESPONDING ELEMENT OF COLUMN ICR OF MATRIX R
C .....
C SUBROUTINE CADD(A,ICA,R,ICR,N,M,MS,L)
C DIMENSION A(1),R(1)
C
C IR=N*(ICR-1)
C DO 2 I=1,N
C IR=IR+1
C
C LOCATE INPUT ELEMENT FOR ANY MATRIX STORAGE MODE
C
C CALL LOC(ICA,I,IA,N,M,MS)
C
C TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
C
C IF(IA) 1,2,1
C
C ADD ELEMENTS
C
C 1 R(IR)=R(IR)+A(IA)
C 2 CONTINUE
C RETURN
C END
CADD 10
CADD 20
CADD 30
CADD 40
CADD 50
CADD 60
CADD 70
CADD 80
CADD 90
CADD 100
CADD 110
CADD 120
CADD 130
CADD 140
CADD 150
CADD 160
CADD 170
CADD 180
CADD 190
CADD 200
CADD 210
CADD 220
CADD 230
CADD 240
CADD 250
CADD 260
CADD 270
CADD 280
CADD 290
CADD 300
CADD 310
CADD 320
CADD 330
CADD 340
CADD 350
CADD 360
CADD 370
CADD 380
CADD 390
CADD 400
CADD 410
CADD 420
CADD 430
CADD 440
CADD 450
CADD 460
CADD 470
CADD 480
CADD 490
CADD 500
CADD 510
CADD 520
CADD 530
CADD 540
CADD 550
CADD 560
CADD 570
CADD 580
CADD 590

```

Subroutine SRMA

```

C ..... SRMA 10
C ..... SRMA 20
C SUBROUTINE SRMA SRMA 30
C ..... SRMA 40
C ..... SRMA 50
C PURPOSE SRMA 60
C MULTIPLY ROW OF MATRIX BY A SCALAR AND ADD TO ANOTHER ROW
C OF THE SAME MATRIX SRMA 70
C ..... SRMA 80
C ..... SRMA 90
C USAGE SRMA 100
C CALL SRMA(A,C,N,M,LA,LB) SRMA 110
C ..... SRMA 120
C DESCRIPTION OF PARAMETERS SRMA 130
C A - NAME OF MATRIX SRMA 140
C C - SCALAR SRMA 150
C N - NUMBER OF ROWS IN A SRMA 160
C M - NUMBER OF COLUMNS IN A SRMA 170
C LA - ROW IN A TO BE MULTIPLIED BY SCALAR SRMA 180
C LB - ROW IN A TO WHICH PRODUCT IS ADDED SRMA 190
C IF 0 IS SPECIFIED, PRODUCT REPLACES ELEMENTS IN ROW LA SRMA 200
C ..... SRMA 210
C REMARKS SRMA 220
C MATRIX A MUST BE A GENERAL MATRIX SRMA 230
C ..... SRMA 240
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SRMA 250
C NONE SRMA 260
C ..... SRMA 270
C METHOD SRMA 280
C EACH ELEMENT OF ROW LA IS MULTIPLIED BY SCALAR C AND THE SRMA 290
C PRODUCT IS ADDED TO THE CORRESPONDING ELEMENT OF ROW LB. SRMA 300
C ROW LA REMAINS UNAFFECTED BY THE OPERATION. SRMA 310
C IF PARAMETER LB CONTAINS ZERO, MULTIPLICATION BY THE SCALAR SRMA 320
C IS PERFORMED AND THE PRODUCT REPLACES ELEMENTS IN ROW LA. SRMA 330
C ..... SRMA 340
C ..... SRMA 350
C SUBROUTINE SRMA(A,C,N,M,LA,LB) SRMA 360
C DIMENSION A(I) SRMA 370
C ..... SRMA 380
C LAJ=LA-N SRMA 390
C LBJ=LB-N SRMA 400
C DO 3 J=1,M SRMA 410
C ..... SRMA 420
C LOCATE ELEMENT IN BOTH ROWS SRMA 430
C ..... SRMA 440
C LAJ=LAJ+N SRMA 450
C LBJ=LBJ+N SRMA 460
C ..... SRMA 470
C CHECK LB FOR ZERO SRMA 480
C ..... SRMA 490
C IF(LB) 1,2,1 SRMA 500
C ..... SRMA 510
C IF NOT, MULTIPLY BY CONSTANT AND ADD TO OTHER ROW SRMA 520
C ..... SRMA 530
C 1 A(LBJ)=A(LAJ)*C+A(LBJ) SRMA 540
C GO TO 3 SRMA 550
C ..... SRMA 560
C OTHERWISE, MULTIPLY ROW BY CONSTANT SRMA 570
C ..... SRMA 580
C 2 A(LAJ)=A(LAJ)*C SRMA 590
C 3 CONTINUE SRMA 600
C RETURN SRMA 610
C END SRMA 620
C ..... SRMA 630

```

Subroutine SCMA

```

C ..... SCMA 10
C ..... SCMA 20
C SUBROUTINE SCMA SCMA 30
C ..... SCMA 40
C ..... SCMA 50
C PURPOSE SCMA 60
C MULTIPLY COLUMN OF MATRIX BY A SCALAR AND ADD TO ANOTHER
C COLUMN OF THE SAME MATRIX SCMA 70
C ..... SCMA 80
C ..... SCMA 90
C USAGE SCMA 100
C CALL SCMA(A,C,N,LA,LB) SCMA 110
C ..... SCMA 120
C DESCRIPTION OF PARAMETERS SCMA 130
C A - NAME OF MATRIX SCMA 140
C C - SCALAR SCMA 150
C N - NUMBER OF ROWS IN A SCMA 160
C LA - COLUMN IN A TO BE MULTIPLIED BY SCALAR SCMA 170
C LB - COLUMN IN A TO WHICH PRODUCT IS ADDED SCMA 180
C IF 0 IS SPECIFIED, PRODUCT REPLACES ELEMENTS IN LA SCMA 190
C ..... SCMA 200
C REMARKS SCMA 210
C MATRIX A MUST BE A GENERAL MATRIX SCMA 220
C ..... SCMA 230
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SCMA 240
C NONE SCMA 250
C ..... SCMA 260
C METHOD SCMA 270
C EACH ELEMENT OF COLUMN LA IS MULTIPLIED BY SCALAR C AND THE SCMA 280
C PRODUCT IS ADDED TO THE CORRESPONDING ELEMENT OF COLUMN LB. SCMA 290
C COLUMN LA REMAINS UNAFFECTED BY THE OPERATION. SCMA 300
C IF PARAMETER LB CONTAINS ZERO, MULTIPLICATION BY THE SCALAR SCMA 310
C IS PERFORMED AND THE PRODUCT REPLACES ELEMENTS IN LA. SCMA 320
C ..... SCMA 330
C ..... SCMA 340
C SUBROUTINE SCMA(A,C,N,LA,LB) SCMA 350
C DIMENSION A(I) SCMA 360
C ..... SCMA 370
C LOCATE STARTING POINT OF BOTH COLUMNS SCMA 380
C ..... SCMA 390
C ILA=N*(LA-1) SCMA 400
C ILB=N*(LB-1) SCMA 410
C ..... SCMA 420
C DO 3 I=1,N SCMA 430
C ILA=ILA+1 SCMA 440
C ILB=ILB+1 SCMA 450
C ..... SCMA 460
C CHECK LB FOR ZERO SCMA 470
C ..... SCMA 480
C IF(LB) 1,2,1 SCMA 490
C ..... SCMA 500
C IF NOT MULTIPLY BY CONSTANT AND ADD TO SECOND COLUMN SCMA 510
C ..... SCMA 520
C 1 A(ILB)=A(ILA)*C+A(ILB) SCMA 530
C GO TO 3 SCMA 540
C ..... SCMA 550
C OTHERWISE, MULTIPLY COLUMN BY CONSTANT SCMA 560
C ..... SCMA 570
C 2 A(ILA)=A(ILA)*C SCMA 580
C 3 CONTINUE SCMA 590
C RETURN SCMA 600
C END SCMA 610
C ..... SCMA 620

```


Subroutine RINT

```

C ..... RINT 10
C ..... RINT 20
C ..... RINT 30
C SUBROUTINE RINT RINT 40
C ..... RINT 50
C PURPOSE RINT 60
C INTERCHANGE TWO ROWS OF A MATRIX RINT 70
C ..... RINT 80
C USAGE RINT 90
C CALL RINT(A,N,M,LA,LB) RINT 100
C ..... RINT 110
C DESCRIPTION OF PARAMETERS RINT 120
C A - NAME OF MATRIX RINT 130
C N - NUMBER OF ROWS IN A RINT 140
C M - NUMBER OF COLUMNS IN A RINT 150
C LA - ROW TO BE INTERCHANGED WITH ROW LB RINT 160
C LB - ROW TO BE INTERCHANGED WITH ROW LA RINT 170
C ..... RINT 180
C REMARKS RINT 190
C MATRIX A MUST BE A GENERAL MATRIX RINT 200
C ..... RINT 210
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED RINT 220
C NONE RINT 230
C ..... RINT 240
C METHOD RINT 250
C EACH ELEMENT OF ROW LA IS INTERCHANGED WITH CORRESPONDING RINT 260
C ELEMENT OF ROW LB RINT 270
C ..... RINT 280
C ..... RINT 290
C ..... RINT 300
C SUBROUTINE RINT(A,N,M,LA,LB) RINT 310
C DIMENSION A(I) RINT 320
C ..... RINT 330
C LAJ=LA-N RINT 340
C LBJ=LB-N RINT 350
C DO 3 J=1,M RINT 360
C ..... RINT 370
C LOCATE ELEMENTS IN BOTH ROWS RINT 380
C ..... RINT 390
C LAJ=LAJ+N RINT 400
C LBJ=LBJ+N RINT 410
C ..... RINT 420
C INTERCHANGE ELEMENTS RINT 430
C ..... RINT 440
C SAVE=A(LAJ) RINT 450
C A(LAJ)=A(LBJ) RINT 460
C 3 A(LBJ)=SAVE RINT 470
C RETURN RINT 480
C END RINT 490

```

Subroutine CINT

```

C ..... CINT 10
C ..... CINT 20
C ..... CINT 30
C SUBROUTINE CINT CINT 40
C ..... CINT 50
C PURPOSE CINT 60
C INTERCHANGE TWO COLUMNS OF A MATRIX CINT 70
C ..... CINT 80
C USAGE CINT 90
C CALL CINT(A,N,LA,LB) CINT 100
C ..... CINT 110
C DESCRIPTION OF PARAMETERS CINT 120
C A - NAME OF MATRIX CINT 130
C N - NUMBER OF ROWS IN A CINT 140
C LA - COLUMN TO BE INTERCHANGED WITH COLUMN LB CINT 150
C LB - COLUMN TO BE INTERCHANGED WITH COLUMN LA CINT 160
C ..... CINT 170
C REMARKS CINT 180
C MATRIX A MUST BE A GENERAL MATRIX CINT 190
C ..... CINT 200
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED CINT 210
C NONE CINT 220
C ..... CINT 230
C METHOD CINT 240
C EACH ELEMENT OF COLUMN LA IS INTERCHANGED WITH CORRESPONDING CINT 250
C ELEMENT OF COLUMN LB CINT 260
C ..... CINT 270
C ..... CINT 280
C ..... CINT 290
C SUBROUTINE CINT(A,N,LA,LB) CINT 300
C DIMENSION A(I) CINT 310
C ..... CINT 320
C LOCATE STARTING POINT OF BOTH COLUMNS CINT 330
C ..... CINT 340
C ILA=N*(LA-1) CINT 350
C ILB=N*(LB-1) CINT 360
C ..... CINT 370
C DO 3 I=1,M CINT 380
C ILA=ILA+1 CINT 390
C ILB=ILB+1 CINT 400
C ..... CINT 410
C INTERCHANGE ELEMENTS CINT 420
C ..... CINT 430
C SAVE=A(ILA) CINT 440
C A(ILA)=A(ILB) CINT 450
C 3 A(ILB)=SAVE CINT 460
C RETURN CINT 470
C END CINT 480

```

Subroutine RSUM

```

C .....
C SUBROUTINE RSUM
C .....
C PURPOSE
C SUM ELEMENTS OF EACH ROW TO FORM COLUMN VECTOR
C USAGE
C CALL RSUM (A,R,N,M,MS)
C .....
C DESCRIPTION OF PARAMETERS
C A - NAME OF INPUT MATRIX
C R - NAME OF VECTOR OF LENGTH N
C N - NUMBER OF ROWS IN A
C M - NUMBER OF COLUMNS IN A
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C .....
C REMARKS
C VECTOR R CANNOT BE IN THE SAME LOCATION AS MATRIX A
C UNLESS A IS GENERAL
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C .....
C METHOD
C ELEMENTS ARE SUMMED ACROSS EACH ROW INTO A CORRESPONDING
C ELEMENT OF OUTPUT COLUMN VECTOR R
C .....
C SUBROUTINE RSUM(A,R,N,M,MS)
C DIMENSION A(I),R(I)
C DO 3 I=1,M
C CLEAR OUTPUT LOCATION
C R(I)=0.0
C DO 3 J=1,N
C LOCATE ELEMENT FOR ANY MATRIX STORAGE MODE
C CALL LOC(I,J,I,J,N,M,MS)
C TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
C IF(IJ) 2,3,2
C ACCUMULATE IN OUTPUT VECTOR
C 2 R(I)=R(I)+A(IJ)
C 3 CONTINUE
C RETURN
C END
RSUM 10
RSUM 20
RSUM 30
RSUM 40
RSUM 50
RSUM 60
RSUM 70
RSUM 80
RSUM 90
RSUM 100
RSUM 110
RSUM 120
RSUM 130
RSUM 140
RSUM 150
RSUM 160
RSUM 170
RSUM 180
RSUM 190
RSUM 200
RSUM 210
RSUM 220
RSUM 230
RSUM 240
RSUM 250
RSUM 260
RSUM 270
RSUM 280
RSUM 290
RSUM 300
RSUM 310
RSUM 320
RSUM 330
RSUM 340
RSUM 350
RSUM 360
RSUM 370
RSUM 380
RSUM 390
RSUM 400
RSUM 410
RSUM 420
RSUM 430
RSUM 440
RSUM 450
RSUM 460
RSUM 470
RSUM 480
RSUM 490
RSUM 500
RSUM 510
RSUM 520
RSUM 530
RSUM 540
RSUM 550
RSUM 560
RSUM 570
RSUM 580
RSUM 590

```

Subroutine CSUM

```

C .....
C SUBROUTINE CSUM
C .....
C PURPOSE
C SUM ELEMENTS OF EACH COLUMN TO FORM ROW VECTOR
C USAGE
C CALL CSUM(A,R,N,M,MS)
C .....
C DESCRIPTION OF PARAMETERS
C A - NAME OF INPUT MATRIX
C R - NAME OF VECTOR OF LENGTH M
C N - NUMBER OF ROWS IN A
C M - NUMBER OF COLUMNS IN A
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C .....
C REMARKS
C VECTOR R CANNOT BE IN THE SAME LOCATION AS MATRIX A
C UNLESS A IS GENERAL
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C .....
C METHOD
C ELEMENTS ARE SUMMED DOWN EACH COLUMN INTO A CORRESPONDING
C ELEMENT OF OUTPUT ROW VECTOR R
C .....
C SUBROUTINE CSUM(A,R,N,M,MS)
C DIMENSION A(I),R(I)
C DO 3 J=1,M
C CLEAR OUTPUT LOCATION
C R(J)=0.0
C DO 3 I=1,N
C LOCATE ELEMENT FOR ANY MATRIX STORAGE MODE
C CALL LOC(I,J,I,J,N,M,MS)
C TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
C IF(IJ) 2,3,2
C ACCUMULATE IN OUTPUT VECTOR
C 2 R(J)=R(J)+A(IJ)
C 3 CONTINUE
C RETURN
C END
CSUM 10
CSUM 20
CSUM 30
CSUM 40
CSUM 50
CSUM 60
CSUM 70
CSUM 80
CSUM 90
CSUM 100
CSUM 110
CSUM 120
CSUM 130
CSUM 140
CSUM 150
CSUM 160
CSUM 170
CSUM 180
CSUM 190
CSUM 200
CSUM 210
CSUM 220
CSUM 230
CSUM 240
CSUM 250
CSUM 260
CSUM 270
CSUM 280
CSUM 290
CSUM 300
CSUM 310
CSUM 320
CSUM 330
CSUM 340
CSUM 350
CSUM 360
CSUM 370
CSUM 380
CSUM 390
CSUM 400
CSUM 410
CSUM 420
CSUM 430
CSUM 440
CSUM 450
CSUM 460
CSUM 470
CSUM 480
CSUM 490
CSUM 500
CSUM 510
CSUM 520
CSUM 530
CSUM 540
CSUM 550
CSUM 560
CSUM 570
CSUM 580
CSUM 590

```

Subroutine RTAB

The function of this subroutine is graphically displayed by Figure 7 (see description under "Method" in the program listing).

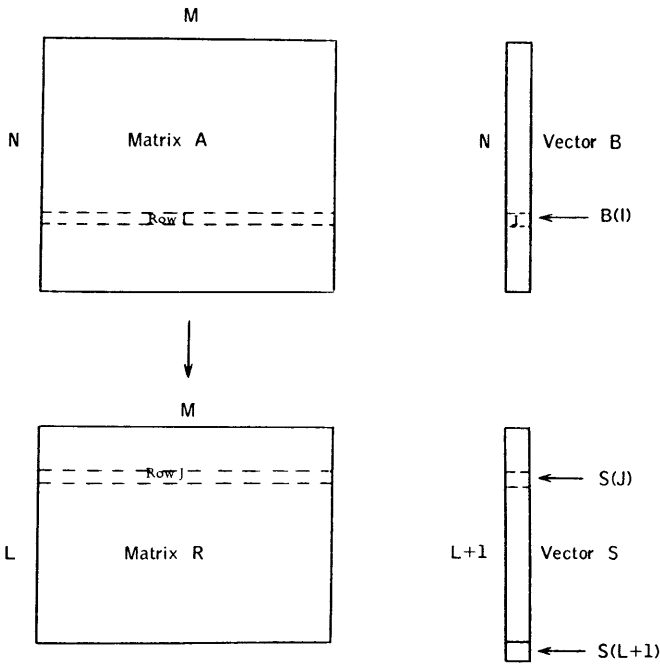


Figure 7. Row tabulation

```

C     RTAB 10
C     .RTAB 20
C     RTAB 30
C     SUBROUTINE RTAB           RTAB 40
C     FLRCSSE                 RTAB 50
C     TABULATE RCNS OF A MATRIX TO FORM A SUMMARY MATRIX  RTAB 60
C     .RTAB 70
C     LSACE                   RTAB 80
C     CALL RTAB(A,B,N,M,S,N,M,PS,L) RTAB 90
C     .RTAB 100
C     DESCRIPTION OF PARAMETERS RTAB 110
C     A - NAME OF INPUT MATRIX  RTAB 120
C     B - NAME OF INPUT VECTOR OF LENGTH N CONTAINING KEY  RTAB 130
C     R - NAME OF OUTPUT MATRIX CONTAINING SUMMARY OF ROW DATA. RTAB 140
C     IT IS INITIALLY SET TO ZERO BY THIS SUBROUTINE.  RTAB 150
C     S - NAME OF OUTPUT VECTOR OF LENGTH L+1 CONTAINING COUNTS RTAB 160
C     N - NUMBER OF RCNS IN A  RTAB 170
C     M - NUMBER OF COLUMNS IN A AND R  RTAB 180
C     L - NUMBER OF RCNS IN R  RTAB 190
C     PS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A  RTAB 200
C     C - GENERAL  RTAB 210
C     I - SYMMETRIC  RTAB 220
C     Z - UPPER TRIANGULAR  RTAB 230
C     .RTAB 240
C     REMARKS  RTAB 250
C     MATRIX R IS ALWAYS A GENERAL MATRIX  RTAB 260
C     .RTAB 270
C     SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED  RTAB 280
C     FPC  RTAB 290
C     .RTAB 300
C     .RTAB 310
C     METHOD  RTAB 320
C     RCNS OF DATA IN MATRIX A ARE TABULATED BASED ON THE KEY  RTAB 340
C     CONTAINED IN VECTOR B. THE FLOATING POINT NUMBER IN B(I) IS  RTAB 350
C     TABULATED TO FORM J. THE ITH RCN OF A IS ADDED TO THE JTH  RTAB 360
C     RCN OF R ELEMENT BY ELEMENT AND ONE IS ADDED TO S(J). IF J  RTAB 370
C     IS NOT BETWEEN ONE AND L, ONE IS ADDED TO S(L+1). THIS  RTAB 380
C     PROCEDURE IS REPEATED FOR EVERY ELEMENT IN VECTOR B.  RTAB 390
C     UPON COMPLETION, THE OUTPUT MATRIX R CONTAINS A SUMMARY OF  RTAB 400
C     ROW DATA AS SPECIFIED BY VECTOR B. EACH ELEMENT IN VECTOR S  RTAB 410
C     CONTAINS A COUNT OF THE NUMBER OF RCNS OF A USED TO FORM THE  RTAB 420
C     CORRESPONDING RCN OF R. ELEMENT S(L+1) CONTAINS A COUNT OF  RTAB 430
C     THE NUMBER OF RCNS OF A NOT INCLUDED IN R AS A RESULT OF J  RTAB 440
C     BEING LESS THAN ONE OR GREATER THAN L.  RTAB 450
C     .RTAB 460
C     .RTAB 470
C     SUBROUTINE RTAB(A,B,R,S,N,M,PS,L)  RTAB 480
C     DIMENSION A(L,M),B(1),R(1),S(1)  RTAB 490
C     .RTAB 500
C     CLEAR OUTPUT AREAS  RTAB 510
C     .RTAB 520
C     CALL LCC(P,L,IT,M,L,C)  RTAB 530
C     CC IC IR=1,IT  RTAB 540
C     IC REIR)=C,C  RTAB 550
C     CC IC IS=1,L  RTAB 560
C     IC SEIS)=C,C  RTAB 570
C     CC SE(SL+1)=C,C  RTAB 580
C     .RTAB 590
C     CC IC I=1,N  RTAB 600
C     .RTAB 610
C     TEST FOR THE KEY OUTSIDE THE RANGE  RTAB 620
C     .RTAB 630
C     JR=B(I)  RTAB 640
C     IF (JR-1) 5C,4C,3C  RTAB 650
C     3C IF (JR-L) 4C,4C,3C  RTAB 660
C     .RTAB 670
C     ADD RCN OF A TO RCN OF R AND 1 TO COUNT  RTAB 680
C     .RTAB 690
C     4C CALL RACC (A,I,R,IR,N,M,PS,L)  RTAB 700
C     S(JR)=S(JR)+1,C  RTAB 710
C     CC IC CC  RTAB 720
C     .RTAB 730
C     5C S(L+1)=S(L+1)+1,C  RTAB 740
C     .RTAB 750
C     .RTAB 760
C     .RTAB 770
C     .RTAB 780
C     .RTAB 790

```

Subroutine CTAB

The function of this subroutine is graphically displayed by Figure 8 (see description under "Method" in the program listing).

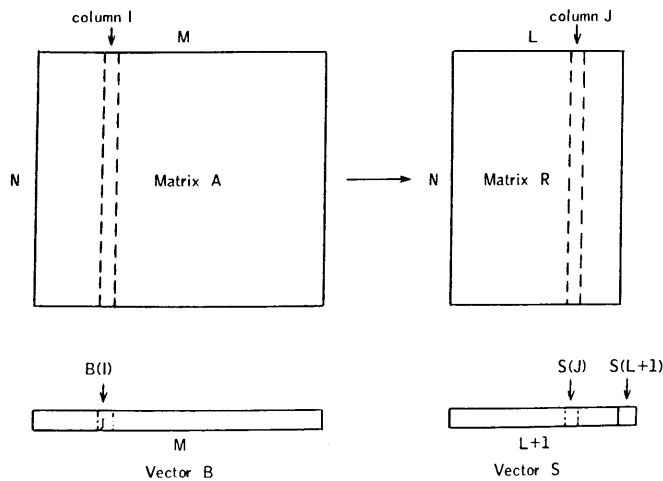


Figure 8. Column tabulation

```

C
C ..... CTAB 10
C ..... CTAB 20
C ..... CTAB 30
C ..... CTAB 40
C ..... CTAB 50
C ..... CTAB 60
C ..... CTAB 70
C ..... CTAB 80
C ..... CTAB 90
C ..... CTAB 100
C ..... CTAB 110
C ..... CTAB 120
C ..... CTAB 130
C ..... CTAB 140
C ..... CTAB 150
C ..... CTAB 160
C ..... CTAB 170
C ..... CTAB 180
C ..... CTAB 190
C ..... CTAB 200
C ..... CTAB 210
C ..... CTAB 220
C ..... CTAB 230
C ..... CTAB 240
C ..... CTAB 250
C ..... CTAB 260
C ..... CTAB 270
C ..... CTAB 280
C ..... CTAB 290
C ..... CTAB 300
C ..... CTAB 310
C ..... CTAB 320
C ..... CTAB 330
C ..... CTAB 340
C ..... CTAB 350
C ..... CTAB 360
C ..... CTAB 370
C ..... CTAB 380
C ..... CTAB 390
C ..... CTAB 400
C ..... CTAB 410
C ..... CTAB 420
C ..... CTAB 430
C ..... CTAB 440
C ..... CTAB 450
C ..... CTAB 460
C ..... CTAB 470
C ..... CTAB 480
C ..... CTAB 490
C ..... CTAB 500
C ..... CTAB 510
C ..... CTAB 520
C ..... CTAB 530
C ..... CTAB 540
C ..... CTAB 550
C ..... CTAB 560
C ..... CTAB 570
C ..... CTAB 580
C ..... CTAB 590
C ..... CTAB 600
C ..... CTAB 610
C ..... CTAB 620
C ..... CTAB 630
C ..... CTAB 640
C ..... CTAB 650
C ..... CTAB 660
C ..... CTAB 670
C ..... CTAB 680
C ..... CTAB 690
C ..... CTAB 700
C ..... CTAB 710
C ..... CTAB 720
C ..... CTAB 730
C ..... CTAB 740
C ..... CTAB 750
C ..... CTAB 760
C ..... CTAB 770
C ..... CTAB 780

```

Subroutine RSRT

```

C ..... RSRT 10
C ..... RSRT 20
C ..... RSRT 30
C ..... RSRT 40
C ..... RSRT 50
C ..... RSRT 60
C ..... RSRT 70
C ..... RSRT 80
C ..... RSRT 90
C ..... RSRT 100
C ..... RSRT 110
C ..... RSRT 120
C ..... RSRT 130
C ..... RSRT 140
C ..... RSRT 150
C ..... RSRT 160
C ..... RSRT 170
C ..... RSRT 180
C ..... RSRT 190
C ..... RSRT 200
C ..... RSRT 210
C ..... RSRT 220
C ..... RSRT 230
C ..... RSRT 240
C ..... RSRT 250
C ..... RSRT 260
C ..... RSRT 270
C ..... RSRT 280
C ..... RSRT 290
C ..... RSRT 300
C ..... RSRT 310
C ..... RSRT 320
C ..... RSRT 330
C ..... RSRT 340
C ..... RSRT 350
C ..... RSRT 360
C ..... RSRT 370
C ..... RSRT 380
C ..... RSRT 390
C ..... RSRT 400
C ..... RSRT 410
C ..... RSRT 420
C ..... RSRT 430
C ..... RSRT 440
C ..... RSRT 450
C ..... RSRT 460
C ..... RSRT 470
C ..... RSRT 480
C ..... RSRT 490
C ..... RSRT 500
C ..... RSRT 510
C ..... RSRT 520
C ..... RSRT 530
C ..... RSRT 540
C ..... RSRT 550
C ..... RSRT 560
C ..... RSRT 570
C ..... RSRT 580
C ..... RSRT 590
C ..... RSRT 600
C ..... RSRT 610
C ..... RSRT 620
C ..... RSRT 630
C ..... RSRT 640
C ..... RSRT 650
C ..... RSRT 660
C ..... RSRT 670
C ..... RSRT 680
C ..... RSRT 690
C ..... RSRT 700
C ..... RSRT 710
C ..... RSRT 720
C ..... RSRT 730
C ..... RSRT 740
C ..... RSRT 750
C ..... RSRT 760
C ..... RSRT 770
C ..... RSRT 780
C ..... RSRT 790
C ..... RSRT 800
C ..... RSRT 810
C ..... RSRT 820
C ..... RSRT 830
C ..... RSRT 840
C ..... RSRT 850
C ..... RSRT 860
C ..... RSRT 870
C ..... RSRT 880
C ..... RSRT 890
C ..... RSRT 900
C ..... RSRT 910
C ..... RSRT 920
C ..... RSRT 930
C ..... RSRT 940
C ..... RSRT 950
C ..... RSRT 960
C ..... RSRT 970
C ..... RSRT 980
C ..... RSRT 990
C ..... RSRT1000
C ..... RSRT1010
C ..... RSRT1020
C ..... RSRT1030
C ..... RSRT1040
C ..... RSRT1050

```

Subroutine CSRT

```

C
C
C ..... CSRT 10
C SUBROUTINE CSRT CSRT 20
C CSRT 30
C CSRT 40
C CSRT 50
C CSRT 60
C CSRT 70
C CSRT 80
C CSRT 90
C CSRT 100
C CSRT 110
C CSRT 120
C CSRT 130
C CSRT 140
C CSRT 150
C CSRT 160
C CSRT 170
C CSRT 180
C CSRT 190
C CSRT 200
C CSRT 210
C CSRT 220
C CSRT 230
C CSRT 240
C CSRT 250
C CSRT 260
C CSRT 270
C CSRT 280
C CSRT 290
C CSRT 300
C CSRT 310
C CSRT 320
C CSRT 330
C CSRT 340
C CSRT 350
C CSRT 360
C CSRT 370
C CSRT 380
C CSRT 390
C CSRT 400
C CSRT 410
C CSRT 420
C CSRT 430
C CSRT 440
C CSRT 450
C CSRT 460
C CSRT 470
C CSRT 480
C CSRT 490
C CSRT 500
C CSRT 510
C CSRT 520
C CSRT 530
C CSRT 540
C CSRT 550
C CSRT 560
C CSRT 570
C CSRT 580
C CSRT 590
C CSRT 600
C CSRT 610
C CSRT 620
C CSRT 630
C CSRT 640
C CSRT 650
C CSRT 660
C CSRT 670
C CSRT 680
C CSRT 690
C CSRT 700
C CSRT 710
C CSRT 720
C CSRT 730
C CSRT 740
C CSRT 750
C CSRT 760
C CSRT 770
C CSRT 780
C CSRT 790
C CSRT 800
C CSRT 810
C CSRT 820
C CSRT 830
C CSRT 840
C CSRT 850
C CSRT 860
C CSRT 870
C CSRT 880
C CSRT 890
C CSRT 900
C CSRT 910
C CSRT 920
C CSRT 930
C CSRT 940
C CSRT 950
C CSRT 960
C CSRT 970
C
C
C .....
C SUBROUTINE CSRT
C
C PURPOSE
C SORT COLUMNS OF A MATRIX
C
C USAGE
C CALL CSRT(A,B,R,N,M,MS)
C
C DESCRIPTION OF PARAMETERS
C A - NAME OF INPUT MATRIX TO BE SORTED
C B - NAME OF INPUT VECTOR WHICH CONTAINS SORTING KEY
C R - NAME OF SORTED OUTPUT MATRIX
C N - NUMBER OF ROWS IN A AND R
C M - NUMBER OF COLUMNS IN A AND R AND LENGTH OF B
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C
C REMARKS
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRIX A
C MATRIX R IS ALWAYS A GENERAL MATRIX
C M MUST BE GREATER THAN ONE.
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C COPY
C
C METHOD
C COLUMNS OF INPUT MATRIX A ARE SORTED TO FORM OUTPUT MATRIX
C R. THE SORTED COLUMN SEQUENCE IS DETERMINED BY THE VALUES OF
C ELEMENTS IN ROW VECTOR B. THE LOWEST VALUED ELEMENT IN
C B WILL CAUSE THE CORRESPONDING COLUMN OF A TO BE PLACED IN
C THE FIRST COLUMN OF R. THE HIGHEST VALUED ELEMENT OF B WILL
C CAUSE THE CORRESPONDING ROW OF A TO BE PLACED IN THE LAST
C COLUMN OF R. IF DUPLICATE VALUES EXIST IN B, THE
C CORRESPONDING COLUMNS OF A ARE MOVED TO R IN THE SAME ORDER
C AS IN A.
C
C .....
C SUBROUTINE CSRT(A,B,R,N,M,MS)
C DIMENSION A(1),B(1),R(1)
C
C MOVE SORTING KEY VECTOR TO FIRST ROW OF OUTPUT MATRIX
C AND BUILD ORIGINAL SEQUENCE LIST IN SECOND ROW
C
C IK=1
C DO 10 J=1,M
C R(IK)=B(J)
C R(IK+1)=J
C 10 IK=IK+N
C
C SORT ELEMENTS IN SORTING KEY VECTOR (ORIGINAL SEQUENCE LIST
C IS RESEQUENCED ACCORDINGLY)
C
C L=M+1
C 20 ISORT=0
C LP=1
C IQ=N+1
C DO 50 J=2,L
C IF(R(IQ)-R(LP)) 30,40,40
C 30 ISORT=1
C RSAVE=R(LP)
C R(LP)=R(IQ)
C R(IQ)=RSAVE
C SAVER=R(LP+1)
C R(LP+1)=R(IQ+1)
C R(IQ+1)=SAVER
C 40 IP=IP+N
C IQ=IQ+N
C 50 CONTINUE
C IF(ISORT) 20,60,20
C
C MOVE COLUMNS FROM MATRIX A TO MATRIX R (NUMBER IN SECOND ROW
C OF R REPRESENTS COLUMN NUMBER OF MATRIX A TO BE MOVED)
C
C 60 IQ=-N
C DO 70 J=1,M
C IQ=IQ+N
C
C GET COLUMN NUMBER IN MATRIX A
C
C I2=IQ+2
C IN=R(I2)
C
C MOVE COLUMN
C
C IR=IQ+1
C CALL COPY(A,IN,R(IR),N,M,MS)
C 70 CONTINUE
C RETURN
C END

```

Subroutine RCUT

```

C
C ..... RCUT 10
C SUBROUTINE RCUT RCUT 20
C RCUT 30
C RCUT 40
C RCUT 50
C RCUT 60
C RCUT 70
C RCUT 80
C RCUT 90
C RCUT 100
C RCUT 110
C RCUT 120
C RCUT 130
C RCUT 140
C RCUT 150
C RCUT 160
C RCUT 170
C RCUT 180
C RCUT 190
C RCUT 200
C RCUT 210
C RCUT 220
C RCUT 230
C RCUT 240
C RCUT 250
C RCUT 260
C RCUT 270
C RCUT 280
C RCUT 290
C RCUT 300
C RCUT 310
C RCUT 320
C RCUT 330
C RCUT 340
C RCUT 350
C RCUT 360
C RCUT 370
C RCUT 380
C RCUT 390
C RCUT 400
C RCUT 410
C RCUT 420
C RCUT 430
C RCUT 440
C RCUT 450
C RCUT 460
C RCUT 470
C RCUT 480
C RCUT 490
C RCUT 500
C RCUT 510
C RCUT 520
C RCUT 530
C RCUT 540
C RCUT 550
C RCUT 560
C RCUT 570
C RCUT 580
C RCUT 590
C RCUT 600
C RCUT 610
C RCUT 620
C RCUT 630
C RCUT 640
C RCUT 650
C RCUT 660
C RCUT 670
C RCUT 680
C RCUT 690
C RCUT 700
C RCUT 710
C RCUT 720
C RCUT 730
C RCUT 740
C RCUT 750
C
C
C .....
C SUBROUTINE RCUT
C
C PURPOSE
C PARTITION A MATRIX BETWEEN SPECIFIED ROWS TO FORM TWO
C RESULTANT MATRICES
C
C USAGE
C CALL RCUT (A,L,R,S,N,M,MS)
C
C DESCRIPTION OF PARAMETERS
C A - NAME OF INPUT MATRIX
C L - ROW OF A ABOVE WHICH PARTITIONING TAKES PLACE
C R - NAME OF MATRIX TO BE FORMED FROM UPPER PORTION OF A
C S - NAME OF MATRIX TO BE FORMED FROM LOWER PORTION OF A
C N - NUMBER OF ROWS IN A
C M - NUMBER OF COLUMNS IN A
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C
C REMARKS
C MATRIX R CANNOT BE IN SAME LOCATION AS MATRIX A
C MATRIX S CANNOT BE IN SAME LOCATION AS MATRIX A
C MATRIX R CANNOT BE IN SAME LOCATION AS MATRIX S
C MATRIX R AND MATRIX S ARE ALWAYS GENERAL MATRICES
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C
C METHOD
C ELEMENTS OF MATRIX A ABOVE ROW L ARE MOVED TO FORM MATRIX R
C AND L-1 ROWS AND M COLUMNS. ELEMENTS OF MATRIX A IN ROW L
C AND BELOW ARE MOVED TO FORM MATRIX S OF N-L+1 ROWS AND M
C COLUMNS
C
C .....
C SUBROUTINE RCUT(A,L,R,S,N,M,MS)
C DIMENSION A(1),R(1),S(1)
C
C IR=C
C IS=C
C DO 70 J=1,M
C DO 70 I=L+1,N
C
C FIND LOCATION IN OUTPUT MATRIX AND SET TO ZERO
C
C IF(I-L) 20,10,10
C 10 IS=IS+1
C S(IS)=0.0
C GO TO 30
C 20 IR=IR+1
C R(IR)=0.0
C
C LOCATE ELEMENT FOR ANY MATRIX STORAGE MODE
C
C 30 CALL LOC(I,J,IJ,N,M,MS)
C
C TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
C
C IF(IJ) 40,70,40
C
C DETERMINE WHETHER ABOVE OR BELOW L
C
C 40 IF(I-L) 50,50,50
C 50 S(IS)=A(IJ)
C GO TO 70
C 50 R(IR)=A(IJ)
C 70 CONTINUE
C RETURN
C END

```

Subroutine CCUT

```

C .....
C SUBROUTINE CCUT
C .....
C PURPOSE
C PARTITION A MATRIX BETWEEN SPECIFIED COLUMNS TO FORM TWO
C RESULTANT MATRICES
C .....
C USAGE
C CALL CCUT (A,L,R,S,N,M,MS)
C .....
C DESCRIPTION OF PARAMETERS
C A - NAME OF INPUT MATRIX
C L - COLUMN OF A TO THE LEFT OF WHICH PARTITIONING TAKES
C PLACE
C R - NAME OF MATRIX TO BE FORMED FROM LEFT PORTION OF A
C S - NAME OF MATRIX TO BE FORMED FROM RIGHT PORTION OF A
C N - NUMBER OF ROWS IN A
C M - NUMBER OF COLUMNS IN A
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C .....
C REMARKS
C MATRIX R CANNOT BE IN SAME LOCATION AS MATRIX A
C MATRIX S CANNOT BE IN SAME LOCATION AS MATRIX A
C MATRIX R CANNOT BE IN SAME LOCATION AS MATRIX S
C MATRIX R AND MATRIX S ARE ALWAYS GENERAL MATRICES
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C .....
C METHOD
C ELEMENTS OF MATRIX A TO THE LEFT OF COLUMN L ARE MOVED TO
C FORM MATRIX R OF N ROWS AND L-1 COLUMNS. ELEMENTS OF
C MATRIX A IN COLUMN L AND TO THE RIGHT OF L ARE MOVED TO FORM
C MATRIX S OF N ROWS AND M-L+1 COLUMNS.
C .....
C .....
C SUBROUTINE CCUT(A,L,R,S,N,M,MS)
C DIMENSION A(1),R(1),S(1)
C .....
C 1R=0
C 1S=0
C DO 70 J=1,M
C DO 70 I=1,N
C .....
C FIND LOCATION IN OUTPUT MATRIX AND SET TO ZERO
C .....
C IF(I=L) 20,10,10
C 10 1S=1S+1
C S(I)=0.0
C GO TO 30
C 20 1R=1R+1
C R(I)=0.0
C .....
C LOCATE ELEMENT FOR ANY MATRIX STORAGE MODE
C .....
C 30 CALL LOC(I,J,IJ,N,M,MS)
C .....
C TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
C .....
C IF(IJ) 40,70,40
C .....
C DETERMINE WHETHER RIGHT OR LEFT OF L
C .....
C 40 IF(I=L) 50,50,50
C 50 S(I)=A(IJ)
C GO TO 70
C 50 R(I)=A(IJ)
C 70 CONTINUE
C RETURN
C END

```

Subroutine RTIE

```

C .....
C SUBROUTINE RTIE
C .....
C PURPOSE
C ADJOIN TWO MATRICES WITH SAME COLUMN DIMENSION TO FORM ONE
C RESULTANT MATRIX (SEE METHOD)
C .....
C USAGE
C CALL RTIE(A,B,R,N,M,MSA,MSB,L)
C .....
C DESCRIPTION OF PARAMETERS
C A - NAME OF FIRST INPUT MATRIX
C B - NAME OF SECOND INPUT MATRIX
C R - NAME OF OUTPUT MATRIX
C N - NUMBER OF ROWS IN A
C M - NUMBER OF COLUMNS IN A+B
C MSA - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C MSB - SAME AS MSA EXCEPT FOR MATRIX B
C L - NUMBER OF ROWS IN B
C .....
C REMARKS
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRICES A OR B
C MATRIX R IS ALWAYS A GENERAL MATRIX
C MATRIX A MUST HAVE THE SAME NUMBER OF COLUMNS AS MATRIX B
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C .....
C METHOD
C MATRIX B IS ATTACHED TO THE BOTTOM OF MATRIX A .
C THE RESULTANT MATRIX R CONTAINS N+L ROWS AND M COLUMNS.
C .....
C .....
C SUBROUTINE RTIE(A,B,R,N,M,MSA,MSB,L)
C DIMENSION A(1),B(1),R(1)
C .....
C NN=N
C IR=0
C NX=NN
C MSX=MSA
C DO 9 J=1,M
C DO 8 I=1,2
C DO 7 I=1,NN
C IR=IR+1
C RTIR=0.0
C .....
C LOCATE ELEMENT FOR ANY MATRIX STORAGE MODE
C .....
C CALL LOC(I,J,IJ,NN,M,MSX)
C .....
C TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
C .....
C IF(IJ) 2,7,2
C .....
C MOVE ELEMENT TO MATRIX R
C .....
C 2 GO TO(3,4),11
C 3 R(IR)=A(IJ)
C GO TO 7
C 4 R(IR)=B(IJ)
C 7 CONTINUE
C .....
C REPEAT ABOVE FOR MATRIX B
C .....
C MSX=MSB
C 8 NN=L
C .....
C RESCT FOR NEXT COLUMN
C .....
C MSA=MSA
C 9 NN=NX
C RETURN
C END

```

Subroutine CTIE

```

C .....
C SUBROUTINE CTIE
C .....
C PURPOSE
C ADJOIN TWO MATRICES WITH SAME ROW DIMENSION TO FORM ONE
C RESULTANT MATRIX (SLE METHOD)
C .....
C USAGE
C CALL CTIE(A,B,R,N,M,MSA,MSB,L)
C .....
C DESCRIPTION OF PARAMETERS
C A - NAME OF FIRST INPUT MATRIX
C B - NAME OF SECOND INPUT MATRIX
C R - NAME OF OUTPUT MATRIX
C N - NUMBER OF ROWS IN A,B,R
C M - NUMBER OF COLUMNS IN A
C MSA - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A
C 0 - GENERAL
C 1 - SYMMETRIC
C 2 - DIAGONAL
C MSB - SAME AS MSA EXCEPT FOR MATRIX B
C L - NUMBER OF COLUMNS IN B
C .....
C REMARKS
C MATRIX R CANNOT BE IN THE SAME LOCATION AS MATRICES A OR B
C MATRIX R IS ALWAYS A GENERAL MATRIX
C MATRIX A MUST HAVE THE SAME NUMBER OF ROWS AS MATRIX B
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C LOC
C .....
C METHOD
C MATRIX B IS ATTACHED TO THE RIGHT OF MATRIX A .
C THE RESULTANT MATRIX R CONTAINS N ROWS AND M+L COLUMNS
C .....
C SUBROUTINE CTIE(A,B,R,N,M,MSA,MSB,L)
C DIMENSION A(1),B(1),R(1)
C .....
C MM=M
C IR=0
C MSX=MSA
C DO 6 JJ=1,2
C DO 5 J=1,MM
C DO 5 I=1,N
C IK=IR+1
C K(IK)=0
C .....
C LOCATE ELEMENT FOR ANY MATRIX STORAGE MODE
C .....
C CALL LOC(I,J,IJ,N,MM,MSX)
C .....
C TEST FOR ZERO ELEMENT IN DIAGONAL MATRIX
C .....
C IF(IJ) 2,5,2
C .....
C MOVE ELEMENT TO MATRIX R
C .....
C 2 GO TO(3,4),JJ
C 3 R(IK)=A(IJ)
C GO TO 5
C 4 R(IK)=B(IJ)
C 5 CONTINUE
C .....
C REPEAT ABOVE FOR MATRIX B
C .....
C MSX=MSB
C MM=L
C 6 CONTINUE
C RETURN
C END

```

Subroutines MPRC and DMPRC

These subroutines permute the rows or columns of a given m by n matrix A according to a transposition vector $ITRA = (t_1, \dots, t_s)$ or its inverse. (See the general discussion under "Permutations" for definitions and notation.)

1. Mathematical background

Permuting the rows or columns of A according to the transposition vector $ITRA$ means applying the permutation $(1, t_1), \dots, (s, t_s)$ to the rows or columns of A , while permuting according to $ITRA^{-1}$ means applying the permutation $(s, t_s), \dots, (1, t_1)$.

2. Programming considerations

If the columns of A are to be permuted, the input parameter $IROCO$ must be nonzero, and $s = n$; if the rows are to be permuted, $IROCO$ must be zero, and $s = m$. Similarly, if the input parameter INV is nonzero, the rows or columns of A are permuted according to $ITRA$; while if INV is zero, the rows or columns of A are permuted according to $ITRA^{-1}$.

If m and n are not both positive, or if $ITRA$ is not a transposition vector on $S = \{1, \dots, s\}$, the subroutines are prematurely terminated and the error parameter IER is set to -1 or 1 , respectively. If there is no error, IER is set to zero.

The matrix A is assumed to be stored columnwise, and the permutation of the rows or columns of A is performed in s steps. At the i^{th} step, if the permutation is according to $ITRA^{-1}$, rows or columns i and s_i are interchanged; if the permutation is according to $ITRA$, rows or columns $s - i + 1$ and $t_{s - i + 1}$ are interchanged.

```

C .....
C SUBROUTINE MPRC
C .....
C PURPOSE
C TO PERMUTE THE ROWS OR COLUMNS OF A GIVEN MATRIX ACCORDING
C TO A GIVEN TRANSPOSITION VECTOR OR ITS INVERSE. (SEE THE
C DISCUSSION ON PERMUTATIONS FOR DEFINITIONS AND NOTATION.)
C .....
C USAGE
C CALL MPRC(A,M,N,ITRA,INV,IROCO,IER)
C .....
C DESCRIPTION OF PARAMETERS
C A - GIVEN M BY N MATRIX AND RESULTING PERMUTED MATRIX
C M - NUMBER OF ROWS OF A
C N - NUMBER OF COLUMNS OF A
C ITRA - GIVEN TRANSPOSITION VECTOR (DIMENSION M IF ROWS ARE
C PERMUTED, N IF COLUMNS ARE PERMUTED)
C INV - INPUT PARAMETER
C INV NON-ZERO - PERMUTE ACCORDING TO ITRA
C INV = 0 - PERMUTE ACCORDING TO ITRA INVERSE
C IROCO - INPUT PARAMETER
C IROCO NON-ZERO - PERMUTE THE COLUMNS OF A
C IROCO = 0 - PERMUTE THE ROWS OF A
C IER - RESULTING ERROR PARAMETER
C IER = -1 - M AND N ARE NOT BOTH POSITIVE
C IER = 0 - NO ERROR
C IER = 1 - ITRA IS NOT A TRANSPOSITION VECTOR ON
C 1,...,M IF ROWS ARE PERMUTED, 1,...,N
C IF COLUMNS ARE PERMUTED
C .....
C REMARKS
C (1) IF IER=-1 THERE IS NO COMPUTATION.
C (2) IF IER= 1, THEN COMPUTATION HAS BEEN UNSUCCESSFUL DUE
C TO ERROR, BUT THE MATRIX A WILL REFLECT THE ROW OR
C COLUMN INTERCHANGES PERFORMED BEFORE THE ERROR WAS
C DETECTED.
C (3) THE MATRIX A IS ASSUMED TO BE STORED COLUMNWISE.

```

```

C          MPRC 400
C          SUBROUTINES AND SUBPROGRAMS REQUIRED
C          NONE
C          MPRC 410
C          MPRC 420
C          MPRC 430
C          MPRC 440
C          METHOD
C          THE ROWS OR COLUMNS ARE PERMUTED ELEMENTWISE, INTERCHANGING
C          ROW OR COLUMN I AND ITRA(1),...,ROW OR COLUMN K AND ITRA(K)
C          IN THAT ORDER IF INV=0, AND OTHERWISE INTERCHANGING ROW OR
C          COLUMN K AND ITRA(K),...,ROW OR COLUMN I AND ITRA(1), WHERE
C          K IS M OR N DEPENDING ON WHETHER WE PERMUTE ROWS OR COLUMNS.
C          MPRC 450
C          MPRC 460
C          MPRC 470
C          MPRC 480
C          MPRC 490
C          MPRC 500
C          MPRC 510
C          SUBROUTINE MPRC(A,M,N,ITRA,INV,IROCO,IER)
C          MPRC 520
C          MPRC 530
C          MPRC 540
C          MPRC 550
C          DIMENSION A(1),ITRA(1)
C          MPRC 560
C          MPRC 570
C          MPRC 580
C          MPRC 590
C          TEST OF DIMENSIONS
C          IF(M)14,14,1
C          1 IF(N)14,14,2
C          MPRC 600
C          MPRC 610
C          DETERMINE WHICH ARE TO BE PERMUTED--THE ROWS OR THE COLUMNS
C          2 IF(IROCO)3,4,3
C          MPRC 620
C          MPRC 630
C          MPRC 640
C          INITIALIZE FOR COLUMN INTERCHANGES
C          3 MM=M
C          MMM=-1
C          L=M
C          LL=N
C          GO TO 5
C          MPRC 650
C          MPRC 660
C          MPRC 670
C          MPRC 680
C          MPRC 690
C          MPRC 700
C          MPRC 710
C          INITIALIZE FOR ROW INTERCHANGES
C          4 MM=1
C          MMM=M
C          L=N
C          LL=M
C          MPRC 720
C          MPRC 730
C          MPRC 740
C          MPRC 750
C          MPRC 760
C          MPRC 770
C          INITIALIZE LOOP OVER ALL ROWS OR COLUMNS
C          5 IA=1
C          ID=1
C          MPRC 780
C          MPRC 790
C          MPRC 800
C          MPRC 810
C          TEST FOR INVERSE OPERATION
C          IF(INV)6,7,6
C          6 IA=LL
C          ID=-1
C          MPRC 820
C          MPRC 830
C          MPRC 840
C          MPRC 850
C          7 DO 12 I=1,LL
C          K=ITRA(IA)
C          IF(K-IA)8,12,9
C          8 IF(K)13,13,10
C          9 IF(LL-K)13,10,10
C          MPRC 860
C          MPRC 870
C          MPRC 880
C          MPRC 890
C          MPRC 900
C          MPRC 910
C          INITIALIZE ROW OR COLUMN INTERCHANGE
C          10 IL=IA+MM
C          K=K+MM
C          MPRC 920
C          MPRC 930
C          MPRC 940
C          MPRC 950
C          PERFORM ROW OR COLUMN INTERCHANGE
C          DO 11 J=1,L
C          SAVE=A(IL)
C          A(IL)=A(K)
C          A(K)=SAVE
C          K=K+MMM
C          11 IL=IL+MMM
C          MPRC1000
C          MPRC1010
C          MPRC1020
C          MPRC1030
C          MPRC1040
C          ADDRESS NEXT INTERCHANGE STEP
C          12 IA=IA+ID
C          MPRC1050
C          MPRC1060
C          MPRC1070
C          NORMAL EXIT
C          IER=0
C          RETURN
C          MPRC1080
C          MPRC1090
C          MPRC1100
C          ERROR RETURN IN CASE ITRA IS NOT A TRANSPOSITION VECTOR
C          13 IER=1
C          RETURN
C          MPRC1110
C          MPRC1120
C          MPRC1130
C          MPRC1140
C          ERROR RETURN IN CASE OF ILLEGAL DIMENSIONS
C          14 IER=-1
C          RETURN
C          END
C          MPRC1150
C          MPRC1160
C          MPRC1170
C          MPRC1180
C          MPRC1180

```

```

C          SUBROUTINES AND SUBPROGRAMS REQUIRED
C          NONE
C          DMPR 420
C          DMPR 430
C          DMPR 440
C          DMPR 450
C          METHOD
C          THE ROWS OR COLUMNS ARE PERMUTED ELEMENTWISE, INTERCHANGING
C          ROW OR COLUMN I AND ITRA(1),...,ROW OR COLUMN K AND ITRA(K)
C          IN THAT ORDER IF INV=0, AND OTHERWISE INTERCHANGING ROW OR
C          COLUMN K AND ITRA(K),...,ROW OR COLUMN I AND ITRA(1), WHERE
C          K IS M OR N DEPENDING ON WHETHER WE PERMUTE ROWS OR COLUMNS.
C          DMPR 460
C          DMPR 470
C          DMPR 480
C          DMPR 490
C          DMPR 500
C          DMPR 510
C          DMPR 520
C          DMPR 530
C          DMPR 540
C          SUBROUTINE DMPRC(A,M,N,ITRA,INV,IROCO,IER)
C          DMPR 550
C          DMPR 560
C          DMPR 570
C          DMPR 580
C          DMPR 590
C          DOUBLE PRECISION A,SAVE
C          TEST OF DIMENSIONS
C          IF(M)14,14,1
C          1 IF(N)14,14,2
C          DMPR 600
C          DMPR 610
C          DMPR 620
C          DMPR 630
C          DETERMINE WHICH ARE TO BE PERMUTED--THE ROWS OR THE COLUMNS
C          2 IF(IROCO)3,4,3
C          DMPR 640
C          DMPR 650
C          DMPR 660
C          INITIALIZE FOR COLUMN INTERCHANGES
C          3 MM=M
C          MMM=-1
C          L=M
C          LL=N
C          GO TO 5
C          DMPR 670
C          DMPR 680
C          DMPR 690
C          DMPR 700
C          DMPR 710
C          DMPR 720
C          DMPR 730
C          INITIALIZE FOR ROW INTERCHANGES
C          4 MM=1
C          MMM=M
C          L=N
C          LL=M
C          DMPR 740
C          DMPR 750
C          DMPR 760
C          DMPR 770
C          DMPR 780
C          DMPR 790
C          INITIALIZE LOOP OVER ALL ROWS OR COLUMNS
C          5 IA=1
C          ID=1
C          DMPR 800
C          DMPR 810
C          DMPR 820
C          DMPR 830
C          TEST FOR INVERSE OPERATION
C          IF(INV)6,7,6
C          6 IA=LL
C          ID=-1
C          DMPR 840
C          DMPR 850
C          DMPR 860
C          DMPR 870
C          7 DO 12 I=1,LL
C          K=ITRA(IA)
C          IF(K-IA)8,12,9
C          8 IF(K)13,13,10
C          9 IF(LL-K)13,10,10
C          DMPR 880
C          DMPR 890
C          DMPR 900
C          DMPR 910
C          DMPR 920
C          DMPR 930
C          INITIALIZE ROW OR COLUMN INTERCHANGE
C          10 IL=IA+MM
C          K=K+MM
C          DMPR 940
C          DMPR 950
C          DMPR 960
C          DMPR 970
C          PERFORM ROW OR COLUMN INTERCHANGE
C          DO 11 J=1,L
C          SAVE=A(IL)
C          A(IL)=A(K)
C          A(K)=SAVE
C          K=K+MMM
C          11 IL=IL+MMM
C          DMPR1000
C          DMPR1010
C          DMPR1020
C          DMPR1030
C          DMPR1040
C          DMPR1050
C          ADDRESS NEXT INTERCHANGE STEP
C          12 IA=IA+ID
C          DMPR1060
C          DMPR1070
C          DMPR1080
C          NORMAL EXIT
C          IER=0
C          RETURN
C          DMPR1090
C          DMPR1100
C          DMPR1110
C          ERROR RETURN IN CASE ITRA IS NOT A TRANSPOSITION VECTOR
C          13 IER=1
C          RETURN
C          DMPR1120
C          DMPR1130
C          DMPR1140
C          DMPR1150
C          DMPR1160
C          ERROR RETURN IN CASE OF ILLEGAL DIMENSIONS
C          14 IER=-1
C          RETURN
C          END
C          DMPR1170
C          DMPR1180
C          DMPR1190
C          DMPR1200

```

```

C          DMPR 10
C          DMPR 20
C          DMPR 30
C          SUBROUTINE DMPRC
C          DMPR 40
C          DMPR 50
C          DMPR 60
C          PURPOSE
C          TO PERMUTE THE ROWS OR COLUMNS OF A GIVEN MATRIX ACCORDING
C          TO A GIVEN TRANSPOSITION VECTOR OR ITS INVERSE. (SEE THE
C          DISCUSSION ON PERMUTATIONS FOR DEFINITIONS AND NOTATION.)
C          DMPR 70
C          DMPR 80
C          DMPR 90
C          DMPR 100
C          USAGE
C          CALL DMPRC(A,M,N,ITRA,INV,IROCO,IER)
C          DMPR 110
C          DMPR 120
C          DMPR 130
C          DESCRIPTION OF PARAMETERS
C          A - GIVEN DOUBLE PRECISION M BY N MATRIX AND RESULTING
C          PERMUTED MATRIX
C          M - NUMBER OF ROWS OF A
C          N - NUMBER OF COLUMNS OF A
C          ITRA - GIVEN TRANSPOSITION VECTOR (DIMENSION M IF ROWS ARE
C          PERMUTED, N IF COLUMNS ARE PERMUTED)
C          INV - INPUT PARAMETER
C          INV NON-ZERO - PERMUTE ACCORDING TO ITRA
C          INV = 0 - PERMUTE ACCORDING TO ITRA INVERSE
C          IROCO - INPUT PARAMETER
C          IROCO NON-ZERO - PERMUTE THE COLUMNS OF A
C          IROCO = 0 - PERMUTE THE ROWS OF A
C          IER - RESULTING ERROR PARAMETER
C          IER = -1 - M AND N ARE NOT BOTH POSITIVE
C          IER = 0 - NO ERROR
C          IER = 1 - ITRA IS NOT A TRANSPOSITION VECTOR ON
C          1,....,M IF ROWS ARE PERMUTED, 1,....,N
C          IF COLUMNS ARE PERMUTED
C          DMPR 240
C          DMPR 250
C          DMPR 260
C          DMPR 270
C          DMPR 280
C          DMPR 290
C          DMPR 300
C          DMPR 310
C          DMPR 320
C          DMPR 330
C          REMARKS
C          (1) IF IER=-1 THERE IS NO COMPUTATION.
C          (2) IF IER= 1, THEN COMPUTATION HAS BEEN UNSUCCESSFUL DUE
C          TO ERROR, BUT THE MATRIX A WILL REFLECT THE ROW OR
C          COLUMN INTERCHANGES PERFORMED BEFORE THE ERROR WAS
C          DETECTED.
C          (3) THE MATRIX A IS ASSUMED TO BE STORED COLUMNWISE.
C          DMPR 340
C          DMPR 350
C          DMPR 360
C          DMPR 370
C          DMPR 380
C          DMPR 390
C          DMPR 400
C          DMPR 410

```


Subroutine MFUN

```

C ..... MFUN 10
C SUBROUTINE MFUN MFUN 20
C MFUN 30
C SUBROUTINE MFUN MFUN 40
C PURPOSE MFUN 50
C APPLY A FUNCTION TO EACH ELEMENT OF A MATRIX TO FORM A MFUN 60
C RESULTANT MATRIX MFUN 70
C USAGE MFUN 80
C CALL MFUN (A,F,R,N,M,MS) MFUN 90
C AN EXTERNAL STATEMENT MUST PRECEDE CALL STATEMENT IN ORDER MFUN 100
C TO IDENTIFY PARAMETER F AS THE NAME OF A FUNCTION MFUN 110
C DESCRIPTION OF PARAMETERS MFUN 120
C A - NAME OF INPUT MATRIX MFUN 130
C F - NAME OF FORTRAN-FURNISHED OR USER FUNCTION SUBPROGRAM MFUN 140
C R - NAME OF OUTPUT MATRIX MFUN 150
C N - NUMBER OF ROWS IN MATRIX A AND R MFUN 160
C M - NUMBER OF COLUMNS IN MATRIX A AND R MFUN 170
C MS - ONE DIGIT NUMBER FOR STORAGE MODE OF MATRIX A (AND R) MFUN 180
C 0 - GENERAL MFUN 190
C 1 - SYMMETRIC MFUN 200
C 2 - DIAGONAL MFUN 210
C REMARKS MFUN 220
C PRECISION IS DEPENDENT UPON PRECISION OF FUNCTION USED MFUN 230
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED MFUN 240
C LOC MFUN 250
C METHOD MFUN 260
C FUNCTION F IS APPLIED TO EACH ELEMENT OF MATRIX A MFUN 270
C TO FORM MATRIX R MFUN 280
C ..... MFUN 290
C SUBROUTINE MFUN(A,F,R,N,M,MS) MFUN 300
C DIMENSION A(LI,RI) MFUN 310
C COMPUTE VECTOR LENGTH, IT MFUN 320
C CALL LUC(LI,RI,N,M,MS) MFUN 330
C BUILD MATRIX R FOR ANY STORAGE MODE MFUN 340
C DO 5 I=1,IT MFUN 350
C R(I)=F(A(I)) MFUN 360
C RETURN MFUN 370
C ENDFUN MFUN 380
C MFUN 390
C MFUN 400
C MFUN 410
C MFUN 420
C MFUN 430
C MFUN 440
C MFUN 450
C MFUN 460
C MFUN 470
C MFUN 480
C MFUN 490
C MFUN 500

```

Subroutine RECP

```

C ..... RECP 10
C FUNCTION RECP RECP 20
C RECP 30
C PURPOSE RECP 40
C CALCULATE RECIPROCAL OF AN ELEMENT. THIS IS A FORTRAN RECP 50
C FUNCTION SUBPROGRAM WHICH MAY BE USED AS AN ARGUMENT BY RECP 60
C SUBROUTINE MFUN. RECP 70
C USAGE RECP 80
C RECP(E) RECP 90
C DESCRIPTION OF PARAMETERS RECP 100
C E - MATRIX ELEMENT RECP 110
C REMARKS RECP 120
C RECIPROCAL OF ZERO IS TAKEN TO BE 1.0E75 RECP 130
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED RECP 140
C NONE RECP 150
C METHOD RECP 160
C RECIPROCAL OF ELEMENT E IS PLACED IN RECP RECP 170
C ..... RECP 180
C FUNCTION RECP(E) RECP 190
C DIG=1.0E75 RECP 200
C TEST ELEMENT FOR ZERO RECP 210
C IF(E) 1,2,1 RECP 220
C IF NON-ZERO, CALCULATE RECIPROCAL RECP 230
C 1 RECP=1.0/E RECP 240
C RETURN RECP 250
C IF ZERO, SET EQUAL TO INFINITY RECP 260
C 2 RECP=SIGN(DIG,E) RECP 270
C RETURN RECP 280
C END RECP 290

```

MATHEMATICS

Matrices: Inversion, Systems of Linear Equations and Related Topics

Subroutine MINV

```

C ..... MINV 10
C ..... MINV 20
C ..... MINV 30
C SUBROUTINE MINV MINV 40
C ..... MINV 50
C PURPOSE MINV 60
C INVERT A MATRIX MINV 70
C ..... MINV 80
C USAGE MINV 90
C CALL MINV(A,N,D,L,M) MINV 100
C ..... MINV 110
C DESCRIPTION OF PARAMETERS MINV 120
C A - INPUT MATRIX, DESTROYED IN COMPUTATION AND REPLACED BY MINV 130
C RESULTANT INVERSE. MINV 140
C N - ORDER OF MATRIX A. MINV 150
C D - RESULTANT DETERMINANT. MINV 160
C L - WORK VECTOR OF LENGTH N. MINV 170
C M - WORK VECTOR OF LENGTH N. MINV 180
C ..... MINV 190
C REMARKS MINV 200
C MATRIX A MUST BE A GENERAL MATRIX. MINV 210
C ..... MINV 220
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED MINV 230
C NONE. MINV 240
C ..... MINV 250
C METHOD MINV 260
C THE STANDARD GAUSS-JORDAN METHOD IS USED. THE DETERMINANT MINV 270
C IS ALSO CALCULATED. A DETERMINANT OF ZERO INDICATES THAT MINV 280
C THE MATRIX IS SINGULAR. MINV 290
C ..... MINV 300
C ..... MINV 310
C SUBROUTINE MINV(A,N,D,L,M) MINV 320
C DIMENSION A(L),L(L),M(L) MINV 330
C ..... MINV 340
C ..... MINV 350
C ..... MINV 360
C ..... MINV 370
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE MINV 380
C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION MINV 390
C STATEMENT WHICH FOLLOWS. MINV 400
C ..... MINV 410
C DOUBLE PRECISION A(D),BIGA,HOLD MINV 420
C ..... MINV 430
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS MINV 440
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS MINV 450
C ROUTINE. MINV 460
C ..... MINV 470
C THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO MINV 480
C CONTAIN DOUBLE PRECISION FORTRAN FUNCTIONS. ABS IN STATEMENT MINV 490
C 10 MUST BE CHANGED TO DABS. MINV 500
C ..... MINV 510
C ..... MINV 520
C SEARCH FOR LARGEST ELEMENT MINV 530
C ..... MINV 540
C D=1.0 MINV 550
C NK=N MINV 560
C DO 80 K=1,N MINV 570
C NK=NK+N MINV 580
C L(K)=K MINV 590
C M(K)=K MINV 600
C KK=NK+K MINV 610
C BIGA=A(KK) MINV 620
C DO 20 J=K,N MINV 630
C IZ=N(J-1) MINV 640
C DO 20 I=K,N MINV 650
C IJ=IZ+I MINV 660
C IF( ABS(A(IJ))- ABS(A(IJ1)) 15,20,20 MINV 680
C 15 BIGA=A(IJ) MINV 690
C L(K)=I MINV 700
C M(K)=J MINV 710
C 25 CONTINUE MINV 720
C ..... MINV 730
C INTERCHANGE ROWS MINV 740
C ..... MINV 750
C J=L(K) MINV 760
C IF(J-K) 35,35,25 MINV 770
C 25 KI=K-N MINV 780
C DO 30 I=1,N MINV 790
C KI=KI+I MINV 800
C HOLD=A(KI) MINV 810
C JI=KI-K+J MINV 820
C A(KI)=A(JI) MINV 830
C 30 A(JI)=HOLD MINV 840
C ..... MINV 850
C INTERCHANGE COLUMNS MINV 860
C ..... MINV 870
C 35 I=M(K) MINV 880
C IF(I-K) 45,45,35 MINV 890
C 35 JP=N(I-1) MINV 900
C DO 40 J=1,N MINV 910
C JK=NK+J MINV 920
C JI=JP+J MINV 930
C HOLD=A(JK) MINV 940
C A(JK)=A(JI) MINV 950
C 40 A(JI)=HOLD MINV 960
C ..... MINV 970
C DIVIDE COLUMN BY MINUS PIVOT (VALUE OF PIVOT ELEMENT IS MINV 980
C CONTAINED IN BIGA) MINV 990
C ..... MINV1000
C 45 IF(A(JA) 45,45,45 MINV1010
C 45 JC=1 MINV1020
C RETURN MINV1030
C ..... MINV1040
C DO 55 I=1,N MINV1050
C IF(I-K) 50,55,50 MINV1060
C IK=NK+I MINV1070
C HOLD=A(IK) MINV1080
C 55 CONTINUE MINV1090
C ..... MINV1100
C REDUCE MATRIX MINV1110
C ..... MINV1120
C DO 55 I=1,N MINV1130
C IK=NK+I MINV1140
C HOLD=A(IK) MINV1150
C IJ=I-1

```

```

MINV1160
MINV1170
MINV1180
MINV1190
MINV1200
MINV1210
MINV1220
MINV1230
MINV1240
MINV1250
MINV1260
MINV1270
MINV1280
MINV1290
MINV1300
MINV1310
MINV1320
MINV1330
MINV1340
MINV1350
MINV1360
MINV1370
MINV1380
MINV1390
MINV1400
MINV1410
MINV1420
MINV1430
MINV1440
MINV1450
MINV1460
MINV1470
MINV1480
MINV1490
MINV1500
MINV1510
MINV1520
MINV1530
MINV1540
MINV1550
MINV1560
MINV1570
MINV1580
MINV1590
MINV1600
MINV1610
MINV1620
MINV1630
MINV1640
MINV1650
MINV1660
MINV1670
MINV1680

```

Subroutines SINV and DSINV

These subroutines invert a given symmetric positive definite matrix, using factorization by subroutines MFSD and DMFSD.

1. Mathematical background

Given an n by n symmetric positive definite matrix A, an upper triangular matrix $R = (r_{ij})$ exists such that

$$A = R^T R$$

Then $A^{-1} = R^{-1}(R^{-1})^T$. The elements \bar{r}_{ik} of R^{-1} are computed using the following recursive formulas:

$$\bar{r}_{ik} = -(1/r_{ii}) \left(\sum_{m=i+1}^k r_{im} \bar{r}_{mk} \right) \quad i < k$$

$$\bar{r}_{ik} = 1/r_{ii} \quad i = k$$

$$\bar{r}_{ik} = 0 \quad i > k$$

2. Programming considerations

The given symmetric positive definite matrix A is stored columnwise in compressed form, that is, only the upper triangular part in $\frac{n(n+1)}{2}$ successive storage locations.

Subroutine MFSD (DMFSD), which is called internally, returns the elements r_{ik} ($i \leq k$) of the upper triangular matrix R in the storage locations of A. The inverse (upper) triangular matrix R^{-1} and at last the resultant upper triangular part of the inverse matrix A^{-1} are calculated and stored columnwise in the same storage locations.

If any calculated radicand r_{kk}^2 ($k = 1, 2, 3, \dots, N$) is not positive, further calculation is bypassed, and the error parameter IER is set to -1. This means that matrix A is not positive definite, possibly due to roundoff errors. IER is also set to -1 if the input parameter N is less than one.

Let all radicands be positive, and let r_{kk}^2 be the first radicand which is no longer greater than the internal tolerance $TOL = |\text{EPS} \cdot a_{kk}|$. The subroutine gives the warning $\text{IER} = k-1$; however, calculation is continued. The warning indicates that there may be loss of significance at factorization step k due to loss of significant digits in the calculation of r_{kk}^2 .

```

C SINV 10
C ----- SINV 20
C SUBROUTINE SINV SINV 30
C SINV 40
C PURPOSE SINV 50
C INVERT A GIVEN SYMMETRIC POSITIVE DEFINITE MATRIX SINV 60
C SINV 70
C USAGE SINV 80
C CALL SINV(A,N,EPS,IER) SINV 90
C SINV 100
C DESCRIPTION OF PARAMETERS SINV 110
C SINV 120
C A - UPPER TRIANGULAR PART OF THE GIVEN SYMMETRIC SINV 130
C POSITIVE DEFINITE N BY N COEFFICIENT MATRIX. SINV 140
C ON RETURN A CONTAINS THE RESULTANT UPPER SINV 150
C TRIANGULAR MATRIX. SINV 160
C N - THE NUMBER OF ROWS (COLUMNS) IN GIVEN MATRIX. SINV 170
C EPS - AN INPUT CONSTANT WHICH IS USED AS RELATIVE SINV 180
C TOLERANCE FOR TEST ON LOSS OF SIGNIFICANCE. SINV 190
C IER - RESULTING ERROR PARAMETER CODED AS FOLLOWS SINV 200
C IER=0 - NO ERROR SINV 210
C IER=-1 - NO RESULT BECAUSE OF WRONG INPUT PARAME- SINV 220
C TER N OR BECAUSE SOME RADICAND IS NON- SINV 230
C POSITIVE (MATRIX A IS NOT POSITIVE SINV 240
C DEFINITE, POSSIBLY DUE TO LOSS OF SIGNI- SINV 250
C FICANCE) SINV 260
C IER=K - WARNING WHICH INDICATES LOSS OF SIGNIFI- SINV 270
C CANCE. THE RADICAND FORMED AT FACTORIZA- SINV 280
C TION STEP K+1 WAS STILL POSITIVE BUT NO SINV 290
C LONGER GREATER THAN ABS(EPS*(K+1,K+1)). SINV 300
C SINV 310
C REMARKS SINV 320
C THE UPPER TRIANGULAR PART OF GIVEN MATRIX IS ASSUMED TO BE SINV 330
C STORED COLUMNWISE IN N*(N+1)/2 SUCCESSIVE STORAGE LOCATIONS. SINV 340
C IN THE SAME STORAGE LOCATIONS THE RESULTING UPPER TRIANGU- SINV 350
C LAR MATRIX IS STORED COLUMNWISE TOO. SINV 360
C THE PROCEDURE GIVES RESULTS IF N IS GREATER THAN 0 AND ALL SINV 370
C CALCULATED RADICANDS ARE POSITIVE. SINV 380
C SINV 390
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED SINV 400
C MFSD SINV 410
C SINV 420
C METHOD SINV 430
C SOLUTION IS DONE USING THE FACTORIZATION BY SUBROUTINE MFSD. SINV 440
C SINV 450
C ----- SINV 460
C SUBROUTINE SINV(A,N,EPS,IER) SINV 470
C SINV 480
C DIMENSION A(1) SINV 490
C DOUBLE PRECISION DIN,WORK SINV 500
C SINV 510
C SINV 520
C SINV 530
C FACTORIZE GIVEN MATRIX BY MEANS OF SUBROUTINE MFSD SINV 540
C A = TRANSPOSE(I) * T SINV 550
C (CALL MFSD(A,N,EPS,IER) SINV 560
C IFT(IER) 9,1,1 SINV 570
C SINV 580
C INVERT UPPER TRIANGULAR MATRIX T SINV 590
C PREPARE INVERSION-LOOP SINV 600
C 1 IPIV=N*(N+1)/2 SINV 610
C IND=IPIV SINV 620
C SINV 630
C INITIALIZE INVERSION-LOOP SINV 640
C DO 6 I=1,N SINV 650
C DIN=1.00/DBLE(A(IPIV)) SINV 660
C A(IPIV)=DIN SINV 670
C MIN=N SINV 680
C KEND=I-1 SINV 690
C LAMF=N-KEND SINV 700
C IF(KEND) 5,5,2 SINV 710
C 2 J=IND SINV 720
C SINV 730
C INITIALIZE POW-LOOP SINV 740
C DO 4 K=1,KEND SINV 750
C WORK=0.00 SINV 760
C MIN=MIN-1 SINV 770
C LHOR=IPIV SINV 780
C LVER=J SINV 790
C SINV 800
C START INNER LOOP SINV 810
C DO 3 L=LAMF,MIN SINV 820
C LVER=LVER+1 SINV 830
C LWOR=LHOR+L SINV 840
C 3 WORK=WORK+DBLE(A(LVER))*A(LHOR)) SINV 850
C END OF INNER LOOP SINV 860
C SINV 870
C A(J)=-WORK*DIN SINV 880
C 4 J=J-MIN SINV 890
C END OF ROW-LOOP SINV 900
C SINV 910
C 5 IPIV=IPIV-MIN SINV 920
C 6 IND=IND-1 SINV 930
C END OF INVERSION-LOOP SINV 940
C SINV 950
C CALCULATE INVERSE(A) BY MEANS OF INVERSE(T) SINV 960
C INVERSE(A) = INVERSE(T) * TRANSPOSE(INVERSE(T)) SINV 970
C INITIALIZE MULTIPLICATION-LOOP SINV 980
C DO 8 I=1,N SINV 990
C IPIV=IPIV+I SINV 1000
C J=IPIV SINV 1010
C SINV 1020
C INITIALIZE ROW-LOOP SINV 1030
C DO 8 K=1,N SINV 1040
C WORK=0.00 SINV 1050
C LHOR=J SINV 1060
C SINV 1070
C START INNER LOOP SINV 1080
C DO 7 L=K,N SINV 1090
C LVER=LHOR+K-I SINV 1100
C WORK=WORK+DBLE(A(LHOR))*A(LVER)) SINV 1110
C 7 LHOR=LHOR+L SINV 1120
C END OF INNER LOOP SINV 1130
C SINV 1140
C A(J)=WORK SINV 1150
C 8 J=J+K SINV 1160
C END OF ROW- AND MULTIPLICATION-LOOP SINV 1170
C SINV 1180
C 9 RETURN SINV 1190
C END SINV 1200

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C ..... DSIN 10
C ..... DSIN 20
C ..... DSIN 30
C ..... DSIN 40
C ..... DSIN 50
C ..... DSIN 60
C ..... DSIN 70
C ..... DSIN 80
C ..... DSIN 90
C ..... DSIN 100
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C ..... DSIN 680
C ..... DSIN 690
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C ..... DSIN 720
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C ..... DSIN 750
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C ..... DSIN 780
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C ..... DSIN1080
C ..... DSIN1090
C ..... DSIN1100
C ..... DSIN1120
C ..... DSIN1130
C ..... DSIN1140
C ..... DSIN1150
C ..... DSIN1160
C ..... DSIN1170
C ..... DSIN1180
C ..... DSIN1190
C ..... DSIN1200
C ..... DSIN1210
C ..... DSIN1220
C ..... DSIN1230
C ..... DSIN1240

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Subroutine SIMQ

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C ..... SIMQ 10
C ..... SIMQ 20
C ..... SIMQ 30
C ..... SIMQ 40
C ..... SIMQ 50
C ..... SIMQ 60
C ..... SIMQ 70
C ..... SIMQ 80
C ..... SIMQ 90
C ..... SIMQ 100
C ..... SIMQ 110
C ..... SIMQ 120
C ..... SIMQ 130
C ..... SIMQ 140
C ..... SIMQ 150
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C ..... SIMQ 170
C ..... SIMQ 180
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C ..... SIMQ 200
C ..... SIMQ 210
C ..... SIMQ 220
C ..... SIMQ 230
C ..... SIMQ 240
C ..... SIMQ 250
C ..... SIMQ 260
C ..... SIMQ 270
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C ..... SIMQ 300
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C ..... SIMQ 610
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C ..... SIMQ 820
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C ..... SIMQ1080
C ..... SIMQ1090
C ..... SIMQ1100
C ..... SIMQ1110
C ..... SIMQ1120
C ..... SIMQ1130
C ..... SIMQ1140
C ..... SIMQ1150
C ..... SIMQ1160
C ..... SIMQ1170
C ..... SIMQ1180
C ..... SIMQ1190
C ..... SIMQ1200
C ..... SIMQ1210
C ..... SIMQ1220

```

Subroutines GELG and DGELG

These subroutines solve a system of general simultaneous linear equations by Gauss elimination. Consider the system of general simultaneous linear equations:

$$A * X = R \tag{1}$$

with an m by m coefficient matrix A and an m by n right-hand side matrix R both stored columnwise. Solution is done by means of Gauss elimination with complete pivoting. If matrix R is the identity matrix, solution X is the inverse of matrix A. The solution X is generated in matrix R. Thus, the computation of the solution requires no additional storage requirements.

Explicitly, the given system (1) is of the form:

$$\begin{pmatrix} a_{11} & a_{12} & \dots & a_{1m} \\ a_{21} & a_{22} & \dots & a_{2m} \\ \dots & \dots & \dots & \dots \\ a_{m1} & a_{m2} & \dots & a_{mm} \end{pmatrix} * \begin{pmatrix} x_{11} & x_{12} & \dots & x_{1n} \\ x_{21} & x_{22} & \dots & x_{2n} \\ \dots & \dots & \dots & \dots \\ x_{m1} & x_{m2} & \dots & x_{mn} \end{pmatrix} = \begin{pmatrix} r_{11} & r_{12} & \dots & r_{1n} \\ r_{21} & r_{22} & \dots & r_{2n} \\ \dots & \dots & \dots & \dots \\ r_{m1} & r_{m2} & \dots & r_{mn} \end{pmatrix} \tag{2}$$

The first step is to search the whole matrix A for the element of greatest absolute value, say a_{ij} , and to select it as first pivot ($p = a_{ij}$). With a_{ij} , generate the internal absolute tolerance for testing loss of significance in the following way:

$$tol = |a_{ij}| * \epsilon$$

with a given relative tolerance ϵ .

Suppose that pivot a_{ij} is equal to a_{11} . If it is not, interchange the first rows of matrices A and R with the i^{th} , and the first column of matrix A with the j^{th} , and save column interchange information by storing the difference $(j-1)$ of pivot column index j and step counter $k = 1$ [interchanging column 1 with column j means interchanging of variables x_{11} with x_{1j} ($l = 1, 2, \dots, n$)].

Now transform the elements of pivot rows in matrices A and R by multiplying with $1/p$, and the other elements by adding $-a_{\nu 1}$ times the new first rows of these two matrices to the other ν rows, thus getting:

$$a_{1l}^{(1)} = + \frac{a_{1l}}{p} \quad (l = 2, 3, \dots, m) \tag{4}$$

$$r_{1l}^{(1)} = + \frac{r_{1l}}{p} \quad (l = 1, 2, \dots, n) \tag{5}$$

$$a_{\nu l}^{(1)} = a_{\nu l} - a_{\nu 1} \cdot a_{1l}^{(1)} \quad (l = 2, 3, \dots, m; \nu = 2, 3, \dots, m) \tag{6}$$

$$r_{\nu l}^{(1)} = r_{\nu l} - a_{\nu 1} \cdot r_{1l}^{(1)} \quad (l = 1, 2, \dots, n; \nu = 2, 3, \dots, m) \tag{7}$$

If column interchange information is saved in the first position of the main diagonal, the result of the first step is the two matrices:

$$A^{(1)} = \begin{pmatrix} (j-1) a_{12}^{(1)} & a_{13}^{(1)} & \dots & a_{1m}^{(1)} \\ 0 & a_{22}^{(1)} & a_{23}^{(1)} & \dots & a_{2m}^{(1)} \\ 0 & a_{32}^{(1)} & a_{33}^{(1)} & \dots & a_{3m}^{(1)} \\ \dots & \dots & \dots & \dots & \dots \\ 0 & a_{m2}^{(1)} & a_{m3}^{(1)} & \dots & a_{mm}^{(1)} \end{pmatrix} \text{ and}$$

$$R^{(1)} = \begin{pmatrix} r_{11}^{(1)} & r_{12}^{(1)} & \dots & r_{1n}^{(1)} \\ r_{21}^{(1)} & r_{22}^{(1)} & \dots & r_{2n}^{(1)} \\ \dots & \dots & \dots & \dots \\ r_{m1}^{(1)} & r_{m2}^{(1)} & \dots & r_{mn}^{(1)} \end{pmatrix}$$

Now repeat this procedure $m-2$ times, starting at each step with the matrix $A^{(k)}$ of the step before

without first k rows and first k columns, and the matrix $R^{(k)}$ without first k rows. The total result after $m-1$ steps is the matrices:

$$A^{(m-1)} = \begin{pmatrix} (j_1-1) & a_{12}^{(1)} & a_{13}^{(1)} & \dots & a_{1m}^{(1)} \\ 0 & (j_2-2) & a_{23}^{(2)} & \dots & a_{2m}^{(2)} \\ 0 & 0 & (j_3-3) & \dots & a_{3m}^{(3)} \\ \dots & \dots & \dots & \dots & \dots \\ 0 & 0 & 0 & \dots & (j_m-m) \end{pmatrix} \quad \text{and}$$

$$R^{(m-1)} = \begin{pmatrix} r_{11}^{(1)} & r_{12}^{(1)} & \dots & r_{1n}^{(1)} \\ r_{21}^{(2)} & r_{22}^{(2)} & \dots & r_{2n}^{(2)} \\ r_{31}^{(3)} & r_{32}^{(3)} & \dots & r_{3n}^{(3)} \\ \dots & \dots & \dots & \dots \\ r_{m1}^{(m)} & r_{m2}^{(m)} & \dots & r_{mn}^{(m)} \end{pmatrix}$$

Now work backward and set:

$$r_{m-1,l}^{(m)} = r_{m-1,l}^{(m-1)} - a_{m-1,m}^{(m-1)} \cdot r_{m,l}^{(m)} \quad (l = 1, 2, \dots, n)$$

$$r_{m-2,l}^{(m)} = r_{m-2,l}^{(m-2)} - a_{m-2,m-1}^{(m-2)} \cdot r_{m-1,l}^{(m)} - a_{m-2,m}^{(m-2)} \cdot r_{m,l}^{(m)} \quad (l = 1, 2, \dots, n)$$

.....

$$r_{1,l}^{(m)} = r_{1,l}^{(1)} - a_{12}^{(1)} \cdot r_{2,l}^{(m)} - a_{13}^{(1)} \cdot r_{3,l}^{(m)} - \dots - a_{1m}^{(1)} \cdot r_{m,l}^{(m)} \quad (l = 1, 2, \dots, n) \quad (8)$$

After each step of back substitution, rows of solution matrix $X = R^{(m)}$ have to be back-interchanged according to interchange information in the corresponding main diagonal element of matrix $A^{(m-1)}$, in order to get the correct sequence of right-hand side column elements $r_{ij}^{(m)}$ corresponding to the sequence of left-hand side column elements $a_{ij}^{(j)}$.

The only case in which the above procedure can fail to give a solution occurs when at any step all elements of the rest-matrix of $A^{(k)}$ become zero, and no pivot element can be found. In this case the procedure is bypassed, and the error message $ier = -1$ is given. Actually, because of rounding errors, a further check of the absolute values of pivot elements is performed by the procedure. If at elimination step k this absolute value becomes less than tol (see equation 3), it is likely that matrix A is singular too. But as this is not necessarily the case, and as this test depends highly on the choice of the relative tolerance ϵ^+ , the procedure gives only the warning $ier = k-1$, indicating that there is a possible loss of significance in the results computed by the algorithm⁺⁺. In case of a well scaled matrix A and an appropriate choice of the relative tolerance, warning $ier = k-1$ may be interpreted to mean that matrix A has the rank $k-1$. If there is only one equation to solve ($m=1$), the test on loss of significance is suppressed.

+For subroutine GELG, a relative tolerance ϵ between 10^{-6} and 10^{-7} is suggested; and for subroutine DGELG, between 10^{-14} and 10^{-16} .

++For example, $\epsilon = 10^{-5}$ and warning $ier = 3$ mean that there is a possible loss of about five or more significant digits in the initial values of elimination step 4, and that matrix A seems to have the rank 3.

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C ..... GELG 950
C ..... GELG 960
C ..... GELG 970
C ..... GELG 980
C ..... GELG 990
C ..... GELG 1000

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C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NAME
C
C METHOD
C SOLUTION IS DONE BY MEANS OF GAUSS-ELIMINATION WITH
C COMPLETE PIVOTING.
C
C .....
C SUBROUTINE UGELG(R,A,M,N,EPS,IER)
C
C DIMENSION A(11,11)
C IFM(12,23)
C
C SEARCH FOR GREATEST ELEMENT IN MATRIX A
1 DO 10 I=1,M
  PIV=0
  K=I
  N=N+1
  DO 3 L=1,N
    T=ABS(A(I,L))
    IF(T>PIV)3,2
2 PIV=T
  I=L
3 CONTINUE
  TOL=EPS*PIV
  A(I) IS PIVOT ELEMENT. PIV CONTAINS THE ABSOLUTE VALUE OF A(I).
C
C START ELIMINATION LOOP
LST=1
DO 17 K=1,M
C
C TEST ON SINGULARITY
IF(PIV)2,2,4
4 IF(IER)7,5,7
5 IF(PIV-TOL)6,6,7
6 IER=K-1
7 PIV=1./A(I)
  J=(I-1)/M
  I=I-J*M
  J=J+1
  I* K IS ROW-INDEX, J* K COLUMN-INDEX OF PIVOT ELEMENT
C
C PIVOT ROW REDUCTION AND ROW INTERCHANGE IN RIGHT HAND SIDE R
DO 8 L=K,M,N
  LL=L+1
  TB=PIV*A(ILL)
  A(ILL)=A(II)
  A(II)=TB
9 A(II)=TB
C
C IS ELIMINATION TERMINATED
IF(K-M)9,10,10
C
C COLUMN INTERCHANGE IN MATRIX A
LEND=LST+M-K
IF(J)11,12,10
10 II=J*M
  DO 11 L=LST,LEND
    TB=A(II)
    LL=L+1
    A(II)=A(ILL)
    A(ILL)=TB
C
C ROW INTERCHANGE AND PIVOT ROW REDUCTION IN MATRIX A
DO 13 L=LST,M+M
  LL=L+1
  TB=PIV*A(ILL)
  A(ILL)=A(II)
  A(II)=TB
C
C SAVE COLUMN INTERCHANGE INFORMATION
A(LST)=J
C
C ELEMENT REDUCTION AND NEXT PIVOT SEARCH
PIV=0
LST=LST+1
J=0
DO 15 II=LST,LEND
  PIV=A(II)
  I=II+1
  I=I+M
  J=J+1
  DO 15 L=LST,M+M
    LL=L+1
    A(L)=A(L)+PIV*A(ILL)
    TB=A(L)
    A(L)=A(ILL)
    A(ILL)=TB
14 PIV=TB
  I=L
15 CONTINUE
  DO 16 L=L+1,M+M
    LL=L+1
    A(LLL)=A(LLL)+PIV*A(ILL)
17 LST=LST+M
  END OF ELIMINATION LOOP
C
C
C
C BACK SUBSTITUTION AND BACK INTERCHANGE
18 IFM=112+22+19
19 I=M+M
  LST=M+1
  DO 21 I=2,M
    II=LST-1
    I=I-1
    LST=LST-1
    L=LST+M
    A(L)=A(L)+A(II)*A(LLL)
    TB=A(L)
    A(L)=A(II)
    A(II)=TB
  DO 20 K=I,M+M
    LL=L+1
    TB=TB+A(K)*A(LLL)
    A(K)=A(K)+A(L)*A(LLL)
21 A(K)=TB
22 RETURN
C
C
C ERROR RETURN
23 IER=-1
  RETURN
  END

```

```

C .....
C SUBROUTINE UGELG
C PURPOSE
C TO SOLVE A GENERAL SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS.
C USAGE
C CALL UGELG(R,A,M,N,EPS,IER)
C DESCRIPTION OF PARAMETERS
C R - DOUBLE PRECISION M BY N RIGHT HAND SIDE MATRIX
  (DESTROYED). ON RETURN R CONTAINS THE SOLUTIONS
  OF THE EQUATIONS.
C A - DOUBLE PRECISION M BY A COEFFICIENT MATRIX
  (DESTROYED).
C M - THE NUMBER OF EQUATIONS IN THE SYSTEM.
C N - THE NUMBER OF RIGHT HAND SIDE VECTORS.
C EPS - SINGLE PRECISION INPUT CONSTANT WHICH IS USED AS
  RELATIVE TOLERANCE FOR TEST ON LOSS OF
  SIGNIFICANCE.
C IER - RESULTING ERROR PARAMETER CODED AS FOLLOWS
  IER=0 - NO ERROR.
  IER=-1 - NO RESULT BECAUSE OF M LESS THAN 1 OR
  PIVOT ELEMENT AT ANY ELIMINATION STEP
  EQUAL TO 0.
  IER=K - WARNING DUE TO POSSIBLE LOSS OF SIGNIFI-
  CANCE INDICATED AT ELIMINATION STEP K+1,
  WHERE PIVOT ELEMENT WAS LESS THAN OR
  EQUAL TO THE INTERNAL TOLERANCE EPS TIMES
  ABSOLUTELY GREATEST ELEMENT OF MATRIX A.
C REMARKS
C INPUT MATRICES R AND A ARE ASSUMED TO BE STORED COLUMNWISE
  IN MAIN RESP. MM SUCCESSIVE STORAGE LOCATIONS. ON RETURN
  SOLUTION MATRIX R IS STORED COLUMNWISE TOO.
C THE PROCEDURE GIVES RESULTS IF THE NUMBER OF EQUATIONS M IS
  GREATER THAN 0 AND PIVOT ELEMENTS AT ALL ELIMINATION STEPS
  ARE DIFFERENT FROM 0. HOWEVER WARNING IER=K - IF GIVEN -
  INDICATES POSSIBLE LOSS OF SIGNIFICANCE. IN CASE OF A WELL
  SCALED MATRIX A AND APPROPRIATE TOLERANCE EPS, IER=K MAY BE
  INTERPRETED THAT MATRIX A HAS THE RANK K. NO WARNING IS
  GIVEN IN CASE M=1.
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C METHOD
C SOLUTION IS DONE BY MEANS OF GAUSS-ELIMINATION WITH
  COMPLETE PIVOTING.
C .....
C SUBROUTINE UGELG(R,A,M,N,EPS,IER)
C
C DIMENSION A(11,11)
C DOUBLE PRECISION R,A,PIV,TB,TOL,PIV1
C IFM(12,23)
C
C SEARCH FOR GREATEST ELEMENT IN MATRIX A
1 IER=0
  PIV=0
  K=I
  N=N+1
  DO 3 L=1,N
    T=ABS(A(I,L))
    IF(T>PIV)3,2
2 PIV=T
  I=L
3 CONTINUE
  TOL=EPS*PIV
  A(I) IS PIVOT ELEMENT. PIV CONTAINS THE ABSOLUTE VALUE OF A(I).
C
C START ELIMINATION LOOP
LST=1
DO 17 K=1,M
C
C TEST ON SINGULARITY
IF(PIV)2,2,4
4 IF(IER)7,5,7
5 IF(PIV-TOL)6,6,7
6 IER=K-1
7 PIV=1./A(I)
  J=(I-1)/M
  I=I-J*M
  J=J+1
  I* K IS ROW-INDEX, J* K COLUMN-INDEX OF PIVOT ELEMENT
C
C PIVOT ROW REDUCTION AND ROW INTERCHANGE IN RIGHT HAND SIDE R
DO 8 L=K,M,N
  LL=L+1
  TB=PIV*A(ILL)
  A(ILL)=A(II)
  A(II)=TB
9 A(II)=TB
C
C SAVE COLUMN INTERCHANGE INFORMATION
A(LST)=J
C
C ELEMENT REDUCTION AND NEXT PIVOT SEARCH
PIV=0
LST=LST+1
J=0
DO 15 II=LST,LEND
  PIV=A(II)
  I=II+1
  I=I+M
  J=J+1
  DO 15 L=LST,M+M
    LL=L+1
    A(L)=A(L)+PIV*A(ILL)
    TB=A(L)
    A(L)=A(II)
    A(II)=TB
14 PIV=TB
  I=L
15 CONTINUE
  DO 16 L=L+1,M+M
    LL=L+1
    A(LLL)=A(LLL)+PIV*A(ILL)
17 LST=LST+M
  END OF ELIMINATION LOOP
C
C
C
C BACK SUBSTITUTION AND BACK INTERCHANGE
18 IFM=112+22+19
19 I=M+M
  LST=M+1
  DO 21 I=2,M
    II=LST-1
    I=I-1
    LST=LST-1
    L=LST+M
    A(L)=A(L)+A(II)*A(LLL)
    TB=A(L)
    A(L)=A(II)
    A(II)=TB
  DO 20 K=I,M+M
    LL=L+1
    TB=TB+A(K)*A(LLL)
    A(K)=A(K)+A(L)*A(LLL)
21 A(K)=TB
22 RETURN
C
C
C ERROR RETURN
23 IER=-1
  RETURN
  END

```

```

      GO 15 L=IST,MM,M
      LL=L+J
      A(L)=A(L)+PIV*ALL
      TB=JABS(ALL)
      IF(TB=PIV)ID=ID+1
14  PIV=TB
      I=K
15  CONTINUE
      GO 15 L=K+MM,M
      LL=L+J
16  K=LL+R(LL)+PIV*(K+L)
17  LST=LST+M
      END OF ELIMINATION LOOP
C
C
C
C
      BACK SUBSTITUTION AND BACK INTERCHANGE
18  IF(I=1)Z=Z+1
19  LST=MM,M
      LST=M+1
      GO 24 I=Z+M
      II=LST-1
      ISF=ISF-LST
      L=I+ST-M
      LRA(L)=Z
      GO 21 J=II,MM,M
      TB=R(L)
      LL=L
      GO 20 K=I+ST,MM,M
      LL=LL+1
20  TB=TB-A(K)*R(LL)
      K=K+1
      K(L)=R(K)
21  R(K)=TB
22  RETURN
C
C
C
      ERR=0, RETURN
23  IER=1
      RETURN
      END

```

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Subroutine RSLMC

This subroutine computes an approximate solution to a system of linear equations when the coefficient matrix has been factored into a product of two triangular matrices.

1. Mathematical background

Consider a system of linear equations

$$Ax = b \tag{1}$$

having a nonsingular coefficient matrix A. There exists a permutation P such that PA = LU, where L is lower triangular with unit diagonal, and U is upper triangular. Putting c = Pb we see that (1) is equivalent to the system

$$\begin{aligned} Ux &= y \\ Ly &= c \end{aligned} \tag{2}$$

Let $x^{(p)}$ be a trial solution of the given system. It can be improved by means of the iterative process

$$\begin{aligned} r^{(p)} &= b - Ax^{(p)} \\ Ad^{(p)} &= r^{(p)} \\ x^{(p+1)} &= x^{(p)} + d^{(p)} \end{aligned} \tag{3}$$

where the correction vector $d^{(p)}$ is computed using L and U as in (2).

If A is not too ill-conditioned, this process will give a satisfactory solution, provided that $r^{(p)}$, the residual vector, is computed with sufficient accuracy.

2. Programming considerations

This routine may be used to solve a nonsingular system of linear equations whose coefficient matrix has been factored by means of subroutine FACTR.

Let $\epsilon > 0$ be a relative precision parameter (input to RSLMC). In the following discussion we use the notation $\|x\| = \sum |x_i|$. The process (3) is applied to the system (1) starting with $x^{(0)} = 0$, and is stopped when one of the following situations occurs:

a. $IER = 0$. The components of the correction vector $d^{(p)}$ satisfy the inequalities

$$\left| d_i^{(p)} \right| \leq \epsilon \left| x_i^{(p)} \right| \quad i = 1, 2, \dots, n. \tag{4}$$

Then $x = x^{(p)}$ is returned as the solution.

b. Assume that $p > 1$, for some i the inequality (4) fails and

$$\|d^{(k)}\| \leq \frac{1}{2} \|d^{(k-1)}\| \quad k = 1, 2, \dots, p-1$$

$$\|d^{(p)}\| > \frac{1}{2} \|d^{(p-1)}\|$$

Then:

$$\text{IER} = 1 \text{ if } \|d^{(p)}\| \leq \epsilon \|x^{(p)}\|,$$

$$\text{IER} = 2 \text{ if } \|d^{(p)}\| > \epsilon \|x^{(p)}\|.$$

c. $\text{IER} = 3$. $\|d^{(1)}\| > \frac{1}{2} \|d^{(0)}\|$. In this case the trial solution is too far from the exact solution and the process cannot converge. In general this happens when A is badly ill-conditioned.

$\text{IER} = 4$. U is singular.

In all cases $x = x^{(p)}$ is returned.

Note: To obtain accuracy in the computation of the residual vector, each component is computed in double-precision arithmetic.

For reference see:

- (1) H. J. Bowdler, R. S. Martin, G. Peters and J. H. Wilkinson, "Solution of Real and Complex Systems of Linear Equations", Numerische Mathematik, vol. 8, no. 3, 1966.
- (2) J. H. Wilkinson, The Algebraic Eigenvalue Problem. Clarendon Press, Oxford, 1965.

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C ..... RSLM 10
C ..... RSLM 20
C ..... RSLM 30
C ..... RSLM 40
C ..... RSLM 50
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C ..... RSLM 70
C ..... RSLM 80
C ..... RSLM 90
C ..... RSLM 100
C ..... RSLM 110
C ..... RSLM 120
C ..... RSLM 130
C ..... RSLM 140
C ..... RSLM 150
C ..... RSLM 160
C ..... RSLM 170
C ..... RSLM 180
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C ..... RSLM 580
C ..... RSLM 590
C ..... RSLM 600
C ..... RSLM 610

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C ..... RSLM 620
C ..... RSLM 630
C ..... RSLM 640
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C ..... RSLM 710
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C ..... RSLM 730
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C ..... RSLM 940
C ..... RSLM 950
C ..... RSLM 960
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C ..... RSLM 980
C ..... RSLM 990
C ..... RSLM 1000

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Subroutine FACTR

This subroutine determines a decomposition of a real nonsingular matrix as a product of a lower triangular matrix with unit diagonal and an upper triangular matrix.

1. Mathematical background

Let A be a real nonsingular matrix of order n. In general, A can be factored into a product of the form $A = LU$, where L is lower triangular with unit diagonal and U is upper triangular.

The elements of L and U may be computed recursively as follows:

$$\bar{a}_{ip} = a_{ip} - \sum_{k=1}^{p-1} l_{ik} u_{kp} \quad i=p, p+1, \dots, n$$

$$l_{ip} = \bar{a}_{ip} / \bar{a}_{pp} \quad i=p, p+1, \dots, n$$

$$u_{pp} = \bar{a}_{pp}$$

$$u_{pj} = a_{pj} - \sum_{k=1}^{p-1} l_{pk} u_{kj} \quad j=p+1, p+2, \dots, n$$

Using these formulas for $p=1, 2, \dots, n$, the decomposition can be carried out in n stages.

2. Programming considerations

Even if A is nonsingular and well-conditioned, the above process can fail when a leading principal submatrix of A is singular; furthermore, the process is numerically unstable whenever a leading principal submatrix is ill-conditioned.

In order to avoid these inconveniences, a technique of partial pivoting combined with an equilibration of the matrix has been built into the algorithm.

Initially, the maximum norm of each row vector is computed:

$$N_p = \max_j |a_{pj}| \quad p=1, 2, \dots, n$$

If any $N_p = 0$, the error parameter IER is set to 3 and further calculations are bypassed. Otherwise the reciprocals $1/N_p$ are computed and stored in the vector PER.

Then, assuming that the first p-1 columns of L and p-1 rows of U have been computed, the pth stage of the factorization process is:

a. Computation of the \bar{a}_{ip} .

$$\bar{a}_{ip} = a_{ip} - \sum_{k=1}^{p-1} l_{ik} u_{kp} \quad i=p, p+1, \dots, n$$

Each term \bar{a}_{ip} replaces the corresponding term of A in storage.

b. Equilibrated partial pivoting.

Let m be the smallest row subscript such that

$$(1/N_p) |\bar{a}_{mp}| = \max_{i \geq p} \left\{ (1/N_i) |\bar{a}_{ip}| \right\}$$

If $\bar{a}_{mp} = 0$, the error message IER = 3 is given and further calculations are bypassed. If $\bar{a}_{mp} \neq 0$, the mth and pth rows of A are interchanged, PER(p) is moved to PER(m), and the number m is stored in PER(p). Thus the first p positions of PER contain the information on the permutations needed so far in the form of a transposition vector.

c. Computation of the pth column of L.

$$l_{ip} = \bar{a}_{ip} / \bar{a}_{pp} \quad i=p+1, p+2, \dots, n$$

These terms of L replace the corresponding terms of A in storage. The diagonal terms of L, which are all equal to 1, are not stored.

d. Computation of the pth row of U

$$u_{pp} = \bar{a}_{pp}$$

$$u_{pj} = a_{pj} - \sum_{k=1}^{p-1} l_{pk} u_{kj} \quad j=p+1, \dots, n$$

These terms replace the corresponding terms of A.

Note: Double-precision arithmetic is used to compute the inner products needed in steps (1) and (4).

For reference see:

- (1) H.J. Bowdler, R.S. Martin, G. Peters, and J.H. Wilkinson, "Solution of Real and Complex Systems of Linear Equations", Numerische Mathematik, vol. 8, no. 3, 1966.
- (2) J.H. Wilkinson, The Algebraic Eigenvalue Problem. Clarendon Press, Oxford, 1965.

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C ..... FCTR 10
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C ..... FCTR 990
C ..... FCTR1000
C ..... FCTR1010
C ..... FCTR1020
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C ..... FCTR1050
C ..... FCTR1060
C ..... FCTR1070
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C ..... FCTR1100
C ..... FCTR1110
C ..... FCTR1120
C ..... FCTR1130
C ..... FCTR1140
C ..... FCTR1150
C ..... FCTR1160
C ..... FCTR1170
C ..... FCTR1180
C ..... FCTR1190
C ..... FCTR1200
C ..... FCTR1210
C ..... FCTR1220
C ..... FCTR1230
C ..... FCTR1240
C ..... FCTR1250
C ..... FCTR1260
C ..... FCTR1270

```

Subroutines MFGR and DMFGR

The following calculations are performed for a general rectangular matrix:

1. Determine rank and linearly independent rows and columns of a given matrix.
2. Express a submatrix of maximal rank as product of triangular factors.
3. Express nonbasic rows in terms of basic ones.
4. Express basic variables in terms of free ones.

1. Theoretical background

Calculation (1) is most critical. It is not claimed that MFGR will give the correct rank in all cases, due to the intrinsic difficulty caused by performing calculations with a finite number of digits.

The rank is determined using the standard Gaussian elimination technique with complete pivoting. This implies that the rows and columns of the given m by n matrix A are interchanged at each elimination step if necessary. The interchange information is recorded in two integer permutation vectors $IROW$ and $ICOL$:

The i^{th} { row } of the interchanged matrix
 { column } corresponds
 to the { $IROW(I)^{\text{th}}$ row } in the original
 { $ICOL(I)^{\text{th}}$ column } matrix A .

Initially $IROW(J) = J$ and $ICOL(J) = J$.

The notation A^i is used for the interchanged matrix implied at the i^{th} elimination step.[†]

a. First elimination step

Let a_{jk} be the absolutely greatest element of matrix A , which is found first in a columnwise scan. The internal tolerance TOL is set equal to $|EPS \cdot a_{jk}|$.

If $|a_{jk}| \leq TOL$, further calculation is bypassed. Otherwise rows i and j and columns l and k of matrix A are interchanged, giving A^1 . The same interchanges must be applied to $IROW$, interpreted as column vector, and to $ICOL$, interpreted as row vector.

A^1 is uniquely expressed as product $L^1 \cdot D^1 \cdot U^1$ by imposing the following conditions:

- (I) U^1 is the n by n identity matrix except for the first row.

[†] Superscripts do not mean powers. They merely indicate the number of the elimination step at which the result is obtained.

- (II) L^1 is the m by m identity matrix except for the first column. The first diagonal element has a value of one.
- (III) D^1 is an m by n matrix with first diagonal element equal to one, while all remaining elements of the first row and column are equal to zero.

Partitioning of matrices A^1 , L^1 , D^1 , U^1 leads to:

$$\begin{pmatrix} a_{11}^1 & A_{12}^1 \\ A_{21}^1 & A_{22}^1 \end{pmatrix} = \begin{pmatrix} 1 & \emptyset \\ L_{21}^1 & I \end{pmatrix} \begin{pmatrix} 1 & \emptyset \\ \emptyset & D_{22}^1 \end{pmatrix} \begin{pmatrix} u_{11}^1 & U_{12}^1 \\ \emptyset & I \end{pmatrix}^\dagger$$

or explicitly:

$$\begin{aligned} a_{11}^1 &= u_{11}^1 \\ A_{12}^1 &= U_{12}^1 \\ A_{21}^1 &= L_{21}^1 \cdot u_{11}^1 \\ A_{22}^1 &= L_{21}^1 U_{12}^1 + D_{22}^1 \end{aligned}$$

This means:

- (I) The elements of the first row of U^1 are
- $$u_{11}^1 = a_{11}^1, \quad u_{12}^1 = a_{12}^1, \dots, \quad u_{1n}^1 = a_{1n}^1$$
- (II) The elements of the first column of L^1 are
- $$l_{11}^1 = 1, \quad l_{21}^1 = a_{21}^1/a_{11}^1, \dots, \quad l_{m1}^1 = a_{m1}^1/a_{11}^1$$
- (III) The elements of submatrix D_{22}^1 of D^1 are

$$d_{ik}^1 = a_{ik}^1 - l_{i1}^1 \cdot u_{1k}^1 = a_{ik}^1 - \frac{a_{i1}^1 a_{1k}^1}{a_{11}^1};$$

$$\begin{aligned} i &= 2, \dots, m \\ k &= 2, \dots, n \end{aligned}$$

† Capital letters are used as notation for matrices or vectors throughout. \emptyset means zero matrix, I means identity matrix; dimensions are implied by compatibility.

Note that it is possible to record all nontrivial entries of L^1 , D^1 , U^1 in the storage locations occupied by the original A , storing only:

$$\begin{pmatrix} u_{11}^1 & U_{12}^1 \\ L_{21}^1 & D_{22}^1 \end{pmatrix}$$

b. Second elimination step

Let d_{jk}^1 , $j \geq 2$, $k \geq 2$ be the absolutely largest element of D_{22}^1 . If $|d_{jk}^1| \leq \text{TOL}$, D_{22}^1 is interpreted as being the zero matrix.

If D_{22}^1 is not zero in the above sense, it may be decomposed analogously. In the compact scheme,

$$\begin{pmatrix} u_{11}^1 & U_{12}^1 \\ L_{21}^1 & D_{22}^1 \end{pmatrix}$$

rows 2 and j and columns 2 and k are interchanged, obtaining:

$$\begin{pmatrix} 1 & U_{12}^2 \\ u_{11}^1 & U_{12}^1 \\ L_{21}^2 & D_{22}^2 \end{pmatrix}$$

The same interchanges must be performed with IROW (interpreted as column vector), with ICOL (interpreted as row vector), and with A^1 giving result A^2 :

$$A^2 = \begin{pmatrix} 1 & \emptyset \\ L_{21}^2 & I \end{pmatrix} \begin{pmatrix} 1 & \emptyset \\ \emptyset & D_{22}^2 \end{pmatrix} \begin{pmatrix} u_{11}^1 & U_{12}^2 \\ \emptyset & I \end{pmatrix}$$

Now D_{22}^2 may be expressed uniquely as the product of the form LDU, imposing conditions I, II, III.

The result is:

$$D_{22}^2 = \begin{pmatrix} 1 & \emptyset \\ L_{32}^2 & I \end{pmatrix} \begin{pmatrix} 1 & \emptyset \\ \emptyset & D_{33}^2 \end{pmatrix} \begin{pmatrix} u_{22}^2 & U_{23}^2 \\ \emptyset & I \end{pmatrix}$$

It is easily seen that $A^2 = L^2 D^2 U^2$,

with:

$$L^2 = \begin{pmatrix} 1 & \emptyset & \emptyset \\ l_{12}^2 & 1 & \emptyset \\ l_{31}^2 & l_{32}^2 & I \end{pmatrix}$$

$$D^2 = \begin{pmatrix} 1 & 0 & \emptyset \\ 0 & 1 & \emptyset \\ \emptyset & \emptyset & D_{33}^2 \end{pmatrix}$$

$$U^2 = \begin{pmatrix} 1 & u_{12}^2 & u_{13}^2 \\ u_{11}^2 & u_{22}^2 & u_{23}^2 \\ 0 & u_{22}^2 & u_{23}^2 \\ \emptyset & \emptyset & I \end{pmatrix}$$

where $L_{21}^2 = \begin{pmatrix} 1 \\ l_{21}^2 \\ l_{31}^2 \end{pmatrix}$, $U_{12}^2 = (u_{12}^2, u_{13}^2)$

c. Final result of elimination process

At the next elimination step D_{33}^2 is factorized, and so on. Now assume that finally $D_{r+1, r+1}^r$ equals zero in the sense that all its elements are absolutely less than TOL. This means that A has the rank r, and the end result is the factorization $A^r = L^r D^r U^r$:

$$A^r = \begin{pmatrix} 1 & 0 & \dots & 0 & \emptyset \\ l_{21}^2 & 1 & \dots & 0 & \emptyset \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ l_{r1}^r & l_{r2}^r & \dots & 1 & \emptyset \\ L_{r+1, 1}^r & L_{r+1, 2}^r & \dots & L_{r+1, r}^r & I \end{pmatrix}$$

$$\begin{pmatrix} 1 & 0 \dots 0 & \emptyset \\ 0 & 1 \dots 0 & \emptyset \\ \vdots & \vdots & \vdots \\ 0 & 0 \dots 1 & \emptyset \\ \emptyset & \emptyset \dots \emptyset & D_{r+1, r+1}^r \end{pmatrix}$$

$$\begin{pmatrix} 1 & u_{12}^2 & \dots & u_{1r}^2 & U_{1, r+1}^r \\ u_{11}^2 & u_{22}^2 & \dots & u_{2r}^2 & U_{2, r+1}^r \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & u_{rr}^2 & U_{r, r+1}^r \\ \emptyset & \emptyset & \dots & \emptyset & I \end{pmatrix}$$

Neglecting the small elements in $D_{r+1, r+1}^r$ this may be written more compactly as:

$$A^r = \begin{pmatrix} L \\ LR \end{pmatrix} \begin{pmatrix} U, UR \end{pmatrix}$$

with: $L = \begin{pmatrix} 1 & 0 \dots 0 \\ l_{21}^2 & 1 & 0 \\ \vdots & \vdots & \vdots \\ l_{r1}^r & l_{r2}^r & \dots 1 \end{pmatrix}$

$$LR = (L_{r+1, 1}^r, L_{r+1, 2}^r, \dots, L_{r+1, r}^r)$$

$$U = \begin{pmatrix} 1 & u_{12}^2 & \dots & u_{1r}^2 \\ u_{11}^2 & u_{22}^2 & \dots & u_{2r}^2 \\ 0 & u_{22}^2 & \dots & u_{2r}^2 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & u_{rr}^2 \end{pmatrix}$$

$$UR = \begin{pmatrix} U_{1, r+1}^r \\ U_{2, r+1}^r \\ \vdots \\ U_{r, r+1}^r \end{pmatrix}$$

L is of dimension r by r and unit lower triangular.

U is of dimension r by r and upper triangular.

LR is of dimension m - r by r; if the given matrix A is row regular (that is, m = r), LR is absent in the final factorization.

UR is of dimension r by n-r; if the given matrix A is column regular (that is, n = r), UR is absent in the final factorization.

d. Further calculations performed

The problem of matrix factorization arises in connection with the solution of systems of equations $AX=R$. Three different cases must be distinguished:

- (1) $r = m = n$
A is nonsingular, and $AX=R$ has a uniquely determined solution.
- (2) $r < m$
A is not row regular; solutions of $AX = R$ exist only if the linear combinations among the rows of A are also valid among the rows of R.

(3) $r < n$

A is not column regular; $AX = \emptyset$ has nontrivial solutions.

The cases (2) and (3) may occur combined.

The solution, if it exists, is uniquely determined if $r = n$; otherwise it contains $n - r$ free parameters. It is quite natural to ask for the linear combinations among the rows of given matrix A and for the linear forms expressing basic variables in terms of free ones. Therefore, instead of LR and UR, matrices C and H are returned, containing linear combinations and homogeneous solutions respectively.

Observe carefully that the calculated factorization belongs to the interchanged matrix A^r . Therefore $A^r X^r = R^r$ is dealt with instead of $AX = R$, where $\begin{Bmatrix} X^r \\ R^r \end{Bmatrix}$ is obtained from $\begin{Bmatrix} X \\ R \end{Bmatrix}$ using the $\begin{Bmatrix} \text{ICOL}(I)^{\text{th}} \\ \text{IROW}(J)^{\text{th}} \end{Bmatrix}$

element of $\begin{Bmatrix} X \\ R \end{Bmatrix}$ as $\begin{Bmatrix} I^{\text{th}} \\ J^{\text{th}} \end{Bmatrix}$ element of

$$\begin{Bmatrix} X^r \\ R^r \end{Bmatrix} ; \begin{matrix} I = 1, \dots, n \\ J = 1, \dots, m \end{matrix}$$

Let X^r, R^r be partitioned into $\begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$ and $\begin{pmatrix} R_1 \\ R_2 \end{pmatrix}$.

Then:

$$\begin{pmatrix} L \\ LR \end{pmatrix} (U, UR) \begin{pmatrix} X_1 \\ X_2 \end{pmatrix} = \begin{pmatrix} R_1 \\ R_2 \end{pmatrix}$$

or explicitly:

$$\begin{aligned} L \cdot U \cdot X_1 + L \cdot UR \cdot X_2 &= R_1 \\ LR \cdot U \cdot X_1 + LR \cdot UR \cdot X_2 &= R_2 \end{aligned}$$

Since L and U are nonsingular, this implies:

$$\begin{aligned} X_1 &= U^{-1} \cdot L^{-1} \cdot R_1 - U^{-1} \cdot UR \cdot X_2 \\ LR \cdot L^{-1} R_1 &= R_2 \end{aligned}$$

For the convenience of the user, LR is replaced by $LR \cdot L^{-1} = C$; UR is replaced by $-U^{-1} UR = H$, while L and U remain untouched. Consistency requires that $R_2 = CR_1$, and homogeneous solutions are given by $X_1 = HX_2$. In case of a consistent system of equations $A^r X^r = R^r$, the general solution is $X^r = \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$ with $X_1 = U^{-1} L^{-1} R_1 + HX_2$,

while the values of the free variables contained in X_2 may be chosen arbitrarily.

2. Format of Results

Subroutine MFGR returns matrices L, U, C, H, D in the storage area originally occupied by the input matrix A in the compact scheme shown in Figure 9.

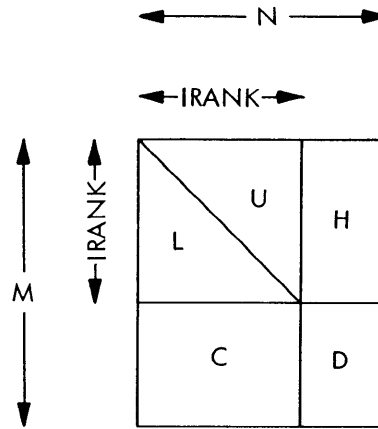


Figure 9. Format scheme (MFGR)

3. Numerical examples

a. Let $A = \begin{pmatrix} 5 & 5 \\ 1 & 1 \end{pmatrix}$, $EPS = 1.0E-7$

Subroutine MFGR returns as results:

$$L = (1), U = (5), C = (0.2), H = (-1.0)$$

combined in the compact scheme:

$$\begin{pmatrix} 5.0 & -1.0 \\ 0.2 & 0.6E-7 \end{pmatrix} = \begin{pmatrix} U & H \\ C & D \end{pmatrix}$$

$$\begin{aligned} \text{IRANK} &= 1 \\ \text{ICOL} &= (1, 2) \\ \text{IROW} &= (1, 2) \end{aligned}$$

The value $0.6E-7$ is obtained instead of the correct value 0, due to roundoff errors.

This example shows that a proper choice of EPS is somewhat greater than 10^{-d} , if d is the number of significant digits in the representation of floating point numbers.

With $EPS = 0$, MFGR would give the incorrect value of 2 for the rank. The choice $EPS = 0$ may well result in an incorrect value less than the correct rank, as shown by the following.

If the element a_{22} is slightly decreased, resulting in a matrix A of correct rank equal to 2, then subroutine MFGR gives an incorrect value of 1 for the rank with any choice of the relative tolerance EPS, even with $EPS = 0$.

b. Let $A = \begin{pmatrix} 1 & 3 & 5 \\ 1 & 3 & 5 \\ 1 & 3 & 1 \\ 1 & 1 & 3 \\ 1 & 3 & 5 \end{pmatrix}$, $EPS = 1.0E-7$


```

C
C
C      INITIALIZE COLUMN INDEX VECTOR
C      SEARCH FIRST PIVOT ELEMENT
C
C      4 IRANK=0
C      PIV=0
C      JJ=0
C      DO 6 J=1,N
C      ICUL(J)=0
C      DO 5 I=1,M
C      JJ=JJ+1
C      HOU=A(JJ)
C      IF(ABS(PIV)-ABS(HOU))>.6*P
C      5 PIV=HOU
C      I=I
C      IC=J
C      6 CONTINUE
C
C      INITIALIZE ROW INDEX VECTOR
C      JJ 7 I=1,M
C      7 IROW(I)=I
C
C      SET UP INTERNAL TOLERANCE
C      TOL=ABS(EPS*PIV)
C
C      INITIALIZE ELIMINATION LOOP
C      NM=NM
C      DO 19 NCOL=M,MM,M
C
C      TEST FOR FEASIBILITY OF PIVOT ELEMENT
C      8 IF(ABS(PIV)-TOL)>.2*P
C
C      UPDATE RANK
C      9 IRANK=IRANK+1
C
C      INTERCHANGE ROWS IF NECESSARY
C      JJ=IRANK
C      IF(JJ<I2+1)
C      10 DO 11 J=IRANK,MM,M
C      I=JJ
C      SAVE=A(JJ)
C      A(JJ)=A(I)
C      A(I)=SAVE
C      11 A(I)=SAVE
C
C      UPDATE ROW INDEX VECTOR
C      JJ=IROW(IR)
C      IROW(IR)=IROW(IRANK)
C      IROW(IRANK)=JJ
C
C      INTERCHANGE COLUMNS IF NECESSARY
C      12 JJ=IC-(IRANK)*M
C      IF(JJ<1)
C      13 KK=NCOL
C      DO 14 J=1,M
C      I=KK+JJ
C      SAVE=A(I)
C      A(I)=A(JJ)
C      A(JJ)=A(I)
C      KK=KK-1
C      14 A(I)=SAVE
C
C      UPDATE COLUMN INDEX VECTOR
C      JJ=L(OL(I))
C      ICUL(I)=ICUL(IRANK)
C      ICUL(IRANK)=JJ
C      15 KK=IRANK+1
C      MM=IRANK+M
C      LL=ICOL(M)
C
C      TEST FOR LAST ROW
C      IF(MA)16,25,25
C
C      TRANSFORM CURRENT SUBMATRIX AND SEARCH NEXT PIVOT
C      16 JJ=LL
C      SAVE=PIV
C      PIV=0
C      DO 19 J=JK,M
C      JJ=JJ+1
C      HOU=A(JJ)/SAVE
C      A(JJ)=HOU
C      L=J-IRANK
C
C      TEST FOR LAST COLUMN
C      IF(IRANK=N)17,19,19
C      17 II=JJ
C      DO 19 I=KK,M
C      II=II+M
C      MM=II-L
C      A(II)=A(II)-HOU*A(MM)
C      IF(ABS(A(II))-ABS(PIV))>.19,19,19
C      18 PIV=A(II)
C      I=I
C      IC=J
C      19 CONTINUE
C
C      SET UP MATRIX EXPRESSING ROW DEPENDENCIES
C      20 IF(IRANK-1)>.25,21
C      21 IR=IR
C      DO 24 J=2,IRANK
C      II=J-1
C      IR=IR-M
C      JJ=LL
C      DO 23 I=KK,M
C      HOU=A(I)
C      JJ=JJ+1
C      MM=JJ
C      IC=IR
C      DO 22 L=1,II
C      HOU=A(L)+A(MM)*HOU
C      L=L-1
C      22 A(MM)=A
C      23 A(MM)=A(MM)-HOU
C      24 CONTINUE
C
C      TEST FOR COLUMN REGULARITY
C      25 IF(N-IRANK)>.3,25
C
C      SET UP MATRIX EXPRESSING BASIC VARIABLES IN TERMS OF FREE
C      PARAMETERS (HOMOGENEOUS SOLUTION).
C      26 IR=LL
C      KK=LL+M
C      DO 30 J=1,IRANK
C      DO 29 I=KK,MM,M
C      JJ=IK
C      LL=I
C      HOU=C
C      II=J
C      27 II=II-1
C      IF(II)>.29,29,29
C      28 HOU=HOU-A(JJ)*A(II)

```

```

MFGK 830
MFGK 840
MFGK 850
MFGK 860
MFGK 870
MFGK 880
MFGK 890
MFGK 900
MFGK 910
MFGK 920
MFGK 930
MFGK 940
MFGK 950
MFGK 960
MFGK 970
MFGK 980
MFGK 990
MFGK 1000
MFGK 1010
MFGK 1020
MFGK 1030
MFGK 1040
MFGK 1050
MFGK 1060
MFGK 1070
MFGK 1080
MFGK 1090
MFGK 1100
MFGK 1110
MFGK 1120
MFGK 1130
MFGK 1140
MFGK 1150
MFGK 1160
MFGK 1170
MFGK 1180
MFGK 1190
MFGK 1200
MFGK 1210
MFGK 1220
MFGK 1230
MFGK 1240
MFGK 1250
MFGK 1260
MFGK 1270
MFGK 1280
MFGK 1290
MFGK 1300
MFGK 1310
MFGK 1320
MFGK 1330
MFGK 1340
MFGK 1350
MFGK 1360
MFGK 1370
MFGK 1380
MFGK 1390
MFGK 1400
MFGK 1410
MFGK 1420
MFGK 1430
MFGK 1440
MFGK 1450
MFGK 1460
MFGK 1470
MFGK 1480
MFGK 1490
MFGK 1500
MFGK 1510
MFGK 1520
MFGK 1530
MFGK 1540
MFGK 1550
MFGK 1560
MFGK 1570
MFGK 1580
MFGK 1590
MFGK 1600
MFGK 1610
MFGK 1620
MFGK 1630
MFGK 1640
MFGK 1650
MFGK 1660
MFGK 1670
MFGK 1680
MFGK 1690
MFGK 1700
MFGK 1710
MFGK 1720
MFGK 1730
MFGK 1740
MFGK 1750
MFGK 1760
MFGK 1770
MFGK 1780
MFGK 1790
MFGK 1800
MFGK 1810
MFGK 1820
MFGK 1830
MFGK 1840
MFGK 1850
MFGK 1860
MFGK 1870
MFGK 1880
MFGK 1890
MFGK 1900
MFGK 1910

```

```

JJ=JJ-M
LL=LL-L
GOTO 27
29 A(II)=(HOU-A(II))/A(JJ)
30 IR=IR-1
RETURN
END

```

```

MFGK1920
MFGK1930
MFGK1940
MFGK1950
MFGK1960
MFGK1970
MFGK1980
MFGK1990
DMGR 10
DMGR 20
DMGR 30
DMGR 40
DMGR 50
DMGR 60
DMGR 70
DMGR 80
DMGR 90
DMGR 100
DMGR 110
DMGR 120
DMGR 130
DMGR 140
DMGR 150
DMGR 160
DMGR 170
DMGR 180
DMGR 190
DMGR 200
DMGR 210
DMGR 220
DMGR 230
DMGR 240
DMGR 250
DMGR 260
DMGR 270
DMGR 280
DMGR 290
DMGR 300
DMGR 310
DMGR 320
DMGR 330
DMGR 340
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DMGR 660
DMGR 670
DMGR 680
DMGR 690
DMGR 700
DMGR 710
DMGR 720
DMGR 730
DMGR 740
DMGR 750
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DMGR 770
DMGR 780
DMGR 790
DMGR 800
DMGR 810
DMGR 820
DMGR 830
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DMGR 850
DMGR 860
DMGR 870
DMGR 880
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DMGR 900
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DMGR 950
DMGR 960
DMGR 970
DMGR 980
DMGR 990
DMGR1000
DMGR1010
DMGR1020
DMGR1030
DMGR1040
DMGR1050
DMGR1060
DMGR1070
DMGR1080
DMGR1090
DMGR1100
DMGR1110
DMGR1120
DMGR1130
DMGR1140
DMGR1150
DMGR1160

```



```

      IF(JJ)15,15,15
13 KK=NCOL
   UU 14 J=1,M
   IF(KK)JJ
   SAVE=A(KK)
   A(KK)=A(1)
   KK=KK-1
14 A(1)=SAVE
C
C      UPDATE COLUMN INDEX VECTOR
C      JC=ICOL(IC)
C      ICOL(IC)=ICOL(IRANK)
C      ICOL(IRANK)=JC
15 KK=IRANK+1
   MM=IRANK-M
   LL=NCOL+MM
C
C      TEST FOR LAST ROW
C      IF(MM)16,25+25
C
C      TRANSFORM CURRENT SUBMATRIX AND SEARCH NEXT PIVOT
16 JJ=LL
   SAVE=PIV
   PIV=0.00
   UU 17 J=KK,M
   JJ=JJ+1
   HOLD=A(JJ)/SAVE
   A(JJ)=HOLD
   L=J-IRANK
C
C      TEST FOR LAST COLUMN
C      IF(IRANK-N)17,17,17
17 II=JJ
   UU 18 I=KK,M
   II=II+1
   MM=II-L
   A(II)=A(II)/HOLD+A(MM)
   IF(CABS(A(II))-CABS(PIV))19,19,18
19 PIV=A(II)
   IR=J
   IC=I
19 CONTINUE
C
C      SET UP MATRIX EXPRESSING ROW DEPENDENCIES
20 IF(IRANK-1)23,23+21
21 IK=LL
   UU 24 J=2,IRANK
   II=J-1
   IM=IK-M
   JJ=LL
   UU 25 I=KK,M
   HOLD=0.00
   JJ=JJ+1
   MM=JJ
   IC=IK
   UU 22 L=1,II
   HOLD=HOLD+A(MM)*A(II)
   IC=IC+L
22 MM=MM+1
   UU 26 K=M+1,(M+1)-HOLD
24 CONTINUE
C
C      TEST FOR COLUMN REGULARITY
C      IF(N-IRANK)3,3+25
C
C      SET UP MATRIX EXPRESSING BASIC VARIABLES IN TERMS OF FREE
C      PARAMETERS (NO MORE GENERAL SOLUTION).
26 IR=LL
   KK=LL+1
   UU 30 J=1,IRANK
   UU 29 I=KK,MM,M
   JJ=IK
   LL=I
   HOLD=0.00
   II=J
27 II=II-1
   IF(II)29,29+23
28 HOLD=HOLD-A(JJ)*A(II)
   JJ=JJ+1
   LL=LL-1
   UU 30 J=J+1
29 A(LL)=(HOLD-A(LL))/A(JJ)
30 IR=IR+1
   RETURN
   END
      DMGR117C
      DMGR118D
      DMGR119D
      DMGR120D
      DMGR121D
      DMGR122C
      DMGR123C
      DMGR124C
      DMGR125D
      DMGR126D
      DMGR127D
      DMGR128D
      DMGR129C
      DMGR130D
      DMGR131D
      DMGR132D
      DMGR133D
      DMGR134D
      DMGR135D
      DMGR136D
      DMGR137D
      DMGR138D
      DMGR139C
      DMGR140D
      DMGR141C
      DMGR142D
      DMGR143D
      DMGR144D
      DMGR145D
      DMGR146D
      DMGR147D
      DMGR148C
      DMGR149C
      DMGR150D
      DMGR151C
      DMGR152D
      DMGR153C
      DMGR154C
      DMGR155C
      DMGR156C
      DMGR157C
      DMGR158C
      DMGR159C
      DMGR160C
      DMGR161C
      DMGR162C
      DMGR163C
      DMGR164C
      DMGR165C
      DMGR167C
      DMGR168D
      DMGR169C
      DMGR170C
      DMGR171C
      DMGR172C
      DMGR173C
      DMGR174C
      DMGR175C
      DMGR176C
      DMGR177C
      DMGR178C
      DMGR179C
      DMGR180C
      DMGR181C
      DMGR182C
      DMGR183C
      DMGR184C
      DMGR185C
      DMGR186C
      DMGR187C
      DMGR188C
      DMGR189C
      DMGR190C
      DMGR191C
      DMGR192C
      DMGR193C
      DMGR194C
      DMGR195C
      DMGR196D
      DMGR197C
      DMGR198C
      DMGR199C
      DMGR200C
      DMGR201C

```

Subroutines GELS and DGELS

These subroutines solve a system of simultaneous linear equations with symmetric coefficient matrix by Gauss elimination. Consider the system of simultaneous linear equations

$$A * X = R \quad (1)$$

with symmetric m by m coefficient matrix, the upper triangular part of which is stored by column in $m * (m+1)/2$ successive storage locations, and an m by n right-hand side matrix R stored by column in $m * n$ successive storage locations. Solution is done by Gauss elimination with pivoting in the main diagonal of matrix A . If matrix R is the identity matrix, solution X is the inverse of matrix A . Solution matrix X is placed in positions of the right-hand side matrix R and is stored by column also. Thus, the computation of the solution requires no extra m by n array of storage. Only an auxiliary storage array named AUX with $(m-1)$ storage locations is necessary.

Explicitly, the given system (1) is of the form:[†]

$$\begin{pmatrix}
 \underline{a_{11}} & \underline{a_{12}} & \underline{a_{13}} & \dots & \underline{a_{1m}} \\
 a_{21} & \underline{a_{22}} & \underline{a_{23}} & \dots & \underline{a_{2m}} \\
 a_{31} & a_{32} & \underline{a_{33}} & \dots & \underline{a_{3m}} \\
 \dots & \dots & \dots & \dots & \dots \\
 a_{m1} & a_{m2} & a_{m3} & \dots & \underline{a_{mm}}
 \end{pmatrix}
 *
 \begin{pmatrix}
 x_{11} & x_{12} & \dots & x_{1n} \\
 x_{21} & x_{22} & \dots & x_{2n} \\
 x_{31} & x_{32} & \dots & x_{3n} \\
 \dots & \dots & \dots & \dots \\
 x_{m1} & x_{m2} & \dots & x_{mn}
 \end{pmatrix}
 =
 \begin{pmatrix}
 r_{11} & r_{12} & \dots & r_{1n} \\
 r_{21} & r_{22} & \dots & r_{2n} \\
 r_{31} & r_{32} & \dots & r_{3n} \\
 \dots & \dots & \dots & \dots \\
 r_{m1} & r_{m2} & \dots & r_{mn}
 \end{pmatrix}
 \quad (2)$$

The first step is to search the main diagonal of matrix A for the element of greatest absolute value, say a_{jj} , and to select it as first pivot ($p = a_{jj}$). The reason for pivoting only in the main diagonal of A is that rest-matrices of $A(k)$

[†]Note that subroutines GELS and DGELS require only the upper triangular part of matrix A ; that is, the elements $a_{11}; a_{12}, a_{22}; a_{13}, a_{23}, a_{33}; \dots; a_{1m}, a_{2m}, \dots, a_{mm}$. These elements are underlined in formula (2).

($k = 1, 2, \dots, m-1$) must remain symmetrical during the whole algorithm. With a_{jj} , generate the internal absolute tolerance for testing usefulness of the symmetric algorithm in the following way:

$$\text{tol} = |a_{jj}| \cdot \epsilon \quad (3)$$

with a given relative tolerance ϵ .

Suppose that pivot element a_{jj} is equal to a_{11} . If it is not, interchange the first rows of matrices A and R with the j^{th} and the first column of matrix A with the j^{th} , and save column interchange information by storing the difference ($j-1$) of pivot column index j and step counter $k = 1$ [interchanging column 1 with column j means interchanging variables x_{11} with x_{1j} ($l = 1, 2, \dots, n$)].

Now transform the elements of pivot rows in matrices A and R by division with p , and the other elements by adding $-a_{\nu 1}$ times the new first rows of these two matrices to the other ν rows, thus getting:††

$$a_{1l}^{(1)} = \frac{a_{1l}}{p} \quad (l = 1, 2, \dots, m) \quad (4)$$

$$r_{1l}^{(1)} = \frac{r_{1l}}{p} \quad (l = 1, 2, \dots, n) \quad (5)$$

$$a_{\nu 1}^{(1)} = a_{\nu 1} - a_{\nu 1} \cdot a_{11}^{(1)} \quad (l = 2, 3, \dots, m, \nu = 2, 3, \dots, m) \quad (6)$$

$$r_{\nu 1}^{(1)} = r_{\nu 1} - a_{\nu 1} \cdot r_{11}^{(1)} \quad (l = 1, 2, \dots, n; \nu = 2, 3, \dots, m) \quad (7)$$

As column interchange information is saved in the first position of the main diagonal, the result of the first step is the two matrices:

$$A^{(1)} = \begin{pmatrix} (j-1) & a_{12}^{(1)} & a_{13}^{(1)} & \dots & a_{1m}^{(1)} \\ 0 & a_{22}^{(1)} & a_{23}^{(1)} & \dots & a_{2m}^{(1)} \\ 0 & a_{32}^{(1)} & a_{33}^{(1)} & \dots & a_{3m}^{(1)} \\ \dots & \dots & \dots & \dots & \dots \\ 0 & a_{m2}^{(1)} & a_{m3}^{(1)} & \dots & a_{mm}^{(1)} \end{pmatrix} \quad \text{and}$$

††Note that transformation of pivot row in matrix A destroys pivot column, which is, due to symmetry, stored in the same locations. As pivot column is used unchanged for transformation of rest of A and R, it has to be saved in auxiliary array AUX before transforming pivot row.

$$R^{(1)} = \begin{pmatrix} r_{11}^{(1)} & r_{12}^{(1)} & \dots & r_{1n}^{(1)} \\ r_{21}^{(1)} & r_{22}^{(1)} & \dots & r_{2n}^{(1)} \\ r_{31}^{(1)} & r_{32}^{(1)} & \dots & r_{3n}^{(1)} \\ \dots & \dots & \dots & \dots \\ r_{m1}^{(1)} & r_{m2}^{(1)} & \dots & r_{mn}^{(1)} \end{pmatrix}$$

It is easily seen from equations (4) - (7) that the rest of matrix $A^{(1)}$ -- that is, matrix $A^{(1)}$ without the first row and first column -- is symmetrical and that actually only the underlined elements must be calculated and stored. Therefore, the range of index l in formula (6) reduces to $l = \nu, \nu + 1, \dots, m$.

Now repeat this procedure $m-2$ times, starting at each step with the matrix $A^{(k)}$ of the step before without the first k rows and first k columns, and the matrix $R^{(k)}$ without the first k rows. The total result after $m-1$ steps is the matrices:

$$A^{(m-1)} = \begin{pmatrix} (j_1-1) & a_{12}^{(1)} & a_{13}^{(1)} & \dots & a_{1m}^{(1)} \\ 0 & (j_2-2) & a_{23}^{(2)} & \dots & a_{2m}^{(2)} \\ 0 & 0 & (j_3-3) & \dots & a_{3m}^{(3)} \\ \dots & \dots & \dots & \dots & \dots \\ 0 & 0 & 0 & \dots & (j_m-m) \end{pmatrix} \quad \text{and}$$

$$R^{(m-1)} = \begin{pmatrix} r_{11}^{(1)} & r_{12}^{(1)} & \dots & r_{1n}^{(1)} \\ r_{21}^{(2)} & r_{22}^{(2)} & \dots & r_{2n}^{(2)} \\ r_{31}^{(3)} & r_{32}^{(3)} & \dots & r_{3n}^{(3)} \\ \dots & \dots & \dots & \dots \\ r_{m1}^{(m)} & r_{m2}^{(m)} & \dots & r_{mn}^{(m)} \end{pmatrix}$$

Now work backward and set:

$$\left. \begin{aligned}
 r_{m-1,1}^{(m)} &= r_{m-1,1}^{(m-1)} - a_{m-1,m}^{(m-1)} \cdot r_{m1}^{(m)} \quad (l = 1, 2, \dots, n) \\
 r_{m-2,1}^{(m)} &= r_{m-2,1}^{(m-2)} - a_{m-2,m-1}^{(m-2)} \cdot r_{m-1,1}^{(m)} \\
 &\dots \dots \dots \\
 r_{11}^{(m)} &= r_{11}^{(1)} - a_{12}^{(1)} \cdot r_{21}^{(m)} - a_{13}^{(1)} \cdot r_{31}^{(m)} \\
 &\quad - a_{m-2,m}^{(m-2)} \cdot r_{m1}^{(m)} \quad (l = 1, 2, \dots, n) \\
 &\quad \dots \dots - a_{1m}^{(1)} \cdot r_{m1}^{(m)} \quad (l = 1, 2, \dots, n)
 \end{aligned} \right\} (8)$$

After each step of back substitution, rows of solution matrix $X = R^{(m)}$ have to be back-interchanged according to interchange information in the corresponding main diagonal element of matrix $A^{(m-1)}$, in order to get the correct sequence of right-hand side column elements corresponding to the sequence of left-hand side row elements.

The only case in which the procedure described above can fail to give a solution occurs when at any step all elements in the main diagonal of the rest-matrix of $A^{(k)}$ become zero, and no pivot element can be found. In this case, the procedure is bypassed and the error message $ier = -1$ is given. This may -- but does not necessarily -- mean, that matrix A is singular. Possibly subroutines GELG or DGELG (which are working with complete pivoting) will be able to find a solution in cases where subroutines GELS or DGELS fail. Actually, because of rounding errors, a further check of the absolute values of pivot elements is performed by the procedure. If at elimination step k this absolute value becomes less than tol (see equation 3), it is likely that there was loss of significance in the computation of the diagonal elements. But as this may not necessarily be the case, and as this test depends highly on the choice of the relative tolerance ϵ^+ , the procedure gives only the warning $ier = k-1$, which indicates that there is a possible loss of significance in the results computed by the algorithm.⁺⁺ But here it is also possible that subroutines GELG or DGELG will give better results. If there is only one equation to solve ($m = 1$), the test on loss of significance is suppressed.

⁺ For subroutine GELS, a relative tolerance between 10^{-6} and 10^{-7} is suggested; and for subroutine DGELS, between 10^{-14} and 10^{-16} .

⁺⁺ For example, $\epsilon = 10^{-5}$ and warning $ier = 3$ mean that there is a possible loss of about five or more significant digits in the initial values of elimination step 4.

```

C ..... GELS 1C
C ..... GELS 2C
C ..... GELS 3C
C ..... GELS 4C
C ..... GELS 5C
C ..... GELS 6C
C ..... GELS 7C
C ..... GELS 8C
C ..... GELS 9C
C ..... GELS 10C
C ..... GELS 11C
C ..... GELS 12C
C ..... GELS 13C
C ..... GELS 14C
C ..... GELS 15C
C ..... GELS 16C
C ..... GELS 17C
C ..... GELS 18C
C ..... GELS 19C
C ..... GELS 20C
C ..... GELS 21C
C ..... GELS 22C
C ..... GELS 23C
C ..... GELS 24C
C ..... GELS 25C
C ..... GELS 26C
C ..... GELS 27C
C ..... GELS 28C
C ..... GELS 29C
C ..... GELS 30C
C ..... GELS 31C
C ..... GELS 32C
C ..... GELS 33C
C ..... GELS 34C
C ..... GELS 35C
C ..... GELS 36C
C ..... GELS 37C
C ..... GELS 38C
C ..... GELS 39C
C ..... GELS 40C
C ..... GELS 41C
C ..... GELS 42C
C ..... GELS 43C
C ..... GELS 44C
C ..... GELS 45C
C ..... GELS 46C
C ..... GELS 47C
C ..... GELS 48C
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C ..... GELS 67C
C ..... GELS 68C
C ..... GELS 69C
C ..... GELS 70C
C ..... GELS 71C
C ..... GELS 72C
C ..... GELS 73C
C ..... GELS 74C
C ..... GELS 75C
C ..... GELS 76C
C ..... GELS 77C
C ..... GELS 78C
C ..... GELS 79C
C ..... GELS 80C
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C ..... GELS 83C
C ..... GELS 84C
C ..... GELS 85C
C ..... GELS 86C
C ..... GELS 87C
C ..... GELS 88C
C ..... GELS 89C
C ..... GELS 90C
C ..... GELS 91C
C ..... GELS 92C
C ..... GELS 93C
C ..... GELS 94C
C ..... GELS 95C
C ..... GELS 96C
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C ..... GELS 98C
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C ..... GELS103C
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C ..... GELS106C
C ..... GELS107C
C ..... GELS108C
C ..... GELS109C
C ..... GELS110C
C ..... GELS111C
C ..... GELS112C
C ..... GELS113C
C ..... GELS114C
C ..... GELS115C
C ..... GELS116C
C ..... GELS117C
C ..... GELS118C
C ..... GELS119C
C ..... GELS120C
C ..... GELS121C
C ..... GELS122C
C ..... GELS123C
C ..... GELS124C
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C ..... GELS127C
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C ..... GELS129C
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C ..... GELS131C
C ..... GELS132C
C ..... GELS133C
C ..... GELS134C
C ..... GELS135C
C ..... GELS136C
C ..... GELS137C
C ..... GELS138C
C ..... GELS139C
C ..... GELS140C
C ..... GELS141C
C ..... GELS142C
C ..... GELS143C
C ..... GELS144C
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C ..... GELS146C
C ..... GELS147C
C ..... GELS148C
C ..... GELS149C
C ..... GELS150C
C ..... GELS151C
C ..... GELS152C
C ..... GELS153C
C ..... GELS154C
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C ..... GELS157C
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C ..... GELS159C
C ..... GELS160C
C ..... GELS161C
C ..... GELS162C
C ..... GELS163C
C ..... GELS164C
C ..... GELS165C
C ..... GELS166C
C ..... GELS167C
C ..... GELS168C
C ..... GELS169C
C ..... GELS170C
C ..... GELS171C
C ..... GELS172C
C ..... GELS173C
C ..... GELS174C
C ..... GELS175C
C ..... GELS176C
C ..... GELS177C
C ..... GELS178C
C ..... GELS179C
C ..... GELS180C
C ..... GELS181C
C ..... GELS182C
C ..... GELS183C
C ..... GELS184C
C ..... GELS185C
C ..... GELS186C
C ..... GELS187C
C ..... GELS188C
C ..... GELS189C
C ..... GELS190C
C ..... GELS191C
C ..... GELS192C
C ..... GELS193C
C ..... GELS194C
C ..... GELS195C
C ..... GELS196C
C ..... GELS197C
C ..... GELS198C
C ..... GELS199C
C ..... GELS200C

```

```

C   SAVE COLUMN INTERCHANGE INFORMATION
C   A(LS1)=LT
C
C   ELEMENT REDUCTION AND SEARCH FOR NEXT PIVOT
PIV=0
LS1=LS1
LT=0
DO 18 I1=N,LEND
  PIV=AUX(I1)
  LL=LS1
  LT=LT+1
  DO 19 LL=I1,LEND
    LL=LL+1
  19 A(LL)=A(LL)+PIV*A(LL)
  LS1=LL
  LR=LS1+1
  TB=AAS(A(LR))
  IF(TB=PIV)17,17,16
16 PIV=TB
  LR=LR+1
  J=I1+1
  DO 19 LR=J,N,M
    LL=LR+1
  16 R(LL)=R(LL)+PIV*R(LL)
  END OF ELIMINATION LOOP
C
C
C   BACK SUBSTITUTION AND BACK INTERCHANGE
19 IF(LEND)24,24,20
20 I1=M
  DO 22 I=2,M
    LST=LST-I
    I1=I-1
    R=LALST+I*J
    DO 22 J=I1,N,M
      TB=R(J)
      CL=J
      K=LST
      DO 21 LT=I1,LEND
        LL=LL+1
        K=K+1
      21 TB=TB-A(K)*R(LL)
      K=K+1
      R(J)=R(K)
  22 R(K)=TB
  23 RETURN
C
C
C   ERROR RETURN
24 IER=-1
  RETURN
END

```

```

GELS130C
GELS131C
GELS1320
GELS1330
GELS1340
GELS1350
GELS1360
GELS1370
GELS1380
GELS1390
GELS1400
GELS1410
GELS1420
GELS1430
GELS1440
GELS1450
GELS1460
GELS1470
GELS1480
GELS1490
GELS1500
GELS1510
GELS1520
GELS1530
GELS1540
GELS1550
GELS1560
GELS1570
GELS1580
GELS1590
GELS1600
GELS1610
GELS1620
GELS1630
GELS1640
GELS1650
GELS1660
GELS1670
GELS1680
GELS1690
GELS1700
GELS1710
GELS1720
GELS1730
GELS1740
GELS1750
GELS1760
GELS1770
GELS1780
GELS1790
GELS1800
GELS1810
GELS1820

```

```

C   .....
C   SUBROUTINE DUGEL(K,M,N,EP,S,IER,AUX)
C
C   DIMENSION A(11),R(11),AUX(11)
C   DOUBLE PRECISION K,M,AUX,PIV,TB,TOL,PIV1
C   IF(A)24,24,1
C
C   SEARCH FOR GREATEST MAIN DIAGONAL ELEMENT
1 IER=0
  PIV=0
  L=0
  DO 3 K=1,M
    LL=M
    TOP=AAS(A(LL))
    IF(TOP>PIV)3,3,2
  2 PIV=TOP
    L=L+1
  3 CONTINUE
  TOP=PIV
C   MAIN DIAGONAL ELEMENT A(1)=A(J,J) IS FIRST PIVOT ELEMENT.
C   PIV CONTAINS THE ABSOLUTE VALUE OF A(1).
C
C   START ELIMINATION LOOP
  LST=0
  NRM=M
  LEAD=M-1
  DO 10 K=1,M
C
C   TEST ON USEFULNESS OF SYMMETRIC ALGORITHM
  IF(PIV)24,24,4
  4 IER=IER+1
  5 IF(PIV<TOL)6,6,7
  6 IER=IER+1
  7 LT=J-K
  8 LST=LST+K
C
C   PIVOT ROW REDUCTION AND ROW INTERCHANGE IN RIGHT HAND SIDE R
  PIV1=L/ABS(A(1))
  DO 9 I=1,N,M
    CL=I
    TE=PIV*R(LL)
    R(LL)=TE
  9 R(L)=R(I)
C
C   IS ELIMINATION TERMINATED
  IER=IER+1
C
C   ROW AND COLUMN INTERCHANGE AND PIVOT ROW REDUCTION IN MATRIX A.
C   ELEMENTS OF PIVOT COLUMN ARE SAVED IN AUXILIARY VECTOR AUX.
  9 LR=LST+LT+IER*J-1
  LL=LR
  L=J
  DO 14 I=K,LEAD
    LR=I
    CL=I+1
    IF(LR<LR+1)10,11
  10 A(LL)=A(LR)
  11 TO=A(L)
  12 TO=A(LL)
  13 AUX(1)=TB
  14 A(L)=PIV*TB
C
C   SAVE COLUMN INTERCHANGE INFORMATION
A(LS1)=LT
C
C   ELEMENT REDUCTION AND SEARCH FOR NEXT PIVOT
PIV=0
LS1=LS1
LT=0
DO 18 I1=N,LEND
  PIV=AUX(I1)
  LL=LS1
  LT=LT+1
  DO 19 LL=I1,LEND
    LL=LL+1
  19 A(LL)=A(LL)+PIV*A(LL)
  LS1=LL
  LR=LS1+1
  TB=AAS(A(LR))
  IF(TB=PIV)17,17,16
16 PIV=TB
  LR=LR+1
  J=I1+1
  DO 19 LR=J,N,M
    LL=LR+1
  16 R(LL)=R(LL)+PIV*R(LL)
  END OF ELIMINATION LOOP
C
C
C   BACK SUBSTITUTION AND BACK INTERCHANGE
19 IF(LEND)24,23,23
20 I1=M
  DO 22 I=2,M
    LST=LST-I
    I1=I-1
    R=LALST+I*J
    DO 22 J=I1,N,M
      TB=R(J)
      CL=J
      K=LST
      DO 21 LT=I1,LEND
        LL=LL+1
        K=K+1
      21 TB=TB-A(K)*R(LL)
      K=K+1
      R(J)=R(K)
  22 R(K)=TB
  23 RETURN
C
C
C   ERROR RETURN
24 IER=-1
  RETURN
END

```

```

C
C
C   .....
C   SUBROUTINE DUGEL
C
C   PURPOSE
C   TO SOLVE A SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS WITH
C   SYMMETRIC COEFFICIENT MATRIX UPPER TRIANGULAR PART OF WHICH
C   IS ASSUMED TO BE STORED COLUMNWISE.
C
C   USAGE
C   CALL DUGEL(K,M,N,EP,S,IER,AUX)
C
C   DESCRIPTION OF PARAMETERS
C   K - DOUBLE PRECISION M BY N RIGHT HAND SIDE MATRIX
C   (DESTROYED). ON RETURN K CONTAINS THE SOLUTION OF
C   THE EQUATIONS.
C   A - UPPER TRIANGULAR PART OF THE SYMMETRIC DOUBLE
C   PRECISION M BY M COEFFICIENT MATRIX. (DESTROYED)
C   M - THE NUMBER OF EQUATIONS IN THE SYSTEM.
C   N - THE NUMBER OF RIGHT HAND SIDE VECTORS.
C   EPS - SINGLE PRECISION INPUT CONSTANT WHICH IS USED AS
C   RELATIVE TOLERANCE FOR TEST ON LOSS OF
C   SIGNIFICANCE.
C   IER - RESULTING ERROR PARAMETER CODED AS FOLLOWS
C   IER=0 - NO ERROR
C   IER=-1 - NO RESULT BECAUSE OF M LESS THAN 1 OR
C   PIVOT ELEMENT AT ANY ELIMINATION STEP
C   EQUAL TO 0.
C   IER=K - WARNING DUE TO POSSIBLE LOSS OF SIGNIFI-
C   CANCE INDICATED AT ELIMINATION STEP K+1,
C   WHERE PIVOT ELEMENT WAS LESS THAN OR
C   EQUAL TO THE INTERNAL TOLERANCE EPS TIMES
C   ABSOLUTELY GREATEST MAIN DIAGONAL
C   ELEMENT OF MATRIX A.
C   AUX - DOUBLE PRECISION AUXILIARY STORAGE ARRAY
C   WITH DIMENSION M-1.
C
C   REMARKS
C   UPPER TRIANGULAR PART OF MATRIX A IS ASSUMED TO BE STORED
C   COLUMNWISE IN M*(M+1)/2 SUCCESSIVE STORAGE LOCATIONS. RIGHT
C   HAND SIDE MATRIX R COLUMNWISE IN N*M SUCCESSIVE STORAGE
C   LOCATIONS. ON RETURN SOLUTION MATRIX R IS STORED COLUMNWISE
C   TOO.
C   THE PROCEDURE GIVES RESULTS IF THE NUMBER OF EQUATIONS M IS
C   GREATER THAN 0 AND PIVOT ELEMENTS AT ALL ELIMINATION STEPS
C   ARE DIFFERENT FROM 0. HOWEVER WARNING IER=K - IF GIVEN -
C   INDICATES POSSIBLE LOSS OF SIGNIFICANCE. IN CASE OF A WELL
C   SCALED MATRIX A AND APPROPRIATE TOLERANCE EPS, IER=K MAY BE
C   INTERPRETED THAT MATRIX A HAS THE RANK K. NO WARNING IS
C   GIVEN IN CASE M=1.
C   ERROR PARAMETER IER=-1 DOES NOT NECESSARILY MEAN THAT
C   MATRIX A IS SINGULAR, AS ONLY MAIN DIAGONAL ELEMENTS
C   ARE USED AS PIVOT ELEMENTS. POSSIBLY SUBROUTINE DUGEL (WHICH)
C   WORKS WITH TOTAL PIVOTING) WOULD BE ABLE TO FIND A SOLUTION.
C
C   SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C   NONE
C
C   METHOD
C   SOLUTION IS DONE BY MEANS OF GAUSS-ELIMINATION WITH
C   PIVOTING IN MAIN DIAGONAL, IN ORDER TO PRESERVE
C   SYMMETRY IN REMAINING COEFFICIENT MATRICES.

```

```

GELS 10
.....
GELS 20
GELS 30
GELS 40
GELS 50
GELS 60
GELS 70
GELS 80
GELS 90
GELS 100
GELS 110
GELS 120
GELS 130
GELS 140
GELS 150
GELS 160
GELS 170
GELS 180
GELS 190
GELS 200
GELS 210
GELS 220
GELS 230
GELS 240
GELS 250
GELS 260
GELS 270
GELS 280
GELS 290
GELS 300
GELS 310
GELS 320
GELS 330
GELS 340
GELS 350
GELS 360
GELS 370
GELS 380
GELS 390
GELS 400
GELS 410
GELS 420
GELS 430
GELS 440
GELS 450
GELS 460
GELS 470
GELS 480
GELS 490
GELS 500
GELS 510
GELS 520
GELS 530
GELS 540
GELS 550
GELS 560
GELS 570
GELS 580
GELS 590
GELS 600
GELS 610
GELS 620
GELS 630
GELS 640

```

```

C
C
C   .....
C   SUBROUTINE DUGEL(K,M,N,EP,S,IER,AUX)
C
C   DIMENSION A(11),R(11),AUX(11)
C   DOUBLE PRECISION K,M,AUX,PIV,TB,TOL,PIV1
C   IF(A)24,24,1
C
C   SEARCH FOR GREATEST MAIN DIAGONAL ELEMENT
1 IER=0
  PIV=0
  L=0
  DO 3 K=1,M
    LL=M
    TOP=AAS(A(LL))
    IF(TOP>PIV)3,3,2
  2 PIV=TOP
    L=L+1
  3 CONTINUE
  TOP=PIV
C   MAIN DIAGONAL ELEMENT A(1)=A(J,J) IS FIRST PIVOT ELEMENT.
C   PIV CONTAINS THE ABSOLUTE VALUE OF A(1).
C
C   START ELIMINATION LOOP
  LST=0
  NRM=M
  LEAD=M-1
  DO 10 K=1,M
C
C   TEST ON USEFULNESS OF SYMMETRIC ALGORITHM
  IF(PIV)24,24,4
  4 IER=IER+1
  5 IF(PIV<TOL)6,6,7
  6 IER=IER+1
  7 LT=J-K
  8 LST=LST+K
C
C   PIVOT ROW REDUCTION AND ROW INTERCHANGE IN RIGHT HAND SIDE R
  PIV1=L/ABS(A(1))
  DO 9 I=1,N,M
    CL=I
    TE=PIV*R(LL)
    R(LL)=TE
  9 R(L)=R(I)
C
C   IS ELIMINATION TERMINATED
  IER=IER+1
C
C   ROW AND COLUMN INTERCHANGE AND PIVOT ROW REDUCTION IN MATRIX A.
C   ELEMENTS OF PIVOT COLUMN ARE SAVED IN AUXILIARY VECTOR AUX.
  9 LR=LST+LT+IER*J-1
  LL=LR
  L=J
  DO 14 I=K,LEAD
    LR=I
    CL=I+1
    IF(LR<LR+1)10,11
  10 A(LL)=A(LR)
  11 TO=A(L)
  12 TO=A(LL)
  13 AUX(1)=TB
  14 A(L)=PIV*TB
C
C   SAVE COLUMN INTERCHANGE INFORMATION
A(LS1)=LT
C
C   ELEMENT REDUCTION AND SEARCH FOR NEXT PIVOT
PIV=0
LS1=LS1
LT=0
DO 18 I1=N,LEND
  PIV=AUX(I1)
  LL=LS1
  LT=LT+1
  DO 19 LL=I1,LEND
    LL=LL+1
  19 A(LL)=A(LL)+PIV*A(LL)
  LS1=LL
  LR=LS1+1
  TB=AAS(A(LR))
  IF(TB=PIV)17,17,16
16 PIV=TB
  LR=LR+1
  J=I1+1
  DO 19 LR=J,N,M
    LL=LR+1
  16 R(LL)=R(LL)+PIV*R(LL)
  END OF ELIMINATION LOOP
C
C
C   BACK SUBSTITUTION AND BACK INTERCHANGE
19 IF(LEND)24,23,23
20 I1=M
  DO 22 I=2,M
    LST=LST-I
    I1=I-1
    R=LALST+I*J
    DO 22 J=I1,N,M
      TB=R(J)
      CL=J
      K=LST
      DO 21 LT=I1,LEND
        LL=LL+1
        K=K+1
      21 TB=TB-A(K)*R(LL)
      K=K+1
      R(J)=R(K)
  22 R(K)=TB
  23 RETURN
C
C
C   ERROR RETURN
24 IER=-1
  RETURN
END

```

Subroutines GELB and DGELB

These subroutines solve a system of simultaneous linear equations with a coefficient matrix of band structure by Gauss elimination. Consider the system of simultaneous linear equations

$$A * X = R \tag{1}$$

with an m by m coefficient matrix A of band structure and an m by n right-hand side matrix R. Solution is done by means of Gauss elimination with column pivoting in matrix A. If R is the identity matrix, solution X is the inverse of matrix A. Solution matrix X is placed in positions of right-hand side matrix R and is stored in the same way -- that is, columnwise in m*n successive storage locations. Thus, the computation of the solution requires no extra m by n array of storage.

As storing matrix A by row results in a much more effective inner loop than storing by column, the procedure assumes that band matrix A is stored by row in successive storage locations, the number of which is equal to the number of elements appearing in the main diagonal and upper and lower codiagonals. The elements to be handed to the procedure by the user are underlined in the following explicit writing of formula (1) in the special case of a 7 by 7 matrix A with three upper and two lower codiagonals:

$$\begin{bmatrix}
 \underline{a_{11}} & \underline{a_{12}} & \underline{a_{13}} & \underline{a_{14}} & 0 & 0 & 0 \\
 \underline{a_{21}} & \underline{a_{22}} & \underline{a_{23}} & \underline{a_{24}} & \underline{a_{25}} & 0 & 0 \\
 \underline{a_{31}} & \underline{a_{32}} & \underline{a_{33}} & \underline{a_{34}} & \underline{a_{35}} & \underline{a_{36}} & 0 \\
 0 & \underline{a_{42}} & \underline{a_{43}} & \underline{a_{44}} & \underline{a_{45}} & \underline{a_{46}} & \underline{a_{47}} \\
 0 & 0 & \underline{a_{53}} & \underline{a_{54}} & \underline{a_{55}} & \underline{a_{56}} & \underline{a_{57}} \\
 0 & 0 & 0 & \underline{a_{64}} & \underline{a_{65}} & \underline{a_{66}} & \underline{a_{67}} \\
 0 & 0 & 0 & 0 & \underline{a_{75}} & \underline{a_{76}} & \underline{a_{77}}
 \end{bmatrix} *$$

$$\begin{pmatrix}
 x_{11} & x_{12} & \dots & x_{1n} \\
 x_{21} & x_{22} & \dots & x_{2n} \\
 x_{31} & x_{32} & \dots & x_{3n} \\
 \dots & \dots & \dots & \dots \\
 x_{71} & x_{72} & \dots & x_{7n}
 \end{pmatrix} = \begin{pmatrix}
 r_{11} & r_{12} & \dots & r_{1n} \\
 r_{21} & r_{22} & \dots & r_{2n} \\
 r_{31} & r_{32} & \dots & r_{3n} \\
 \dots & \dots & \dots & \dots \\
 r_{71} & r_{72} & \dots & r_{7n}
 \end{pmatrix} \tag{2}$$

Immediately following the matrix elements there must be some auxiliary storage locations used by the procedure, such that in the general case of an m by m matrix A with "mud" upper and "mld" lower codiagonals the total number of storage locations of array A is:⁺

$$ma = m \cdot mc - \frac{(mc-mld - 1)(mc-mld)}{2} \tag{3}$$

$$\text{with } mc = \min(m, 1 + mud + mld). \tag{4}$$

That means, in the special case of formula (2), that the 33 underlined elements of matrix A must be stored by row in the first 33 successive locations of array A, which consists of 36 storage locations.

In the first part of the procedure, matrix A is searched for its absolutely greatest element, say a_{ij}, and the absolute tolerance for testing loss of significance

$$tol = \epsilon \cdot |a_{ij}| \tag{5}$$

is generated with a given relative tolerance ϵ^{++} . Close together with this search, the elements of matrix A are moved backward, and a triangular area of zeros is inserted in the last positions of the first (mc-mud-1) rows, according to storage requirements of the Gauss algorithm for band matrices. After these manipulations, the special matrix A of formula (2) will occupy the 36 positions of array A by row as shown in Figure 10 (the underlined elements are the main diagonal elements of matrix A).

In order to make the description of the band-algorithm easier, the elements of array A are renamed according to their arrangement in Figure 10,

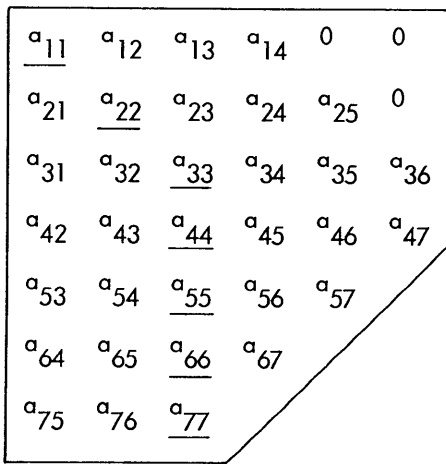


Figure 10. Array A

thus generally giving the array shown in Figure 11 (main diagonal elements are underlined).

Each of the first $mr = m - (mc - mld - 1)$ rows in this array contains mc elements; in the following rows the number of elements decreases steadily by 1 until the last row, which contains $mld + 1$ elements.

Now Gauss elimination can start. In the first step, search the first column of matrix A (that is, the elements of the first column of array A with row indexes from 1 up to $1 + mld$) for the absolutely greatest element, say a_{j1} ($1 \leq j \leq 1 + mld$), and select it as pivot element ($p = a_{j1}$). Assume that $j = 1$. If it is not, interchange the first rows in array A and matrix R with the j^{th} rows. Now, transform the elements of the pivot rows (that is, the first rows) of array A and matrix R by division with p , and the elements of the following mld rows by adding $-a_{\nu 1}$ times the first rows to the ν^{th} rows ($\nu = 2, 3, \dots, 1 + mld$). At the same time, shift back the elements of the ν^{th} rows in array A by one position and insert a zero in the last position of each transformed row. This transformation is described by the following set of formulas:

$$a_{1l}^{(1)} = \frac{a_{1l}}{p} \quad (l = 1, 2, \dots, mc) \quad (6)$$

$$r_{1l}^{(1)} = \frac{r_{1l}}{p} \quad (l = 1, 2, \dots, n) \quad (7)$$

$$\left. \begin{aligned} a_{\nu, l-1}^{(1)} &= a_{\nu l} - a_{\nu 1} \cdot a_{1l}^{(1)} \\ &\quad (l = 2, 3, \dots, mc) \\ a_{\nu, mc}^{(1)} &= 0 \end{aligned} \right\} \begin{aligned} &(\nu = 2, 3, \dots, \\ &1 + mld) \end{aligned} \quad (8)$$

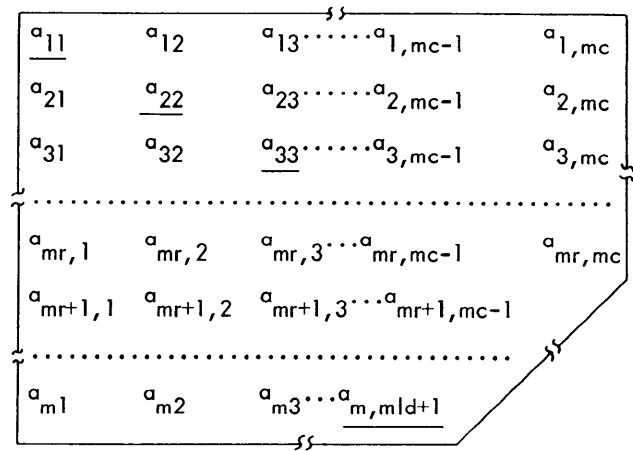


Figure 11. Array A renamed

$$r_{\nu l}^{(1)} = r_{\nu l} - a_{\nu 1} \cdot r_{1l}^{(1)} \quad (l = 1, 2, \dots, n; \quad (9) \\ \nu = 2, 3, \dots, \\ 1 + mld)$$

Rows with row indexes greater than $1 + mld$ remain unchanged; nevertheless, they are marked with the superscript 1. The result of the first step is shown in Figure 12 (main diagonal elements are underlined).

$$R^{(1)} = \begin{pmatrix} r_{11}^{(1)} & r_{12}^{(1)} & \dots & r_{1n}^{(1)} \\ r_{21}^{(1)} & r_{22}^{(1)} & \dots & r_{2n}^{(1)} \\ r_{31}^{(1)} & r_{32}^{(1)} & \dots & r_{3n}^{(1)} \\ \vdots & \vdots & \vdots & \vdots \\ r_{m1}^{(1)} & r_{m2}^{(1)} & \dots & r_{mn}^{(1)} \end{pmatrix}$$

This procedure is now repeated $(m-1)$ times, starting at the k^{th} step with array $A^{(k-1)}$ and matrix $R^{(k-1)}$.

+Note that the user must provide this number of storage locations of array A by the dimension statement in his main program.

++In case of a matrix A without lower codiagonals, tol is set equal to zero, whether ϵ is zero or not.

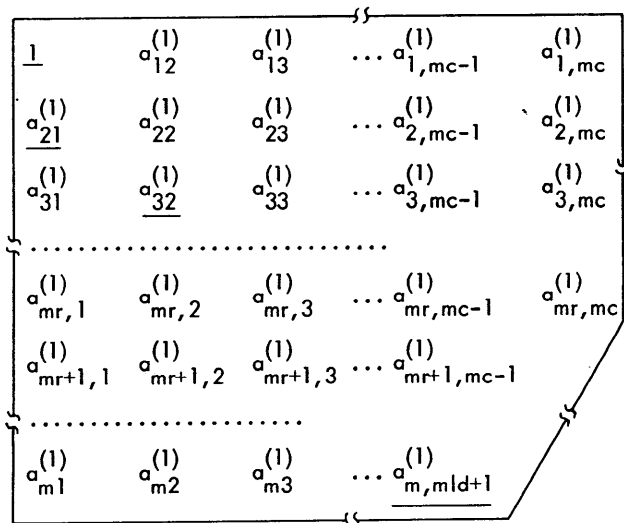


Figure 12. Array $A^{(1)}$

The rows which must be worked through at the k^{th} step are the rows with indexes $i = k, k + 1, \dots, \text{ilr} = \min(m, k + \text{mld})$. As soon as ilr becomes greater than mr , the number of elements in any row of array A which have to be transformed decreases by one in each step k . The total results after m steps are shown in Figure 13.

$$R^{(m)} = \begin{bmatrix} r_{11}^{(1)} & r_{12}^{(1)} & \dots & r_{1n}^{(1)} \\ r_{21}^{(2)} & r_{22}^{(2)} & \dots & r_{2n}^{(2)} \\ r_{31}^{(3)} & r_{32}^{(3)} & \dots & r_{3n}^{(3)} \\ \vdots & \vdots & \vdots & \vdots \\ r_{\text{mr},1}^{(\text{mr})} & r_{\text{mr},2}^{(\text{mr})} & \dots & r_{\text{mr},n}^{(\text{mr})} \\ \vdots & \vdots & \vdots & \vdots \\ r_{m1}^{(m)} & r_{m2}^{(m)} & \dots & r_{mn}^{(m)} \end{bmatrix}$$

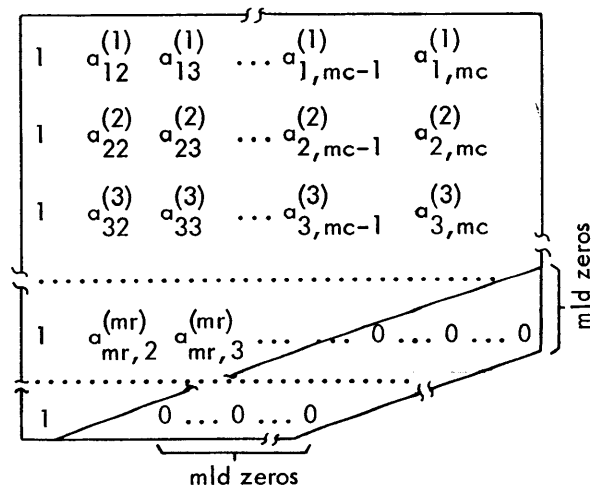


Figure 13. Array $A^{(m)}$

Now, working backward, generate solution matrix X in the locations of right-hand side matrix R by means of the following equations:

$$\begin{aligned} r_{m-1,1}^{(m)} &= r_{m-1,1}^{(m-1)} - a_{m-1,2}^{(m-1)} \cdot r_{m,1}^{(m)} \\ &\quad (l = 1, 2, \dots, n) \\ r_{m-2,1}^{(m)} &= r_{m-2,1}^{(m-2)} - a_{m-2,2}^{(m-2)} \cdot r_{m-1,1}^{(m)} \\ &\quad - a_{m-2,3}^{(m-2)} \cdot r_{m,1}^{(m)} \quad (l = 1, 2, \dots, n) \\ &\dots\dots\dots \\ r_{m-mc+1,1}^{(m)} &= r_{m-mc+1,1}^{(m-mc+1)} - a_{m-mc+1,2}^{(m-mc+1)} \\ &\quad \cdot r_{m-mc+2,1}^{(m)} \dots - a_{m-mc+1,mc}^{(m-mc+1)} \\ &\quad \cdot r_{m,1}^{(m)} \quad (l = 1, 2, \dots, n) \\ r_{11}^{(m)} &= r_{11}^{(1)} - a_{12}^{(1)} \cdot r_{21}^{(m)} - a_{13}^{(1)} \cdot r_{31}^{(m)} \\ &\quad - \dots - a_{1,mc}^{(1)} \cdot r_{mc,1}^{(m)} \quad (l = 1, 2, \dots, n) \end{aligned} \quad (10)$$

Note that in the first $mc-1$ equations of formula (10) the number of terms to be subtracted increases steadily by 1 until this number has reached $mc-1$. From the $(mc-1)$ st equation up to the last equation the number of terms to be subtracted remains constant.

The only case in which the procedure described above can fail to give a solution occurs when at any step (say the k^{th} step) all elements in the k^{th} column of the transformed matrix A [that is, the elements in the first column of array A with row indexes k up to $ilr = \min(m, k + mld)$] become zero, and no pivot element can be found. In this case, the procedure is bypassed and the error message $ier = -1$ is given. Actually, because of rounding errors, a further check of the absolute values of pivot elements is performed by the procedure. If at elimination step k this absolute value becomes less than tol (see equation 5 and second footnote), it is likely that matrix A is singular, too. But, as this may not necessarily be the case and as this test depends highly on the choice of the relative tolerance ϵ^+ , the procedure gives only the warning $ier = k-1$, which indicates that there is a possible loss of significance in the results computed by the algorithm.⁺⁺ In case of a well scaled matrix A and an appropriate choice of the relative tolerance, warning $ier = k-1$ may be interpreted as meaning that the rank of A is less than m but not less than $k - 1$. If there are no lower codiagonals ($mld = 0$), the test on loss of significance is suppressed.

+For subroutine GELB, a relative tolerance between 10^{-6} and 10^{-7} is suggested; and for subroutine DGELB, between 10^{-14} and 10^{-16} .

++For example, $\epsilon = 10^{-5}$ and warning $ier = 3$ mean that there is a possible loss of about 5 or more significant digits in the initial values of elimination step 4, and that matrix A seems to have a rank less than m but not less than 3.

```

C
C ..... GELB 13
C ..... GELB 20
C ..... GELB 30
SUBROUTINE GELB ..... GELB 40
C ..... GELB 50
PURPOSE ..... GELB 60
C ..... GELB 70
TO SOLVE A SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS WITH A
C ..... GELB 80
COEFFICIENT MATRIX OF BAND STRUCTURE.
C ..... GELB 90
C ..... GELB 100
USAGE ..... GELB 110
CALL GELB(R,A,M,N,MUD,MLD,EPS,IER)
C ..... GELB 120
C ..... GELB 130
DESCRIPTION OF PARAMETERS
C ..... GELB 140
R - M BY N RIGHT HAND SIDE MATRIX (DESTROYED).
C ..... GELB 150
ON RETURN R CONTAINS THE SOLUTION OF THE EQUATIONS.
C ..... GELB 160
A - M BY M COEFFICIENT MATRIX WITH BAND STRUCTURE
C ..... GELB 170
(DESTROYED).
C ..... GELB 180
M - THE NUMBER OF EQUATIONS IN THE SYSTEM.
C ..... GELB 190
N - THE NUMBER OF RIGHT HAND SIDE VECTORS.
C ..... GELB 200
MUD - THE NUMBER OF UPPER CODIAGONALS (THAT MEANS
C ..... GELB 210
CODIAGONALS ABOVE MAIN DIAGONAL).
C ..... GELB 220
MLD - THE NUMBER OF LOWER CODIAGONALS (THAT MEANS
C ..... GELB 230
CODIAGONALS BELOW MAIN DIAGONAL).
C ..... GELB 240
EPS - AN INPUT CONSTANT WHICH IS USED AS RELATIVE
C ..... GELB 250
TOLERANCE FOR TEST ON LOSS OF SIGNIFICANCE.
C ..... GELB 260
IER - RESULTING ERROR PARAMETER CODED AS FOLLOWS
C ..... GELB 270
IER=0 - NO ERROR.
C ..... GELB 280
IER=-1 - NO RESULT BECAUSE OF WRONG INPUT PARAM-
C ..... GELB 290
ETERS M,MUD,MLD OR BECAUSE OF PIVOT ELEMENT GELB 290
AT ANY ELIMINATION STEP EQUAL TO 0.
C ..... GELB 300
IER=K - WARNING DUE TO POSSIBLE LOSS OF SIGNIFI-
C ..... GELB 310
CANCE INDICATED AT ELIMINATION STEP K+1,
C ..... GELB 320
WHERE PIVOT ELEMENT WAS LESS THAN OR
C ..... GELB 330
EQUAL TO THE INTERNAL TOLERANCE EPS TIMES
C ..... GELB 340
ABSOLUTELY GREATEST ELEMENT OF MATRIX A.
C ..... GELB 350
C ..... GELB 360
REMARKS
C ..... GELB 370
BAND MATRIX A IS ASSUMED TO BE STORED ROWWISE IN THE FIRST
C ..... GELB 380
MC SUCCESSIVE STORAGE LOCATIONS OF TOTALLY REPEATED MA
C ..... GELB 390
STORAGE LOCATIONS, WHERE
C ..... GELB 400
N*(M+M)-M*(M+1)/2 ANU M*(M+M)+M*(M+1)/2 WITH
C ..... GELB 410
M*(M+M)-M*(M+1)/2, M*(M+1)-M*(M), M*(M+1)-M*(M).
C ..... GELB 420
RIGHT HAND SIDE MATRIX R IS ASSUMED TO BE STORED COLUMNWISE
C ..... GELB 430
IN N*M SUCCESSIVE STORAGE LOCATIONS. ON RETURN SOLUTION
C ..... GELB 440
MATRIX R IS STORED COLUMNWISE TOO.
C ..... GELB 450
INPUT PARAMETERS M, MUD, MLD SHOULD SATISFY THE FOLLOWING
C ..... GELB 460
RESTRICTIONS
C ..... GELB 470
MUD NOT LESS THAN ZERO
C ..... GELB 480
MLD NOT LESS THAN ZERO
C ..... GELB 490
MUD+MLD NOT GREATER THAN 2*M-2.
C ..... GELB 500
NO ACTION BESIDES ERROR MESSAGE IER=-1 TAKES PLACE IF THESE
C ..... GELB 510
RESTRICTIONS ARE NOT SATISFIED.
C ..... GELB 520
THE PROCEDURE GIVES RESULTS IF THE RESTRICTIONS ON INPUT
C ..... GELB 530
PARAMETERS ARE SATISFIED AND IF PIVOT ELEMENTS AT ALL
C ..... GELB 540
ELIMINATION STEPS ARE DIFFERENT FROM 0. HOWEVER WARNING
C ..... GELB 550
IER=K - IF GIVEN - INDICATES POSSIBLE LOSS OF SIGNIFICANCE.
C ..... GELB 560
IN CASE OF A WELL SCALED MATRIX A AND APPROPRIATE TOLERANCE
C ..... GELB 570
EPS, IER=K MAY BE INTERPRETED THAT MATRIX A HAS THE RANK K.
C ..... GELB 580
NO WARNING IS GIVEN IF MATRIX A HAS NO LOWER CODIAGONAL.
C ..... GELB 590
C ..... GELB 600
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C ..... GELB 610
NAME
C ..... GELB 620
C ..... GELB 630
METHOD
C ..... GELB 640
SOLUTION IS DONE BY MEANS OF GAUSS ELIMINATION WITH
C ..... GELB 650
COLUMN PIVOTING ONLY, IN ORDER TO PRESERVE BAND STRUCTURE
C ..... GELB 660
IN REMAINING COEFFICIENT MATRICES.
C ..... GELB 670
C ..... GELB 680
C ..... GELB 690
SUBROUTINE GELB(R,A,M,N,MUD,MLD,EPS,IER)
C ..... GELB 700
C ..... GELB 710
C ..... GELB 720
DIMENSION R(1),A(1)
C ..... GELB 730
C ..... GELB 740
TEST ON WRONG INPUT PARAMETERS
C ..... GELB 750
IF(MLD)47,1,4
C ..... GELB 760
1 IF(MUD)47,2,2
C ..... GELB 770
2 MC=1+MLD+MUD
C ..... GELB 780
IF(MC+1-M-N)3,3,47
C ..... GELB 790
C ..... GELB 800
PREPARE INTEGER PARAMETERS
C ..... GELB 810
MC=NUMBER OF COLUMNS IN MATRIX A
C ..... GELB 820
MU=NUMBER OF ZEROS TO BE INSERTED IN FIRST ROW OF MATRIX A
C ..... GELB 830
ML=NUMBER OF MISSING ELEMENTS IN LAST ROW OF MATRIX A
C ..... GELB 840
MR=INDEX OF LAST ROW IN MATRIX A WITH MC ELEMENTS
C ..... GELB 850
M2=TOTAL NUMBER OF ZEROS TO BE INSERTED IN MATRIX A
C ..... GELB 860
M3=TOTAL NUMBER OF STORAGE LOCATIONS NECESSARY FOR MATRIX A
C ..... GELB 870
NM=NUMBER OF ELEMENTS IN MATRIX R
C ..... GELB 880
3 IF(MC-N)3,5,4
C ..... GELB 890
4 MC=M
C ..... GELB 900
5 MU=MC-MUD-1
C ..... GELB 910
ML=MC-MLD-1
C ..... GELB 920
MR=M-ML
C ..... GELB 930
M2=(MU+MU+1)/2
C ..... GELB 940
M3=M*(M+1)-M*(M+1)/2
C ..... GELB 950
NM=N*M
C ..... GELB 960
C ..... GELB 970
MOVE ELEMENTS BACKWARD AND SEARCH FOR ABSOLUTELY GREATEST ELEMENT
C ..... GELB 980
(NOT NECESSARY IN CASE OF A MATRIX WITHOUT LOWER CODIAGONALS)
C ..... GELB 990
IER=0
C ..... GELB 1000
PIV=0.
C ..... GELB 1010
IF(MLD)14,14,6
C ..... GELB 1020
6 JJ=MA
C ..... GELB 1030
J=MA-M2
C ..... GELB 1040
KST=J
C ..... GELB 1050
DO 9 K=1,KST
C ..... GELB 1060
TB=A(J)
C ..... GELB 1070
A(JJ)=TB
C ..... GELB 1080
TB=ABS(TB)
C ..... GELB 1090
IF(TB-PIV)8,8,7
C ..... GELB 1100
7 PIV=TB
C ..... GELB 1110
8 J=J-1
C ..... GELB 1120
9 JJ=JJ-1
C ..... GELB 1130
C ..... GELB 1140
INSERT ZEROS IN FIRST MU ROWS (NOT NECESSARY IN CASE M2=0)
C ..... GELB 1150
IF(M2)14,14,10
C ..... GELB 1160
10 JJ=1
C ..... GELB 1170
J=1+M2
C ..... GELB 1180
IC=1+MUD
C ..... GELB 1190
DO 13 I=1,MU
C ..... GELB 1200
DO 12 K=1,MC
C ..... GELB 1210
A(I,J)=0.
C ..... GELB 1220
11 IF(K-IC)11,11,12
C ..... GELB 1230
11 A(I,J)=A(I,J)
C ..... GELB 1240
J=J+1
C ..... GELB 1250
12 JJ=JJ+1
C ..... GELB 1260
13 IC=IC+1
C ..... GELB 1270
C ..... GELB 1280

```



```

C GENERATE TEST VALUE FOR SINGULARITY
14 TOL=EPS*PIV
C
C START DECOMPOSITION LOOP
KST=1
IUST=MC
IC=MC-1
DU 38 K=1,M
IF (K-MR-1) 16,16,15
15 IOST=IOST+1
16 IO=IOST
ILR=K+MLO
IF (ILR-MI) 18,18,17
17 ILR=M
18 II=KST
C
C PIVOT SEARCH IN FIRST COLUMN (ROW INDEXES FROM I=K UP TO I=ILR)
PIV=0
DU 22 I=K,ILR
ID=ABS(A(II))
IF (ID-PIV) 20,20,19
19 PIV=ID
J=I
J=I+1
20 IF (I-MR) 22,22,21
21 IO=IO+1
22 II=II+ID
C
C TEST ON SINGULARITY
IF (PIV) 47,47,23
23 IF (IER) 26,24,26
24 IF (PIV-TOL) 25,25,26
25 IER=K-1
26 PIV=1./A(JJ)
C
C PIVOT ROW REDUCTION AND ROW INTERCHANGE IN RIGHT HAND SIDE R
ID=J-K
DU 27 I=K,MM,M
II=I+ID
TB=PIV*(II)
A(II)=A(II)
K(II)=TB
27 K(II)=TB
C
C PIVOT ROW REDUCTION AND ROW INTERCHANGE IN COEFFICIENT MATRIX A
II=KST
J=J+1
DU 28 I=J,J
TB=PIV*(II)
A(II)=A(II)
A(II)=TB
28 II=II+1
C
C ELEMENT REDUCTION
IF (I-ILR) 29,34,34
29 IO=KST
II=K+1
MU=KST+1
MZ=KST+IC
DU 33 J=I+1,ILR
C
C IN MATRIX A
ID=IO+MC
JJ=I-MR-1
IF (JJ) 31,31,30
30 ID=ID+JJ
31 PIV=A(II)
J=J+1
DU 32 J=MU,MC
A(J-1)=A(J)+PIV*(A(JJ))
J=J+1
A(J)=A(J)+C
C
C IN MATRIX R
J=K
DU 33 JJ=I,MM,M
R(JJ)=R(JJ)+PIV*(A(J))
33 J=J+M
34 KST=KST+MC
35 IC=IC-1
36 IO=K-MR
IF (IO) 38,38,37
37 KST=KST-ID
38 CONTINUE
C
C END OF DECOMPOSITION LOOP
C
C LACK SUBSTITUTION
IF (MC-1) 40,40,39
39 IC=2
KST=MA+ML-MU+2
II=M
DU 41 I=2,M
KST=KST+MC
II=II-1
J=I-MR
IF (J) 41,41,40
40 KST=KST+J
41 DU 43 J=I,MM,M
TB=R(J)
MZ=KST+IC-2
ID=J
DU 42 JJ=KST,MZ
ID=ID+1
42 TB=TB-A(JJ)*R(ID)
43 R(J)=TB
44 IF (IC-NC) 44,45,45
45 IC=IC+1
46 CONTINUE
47 RETURN
C
C ERROR RETURN
IER=-1
RETURN
END

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GELB1290
GELB1300
GELB1310
GELB1320
GELB1330
GELB1340
GELB1350
GELB1360
GELB1370
GELB1380
GELB1390
GELB1400
GELB1410
GELB1420
GELB1430
GELB1440
GELB1450
GELB1460
GELB1470
GELB1480
GELB1490
GELB1500
GELB1510
GELB1520
GELB1530
GELB1540
GELB1550
GELB1560
GELB1570
GELB1580
GELB1590
GELB1600
GELB1610
GELB1620
GELB1630
GELB1640
GELB1650
GELB1660
GELB1670
GELB1680
GELB1690
GELB1700
GELB1710
GELB1720
GELB1730
GELB1740
GELB1750
GELB1760
GELB1770
GELB1780
GELB1790
GELB1800
GELB1810
GELB1820
GELB1830
GELB1840
GELB1850
GELB1860
GELB1870
GELB1880
GELB1890
GELB1900
GELB1910
GELB1920
GELB1930
GELB1940
GELB1950
GELB1960
GELB1970
GELB1980
GELB1990
GELB2000
GELB2010
GELB2020
GELB2030
GELB2040
GELB2050
GELB2060
GELB2070
GELB2080
GELB2090
GELB2100
GELB2110
GELB2120
GELB2130
GELB2140
GELB2150
GELB2160
GELB2170
GELB2180
GELB2190
GELB2200
GELB2210
GELB2220
GELB2230
GELB2240
GELB2250
GELB2260
GELB2270
GELB2280
GELB2290
GELB2300
GELB2310
GELB2320
GELB2330
GELB2340
GELB2350
GELB2360
GELB2370
GELB2380
GELB2390
GELB2400
GELB2410
GELB2420
GELB2430
GELB2440
GELB2450
C
C ..... DELB 10
C SUBROUTINE UOGLB DELB 20
C PURPOSE DELB 30
C TO SOLVE A SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS WITH A DELB 40
C COEFFICIENT MATRIX OF BAND STRUCTURE. DELB 50
C USAGE DELB 60
C CALL UOGLB(R,A,M,N,MU,D,MLD,EPS,IER) DELB 70
C DESCRIPTION OF PARAMETERS DELB 80
C K - DOUBLE PRECISION M BY N RIGHT HAND SIDE MATRIX DELB 130
C (DESTROYED). ON RETURN R CONTAINS THE SOLUTION DELB 150
C OF THE EQUATIONS. DELB 160
C M - DOUBLE PRECISION M BY M COEFFICIENT MATRIX WITH DELB 170
C BAND STRUCTURE (DESTROYED). DELB 180
C N - THE NUMBER OF EQUATIONS IN THE SYSTEM. DELB 190
C MU - THE NUMBER OF RIGHT HAND SIDE VECTORS. DELB 200
C MLD - THE NUMBER OF UPPER CUDIAGONALS (THAT MEANS DELB 210
C CUDIAGONALS ABOVE MAIN DIAGONAL). DELB 220
C MLD - THE NUMBER OF LOWER CUDIAGONALS (THAT MEANS DELB 230
C CUDIAGONALS BELOW MAIN DIAGONAL). DELB 240
C EPS - SINGLE PRECISION INPUT CONSTANT WHICH IS USED AS DELB 250
C RELATIVE TOLERANCE FOR TEST ON LCSS OF DELB 260
C SIGNIFICANCE. DELB 270
C IER - RESULTING IER,K PARAMETER CODED AS FOLLOWS DELB 280
C IER=0 - NO ERROR. DELB 290
C IER=-1 - NO RESULT BECAUSE OF WRONG INPUT PARAME- DELB 300
C TERS M,MU,MU,D OR BECAUSE OF PIVOT ELEMENT DELB 310
C AT ANY ELIMINATION STEP EQUAL TO C. DELB 320
C IER=K - WARNING DUE TO POSSIBLE LOSS OF SIGNIFI- DELB 330
C CANCE INDICATED AT ELIMINATION STEP K+1, DELB 340
C WHERE PIVOT ELEMENT WAS LESS THAN OR DELB 350
C EQUAL TO THE INTERNAL TOLERANCE EPS TIMES DELB 360
C ABSOLUTELY GREATEST ELEMENT OF MATRIX A. DELB 370
C REMARKS DELB 380
C BAND MATRIX A IS ASSUMED TO BE STORED ROWWISE IN THE FIRST DELB 390
C ME SUCCESSIVE STORAGE LOCATIONS OF TOTALLY NEEDED MA DELB 400
C STORAGE LOCATIONS, WHERE DELB 410
C M=MM*(M+1)/2 AND M=MM*(MU+1)/2 WITH DELB 420
C MM=MIN(M,MU+MLD), M=MM*(1+MLD), M=MM*(1+MLD) DELB 430
C RIGHT HAND SIDE MATRIX R IS ASSUMED TO BE STORED COLUMNWISE DELB 440
C IN MM SUCCESSIVE STORAGE LOCATIONS. ON RETURN SOLUTION DELB 450
C MATRIX R IS STORED COLUMNWISE TOO. DELB 460
C INPUT PARAMETERS M, MU, MLD SHOULD SATISFY THE FOLLOWING DELB 470
C RESTRICTIONS: DELB 480
C MU NOT LESS THAN ZERO DELB 490
C MLD NOT LESS THAN ZERO DELB 500
C M+MLD NOT GREATER THAN 2*M-2. DELB 510
C NO ACTION BESIDES ERROR MESSAGE IER=-1 TAKES PLACE IF THESE DELB 520
C RESTRICTIONS ARE NOT SATISFIED. DELB 530
C THE PROCEDURE GIVES RESULTS IF THE RESTRICTIONS ON INPUT DELB 540
C PARAMETERS ARE SATISFIED AND IF PIVOT ELEMENTS AT ALL DELB 550
C ELIMINATION STEPS ARE DIFFERENT FROM C, HOWEVER WARNING DELB 560
C IER=K - IF GIVEN - INDICATES POSSIBLE LOSS OF SIGNIFI- DELB 570
C CANCE IN CASE OF A WELL SCALED MATRIX A AND APPROPRIATE TOLERANCE DELB 580
C EPS. IER=K MAY BE INTERPRETED THAT MATRIX A HAS THE RANK K. DELB 590
C NO WARNING IS GIVEN IF MATRIX A HAS NO LOWER CUDIAGONAL. DELB 600
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DELB 610
C NONE DELB 620
C METHOD DELB 630
C SOLUTION IS DONE BY MEANS OF GAUSS ELIMINATION WITH DELB 640
C COLUMN PIVOTING ONLY, IN ORDER TO PRESERVE BAND STRUCTURE DELB 650
C IN REMAINING COEFFICIENT MATRICES. DELB 660
C ..... DELB 700
C SUBROUTINE UOGLB(R,A,M,N,MU,D,MLD,EPS,IER) DELB 710
C DIMENSION A(1),A(1) DELB 720
C DOUBLE PRECISION R,A,PIV,TB,TOL DELB 730
C TEST ON WRONG INPUT PARAMETERS DELB 740
C IF (MLD) 47,47,1
C 1 IF (MU) 47,47,2
C 2 MC=1+MLD+MU
C IF (MC+1-M) 3,3,47
C PARAMETER INTEGER PARAMETERS DELB 670
C MC=NUMBER OF COLUMNS IN MATRIX A DELB 680
C MU=NUMBER OF ZEROS TO BE INSERTED IN LAST ROW OF MATRIX A DELB 690
C ML=NUMBER OF MISSING ELEMENTS IN LAST ROW OF MATRIX A DELB 670
C M=INDEX OF LAST ROW IN MATRIX A WITH MC ELEMENTS DELB 680
C MZ=TOTAL NUMBER OF ZEROS TO BE INSERTED IN MATRIX A DELB 690
C MA=TOTAL NUMBER OF STORAGE LOCATIONS NECESSARY FOR MATRIX A DELB 700
C M=NUMBER OF ELEMENTS IN MATRIX A DELB 710
C 3 IF (MC-K) 3,3,47
C 4 MC=M
C 5 MU=MC-MU-1
C ML=MC-ML-1
C MR=M-ML
C MZ=(MU+(MU+1))/2
C MA=(MC+MC-1+ML+1)/2
C M=MR+M
C MOVE ELEMENTS BACKWARD AND SEARCH FOR ABSOLUTELY GREATEST ELEMENT DELB 710
C (NOT NECESSARY IN CASE OF A MATRIX WITHOUT LOWER CUDIAGONALS) DELB 720
C IER=0 DELB 730
C PIV=0 DELB 740
C IF (A(J)) 11,11,40 DELB 750
C JJ=M DELB 760
C J=MA-MC DELB 770
C KST=J DELB 780
C DU 9 K=1,KST DELB 790
C TB=A(J) DELB 800
C ID=0 DELB 810
C IF (A(I)) 11,11,40 DELB 820
C IF (ID-PIV) 9,9,7 DELB 830
C 7 PIV=ID DELB 840
C 8 J=J-1 DELB 850
C 9 JJ=J-1 DELB 860
C INSERT ZEROS IN FIRST MU ROWS (NOT NECESSARY IN CASE MZ=0) DELB 870
C JJ=1 DELB 880
C J=1+MZ DELB 890
C L=1+MU DELB 900
C DU 13 I=1,MU DELB 910
C DU 12 K=1,MC DELB 920
C A(JJ)=0,00 DELB 930
C IF (K-IC) 11,11,12 DELB 940
C 11 A(JJ)=A(I) DELB 950
C J=J+1 DELB 960
C 12 JJ=JJ+1 DELB 970

```

```

13 IC=IC+1
C
C GENERATE TEST VALUE FOR SINGULARITY
14 TOL=EPS*PIV
C
C START DECOMPOSITION LOOP
C
KST=1
IDST=MC
IC=MC-1
DO 32 K=1,M
IF(IK-M)13,10,15
15 IDST=IDST+1
16 IJ=IDST
IKR=K+MLU
IF(IKR-M)18,18,17
17 IIR=M
18 II=KST
C
C PIVOT SEARCH IN FIRST COLUMN (ROW INDEXES FROM IFA UP TO I=IKR)
PIV=0.0
DO 22 I=K,IKR
TB=ABS(A(I,1))
IF(TB>PIV)22,22,19
19 PIV=TB
J=I
JJ=1
20 IF(I-M)22,22,21
21 ID=ID+1
22 II=II+1
C
C TEST ON SINGULARITY
IF(PIV)7,7,23
23 IF(IER)26,24,25
24 IF(PIV-TOL)25,25,25
25 IER=K-1
26 PIV=1.0/A(JJ)
C
C PIVOT ROW REDUCTION AND ROW INTERCHANGE IN RIGHT HAND SIDE R
ID=J-K
DO 27 I=K+1,M
II=I+10
TB=PIV*(II)
K(II)=K(II)
27 K(II)=I
C
C PIVOT ROW REDUCTION AND ROW INTERCHANGE IN COEFFICIENT MATRIX A
II=KST
J=JJ+10
DO 28 I=J,JJ
TB=PIV*(II)
A(II)=A(II)
A(II)=TB
28 II=II+1
C
C ELEMENT REDUCTION
IF(K-1)29,34,34
29 IFA=K+1
II=K+1
MFA=KST+1
MFA=KST+10
DO 33 I=II,IKR
C
C IN MATRIX A
ID=ID+MC
JJ=I-M+1
IF(JJ)31,31,30
30 ID=ID+JJ
31 PIV=A(I,J)
J=I+1
DO 32 J=J,M
A(I,J)=A(I,J)+PIV*(JJ)
32 J=J+1
A(I,J)=0.0
C
C IN MATRIX R
J=K
DO 33 JJ=I+1,M
K(I,J)=K(I,J)+PIV*(JJ)
33 J=J+1
34 KST=KST+MC
IF(IKR-M)35,35,35
35 IC=IC-1
36 ID=K-M
IF(ID)38,38,37
37 KST=KST+10
38 CONTINUE
END OF DECOMPOSITION LOOP
C
C
C
C BACK SUBSTITUTION
IF(MC-1)46,46,39
39 IC=2
KST=MA+ML-MC+2
II=M
DO 40 I=2,M
KST=KST-MC
II=II-1
J=II-M
IF(I)41,41,40
40 KST=KST+J
41 DO 43 J=1,II,M+M
TR=R(I,J)
M2=KST+IC-2
ID=J
DO 42 JJ=KST,M2
ID=ID+1
42 TR=TR-A(JJ)*R(II)
43 R(IJ)=TR
IF(IC-MC)44,44,45
44 IC=IC+1
45 CONTINUE
46 RETURN
C
C
C ERROR RETURN
47 IER=-1
RETURN
END

```

```

DELB1322
DELB1310
DELB1325
DELB1313
DELB1340
DELB1350
DELB1360
DELB1370
DELB1380
DELB1390
DELB1400
DELB1410
DELB1420
DELB1430
DELB1440
DELB1450
DELB1460
DELB1470
DELB1480
DELB1490
DELB1500
DELB1510
DELB1520
DELB1530
DELB1540
DELB1550
DELB1560
DELB1570
DELB1580
DELB1590
DELB1600
DELB1610
DELB1620
DELB1630
DELB1640
DELB1650
DELB1660
DELB1670
DELB1680
DELB1690
DELB1700
DELB1710
DELB1720
DELB1730
DELB1740
DELB1750
DELB1760
DELB1770
DELB1780
DELB1790
DELB1800
DELB1810
DELB1820
DELB1830
DELB1840
DELB1850
DELB1860
DELB1870
DELB1880
DELB1890
DELB1900
DELB1910
DELB1920
DELB1930
DELB1940
DELB1950
DELB1960
DELB1970
DELB1980
DELB1990
DELB2000
DELB2010
DELB2020
DELB2030
DELB2040
DELB2050
DELB2060
DELB2070
DELB2080
DELB2090
DELB2100
DELB2110
DELB2120
DELB2130
DELB2140
DELB2150
DELB2160
DELB2170
DELB2180
DELB2190
DELB2200
DELB2210
DELB2220
DELB2230
DELB2240
DELB2250
DELB2260
DELB2270
DELB2280
DELB2290
DELB2300
DELB2310
DELB2320
DELB2330
DELB2340
DELB2350
DELB2360
DELB2370
DELB2380
DELB2390
DELB2400
DELB2410
DELB2420
DELB2430
DELB2440
DELB2450
DELB2460
DELB2470
DELB2480

```

Subroutines MTDS and DMTDS

Given a general matrix A and a nonsingular upper triangular matrix T, these subroutines will perform one of the following six operations, depending on the value of an input parameter IOP:

- IOP = 1: A is replaced by $T^{-1}A$.
- IOP = -1: A is replaced by AT^{-1} .
- IOP = 2: A is replaced by $(T^{-1})^T A$.
- IOP = -2: A is replaced by $A(T^{-1})^T$.
- IOP = 3: A is replaced by $(T^T T)^{-1}A$.
- IOP = -3: A is replaced by $A(T^T T)^{-1}$.

1. Mathematical background

- a. Calculation of $X = T^{-1}A$ is done using backward substitution to obtain X from $TX = A$.
- b. Calculation of $Y = (T^{-1})^T A$ is done using forward substitution to obtain Y from $T^T Y = A$.
- c. Calculation of $Z = (T^T T)^{-1}A$ is done by first solving $T^T Y = A$ and then solving $TZ = Y$.

The remaining three operations are reducible to the above three.

2. Applications

Subroutines MTDS and DMTDS may be used to compute the solution of a system of equations $BX = A$ with symmetric positive definite coefficient matrix B. The first step towards the solution is the triangular factorization of B by means of subroutine MFSD or DMFSD. The second step, which may be repeated for different sets of right-hand sides A, is the calculation of $(T^T T)^{-1}A$ by means of MTDS or DMTDS with IOP = 3. Another useful application is the computation of the product $A^T B^{-1}A$ with symmetric positive definite B and arbitrary A in only three steps and without additional storage requirements:

- a. Replace B by T where $B = T^T T$.
- b. Replace A by $C = (T^T)^{-1}A$.
- c. Replace B by $C^T C$.

```

C .....
C SUBROUTINE MTD5
C .....
C PURPOSE
C MULTIPLY A GENERAL MATRIX A ON THE LEFT OF RIGHT BY
C INVERSE(T), INVERSE(TRANSPOSE(T)) OR INVERSE(TRANSPOSE(T)*T)
C THE TRIANGULAR MATRIX T IS STORED COLUMNWISE IN COMPRESSED
C FORM, I.E. UPPER TRIANGULAR PART ONLY.
C .....
C USAGE
C CALL MTD5(A,M,N,T, IOP, IER)
C .....
C DESCRIPTION OF PARAMETERS
C A - GIVEN GENERAL MATRIX WITH M ROWS AND N COLUMNS.
C M - NUMBER OF ROWS OF MATRIX A
C N - NUMBER OF COLUMNS OF MATRIX A
C T - GIVEN TRIANGULAR MATRIX STORED COLUMNWISE UPPER
C TRIANGULAR PART ONLY. ITS NUMBER OF ROWS AND
C COLUMNS K IS IMPLIED BY COMPATIBILITY.
C K = M IF IOP IS POSITIVE.
C K = N IF IOP IS NEGATIVE.
C T OCCUPIES K*(K+1)/2 STORAGE POSITIONS.
C IOP - INPUT VARIABLE FOR SELECTION OF OPERATION
C IOP = 1 - A IS REPLACED BY INVERSE(T)*A
C IOP = -1 - A IS REPLACED BY A*INVERSE(T)
C IOP = 2 - A IS REPLACED BY INVERSE(TRANSPOSE(T))*A
C IOP = -2 - A IS REPLACED BY A*INVERSE(TRANSPOSE(T))
C IOP = 3 - A IS REPLACED BY INVERSE(TRANSPOSE(T)*T)*A
C IOP = -3 - A IS REPLACED BY A*INVERSE(TRANSPOSE(T)*T)
C IER - RESULTING ERROR PARAMETER
C IER = -1 MEANS M AND N ARE NOT BOTH POSITIVE
C AND/OR IOP IS ILLEGAL
C IER = 0 MEANS OPERATION WAS SUCCESSFUL
C IER = 1 MEANS TRIANGULAR MATRIX T IS SINGULAR
C .....
C REMARKS
C SUBROUTINE MTD5 MAY BE USED TO CALCULATE THE SOLUTION OF
C A SYSTEM OF EQUATIONS WITH SYMMETRIC POSITIVE DEFINITE
C COEFFICIENT MATRIX. THE FIRST STEP TOWARDS THE SOLUTION
C IS TRIANGULAR FACTORIZATION BY MEANS OF MFD5. THE SECOND
C STEP IS APPLICATION OF MTD5.
C SUBROUTINES MFD5 AND MTD5 MAY BE USED IN ORDER TO CALCULATE
C THE PRODUCT TRANSPOSE(A)*INVERSE(B)*A WITH GIVEN SYMMETRIC
C POSITIVE DEFINITE A AND GIVEN B EFFICIENTLY IN THREE STEPS
C 1) TRIANGULAR FACTORIZATION OF B (B=TRANSPOSE(T)*T)
C 2) MULTIPLICATION OF A ON THE LEFT BY INVERSE(TRANSPOSE(T))
C A IS REPLACED BY C=INVERSE(TRANSPOSE(T))*A
C 3) CALCULATION OF THE RESULT FORMING TRANSPOSE(C)*C
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C .....
C METHOD
C CALCULATION OF X = INVERSE(T)*A IS DONE USING BACKWARD
C SUBSTITUTION TO OBTAIN X FROM TX = A.
C CALCULATION OF Y = INVERSE(TRANSPOSE(T))*A IS DONE USING
C FORWARD SUBSTITUTION TO OBTAIN Y FROM TRANSPOSE(T)*Y = A.
C CALCULATION OF Z = INVERSE(TRANSPOSE(T)*T)*A IS DONE
C SOLVING FIRST TRANSPOSE(T)*Y = A AND THEN TZ = Y. I.E.
C USING THE ABOVE TWO STEPS IN REVERSE ORDER
C .....
C SUBROUTINE MTD5(A,M,N,T, IOP, IER)
C .....
C DIMENSION L(1),T(1)
C DOUBLE PRECISION DUM
C .....
C TEST FOR DIMENSION
C IF (M).LT.1
C 1 IF (N).LT.1
C .....
C ERROR RETURN IN CASE OF ILLEGAL DIMENSIONS
C 2 IER=-1
C RETURN
C .....
C ERROR RETURN IN CASE OF SINGULAR MATRIX T
C 3 IER=1
C RETURN
C .....
C INITIALIZE DIVISION PROCESS
C 4 MN=M*N
C MDEL=M*(M+1)/2
C MDEL=M-1
C IOP=0
C ICS=M
C IRS=1
C IMEND=M
C .....
C TEST FOR ILLEGAL OPERATION
C IF (IOP).GT.3
C 5 MN=M*(M+1)/2
C MDEL=M-1
C IRS=M
C ICS=1
C IMEND=M*N+1
C MDEL=0
C .....
C IOP=M*DEL+(M+1)
C IF (ABS(IOP)-3).GT.7
C 7 IF (IOP-1).GT.18
C .....
C INITIALIZE SOLUTION OF TRANSPOSE(T)*X = A
C 8 MEND=1
C LD=1
C MST=M
C MDEL=1
C MX=1
C LD=1
C LX=0

```

```

C .....
C TEST FOR SINGULAR DIAGONAL TERM IN T
C IF (MST).EQ.0
C 10 DO 11 I=MND, MDEL
C 11 A(I)=A(I)/L(I*(MST+1))
C .....
C IS M SINGULAR
C IF (MDEL-1)
C 12 DO 14 J=1, M-1
C MST=MST+MDEL
C MDEL=MDEL-MX
C DO 14 I=MND, M-1
C DSUM=M*LD
C LEX=LX
C LEX=LX
C LL=1
C DO 13 K=1, J
C DSUM=DSUM+T(L)*A(KLL)
C LL=LL+LD
C LEX=LX
C 13 LEX=LX+K
C 14 A(LL)=D(SUM+A(LL))/T(LL)
C .....
C TEST END OF OPERATION
C 15 IF (IER).GT.1
C 16 IER=0
C RETURN
C 17 IF (IOP).GT.18
C .....
C INITIALIZE SOLUTION OF TX = A
C 18 IER=1
C MEND=IMEND
C MDEL=M
C LD=LD+1
C MST=M+M
C MDEL=M
C MX=0
C LD=M-1
C LX=1
C GOTO 9
C END

```

```

C .....
C SUBROUTINE DMTD5
C .....
C PURPOSE
C MULTIPLY A GENERAL MATRIX A ON THE LEFT OF RIGHT BY
C INVERSE(T), INVERSE(TRANSPOSE(T)) OR INVERSE(TRANSPOSE(T)*T)
C THE TRIANGULAR MATRIX T IS STORED COLUMNWISE IN COMPRESSED
C FORM, I.E. UPPER TRIANGULAR PART ONLY.
C .....
C USAGE
C CALL DMTD5(A,M,N,T, IOP, IER)
C .....
C DESCRIPTION OF PARAMETERS
C A - GIVEN GENERAL MATRIX WITH M ROWS AND N COLUMNS.
C M - A MUST BE OF DOUBLE PRECISION
C N - NUMBER OF ROWS OF MATRIX A
C T - GIVEN TRIANGULAR MATRIX STORED COLUMNWISE UPPER
C TRIANGULAR PART ONLY. ITS NUMBER OF ROWS AND
C COLUMNS K IS IMPLIED BY COMPATIBILITY.
C K = M IF IOP IS POSITIVE.
C K = N IF IOP IS NEGATIVE.
C T OCCUPIES K*(K+1)/2 STORAGE POSITIONS.
C T MUST BE OF DOUBLE PRECISION.
C IOP - INPUT VARIABLE FOR SELECTION OF OPERATION
C IOP = 1 - A IS REPLACED BY INVERSE(T)*A
C IOP = -1 - A IS REPLACED BY A*INVERSE(T)
C IOP = 2 - A IS REPLACED BY INVERSE(TRANSPOSE(T))*A
C IOP = -2 - A IS REPLACED BY A*INVERSE(TRANSPOSE(T))
C IOP = 3 - A IS REPLACED BY INVERSE(TRANSPOSE(T)*T)*A
C IOP = -3 - A IS REPLACED BY A*INVERSE(TRANSPOSE(T)*T)
C IER - RESULTING ERROR PARAMETER
C IER = -1 MEANS M AND N ARE NOT BOTH POSITIVE
C AND/OR IOP IS ILLEGAL
C IER = 0 MEANS OPERATION WAS SUCCESSFUL
C IER = 1 MEANS TRIANGULAR MATRIX T IS SINGULAR
C .....
C REMARKS
C SUBROUTINE DMTD5 MAY BE USED TO CALCULATE THE SOLUTION OF
C A SYSTEM OF EQUATIONS WITH SYMMETRIC POSITIVE DEFINITE
C COEFFICIENT MATRIX. THE FIRST STEP TOWARDS THE SOLUTION
C IS TRIANGULAR FACTORIZATION BY MEANS OF DMFD5. THE SECOND
C STEP IS APPLICATION OF DMTD5.
C SUBROUTINES DMFD5 AND DMTD5 MAY BE USED IN ORDER TO
C CALCULATE THE PRODUCT TRANSPOSE(A)*INVERSE(B)*A WITH GIVEN
C SYMMETRIC POSITIVE DEFINITE B AND GIVEN A IN THREE STEPS
C 1) TRIANGULAR FACTORIZATION OF B (B=TRANSPOSE(T)*T)
C 2) MULTIPLICATION OF A ON THE LEFT BY INVERSE(TRANSPOSE(T))
C A IS REPLACED BY C=INVERSE(TRANSPOSE(T))*A
C 3) CALCULATION OF THE RESULT FORMING TRANSPOSE(C)*C
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C .....
C METHOD
C CALCULATION OF X = INVERSE(T)*A IS DONE USING BACKWARD
C SUBSTITUTION TO OBTAIN X FROM TX = A.
C CALCULATION OF Y = INVERSE(TRANSPOSE(T))*A IS DONE USING
C FORWARD SUBSTITUTION TO OBTAIN Y FROM TRANSPOSE(T)*Y = A.
C CALCULATION OF Z = INVERSE(TRANSPOSE(T)*T)*A IS DONE
C SOLVING FIRST TRANSPOSE(T)*Y = A AND THEN TZ = Y. I.E.
C USING THE ABOVE TWO STEPS IN REVERSE ORDER

```

```

C .....DMTD 660
C SUBROUTINE DMTDS(A,M,N,T, IOP, IER) DMTD 670
C DMTD 680
C DMTD 690
C DMTD 700
C DIMENSION A(1),T(1) DMTD 710
C DOUBLE PRECISION DSUM,A,T DMTD 720
C TEST OF DIMENSION DMTD 730
1 IF(M)2,2,1 DMTD 740
1 IF(N)2,2,4 DMTD 750
C ERROR RETURN IN CASE OF ILLEGAL DIMENSIONS DMTD 760
2 IER=1 DMTD 770
RETURN DMTD 780
C ERROR RETURN IN CASE OF SINGULAR MATRIX T DMTD 790
3 IER=1 DMTD 800
RETURN DMTD 810
C INITIALIZE DIVISION PROCESS DMTD 820
4 MN=M*N DMTD 830
MM=(M+1)/2 DMTD 840
MM1=M-1 DMTD 850
IES=0 DMTD 860
ICS=M DMTD 870
IR5=1 DMTD 880
IMEND=M DMTD 890
C TEST SPECIFIED OPERATION DMTD 900
IF(IOP)5,2,6 DMTD 910
5 MM=N*(N+1)/2 DMTD 920
MM1=N-1 DMTD 930
IR5=M DMTD 940
ICS=1 DMTD 950
IMEND=MN-M+1 DMTD 960
MN=M DMTD 970
6 IOPE=MCD(IOP,3,3) DMTD 980
IF(IABS(IOP)-3)7,7,2 DMTD 990
7 IF(IOPE-1)8,18,8 DMTD1000
C INITIALIZE SOLUTION OF TRANSPOSE(T)*X = A DMTD1010
8 MEND=1 DMTD1020
LLD=IRS DMTD1030
MSTA=1 DMTD1040
DMTD1050
DMTD1060
DMTD1070
DMTD1080
DMTD1090
DMTD1100
MDEL=1
MX=1
LD=1
LX=0
C TEST FOR NONZERO DIAGONAL TERM IN T
9 IF(T(MSTA))10,3,10
10 DO 11 I=MEND,MN,ICS
11 A(I)=A(I)/T(MSTA)
C IS M EQUAL 1
IF(MM1)2,15,12
12 DO 14 J=1,MM1
MSTA=MSTA+MDEL
MDEL=MDEL+MX
DO 14 I=MEND,MN,ICS
USUM=0.00
L=MSTA
LDX=LD
LL=1
DO 13 K=1,J
OSUM=OSUM-T(L)*A(LL)
LL=LL+LLD
L=L+LDX
13 LDX=LDX+LX
IF(T(L))14,3,14
14 A(LL)=(OSUM+A(LL))/T(L)
C TEST END OF OPERATION
15 IF(IEF)16,17,16
16 IER=0
RETURN
17 IF(IOPE)18,18,16
C INITIALIZE SOLUTION OF T*X = A
18 IER=1
MEND=IMEND
MN=M*N
LLD=IRS
MSTA=MM
MDEL=-1
MX=0
LD=-MM1
LX=1
GOTO 9
END
DMTD1110
DMTD1120
DMTD1130
DMTD1140
DMTD1150
DMTD1160
DMTD1170
DMTD1180
DMTD1190
DMTD1200
DMTD1210
DMTD1220
DMTD1230
DMTD1240
DMTD1250
DMTD1260
DMTD1270
DMTD1280
DMTD1290
DMTD1300
DMTD1310
DMTD1320
DMTD1330
DMTD1340
DMTD1350
DMTD1360
DMTD1370
DMTD1380
DMTD1390
DMTD1400
DMTD1410
DMTD1420
DMTD1430
DMTD1440
DMTD1450
DMTD1460
DMTD1470
DMTD1480
DMTD1490
DMTD1500
DMTD1510
DMTD1520
DMTD1530
DMTD1540
DMTD1550

```

Subroutines MLSS and DMLSS

These subroutines will compute the least-squares solution of minimal length of a system of linear equations

$$AX = R \quad (1)$$

with symmetric positive semidefinite coefficient matrix A . That is, they will determine that vector X of smallest Euclidean length $\|X\|$ for which $\|AX - R\| = \text{minimum}$.

The matrix A is not used directly as input. Instead, MLSS expects the matrices U , T , and T_u and the permutation P that would be obtained if subroutine MFSS were used with A as input matrix (for details see MFSS under "Final result of elimination").

The given vector R is replaced by the solution vector X .

1. Mathematical background

Instead of (1), solve the system of equations:

$$(PAP^T)PX = PR \quad (2)$$

Any solution PX of (2) determines the solution $P^{-1}(PX)$ of (1); therefore it suffices to consider (2).

Using the decomposition:

$$PAP^T = \begin{bmatrix} I & O \\ U^T & I \end{bmatrix} \begin{bmatrix} A_S & O \\ O & O \end{bmatrix} \begin{bmatrix} I & U \\ O & I \end{bmatrix} \quad (3)$$

where $A_S = (T)^T T$ (see MFSS), it is easy to see that (2) is equivalent to the system:

$$A_S(X_1 + UX_2) = R_1 \quad (4)$$

$$OX_2 = R_2 - U^T R_1$$

where $PX = \begin{bmatrix} X_1 \\ X_2 \end{bmatrix}$ and $PR = \begin{bmatrix} R_1 \\ R_2 \end{bmatrix}$. If $\text{rank}(A) = n$,

formula (3) reduces to $PAP^T = A_S$, and (4) is

$$A_S X = R \quad (4')$$

In solving (2), or equivalently (4), three cases must be distinguished:

a. $\text{Rank}(A) = n$. Then the unique solution PX is given by $PX = A_S^{-1} R$, which is computed easily using the triangular decomposition $A_S = (T)^T T$.

b. $\text{Rank}(A) = r < n$ and $R_2 = U^T R_1$ (a compatible system). Then the solution of minimal length is:

$$X_1 = (I + UU^T)^{-1} T^{-1} (T^T)^{-1} T R_1$$

$$X_2 = U^T X_1$$

Using the identity $(I + UU^T)^{-1} = I - U(I + U^T U)^{-1} U^T$ and the triangular factorization of $(I + U^T U) = T_u^T T_u$, X_1 may be computed by the following sequence of operations:

$$X_1 = T^{-1} (T^T)^{-1} R_1$$

$$X_2 = T_u^{-1} (T_u^T)^{-1} T_u^T X_1$$

$$X_1 = X_1 - UX_2$$

c. $\text{Rank}(A) = r < n$ and $R_2 \neq U^T R_1$ (an incompatible system). Then the least-squares solution of minimal length is:

$$X_1 = (I + UU^T)^{-1} T^{-1} (T^T)^{-1} (I + UU^T)^{-1} (R_1 + UR_2)$$

$$X_2 = U^T X_1$$

X_1 may be computed using the following sequence of operations:

$$X_1 = R_1 + UR_2$$

$$X_2 = -T_u^{-1} (T_u^T)^{-1} T_u^T X_1$$

$$X_1 = T^{-1} (T^T)^{-1} (X_1 + UX_2)$$

$$X_2 = -T_u^{-1} (T_u^T)^{-1} T_u^T X_1$$

$$X_1 = X_1 + UX_2$$

2. Programming considerations

Cases a, b and c above are easily combined into one sequence of operations:

- (1) $X = PR$ (interchange given right-hand side)
- (2) $X_1 = X_1 + U X_2$
- (3) $X_2 = -U^T X_1$
- (4) $X_2 = (T_u)^{-1} ((T_u)^T)^{-1} X_2$
- (5) $X_1 = X_1 + U X_2$
- (6) $X_1 = T^{-1} (T^T)^{-1} X_1$
- (7) $X_2 = -U^T X_1$
- (8) $X_2 = (T_u)^{-1} ((T_u)^T)^{-1} X_2$
- (9) $X_1 = X_1 + U X_2$
- (10) $X_2 = (U^T) X_1$
- (11) $X = P^{-1} X$ (reinterchange calculated solution)

In case a, the only steps performed are (1), (6), (11). In case b, only steps (1) and (6) up to (11) are performed.

In case c, all steps are performed.

```

C
C
C ..... MLSS 10
C
C
C SUBROUTINE MLSS
C
C PURPOSE
C
C SUBROUTINE MLSS IS THE SECOND STEP IN THE PROCEDURE FOR
C CALCULATING THE LEAST SQUARES SOLUTION OF MINIMAL LENGTH
C OF A SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS WITH SYMMETRIC
C POSITIVE SEMI-DEFINITE COEFFICIENT MATRIX.
C
C USAGE
C
C CALL MLSS(A,N,IRANK,TRAC,INC,RHS,IER)
C
C DESCRIPTION OF PARAMETERS
C
C A - COEFFICIENT MATRIX IN FACTORED FORM AS GENERATED
C BY SUBROUTINE MFSS FROM INITIALLY GIVEN SYMMETRIC
C COEFFICIENT MATRIX A STORED IN N*(N+1)/2 LOCATIONS
C A REMAINS UNCHANGED
C
C N - DIMENSION OF COEFFICIENT MATRIX
C
C IRANK - RANK OF COEFFICIENT MATRIX, CALCULATED BY MEANS OF
C SUBROUTINE MFSS
C
C TRAC - VECTOR OF DIMENSION N CONTAINING THE
C SUBSCRIPTS OF PIVOT ROWS AND COLUMNS, I.E. THE
C PRODUCT REPRESENTATION IN TRANSPOSITIONS OF THE
C PERMUTATION WHICH WAS APPLIED TO ROWS AND COLUMNS
C OF A IN THE FACTORIZATION PROCESS
C
C TRAC IS A RESULTANT ARRAY OF SUBROUTINE MFSS
C
C INC - INPUT VARIABLE WHICH SHOULD CONTAIN THE VALUE ZERO
C IF THE SYSTEM OF SIMULTANEOUS EQUATIONS IS KNOWN
C TO BE COMPATIBLE AND A NONZERO VALUE OTHERWISE
C
C RHS - VECTOR OF DIMENSION N CONTAINING THE RIGHT HAND SIDE
C ON RETURN RHS CONTAINS THE MINIMAL LENGTH SOLUTION
C
C IER - RESULTANT ERROR PARAMETER
C
C IER = 0 MEANS NO ERRORS
C
C IER == 1 MEANS N AND/OR IRANK IS NOT POSITIVE AND/OR
C IRANK IS GREATER THAN N
C
C IER = 1 MEANS THE FACTORIZATION CONTAINED IN A HAS
C ZERO DIVISORS AND/OR TRAC CONTAINS
C VALUES OUTSIDE THE FEASIBLE RANGE 1 UP TO N
C
C REMARKS
C
C THE MINIMAL LENGTH SOLUTION IS PRODUCED IN THE STORAGE
C LOCATIONS OCCUPIED BY THE RIGHT HAND SIDE
C
C SUBROUTINE MLSS DOES TAKE CARE OF THE PERMUTATION
C WHICH WAS APPLIED TO ROWS AND COLUMNS OF A
C
C OPERATION IS BYPASSED IN CASE OF A NON POSITIVE VALUE
C OF IRANK
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C
C NONE
C
C METHOD
C
C LET T, U, TO BE THE COMPONENTS OF THE FACTORIZATION OF A,
C AND LET THE RIGHT HAND SIDE BE PARTITIONED INTO A FIRST
C PART X1 OF DIMENSION IRANK AND A SECOND PART X2 OF DIMENSION
C N-IRANK, THEN THE FOLLOWING OPERATIONS ARE APPLIED IN
C SEQUENCE
C
C (1) INTERCHANGE RIGHT HAND SIDE
C (2) X1 = X1 + U * X2
C (3) X2 = -TRANSPOSE(U) * X1
C (4) X2 = INVERSE(TU) * INVERSE(TRANSPOSE(TU) * X2)
C (5) X1 = X1 + U * X2
C (6) X1 = INVERSE(S1) * INVERSE(TRANSPOSE(S1) * X1)
C (7) X2 = -TRANSPOSE(U) * X1
C (8) X2 = INVERSE(TU) * INVERSE(TRANSPOSE(TU) * X2)
C (9) X1 = X1 + U * X2
C (10) X2 = TRANSPOSE(U) * X1
C (11) REINTERCHANGE CALCULATED SOLUTION
C
C IF THE SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS IS SPECIFIED
C TO BE COMPATIBLE THEN STEPS (2), (3), (4) AND (5) ARE
C CANCELLED.
C
C IF THE COEFFICIENT MATRIX HAS RANK N, THEN THE ONLY STEPS
C PERFORMED ARE (1), (6) AND (11).
C
C ..... MLSS 750
C
C SUBROUTINE MLSS(A,N,IRANK,TRAC,INC,RHS,IER)
C
C DIMENSIONED DIMMY VARIABLES
C
C DIMENSION A(1),TRAC(1),RHS(1)
C
C DOUBLE PRECISION SUM
C
C TEST OF SPECIFIED DIMENSIONS
C
C IDEF=N-IRANK
C
C 1 IF(N)33,33,1
C
C 2 IF(IRANK)33,33,2
C
C 1 IF(IDEF)33,33,2
C
C CALCULATE AUXILIARY VALUES
C
C 3 ITC=IRANK*(IRANK+1)/2
C
C IX2=IRANK*4
C
C NP1=N+1
C
C IER=0
C
C INTERCHANGE RIGHT HAND SIDE
C
C JJ=1
C
C II=1
C
C DO 5 I=1,N
C
C JJ=FRAC(II)
C
C IF(JJ)31,31,5
C
C 5 HOLD=RHS(II)
C
C FHS(II)=FHS(JJ)
C
C RHS(JJ)=HOLD
C
C II=II+JJ
C
C IF(JJ)32,7,7
C
C PERFORM STEP 2 IF NECESSARY
C
C 7 ISW=1
C
C IF(ITC*IDEF)9,28,8
C
C CALCULATE X1 = X1 + U * X2
C
C 8 ISTAT=ITE
C
C DO 10 I=1,IRANK
C
C ISTAT=I+1
C
C JJ=I+1
C
C SUM=0.00
C
C DO 9 J=I+1,N
C
C SUM=SUM+A(JJ)*RHS(JJ)
C
C 9 JJ=JJ+1
C
C 10 RHS(II)=RHS(II)+SUM
C
C GOTO(11,29,30),ISW
C
C CALCULATE X2 = TRANSPOSE(U) * X1
C
C 11 ISTAT=ITE
C
C DO 15 I=I+1,N
C
C JJ=I+1
C
C SUM=0.00

```

```

C
C
C DO 12 J=1,IRANK
C
C JJ=JJ+1
C
C 12 SUM=SUM+A(JJ)*RHS(JJ)
C
C GOTO(11,13,14),ISW
C
C 13 SUM=-SUM
C
C 14 FHS(II)=SUM
C
C 15 ISTAT=I+1
C
C GOTO(11,29,30),ISW
C
C INITIALIZE STEP (4) OF STEP (6)
C
C 16 ISTAT=IX2
C
C IEND=N
C
C JJ=ITE+I+1
C
C DIVISION OF X1 BY TRANSPOSE OF TRIANGULAR MATRIX
C
C 17 SUM=0.00
C
C DO 20 I=I+1,IEND
C
C IF(A(JJ)I)18,31,18
C
C FHS(II)=FHS(II)-SUM/A(JJ)
C
C IF(II=IEND)21,21
C
C 19 JJ=JJ+1
C
C SUM=0.00
C
C DO 20 J=I+1,I
C
C SUM=SUM+A(JJ)*FHS(JJ)
C
C JJ=JJ+1
C
C DIVISION OF X1 BY TRIANGULAR MATRIX
C
C 21 SUM=0.00
C
C II=IEND
C
C DO 24 I=I+1,IEND
C
C RHS(II)=(RHS(II)-SUM)/A(JJ)
C
C IF(II=I+1)25,29,22
C
C 22 KK=JJ-1
C
C SUM=0.00
C
C DO 23 J=II,IEND
C
C SUM=SUM+A(KK)*RHS(JJ)
C
C 23 KK=KK+1
C
C JJ=JJ-1
C
C 24 II=II-1
C
C 25 IF(IDEF)26,30,26
C
C 26 GOTO(27,11,6),ISW
C
C PERFORM STEP (5)
C
C 27 ISW=2
C
C GOTO 8
C
C PERFORM STEP (6)
C
C 28 ISTAT=1
C
C IEND=IRANK
C
C JJ=1
C
C ISW=2
C
C GOTO 17
C
C PERFORM STEP (8)
C
C 29 ISW=3
C
C GOTO 16
C
C REINTERCHANGE CALCULATED SOLUTION
C
C 30 IIN=
C
C JJ=1
C
C GOTO 4
C
C ERROR RETURN IN CASE OF ZERO DIVISOR
C
C 31 IER=1
C
C 32 RETURN
C
C ERROR RETURN IN CASE OF ILLEGAL DIMENSION
C
C 33 IER=-1
C
C RETURN
C
C END

```

DMLS 10
DMLS 20
DMLS 30
DMLS 40
DMLS 50
DMLS 60
DMLS 70
DMLS 80
DMLS 90
DMLS 100
DMLS 110
DMLS 120
DMLS 130
DMLS 140
DMLS 150
DMLS 160
DMLS 170
DMLS 180
DMLS 190
DMLS 200
DMLS 210
DMLS 220
DMLS 230
DMLS 240
DMLS 250
DMLS 260
DMLS 270
DMLS 280
DMLS 290
DMLS 300
DMLS 310
DMLS 320
DMLS 330
DMLS 340
DMLS 350
DMLS 360
DMLS 370
DMLS 380
DMLS 390
DMLS 400
DMLS 410
DMLS 420
DMLS 430
DMLS 440
DMLS 450
DMLS 460
DMLS 470
DMLS 480
DMLS 490
DMLS 500
DMLS 510
DMLS 520
DMLS 530
DMLS 540

```

C
C METHOD
C LEFT T, U, TO BE THE COMPONENTS OF THE FACTORIZATION OF A,
C AND LET THE RIGHT HAND SIDE BE PARTITIONED INTO A FIRST
C PART XI OF DIMENSION IRANK AND A SECOND PART X2 OF DIMENSION
C N-IRANK, THEN THE FOLLOWING OPERATIONS ARE APPLIED IN
C SEQUENCE
C (1) INTERCHANGE RIGHT HAND SIDE
C (2)  $X1 = X1 + U * X2$ 
C (3)  $X2 = -TRANSPOSE(U) * X1$ 
C (4)  $X2 = INVERSE(TU) * INVERSE(TRANSPOSE(TU)) * X2$ 
C (5)  $X1 = X1 + U * X2$ 
C (6)  $X1 = INVERSE(T) * INVERSE(TRANSPOSE(T)) * X1$ 
C (7)  $X2 = -TRANSPOSE(U) * X1$ 
C (8)  $X2 = INVERSE(TU) * INVERSE(TRANSPOSE(TU)) * X2$ 
C (9)  $X1 = X1 + U * X2$ 
C (10)  $X2 = TRANSPOSE(U) * X1$ 
C (11) REINTERCHANGE CALCULATED SOLUTION
C IF THE SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS IS SPECIFIED
C TO BE COMPATIBLE THEN STEPS (2), (3), (4) AND (5) ARE
C CANCELLED.
C IF THE COEFFICIENT MATRIX HAS RANK N, THEN THE ONLY STEPS
C PERFORMED ARE (1), (6) AND (11).
C
C .....
C SUBROUTINE DMLS(A,N,IRANK,TRAC,INC,RHS,IER)
C
C DIMENSIONED DUMMY VARIABLES
C DIMENSION A(1),TRAC(1),RHS(1)
C DOUBLE PRECISION SUM,A,RHS,TRAC,HOLD
C
C TEST OF SPECIFIED DIMENSIONS
C IDEF=N-IRANK
C IF(N)33,33,1
C 1 IF(IRANK)33,33,2
C 2 IF(IDEF)33,33,3
C
C CALCULATE AUXILIARY VALUES
C 3 IT=IRANK*(IRANK+1)/2
C IX2=IRANK+1
C NP1=N+1
C IER=0
C
C INTERCHANGE RIGHT HAND SIDE
C JJ=1
C II=1
C 4 DO 6 I=1,N
C J=TRAC(II)
C IF(I)31,31,5
C 5 HOLD=RHS(II)
C RHS(II)=RHS(J)
C RHS(J)=HOLD
C 6 II=II+JJ
C IF(JJ)2,7,7
C
C PERFORM STEP 2 IF NECESSARY
C 7 ISW=1
C IF(INEC)26,26,8
C
C CALCULATE  $X1 = X1 + U * X2$ 
C 8 ISTA=ITE
C DO 10 I=1,IRANK
C ISTA=ISTA+1
C JJ=ISTA
C SUM=0.00
C DO 9 J=IX2,N
C SUM=SUM+A(I,J)*RHS(J)
C 9 JJ=JJ+J
C 10 RHS(I)=RHS(I)+SUM
C GOTO(11,29,11),ISW
C
C CALCULATE  $X2 = TRANSPOSE(U) * X1$ 
C 11 ISTA=ITE
C DO 15 I=IX2,N
C JJ=ISTA
C SUM=0.00
C DO 12 J=1,IRANK
C JJ=JJ+1
C 12 SUM=SUM+A(I,J)*RHS(J)
C GOTO(13,13,14),ISW
C 13 SUM=-SUM
C 14 RHS(I)=SUM
C 15 ISTA=ISTA+1
C GOTO(16,29,30),ISW
C
C INITIALIZE STEP (4) OR STEP (8)
C 16 ISTA=IX2
C IEND=N
C JJ=ITE+ISTA
C
C DIVISION OF X1 BY TRANSPOSE OF TRIANGULAR MATRIX
C 17 SUM=0.00
C DO 20 I=ISTA,IEND
C IF(A(I,J))18,31,18
C 18 RHS(I)=RHS(I)-SUM/A(I,J)
C IF(I-ICNO)19,21,21
C 19 JJ=JJ+ISTA
C SUM=0.00
C DO 20 J=ISTA,I
C SUM=SUM+A(I,J)*RHS(J)
C 20 JJ=JJ+1
C
C DIVISION OF X1 BY TRIANGULAR MATRIX
C 21 SUM=0.00
C II=IFND
C DO 24 I=ISTA,IEND
C RHS(I)=RHS(I)-SUM/A(I,J)
C IF(II-ISTA)25,25,22
C 22 KK=JJ-1
C SUM=0.00
C DO 23 J=II,IEND
C SUM=SUM+A(I,K)*RHS(J)
C 23 KK=KK+J
C JJ=JJ-1
C 24 II=II-1
C 25 IF(IDEF)26,30,26
C 26 GOTO(27,11,8),ISW
C
C PERFORM STEP (5)
C 27 ISW=2
C GOTO 8
C
C PERFORM STEP (6)
C 28 ISTA=1
C IEND=IRANK
C JJ=1
C ISW=2

```

```

DMLS 550
DMLS 560
DMLS 570
DMLS 580
DMLS 590
DMLS 600
DMLS 610
DMLS 620
DMLS 630
DMLS 640
DMLS 650
DMLS 660
DMLS 670
DMLS 680
DMLS 690
DMLS 700
DMLS 710
DMLS 720
DMLS 730
DMLS 740
DMLS 750
DMLS 760
DMLS 770
DMLS 780
DMLS 790
DMLS 800
DMLS 810
DMLS 820
DMLS 830
DMLS 840
DMLS 850
DMLS 860
DMLS 870
DMLS 880
DMLS 890
DMLS 900
DMLS 910
DMLS 920
DMLS 930
DMLS 940
DMLS 950
DMLS 960
DMLS 970
DMLS 980
DMLS 990
DMLS1000
DMLS1010
DMLS1020
DMLS1030
DMLS1040
DMLS1050
DMLS1060
DMLS1070
DMLS1080
DMLS1090
DMLS1100
DMLS1110
DMLS1120
DMLS1130
DMLS1140
DMLS1150
DMLS1160
DMLS1170
DMLS1180
DMLS1190
DMLS1200
DMLS1210
DMLS1220
DMLS1230
DMLS1240
DMLS1250
DMLS1260
DMLS1270
DMLS1280
DMLS1290
DMLS1300
DMLS1310
DMLS1320
DMLS1330
DMLS1340
DMLS1350
DMLS1360
DMLS1370
DMLS1380
DMLS1390
DMLS1400
DMLS1410
DMLS1420
DMLS1430
DMLS1440
DMLS1450
DMLS1460
DMLS1470
DMLS1480
DMLS1490
DMLS1500
DMLS1510
DMLS1520
DMLS1530
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DMLS1550
DMLS1560
DMLS1570
DMLS1580
DMLS1590
DMLS1600
DMLS1610
DMLS1620
DMLS1630
DMLS1640
DMLS1650
DMLS1660
DMLS1670
DMLS1680
DMLS1690
DMLS1700
DMLS1710
DMLS1720
DMLS1730
DMLS1740
DMLS1750
DMLS1760
DMLS1770
DMLS1780
DMLS1790
DMLS1800
DMLS1810
DMLS1820
DMLS1830

```

```

GOTO 17
C
C PERFORM STEP (8)
C 29 ISW=3
C GOTO 16
C
C REINTERCHANGE CALCULATED SOLUTION
C 30 II=N
C JJ=1
C GOTO 4
C
C ERROR RETURN IN CASE OF ZERO DIVISOR
C 31 IEP=1
C 32 RETURN
C
C ERROR RETURN IN CASE OF ILLEGAL DIMENSION
C 33 IEP=-1
C RETURN
C END

```

```

DMLS1840
DMLS1850
DMLS1860
DMLS1870
DMLS1880
DMLS1890
DMLS1900
DMLS1910
DMLS1920
DMLS1930
DMLS1940
DMLS1950
DMLS1960
DMLS1970
DMLS1980
DMLS1990
DMLS2000
DMLS2010
DMLS2020

```

Subroutines MCHB and DMCHB

These subroutines will compute a triangular factorization

$$A = (T_u)^T T_u \tag{1}$$

of an m by m symmetric positive definite band matrix A. They may also be used to replace a given m by n matrix R by $A^{-1}R$, $T_u^{-1}R$, or $(T_u^{-1})^T R$, depending on the value of an input parameter IOP, as shown in Table 3.

1. Mathematical background

The upper triangular matrix T_u is computed using the following recursive formulas:

$$t_{kj} = (1/t_{kk}) (a_{kj} - \sum_{i=1}^{k-1} t_{ik} t_{ij}) \quad k = 1, \dots, m \tag{2}$$

$$j = k, k+1, \dots, m$$

(Any symbol $\sum_{i=j}^k x_i$ is to be interpreted as zero if $j > k$.)

In the special case $j = k$, equation (2) may be written:

$$t_{kk} = \sqrt{a_{kk} - \sum_{i=1}^{k-1} t_{ik}^2}, \quad k = 1, 2, \dots, m \tag{3}$$

When A is a symmetric band matrix with mud upper codiagonals, all elements a_{kj} are equal to zero if $j > k + mud$. From formulas (2) and (3) it is easy to see that the same is true for t_{kj} :

$$t_{kj} = 0 \text{ if } j > k + mud \tag{4}$$

Therefore formulas (2) and (3) reduce to:

$$t_{kj} = (1/t_{kk}) (a_{kj} - \sum_{i=i_0}^{k-1} t_{ik} t_{ij}) \quad k = 1, 2, \dots, m \tag{5}$$

$$j = k+1, \dots, \min(m, k+mud)$$

$$i_0 = \max(1, j-mud)$$

$$t_{kk} = \sqrt{a_{kk} - \sum_{i=i_0}^{k-1} t_{ik}^2} \quad k = 1, 2, \dots, m \tag{6}$$

$$i_0 = \max(1, k-mud)$$

Computing $(T_u^{-1})^T$ is equivalent to solving for Y in the system of equations:

$$T_u^T Y = R \tag{7}$$

The solution of (7) is computed using the following recursive scheme:

$$y_{kj} = (1/t_{kk}) (r_{kj} - \sum_{i=i_0}^{k-1} t_{ik} y_{ij}) \quad k = 1, 2, \dots, m \tag{8}$$

$$j = 1, 2, \dots, n$$

$$i_0 = \max(1, k-mud)$$

After each y_{kj} is computed, it may be stored in the location of r_{kj} .

Analogously, computing $T_u^{-1} R$ is the same as solving for X in the system of equations:

$$T_u X = R \tag{9}$$

The solution of (9) is given using a similar recursive scheme:

$$x_{kj} = (1/t_{kk}) (r_{kj} - \sum_{i=k+1}^{i_0} t_{ki} x_{ij}) \quad k = m, m-1, \dots, 1 \tag{10}$$

$$j = 1, 2, \dots, n$$

$$i_0 = \min(m, k+mud)$$

$A^{-1}R$ is computed by first computing $S = (T_u^T)^{-1}R$ in the locations of R, and then computing $T_u^{-1}S$, again in the locations of R. If $R = I$, this process replaces R with the inverse A^{-1} of A. Note that in general A^{-1} is no longer a band matrix.

2. Programming considerations

The input matrix A is assumed to be stored in compressed form, that is, main diagonal and mud upper codiagonals rowwise in successive storage locations. Therefore, the total storage requirement for matrix A is $m + mud(2m-mud-1)/2$ storage locations. The general m by n matrix R is assumed to be stored columnwise in nm successive storage locations.

The operations performed by the subroutines depend on the actual value of the decision parameter IOP.

Table 3 shows input and output depending on the value of IOP.

Table 3. Dependence of Input and Output on IOP

		IOP	0	1	-1	2	-2	3	-3
INPUT	A in compressed form	A	A	T _u	A	T _u	A	T _u	T _u
	R column-wise	irrelevant	R	R	R	R	R	R	R
OUTPUT	A in compressed form	T _u	T _u	T _u	T _u	T _u	T _u	T _u	T _u
	R column-wise	unchanged	A ⁻¹ R	A ⁻¹ R	T _u ⁻¹ R	T _u ⁻¹ R	(T _u ⁻¹) ^T R	(T _u ⁻¹) ^T R	

If IOP is not equal to one of the values listed in Table 3, no action except error message IER = -1 takes place. In this case A and R remain unchanged. The same is true if mud (the number of upper codiagonals of A) is negative or if m (the number of rows of A) is less than 1+mud.

There is one way in which the factorization described above may fail to give a solution, which is easily seen from equation (6). If at any step the radicand of equation (6) is not positive, the procedure is bypassed, and the error message IER = -1 is given. The interpretation may be that matrix A is not positive-definite; however, failure is also possible due to roundoff errors.

Backsubstitutions may fail too, as is easily seen from equations (8) and (10). If any main diagonal element of T_u is equal to zero (this is only possible if T_u is given by input), the procedure is bypassed, and the error message IER = -1 is given.

A further test on possible loss of significance in the factorization part is performed by the subroutines. If at the kth factorization step the radicand of equation (6) is not greater than |EPS* a_{kk}|, with the relative tolerance EPS given by input, the subroutines give the message IER = k-1.

For subroutine MCHB a relative tolerance between 10⁻⁶ and 10⁻⁷ is suggested, and for subroutine DMCHB, between 10⁻¹⁴ and 10⁻¹⁶. The message IER = k-1, in case EPS = 10^{-D}, means that there are about D or more significant digits lost in the computation of the radicand in formula (6) at the kth factorization step. The interpretation may be that there is loss of significance in the factorized matrix from the kth row on, while the results of rows 1 up to k-1 may be better. Loss of significance in the lower part of the factorized matrix may affect the results of matrix divisions.

For reference see H. Rutishauser, "Algorithmus 1 - Lineares Gleichungssystem mit symmetrischer positiv-definiten Bandmatrix nach Cholesky-Computing," Archives for Electronic Computing, vol. 1, iss. 1 (1966), pp. 77-78.

C										MCHB 10
C										MCHB 20
C										MCHB 30
C										MCHB 40
C										MCHB 50
C										MCHB 50
C										MCHB 70
C										MCHB 80
C										MCHB 90
C										MCHB 100
C										MCHB 110
C										MCHB 120
C										MCHB 130
C										MCHB 140
C										MCHB 150
C										MCHB 160
C										MCHB 170
C										MCHB 190
C										MCHB 200
C										MCHB 210
C										MCHB 220
C										MCHB 230
C										MCHB 240
C										MCHB 250
C										MCHB 250
C										MCHB 270
C										MCHB 280
C										MCHB 290
C										MCHB 300
C										MCHB 310
C										MCHB 320
C										MCHB 330
C										MCHB 340
C										MCHB 350
C										MCHB 360
C										MCHB 370
C										MCHB 380
C										MCHB 390
C										MCHB 400
C										MCHB 410
C										MCHB 420
C										MCHB 430
C										MCHB 440
C										MCHB 450
C										MCHB 460
C										MCHB 470
C										MCHB 480
C										MCHB 490
C										MCHB 500
C										MCHB 510
C										MCHB 520
C										MCHB 530
C										MCHB 540
C										MCHB 550
C										MCHB 570
C										MCHB 580
C										MCHB 590
C										MCHB 600
C										MCHB 610
C										MCHB 670
C										MCHB 680
C										MCHB 690
C										MCHB 700
C										MCHB 710
C										MCHB 720
C										MCHB 730
C										MCHB 740
C										MCHB 750
C										MCHB 760
C										MCHB 770
C										MCHB 780
C										MCHB 790
C										MCHB 800
C										MCHB 810
C										MCHB 820
C										MCHB 830
C										MCHB 840
C										MCHB 850
C										MCHB 860
C										MCHB 870
C										MCHB 880
C										MCHB 890
C										MCHB 900
C										MCHB 910
C										MCHB 920
C										MCHB 930
C										MCHB 940
C										MCHB 950
C										MCHB 960
C										MCHB 970
C										MCHB 980
C										MCHB 990
C										MCH1000
C										MCH1010
C										MCH1020
C										MCH1030
C										MCH1040
C										MCH1050
C										MCH1060
C										MCH1070
C										MCH1080
C										MCH1090
C										MCH1100
C										MCH1110
C										MCH1120
C										MCH1130
C										MCH1140
C										MCH1150
C										MCH1160
C										MCH1170
C										MCH1180
C										MCH1190
C										MCH1200
C										MCH1210
C										MCH1220
C										MCH1230
C										MCH1240
C										MCH1250
C										MCH1260
C										MCH1270
C										MCH1280
C										MCH1290

```

IEND=IST+MUD
J=K-M
IF(J)4,4,5
5 IEND=IEND-J
6 IF(J-1)4,3,7
7 LLDST=LLDST-1
8 LMAX=MUD
J=K-K
IF(J)10,10,9
9 LMAX=LMAX-J
10 ID=0
TOL=ALIST*EPS
C
START FACTORIZATION-LOOP OVER K-TH ROW
DO 23 I=1ST,IEND
SUM=0,0
IF(LMAX)1,14,11
C
PREPARE INNER LOOP
11 LL=IST
LLD=LLDST
C
START INNER LOOP
DO 13 L=1,LMAX
LL=LL-LLD
LL+LL+1D
SUM=SUM+A(LL)*A(LL)
IF(LLD-MUD)12,13,13
12 LLD=LLD+1
13 CONTINUE
END OF INNER LOOP
C
TRANSFORM ELEMENT A(I)
14 SUM=DOUBLE(A(I))-SUM
IF(I-1ST)15,15,20
C
A(I) IS DIAGONAL ELEMENT, ERROR TEST.
15 IF(SUM)43,16
C
TEST IN LOSS OF SIGNIFICANT DIGITS AND WARNING.
16 IF(SUM-TOL)17,17,19
17 IF(IEP)14,14,16
18 IER=-1
C
COMPUTATION OF PIVOT ELEMENT
19 PIV=DOUBLE(SUM)
A(I)=PIV
PIV=1,0D0/PIV
GO TO 21
C
A(I) IS NOT DIAGONAL ELEMENT
20 A(I)=SUM*PIV
C
UPDATE ID AND LMAX
21 ID=ID+1
IF(ID-J)22,22,22
22 LMAX=LMAX+1
23 CONTINUE
C
END OF FACTORIZATION-LOOP OVER K-TH ROW
END OF FACTORIZATION OF MATRIX A
C
*****
PREPARE MATRIX DIVISIONS
IF(IP)24,44,24
24 ID=MM
IFND=ABS(ID)-2
IF(IEND)25,35,25
C
*****
START DIVISION BY TRANSPOSE OF MATRIX TU (TU IS STORED IN
LOCATIONS OF A)
25 IST=1
LMAX=J
J=M
LLDST=M
DO 34 L=1,M
PIV=A(LL)
IF(PIV)26,43,26
26 PIV=1,0D0/PIV
C
START BACKSUBSTITUTION-LOOP FOR K-TH ROW OF MATRIX B
DO 30 I=1,1D,M
SUM=0,0
IF(LMAX)30,30,27
C
PREPARE INNER LOOP
27 LL=IST
LLL=I
LLD=LLDST
C
START INNER LOOP
DO 29 L=1,LMAX
LL=LL-LLD
LL+LL+1
SUM=SUM+A(LL)*A(LL)
IF(LLD-MUD)28,29,29
28 LLD=LLD+1
29 CONTINUE
END OF INNER LOOP
C
TRANSFORM ELEMENT P(I)
30 P(I)=PIV*(DOUBLE(P(I))-SUM)
END OF BACKSUBSTITUTION-LOOP FOR K-TH ROW OF MATRIX B
C
UPDATE PARAMETERS LMAX, IST AND LLDST
IF(MC-K)32,32,31
31 LMAX=K
32 IST=IST+K
J=J+1
IF(J)34,34,33
33 IST=IST-J
LLDST=LLDST-1
34 CONTINUE
C
END OF DIVISION BY TRANSPOSE OF MATRIX TU
C
*****
START DIVISION BY MATRIX TU (TU IS STORED ON LOCATIONS OF A)
IF(IEND)35,35,44
35 IST=IMUD*(M+M-1)/2+1
LMAX=0
K=M
IEND=IST-1
IST=IEND-LMAX
PIV=A(IST)
MCH1300
MCH1310
MCH1320
MCH1330
MCH1340
MCH1350
MCH1360
MCH1370
MCH1380
MCH1390
MCH1400
MCH1410
MCH1420
MCH1430
MCH1440
MCH1450
MCH1460
MCH1470
MCH1480
MCH1490
MCH1500
MCH1510
MCH1520
MCH1530
MCH1540
MCH1550
MCH1560
MCH1570
MCH1580
MCH1590
MCH1600
MCH1610
MCH1620
MCH1630
MCH1640
MCH1650
MCH1660
MCH1670
MCH1680
MCH1690
MCH1700
MCH1710
MCH1720
MCH1730
MCH1740
MCH1750
MCH1760
MCH1770
MCH1780
MCH1790
MCH1800
MCH1810
MCH1820
MCH1830
MCH1840
MCH1850
MCH1860
MCH1870
MCH1880
MCH1890
MCH1900
MCH1910
MCH1920
MCH1930
MCH1940
MCH1950
MCH1960
MCH1970
MCH1980
MCH1990
MCH2000
MCH2010
MCH2020
MCH2030
MCH2040
MCH2050
MCH2060
MCH2070
MCH2080
MCH2090
MCH2100
MCH2110
MCH2120
MCH2130
MCH2140
MCH2150
MCH2160
MCH2170
MCH2180
MCH2190
MCH2200
MCH2210
MCH2220
MCH2230
MCH2240
MCH2250
MCH2260
MCH2270
MCH2280
MCH2290
MCH2300
MCH2310
MCH2320
MCH2330
MCH2340
MCH2350
MCH2360
MCH2370
MCH2380
MCH2390
MCH2400
MCH2410
MCH2420
MCH2430
MCH2440
MCH2450
MCH2460
MCH2470
MCH2480
MCH2490
MCH2500
MCH2510
MCH2520
MCH2530
MCH2540
MCH2550
MCH2560
MCH2570
MCH2580
MCH2590
MCH2600
MCH2610
MCH2620
MCH2630
MCH2640
MCH2650
MCH2660
MCH2670
MCH2680
MCH2690
MCH2700
MCH2710
MCH2720
MCH2730
MCH2740
MCH2750
MCH2760
MCH2770
MCH2780
MCH2790
MCH2800
MCH2810
MCH2820
MCH2830
MCH2840
MCH2850
MCH2860
MCH2870
MCH2880
MCH2890
MCH2900
MCH2910
MCH2920
MCH2930
MCH2940
MCH2590
MCH2600
MCH2610
MCH2620
MCH2630
MCH2640
MCH2650
MCH2660
MCH2670
MCH2680
MCH2690
MCH2700
MCH2710
MCH2720
MCH2730
MCH2740
MCH2750
MCH2760
MCH2770
MCH2780
MCH2790
MCH2800
MCH2810
MCH2820
MCH2830
MCH2840
MCH2850
MCH2860
MCH2870
MCH2880
MCH2890
MCH2900
MCH2910
MCH2920
MCH2930
MCH2940
IF(PIV)37,43,37
37 PIV=1,0D0/PIV
L=IST+1
C
START BACKSUBSTITUTION-LOOP FOR K-TH ROW OF MATRIX P
DO 40 I=1,1D,M
SUM=0,0
IF(LMAX)40,40,38
38 LLL=I
C
START INNER LOOP
DO 39 L=1,LEND
LLL=LLL+1
39 SUM=SUM+A(LL)*A(LL)
END OF INNER LOOP
C
TRANSFORM ELEMENT P(I)
40 P(I)=PIV*(DOUBLE(P(I))-SUM)
END OF BACKSUBSTITUTION-LOOP FOR K-TH ROW OF MATRIX P
C
UPDATE PARAMETERS LMAX AND K
IF(K-M)42,42,41
41 LMAX=LMAX+1
42 K=K-1
IF(K)44,44,36
C
END OF DIVISION BY MATRIX TU
C
*****
ERROR EXIT IN CASE OF WRONG INPUT PARAMETERS OR PIVOT ELEMENT
LESS THAN OR EQUAL TO ZERO
43 IER=-1
44 RETURN
END
DMCH 10
DMCH 20
SUBROUTINE DMCH
DMCH 30
DMCH 40
DMCH 50
DMCH 60
DMCH 70
DMCH 80
DMCH 90
DMCH 100
DMCH 110
DMCH 120
DMCH 130
DMCH 140
DMCH 150
DMCH 160
DMCH 170
DMCH 180
DMCH 190
DMCH 200
DMCH 210
DMCH 220
DMCH 230
DMCH 240
DMCH 250
DMCH 260
DMCH 270
DMCH 280
DMCH 290
DMCH 300
DMCH 310
DMCH 320
DMCH 330
DMCH 340
DMCH 350
DMCH 360
DMCH 370
DMCH 380
DMCH 390
DMCH 400
DMCH 410
DMCH 420
DMCH 430
DMCH 440
DMCH 450
DMCH 460
DMCH 470
DMCH 480
DMCH 490
DMCH 500
DMCH 510
DMCH 520
DMCH 530
DMCH 540
DMCH 550
DMCH 560
DMCH 570
DMCH 580
DMCH 590
DMCH 600
DMCH 610
DMCH 620
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DMCH 640
DMCH 650
DMCH 660
DMCH 670
DMCH 680
DMCH 690
DMCH 700
DMCH 710
DMCH 720
DMCH 730
DMCH 740
DMCH 750
DMCH 760
DMCH 770
DMCH 780
DMCH 790
DMCH 800
DMCH 810
DMCH 820
DMCH 830
DMCH 840
DMCH 850
DMCH 860
DMCH 870
DMCH 880
DMCH 890
DMCH 900
DMCH 910
DMCH 920
DMCH 930
DMCH 940
DMCH 950
DMCH 960
DMCH 970
DMCH 980
DMCH 990

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C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C
C METHOD
C FACTORIZATION IS DONE USING CHOLSKY-S SQUARE-ROOT METHOD,
C WHICH GENERATES THE UPPER BAND MATRIX TO SUCH THAT
C TRANSPOSE(TU)*TU=A. TU IS DEFINED AS RESULT ON THE
C LOCATIONS OF A. FURTHER, DEPENDENT ON THE ACTUAL VALUE OF
C TOP, DIVISION OF  $\rho$  BY TRANSPOSE(TU) AND/OR TU IS PERFORMED
C AND THE RESULT IS RETURNED ON THE LOCATIONS OF  $\rho$ .
C FOR REFERENCE, SEE H. FUJISHEPERS, ALGORITHMUS 1 - LINEARES
C GLEICHUNGSSYSTEM MIT SYMMETRISCHER POSITIV-DEFINITIV
C BANDMATRIX NACH CHOLESKY - , COMPUTING (ARCHIVES FOR
C ELECTRONIC COMPUTING), VOL.1, ISS.1 (1966), PP.77-78.
C
C .....
C SUBROUTINE DMCHEIR,A,M,P,MUD,IPR,IPS,IER)
C
C DIMENSION K(1),A(1)
C DOUBLE PRECISION TOL,SUM,PIV,R,A
C
C TEST ON WRONG INPUT PARAMETERS
C IF(IABS(TOP)-311,1,43
C 1 IF(MOD)43,2,7
C 2 MC=MUD+1
C IF(M-MC)43,3,3
C 3 MR=M-MUD
C IPR=0
C
C MC IS THE MAXIMUM NUMBER OF ELEMENTS IN THE ROWS OF ARRAY A
C MR IS THE INDEX OF THE LAST ROW IN ARRAY A WITH MC ELEMENTS
C
C .....
C START FACTORIZATION OF MATRIX A
C IF(IOP)24,44,4
C IEND=0
C LLDST=MUD
C DO 21 K=1,M
C IST=IEND+1
C IEND=IST+MUD
C J=K-MR
C IF(J)16,4,5
C 5 IEND=IEND-J
C 6 IF(J-1)8,9,7
C 7 LLDST=LLDST-1
C 8 LMAX=MUD
C J=MC-K
C IF(J)10,10,9
C 9 LMAX=LMAX-J
C 10 ID=0
C TOL=A(IIST)*EPS
C
C START FACTORIZATION-LOOP OVER K-TH ROW
C DO 23 I=IST,IEND
C SUM=0.00
C IF(LMAX)14,14,11
C
C PREPARE INNER LOOP
C 11 LL=IST
C LLD=LLDST
C
C START INNER LOOP
C DO 13 L=1,LMAX
C LL=LL-LLD
C LLL=LL+LD
C SUM=SUM+A(LLL)*A(LLL)
C IF(LLD-MUD)12,13,13
C 12 LL=LLD+1
C 13 CONTINUE
C
C END OF INNER LOOP
C
C TRANSFORM ELEMENT A(I)
C 14 SUM=A(II)-SUM
C IF(I-IST)15,15,20
C
C A(II) IS DIAGONAL ELEMENT. ERROR TEST.
C 15 IF(SUM)143,43,16
C
C TEST ON LOSS OF SIGNIFICANT DIGITS AND WARNING
C 16 IF(SUM-TOL)17,17,19
C 17 IF(I)18,18,19
C 18 IEP=K-1
C
C COMPUTATION OF PIVOT ELEMENT
C 19 PIV=DSORT(SUM)
C A(II)=PIV
C PIV=1.00/PIV
C GO TO 21
C
C A(II) IS NOT DIAGONAL ELEMENT
C 20 A(II)=SUM*PIV
C
C UPDATE ID AND LMAX
C 21 ID=ID+1
C IF(I-ID)23,23,22
C 22 LMAX=LMAX-1
C 23 CONTINUE
C
C END OF FACTORIZATION-LOOP OVER K-TH ROW
C END OF FACTORIZATION OF MATRIX A
C
C .....
C PREPARE MATRIX DIVISIONS
C IF(IOP)24,44,24
C 24 ID=N*M
C IEND=IABS(TOP)-2
C IF(IEND)25,35,25
C
C .....
C START DIVISION BY TRANSPOSE OF MATRIX TU (TU IS STORED IN
C LOCATIONS OF A)
C 25 IST=1
C LMAX=0
C J=MP
C LLDST=MUD
C DO 34 K=1,M
C PIV=A(IIST)
C IF(PIV)26,43,26
C 26 PIV=1.00/PIV
C
C STA-T BACKSUBSTITUTION-LOOP FOR K-TH ROW OF MATRIX R
C DO 30 I=K,LD,M
C SUM=0.00
C
C IF(LMAX)30,30,27
C
C PREPARE INNER LOOP
C 27 LL=IST
C LLL=I
C LLD=LLDST
C
C START INNER LOOP
C DO 29 L=1,LMAX
C LL=LL-LLD
C LLL=LLL-1
C SUM=SUM+A(LLL)*R(LLL)
C IF(LLD-MUD)28,29,29
C 28 LL=LD+1
C 29 CONTINUE
C
C END OF INNER LOOP
C
C TRANSFORM ELEMENT R(I)
C 30 R(I)=PIV*(R(I)-SUM)
C
C END OF BACKSUBSTITUTION-LOOP FOR K-TH ROW OF MATRIX R
C
C UPDATE PARAMETERS LMAX, IST AND LDST
C IF(MC-K)32,32,31
C 31 LMAX=K
C 32 IST=IST+MC
C J=J+1
C IF(J)34,34,33
C 33 IST=IST-J
C LDST=LDST-1
C 34 CONTINUE
C
C END OF DIVISION BY TRANSPOSE OF MATRIX TU
C
C .....
C START DIVISION BY MATRIX TU (TU IS STORED ON LOCATIONS OF A)
C IF(IEND)35,35,44
C 35 IST=M+(MUD*(M+M-MC))/2+1
C LMAX=0
C K=M
C 36 IEND=IST-1
C IST=IEND-LMAX
C PIV=A(IIST)
C IF(PIV)37,43,37
C 37 PIV=1.00/PIV
C L=IST+1
C
C START BACKSUBSTITUTION-LOOP FOR K-TH ROW OF MATRIX R
C DO 40 I=K,LD,M
C SUM=0.00
C IF(LMAX)40,40,33
C 38 LLL=I
C
C START INNER LOOP
C DO 39 I=1,IEND
C LLL=LLL-1
C 39 SUM=SUM+A(LLL)*R(LLL)
C
C END OF INNER LOOP
C
C TRANSFORM ELEMENT R(I)
C 40 R(I)=PIV*(R(I)-SUM)
C
C END OF BACKSUBSTITUTION-LOOP FOR K-TH ROW OF MATRIX R
C
C UPDATE PARAMETERS LMAX AND K
C IF(K-MR)42,42,41
C 41 LMAX=LMAX+1
C 42 K=K-1
C IF(K)44,44,36
C
C END OF DIVISION BY MATRIX TU
C
C .....
C ERROR EXIT IN CASE OF WRONG INPUT PARAMETERS OR PIVOT ELEMENT
C LESS THAN OR EQUAL TO ZERO
C 43 IFR=-1
C 44 RETURN
C END

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Subroutine MFSS and DMFSS

Given a symmetric positive semidefinite matrix A, MFSS will:

- (1) Determine the rank and linearly independent rows (and columns)
- (2) Compute a triangular factorization of a symmetric submatrix of maximal rank
- (3) Express nonbasic rows (and columns) in terms of basic ones and express nonbasic variables in terms of free ones.

1. Mathematical background

The rank is determined using the method of Cholesky (square root method) with pivoting along the main diagonal. Pivoting on diagonal elements means that the same permutation is applied to the rows and columns of A, thereby preserving symmetry. The interchange information is recorded in the auxiliary vector TRAC. The notation A^m is used for the interchanged matrix determined during the mth step. The given matrix A is assumed to be stored columnwise in compressed form, that is, upper triangular part only.

$$A = \begin{bmatrix} a_{11} & a_{12} & \dots & a_{1n} \\ & a_{22} & \dots & a_{2n} \\ & & & a_{nn} \end{bmatrix}$$

To allow for easy pivoting, the diagonal terms of A are moved into vector TRAC.

The following two facts will be used repeatedly:

- (I) If $S = (s_{ik})$ is symmetric with $s_{11} > 0$, then S admits the unique decomposition:

$$S = \begin{bmatrix} t & 0 \\ V^T & I \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & D \end{bmatrix} \begin{bmatrix} t & V \\ 0 & I \end{bmatrix} = \tag{1}$$

$$\begin{bmatrix} s_{11} & s_{12} \\ s_{21} & s_{22} \end{bmatrix}$$

where $t = \sqrt{s_{11}}$, $V = (1/t)S_{12}$ and $D = S_{22} - V^T V$.

- (II) If S is symmetric positive semidefinite:

$$s_{jj} \geq 0 \text{ for all } j \text{ and } |s_{ik}| \leq \max_j (s_{jj}) \text{ for all } i, k \tag{2}$$

a. First step

Let $a_{jj} = \max_i (a_{ij})$. If $a_{jj} = 0$, formula (2) implies

$A = 0$, and further calculations are bypassed. Assuming $a_{jj} > 0$, rows 1 and $k_1 = j$ and columns 1 and k_1 of A are interchanged, obtaining A^1 .

TRAC(k_1) is replaced by TRAC(1), and k_1 is stored in TRAC(1). Decomposition of A^1 gives:

$$A^1 = \begin{bmatrix} A_{11}^1 & A_{12}^1 \\ A_{21}^1 & A_{22}^1 \end{bmatrix} = \begin{bmatrix} t_{11}^1 & 0 \\ (V^1)^T & I \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & D^1 \end{bmatrix} \begin{bmatrix} t_{11}^1 & V^1 \\ 0 & I \end{bmatrix}$$

where $t_{11}^1 = \sqrt{a_{11}^1}$, $V^1 = (1/t_{11}^1)A_{12}^1$ and

$D^1 = A_{22}^1 - (V^1)^T V^1$. D^1 is not calculated explicitly, only its diagonal terms are computed and stored in locations TRAC(2) through TRAC(n).

The first row of A^1 is replaced by t_{11}^1, V^1 . The compressed storage scheme now looks like this:

$$\begin{matrix} t_{11}^1 & V^1 \\ & A_{22}^1 \end{matrix}$$

b. General step

Suppose that after m steps ($1 \leq m < n$) we have determined a transposition vector (k_1, k_2, \dots, k_m) , an m by m nonsingular upper triangular matrix:

$$T^m = \begin{bmatrix} t_{11}^1 & t_{12}^2 & \dots & t_{1m}^m \\ & t_{22}^2 & \dots & t_{2m}^m \\ & & & t_{mm}^m \end{bmatrix}$$

an m by (n-m) matrix:

$$V^m = \begin{bmatrix} v_1^m \\ v_2^m \\ \vdots \\ v_m^m \end{bmatrix}$$

and an $(n-m)$ by $(n-m)$ matrix D^m such that:

$$A^m = \begin{bmatrix} A_{11}^m & A_{12}^m \\ A_{21}^m & A_{22}^m \end{bmatrix} = \begin{bmatrix} (T^m)^T & 0 \\ (V^m)^T & I \end{bmatrix} \cdot \begin{bmatrix} I & 0 \\ 0 & D^m \end{bmatrix} = \begin{bmatrix} T^m & V^m \\ 0 & I \end{bmatrix} \quad (3)$$

where $A^m = P^m A (P^m)^T$, and P^m is the permutation matrix associated with the transposition vector (k_1, \dots, k_m) . Again, D^m is not known explicitly, but is computable from:

$$D^m = A_{22}^m - (V^m)^T V^m \quad (4)$$

T^m , V^m and A_{22}^m are assumed to be stored in the following way:

$$\begin{array}{cc} T^m & V^m \\ & A_{22}^m \end{array}$$

If $A_{22}^m = 0$, it follows from (4) and the fact that D^m is positive semidefinite that $D^m = 0$. Then (3) is the desired factorization, and the process terminates. If $A_{22}^m \neq 0$, there is at least one positive diagonal term a_{kk}^m , and we may compute:

$$t = d_{jj}^m / a_{jj}^m = \max_k \left\{ d_{kk}^m / a_{kk}^m \mid a_{kk}^m > 0 \right\}$$

$$\text{From (4) and (2), } \max_{i,k} |d_{ik}^m| \leq t \max_{i,k} |a_{ik}^m|.$$

If $t \leq \epsilon$, the norm of D^m is small compared to the norm of A_{22}^m , and we interpret this as $D^m = 0$. Assuming $t > \epsilon$, rows $m+1$ and $k_{m+1} = m+j$ and columns $m+1$ and k_{m+1} are interchanged in the compressed storage areas, obtaining

$$\begin{array}{cc} T^m & V^m \\ & A_{22}^m \end{array}$$

TRAC(k_{m+1}) is replaced by TRAC($m+1$), and k_{m+1} is stored in TRAC($m+1$). As a result of these interchanges:

$$QA^m Q = \begin{bmatrix} (T^m)^T & 0 \\ (V^m)^T & I \end{bmatrix} \begin{bmatrix} I & 0 \\ 0 & D^m \end{bmatrix} \begin{bmatrix} T^m & V^m \\ 0 & I \end{bmatrix} \quad (5)$$

where $D^m = A_{22}^m - (V^m)^T V^m$, and Q is the permutation matrix associated with the transposition $(m+1, k_{m+1})$. Now decompose D^m :

$$D^m = \begin{bmatrix} t_{m+1, m+1}^{m+1} & 0 \\ (V^{m+1})^T & I \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & D^{m+1} \end{bmatrix}$$

$$\begin{bmatrix} t_{m+1, m+1}^{m+1} & V_{m+1}^{m+1} \\ 0 & I \end{bmatrix}$$

and store $t_{m+1, m+1}^{m+1}$, V_{m+1}^{m+1} in the first row of A_{22}^{m+1} . Let A_{22}^{m+1} denote the remaining rows and columns of A_{22}^m , and rename the elements of V^m as follows:

$$V^m = \begin{bmatrix} t_{1, m+1}^{m+1} & V_1^{m+1} \\ t_{m, m+1}^{m+1} & V_m^{m+1} \end{bmatrix}$$

The storage area now looks like this:

$$\begin{array}{cc} T^m & t_{1, m+1}^{m+1} & V_1^{m+1} \\ & 1, m+1 & 1 \\ & t_{m+1, m+1}^{m+1} & V_{m+1}^{m+1} \\ & & A_{22}^{m+1} \end{array}$$

Let T^{m+1} be the enlarged triangular t -array indicated above, (that is, add the column of t 's to T^m), and let V^{m+1} be the V -array. An easy calculation shows that we are back in the situation (3), (4) with m replaced by $m+1$. This completes step $m+1$.

c. Final result of elimination

The above process is continued until for some $m=r$, say, $D^r = 0$ (in the sense mentioned above) or until $m=n$ whichever comes first. In the case $r < n$, the result is the factorization:

$$A^r = P^r A (P^r)^T = \begin{bmatrix} (T^r)^T & 0 \\ (V^r)^T & I \end{bmatrix} \begin{bmatrix} I & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} T^r & V^r \\ 0 & I \end{bmatrix}$$

where P^r is the permutation matrix associated with the permutation:

$$P^r = (r, k_r)(r-1, k_{r-1}) \dots (1, k_1)$$

T^r is nonsingular, and we may compute $U^r = (T^r)^{-1}V^r$ in the same storage locations occupied by V^r . An easy calculation shows:

$$A^r = \begin{bmatrix} I & 0 \\ (U^r)^T & I \end{bmatrix} \begin{bmatrix} A_s & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} I & U^r \\ 0 & I \end{bmatrix}$$

where $A_s = (T^r)^T T^r$. We also compute $I + (U^r)^T U^r$ and store it in the last $n-r$ rows and columns of A , producing the storage scheme:

$$\begin{array}{cc} T^r & U^r \\ I + (U^r)^T U^r & \end{array}$$

We now operate on $I + (U^r)^T U^r$ in the same way that we operated on A . Whenever it is necessary to interchange two columns of this matrix, we also interchange the same columns of U^r in the storage area. Interchange information is recorded in TRAC ($r+1$) up to TRAC(n). The foregoing proof establishes a permutation matrix Q and an $(n-r)$ by $(n-r)$ nonsingular upper triangular T_u such that:

$$(T_u)^T T_u = Q(I + (U^r)^T U^r)Q^T = I + (U^r Q^T)^T (U^r Q^T)$$

Let $T = T^r$, $U = U^r Q^T$ and $P^{n-r} = \begin{bmatrix} I & 0 \\ 0 & Q \end{bmatrix}$. An easy calculation then gives the final results:

$$A^n = PAP^T = \begin{bmatrix} I & 0 \\ U^T & I \end{bmatrix} \begin{bmatrix} A_s & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} I & U \\ 0 & I \end{bmatrix} \quad (6)$$

$$(T_u)^T T_u = I + U^T U \quad (7)$$

where $P = P^{n-r} P^r$. The final storage scheme is

$$\begin{array}{cc} T & U \\ & T_u \end{array}$$

TRAC contains the permutation P^T in the form of a transposition vector (k_1, k_2, \dots, k_n) .

d. Dependencies among rows and columns

The basic rows of A^n are $A_b = A_s [I, U]$. The nonbasic rows are then $U^T A_b$. Of course basic columns are $(A_b)^T$, and nonbasic columns are $(A_b)^T U$.

e. Systems of equations

Subroutines MFSS and DMFSS may be used to solve systems of equations

$$AX = R$$

with positive semidefinite coefficient matrix A . Using the permutation P , this system is transformed into the system

$$A^n X^n = R^n \quad (8)$$

where $X^n = PX$ and $R^n = PR$. If A has rank $r=n$, equation (8) is

$$A_s X^n = R^n$$

which is easily solved since $A_s^{-1} = T^{-1}(T^{-1})^T$.

Assuming $r < n$, the vectors X^n , R^n are partitioned as follows:

$$X^n = \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} \text{ and } R^n = \begin{bmatrix} R_1 \\ R_2 \end{bmatrix},$$

where X_1 consists of the first r elements of X^n , etc. Using the decomposition (6), it is easy to see that (8) is equivalent to:

$$\begin{aligned} A_s(X_1 + UX_2) &= R_1 \\ 0X_2 &= -U^T R_1 + R_2 \end{aligned} \quad (9)$$

(By equivalent systems we mean they have the same solutions.)

If $R_2 = U^T R_1$ (a compatible system), equation (9) has the $n-r$ parameter family of solutions:

$$\begin{aligned} X_1 &= A_s^{-1} R_1 - UX_2 \\ X_2 &= \text{arbitrary} \end{aligned} \quad (10)$$

If $R_2 \neq U^T R_1$ (an incompatible system), it is natural to ask for a least-squares solution of (8), that is a vector X^n such that $\|A^n X^n - R^n\|^2 = \text{minimum}$. This problem leads to the system of equations:

$$(A^n)^2 X^n = A^n R^n \quad (11)$$

Given the factorization (6) of A^n , it is easy to show that $B^n = (A^n)^2$ admits the factorization:

$$B^n = \begin{bmatrix} I & 0 \\ U^T & I \end{bmatrix} \begin{bmatrix} B_s & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} I & U \\ 0 & I \end{bmatrix}$$

where $B_s = A_s(I + UU^T)A_s$. Using this fact, (11) is equivalent to:

$$\begin{aligned} B_s(X_1 + UX_2) &= A_s(R_1 + UR_2) \\ 0 \cdot X_2 &= 0 \cdot R_2 \end{aligned} \quad (12)$$

which is clearly a compatible system. Therefore (12) has the solutions:

$$X_1 = B_s^{-1} A_s (R_1 + UR_2) - UX_2 \quad (13)$$

$$X_2 = \text{arbitrary}$$

Now the identity $(I + UU^T)^{-1} = I - U(I + U^T U)^{-1} U^T$ shows that it suffices to know $(I + U^T U)^{-1}$ in order to compute B_s^{-1} . But by (7):

$$(I + U^T U)^{-1} = T_u^{-1} (T_u^{-1})^T$$

and T_u^{-1} is easy to compute, since T_u is upper triangular.

f. Solutions of minimal length

The solutions (10) or (13) contain $n-r$ free parameters X_2 , and it is possible to choose them so that X^n has minimal Euclidean length, that is so that $\|X^n\| = \min$. Some easy calculations show that in the compatible case (10), X^n is given by:

$$X_1 = (I + UU^T)^{-1} A_s^{-1} R_1$$

$$X_2 = U^T X_1$$

and in the incompatible case (13), X^n is:

$$X_1 = (I + UU^T)^{-1} A_s^{-1} (I + UU^T)^{-1} (R_1 + UR_2)$$

$$X_2 = U^T X_1$$

g. Accuracy

Determining the rank of a matrix on a computer is a difficult matter, and it is not claimed that MFSS will compute the correct rank in all cases. This is an intrinsic difficulty due to the fact that we work with finite arithmetic.

h. Error returns

Normally IRANK contains the computed rank r . A nonpositive value returned in IRANK means:

- IRANK = 0 A has no positive diagonal element, or $|\epsilon| \geq 1$.
- IRANK = -1 A nonpositive dimension of A was specified.
- IRANK = -2 $I + U^T U$ is ill-conditioned and/or the relative tolerance ϵ was specified incorrectly.

C		MFSS 19
C		MFSS 20
C		MFSS 30
C	SUBROUTINE MFSS	MFSS 40
C		MFSS 50
C	PURPOSE	MFSS 60
C	GIVEN A SYMMETRIC POSITIVE SEMI DEFINITE MATRIX, MFSS WILL	MFSS 70
C	(1) DETERMINE THE RANK AND LINEARLY INDEPENDENT ROWS AND	MFSS 80
C	COLUMNS	MFSS 90
C	(2) FACTOR A SYMMETRIC SUBMATRIX OF MAXIMAL RANK	MFSS 100
C	(3) EXPRESS NONBASIC COLUMNS IN TERMS OF BASIC ONES	MFSS 110
C	EXPRESS BASIC VARIABLES IN TERMS OF FREE ONES	MFSS 120
C	SUBROUTINE MFSS MAY BE USED AS A PREPARATORY STEP FOR THE	MFSS 130
C	CALCULATION OF THE LEAST SQUARES SOLUTION OF MINIMAL	MFSS 140
C	LENGTH OF A SYSTEM OF LINEAR EQUATIONS WITH SYMMETRIC	MFSS 150
C	POSITIVE SEMI-DEFINITE COEFFICIENT MATRIX	MFSS 160
C		MFSS 170
C		MFSS 180
C	USAGE	MFSS 190
C	CALL MFSS(A,N,EPS,IRANK,TRAC)	MFSS 200
C		MFSS 210
C	DESCRIPTION OF PARAMETERS	MFSS 220
C	A - UPPER TRIANGULAR PART OF GIVEN SYMMETRIC SEMI-	MFSS 230
C	DEFINITE MATRIX STORED COLUMNWISE IN COMPRESSED FORM	MFSS 240
C	ON RETURN A CONTAINS THE MATRIX T AND, IF IRANK IS	MFSS 250
C	LESS THAN N, THE MATRICES U AND TU	MFSS 260
C	N - DIMENSION OF GIVEN MATRIX A	MFSS 270
C	EPS - TESTVALUE FOR ZERO AFFECTED BY ROUND-OFF NOISE	MFSS 280
C	IRANK - RESULTANT VARIABLE, CONTAINING THE RANK OF GIVEN	MFSS 290
C	MATRIX A IF A IS SEMI-DEFINITE	MFSS 300
C	IRANK = 0 MEANS A HAS NO POSITIVE DIAGONAL ELEMENT	MFSS 310
C	AND/OR EPS IS NOT ABSOLUTELY LESS THAN ONE	MFSS 320
C	IRANK = -1 MEANS DIMENSION N IS NOT POSITIVE	MFSS 330
C	IRANK = -2 MEANS COMPLETE FAILURE, POSSIBLY DUE TO	MFSS 340
C	INADEQUATE RELATIVE TOLERANCE EPS	MFSS 350
C	TRAC - VECTOR OF DIMENSION N CONTAINING THE	MFSS 360
C	SOURCE INDEX OF THE I-TH PIVOT ROW IN ITS I-TH	MFSS 370
C	LOCATION, THIS MEANS THAT TRAC CONTAINS THE	MFSS 380
C	PRODUCT REPRESENTATION OF THE PERMUTATION WHICH	MFSS 390
C	IS APPLIED TO ROWS AND COLUMNS OF A IN TERMS OF	MFSS 400
C	TRANSPOSITIONS	MFSS 410
C		MFSS 420
C	REMARKS	MFSS 430
C	EPS MUST BE ABSOLUTELY LESS THAN ONE. A SENSIBLE VALUE IS	MFSS 440
C	SOMEWHERE IN BETWEEN 10**(-4) AND 10**(-9)	MFSS 450
C	THE ABSOLUTE VALUE OF INPUT PARAMETER EPS IS USED AS	MFSS 460
C	RELATIVE TOLERANCE.	MFSS 470
C	IN ORDER TO PRESERVE SYMMETRY ONLY PIVOTING ALONG THE	MFSS 480
C	DIAGONAL IS BUILT IN.	MFSS 490
C	ALL PIVOTELEMENTS MUST BE GREATER THAN THE ABSOLUTE VALUE	MFSS 500
C	OF EPS TIMES ORIGINAL DIAGONAL ELEMENT	MFSS 510
C	OTHERWISE THEY ARE TREATED AS IF THEY WERE ZERO	MFSS 520
C	MATRIX A REMAINS UNCHANGED IF THE RESULTANT VALUE IRANK	MFSS 530
C	EQUALS ZERO	MFSS 540
C		MFSS 550
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	MFSS 560
C	NONE	MFSS 570
C		MFSS 580
C		MFSS 590
C	METHOD	MFSS 600
C	THE SQUARE ROOT METHOD WITH DIAGONAL PIVOTING IS USED FOR	MFSS 610
C	CALCULATION OF THE RIGHT HAND TRIANGULAR FACTOR.	MFSS 620
C	IN CASE OF AN ONLY SEMI-DEFINITE MATRIX THE SUBROUTINE	MFSS 630
C	RETURNS THE IRANK X IRANK UPPER TRIANGULAR FACTOR T OF A	MFSS 640
C	SUBMATRIX OF MAXIMAL RANK, THE IRANK X (N-IRANK) MATRIX U	MFSS 650
C	AND THE (N-IRANK) X (N-IRANK) UPPER TRIANGULAR TU SUCH	MFSS 660
C	THAT TRANSPOSE(TU)*TU=I+TRANSPOSE(U)*U	MFSS 670
C		MFSS 680
C		MFSS 690
C	SUBROUTINE MFSS(A,N,EPS,IRANK,TRAC)	MFSS 700
C		MFSS 710
C		MFSS 720
C		MFSS 730
C	DIMENSIONED DUMMY VARIABLES	MFSS 740
C	DIMENSION A(1),TRAC(1)	MFSS 750
C	DOUBLE PRECISION SUM	MFSS 760
C		MFSS 770
C	TEST OF SPECIFIED DIMENSION	MFSS 780
C	IF(N136,36,1	

```

C
C      INITIALIZE TRIANGULAR FACTORIZATION
1  IRANK=0
  ISUB=0
  KPIV=0
  J=0
  PIV=0.
C
C      SEARCH FIRST PIVOT ELEMENT
DO 3 K=1,N
  J=J+K
  TRAC(K)=A(J)
  IF (A(J)-PIV) 3,3,2
2  PIV=A(J)
  KSUB=J
  KPIV=K
3  CONTINUE
C
C      START LOOP OVER ALL ROWS OF A
DO 32 I=1,N
  ISUB=ISUB+1
  IMI=I-1
4  KMI=KPIV-I
  IF (KMI) 5,9,5
C
C      PERFORM PARTIAL COLUMN INTERCHANGE
5  JI=KSUB-KMI
  IDC=JI-ISUB
  JJ=ISUB-IMI
  DO 6 K=J,ISUB
    KK=K+IDC
    HOLD=A(K)
    A(K)=A(KK)
    A(KK)=HOLD
6  A(KK)=HOLD
C
C      PERFORM PARTIAL ROW INTERCHANGE
7  KK=KSUB
  DO 7 K=KPIV,N
    II=KK-K+1
    HOLD=A(II)
    A(II)=A(KK)
    A(KK)=HOLD
7  KK=KK+K
C
C      PERFORM REMAINING INTERCHANGE
JJ=KPIV-1
II=ISUB
DO 8 K=1,JJ
  HOLD=A(II)
  A(II)=A(K)
  A(K)=HOLD
  II=II+K
8  JI=JI+1
9  IF (IRANK) 22,10,10
C
C      RECORD INTERCHANGE IN TRANSPOSITION VECTOR
10 TRAC(KPIV)=TRAC(II)
  TRAC(II)=KPIV
C
C      MODIFY CURRENT PIVOT ROW
KK=IMI-IRANK
KMI=ISUB-KK
PIV=0.
IDC=IRANK+1
JI=ISUB-I
JK=KMI
JJ=ISUB-I
DO 19 K=1,N
  SUM=0.,DO
C
C      BUILD UP SCALAR PRODUCT IF NECESSARY
IF (KK) 13,13,11
11 DO 12 J=KMI,JI
  SUM=SUM+A(J)*A(JK)
12 JK=JK+1
13 JJ=JJ+K
  IF (K-1) 14,14,16
14 SUM=A(ISUB)*SUM
C
C      TEST RADIAND FOR LOSS OF SIGNIFICANCE
IF (SUM) A55(A(SUB)*EPS) 20,20,15
15 A(ISUB)=DSORT(SUM)
  KPIV=I+1
  GO TO 19
16 SUM=(A(I,K)+SUM)/A(ISUB)
  A(I,K)=SUM
C
C      SEARCH FOR NEXT PIVOT ROW
IF (A(JJ)) 19,19,17
17 TRAC(K)=TRAC(I)-SUM*SUH
  HOLD=TRAC(K)/A(JJ)
  IF (PIV-HOLD) 18,19,19
18 PIV=HOLD
  KPIV=K
  KSUB=JJ
19 JK=J+IDC
  GO TO 32
C
C      CALCULATE MATRIX OF DEPENDENCIES U
20 IF (IRANK) 21,21,37
21 IRANK=-1
  GO TO 4
22 IRANK=IMI
  II=ISUB-IRANK
  JI=II
  DO 26 K=1,IRANK
    JI=JI-1
    JK=ISUB-I
    JJ=K-1
    DO 26 J=1,N
      IDC=IRANK
      SUM=0.,DO
      KMI=JI
      KK=JK
      IF (JJ) 25,25,23
23 DO 24 L=1,JI
  IDC=IDC-1
  SUM=SUM-(KMI)*A(KK)
  KMI=KMI-IDC
24 KK=KK-1
25 A(KK)=(SUM+A(KK))/A(KMI)
26 JK=JK+J
C
C      CALCULATE I+TRANSPOSE(U)+U
JJ=ISUB-1
PIV=0.
KK=ISUB-1
DO 31 K=1,N
  JJ=JJ+K
  IDC=0
  DO 28 J=K,N
    SUM=0.,DO
    KMI=JJ+IDC
    DO 27 L=1,KK
      JK=L+IDC
      SUM=SUM+A(L)*A(JK)
      A(KMI)=SUM
27 IDC=IDC+J
    A(JJ)=A(JJ)+1.,DO
    TRAC(K)=A(JJ)
C
C      SEARCH NEXT DIAGONAL ELEMENT
29 KPIV=K
  KSUB=JJ
  PIV=A(JJ)
30 II=II+K
  KK=KK+K
31 CONTINUE
  GO TO 4
32 CONTINUE
33 IF (IRANK) 35,34,35
34 IRANK=N
35 RETURN
C
C      ERROR RETURNS
C
C      RETURN IN CASE OF ILLEGAL DIMENSION
36 IRANK=-1
  RETURN
C
C      INSTABLE FACTORIZATION OF I+TRANSPOSE(U)+U
37 IRANK=-2
  RETURN
  END

```



```

KPIV=0
J=0
PIV=0.00
SEARCH FIRST PIVOT ELEMENT
DO 3 K=1,N
  J=K
  TRAC(K)=A(J)
  IF(A(J)-PIV)3,3,2
2 PIV=A(J)
  KSUB=J
  KPIV=K
3 CONTINUE
START LOOP OVER ALL ROWS OF A
DO 32 I=1,N
  ISUB=ISUB+1
  IMI=I-1
4 KMI=KPIV-I
  IF(KMI)35,4,5
PERFORM PARTIAL COLUMN INTERCHANGE
5 JI=KSUB-KMI
  IDC=JI-ISUB
  JJ=ISUB-IMI
  DO 6 K=JJ,ISUB
    KK=K+IDC
    HOLD=A(KI)
    A(KI)=A(KK)
    A(KK)=HOLD
6 AKK)=HOLD
PERFORM PARTIAL ROW INTERCHANGE
KK=KSUB
DO 7 K=KPIV,N
  II=KK-KMI
  HOLD=A(KK)
  A(KK)=A(II)
  A(II)=HOLD
7 KK=KK+K
PERFORM REMAINING INTERCHANGE
JJ=KPIV-1
II=ISUB
DO 8 K=1,II
  HOLD=A(II)
  A(II)=A(K)
  A(K)=HOLD
  II=II+K
8 JI=JI+1
9 IF(IRANK)22,10,10
RECORD INTERCHANGE IN TRANSPOSITION VECTOR
10 TRAC(KPIV)=TRAC(II)
  TRAC(II)=PIV
MODIFY CURRENT PIVOT ROW
KK=IMI-IRANK
KMI=ISUB-KK
PIV=0.00
IDC=IRANK+1
JI=ISUB-1
JK=KMI
JJ=ISUB-1
DO 15 K=1,N
  SUM=0.00
BUILD UP SCALAR PRODUCT IF NECESSARY
IF(KK)13,13,11
11 DO 12 J=KMI,JI
  SUM=SUM-A(J)*A(JK)
12 JK=JK+1
13 JJ=JJ+K
  IF(K-1)14,14,15
14 SUM=A(JISUB)+SUM
TEST RADIAND FOR LOSS OF SIGNIFICANCE
IF(SUM-DA)5(A(IISUB)*DBLE(EPS))120,22,15
15 A(IISUB)=DSQRT(SUM)
  KPIV=II
  GOTO 15
16 SUM=(A(JK)+SUM)/A(IISUB)
  A(JK)=SUM
SEARCH FOR NEXT PIVOT ROW
IF(A(IJJ))15,19,17
17 TRAC(KI)=TRAC(KI)+SUM*SUM
  HOLD=TRAC(KI)/A(IJJ)
  IF(PIV-HOLD)18,19,19
18 PIV=HOLD
  KPIV=K
  KSUB=JJ
19 JK=JJ+IDC
  GOTO 32
CALCULATE MATRIX OF DEPENDENCIES U
20 IF(IRANK)21,21,37
21 IRANK=-1
  GOTO 4
22 IRANK=IMI
  II=ISUB-IRANK
  JI=II
  DO 26 K=1,IRANK
    JI=JI-1
    JK=ISUB-1
    JJ=K-1
    DO 25 J=1,K
      IDC=IRANK
      SUM=0.00
      KMI=JI
      KK=JK
      IF(JJ)25,25,23
23 DO 24 L=1,II
      IDC=IDC-1
      SUM=SUM-A(KMI)*A(KK)
      KMI=KMI-IDC
24 KK=KK-1
25 A(KK)=(SUM+A(KK))/A(KMI)
26 JK=JK+J
CALCULATE I+TRANPOSE(U)*U
JJ=ISUB-1
PIV=0.00
KK=ISUB-1
DO 31 K=1,N
  JJ=JJ+K
  IDC=0
  DO 28 J=K,N
    SUM=0.00
    KMI=JJ+IDC

```

```

DMS5 850
DMS5 860
DMS5 870
DMS5 880
DMS5 890
DMS5 900
DMS5 910
DMS5 920
DMS5 930
DMS5 940
DMS5 950
DMS5 960
DMS5 970
DMS5 980
DMS5 990
DMS51000
DMS51010
DMS51020
DMS51030
DMS51040
DMS51050
DMS51060
DMS51070
DMS51080
DMS51090
DMS51100
DMS51110
DMS51120
DMS51130
DMS51140
DMS51150
DMS51160
DMS51170
DMS51180
DMS51190
DMS51200
DMS51210
DMS51220
DMS51230
DMS51240
DMS51250
DMS51260
DMS51270
DMS51280
DMS51290
DMS51300
DMS51310
DMS51320
DMS51330
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DMS51370
DMS51380
DMS51390
DMS51400
DMS51410
DMS51420
DMS51430
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DMS51450
DMS51460
DMS51470
DMS51480
DMS51490
DMS51500
DMS51510
DMS51520
DMS51530
DMS51540
DMS51550
DMS51560
DMS51570
DMS51580
DMS51590
DMS51600
DMS51610
DMS51620
DMS51630
DMS51640
DMS51650
DMS51660
DMS51670
DMS51680
DMS51690
DMS51700
DMS51710
DMS51720
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DMS51740
DMS51750
DMS51760
DMS51770
DMS51780
DMS51790
DMS51800
DMS51810
DMS51820
DMS51830
DMS51840
DMS51850
DMS51860
DMS51870
DMS51880
DMS51890
DMS51900
DMS51910
DMS51920
DMS51930
DMS51940
DMS51950
DMS51960
DMS51970
DMS51980
DMS51990
DMS52000
DMS52010
DMS52020
DMS52030
DMS52040
DMS52050
DMS52060
DMS52070
DMS52080
DMS52090
DMS52100
DMS52110
DMS52120
DMS52130

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```

DO 27 L=1,KK
  JK=L+IDC
  SUM=SUM+A(L)*A(JK)
  A(KM)=SUM
27 IDC=IDC+J
  A(IJJ)=A(IJJ)+1.00
  TRAC(KI)=A(IJJ)
SEARCH NEXT DIAGONAL ELEMENT
IF(PIV-A(IJJ))29,30,30
29 KPIV=K
  KSUB=JJ
  PIV=A(IJJ)
30 II=II+K
  KK=KK+K
31 CONTINUE
  GOTO 4
32 CONTINUE
33 IF(IRANK)35,34,35
24 IRANK=N
25 RETURN
ERROR RETURNS
RETURN IN CASE OF ILLEGAL DIMENSION
36 IRANK=-1
  RETURN
UNSTABLE FACTORIZATION OF I+TRANPOSE(U)*U
37 IRANK=-2
  RETURN
END

```

```

DMS52140
DMS52150
DMS52160
DMS52170
DMS52180
DMS52190
DMS52200
DMS52210
DMS52220
DMS52230
DMS52240
DMS52250
DMS52260
DMS52270
DMS52280
DMS52290
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DMS52370
DMS52380
DMS52390
DMS52400
DMS52410
DMS52420
DMS52430
DMS52440
DMS52450

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Subroutines MFSD and DMFSD

These subroutines will compute a triangular factorization of a symmetric positive definite matrix using the square root method of Cholesky.

1. Mathematical background

Given an n by n symmetric positive definite matrix A, we compute an upper triangular matrix R such that

A = R^T R

The elements r_jk of R are computed using the following recursive formulas:

r_lk = a_lk / r_ll, k=1, 2, 3, ..., n

r_jk = (1/r_jj)(a_jk - sum_{i=1}^{j-1} r_ij r_ik), j=2, 3, ..., n, k=j, j+1, ..., n

Note: The determinant of A is det(A) = (product_{i=1}^n r_ii)^2.

2. Programming considerations

The given matrix A is assumed stored columnwise in compressed form, that is upper triangular part only. MFSD stores the solution R in the same locations as A.

If any calculated radicand r_kk^2 (k=1, 2, ..., n) is not positive, further calculation is bypassed, and the error parameter IER is set to -1. This means that A is not positive definite, possibly due to roundoff errors. IER is also set to -1 if the input parameter n is less than 1.

Let all radicands be positive and let r_kk^2 be the first radicand which is no longer greater than the internal tolerance TOL = |EPS a_kk|. The subroutine then gives the warning IER = k-1; however, calculation is continued. The warning indicates that there may be loss of significance at factorization step k due to loss of significant digits in the calculation of r_kk^2.

C MFSD 10
C MFSD 20
C MFSD 30
SUBROUTINE MFSD MFSD 40
C MFSD 50
PURPOSE MFSD 60
FACTO A GIVEN SYMMETRIC POSITIVE DEFINITE MATRIX MFSD 70
C MFSD 80
USAGE MFSD 90
CALL MFSD(A,N,EPS,IER) MFSD 100
C MFSD 110
DESCRIPTION OF PARAMETERS MFSD 120
A - UPPER TRIANGULAR PART OF THE GIVEN SYMMETRIC MFSD 130
POSITIVE DEFINITE N BY N COEFFICIENT MATRIX. MFSD 140
ON RETURN A CONTAINS THE RESULTANT UPPER MFSD 150
TRIANGULAR MATRIX. MFSD 160
N - THE NUMBER OF ROWS (COLUMNS) IN GIVEN MATRIX. MFSD 170
EPS - AN INPUT CONSTANT WHICH IS USED AS RELATIVE MFSD 180
TOLERANCE FOR TEST ON LOSS OF SIGNIFICANCE. MFSD 190
IER - RESULTING ERROR PARAMETER CODED AS FOLLOWS MFSD 200
IEP=0 - NO ERROR MFSD 210
IER=-1 - NO RESULT BECAUSE OF WRONG INPUT PARAME- MFSD 220
TER N OR BECAUSE SOME RADICAND IS NON- MFSD 230
POSITIVE (MATRIX A IS NOT POSITIVE MFSD 240
DEFINITE, POSSIBLY DUE TO LOSS OF SIGNI- MFSD 250
FICANCE) MFSD 260
IER=K - WARNING WHICH INDICATES LOSS OF SIGNIFI- MFSD 270
CANCE. THE RADICAND FORMED AT FACTORIZA- MFSD 280
TION STEP K+1 WAS STILL POSITIVE BUT NO MFSD 290
LONGER GREATER THAN ABS(EPS*(K+1,K+1)). MFSD 300
C MFSD 310
REMARKS MFSD 320
THE UPPER TRIANGULAR PART OF GIVEN MATRIX IS ASSUMED TO BE MFSD 330
STORED COLUMNWISE IN N*(N+1)/2 SUCCESSIVE STORAGE LOCATIONS. MFSD 340
IN THE SAME STORAGE LOCATIONS THE RESULTING UPPER TRIANGU- MFSD 350
LAR MATRIX IS STORED COLUMNWISE TO. MFSD 360
THE PROCEDURE GIVES RESULTS IF N IS GREATER THAN 0 AND ALL MFSD 370
CALCULATED RADICANDS ARE POSITIVE. MFSD 380
THE PRODUCT OF RETURNED DIAGONAL TERMS IS EQUAL TO THE MFSD 390
SQUARE-ROOT OF THE DETERMINANT OF THE GIVEN MATRIX. MFSD 400
C MFSD 410
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED MFSD 420
NONE MFSD 430
C MFSD 440
METHOD MFSD 450
SOLUTION IS DONE USING THE SQUARE-ROOT METHOD OF CHOLESKY. MFSD 460
THE GIVEN MATRIX IS REPRESENTED AS PRODUCT OF TWO TRIANGULAR MFSD 470
MATRICES, WHERE THE LEFT HAND FACTOR IS THE TRANSPOSE OF MFSD 480
THE RETURNED RIGHT HAND FACTOR. MFSD 490
C MFSD 500
C MFSD 510
SUBROUTINE MFSD(A,N,EPS,IER) MFSD 520
C MFSD 530
DIMENSION A(1) MFSD 540
DOUBLE PRECISION DPIV,DSUM MFSD 550
C MFSD 560
TEST ON WRONG INPUT PARAMETER N MFSD 570
IF (N-1) 12,1,1 MFSD 580
1 IER=0 MFSD 590
C MFSD 600
INITIALIZE DIAGONAL-LOOP MFSD 610
KPIV=0 MFSD 620
DO 11 I=K,N MFSD 630
KPIV=KPIV+K MFSD 640
IND=KPIV MFSD 650
LEND=K-1 MFSD 660
C MFSD 670
CALCULATE TOLERANCE MFSD 680
TOL=ABS(EPS*(KPIV)) MFSD 690
C MFSD 700
START FACTORIZATION-LOOP OVER K-TH ROW MFSD 710
DO 11 I=K,N MFSD 720
DSUM=0.00 MFSD 730
IF (LEND) 2,4,2 MFSD 740
C MFSD 750
START INNER LOOP MFSD 760
2 DO 3 L=1,LEND MFSD 770
LANF=KPIV-L MFSD 780
LIND=IND-L MFSD 790
3 DSUM=DSUM+DBLE(A(LANF)*A(LIND)) MFSD 800
END OF INNER LOOP MFSD 810
C MFSD 820
TRANSFORM ELEMENT A(LIND) MFSD 830
4 DSUM=DBLE(A(LIND))-DSUM MFSD 840
IF (I-K) 10,5,10 MFSD 850
C MFSD 860
TEST FOR NEGATIVE PIVOT ELEMENT AND FOR LOSS OF SIGNIFICANCE MFSD 870
5 IF (SINGL(DSUM)-TOL) 6,6,9 MFSD 880
6 IF (DSUM) 12,12,7 MFSD 890
7 IF (IER) 8,8,9 MFSD 900
8 IER=K-1 MFSD 910
C MFSD 920
COMPUTE PIVOT ELEMENT MFSD 930
9 DPIV=DSORT(DSUM) MFSD 940
A(KPIV)=DPIV MFSD 950
CPIV=1.00/DPIV MFSD 960
GO TO 11 MFSD 970
C MFSD 980
CALCULATE TERMS IN ROW MFSD 990
10 A(LIND)=DSUM*DPIV MFSD 1000
11 IND=IND+1 MFSD 1010
C MFSD 1020
END OF DIAGONAL-LOOP MFSD 1030
RETURN MFSD 1040
12 IER=-1 MFSD 1050
RETURN MFSD 1060
END MFSD 1070

```

C
C ----- DMSD 10
C
C SUBROUTINE DMFSD DMSD 20
C DMSD 30
C DMSD 40
C DMSD 50
C PURPOSE DMSD 60
C FACTOR A GIVEN SYMMETRIC POSITIVE DEFINITE MATRIX A DMSD 70
C
C USAGE DMSD 80
C CALL DMFSD(A,N,EPS,IER) DMSD 90
C
C DESCRIPTION OF PARAMETERS DMSD 100
C A - DOUBLE PRECISION UPPER TRIANGULAR PART OF GIVEN DMSD 110
C SYMMETRIC POSITIVE DEFINITE N BY N COEFFICIENT DMSD 120
C MATRIX. DMSD 130
C ON RETURN A CONTAINS THE RESULTANT UPPER DMSD 140
C TRIANGULAR MATRIX IN DOUBLE PRECISION. DMSD 150
C N - THE NUMBER OF ROWS (COLUMNS) IN GIVEN MATRIX. DMSD 160
C EPS - SINGLE PRECISION INPUT CONSTANT WHICH IS USED DMSD 170
C AS RELATIVE TOLERANCE FOR TEST ON LOSS OF DMSD 180
C SIGNIFICANCE. DMSD 190
C IER - RESULTING ERROR PARAMETER CODED AS FOLLOWS DMSD 200
C IER=0 - NO ERROR DMSD 210
C IER=-1 - NO RESULT BECAUSE OF WRONG INPUT PARAMETER DMSD 220
C OR BECAUSE SOME RADICAND IS NON- DMSD 230
C POSITIVE (MATRIX A IS NOT POSITIVE DMSD 240
C DEFINITE, POSSIBLY DUE TO LOSS OF SIGNI- DMSD 250
C FICANCE). DMSD 260
C IER=K - WARNING WHICH INDICATES LOSS OF SIGNIFI- DMSD 270
C CANCE. THE RADICAND FORMED AT FACTORIZA- DMSD 280
C TION STEP K+1 WAS STILL POSITIVE BUT NO DMSD 290
C LONGER GREATER THAN ABS(EPS*A(K+1,K+1)). DMSD 300
C
C REMARKS DMSD 310
C THE UPPER TRIANGULAR PART OF GIVEN MATRIX IS ASSUMED TO BE DMSD 320
C STORED COLUMNWISE IN N*(N+1)/2 SUCCESSIVE STORAGE LOCATIONS. DMSD 330
C IN THE SAME STORAGE LOCATIONS THE RESULTING UPPER TRIANGU- DMSD 340
C LAR MATRIX IS STORED COLUMNWISE TOO. DMSD 350
C THE PROCEDURE GIVES RESULTS IF N IS GREATER THAN 0 AND ALL DMSD 360
C CALCULATED RADICANDS ARE POSITIVE. DMSD 370
C THE PRODUCT OF RETURNED DIAGONAL TERMS IS EQUAL TO THE DMSD 380
C SQUARE-ROOT OF THE DETERMINANT OF THE GIVEN MATRIX. DMSD 390
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DMSD 400
C ACMF DMSD 410
C
C METHOD DMSD 420
C SOLUTION IS DONE USING THE SQUARE-ROOT METHOD OF CHOLFSKY. DMSD 430
C THE GIVEN MATRIX IS REPRESENTED AS PRODUCT OF TWO TRIANGULAR DMSD 440
C MATRICES, WHERE THE LEFT HAND FACTOR IS THE TRANSPOSE OF DMSD 450
C THE RETURNED RIGHT HAND FACTOR. DMSD 460
C
C ----- DMSD 470
C
C SUBROUTINE DMFSD(A,N,EPS,IER) DMSD 480
C DMSD 490
C DMSD 500
C DMSD 510
C DMSD 520
C DMSD 530
C DMSD 540
C DMSD 550
C DMSD 560
C
C DIMENSION A(1) DMSD 570
C DOUBLE PRECISION DP,DPV,DSUM,A DMSD 580
C
C TEST ON WRONG INPUT PARAMETER N DMSD 590
C IF(N-1) 1?,1,1 DMSD 600
C 1 IER=0 DMSD 610
C
C INITIALIZE DIAGONAL-LOOP DMSD 620
C KPIV=0 DMSD 630
C DO 11 K=1,N DMSD 640
C KPIV=KPIV+K DMSD 650
C IND=KPIV DMSD 660
C LEND=K-1 DMSD 670
C
C CALCULATE TOLERANCE DMSD 700
C TOL=ABS(EPS*SNGL(A(K,PIV))) DMSD 710
C
C START FACTORIZATION-LOOP OVER K-TH ROW DMSD 720
C DO 11 I=K,N DMSD 730
C DSUM=0.0 DMSD 740
C IF(LEND) 2,4,2 DMSD 750
C
C START INNER LOOP DMSD 760
C DO 3 L=LEND DMSD 770
C LANF=KPIV-L DMSD 780
C LIND=IND-L DMSD 790
C 3 DSUM=DSUM+A(LANF)*A(LIND) DMSD 800
C END OF INNER LOOP DMSD 810
C
C TRANSFORM ELEMENT A(LIND) DMSD 820
C 4 DSUM=A(LIND)-DSUM DMSD 830
C IF(I-K) 10,5,10 DMSD 840
C
C TEST FOR NEGATIVE PIVOT ELEMENT AND FOR LOSS OF SIGNIFICANCE DMSD 850
C 5 IF(SNGL(DSUM)-TOL) 6,6,9 DMSD 860
C 6 IF(DSUM) 12,12,7 DMSD 870
C 7 IF(IEE) 8,8,9 DMSD 880
C 8 IER=K-1 DMSD 890
C
C COMPUTE PIVOT ELEMENT DMSD 900
C 9 DPV=DSORT(DSUM) DMSD 910
C A(KPIV)=DPV DMSD 920
C DPV=1.0/DPV DMSD 930
C GO TO 11 DMSD 940
C
C CALCULATE TERMS IN ROW DMSD 950
C 10 A(LIND)=DSUM*DPV DMSD 960
C 11 IND=IND+1 DMSD 970
C END OF DIAGONAL-LOOP DMSD 980
C
C RETURN DMSD 990
C 12 IER=-1 DMSD 1000
C RETURN DMSD 1010
C END DMSD 1020
C

```

Subroutines LLSQ and DLLSQ

These subroutines obtain the solution of linear least-squares problems. Consider a real m by n matrix A of rank n ($m \geq n$) with elements a_{ik} ($i = 1, 2, \dots, m$; $k = 1, 2, \dots, n$) and l right-hand side column vectors B_j ($j = 1, 2, \dots, l$) of dimension m , written as an m by l right-hand side matrix B with elements b_{jk} ($i = 1, 2, \dots, m$; $k = 1, 2, \dots, l$). The problem is to determine l column vectors X_j ($j = 1, 2, \dots, l$) of dimension n -- written as an n by l matrix X with elements x_{ik} ($i = 1, 2, \dots, n$; $k = 1, 2, \dots, l$) -- such that:

$$\|B_j - A * X_j\| = \min_j \quad (j = 1, 2, \dots, l) \quad (1)$$

where $\|R\|$ indicates the Euclidean norm of any column vector R with elements r_i ($i = 1, 2, \dots, m$); that is:

$$\|R\| = \sqrt{\sum_{i=1}^m r_i^2} \quad (2)$$

In the special case $m = n$, solution of the linear least-squares problem means solution of the system of simultaneous linear equations:

$$A * X = B \quad (3)$$

Solution of the given problem is based on the well known principle that transformation of any column vector R by an orthogonal matrix Q does not change its norm $\|R\|$; that is:

$$\|Q * R\| = \|R\| \quad (4)$$

Writing the given problem in the following form:

$$\begin{pmatrix} b_{11} & b_{12} & \dots & b_{1l} \\ b_{21} & b_{22} & \dots & b_{2l} \\ b_{31} & b_{32} & \dots & b_{3l} \\ \vdots & \vdots & & \vdots \\ b_{m1} & b_{m2} & \dots & b_{ml} \end{pmatrix} = \begin{pmatrix} a_{11} & a_{12} & \dots & a_{1n} \\ a_{21} & a_{22} & \dots & a_{2n} \\ a_{31} & a_{32} & \dots & a_{3n} \\ \vdots & \vdots & & \vdots \\ a_{m1} & a_{m2} & \dots & a_{mn} \end{pmatrix} \cdot$$

$$\begin{pmatrix} x_{11} & x_{12} & \dots & x_{1l} \\ x_{21} & x_{22} & \dots & x_{2l} \\ \vdots & \vdots & & \vdots \\ x_{n1} & x_{n2} & \dots & x_{nl} \end{pmatrix} = \begin{pmatrix} r_{11} & r_{12} & \dots & r_{1l} \\ r_{21} & r_{22} & \dots & r_{2l} \\ r_{31} & r_{32} & \dots & r_{3l} \\ \vdots & \vdots & & \vdots \\ r_{m1} & r_{m2} & \dots & r_{ml} \end{pmatrix} \quad (5)$$

the orthogonal transformation matrix Q is determined so that matrix A is transformed to upper triangular form; that is, all elements a_{ik} with $i > k$ are transformed to zero. An effective way to realize this decomposition is via Householder transformations. The algorithm is a recursive n -step procedure defined by the following recursion formulas:

$$A^{(1)} = A \quad (6)$$

$$A^{(k+1)} = P^{(k)} * A^{(k)} \quad (k = 1, 2, \dots, n) \quad (7)$$

In order to get an upper triangular matrix $A^{(n+1)}$, every matrix $P^{(k)}$ ($k = 1, 2, \dots, n$) should be defined so that it is symmetric and orthogonal, and so that it transforms all elements of the k^{th} column of $A^{(k)}$ below the main diagonal to zero. All these restrictions to $P^{(k)}$ are satisfied, setting:

$$P^{(k)} = I - \beta_k * U^{(k)} * U^{(k)T} \quad (8)$$

with

$$\beta_k = \frac{1}{\sigma_k (\sigma_k + a_{kk}^{(k)})} \quad (9)$$

and

$$\sigma_k = \pm \sqrt{\sum_{i=k}^m (a_{ik}^{(k)})^2} \quad \text{with} \quad \left\{ \begin{array}{l} + \text{ for } a_{kk}^{(k)} \geq 0 \\ - \text{ for } a_{kk}^{(k)} < 0 \end{array} \right. \quad (10)$$

where I is the identity matrix.

$U^{(k)T}$ denotes the transpose of column vector $U^{(k)}$, the m components of which are defined as follows:

$$u_i^{(k)} = 0 \text{ for } i < k \quad (11)$$

$$u_k^{(k)} = \sigma_k + a_{kk}^{(k)} \quad (12)$$

$$u_i^{(k)} = a_{ik}^{(k)} \text{ for } i > k \quad (13)$$

Neither matrices $P^{(k)}$ ($k = 1, 2, \dots, n$) nor matrix $Q = P^{(n)} * P^{(n-1)} * \dots * P^{(1)}$ are computed explicitly, since from (7) and (8):

$$A^{(k+1)} = A^{(k)} - U^{(k)} * Y^{(k)T} \quad (14)$$

with

$$Y^{(k)T} = \beta_k * U^{(k)T} * A^{(k)} \quad (15)$$

Writing the components of row vector $Y^{(k)T}$ explicitly:

$$y_j^{(k)} = 0 \text{ for } j < k \quad (16)$$

$$y_k^{(k)} = 1 \quad (17)$$

$$y_j^{(k)} = \beta_k \sum_{i=k}^m u_i^{(k)} \cdot a_{ij}^{(k)} \text{ for } j > k \quad (18)$$

Using (14), (16), (17), and (18), the explicit transformation formulas for matrix $A^{(k)}$ appear as follows:

$$a_{kk}^{(k+1)} = -\sigma_k \quad (19)$$

$$a_{ik}^{(k+1)} = 0 \quad (i = k+1, k+2, \dots, m) \quad (20)$$

$$a_{ij}^{(k+1)} = a_{ij}^{(k)} - u_i^{(k)} \cdot y_j^{(k)} \quad (j = k+1, k+2, \dots, n \text{ and for fixed } j, i = k, k+1, \dots, m) \quad (21)$$

All other elements of matrix $A^{(k)}$ do not change.

Naturally, the same transformation is performed on matrix B .

Using (6) and (7):

$$B^{(1)} = B \quad (22)$$

$$B^{(k+1)} = P^{(k)} * B^{(k)} \quad (k = 1, 2, \dots, n) \quad (23)$$

Using (8) and (23):

$$B^{(k+1)} = B^{(k)} - U^{(k)} * Z^{(k)T} \quad (24)$$

with

$$Z^{(k)T} = \beta_k * U^{(k)T} * B^{(k)} \quad (25)$$

or explicitly:

$$b_{ij}^{(k+1)} = b_{ij}^{(k)} - u_i^{(k)} \cdot z_j^{(k)} \quad (j = 1, 2, \dots, l; i = 1, 2, \dots, m) \quad (26)$$

with

$$z_j^{(k)} = \beta_k \sum_{i=k}^m u_i^{(k)} \cdot b_{ij}^{(k)} \quad (j = 1, 2, \dots, l) \quad (27)$$

In order to keep roundoff errors as small as possible, column interchange is performed in such a way that, at the k^{th} stage, the column of $A^{(k)}$ is chosen to be reduced next, which will maximize $|a_{kk}^{(k+1)}|$. Using (19) and (10), the index of this column is determined by giving the maximum overall j of:

$$s_j^{(k)} = \sum_{i=k}^m (a_{ij}^{(k)})^2 \quad (j = k, k+1, \dots, n) \quad (28)$$

After $A^{(k+1)}$ has been computed, it is possible to compute $s_j^{(k+1)}$ as follows:

$$s_j^{(k+1)} = s_j^{(k)} - (a_{kj}^{(k+1)})^2 \quad (j = k+1, k+2, \dots, n) \quad (29)$$

since the orthogonal transformations leave the column lengths invariant.

After having computed matrices $A^{(n+1)}$ (upper triangular matrix) and $B^{(n+1)}$, the computation of the n by l solution matrix X is performed by back substitution according to the following formulas:

$$x_{ni} = \frac{1}{a_{nn}^{(n+1)}} \cdot b_{ni}^{(n+1)} \quad (i = 1, 2, \dots, l) \quad (30)$$

$$x_{ki} = \frac{1}{a_{kk}^{(n+1)}} (b_{ki}^{(n+1)} - a_{k,k+1}^{(n+1)} \cdot x_{k+1,i} - a_{k,k+2}^{(n+1)} \cdot x_{k+2,i} - \dots - a_{k,n-1}^{(n+1)} \cdot x_{n-1,i} - a_{kn}^{(n+1)} \cdot x_{ni})$$

$$(k = n-j+1; j = 2, 3, \dots, n \text{ and } i = 1, 2, \dots, l \text{ for fixed } j) \quad (31)$$

After any row of matrix X has been computed, back interchange of rows is performed according to column interchanges in matrices $A^{(k)}$ in order to get the correct sequence of components in the solution vectors X_j .

Finally, the vector of linear least squares with components

$$lsq_j = \sum_{i=n+1}^m (b_{ij}^{(n+1)})^2 \quad (j = 1, 2, \dots, l) \quad (32)$$

is computed, which gives the squares of the minimized Euclidean norms $\|B_j - A * X_j\|$ for all right-hand side column vectors B_j ($j = 1, 2, \dots, l$).

The only case in which the whole procedure can fail occurs when, at any stage k , no column with nonzero parameter σ_k can be found; that is, no nonzero main diagonal element can be generated. In this case, the rank of matrix A is less than n . With respect to roundoff errors, the test is made in the following way.

At first, all elements $s_j^{(1)}$ are computed according to (28) and the maximum overall j (that is, σ_1^2) is determined. With the relative tolerance ϵ given by input, the following absolute tolerance is generated:

$$tol = \sigma_1 \cdot \epsilon \quad (33)$$

If at any stage k ($= 1, 2, \dots, n+1$) the square root of the maximum overall $j = k+1, \dots, n$ of $s_j^{(k+1)}$, say piv , is not greater than tol , the rank of matrix A is declared to be $k < n$, and the procedure returns an error message to the calling program, thus indicating that no solution could be found. In this case, the last $n - k$ elements of vector $IPIV$ denote the useless columns of matrix A ; the remaining useful columns form a base of matrix A .

For reference see G. Golub, "Numerical Method for Solving Linear Least Squares Problems", Numerische Mathematik, vol. 7, no. 3 (1965), pp. 206 - 216.

```

C ..... LLSQ 10
C ..... LLSQ 20
C ..... LLSQ 30
C ..... LLSQ 40
C ..... LLSQ 50
C ..... LLSQ 60
C ..... LLSQ 70
C ..... LLSQ 80
C ..... LLSQ 90
C ..... LLSQ 100
C ..... LLSQ 110
C ..... LLSQ 120
C ..... LLSQ 130
C ..... LLSQ 140
C ..... LLSQ 150
C ..... LLSQ 160
C ..... LLSQ 170
C ..... LLSQ 180
C ..... LLSQ 190
C ..... LLSQ 200
C ..... LLSQ 210
C ..... LLSQ 220
C ..... LLSQ 230
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C ..... LLSQ 250
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C ..... LLSQ 280
C ..... LLSQ 290
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C ..... LLSQ 440
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C ..... LLSQ 630
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C ..... LLSQ 650
C ..... LLSQ 660
C ..... LLSQ 670
C ..... LLSQ 680
C ..... LLSQ 690
C ..... LLSQ 700
C ..... LLSQ 710
C ..... LLSQ 720
C ..... LLSQ 730
C ..... LLSQ 740
C ..... LLSQ 750
C ..... LLSQ 760
C ..... LLSQ 770
C ..... LLSQ 780
C ..... LLSQ 790
C ..... LLSQ 800
C ..... LLSQ 810
C ..... LLSQ 820
C ..... LLSQ 830
C ..... LLSQ 840
C ..... LLSQ 850
C ..... LLSQ 860
C ..... LLSQ 870
C ..... LLSQ 880
C ..... LLSQ 890
C ..... LLSQ 900
C ..... LLSQ 910
C ..... LLSQ 920
C ..... LLSQ 930
C ..... LLSQ 940
C ..... LLSQ 950
C ..... LLSQ 960

```

```

LEND=IST+M-K
LKPJV=K
IF(I)S,8+6
C
C INTERCHANGE K-TH COLUMN OF A WITH KPIV-TH IN CASE KPIV.GT.K
6 M=AUX(K)
  AUX(K)=AUX(KPIV)
  AUX(KPIV)=M
  IO=I+M
  DO 7 I=IST,IEND
    J=I+IO
    H=A(I)
    A(I)=A(J)
    A(J)=H
  7 A(J)=M
C
C COMPUTATION OF PARAMETER SIG
8 IF(K-1)11,11+9
9 SIG=C
  DO 10 I=IST,IEND
    SIG=SIG+(A(I)*A(I))
  10 SIG=SIG*(I+SIG)
C
C TEST ON SINGULARITY
IF(SIG-TOL)32,32+11
C
C GENERATE CORRECT SIGN OF PARAMETER SIG
11 H=A(IST)
  IF(M)2,13,13
12 SIG=-SIG
C
C SAVE INTERCHANGE INFORMATION
13 IPIV(KPIV)=IPIV(K)
  IPIV(K)=KPIV
C
C GENERATION OF VECTOR UK IN K-TH COLUMN OF MATRIX A AND OF
PARAMETER DELTA
  IPIV(K)=KPIV
  IPIV(K)=KPIV
  DELTA=SIG
  A(IST)=DELTA
  BETA=L/(SIG*DELTA)
  J=N+K
  AUX(J)=SIG
  IF(K-N)14,14+14
C
C TRANSFORMATION OF MATRIX A
14 PIV=J
  IO=0
  JST=K+1
  KPIV=JST
  DO 15 I=JST,N
    IO=IO+M
    H=C
    DO 15 I=IST,IEND
      II=I+IO
      H=A(II)*A(II)
      H=HETA*M
      DO 16 I=IST,IEND
        II=I+IO
        A(II)=A(II)-A(II)*H
C
C UPDATING OF ELEMENT (K,J) STORED IN LOCATION AUX(J)
  II=IST+IO
  H=AUX(J)-A(II)*A(II)
  AUX(J)=H
  IF(H-PIV)18,18+17
17 PIV=H
  KPIV=J
18 CONTINUE
C
C TRANSFORMATION OF RIGHT HAND SIDE MATRIX B
19 DO 21 JK=L,N
  H=C
  IEND=J+M-K
  II=IST
  DO 20 I=J,IEND
    H=A(II)*B(I)
  20 H=H+I*M
  II=IST
  DO 21 I=J,IEND
    B(I)=B(I)-A(II)*H
21 II=I+1
END OF DECOMPOSITION LOOP
C
C BACK SUBSTITUTION AND BACK INTERCHANGE
IER=0
I=N
LN=L*N
PIV=L/AUX(L*N)
DO 22 A=N,L,N
  X(K)=PIV*A(II)
22 I=I+M
  IF(N-1)23,23+23
23 JST=(N-1)*M+N
  DO 25 J=2,N
    JST=JST-M+1
    K=N+M+1-J
    PIV=L/AUX(K)
    KST=K-N
    IO=PIV*(KST)-KST
    IST=2+J
    DO 25 K=1,L
      H=B(KST)
      IST=IST+N
      IEND=IST+J-2
      II=JST
      DO 24 I=IST,IEND
        II=I+M
        H=A(II)*X(II)
        I=IST+1
        II=I+IO
        X(II)=X(II)
        X(II)=PIV*H
24 KST=KST+M
C
C COMPUTATION OF LEAST SQUARES
26 IST=N+1
  IEND=C
  DO 29 J=L,N
    IEND=IEND+M
    H=C
    IF(M-N)29,29+27
  27 DO 28 I=IST,IEND
  28 H=A(II)*X(II)
  28 H=A(II)*X(II)
  28 I=IST+M
  29 AUX(J)=H
  RETURN

```

```

LSSQ 970
LSSQ 980
LSSQ 990
LSSQ1000
LSSQ1010
LSSQ1020
LSSQ1030
LSSQ1040
LSSQ1050
LSSQ1060
LSSQ1070
LSSQ1080
LSSQ1090
LSSQ1100
LSSQ1110
LSSQ1120
LSSQ1130
LSSQ1140
LSSQ1150
LSSQ1160
LSSQ1170
LSSQ1180
LSSQ1190
LSSQ1200
LSSQ1210
LSSQ1220
LSSQ1230
LSSQ1240
LSSQ1250
LSSQ1260
LSSQ1270
LSSQ1280
LSSQ1290
LSSQ1300
LSSQ1310
LSSQ1320
LSSQ1330
LSSQ1340
LSSQ1350
LSSQ1360
LSSQ1370
LSSQ1380
LSSQ1390
LSSQ1400
LSSQ1410
LSSQ1420
LSSQ1430
LSSQ1440
LSSQ1450
LSSQ1460
LSSQ1470
LSSQ1480
LSSQ1490
LSSQ1500
LSSQ1510
LSSQ1520
LSSQ1530
LSSQ1540
LSSQ1550
LSSQ1560
LSSQ1570
LSSQ1580
LSSQ1590
LSSQ1600
LSSQ1610
LSSQ1620
LSSQ1630
LSSQ1640
LSSQ1650
LSSQ1660
LSSQ1670
LSSQ1680
LSSQ1690
LSSQ1700
LSSQ1710
LSSQ1720
LSSQ1730
LSSQ1740
LSSQ1750
LSSQ1760
LSSQ1770
LSSQ1780
LSSQ1790
LSSQ1800
LSSQ1810
LSSQ1820
LSSQ1830
LSSQ1840
LSSQ1850
LSSQ1860
LSSQ1870
LSSQ1880
LSSQ1890
LSSQ1900
LSSQ1910
LSSQ1920
LSSQ1930
LSSQ1940
LSSQ1950
LSSQ1960
LSSQ1970
LSSQ1980
LSSQ1990
LSSQ2000
LSSQ2010
LSSQ2020
LSSQ2030
LSSQ2040
LSSQ2050
LSSQ2060
LSSQ2070
LSSQ2080
LSSQ2090
LSSQ2100
LSSQ2110
LSSQ2120
LSSQ2130
LSSQ2140
LSSQ2150
LSSQ2160
LSSQ2170
LSSQ2180
LSSQ2190
LSSQ2200
LSSQ2210
LSSQ2220
LSSQ2230
LSSQ2240
LSSQ2250

```

```

C ERROR RETURN IN CASE M LESS THAN N
30 IER=-2
  RETURN
C
C ERROR RETURN IN CASE OF ZERO-MATRIX A
31 IER=-1
  RETURN
C
C ERROR RETURN IN CASE OF RANK OF MATRIX A LESS THAN N
32 IER=K-1
  RETURN
  END
LSSQ2260
LSSQ2270
LSSQ2280
LSSQ2290
LSSQ2300
LSSQ2310
LSSQ2320
LSSQ2330
LSSQ2340
LSSQ2350
LSSQ2360
LSSQ2370
C
C .....
DLLS 10
C .....
DLLS 20
C .....
DLLS 30
C .....
DLLS 40
C .....
DLLS 50
C .....
DLLS 60
C .....
DLLS 70
C .....
DLLS 80
C .....
DLLS 90
C .....
DLLS 100
C .....
DLLS 110
C .....
DLLS 120
C .....
DLLS 130
C .....
DLLS 140
C .....
DLLS 150
C .....
DLLS 160
C .....
DLLS 170
C .....
DLLS 180
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DLLS 190
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DLLS 670
C .....
DLLS 680
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DLLS 690
C .....
DLLS 700
C .....
DLLS 710
C .....
DLLS 720
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DLLS 730
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DLLS 740
C .....
DLLS 750
C .....
DLLS 760
C .....
DLLS 770
C .....
DLLS 780
C .....
DLLS 790
C .....
DLLS 800
C .....
DLLS 810
C .....
DLLS 820
C .....
DLLS 830
C .....
DLLS 840
C .....
DLLS 850
C .....
DLLS 860
C .....
DLLS 870
C .....
DLLS 880
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DLLS 890
C .....
DLLS 900
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DLLS 950
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DLLS 980
C .....
DLLS 990
C .....
DLLS 1000
C .....
DLLS 1010
C .....
DLLS 1020
C .....
DLLS 1030
C .....
DLLS 1040
C .....
DLLS 1050
C .....
DLLS 1060
C .....
DLLS 1070
C .....
DLLS 1080
C .....
DLLS 1090
C .....
DLLS 1100

```

```

      J=I+10
      H=A(I)
      A(I)=A(J)
      A(J)=H
C
C   COMPUTATION OF PARAMETER SIG
      8 IF(K-1)11,11,9
      9 SIG=0.00
      10 I=1,IST,1END
      SIG=SIG+A(I)*A(I)
      SIG=DSQRT(SIG)
C
C   TEST ON SINGULARITY
      IF(SIG-TOL)2,2,11
C
C   GENERATE CORRECT SIGN OF PARAMETER SIG
      11 H=A(IST)
      IF(H)12,13,13
      12 SIG=-SIG
C
C   SAVE INTERCHANGE INFORMATION
      13 IPIV(K)=IPIV(A)
      IPIV(K)=KPIV
C
C   GENERATION OF VECTOR UK IN K-TH COLUMN OF MATRIX A AND OF
C   PARAMETER BETA
      BETA=H*SIG
      A(IST)=BETA
      BETA=1.00/(SIG*BETA)
      J=N+K
      AUX(J)=-SIG
      IF(K=N)14,19,19
C
C   TRANSFORMATION OF MATRIX A
      14 PIV=0.00
      15 I=1
      JST=K+1
      KPIV=JST
      16 I=1, J=JST, N
      IU=I+M
      H=0.00
      17 I=1, I=IST, IEND
      II=I+10
      18 H=A(I)*A(II)
      H=BETA*H
      19 I=1, I=IST, IEND
      II=I+10
      20 A(II)=A(II)-A(I)*H
C
C   UPDATING OF ELEMENT S(I,J) STORED IN LOCATION AUX(J)
      II=IST+10
      H=AUX(J)-A(II)*A(II)
      AUX(J)=H
      IF(H-PIV)18,19,17
      17 PIV=H
      KPIV=J
C
C   TRANSFORMATION OF RIGHT HAND SIDE MATRIX B
      19 DO 21 J=K,L,N,M
      H=0.00
      IEND=J+M-K
      I=IST
      20 DO 22 I=J, IEND
      H=A(I)*A(II)*B(II)
      21 II=I+1
      H=BETA*H
      I=IST
      22 I=J, I=END
      B(I)=B(I)-A(II)*H
      23 II=I+1
      ENDOF DECOMPOSITION LOOP
C
C   BACK SUBSTITUTION AND BACK INTERCHANGE
      IER=0
      IS=N
      LN=L*N
      PIV=1.00/AUX(2*N)
      24 DO 25 K=N, L+1
      X(K)=PIV*B(I)
      25 I=I+M
      IF(N-1)25,25,23
      26 JST=(N-1)*M+N
      27 DO 28 J=2,N
      JST=JST-M-1
      K=N+M+1-J
      PIV=1.00/AUX(K)
      KST=K-N
      28 I=PIV(KST)-KST
      I=I+M
      29 DO 29 K=I, L
      H=B(KST)
      I=IST+M
      IEND=IST+J-2
      X(I)=JST
      30 DO 30 I=IST, IEND
      II=I+M
      31 H=A(I)*A(II)
      I=IST-1
      II=I+10
      X(II)=X(II)
      X(I)=PIV*H
      32 KST=KST+M
C
C   COMPUTATION OF LEAST SQUARES
      26 IST=N+1
      IEND=C
      27 DO 29 J=1, L
      IEND=IEND+M
      H=0.00
      IF(M=N)29,29,27
      28 DO 28 I=IST, IEND
      H=A(I)*A(II)
      29 IST=IST+M
      30 AUX(I)=H
      RETURN
C
C   ERROR RETURN IN CASE M LESS THAN N
      30 IER=-2
      RETURN
C
C   ERROR RETURN IN CASE OF ZERO-MATRIX A
      31 IER=-1
      RETURN
C
C   ERROR RETURN IN CASE OF RANK OF MATRIX A LESS THAN N
      32 IER=-1
      RETURN
      END

```

Matrices: Eigenanalysis and Related Topics

Subroutine EIGEN

This subroutine computes the eigenvalues and eigenvectors of a real symmetric matrix.

Given a symmetric matrix A of order N, eigenvalues are to be developed in the diagonal elements of the matrix. A matrix of eigenvectors R is also to be generated.

An identity matrix is used as a first approximation of R.

The initial off-diagonal norm is computed:

$$\nu_I = \left\{ \sum_{i < k} 2A_{ik}^2 \right\}^{1/2} \quad (1)$$

ν_I = initial norm

A = input matrix (symmetric)

This norm is divided by N at each stage to produce the threshold.

The final norm is computed:

$$\nu_F = \frac{\nu_I \times 10^{-6}}{N} \quad (2)$$

This final norm is set sufficiently small that the requirement that any off-diagonal element A_{lm} shall be smaller than ν_F in absolute magnitude defines the convergence of the process.

An indicator is initialized. This indicator is later used to determine whether any off-diagonal elements have been found that are greater than the present threshold.

Each off-diagonal element is selected in turn and a transformation is performed to annihilate the off-diagonal (pivotal) element, as shown by the following equations:

$$\lambda = -A_{lm} \quad (3)$$

$$\mu = 1/2 (A_{11} - A_{mm}) \quad (4)$$

$$\omega = \text{sign}(\mu) \frac{\lambda}{\sqrt{\lambda^2 + \mu^2}} \quad (5)$$

$$\sin \theta = \frac{\omega}{\sqrt{2(1 + \sqrt{1 - \omega^2})}} \quad (6)$$

$$\cos \theta = \sqrt{1 - \sin^2 \theta} \quad (7)$$

$$B = A_{il} \cos \theta - A_{im} \sin \theta \quad (8)$$

$$A_{im} = A_{il} \sin \theta + A_{im} \cos \theta \quad (9)$$

$$A_{il} = B \quad (10)$$

$$B = R_{il} \cos \theta - R_{im} \sin \theta \quad (11)$$

$$R_{im} = R_{il} \sin \theta + R_{im} \cos \theta \quad (12)$$

$$R_{il} = B \quad (13)$$

$$A_{ll} = A_{ll} \cos^2 \theta + A_{mm} \sin^2 \theta - 2A_{lm} \sin \theta \cos \theta \quad (14)$$

$$A_{mm} = A_{ll} \sin^2 \theta + A_{mm} \cos^2 \theta + 2A_{lm} \sin \theta \cos \theta \quad (15)$$

$$A_{lm} = (A_{ll} - A_{mm}) \sin \theta \cos \theta + A_{lm} (\cos^2 \theta - \sin^2 \theta) \quad (16)$$

The above calculations are repeated until all of the pivotal elements are less than the threshold.

```

C ..... EIGE 10
C ..... EIGE 20
C ..... EIGE 30
C ..... EIGE 40
C ..... EIGE 50
C ..... EIGE 60
C ..... EIGE 70
C ..... EIGE 80
C ..... EIGE 90
C ..... EIGE 100
C ..... EIGE 110
C ..... EIGE 120
C ..... EIGE 130
C ..... EIGE 140
C ..... EIGE 150
C ..... EIGE 160
C ..... EIGE 170
C ..... EIGE 180
C ..... EIGE 190
C ..... EIGE 200
C ..... EIGE 210
C ..... EIGE 220
C ..... EIGE 230
C ..... EIGE 240
C ..... EIGE 250
C ..... EIGE 260
C ..... EIGE 270
C ..... EIGE 280
C ..... EIGE 290
C ..... EIGE 300
C ..... EIGE 310
C ..... EIGE 320
C ..... EIGE 330
C ..... EIGE 340
C ..... EIGE 350
C ..... EIGE 360
C ..... EIGE 370
C ..... EIGE 380
C ..... EIGE 390
C ..... EIGE 400
C ..... EIGE 410
C ..... EIGE 420
C ..... EIGE 430
C ..... EIGE 440
C ..... EIGE 450
C ..... EIGE 460
C ..... EIGE 470
C ..... EIGE 480
C ..... EIGE 490
C ..... EIGE 500
C ..... EIGE 510
C ..... EIGE 520
C ..... EIGE 530
C ..... EIGE 540
C ..... EIGE 550
C ..... EIGE 560
C ..... EIGE 570
C ..... EIGE 580
C ..... EIGE 590
C ..... EIGE 600
C ..... EIGE 610
C ..... EIGE 620
C ..... EIGE 630
C ..... EIGE 640
C ..... EIGE 650
C ..... EIGE 660
C ..... EIGE 670
C ..... EIGE 680
C ..... EIGE 690

```

```

DD 20 J=1,N EIGE 700
IQ=IQ+N EIGE 710
DD 20 I=1,N EIGE 720
IJ=IQ+1 EIGE 730
R(IJ)=0.0 EIGE 740
IF(I-J) 20,15,20 EIGE 750
15 R(IJ)=1.0 EIGE 760
20 CONTINUE EIGE 770
C ..... EIGE 780
C ..... EIGE 790
C ..... EIGE 800
C ..... EIGE 810
C ..... EIGE 820
C ..... EIGE 830
C ..... EIGE 840
C ..... EIGE 850
C ..... EIGE 860
C ..... EIGE 870
C ..... EIGE 880
C ..... EIGE 890
C ..... EIGE 900
C ..... EIGE 910
C ..... EIGE 920
C ..... EIGE 930
C ..... EIGE 940
C ..... EIGE 950
C ..... EIGE 960
C ..... EIGE 970
C ..... EIGE 980
C ..... EIGE 990
C ..... EIGE1000
C ..... EIGE1010
C ..... EIGE1020
C ..... EIGE1030
C ..... EIGE1040
C ..... EIGE1050
C ..... EIGE1060
C ..... EIGE1070
C ..... EIGE1080
C ..... EIGE1090
C ..... EIGE1100
C ..... EIGE1110
C ..... EIGE1120
C ..... EIGE1130
C ..... EIGE1140
C ..... EIGE1150
C ..... EIGE1160
C ..... EIGE1170
C ..... EIGE1180
C ..... EIGE1190
C ..... EIGE1200
C ..... EIGE1210
C ..... EIGE1220
C ..... EIGE1230
C ..... EIGE1240
C ..... EIGE1250
C ..... EIGE1260
C ..... EIGE1270
C ..... EIGE1280
C ..... EIGE1290
C ..... EIGE1300
C ..... EIGE1310
C ..... EIGE1320
C ..... EIGE1330
C ..... EIGE1340
C ..... EIGE1350
C ..... EIGE1360
C ..... EIGE1370
C ..... EIGE1380
C ..... EIGE1390
C ..... EIGE1400
C ..... EIGE1410
C ..... EIGE1420
C ..... EIGE1430
C ..... EIGE1440
C ..... EIGE1450
C ..... EIGE1460
C ..... EIGE1470
C ..... EIGE1480
C ..... EIGE1490
C ..... EIGE1500
C ..... EIGE1510
C ..... EIGE1520
C ..... EIGE1530
C ..... EIGE1540
C ..... EIGE1550
C ..... EIGE1560
C ..... EIGE1570
C ..... EIGE1580
C ..... EIGE1590
C ..... EIGE1600
C ..... EIGE1610
C ..... EIGE1620
C ..... EIGE1630
C ..... EIGE1640
C ..... EIGE1650
C ..... EIGE1660
C ..... EIGE1670
C ..... EIGE1680
C ..... EIGE1690
C ..... EIGE1700
C ..... EIGE1710
C ..... EIGE1720
C ..... EIGE1730
C ..... EIGE1740
C ..... EIGE1750
C ..... EIGE1760
C ..... EIGE1770
C ..... EIGE1780
C ..... EIGE1790
C ..... EIGE1800
C ..... EIGE1810
C ..... EIGE1820
C ..... EIGE1830
C ..... EIGE1840
C ..... EIGE1850
C ..... EIGE1860
C ..... EIGE1870
C ..... EIGE1880
C ..... EIGE1890
C ..... EIGE1900
C ..... EIGE1910
C ..... EIGE1920
C ..... EIGE1930
C ..... EIGE1940
C ..... EIGE1950

```

Subroutine NROOT

This subroutine calculates the eigenvalues, λ_i , and the matrix of eigenvectors, V , of a real square non-symmetric matrix of the special form $B^{-1}A$, where both B and A are real symmetric matrices and B is positive-definite. This subroutine is normally called by the subroutine CANOR in performing a canonical correlation analysis. The computational steps are as follows.

A symmetric matrix (storage mode 1) is formed by using the upper triangle elements of the square matrix B . Then the eigenvalues, h_i , and the matrix of eigenvectors, H , of the symmetric matrix are calculated by the subroutine EIGEN.

The reciprocal of square root of each eigenvalue is formed as follows:

$$\mu_i = \frac{1}{\sqrt{h_i}} \quad (1)$$

where $i = 1, 2, \dots, m$

$m =$ order of matrix B

The matrix $B^{-1/2}$ is formed by multiplying the j th column vector of H by μ_j , where $j = 1, 2, \dots, m$. The symmetric matrix $S = (B^{-1/2})' A B^{-1/2}$ is formed in the following two matrix multiplications:

$$Q = (B^{-1/2})' A \quad (2)$$

$$S = QB^{-1/2} \quad (3)$$

and eigenvalues, λ_i , and the matrix of eigenvectors, M , of S are calculated by the subroutine EIGEN.

The matrix $W = B^{-1/2}M$ is formed, and the vectors in W are normalized to form the matrix of eigenvectors, V , by the following equation:

$$V_{ij} = \frac{W_{ij}}{\sqrt{\text{SUMV}_j}} \quad (4)$$

where $i = 1, 2, \dots, m$

$j = 1, 2, \dots, m$

$$\text{SUMV}_j = \sum_{i=1}^m W_{ij}^2 \quad (5)$$

```

C ..... NR00 10
C ..... NR00 20
C SUBROUTINE NROOT NR00 30
C ..... NR00 40
C ..... NR00 50
C PURPOSE NR00 60
C COMPUTE EIGENVALUES AND EIGENVECTORS OF A REAL NONSYMMETRIC NR00 70
C MATRIX OF THE FORM B-INVERSE TIMES A. THIS SUBROUTINE IS NR00 80
C NORMALLY CALLED BY SUBROUTINE CANOR IN PERFORMING A NR00 90
C CANONICAL CORRELATION ANALYSIS. NR00 100
C ..... NR00 110
C USAGE NR00 120
C CALL NROOT (M,A,B,XL,X) NR00 130
C ..... NR00 140

```

```

C ..... NR00 150
C DESCRIPTION OF PARAMETERS NR00 160
C M - ORDER OF SQUARE MATRICES A, B, AND X. NR00 170
C A - INPUT MATRIX (M X M). NR00 180
C B - INPUT MATRIX (M X M). NR00 190
C XL - OUTPUT VECTOR OF LENGTH M CONTAINING EIGENVALUES OF NR00 200
C B-INVERSE TIMES A. NR00 210
C X - OUTPUT MATRIX (M X M) CONTAINING EIGENVECTORS COLUMN- NR00 220
C WISE. NR00 230
C ..... NR00 240
C REMARKS NR00 250
C NONE NR00 260
C ..... NR00 270
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED NR00 280
C EIGEN NR00 290
C ..... NR00 300
C METHOD NR00 310
C REFER TO W. W. COOLEY AND P. R. LOMNES, 'MULTIVARIATE PRO- NR00 320
C CEDURES FOR THE BEHAVIORAL SCIENCES', JOHN WILEY AND SONS, NR00 330
C 1962, CHAPTER 3. NR00 340
C ..... NR00 350
C SUBROUTINE NROOT (M,A,B,XL,X) NR00 360
C DIMENSION A(1),B(1),XL(1),X(1) NR00 370
C ..... NR00 380
C ..... NR00 390
C ..... NR00 400
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE NR00 410
C C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION NR00 420
C STATEMENT WHICH FOLLOWS. NR00 430
C ..... NR00 440
C DOUBLE PRECISION A,B,XL,X,SUMV NR00 450
C ..... NR00 460
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS NR00 470
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS NR00 480
C ROUTINE. NR00 490
C ..... NR00 500
C THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO NR00 510
C CONTAIN DOUBLE PRECISION FORTRAN FUNCTIONS. SORT IN STATEMENT NR00 520
C 110 AND 175 MUST BE CHANGED TO DSORT. ABS IN STATEMENT 110 NR00 530
C MUST BE CHANGED TO DABS. NR00 540
C ..... NR00 550
C ..... NR00 560
C ..... NR00 570
C COMPUTE EIGENVALUES AND EIGENVECTORS OF B NR00 580
C ..... NR00 590
C K=1 NR00 600
C DO 100 J=2,M NR00 610
C L=M*(J-1) NR00 620
C DO 100 I=1,J NR00 630
C L=L+1 NR00 640
C K=K+1 NR00 650
C 100 B(K)=B(L) NR00 660
C ..... NR00 670
C THE MATRIX B IS A REAL SYMMETRIC MATRIX. NR00 680
C ..... NR00 690
C MV=0 NR00 700
C CALL EIGEN (B,X,M,MV) NR00 710
C ..... NR00 720
C FORM RECIPROCAL OF SQUARE ROOT OF EIGENVALUES. THE RESULTS NR00 730
C ARE PREMULTIPLIED BY THE ASSOCIATED EIGENVECTORS. NR00 740
C ..... NR00 750
C L=0 NR00 760
C DO 110 J=1,M NR00 770
C L=L+J NR00 780
C 110 XL(J)=1.0/ SQRT( ABS(B(L)) ) NR00 790
C ..... NR00 800
C K=0 NR00 810
C DO 115 J=1,M NR00 820
C DO 115 I=1,M NR00 830
C K=K+1 NR00 840
C 115 B(K)=X(K)*XL(J) NR00 850
C ..... NR00 860
C FORM (B**(-1/2))PRIME * A * (B**(-1/2)) NR00 870
C ..... NR00 880
C DO 120 I=1,M NR00 890
C N2=0 NR00 900
C DO 120 J=1,M NR00 910
C N1=M*(I-1) NR00 920
C L=M*(J-1)+1 NR00 930
C XL(I)=0 NR00 940
C DO 120 K=1,M NR00 950
C N1=N1+1 NR00 960
C N2=N2+1 NR00 970
C 120 X(L)=X(L)+B(N1)*A(N2) NR00 980
C ..... NR00 990
C L=0 NR00 1000
C DO 130 J=1,M NR00 1010
C DO 130 I=1,J NR00 1020
C N1=I-M NR00 1030
C N2=M*(J-1) NR00 1040
C L=L+1 NR00 1050
C A(L)=0.0 NR00 1060
C DO 130 K=1,M NR00 1070
C N1=N1+M NR00 1080
C N2=N2+1 NR00 1090
C 130 A(L)=A(L)+X(N1)*B(N2) NR00 1100
C ..... NR00 1110
C COMPUTE EIGENVALUES AND EIGENVECTORS OF A NR00 1120
C ..... NR00 1130
C CALL EIGEN (A,X,M,MV) NR00 1140
C L=0 NR00 1150
C DO 140 I=1,M NR00 1160
C L=L+I NR00 1170
C 140 XL(I)=A(L) NR00 1180
C ..... NR00 1190
C COMPUTE THE NORMALIZED EIGENVECTORS NR00 1200
C ..... NR00 1210
C DO 150 I=1,M NR00 1220
C N2=0 NR00 1230
C DO 150 J=1,M NR00 1240
C N1=I-M NR00 1250
C L=M*(J-1)+1 NR00 1260
C A(L)=0.0 NR00 1270
C DO 150 K=1,M NR00 1280
C N1=N1+M NR00 1290
C N2=N2+1 NR00 1300
C 150 A(L)=A(L)+B(N1)*X(N2) NR00 1310
C ..... NR00 1320
C L=0 NR00 1330
C K=0 NR00 1340
C DO 180 J=1,M NR00 1350
C SUMV=0.0 NR00 1360
C DO 170 I=1,M NR00 1370
C L=L+1 NR00 1380
C 170 SUMV=SUMV+A(L)*A(L) NR00 1390
C 175 SUMV= SQRT(SUMV) NR00 1400
C DO 180 I=1,M NR00 1410
C K=K+1 NR00 1420
C 180 X(K)=A(K)/SUMV NR00 1430
C RETURN NR00 1440
C END NR00 1450

```

Subroutine ATEIG

This subroutine computes the eigenvalues of a real upper almost-triangular matrix (Hessenberg form -- see subroutine HSBG) using the double QR iteration of J. G. F. Francis.

1. Mathematical background

a. Definition of the QR iteration

Let A be a real or complex nonsingular matrix of order n . Then a decomposition of A exists of the form

$$A = Q R$$

where Q is unitary and R is upper triangular. If the diagonal elements of R are real and positive, Q is unique. Consider now the sequence of matrices $A^{(p)}$ defined recursively by

$$A^{(0)} = A, \quad A^{(p)} = Q^{(p)} R^{(p)}, \quad A^{(p+1)} = R^{(p)} Q^{(p)} \quad p \geq 0.$$

Note that $A^{(p+1)} = Q^{(p)*} A^{(p)} Q^{(p)}$ for $p \geq 0$; hence it follows that $A^{(p)}$ is similar to A for all p .

Furthermore, if A satisfies certain conditions, it can be proved that $A^{(p)}$ tends to an upper triangular matrix as $p \rightarrow \infty$; thus the eigenvalues of A are the diagonal elements of this limit matrix.

b. Convergence

If the moduli of the eigenvalues are distinct, the elements $a_{ij}^{(p)}$ below the main diagonal of $A^{(p)}$ tend to zero, as do $|\lambda_i|^{p/|\lambda_j|}$, the eigenvalues being subscripted so that $|\lambda_i| > |\lambda_{i+1}|$.

Thus, in general, the eigenvalues appear on the main diagonal, starting from the last position, in increasing order of moduli.

So, when the smallest eigenvalue λ_n has been found, we can reduce the order of the matrix by neglecting the last row and column and find λ_{n-1} by the same process, without any special deflation.

Note that the speed of convergence is considerably improved when the origin of the eigenvalues is shifted close to λ_n .

Such a shift, say $s^{(p)}$, can be introduced before an iteration and the opposite one afterwards. Then the iteration can be written as:

$$A^{(p)} - s^{(p)} I = Q^{(p)} R^{(p)}$$

$$A^{(p+1)} = R^{(p)} Q^{(p)} + s^{(p)} I$$

In general, $A_{n,n}^{(p)}$, for p large enough, can provide an efficient value for $s^{(p)}$.

c. Use of the Hessenberg form

The Hessenberg form is preserved under the QR iteration. Thus, a reduction of the initial matrix to the Hessenberg form can give a significant saving of computation in each iteration for the QR decomposition, the lower part of the matrix consisting only of the codiagonal terms.

Before each iteration, the codiagonal terms will be inspected. If some of these are zero, the matrix will be split according to this occurrence, and the iteration will be applied to the lower main submatrix only.

d. The double QR iteration

Let A be a diagonalizable real upper Hessenberg matrix. Such a matrix must be expected to have complex conjugate pairs of eigenvalues. If these pairs are the only eigenvalues of equal modulus, it can be shown that they will appear as the latent roots of main submatrices of order 2. In this case, if a shift is close to one of these roots, it will be complex, and we will have to deal with complex matrices, although the initial one is real. The use of the double QR iteration avoids this inconvenience.

Taking $s^{(p+1)} = \bar{s}^{(p)}$, consider the transformation giving $A^{(p+2)}$ from $A^{(p)}$:

$$A^{(p+2)} = Q^{(p+1)*} Q^{(p)*} A^{(p)} Q^{(p)} Q^{(p+1)}$$

It can be proved that the product $Q^{(p)} Q^{(p+1)}$ derives from the QR decomposition of the matrix $M = (A^{(p)} - s^{(p)} I) (A^{(p)} - \bar{s}^{(p)} I)$, which is real.

In fact, Francis (1961, 1962) showed that only the first column m_1 of M is necessary for determining the transformation which gives $A^{(p+2)}$ from $A^{(p)}$, if they both have the Hessenberg form.

Practically, the first part of the double iteration consists of the application of an initial transformation $N_1^* A^{(p)} N_1$ where N_1 is unitary and such that $N_1^* m_1 = \pm \|m_1\| e_1$. This leads to a matrix which no longer has the Hessenberg form.

Thus, the remaining part of the iteration will involve the application of $(n-1)$ successive transformations, which have the same form as the initial one whose matrices N_i are such that the resulting matrix $A^{(p+2)}$ has the Hessenberg form.

This process can fail when a subdiagonal term of the given matrix is zero. In this case, the matrix can be split, and the iteration is performed on the lower main submatrix only.

In the subroutine, N_j are Householder's matrices.

2. Programming considerations

At each iteration, the latent roots x_1 and x_2 of the lower main submatrix of order 2 are computed. Then, the following situations can occur:

a. The term $a_{n-1, n-2}$ can be taken as zero. Then, x_1 and x_2 are eigenvalues of the original matrix, and the order of the matrix is reduced by 2. IANA(N) and IANA(N-1) are set to 0 and 2 respectively.

b. The term $a_{n, n-1}$ can be taken as zero. In this case, $a_{n, n}$ is an eigenvalue of the original matrix, and the order of the matrix is reduced by 1. IANA(N) is set to 1.

c. One of the last two subdiagonal terms is stable through one iteration. Then the smaller one is considered as zero. The corresponding components of IANA are set to 0, 1, or 2, according to a. or b.

d. The maximum number of iterations is reached. In this case, the smaller of the last two subdiagonal elements is taken as zero. The corresponding components of IANA are set to 0, 1, or 2, according to a. or b.

The user can check the results by inspecting the subdiagonal terms of the matrix on return from the subroutine, according to the vector IANA, in the following way:

If for each IANA(I) containing 1 or 2, $2 \leq I \leq M$,

$$|A(I, I-1)| \leq 10^{-7} (|RR(I)| + |RI(I)|),$$

then RR(I) and RI(I) were computed with a satisfactory accuracy.

For reference see:

- (1) J. G. F. Francis, Computer Journal, October, 1961 4-3, January, 1962 4-4.
- (2) J. H. Wilkinson, The Algebraic Eigenvalue Problem. Clarendon Press, Oxford, 1965.

C	ATEI 10
C	ATEI 20
C	ATEI 30
C	SLEPCLTIME ATEIC	ATEI 40
C	FLPFSE	ATEI 50
C	CCPFUTE THE EIGENVALLES OF A REAL ALMST TRIANGULAR MATRIX	ATEI 60
C	LSAGE	ATEI 70
C	CALL ATEIC(M,A,RR,R1,IANA,IA)	ATEI 80
C	DESCRIPTION OF THE PARAMETERS	ATEI 90
C	M	ATEI 100
C	ORDER OF THE MATRIX	ATEI 110
C	A	ATEI 120
C	THE IMPLT MATRIX, P BY M	ATEI 130
C	R	ATEI 140
C	VECTOR CONTAINING THE REAL PARTS OF THE EIGENVALUES	ATEI 150
C	CA RETURN	ATEI 160
C	RI	ATEI 170
C	VECTOR CONTAINING THE IMAGINARY PARTS OF THE EIGENVALUES CA RETURN	ATEI 180
C	IANAP	ATEI 190
C	VECTOR WHICH DIMENSION MUST BE GREATER THAN OR EQUAL TO M, CONTAINING CA RETURN INDICATIONS ABOUT THE WAY THE EIGENVALUES APPEARED (SEE MATH. DESCRIPTION)	ATEI 200
C	IA	ATEI 210
C	SIZE OF THE FIRST DIMENSION ASSIGNED TO THE ARRAY A IN THE CALLING PROGRAM WHEN THE MATRIX IS IN DOUBLE	ATEI 220
C	SUBSCRIPTED DATA STORAGE MODE.	ATEI 230
C	IA=M WHEN THE MATRIX IS IN SSP VECTOR STORAGE MODE.	ATEI 240
C	REMARKS	ATEI 250
C	THE ORIGINAL MATRIX IS DESTROYED	ATEI 260
C	THE DIMENSION OF RR AND RI MUST BE GREATER OR EQUAL TO M	ATEI 270
C	SLEPCLTIMES AND FUNCTION SUBPROGRAMS REQUIRED	ATEI 280
C	ACNE	ATEI 290
C	ATEI 300	ATEI 310
C	ATEI 320	ATEI 330
C	ATEI 340	ATEI 350
C	ATEI 360	ATEI 370
C	ATEI 380	ATEI 390
C	ATEI 400	ATEI 410
C	ATEI 420	ATEI 430
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C	ATEI 620	ATEI 630
C	ATEI 640	ATEI 650
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C	ATEI 1140	ATEI 1150
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53C IP1P=IP1+IA ATEI1720
IF1P=IP1+IA ATEI1730
C=A(IIP1P)*(IIP1P)-S1+A(IIP2P)*A(IIP1P)+R ATEI1740
IF(C)54C,56C,54C ATEI1750
54C IF(ABS(A(IIP1P)*A(IIP1P)+S1)*ABS(A(IIP1P)+A(IIP2P)-S1)+ABS(A(IIP2P)*A(IIP1P)+R) ATEI1760
I) ) -ABS(C)*EPS) 62C,62C,56C ATEI1770
56C F=N1-J ATEI1780
58C CC=TITLE ATEI1790
60C CC=TITLE ATEI1800
62C F1=F-1 ATEI1810
G=F1 ATEI1820
IF (F1-1) 68C,68C,65C ATEI1830
65C CC=6C, I=2, P1 ATEI1840
IF1=IP1-IP-1 ATEI1850
IF(ABS(A(IIP1P))-EPS)66C,68C,66C ATEI1860
66C C=C-1 ATEI1870
C ATEI1880
C CR=CLELE ITERATION ATEI1890
C ATEI1900
68C I1=(P-1)*IA+P ATEI1910
CC=I-2C, I=P, A1 ATEI1920
I11=I1-I1 ATEI1930
I1P=I1+IA ATEI1940
IF(I1-P)72C,70C,72C ATEI1950
70C IF1=I1+1 ATEI1960
IF1P=I1P+1 ATEI1970
C ATEI1980
C INITIALIZATION OF THE TRANSFORMATION ATEI1990
C ATEI2000
G1=A(I11)*A(I11)-S1+A(IIP1P)*A(IIP1P)+R ATEI2010
G2=A(IIP1P)*A(IIP1P)+A(I11)-S1 ATEI2020
G3=A(IIP1P)*A(IIP1P)+1 ATEI2030
A(IIP1P)=C, C ATEI2040
CC=TC, 76C ATEI2050
72C G1=A(I11) ATEI2060
G2=A(I11+1) ATEI2070
IF(I1-A2)74C,74C,76C ATEI2080
74C G2=A(I11+2) ATEI2090
CC=TC, 76C ATEI2100
76C G3=C, C ATEI2110
78C CAP=SCRIPT(C1+C1+G2+G2+G3) ATEI2120
IF(CAP)80C,66C,80C ATEI2130
80C IF(C1)82C,84C,84C ATEI2140
82C CAP=-CAP ATEI2150
84C T=C1+CAP ATEI2160
FS12=G3/1 ATEI2170
FS12=C3/1 ATEI2180
ALPH=A-2, C/(1, C+PS11*FS12+PS12+PS12) ATEI2190
CC=TC, 88C ATEI2200
88C ALPH=A-2, C ATEI2210
FS12=C, C ATEI2220
FS12=C, C ATEI2230
88C IF(I1-C)50C,56C,50C ATEI2240
50C IF(I1-P)52C,54C,52C ATEI2250
52C A(I11)=-CAP ATEI2260
CC=TC, 56C ATEI2270
54C A(I11)=A(I11) ATEI2280
C ATEI2290
C FCN OPERATION ATEI2300
C ATEI2310
56C IJ=I1 ATEI2320
CC=IC4C, J=I, N ATEI2330
T=FS11*(IJ+1) ATEI2340
IF(I1-N)58C,100C,100C ATEI2350
58C IF2=IJ+2 ATEI2360
T=T+FS12*(IJ+1) ATEI2370
100C ETA=ALPH*(I+T*(IJ+1)) ATEI2380
A(IJ)=A(IJ)-ETA ATEI2390
A(IJ+1)=A(IJ+1)-PS11*ETA ATEI2400
IF(I1-N)102C,104C,104C ATEI2410
102C A(IF2J)=A(IF2J)-FS12*ETA ATEI2420
104C IJ=IJ+1 ATEI2430
C ATEI2440
C CCLUPN OPERATION ATEI2450
C ATEI2460
IF(I1-N)106C,106C,106C ATEI2470
106C K=N ATEI2480
CC=TC, 110C ATEI2490
108C K=I+2 ATEI2500
110C IF=IIF-I ATEI2510
CC=118C, J=K, K ATEI2520
JIF=IP+J ATEI2530
JI=JIF-IA ATEI2540
T=SI1*(IJ+1) ATEI2550
IF(I1-N)112C,114C,114C ATEI2560
112C JIF2=JIF+IA ATEI2570
T=T+PS12*(IJ+1) ATEI2580
114C ETA=ALPH*(I+T*(IJ+1)) ATEI2590
A(IJ)=A(IJ)-ETA ATEI2600
A(JIF)=A(JIF)-ETA*PS11 ATEI2610
IF(I1-N)116C,116C,116C ATEI2620
116C A(IJF2)=A(IJF2)-ETA*PS12 ATEI2630
118C CC=TITLE ATEI2640
IF(I1-A2)120C,122C,122C ATEI2650
120C JI=I1+3 ATEI2660
JIF=JI+1A ATEI2670
JIF2=JIF+IA ATEI2680
ETA=ALPH*(PS12*(IJ+1)) ATEI2690
A(IJ)=A(IJ)-ETA ATEI2700
A(JIF)=A(JIF)-ETA*PS11 ATEI2710
A(IJF2)=A(IJF2)-ETA*PS12 ATEI2720
122C IJ=IJ+1 ATEI2730
IT=IT+1 ATEI2740
CC=TC, 6C ATEI2750
C ATEI2760
C END OF ITERATION ATEI2770
C ATEI2780
124C IF(ABS(A(I1N1))-ABS(A(I1N2))) 130C,128C,128C ATEI2790
C THE EIGENVALUES HAVE BEEN FOUND ATEI2800
C ATEI2810
128C IAN(I)=C ATEI2820
IAN(I)=I ATEI2830
IAN(I)=I ATEI2840
IF(I2)140C,140C,12C ATEI2850
C ONE EIGENVALUE HAS BEEN FOUND ATEI2860
C ATEI2870
130C IAN(I)=A(I1N1) ATEI2880
I(I1N1)=C, C ATEI2890
I(I1N1)=I ATEI2900
IF(I1N1)140C,140C,132C ATEI2910
132C A=A1 ATEI2920
CC=TC, 2C ATEI2930
140C FEI(LN) ATEI2940
ENC ATEI2950
ATEI2960
ATEI2970

```

Subroutine HSBG

This subroutine reduces an n by n real matrix A by a similarity transformation to upper almost-triangular (Hessenberg) form. Each row is reduced in turn, starting from the last one, by applying a suitable right elimination matrix, and similarity is achieved by also applying the left inverse transformation. Thus the eigenvalues of A are preserved.

1. Mathematical background

Let $A^{(p)}$ denote the matrix obtained from $A^{(0)} = A$ after reducing rows $n, n-1, \dots, n-p+1$. The similarity which transforms $A^{(p)}$ to $A^{(p+1)}$ is as follows:

a. First we determine a pivot element $a_{n-p, k}^{(p)}$, whose column subscript k is such that

$$\left| a_{n-p, k}^{(p)} \right| = \max_i \left| a_{n-p, i}^{(p)} \right|, i = 1, 2, \dots, n-p-1$$

b. If the pivot element $a_{n-p, k}^{(p)} = 0$, no transformations are necessary; that is, the $(p+1)$ th similarity is the identity transformation. Otherwise, if it is necessary ($k \neq n-p-1$), we interchange the k th and $(n-p-1)$ th columns so that the pivot element is in the subdiagonal position. The same interchange is applied to the rows of $A^{(p)}$. The resulting matrix is similar to $A^{(p)}$, and, to ease the notation, we denote it by $A^{(p)}$.

c. Define multipliers

$$b_j^{(p)} = a_{n-p, j}^{(p)} / a_{n-p, n-p-1}^{(p)} \quad j=1, 2, \dots, n-p-2$$

Then the $(p+1)$ th similarity is given by the following.

Right elimination:

$$\bar{a}_{ij}^{(p)} = a_{ij}^{(p)} - b_j^{(p)} a_{i, n-p-1}^{(p)}$$

$$i=1, 2, \dots, n-p$$

$$j=1, 2, \dots, n-p-2$$

$$\bar{a}_{ij}^{(p)} = a_{ij}^{(p)} \quad \text{other indices}$$

Left inverse transformation:

$$a_{n-p-1, j}^{(p+1)} = \bar{a}_{n-p-1, j}^{(p)} + \sum_{i=1}^{n-p-2} b_i^{(p)} \bar{a}_{ij}^{(p)}$$

$$a_{ij}^{(p+1)} = \bar{a}_{ij}^{(p)} \quad i \neq n-p-1$$

Finally, $A^{(n-2)}$ will have the upper almost-triangular form.

For reference see J. H. Wilkinson, The Algebraic Eigenvalue Problem. Clarendon Press, Oxford, 1965.

```

K=K+IA
LK=K+L1
S=A(LK)
LJ=L-IA
DO 280 J=1,L2
JK=K+J
LJ=L+IA
280 S=S+A(LJ)*A(JK)*1.000
300 A(LK)=S
C
C          SET THE LOWER PART OF THE MATRIX TO ZERO
C
DO 310 I=L,LTA,IA
310 A(I)=0.0
320 L=L1
GO TO 20
360 RETURN
END
HSBG1070
HSBG1080
HSBG1090
HSBG1100
HSBG1110
HSBG1120
HSBG1130
HSBG1140
HSBG1150
HSBG1160
HSBG1170
HSBG1180
HSBG1190
HSBG1200
HSBG1210
HSBG1220
HSBG1230
HSBG1240

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C
C .....
C          SUBROUTINE HSBG
C          PURPOSE
C          TO REDUCE A REAL MATRIX INTO UPPER ALMOST TRIANGULAR FORM
C          USAGE
C          CALL HSBG(N,A,IA)
C          DESCRIPTION OF THE PARAMETERS
C          N      ORDER OF THE MATRIX
C          A      THE INPUT MATRIX, N BY N
C          IA     SIZE OF THE FIRST DIMENSION ASSIGNED TO THE ARRAY
C          A IN THE CALLING PROGRAM WHEN THE MATRIX IS IN
C          DOUBLE SUBSCRIPTED DATA STORAGE MODE. IA=N WHEN
C          THE MATRIX IS IN SSP VECTOR STORAGE MODE.
C          REMARKS
C          THE HESSENBERG FORM REPLACES THE ORIGINAL MATRIX IN THE
C          ARRAY A.
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          NONE
C          METHOD
C          SIMILARITY TRANSFORMATIONS USING ELEMENTARY ELIMINATION
C          MATRICES, WITH PARTIAL PIVOTING.
C          REFERENCES
C          J.H. WILKINSON - THE ALGEBRAIC EIGENVALUE PROBLEM -
C          CLARENDON PRESS, OXFORD, 1965.
C .....
C          SUBROUTINE HSBG(N,A,IA)
C          DIMENSION A(1)
C          DOUBLE PRECISION S
C          L=N
C          NIA=L*IA
C          LIA=NIA-IA
C          L IS THE ROW INDEX OF THE ELIMINATION
C
C          20 IF(L-3) 360,40,40
C          40 LIA=LIA-IA
C          L1=L-1
C          L2=L1-1
C          SEARCH FOR THE PIVOTAL ELEMENT IN THE LTH ROW
C
C          ISUB=LIA+L
C          IPIV=ISUB-IA
C          PIV=ABS(A(IPIV))
C          IF(L-3) 90,90,50
C          50 M=IPIV-IA
C          DO 90 I=L,M,IA
C          T=ABS(A(I))
C          IF(T-PIV) 80,80,60
C          60 IPIV=I
C          PIV=T
C          80 CONTINUE
C          90 IF(PIV) 100,320,100
C          100 IF(PIV-ABS(A(ISUB))) 180,180,120
C          INTERCHANGE THE COLUMNS
C
C          120 M=IPIV-L
C          DO 140 I=L,L
C          J=M+I
C          T=A(J)
C          K=LIA+I
C          A(J)=A(K)
C          140 A(K)=T
C          INTERCHANGE THE ROWS
C
C          M=L2-M/IA
C          DO 160 I=L1,NIA,IA
C          T=A(I)
C          J=-M
C          A(I)=A(J)
C          160 A(J)=T
C          TERMS OF THE ELEMENTARY TRANSFORMATION
C
C          180 DO 200 I=L,LIA,IA
C          200 A(I)=A(I)/A(ISUB)
C          RIGHT TRANSFORMATION
C
C          J=-IA
C          DO 240 I=1,L2
C          J=J+IA
C          LJ=L+J
C          DO 220 K=1,L1
C          KJ=K+J
C          KL=K+LIA
C          220 A(KJ)=A(KJ)-A(LJ)*A(KL)
C          240 CONTINUE
C          LEFT TRANSFORMATION
C
C          K=-IA
C          DO 300 I=1,N

```

Polynomials: Operations

Subroutine PADD

```

C
C .....
C          PADD 10
C          PADD 20
C          PADD 30
C          PADD 40
C          PADD 50
C          PADD 60
C          PADD 70
C          PADD 80
C          PADD 90
C          PADD 100
C          PADD 110
C          PADD 120
C          PADD 130
C          PADD 140
C          PADD 150
C          PADD 160
C          PADD 170
C          PADD 180
C          PADD 190
C          PADD 200
C          PADD 210
C          PADD 220
C          PADD 230
C          PADD 240
C          PADD 250
C          PADD 260
C          PADD 270
C          PADD 280
C          PADD 290
C          PADD 300
C          PADD 310
C          PADD 320
C          PADD 330
C          PADD 340
C          PADD 350
C          PADD 360
C          PADD 370
C          PADD 380
C          PADD 390
C          PADD 400
C          PADD 410
C          PADD 420
C          PADD 430
C          PADD 440
C          PADD 450
C          PADD 460
C          PADD 470
C          PADD 480
C          PADD 490
C          PADD 500
C          PADD 510
C          PADD 520
C          PADD 530
C          PADD 540
C          PADD 550
C          PADD 560
C          PADD 570
C          PADD 580
C          PADD 590
C          PADD 590
C          END
C
SUBROUTINE PADD
C
PURPOSE
  ADD TWO POLYNOMIALS
C
USAGE
  CALL PADD(Z, IDIMZ, X, IDIMX, Y, IDIMY)
C
DESCRIPTION OF PARAMETERS
  Z - VECTOR OF RESULTANT COEFFICIENTS, ORDERED FROM
    SMALLEST TO LARGEST POWER
  IDIMZ - DIMENSION OF Z (CALCULATED)
  X - VECTOR OF COEFFICIENTS FOR FIRST POLYNOMIAL, ORDERED
    FROM SMALLEST TO LARGEST POWER
  IDIMX - DIMENSION OF X (DEGREE IS IDIMX-1)
  Y - VECTOR OF COEFFICIENTS FOR SECOND POLYNOMIAL,
    ORDERED FROM SMALLEST TO LARGEST POWER
  IDIMY - DIMENSION OF Y (DEGREE IS IDIMY-1)
C
REMARKS
  VECTOR Z MAY BE IN SAME LOCATION AS EITHER VECTOR X OR
  VECTOR Y ONLY IF THE DIMENSION OF THAT VECTOR IS NOT LESS
  THAN THE OTHER INPUT VECTOR
  THE RESULTANT POLYNOMIAL MAY HAVE TRAILING ZERO COEFFICIENTS
C
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
C
METHOD
  DIMENSION OF RESULTANT VECTOR IDIMZ IS CALCULATED AS THE
  LARGER OF THE TWO INPUT VECTOR DIMENSIONS. CORRESPONDING
  COEFFICIENTS ARE THEN ADDED TO FORM Z.
C
SUBROUTINE PADD(Z, IDIMZ, X, IDIMX, Y, IDIMY)
  DIMENSION Z(1), X(1), Y(1)
C
TEST DIMENSIONS OF SUMMANDS
  NDIM=IDIMX
  IF (IDIMX-IDIMY) 10,20,20
10  NDIM=IDIMY
20  IF (NDIM) 90,90,30
30  DO 80 I=1,NDIM
   IF (I-IDIMX) 40,40,60
   IF (I-IDIMY) 50,50,70
40  Z(I)=X(I)+Y(I)
   GO TO 80
50  Z(I)=X(I)+Y(I)
   GO TO 80
60  Z(I)=Y(I)
   GO TO 80
70  Z(I)=X(I)
80  CONTINUE
90  IDIMZ=NDIM
   RETURN
   END

```

Subroutine PSUB

```

C .....
C          PSUB 10
C          PSUB 20
C          PSUB 30
C          PSUB 40
C          PSUB 50
C          PSUB 60
C          PSUB 70
C          PSUB 80
C          PSUB 90
C          PSUB 100
C          PSUB 110
C          PSUB 120
C          PSUB 130
C          PSUB 140
C          PSUB 150
C          PSUB 160
C          PSUB 170
C          PSUB 180
C          PSUB 190
C          PSUB 200
C          PSUB 210
C          PSUB 220
C          PSUB 230
C          PSUB 240
C          PSUB 250
C          PSUB 260
C          PSUB 270
C          PSUB 280
C          PSUB 290
C          PSUB 300
C          PSUB 310
C          PSUB 320
C          PSUB 330
C          PSUB 340
C          PSUB 350
C          PSUB 360
C          PSUB 370
C          PSUB 380
C          PSUB 390
C          PSUB 400
C          PSUB 410
C          PSUB 420
C          PSUB 430
C          PSUB 440
C          PSUB 450
C          PSUB 460
C          PSUB 470
C          PSUB 480
C          PSUB 490
C          PSUB 500
C          PSUB 510
C          PSUB 520
C          PSUB 530
C          PSUB 540
C          PSUB 550
C          PSUB 560
C          PSUB 570
C          PSUB 580
C          PSUB 590
C          PSUB 600
C
SUBROUTINE PSUB
C
PURPOSE
  SUBTRACT ONE POLYNOMIAL FROM ANOTHER
C
USAGE
  CALL PSUB(Z, IDIMZ, X, IDIMX, Y, IDIMY)
C
DESCRIPTION OF PARAMETERS
  Z - VECTOR OF RESULTANT COEFFICIENTS, ORDERED FROM
    SMALLEST TO LARGEST POWER
  IDIMZ - DIMENSION OF Z (CALCULATED)
  X - VECTOR OF COEFFICIENTS FOR FIRST POLYNOMIAL, ORDERED
    FROM SMALLEST TO LARGEST POWER
  IDIMX - DIMENSION OF X (DEGREE IS IDIMX-1)
  Y - VECTOR OF COEFFICIENTS FOR SECOND POLYNOMIAL,
    ORDERED FROM SMALLEST TO LARGEST POWER
  IDIMY - DIMENSION OF Y (DEGREE IS IDIMY-1)
C
REMARKS
  VECTOR Z MAY BE IN SAME LOCATION AS EITHER VECTOR X OR
  VECTOR Y ONLY IF THE DIMENSION OF THAT VECTOR IS NOT LESS
  THAN THE OTHER INPUT VECTOR
  THE RESULTANT POLYNOMIAL MAY HAVE TRAILING ZERO COEFFICIENTS
C
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
C
METHOD
  DIMENSION OF RESULTANT VECTOR IDIMZ IS CALCULATED AS THE
  LARGER OF THE TWO INPUT VECTOR DIMENSIONS. COEFFICIENTS IN
  VECTOR Y ARE THEN SUBTRACTED FROM CORRESPONDING COEFFICIENTS
  IN VECTOR X.
C
SUBROUTINE PSUB(Z, IDIMZ, X, IDIMX, Y, IDIMY)
  DIMENSION Z(1), X(1), Y(1)
C
TEST DIMENSIONS OF SUMMANDS
  NDIM=IDIMX
  IF (IDIMX-IDIMY) 10,20,20
10  NDIM=IDIMY
20  IF (NDIM) 90,90,30
30  DO 80 I=1,NDIM
   IF (I-IDIMX) 40,40,60
   IF (I-IDIMY) 50,50,70
40  Z(I)=X(I)-Y(I)
   GO TO 80
50  Z(I)=X(I)-Y(I)
   GO TO 80
60  Z(I)=X(I)
   GO TO 80
70  Z(I)=X(I)
80  CONTINUE
90  IDIMZ=NDIM
   RETURN
   END

```

Subroutine PMPY

```

C ..... PMPY 10
C ..... PMPY 20
C ..... PMPY 30
SUBROUTINE PMPY PMPY 40
C ..... PMPY 50
PURPOSE PMPY 60
C ..... PMPY 70
MULTIPLY TWO POLYNOMIALS PMPY 80
C ..... PMPY 90
USAGE PMPY 100
C ..... PMPY 110
CALL PMPY(Z, IDIMZ, X, IDIMX, Y, IDIMY) PMPY 120
C ..... PMPY 130
DESCRIPTION OF PARAMETERS PMPY 140
C ..... PMPY 150
Z - VECTOR OF RESULTANT COEFFICIENTS, ORDERED FROM PMPY 160
C ..... PMPY 170
SMALLEST TO LARGEST POWER PMPY 180
C ..... PMPY 190
IDIMZ - DIMENSION OF Z (CALCULATED) PMPY 200
C ..... PMPY 210
X - VECTOR OF COEFFICIENTS FOR FIRST POLYNOMIAL, ORDERED PMPY 220
C ..... PMPY 230
FROM SMALLEST TO LARGEST POWER PMPY 240
C ..... PMPY 250
IDIMX - DIMENSION OF X (DEGREE IS IDIMX-1) PMPY 260
C ..... PMPY 270
Y - VECTOR OF COEFFICIENTS FOR SECOND POLYNOMIAL, PMPY 280
C ..... PMPY 290
ORDERED FROM SMALLEST TO LARGEST POWER PMPY 300
C ..... PMPY 310
IDIMY - DIMENSION OF Y (DEGREE IS IDIMY-1) PMPY 320
C ..... PMPY 330
REMARKS PMPY 340
C ..... PMPY 350
Z CANNOT BE IN THE SAME LOCATION AS X PMPY 360
C ..... PMPY 370
Z CANNOT BE IN THE SAME LOCATION AS Y PMPY 380
C ..... PMPY 390
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED PMPY 400
C ..... PMPY 410
NONE PMPY 420
C ..... PMPY 430
METHOD PMPY 440
C ..... PMPY 450
DIMENSION OF Z IS CALCULATED AS IDIMX+IDIMY-1 PMPY 460
C ..... PMPY 470
THE COEFFICIENTS OF Z ARE CALCULATED AS SUM OF PRODUCTS PMPY 480
C ..... PMPY 490
OF COEFFICIENTS OF X AND Y, WHOSE EXPONENTS ADD UP TO THE PMPY 500
C ..... PMPY 510
CORRESPONDING EXPONENT OF Z. PMPY 520
C ..... PMPY 530
C ..... PMPY 540
C ..... PMPY 550
C ..... PMPY 560
C ..... PMPY 570
C ..... PMPY 580
C ..... PMPY 590
C ..... PMPY 600
C ..... PMPY 610
C ..... PMPY 620
C ..... PMPY 630
C ..... PMPY 640
C ..... PMPY 650
C ..... PMPY 660
C ..... PMPY 670
C ..... PMPY 680
C ..... PMPY 690
C ..... PMPY 700
C ..... PMPY 710
C ..... PMPY 720
C ..... PMPY 730
C ..... PMPY 740
C ..... PMPY 750
C ..... PMPY 760
C ..... PMPY 770
C ..... PMPY 780
C ..... PMPY 790
C ..... PMPY 800
C ..... PMPY 810
C ..... PMPY 820
C ..... PMPY 830
C ..... PMPY 840
C ..... PMPY 850
C ..... PMPY 860
C ..... PMPY 870
C ..... PMPY 880
C ..... PMPY 890
C ..... PMPY 900
C ..... PMPY 910
C ..... PMPY 920
C ..... PMPY 930
C ..... PMPY 940
C ..... PMPY 950
C ..... PMPY 960
C ..... PMPY 970
C ..... PMPY 980
C ..... PMPY 990
C ..... PMPY 1000
SUBROUTINE PMPY(Z, IDIMZ, X, IDIMX, Y, IDIMY)
DIMENSION Z(1), X(1), Y(1)
IF (IDIMX+IDIMY) 10, 10, 20
10 IDIMZ=0
GO TO 50
20 IDIMZ=IDIMX+IDIMY-1
DO 30 I=1, IDIMZ
30 Z(I)=0.
DO 40 I=1, IDIMX
DO 40 J=1, IDIMY
K=I+J-1
40 Z(K)=X(I)*Y(J)+Z(K)
50 RETURN
END

```

Subroutine PDIV

```

C ..... PDIV 10
C ..... PDIV 20
C ..... PDIV 30
SUBROUTINE PDIV PDIV 40
C ..... PDIV 50
PURPOSE PDIV 60
C ..... PDIV 70
DIVIDE ONE POLYNOMIAL BY ANOTHER PDIV 80
C ..... PDIV 90
USAGE PDIV 100
C ..... PDIV 110
CALL PDIV(P, IDIMP, X, IOIMX, Y, IDIMY, TOL, IER) PDIV 120
C ..... PDIV 130
DESCRIPTION OF PARAMETERS PDIV 140
C ..... PDIV 150
P - RESULTANT VECTOR OF INTEGRAL PART PDIV 160
C ..... PDIV 170
IDIMP - DIMENSION OF P PDIV 180
C ..... PDIV 190
X - VECTOR OF COEFFICIENTS FOR DIVIDEND POLYNOMIAL, PDIV 200
C ..... PDIV 210
ORDERED FROM SMALLEST TO LARGEST POWER. IT IS PDIV 220
REPLACED BY REMAINDER AFTER DIVISION. PDIV 230
C ..... PDIV 240
IDIMX - DIMENSION OF X PDIV 250
C ..... PDIV 260
Y - VECTOR OF COEFFICIENTS FOR DIVISOR POLYNOMIAL, PDIV 270
C ..... PDIV 280
ORDERED FROM SMALLEST TO LARGEST POWER PDIV 290
C ..... PDIV 300
IDIMY - DIMENSION OF Y PDIV 310
C ..... PDIV 320
TOL - TOLERANCE VALUE BELOW WHICH COEFFICIENTS ARE PDIV 330
ELIMINATED DURING NORMALIZATION PDIV 340
C ..... PDIV 350
IER - ERROR CODE. 0 IS NORMAL, 1 IS FOR ZERO DIVISOR PDIV 360
C ..... PDIV 370
REMARKS PDIV 380
C ..... PDIV 390
THE REMAINDER R REPLACES X. PDIV 400
C ..... PDIV 410
THE DIVISOR Y REMAINS UNCHANGED. PDIV 420
C ..... PDIV 430
IF DIMENSION OF Y EXCEEDS DIMENSION OF X, IDIMP IS SET TO PDIV 440
ZERO AND CALCULATION IS BYPASSED PDIV 450
C ..... PDIV 460
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED PDIV 470
C ..... PDIV 480
PNORM PDIV 490
C ..... PDIV 500
METHOD PDIV 510
C ..... PDIV 520
POLYNOMIAL X IS DIVIDED BY POLYNOMIAL Y GIVING INTEGER PART PDIV 530
C ..... PDIV 540
P AND REMAINDER R SUCH THAT X = P*Y + R. PDIV 550
C ..... PDIV 560
DIVISOR Y AND REMAINDER VECTOR GET NORMALIZED. PDIV 570
C ..... PDIV 580
C ..... PDIV 590
C ..... PDIV 600
C ..... PDIV 610
C ..... PDIV 620
C ..... PDIV 630
C ..... PDIV 640
C ..... PDIV 650
C ..... PDIV 660
C ..... PDIV 670
C ..... PDIV 680
C ..... PDIV 690
C ..... PDIV 700
C ..... PDIV 710
C ..... PDIV 720
C ..... PDIV 730
C ..... PDIV 740
C ..... PDIV 750
C ..... PDIV 760
C ..... PDIV 770
C ..... PDIV 780
C ..... PDIV 790
C ..... PDIV 800
C ..... PDIV 810
C ..... PDIV 820
C ..... PDIV 830
C ..... PDIV 840
C ..... PDIV 850
C ..... PDIV 860
C ..... PDIV 870
C ..... PDIV 880
C ..... PDIV 890
C ..... PDIV 900
C ..... PDIV 910
C ..... PDIV 920
C ..... PDIV 930
C ..... PDIV 940
C ..... PDIV 950
C ..... PDIV 960
C ..... PDIV 970
C ..... PDIV 980
C ..... PDIV 990
C ..... PDIV 1000
SUBROUTINE PDIV(P, IDIMP, X, IOIMX, Y, IDIMY, TOL, IER)
DIMENSION P(1), X(1), Y(1)
CALL PNORM (Y, IDIMY, TOL)
IF (IDIMY) 50, 50, 10
10 IDIMP=IDIMX-IDIMY+1
IF (IDIMP) 20, 30, 60
C ..... PDIV 400
DEGREE OF DIVISOR WAS GREATER THAN DEGREE OF DIVIDEND PDIV 410
C ..... PDIV 420
20 IDIMP=0 PDIV 430
C ..... PDIV 440
30 IER=0 PDIV 450
C ..... PDIV 460
40 RETURN PDIV 470
C ..... PDIV 480
C ..... PDIV 490
C ..... PDIV 500
C ..... PDIV 510
C ..... PDIV 520
C ..... PDIV 530
C ..... PDIV 540
C ..... PDIV 550
C ..... PDIV 560
C ..... PDIV 570
C ..... PDIV 580
C ..... PDIV 590
C ..... PDIV 600
C ..... PDIV 610
C ..... PDIV 620
C ..... PDIV 630
C ..... PDIV 640
C ..... PDIV 650
C ..... PDIV 660
C ..... PDIV 670
C ..... PDIV 680
C ..... PDIV 690
C ..... PDIV 700
C ..... PDIV 710
C ..... PDIV 720
C ..... PDIV 730
C ..... PDIV 740
C ..... PDIV 750
C ..... PDIV 760
C ..... PDIV 770
C ..... PDIV 780
C ..... PDIV 790
C ..... PDIV 800
C ..... PDIV 810
C ..... PDIV 820
C ..... PDIV 830
C ..... PDIV 840
C ..... PDIV 850
C ..... PDIV 860
C ..... PDIV 870
C ..... PDIV 880
C ..... PDIV 890
C ..... PDIV 900
C ..... PDIV 910
C ..... PDIV 920
C ..... PDIV 930
C ..... PDIV 940
C ..... PDIV 950
C ..... PDIV 960
C ..... PDIV 970
C ..... PDIV 980
C ..... PDIV 990
C ..... PDIV 1000
50 IER=1
GO TO 40
C ..... PDIV 600
START REDUCTION PDIV 610
C ..... PDIV 620
60 IDIMX=IDIMY-1 PDIV 630
C ..... PDIV 640
I=IDIMP PDIV 650
C ..... PDIV 660
70 II=I+IDIMX PDIV 670
C ..... PDIV 680
P(I)=X(II)/Y(IDIMY) PDIV 690
C ..... PDIV 700
SUBTRACT MULTIPLE OF DIVISOR PDIV 710
C ..... PDIV 720
DO 80 K=1, IDIMX PDIV 730
C ..... PDIV 740
J=K-I+1 PDIV 750
C ..... PDIV 760
X(J)=X(J)-P(I)*Y(K) PDIV 770
C ..... PDIV 780
80 CONTINUE PDIV 790
C ..... PDIV 800
I=I-1 PDIV 810
C ..... PDIV 820
IF (I) 90, 90, 70 PDIV 830
C ..... PDIV 840
NORMALIZE REMAINDER POLYNOMIAL PDIV 850
C ..... PDIV 860
90 CALL PNORM(X, IDIMX, TOL) PDIV 870
C ..... PDIV 880
GO TO 30 PDIV 890
C ..... PDIV 900
END PDIV 910

```


Subroutine PCLA

```

C ..... PCLA 10
C ..... PCLA 20
C ..... PCLA 30
C ..... PCLA 40
C ..... PCLA 50
C ..... PCLA 60
C ..... PCLA 70
C ..... PCLA 80
C ..... PCLA 90
C ..... PCLA 100
C ..... PCLA 110
C ..... PCLA 120
C ..... PCLA 130
C ..... PCLA 140
C ..... PCLA 150
C ..... PCLA 160
C ..... PCLA 170
C ..... PCLA 180
C ..... PCLA 190
C ..... PCLA 200
C ..... PCLA 210
C ..... PCLA 220
C ..... PCLA 230
C ..... PCLA 240
C ..... PCLA 250
C ..... PCLA 260
C ..... PCLA 270
C ..... PCLA 280
C ..... PCLA 290
C ..... PCLA 300
C ..... PCLA 310
C ..... PCLA 320
C ..... PCLA 330
C ..... PCLA 340
C ..... PCLA 350
C ..... PCLA 360
C ..... PCLA 370
C ..... PCLA 380
C ..... PCLA 390
C ..... PCLA 400

SUBROUTINE PCLA
PURPOSE
  MOVE POLYNOMIAL X TO Y
USAGE
  CALL PCLA(Y, IDIMY, X, IDIMX)
DESCRIPTION OF PARAMETERS
  Y - VECTOR OF RESULTANT COEFFICIENTS, ORDERED FROM
      SMALLEST TO LARGEST POWER
  IDIMY - DIMENSION OF Y
  X - VECTOR OF COEFFICIENTS FOR POLYNOMIAL, ORDERED
      FROM SMALLEST TO LARGEST POWER
  IDIMX - DIMENSION OF X
REMARKS
  NONE
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
METHOD
  IDIMY IS REPLACED BY IDIMX AND VECTOR X IS MOVED TO Y
.....
SUBROUTINE PCLA (Y, IDIMY, X, IDIMX)
DIMENSION X(1), Y(1)
IDIMY=IDIMX
IF (IDIMX) 30, 30, 10
10 DO 20 I=1, IDIMX
20 Y(I)=X(I)
30 RETURN
END

```

Subroutine PADDM

```

C ..... PDDM 10
C ..... PDDM 20
C ..... PDDM 30
C ..... PDDM 40
C ..... PDDM 50
C ..... PDDM 60
C ..... PDDM 70
C ..... PDDM 80
C ..... PDDM 90
C ..... PDDM 100
C ..... PDDM 110
C ..... PDDM 120
C ..... PDDM 130
C ..... PDDM 140
C ..... PDDM 150
C ..... PDDM 160
C ..... PDDM 170
C ..... PDDM 180
C ..... PDDM 190
C ..... PDDM 200
C ..... PDDM 210
C ..... PDDM 220
C ..... PDDM 230
C ..... PDDM 240
C ..... PDDM 250
C ..... PDDM 260
C ..... PDDM 270
C ..... PDDM 280
C ..... PDDM 290
C ..... PDDM 300
C ..... PDDM 310
C ..... PDDM 320
C ..... PDDM 330
C ..... PDDM 340
C ..... PDDM 350
C ..... PDDM 360
C ..... PDDM 370
C ..... PDDM 380
C ..... PDDM 390
C ..... PDDM 400
C ..... PDDM 410
C ..... PDDM 420
C ..... PDDM 430
C ..... PDDM 440
C ..... PDDM 450
C ..... PDDM 460
C ..... PDDM 470
C ..... PDDM 480
C ..... PDDM 490
C ..... PDDM 500
C ..... PDDM 510
C ..... PDDM 520
C ..... PDDM 530
C ..... PDDM 540
C ..... PDDM 550
C ..... PDDM 560
C ..... PDDM 570
C ..... PDDM 580
C ..... PDDM 590
C ..... PDDM 600
C ..... PDDM 610
C ..... PDDM 620

SUBROUTINE PADDM
PURPOSE
  ADD COEFFICIENTS OF ONE POLYNOMIAL TO THE PRODUCT OF A
  FACTOR BY COEFFICIENTS OF ANOTHER POLYNOMIAL
USAGE
  CALL PADDM(Z, IDIMZ, X, IDIMX, FACT, Y, IDIMY)
DESCRIPTION OF PARAMETERS
  Z - VECTOR OF RESULTANT COEFFICIENTS, ORDERED FROM
      SMALLEST TO LARGEST POWER
  IDIMZ - DIMENSION OF Z (CALCULATED)
  X - VECTOR OF COEFFICIENTS FOR FIRST POLYNOMIAL, ORDERED
      FROM SMALLEST TO LARGEST POWER
  IDIMX - DIMENSION OF X (DEGREE IS IDIMX-1)
  FACT - FACTOR TO BE MULTIPLIED BY VECTOR Y
  Y - VECTOR OF COEFFICIENTS FOR SECOND POLYNOMIAL,
      ORDERED FROM SMALLEST TO LARGEST POWER
  IDIMY - DIMENSION OF Y (DEGREE IS IDIMY-1)
REMARKS
  VECTOR Z MAY BE IN SAME LOCATION AS EITHER VECTOR X OR
  VECTOR Y ONLY IF THE DIMENSION OF THAT VECTOR IS NOT LESS
  THAN THE OTHER INPUT VECTOR
  THE RESULTANT POLYNOMIAL MAY HAVE TRAILING ZERO COEFFICIENTS
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
METHOD
  DIMENSION OF RESULTANT VECTOR IDIMZ IS CALCULATED AS THE
  LARGER OF THE TWO INPUT VECTOR DIMENSIONS. COEFFICIENT IN
  VECTOR X IS THEN ADDED TO COEFFICIENT IN VECTOR Y MULTIPLIED
  BY FACTOR TO FORM Z.
.....
SUBROUTINE PADDM(Z, IDIMZ, X, IDIMX, FACT, Y, IDIMY)
DIMENSION Z(1), X(1), Y(1)
TEST DIMENSIONS OF SUMMANDS
NDIM=IDIMX
IF (IDIMX-IDIMY) 10, 20, 20
10 NDIM=IDIMY
20 IF (NDIM) 90, 90, 30
30 DO 80 I=1, NDIM
  IF (I-IDIMX) 40, 40, 60
  IF (I-IDIMY) 50, 50, 70
  Z(I)=FACT*Y(I)+X(I)
  GO TO 80
40 Z(I)=FACT*Y(I)
  GO TO 80
70 Z(I)=X(I)
80 CONTINUE
90 IDIMZ=NDIM
RETURN
END

```

Subroutine PVAL

```

C ..... PVAL 10
C ..... PVAL 20
C ..... PVAL 30
C ..... PVAL 40
C ..... PVAL 50
C ..... PVAL 60
C ..... PVAL 70
C ..... PVAL 80
C ..... PVAL 90
C ..... PVAL 100
C ..... PVAL 110
C ..... PVAL 120
C ..... PVAL 130
C ..... PVAL 140
C ..... PVAL 150
C ..... PVAL 160
C ..... PVAL 170
C ..... PVAL 180
C ..... PVAL 190
C ..... PVAL 200
C ..... PVAL 210
C ..... PVAL 220
C ..... PVAL 230
C ..... PVAL 240
C ..... PVAL 250
C ..... PVAL 260
C ..... PVAL 270
C ..... PVAL 280
C ..... PVAL 290
C ..... PVAL 300
C ..... PVAL 310
C ..... PVAL 320
C ..... PVAL 330
C ..... PVAL 340
C ..... PVAL 350
C ..... PVAL 360
C ..... PVAL 370
C ..... PVAL 380
C ..... PVAL 390
C ..... PVAL 400
C ..... PVAL 410
C ..... PVAL 420
C ..... PVAL 430
C ..... PVAL 440
C ..... PVAL 450
C ..... PVAL 460
C ..... PVAL 470
C ..... PVAL 480
C ..... PVAL 490
C ..... PVAL 500
C ..... PVAL 510
C ..... PVAL 520
C ..... PVAL 530
C ..... PVAL 540
C ..... PVAL 550
C ..... PVAL 560
C ..... PVAL 570
C ..... PVAL 580
C ..... PVAL 590
C ..... PVAL 600
C ..... PVAL 610
C ..... PVAL 620
C ..... PVAL 630
C ..... PVAL 640
C ..... PVAL 650
C ..... PVAL 660
C ..... PVAL 670
C ..... PVAL 680
C ..... PVAL 690
C ..... PVAL 700
C ..... PVAL 710
C ..... PVAL 720
C ..... PVAL 730
C ..... PVAL 740
C ..... PVAL 750
C ..... PVAL 760
C ..... PVAL 770
C ..... PVAL 780
C ..... PVAL 790
C ..... PVAL 800
C ..... PVAL 810
C ..... PVAL 820
C ..... PVAL 830
C ..... PVAL 840
C ..... PVAL 850
C ..... PVAL 860
C ..... PVAL 870
C ..... PVAL 880
C ..... PVAL 890
C ..... PVAL 900
C ..... PVAL 910
C ..... PVAL 920
C ..... PVAL 930
C ..... PVAL 940
C ..... PVAL 950
C ..... PVAL 960
C ..... PVAL 970
C ..... PVAL 980
C ..... PVAL 990
C ..... PVAL 1000

```

Subroutine PVSUB

```

C ..... PVSU 10
C ..... PVSU 20
C ..... PVSU 30
C ..... PVSU 40
C ..... PVSU 50
C ..... PVSU 60
C ..... PVSU 70
C ..... PVSU 80
C ..... PVSU 90
C ..... PVSU 100
C ..... PVSU 110
C ..... PVSU 120
C ..... PVSU 130
C ..... PVSU 140
C ..... PVSU 150
C ..... PVSU 160
C ..... PVSU 170
C ..... PVSU 180
C ..... PVSU 190
C ..... PVSU 200
C ..... PVSU 210
C ..... PVSU 220
C ..... PVSU 230
C ..... PVSU 240
C ..... PVSU 250
C ..... PVSU 260
C ..... PVSU 270
C ..... PVSU 280
C ..... PVSU 290
C ..... PVSU 300
C ..... PVSU 310
C ..... PVSU 320
C ..... PVSU 330
C ..... PVSU 340
C ..... PVSU 350
C ..... PVSU 360
C ..... PVSU 370
C ..... PVSU 380
C ..... PVSU 390
C ..... PVSU 400
C ..... PVSU 410
C ..... PVSU 420
C ..... PVSU 430
C ..... PVSU 440
C ..... PVSU 450
C ..... PVSU 460
C ..... PVSU 470
C ..... PVSU 480
C ..... PVSU 490
C ..... PVSU 500
C ..... PVSU 510
C ..... PVSU 520
C ..... PVSU 530
C ..... PVSU 540
C ..... PVSU 550
C ..... PVSU 560
C ..... PVSU 570
C ..... PVSU 580
C ..... PVSU 590
C ..... PVSU 600
C ..... PVSU 610
C ..... PVSU 620
C ..... PVSU 630
C ..... PVSU 640
C ..... PVSU 650
C ..... PVSU 660
C ..... PVSU 670
C ..... PVSU 680
C ..... PVSU 690
C ..... PVSU 700
C ..... PVSU 710
C ..... PVSU 720
C ..... PVSU 730
C ..... PVSU 740
C ..... PVSU 750
C ..... PVSU 760
C ..... PVSU 770
C ..... PVSU 780
C ..... PVSU 790
C ..... PVSU 800
C ..... PVSU 810
C ..... PVSU 820
C ..... PVSU 830
C ..... PVSU 840
C ..... PVSU 850
C ..... PVSU 860
C ..... PVSU 870
C ..... PVSU 880
C ..... PVSU 890
C ..... PVSU 900
C ..... PVSU 910
C ..... PVSU 920
C ..... PVSU 930
C ..... PVSU 940
C ..... PVSU 950
C ..... PVSU 960
C ..... PVSU 970
C ..... PVSU 980
C ..... PVSU 990
C ..... PVSU 1000

```

Subroutine PILD

```

C .....
C SUBROUTINE PILD
C .....
C PURPOSE
C EVALUATE POLYNOMIAL AND ITS FIRST DERIVATIVE FOR A GIVEN
C ARGUMENT
C .....
C USAGE
C CALL PILD(POLY,DVAL,ARGUM,X,IDIMX)
C .....
C DESCRIPTION OF PARAMETERS
C POLY - VALUE OF POLYNOMIAL
C DVAL - DERIVATIVE
C ARGUM - ARGUMENT
C X - VECTOR OF COEFFICIENTS FOR POLYNOMIAL, ORDERED
C FROM SMALLEST TO LARGEST POWER
C IDIMX - DIMENSION OF X
C .....
C REMARKS
C NONE
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C PQSD
C .....
C METHOD
C EVALUATION IS DONE BY MEANS OF SUBROUTINE PQSD (QUADRATIC
C SYNTHETIC DIVISION)
C .....
C SUBROUTINE PILD (POLY,DVAL,ARGUM,X,IDIMX)
C DIMENSION X(1)
C .....
C P=ARGUM*ARGUM
C Q=-ARGUM*ARGUM
C .....
C CALL PQSD (DVAL,POLY,P,Q,X,IDIMX)
C .....
C POLY=ARGUM*DVAL+POLY
C .....
C RETURN
C END
PILD 10
PILD 20
PILD 30
PILD 40
PILD 50
PILD 60
PILD 70
PILD 80
PILD 90
PILD 100
PILD 110
PILD 120
PILD 130
PILD 140
PILD 150
PILD 160
PILD 170
PILD 180
PILD 190
PILD 200
PILD 210
PILD 220
PILD 230
PILD 240
PILD 250
PILD 260
PILD 270
PILD 280
PILD 290
PILD 300
PILD 310
PILD 320
PILD 330
PILD 340
PILD 350
PILD 360
PILD 370
PILD 380
PILD 390
PILD 400
PILD 410
PILD 420
PILD 430
PILD 440

```

Subroutine PDER

```

C .....
C SUBROUTINE PDER
C .....
C PURPOSE
C FIND FIRST DERIVATIVE OF A POLYNOMIAL
C .....
C USAGE
C CALL PDER(Y,IDIMY,X,IDIMX)
C .....
C DESCRIPTION OF PARAMETERS
C Y - VECTOR OF COEFFICIENTS FOR DERIVATIVE, ORDERED FROM
C SMALLEST TO LARGEST POWER
C IDIMY - DIMENSION OF Y (EQUAL TO IDIMX-1)
C X - VECTOR OF COEFFICIENTS FOR ORIGINAL POLYNOMIAL,
C ORDERED FROM SMALLEST TO LARGEST POWER
C IDIMX - DIMENSION OF X
C .....
C REMARKS
C NONE
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C .....
C METHOD
C DIMENSION OF Y IS SET AT DIMENSION OF X LESS ONE. DERIVATIVE
C IS THEN CALCULATED BY MULTIPLYING COEFFICIENTS BY THEIR
C RESPECTIVE EXPONENTS.
C .....
C SUBROUTINE PDER(Y, IDIMY, X, IDIMX)
C DIMENSION X(1), Y(1)
C .....
C TEST OF DIMENSION
C IF (IDIMX-1) 3,3,1
C 1 IDIMY=IDIMX-1
C EXPT=0
C DO 2 I=1, IDIMY
C EXPT=EXPT+1
C 2 Y(I)=X(I+1)*EXPT
C GO TO 4
C 3 IDIMY=0
C 4 RETURN
C END
PDER 10
PDER 20
PDER 30
PDER 40
PDER 50
PDER 60
PDER 70
PDER 80
PDER 90
PDER 100
PDER 110
PDER 120
PDER 130
PDER 140
PDER 150
PDER 160
PDER 170
PDER 180
PDER 190
PDER 200
PDER 210
PDER 220
PDER 230
PDER 240
PDER 250
PDER 260
PDER 270
PDER 280
PDER 290
PDER 300
PDER 310
PDER 320
PDER 330
PDER 340
PDER 350
PDER 360
PDER 370
PDER 380
PDER 390
PDER 400
PDER 410
PDER 420
PDER 430
PDER 440
PDER 450
PDER 460

```

Subroutine PINT

```

C ..... PINT 10
C ..... PINT 20
C ..... PINT 30
C ..... PINT 40
C ..... PINT 50
C ..... PINT 60
C ..... PINT 70
C ..... PINT 80
C ..... PINT 90
C ..... PINT 100
C ..... PINT 110
C ..... PINT 120
C ..... PINT 130
C ..... PINT 140
C ..... PINT 150
C ..... PINT 160
C ..... PINT 170
C ..... PINT 180
C ..... PINT 190
C ..... PINT 200
C ..... PINT 210
C ..... PINT 220
C ..... PINT 230
C ..... PINT 240
C ..... PINT 250
C ..... PINT 260
C ..... PINT 270
C ..... PINT 280
C ..... PINT 290
C ..... PINT 300
C ..... PINT 310
C ..... PINT 320
C ..... PINT 330
C ..... PINT 340
C ..... PINT 350
C ..... PINT 360
C ..... PINT 370
C ..... PINT 380
C ..... PINT 390
C ..... PINT 400
C ..... PINT 410
C ..... PINT 420
C ..... PINT 430
C ..... PINT 440
C ..... PINT 450
C ..... PINT 460
C ..... PINT 470
C ..... PINT 480
C ..... PINT 490
C ..... PINT 500
C ..... PINT 510
C ..... PINT 520
C ..... PINT 530
C ..... PINT 540
C ..... PINT 550
C ..... PINT 560
C ..... PINT 570
C ..... PINT 580
C ..... PINT 590
C ..... PINT 600
C ..... PINT 610
C ..... PINT 620
C ..... PINT 630
C ..... PINT 640
C ..... PINT 650
C ..... PINT 660
C ..... PINT 670
C ..... PINT 680
C ..... PINT 690
C ..... PINT 700
C ..... PINT 710
C ..... PINT 720
C ..... PINT 730
C ..... PINT 740
C ..... PINT 750
C ..... PINT 760
C ..... PINT 770
C ..... PINT 780
C ..... PINT 790
C ..... PINT 800
C ..... PINT 810
C ..... PINT 820
C ..... PINT 830
C ..... PINT 840
C ..... PINT 850
C ..... PINT 860
C ..... PINT 870
C ..... PINT 880
C ..... PINT 890
C ..... PINT 900
C ..... PINT 910
C ..... PINT 920
C ..... PINT 930
C ..... PINT 940
C ..... PINT 950
C ..... PINT 960
C ..... PINT 970
C ..... PINT 980
C ..... PINT 990
C ..... PINT 1000

```

Subroutine PQSD

```

C ..... PQSD 10
C ..... PQSD 20
C ..... PQSD 30
C ..... PQSD 40
C ..... PQSD 50
C ..... PQSD 60
C ..... PQSD 70
C ..... PQSD 80
C ..... PQSD 90
C ..... PQSD 100
C ..... PQSD 110
C ..... PQSD 120
C ..... PQSD 130
C ..... PQSD 140
C ..... PQSD 150
C ..... PQSD 160
C ..... PQSD 170
C ..... PQSD 180
C ..... PQSD 190
C ..... PQSD 200
C ..... PQSD 210
C ..... PQSD 220
C ..... PQSD 230
C ..... PQSD 240
C ..... PQSD 250
C ..... PQSD 260
C ..... PQSD 270
C ..... PQSD 280
C ..... PQSD 290
C ..... PQSD 300
C ..... PQSD 310
C ..... PQSD 320
C ..... PQSD 330
C ..... PQSD 340
C ..... PQSD 350
C ..... PQSD 360
C ..... PQSD 370
C ..... PQSD 380
C ..... PQSD 390
C ..... PQSD 400
C ..... PQSD 410
C ..... PQSD 420
C ..... PQSD 430
C ..... PQSD 440
C ..... PQSD 450
C ..... PQSD 460
C ..... PQSD 470
C ..... PQSD 480
C ..... PQSD 490
C ..... PQSD 500
C ..... PQSD 510
C ..... PQSD 520
C ..... PQSD 530
C ..... PQSD 540
C ..... PQSD 550
C ..... PQSD 560
C ..... PQSD 570
C ..... PQSD 580
C ..... PQSD 590
C ..... PQSD 600
C ..... PQSD 610
C ..... PQSD 620
C ..... PQSD 630
C ..... PQSD 640
C ..... PQSD 650
C ..... PQSD 660
C ..... PQSD 670
C ..... PQSD 680
C ..... PQSD 690
C ..... PQSD 700
C ..... PQSD 710
C ..... PQSD 720
C ..... PQSD 730
C ..... PQSD 740
C ..... PQSD 750
C ..... PQSD 760
C ..... PQSD 770
C ..... PQSD 780
C ..... PQSD 790
C ..... PQSD 800
C ..... PQSD 810
C ..... PQSD 820
C ..... PQSD 830
C ..... PQSD 840
C ..... PQSD 850
C ..... PQSD 860
C ..... PQSD 870
C ..... PQSD 880
C ..... PQSD 890
C ..... PQSD 900
C ..... PQSD 910
C ..... PQSD 920
C ..... PQSD 930
C ..... PQSD 940
C ..... PQSD 950
C ..... PQSD 960
C ..... PQSD 970
C ..... PQSD 980
C ..... PQSD 990
C ..... PQSD 1000

```

Subroutine PCLD

```

C ..... PCLD 10
C ..... PCLD 20
C ..... PCLD 30
C ..... PCLD 40
C ..... PCLD 50
C ..... PCLD 60
C ..... PCLD 70
C ..... PCLD 80
C ..... PCLD 90
C ..... PCLD 100
C ..... PCLD 110
C ..... PCLD 120
C ..... PCLD 130
C ..... PCLD 140
C ..... PCLD 150
C ..... PCLD 160
C ..... PCLD 170
C ..... PCLD 180
C ..... PCLD 190
C ..... PCLD 200
C ..... PCLD 210
C ..... PCLD 220
C ..... PCLD 230
C ..... PCLD 240
C ..... PCLD 250
C ..... PCLD 260
C ..... PCLD 270
C ..... PCLD 280
C ..... PCLD 290
C ..... PCLD 300
C ..... PCLD 310
C ..... PCLD 320
C ..... PCLD 330
C ..... PCLD 340
C ..... PCLD 350
C ..... PCLD 360
C ..... PCLD 370
C ..... PCLD 380
C ..... PCLD 390
C ..... PCLD 400
C ..... PCLD 410
C ..... PCLD 420
C ..... PCLD 430
C ..... PCLD 440

SUBROUTINE PCLD
PURPOSE
  SHIFT OF ORIGIN (COMPLETE LINEAR SYNTHETIC DIVISION)
USAGE
  CALL PCLD(X, IDIMX, U)
DESCRIPTION OF PARAMETERS
  X - VECTOR OF COEFFICIENTS, ORDERED FROM SMALLEST TO
      LARGEST POWER. IT IS REPLACED BY VECTOR OF
      TRANSFORMED COEFFICIENTS.
  IDIMX - DIMENSION OF X
  U - SHIFT PARAMETER
REMARKS
  NONE
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
METHOD
  COEFFICIENT VECTOR X(I) OF POLYNOMIAL P(Z) IS TRANSFORMED
  SUCH THAT Q(Z)=P(Z-U) WHERE Q(Z) DENOTES THE POLYNOMIAL
  WITH TRANSFORMED COEFFICIENT VECTOR.
.....
SUBROUTINE PCLD (X, IDIMX, U)
DIMENSION X(1)
K=1
1 J=IDIMX
2 IF (J-K) 4,4,3
3 X(J-1)=X(J-1)+U*X(J)
J=J-1
GO TO 2
4 K=K+1
IF (IDIMX-K) 5,5,1
5 RETURN
END

```

Subroutine PGCD

```

C ..... PGCD 10
C ..... PGCD 20
C ..... PGCD 30
C ..... PGCD 40
C ..... PGCD 50
C ..... PGCD 60
C ..... PGCD 70
C ..... PGCD 80
C ..... PGCD 90
C ..... PGCD 100
C ..... PGCD 110
C ..... PGCD 120
C ..... PGCD 130
C ..... PGCD 140
C ..... PGCD 150
C ..... PGCD 160
C ..... PGCD 170
C ..... PGCD 180
C ..... PGCD 190
C ..... PGCD 200
C ..... PGCD 210
C ..... PGCD 220
C ..... PGCD 230
C ..... PGCD 240
C ..... PGCD 250
C ..... PGCD 260
C ..... PGCD 270
C ..... PGCD 280
C ..... PGCD 290
C ..... PGCD 300
C ..... PGCD 310
C ..... PGCD 320
C ..... PGCD 330
C ..... PGCD 340
C ..... PGCD 350
C ..... PGCD 360
C ..... PGCD 370
C ..... PGCD 380
C ..... PGCD 390
C ..... PGCD 400
C ..... PGCD 410
C ..... PGCD 420
C ..... PGCD 430
C ..... PGCD 440
C ..... PGCD 450
C ..... PGCD 460
C ..... PGCD 470
C ..... PGCD 480
C ..... PGCD 490
C ..... PGCD 500
C ..... PGCD 510
C ..... PGCD 520
C ..... PGCD 530
C ..... PGCD 540
C ..... PGCD 550
C ..... PGCD 560
C ..... PGCD 570
C ..... PGCD 580
C ..... PGCD 590
C ..... PGCD 600
C ..... PGCD 610
C ..... PGCD 620
C ..... PGCD 630
C ..... PGCD 640

SUBROUTINE PGCD
PURPOSE
  DETERMINE GREATEST COMMON DIVISOR OF TWO POLYNOMIALS
USAGE
  CALL PGCD(X, IDIMX, Y, IDIMY, WORK, EPS, IER)
DESCRIPTION OF PARAMETERS
  X - VECTOR OF COEFFICIENTS FOR FIRST POLYNOMIAL,
      ORDERED FROM SMALLEST TO LARGEST POWER
  IDIMX - DIMENSION OF X
  Y - VECTOR OF COEFFICIENTS FOR SECOND POLYNOMIAL,
      ORDERED FROM SMALLEST TO LARGEST POWER,
      THIS IS REPLACED BY GREATEST COMMON DIVISOR
  IDIMY - DIMENSION OF Y
  WORK - WORKING STORAGE ARRAY
  EPS - TOLERANCE VALUE BELOW WHICH COEFFICIENT IS
      ELIMINATED DURING NORMALIZATION
  IER - RESULTANT ERROR CODE WHERE
      IER=0 NO ERROR
      IER=1 X OR Y IS ZERO POLYNOMIAL
REMARKS
  IDIMX MUST BE GREATER THAN IDIMY
  IDIMY=1 ON RETURN MEANS X AND Y ARE PRIME, THE GCD IS A
  CONSTANT. IDIMX IS DESTROYED DURING COMPUTATION.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  PDIV
  PNORM
METHOD
  GREATEST COMMON DIVISOR OF TWO POLYNOMIALS X AND Y IS
  DETERMINED BY MEANS OF EUCLIDEAN ALGORITHM. COEFFICIENT
  VECTORS X AND Y ARE DESTROYED AND GREATEST COMMON
  DIVISOR IS GENERATED IN Y.
.....
SUBROUTINE PGCD(X, IDIMX, Y, IDIMY, WORK, EPS, IER)
DIMENSION X(1), Y(1), WORK(1)
DIMENSION REQUIRED FOR VECTOR NAMED WORK IS IDIMX-IDIMY+1
1 CALL PDIV(WORK, NDIM, X, IDIMX, Y, IDIMY, EPS, IER)
IF (IER) 5, 2, 5
2 IF (IDIMX) 5, 5, 3
C
C INTERCHANGE X AND Y
C
3 DO 4 J=1, IDIMY
  WORK(1)=X(J)
  X(J)=Y(J)
  Y(J)=WORK(1)
4 NDIM=IDIMX
  IDIMX=IDIMY
  IDIMY=NDIM
GO TO 1
5 RETURN
END

```

Subroutine PNORM

```

C ..... PNDR 10
C SUBROUTINE PNORM PNDR 20
C PNDR 30
C SUBROUTINE PNORM PNDR 40
C PNDR 50
C PURPOSE PNDR 60
C NORMALIZE COEFFICIENT VECTOR OF A POLYNOMIAL PNDR 70
C PNDR 80
C USAGE PNDR 90
C CALL PNORM(X, IDIMX, EPS) PNDR 100
C PNDR 110
C DESCRIPTION OF PARAMETERS PNDR 120
C X - VECTOR OF ORIGINAL COEFFICIENTS, ORDERED FROM PNDR 130
C SMALLEST TO LARGEST POWER. IT REMAINS UNCHANGED PNDR 140
C IDIMX - DIMENSION OF X. IT IS REPLACED BY FINAL DIMENSION PNDR 150
C EPS - TOLERANCE BELOW WHICH COEFFICIENT IS ELIMINATED PNDR 160
C PNDR 170
C REMARKS PNDR 180
C IF ALL COEFFICIENTS ARE LESS THAN EPS, RESULT IS A ZERO PNDR 190
C POLYNOMIAL WITH IDIMX=0 BUT VECTOR X REMAINS INTACT PNDR 200
C PNDR 210
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED PNDR 220
C NONE PNDR 230
C PNDR 240
C METHOD PNDR 250
C DIMENSION OF VECTOR X IS REDUCED BY ONE FOR EACH TRAILING PNDR 260
C COEFFICIENT WITH AN ABSOLUTE VALUE LESS THAN OR EQUAL TO EPS PNDR 270
C PNDR 280
C ..... PNDR 290
C SUBROUTINE PNORM(X, IDIMX, EPS) PNDR 300
C DIMENSION X(1) PNDR 310
C PNDR 320
C 1 IF (IDIMX) 4,4,2 PNDR 330
C 2 IF (ABS(X(IDIMX))-EPS) 3,3,4 PNDR 340
C 3 IDIMX=IDIMX-1 PNDR 350
C GO TO 1 PNDR 360
C 4 RETURN PNDR 370
C END PNDR 380
C PNDR 390

```

Subroutines PECN and DPECN

These subroutines perform the economization of a polynomial for symmetric range.

A given polynomial $P(x)$ with coefficient vector $P = (p_1, \dots, p_n)$, representing a function $f(x)$ with a maximum error eps over the range $(-\text{bound}, \text{bound})$

$$\text{-- that is, } \left| f(x) - \sum_{i=1}^n p_i x^{i-1} \right| \leq \text{eps for } |x| \leq$$

bound -- is reduced to a shorter coefficient vector, if possible, representing $f(x)$ over the same range with a maximal error absolutely less than tol by means of telescoping.

The Chebyshev polynomial $T_{n-1}(t)$ has 2^{n-2} as coefficient of t^{n-1} . As a consequence, t^{n-1} may be replaced by $T_{n-1}(t)/2^{n-2}$ plus a polynomial in t of degree $n-2$.

This means that the telescoped polynomial:

$$P_1(x) = \sum_{i=1}^n p_i x^{i-1} - (p_n \cdot \text{bound}^{n-1} / 2^{n-2}) T_{n-1}(x/\text{bound})$$

is of degree $n-2$ representing $f(x)$ over the range $|x| \leq \text{bound}$ with a maximal error err absolutely less than $\text{eps}_1 = \text{eps} + |p_n| \cdot \text{bound}^{n-1} / 2^{n-2}$, since $|T_{n-1}(t)| \leq 1$ for $|t| \leq 1$.

If eps_1 is less than the tolerance tol , the procedure may be repeated with P_1 instead of P , and eps_1 instead of eps .

This iterative scheme results in a polynomial approximation to $f(x)$ which possibly consists of fewer terms and thus may allow the computation of $f(x)$ with less effort than the original approximation $P(x)$.

Naturally, tol should be greater than eps .

For reference see K.A. Brons, Algorithm 38, Telescope 2, CACM vol. 4, 1961, no. 3, pp. 151-152.

```

C          PECN 10
C          ..... PECN 20
C          SUBROUTINE PECN          PECN 30
C          PURPOSE                  PECN 40
C          ECONOMIZE A POLYNOMIAL FOR SYMMETRIC RANGE          PECN 50
C          CALL PECN (P,N,BOUND,EPS,TOL,WORK)          PECN 60
C          USAGE                    PECN 70
C          CALL PECN (P,N,BOUND,EPS,TOL,WORK)          PECN 80
C          DESCRIPTION OF PARAMETERS          PECN 90
C          P - COEFFICIENT VECTOR OF GIVEN POLYNOMIAL          PECN 100
C          ON RETURN P CONTAINS THE ECONOMIZED POLYNOMIAL          PECN 110
C          N - DIMENSION OF COEFFICIENT VECTOR P          PECN 120
C          ON RETURN N CONTAINS DIMENSION OF ECONOMIZED          PECN 130
C          POLYNOMIAL          PECN 140
C          BOUND - RIGHT HAND BOUNDARY OF RANGE          PECN 150
C          EPS - INITIAL ERROR BOUND          PECN 160
C          ON RETURN EPS CONTAINS AN ERROR BOUND FOR THE          PECN 170
C          ECONOMIZED POLYNOMIAL          PECN 180
C          TOL - TOLERANCE FOR ERROR          PECN 190
C          FINAL VALUE OF EPS MUST BE LESS THAN TOL          PECN 200
C          WORK - WORKING STORAGE OF DIMENSION N (STARTING VALUE          PECN 210
C          OF N RATHER THAN FINAL VALUE)          PECN 220
C          REMARKS                    PECN 230
C          THE OPERATION IS BYPASSED IN CASE OF N LESS THAN 1.          PECN 240
C          IN CASE OF AN ARBITRARY INTERVAL (XL,XR) IT IS NECESSARY          PECN 250
C          FIRST TO CALCULATE THE EXPANSION OF THE GIVEN POLYNOMIAL          PECN 260
C          WITH ARGUMENT X IN POWERS OF T = (X-(XR+XL)/2).          PECN 270
C          THIS IS ACCOMPLISHED THROUGH SUBROUTINE PCLO.          PECN 280
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED          PECN 290
C          NONE          PECN 300
C          METHOD                    PECN 310
C          SUBROUTINE PECN TAKES AN (N-1)ST DEGREE POLYNOMIAL          PECN 320
C          APPROXIMATION TO A FUNCTION F(X) VALID WITHIN A TOLERANCE          PECN 330
C          EPS OVER THE INTERVAL (-BOUND,BOUND) AND REDUCES IT IF          PECN 340
C          POSSIBLE TO A POLYNOMIAL OF LOWER DEGREE VALID WITHIN          PECN 350
C          THE GIVEN TOLERANCE TOL.          PECN 360
C          THE INITIAL COEFFICIENT VECTOR P IS REPLACED BY THE FINAL          PECN 370
C          VECTOR. THE INITIAL ERROR BOUND EPS IS REPLACED BY A FINAL          PECN 380
C          ERROR BOUND.          PECN 390
C          N IS REPLACED BY THE DIMENSION OF THE REDUCED POLYNOMIAL.          PECN 400
C          THE COEFFICIENT VECTOR OF THE N-TH CHEBYSHEV POLYNOMIAL          PECN 410
C          IS CALCULATED FROM THE RECURSION FORMULA          PECN 420
C          A(K-1)=-A(K+1)*K*L*L*(K-1)/(1+N*K-2)*(N-K+2))          PECN 430
C          REFERENCE          PECN 440
C          K. A. BRONS, ALGORITHM 38, TELESCOPE 2, CACM VOL. 4, 1961,          PECN 450
C          NO. 3, PP. 151-152.          PECN 460
C          ..... PECN 470
C          SUBROUTINE PECN(P,N,BOUND,EPS,TOL,WORK)          PECN 480
C          DIMENSION P(1),WORK(1)          PECN 490
C          FL=BOUND*BOUND          PECN 500
C          TEST OF DIMENSION          PECN 510
C          1 IF(N-1)2,3,6          PECN 520
C          2 RETURN          PECN 530
C          3 IF(EPS+ABS(P(1))-TOL)4,4,5          PECN 540
C          4 N=0          PECN 550
C          EPS=EPS+ABS(P(1))          PECN 560
C          5 RETURN          PECN 570
C          CALCULATE EXPANSION OF CHEBYSHEV POLYNOMIAL          PECN 580
C          6 NEND=N-2          PECN 590
C          WORK(N)=-P(N)          PECN 600
C          DO 7 J=1,NEND,2          PECN 610
C          K=N-J          PECN 620
C          FN=(NEND-1+K)*(NEND+3-K)          PECN 630
C          FK=K*(K-1)          PECN 640
C          7 WORK(K-1)=-WORK(K+1)*FK*FL/FN          PECN 650
C          TEST FOR FEASIBILITY OF REDUCTION          PECN 660
C          IF(K-2)8,8,9          PECN 670
C          8 FN=ABS(WORK(1))          PECN 680
C          GOTD 10          PECN 690
C          9 FN=N-1          PECN 700
C          FN=ABS(WORK(2)/FN)          PECN 710
C          10 IF(EPS+FN-TOL)11,11,5          PECN 720
C          REDUCE POLYNOMIAL          PECN 730
C          11 EPS=EPS+FN          PECN 740
C          N=N-1          PECN 750
C          DO 12 J=K,N,2          PECN 760
C          12 P(J-1)=P(J-1)+WORK(J-1)          PECN 770
C          GOTD 1          PECN 780
C          END          PECN 790

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C          ..... DPCN 10
C          SUBROUTINE DPECN          DPCN 20
C          PURPOSE                  DPCN 30
C          ECONOMIZE A POLYNOMIAL FOR SYMMETRIC RANGE          DPCN 40
C          CALL DPECN(P,N,BOUND,EPS,TOL,WORK)          DPCN 50
C          USAGE                    DPCN 60
C          CALL DPECN(P,N,BOUND,EPS,TOL,WORK)          DPCN 70
C          DESCRIPTION OF PARAMETERS          DPCN 80
C          P - DOUBLE PRECISION COEFFICIENT VECTOR OF GIVEN          DPCN 90
C          POLYNOMIAL          DPCN 100
C          ON RETURN P CONTAINS THE ECONOMIZED POLYNOMIAL          DPCN 110
C          N - DIMENSION OF COEFFICIENT VECTOR P          DPCN 120
C          ON RETURN N CONTAINS DIMENSION OF ECONOMIZED          DPCN 130
C          POLYNOMIAL          DPCN 140
C          BOUND - SINGLE PRECISION RIGHT HAND BOUNDARY OF RANGE          DPCN 150
C          EPS - SINGLE PRECISION INITIAL ERROR BOUND          DPCN 160
C          ON RETURN EPS CONTAINS AN ERROR BOUND FOR THE          DPCN 170
C          ECONOMIZED POLYNOMIAL          DPCN 180
C          TOL - SINGLE PRECISION TOLERANCE FOR ERROR          DPCN 190
C          FINAL VALUE OF EPS MUST BE LESS THAN TOL          DPCN 200
C          WORK - DOUBLE PRECISION WORKING STORAGE OF DIMENSION N          DPCN 210
C          (STARTING VALUE OF N RATHER THAN FINAL VALUE)          DPCN 220
C          REMARKS                    DPCN 230
C          THE OPERATION IS BYPASSED IN CASE OF N LESS THAN 1.          DPCN 240
C          IN CASE OF AN ARBITRARY INTERVAL (XL,XR) IT IS NECESSARY          DPCN 250
C          FIRST TO CALCULATE THE EXPANSION OF THE GIVEN POLYNOMIAL          DPCN 260
C          WITH ARGUMENT X IN POWERS OF T = (X-(XR+XL)/2).          DPCN 270
C          THIS IS ACCOMPLISHED THROUGH SUBROUTINE DPCLD.          DPCN 280
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED          DPCN 290
C          NONE          DPCN 300
C          METHOD                    DPCN 310
C          SUBROUTINE DPECN TAKES AN (N-1)ST DEGREE POLYNOMIAL          DPCN 320
C          APPROXIMATION TO A FUNCTION F(X) VALID WITHIN A TOLERANCE          DPCN 330
C          EPS OVER THE INTERVAL (-BOUND,BOUND) AND REDUCES IT IF          DPCN 340
C          POSSIBLE TO A POLYNOMIAL OF LOWER DEGREE VALID WITHIN          DPCN 350
C          THE GIVEN TOLERANCE TOL.          DPCN 360
C          THE INITIAL COEFFICIENT VECTOR P IS REPLACED BY THE FINAL          DPCN 370
C          VECTOR. THE INITIAL ERROR BOUND EPS IS REPLACED BY A FINAL          DPCN 380
C          ERROR BOUND.          DPCN 390
C          N IS REPLACED BY THE DIMENSION OF THE REDUCED POLYNOMIAL.          DPCN 400
C          THE COEFFICIENT VECTOR OF THE N-TH CHEBYSHEV POLYNOMIAL          DPCN 410
C          IS CALCULATED FROM THE RECURSION FORMULA          DPCN 420
C          A(K-1)=-A(K+1)*K*L*L*(K-1)/(1+N*K-2)*(N-K+2))          DPCN 430
C          REFERENCE          DPCN 440
C          K. A. BRONS, ALGORITHM 38, TELESCOPE 2, CACM VOL. 4, 1961,          DPCN 450
C          NO. 3, PP. 151-152.          DPCN 460
C          ..... DPCN 470
C          SUBROUTINE DPECN(P,N,BOUND,EPS,TOL,WORK)          DPCN 480
C          DIMENSION P(1),WORK(1)          DPCN 490
C          DOUBLE PRECISION P,WORK          DPCN 500
C          FL=BOUND*BOUND          DPCN 510
C          TEST OF DIMENSION          DPCN 520
C          1 IF(N-1)2,3,6          DPCN 530
C          2 RETURN          DPCN 540
C          3 IF(EPS+ABS(SNGL(P(1)))-TOL)4,4,5          DPCN 550
C          4 N=0          DPCN 560
C          EPS=EPS+ABS(SNGL(P(1)))          DPCN 570
C          5 RETURN          DPCN 580
C          CALCULATE EXPANSION OF CHEBYSHEV POLYNOMIAL          DPCN 590
C          6 NEND=N-2          DPCN 600
C          WORK(N)=-P(N)          DPCN 610
C          DO 7 J=1,NEND,2          DPCN 620
C          K=N-J          DPCN 630
C          FN=(NEND-1+K)*(NEND+3-K)          DPCN 640
C          FK=K*(K-1)          DPCN 650
C          7 WORK(K-1)=-WORK(K+1)*0BLE(FK*FL/FN)          DPCN 660
C          TEST FOR FEASIBILITY OF REDUCTION          DPCN 670
C          IF(K-2)8,8,9          DPCN 680
C          8 FN=DABS(WORK(1))          DPCN 690
C          GOTD 10          DPCN 700
C          9 FN=N-1          DPCN 710
C          FN=ABS(SNGL(WORK(2))/FN)          DPCN 720
C          10 IF(EPS+FN-TOL)11,11,5          DPCN 730
C          REDUCE POLYNOMIAL          DPCN 740
C          11 EPS=EPS+FN          DPCN 750
C          N=N-1          DPCN 760
C          DO 12 J=K,N,2          DPCN 770
C          12 P(J-1)=P(J-1)+WORK(J-1)          DPCN 780
C          GOTD 1          DPCN 790
C          END          DPCN 800

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Subroutines PECS and DPECS

These subroutines perform the economization of a polynomial for unsymmetric range.

A given polynomial $P(x)$ with coefficient vector $P = (p_1, \dots, p_n)$, representing a function $f(x)$ with a maximal error eps over the range $(0, \text{bound})$ --

$$\text{that is, } \left| f(x) - \sum_{i=1}^n p_i x^{i-1} \right| \leq \text{eps for } 0 \leq x \leq \text{bound}$$

-- is reduced to a shorter coefficient vector, if possible, representing $f(x)$ over the same range with a maximal error absolutely less than tol by means of telescoping.

The shifted Chebyshev polynomial $T_{n-1}^S(t) = T_{n-1}(2t-1)$ has 2^{2n-3} as coefficient of t^{n-1} . As a consequence, t^{n-1} may be replaced by $T_{n-1}^S(t)/2^{2n-3}$ plus a polynomial in t of degree $n-2$.

This means that the telescoped polynomial

$$P_1(x) = \sum_{i=1}^n p_i x^{i-1} - (p_n \cdot (\text{bound})^{n-1} / 2^{2n-3}) T_{n-1}^S(x/\text{bound})$$

is of degree $n-2$ representing $f(x)$ over the range $0 \leq x \leq \text{bound}$ with a maximal error err absolutely less than $\text{eps}_1 = \text{eps} + |p_n| \cdot \text{bound}^{n-1} / 2^{2n-3}$, since $|T_{n-1}^S(t)| \leq 1$ for $0 \leq t \leq 1$.

If eps_1 is less than the tolerance tol , the procedure may be repeated with P_1 instead of P , and eps_1 instead of eps .

This iterative scheme results in a polynomial approximation to $f(x)$ which possibly consists of fewer terms and thus may allow the computation of $f(x)$ with less effort than the original approximation $P(x)$.

Naturally, tol should be greater than eps .

For reference see K. A. Brons, Algorithm 37, Telescope 1, CACM vol. 4, 1961, no. 3, p. 151.

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C
C
C ..... PECS 10
C SUBROUTINE PECS PECS 20
C PURPOSE PECS 30
C ECONOMICIZATION OF A POLYNOMIAL FOR UNSYMMETRIC RANGE PECS 40
C PECS 50
C PECS 60
C USAGE PECS 70
C CALL PECS (P,N,BOUND,EPS,TOL,WORK) PECS 80
C PECS 90
C DESCRIPTION OF PARAMETERS PECS 100
C P - COEFFICIENT VECTOR OF GIVEN POLYNOMIAL PECS 110
C N - DIMENSION OF COEFFICIENT VECTOR PECS 120
C BOUND - RIGHT HAND BOUNDARY OF INTERVAL PECS 130
C EPS - INITIAL ERROR BOUND PECS 140
C TOL - TOLERANCE FOR ERROR PECS 150
C WORK - WORKING STORAGE OF DIMENSION N PECS 160
C PECS 170
C PECS 180
C REMARKS PECS 190
C THE INITIAL COEFFICIENT VECTOR P IS REPLACED BY THE PECS 200
C ECONOMICIZED VECTOR. PECS 210
C THE INITIAL ERROR BOUND EPS IS REPLACED BY A FINAL PECS 220
C ERROR BOUND. PECS 230
C N IS REPLACED BY THE DIMENSION OF THE REDUCED POLYNOMIAL. PECS 240
C IN CASE OF AN ARBITRARY INTERVAL (XL,XR) IT IS NECESSARY PECS 250
C FIRST TO CALCULATE THE EXPANSION OF THE GIVEN POLYNOMIAL PECS 260
C WITH ARGUMENT X IN POWERS OF T = (X-XL). PECS 270
C THIS IS ACCOMPLISHED THROUGH SUBROUTINE PCLD. PECS 280
C OPERATION IS BYPASSED IN CASE OF N LESS THAN 1. PECS 290
C PECS 300
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED PECS 310
C NONE PECS 320
C PECS 330
C METHOD PECS 340
C SUBROUTINE PECS TAKES AN (N-1)ST DEGREE POLYNOMIAL PECS 350
C APPROXIMATION TO A FUNCTION F(X) VALID WITHIN A TOLERANCE PECS 360
C EPS OVER THE INTERVAL (0,BOUND) AND REDUCES IT IF POSSIBLE PECS 370
C TO A POLYNOMIAL OF LOWER DEGREE VALID WITHIN TOLERANCE PECS 380
C TOL. PECS 390
C THE COEFFICIENT VECTOR OF THE N-TH SHIFTED CHEBYSHEV PECS 400
C POLYNOMIAL IS CALCULATED FROM THE RECURSION FORMULA PECS 410
C A(K) = -A(K+1)*K*(1+2*K-1)/(2*IN*K-1)*(N-K+1). PECS 420
C REFERENCE PECS 430
C K. A. BRONS, ALGORITHM 37, TELESCOPE 1, CACM VOL. 4, 1961, PECS 440
C NO. 3, PP. 151. PECS 450
C PECS 460
C PECS 470
C ..... PECS 480
C SUBROUTINE PECS(P,N,BOUND,EPS,TOL,WORK) PECS 490
C DIMENSION P(1),WORK(1) PECS 500
C FL=BOUND*0.5 PECS 510
C TEST OF DIMENSION PECS 520
C 1 IF(N-1)2,3,6 PECS 530
C 2 RETURN PECS 540
C 3 IF(EPS+ABS(P(1))-TOL)4,4,5 PECS 550
C 4 N=0 PECS 560
C EPS=EPS+ABS(P(1)) PECS 570
C 5 RETURN PECS 580
C CALCULATE EXPANSION OF CHEBYSHEV POLYNOMIAL PECS 590
C 6 NEND=N-1 PECS 600
C WORK(N)=-P(N) PECS 610
C DO 7 J=1,NEND PECS 620
C K=N-J PECS 630
C FK=(NEND-1+K)*(N-K) PECS 640
C FK=K*(K-1) PECS 650
C 7 WORK(K)=-WORK(K+1)*FK*FL/FN PECS 660
C TEST FOR FEASIBILITY OF REDUCTION PECS 670
C FN=ABS(WORK(1)) PECS 680
C IF(EPS+FN-TOL)8,8,5 PECS 690
C REDUCE POLYNOMIAL PECS 700
C 8 EPS=EPS+FN PECS 710
C N=NEND PECS 720
C DO 9 J=1,NEND PECS 730
C 9 P(J)=P(J)+WORK(J) PECS 740
C GO TO 1 PECS 750
C END PECS 760

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..... DPCS 10
SUBROUTINE DPECS DPCS 20
PURPOSE DPCS 30
ECONOMIZATION OF A POLYNOMIAL FOR UNSYMMETRIC RANGE DPCS 40
USAGE DPCS 50
CALL DPECS(P,N,BOUND,EPS,TOL,WORK) DPCS 60
DESCRIPTION OF PARAMETERS DPCS 70
P - DOUBLE PRECISION COEFFICIENT VECTOR OF GIVEN DPCS 80
POLYNOMIAL DPCS 90
N - DIMENSION OF COEFFICIENT VECTOR P DPCS 100
BOUND - SINGLE PRECISION RIGHT HAND BOUNDARY OF INTERVAL DPCS 110
EPS - SINGLE PRECISION INITIAL ERROR BOUND DPCS 120
TOL - SINGLE PRECISION TOLERANCE FOR ERROR DPCS 130
WORK - DOUBLE PRECISION WORKING STORAGE OF DIMENSION N DPCS 140
REMARKS DPCS 150
THE INITIAL COEFFICIENT VECTOR P IS REPLACED BY THE DPCS 160
ECONOMIZED VECTOR. DPCS 170
THE INITIAL ERROR BOUND EPS IS REPLACED BY A FINAL DPCS 180
ERROR BOUND. DPCS 190
N IS REPLACED BY THE DIMENSION OF THE REDUCED POLYNOMIAL. DPCS 200
IN CASE OF AN ARBITRARY INTERVAL (XL,XR) IT IS NECESSARY DPCS 210
FIRST TO CALCULATE THE EXPANSION OF THE GIVEN POLYNOMIAL DPCS 220
WITH ARGUMENT X IN POWERS OF T = (X-XL). DPCS 230
THIS IS ACCOMPLISHED THROUGH SUBROUTINE DPCLD. DPCS 240
OPERATION IS BYPASSED IN CASE OF N LESS THAN 1. DPCS 250
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DPCS 260
NONE DPCS 270
METHOD DPCS 280
SUBROUTINE DPECS TAKES AN (N-1)ST DEGREE POLYNOMIAL DPCS 290
APPROXIMATION TO A FUNCTION F(X) VALID WITHIN A TOLERANCE DPCS 300
EPS OVER THE INTERVAL (0,BOUND) AND REDUCES IT IF POSSIBLE DPCS 310
TO A POLYNOMIAL OF LOWER DEGREE VALID WITHIN TOLERANCE DPCS 320
TOL. DPCS 330
THE COEFFICIENT VECTOR OF THE N-TH SHIFTED CHEBYSHEV DPCS 340
POLYNOMIAL IS CALCULATED FROM THE RECURSION FORMULA DPCS 350
A(K) = -A(K+1)*K*(2*K-1)/(2*(N+K-1)*(N-K+1)). DPCS 360
REFERENCE DPCS 370
K. A. BRONS, ALGORITHM 37, TELESCOPE 1, CACM VOL. 4, 1961, DPCS 380
NO. 3, PP. 151. DPCS 390
..... DPCS 400
SUBROUTINE DPECS(P,N,BOUND,EPS,TOL,WORK) DPCS 410
DIMENSION P(1),WORK(1) DPCS 420
DOUBLE PRECISION P,WORK DPCS 430
FL=BOUND*0.5 DPCS 440
TEST OF DIMENSION DPCS 450
1 IF(N-1)2,3,6 DPCS 460
2 RETURN DPCS 470
3 IF(EPS+ABS(SNGL(P(1)))-TOL)4,4,5 DPCS 480
4 N=0 DPCS 490
EPS=EPS+ABS(SNGL(P(1))) DPCS 500
5 RETURN DPCS 510
CALCULATE EXPANSION OF CHEBYSHEV POLYNOMIAL DPCS 520
6 NEND=N-1 DPCS 530
WORK(N)=-P(N) DPCS 540
DO 7 J=1,NEND DPCS 550
K=N-J DPCS 560
FN=(NEND-1+K)*(N-K) DPCS 570
FK=K*(K-1) DPCS 580
7 WORK(K)=-WORK(K+1)*DBLE(FK)*DBLE(FL)/DBLE(FN) DPCS 590
TEST FOR FEASIBILITY OF REDUCTION DPCS 600
FN=DABS(WORK(1)) DPCS 610
IF(EPS+FN-TOL)8,8,5 DPCS 620
REDUCE POLYNOMIAL DPCS 630
8 EPS=EPS+FN DPCS 640
N=NEND DPCS 650
DO 9 J=1,NEND DPCS 660
9 P(J)=P(J)+WORK(J) DPCS 670
GOTO 1 DPCS 680
END DPCS 690

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Polynomials: Roots

Subroutine POLRT

This subroutine computes the real and complex roots of a real polynomial.

Given a polynomial

$$f(z) = \sum_{n=0}^N a_n z^n \tag{1}$$

let

$$Z = X + iY \text{ be a starting value for a root of } f(z).$$

Then:

$$Z^n = (X + iY)^n \tag{2}$$

Define X_n as real terms of expanded equation (2).

Define Y_n as imaginary terms of expanded equation (2).

Then for:

$$n = 0$$

$$X_0 = 1.0$$

$$Y_0 = 0.0$$

$$n > 0$$

$$X_n = X \cdot X_{n-1} - Y \cdot Y_{n-1} \tag{3}$$

$$Y_n = X \cdot Y_{n-1} + Y \cdot X_{n-1} \tag{4}$$

Let:

U be the real terms of (1)

V be the imaginary terms of (1)

Then:

$$U = \sum_{n=0}^N a_n X_n \tag{5}$$

$$V = \sum_{n=0}^N a_n Y_n \tag{6}$$

or:

$$U = a_0 + \sum_{n=1}^N a_n X_n \tag{7}$$

$$V = \sum_{n=1}^N a_n Y_n \tag{8}$$

$$\frac{\partial U}{\partial X} = \sum_{n=1}^N n \cdot X_{n-1} \cdot a_n \quad (9)$$

$$\frac{\partial U}{\partial Y} = - \sum_{n=1}^N n Y_{n-1} a_n \quad (10)$$

Note that equations (3), (4), (7), (8), (9), and (10) can be performed iteratively for $n = 1$ to N by saving X_{n-1} and Y_{n-1} .

Using the Newton-Raphson method for computing ΔX , ΔY , the result is:

$$\Delta X = \left(v \frac{\partial U}{\partial Y} - U \frac{\partial U}{\partial X} \right) / \left[\left(\frac{\partial U}{\partial X} \right)^2 + \left(\frac{\partial U}{\partial Y} \right)^2 \right] \quad (11)$$

$$\Delta Y = - \left(U \frac{\partial U}{\partial Y} + v \frac{\partial U}{\partial X} \right) / \left[\left(\frac{\partial U}{\partial X} \right)^2 + \left(\frac{\partial U}{\partial Y} \right)^2 \right] \quad (12)$$

after applying the Cauchy-Riemann equations.

Thus, for the next iteration:

$$X' = X + \Delta X$$

$$Y' = Y + \Delta Y$$

```

C THE DOUBLE PRECISION VERSION MAY BE MODIFIED BY CHANGING THE PLRT 610
C CONSTANT IN STATEMENT 78 TO 1.0D-12 AND IN STATEMENT 122 TO PLRT 620
C 1.0D-10. THIS WILL PROVIDE HIGHER PRECISION RESULTS AT THE PLRT 630
C COST OF EXECUTION TIME. PLRT 640
C ..... PLRT 650
C ..... PLRT 660
C IFIT=0 PLRT 670
C N=M PLRT 680
C IER=0 PLRT 690
C IF(XCOF(N+1))10,25,10 PLRT 700
C 10 IF(N) 15,15,32 PLRT 710
C ..... PLRT 720
C SET ERROR CODE TO 1 PLRT 730
C ..... PLRT 740
C 15 IER=1 PLRT 750
C 20 RETURN PLRT 760
C ..... PLRT 770
C SET ERROR CODE TO 4 PLRT 780
C ..... PLRT 790
C 25 IER=4 PLRT 800
C GO TO 20 PLRT 810
C ..... PLRT 820
C SET ERROR CODE TO 2 PLRT 830
C ..... PLRT 840
C 30 IER=2 PLRT 850
C GO TO 20 PLRT 860
C 32 IF(IN-36) 35,35,30 PLRT 870
C 35 NX=N PLRT 880
C NXX=N+1 PLRT 890
C NZ=1 PLRT 900
C KJ1 = N+1 PLRT 910
C DO 40 L=1,KJ1 PLRT 920
C NT=KJ1-L+1 PLRT 930
C 40 COF(NT)=XCOF(L) PLRT 940
C ..... PLRT 950
C SET INITIAL VALUES PLRT 960
C ..... PLRT 970
C 45 XO=.00500101 PLRT 980
C YO=.01000101 PLRT 990
C ..... PLRT 1000
C ZERO INITIAL VALUE COUNTER PLRT 1010
C ..... PLRT 1020
C IN=0 PLRT 1030
C 50 X=XO PLRT 1040
C ..... PLRT 1050
C INCREMENT INITIAL VALUES AND COUNTER PLRT 1060
C ..... PLRT 1070
C XO=-10.0*YO PLRT 1080
C YO=-10.0*X PLRT 1090
C ..... PLRT 1100
C SET X AND Y TO CURRENT VALUE PLRT 1110
C ..... PLRT 1120
C X=XO PLRT 1130
C Y=YO PLRT 1140
C IN=IN+1 PLRT 1150
C GO TO 59 PLRT 1160
C 55 IFIT=1 PLRT 1170
C XPR=X PLRT 1180
C YPR=Y PLRT 1190
C ..... PLRT 1200
C EVALUATE POLYNOMIAL AND DERIVATIVES PLRT 1210
C ..... PLRT 1220
C 59 ICT=0 PLRT 1230
C 60 UX=0.0 PLRT 1240
C UY=0.0 PLRT 1250
C V=0.0 PLRT 1260
C VT=0.0 PLRT 1270
C XT=1.0 PLRT 1280
C U=COF(N+1) PLRT 1290
C IF(U) 65,130,65 PLRT 1300
C 65 DO 70 I=1,N PLRT 1310
C L =N-I+1 PLRT 1320
C TEMP=COF(L) PLRT 1330
C XT2=X*XT-Y*YT PLRT 1340
C YT2=X*YT+Y*XT PLRT 1350
C U=U+TEMP*XT2 PLRT 1360
C V=V+TEMP*YT2 PLRT 1370
C FI=I PLRT 1380
C UX=UX+FI*XT*TEMP PLRT 1390
C UY=UY-FI*YT*TEMP PLRT 1400
C XT=XT2 PLRT 1410
C 70 YT=YT2 PLRT 1420
C SUMSQ=UX*UX+UY*UY PLRT 1430
C IF(SUMSQ) 75,110,75 PLRT 1440
C 75 DX=(V*UY-U*VX)/SUMSQ PLRT 1450
C X=X+DX PLRT 1460
C DY=- (U*UY+V*UX)/SUMSQ PLRT 1470
C Y=Y+DY PLRT 1480
C ..... PLRT 1490
C 78 IF(DABS(DY)+DABS(DX)-1.0D-05) 100,80,80 PLRT 1500
C ..... PLRT 1510
C STEP ITERATION COUNTER PLRT 1520
C ..... PLRT 1530
C 80 ICT=ICT+1 PLRT 1540
C IF(ICT-500) 60,85,85 PLRT 1550
C 85 IF(ICT)100,90,100 PLRT 1560
C 90 IF(IN-5) 50,95,95 PLRT 1570
C ..... PLRT 1580
C SET ERROR CODE TO 3 PLRT 1590
C ..... PLRT 1600
C 95 IER=3 PLRT 1610
C GO TO 20 PLRT 1620
C 100 DO 105 L=1,NXX PLRT 1630
C NT=KJ1-L+1 PLRT 1640
C TEMP=XCOF(NT) PLRT 1650
C XCOF(NT)=COF(L) PLRT 1660
C 105 COF(L)=TEMP PLRT 1670
C ITEMP=N PLRT 1680
C N=N+1 PLRT 1690
C NX=ITEMP PLRT 1700
C IF(IFIT) 120,55,120 PLRT 1710
C 110 IF(IFIT) 115,50,115 PLRT 1720
C ..... PLRT 1730
C 115 X=XPR PLRT 1740
C Y=YPR PLRT 1750
C 120 IFIT=0 PLRT 1760
C 122 IF(DABS(Y)-1.0D-4*DABS(X)) 135,125,125 PLRT 1770
C 125 ALPHA=X*X PLRT 1780
C SUMSQ=X*X+Y*Y PLRT 1790
C N=N-2 PLRT 1800
C GO TO 140 PLRT 1810
C 130 X=0.0 PLRT 1820
C NX=NX-1 PLRT 1830
C NXX=NXX-1 PLRT 1840
C 135 Y=0.0 PLRT 1850
C SUMSQ=0.0 PLRT 1860
C ALPHA=X PLRT 1870
C N=N-1 PLRT 1880
C 140 COF(2)=COF(2)+ALPHA*COF(L) PLRT 1890

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C ..... PLRT 10
C ..... PLRT 20
C ..... PLRT 30
C SUBROUTINE POLRT PLRT 40
C ..... PLRT 50
C PURPOSE PLRT 60
C COMPUTES THE REAL AND COMPLEX ROOTS OF A REAL POLYNOMIAL PLRT 70
C ..... PLRT 80
C USAGE PLRT 90
C CALL POLRT(XCOF,COF,M,ROOTR,ROOTI,IER) PLRT 100
C ..... PLRT 110
C DESCRIPTION OF PARAMETERS PLRT 120
C XCOF--VECTOR OF M+1 COEFFICIENTS OF THE POLYNOMIAL PLRT 130
C ORDERED FROM SMALLEST TO LARGEST POWER PLRT 140
C COF --WORKING VECTOR OF LENGTH M+1 PLRT 150
C M --ORDER OF POLYNOMIAL PLRT 160
C ROOTR--RESULTANT VECTOR OF LENGTH M CONTAINING REAL ROOTS PLRT 170
C OF THE POLYNOMIAL PLRT 180
C ROOTI--RESULTANT VECTOR OF LENGTH M CONTAINING THE PLRT 190
C CORRESPONDING IMAGINARY ROOTS OF THE POLYNOMIAL PLRT 200
C IER --ERROR CODE WHERE PLRT 210
C IER=0 NO ERROR PLRT 220
C IER=1 M LESS THAN ONE PLRT 230
C IER=2 M GREATER THAN 36 PLRT 240
C IER=3 UNABLE TO DETERMINE ROOT WITH 500 ITERATIONS PLRT 250
C ON 5 STARTING VALUES PLRT 260
C IER=4 HIGH ORDER COEFFICIENT IS ZERO PLRT 270
C ..... PLRT 280
C REMARKS PLRT 290
C LIMITED TO 36TH ORDER POLYNOMIAL OR LESS. PLRT 300
C FLOATING POINT OVERFLOW MAY OCCUR FOR HIGH ORDER PLRT 310
C POLYNOMIALS BUT WILL NOT AFFECT THE ACCURACY OF THE RESULTS. PLRT 320
C ..... PLRT 330
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED PLRT 340
C NONE PLRT 350
C ..... PLRT 360
C METHOD PLRT 370
C NEWTON-RAPHSON ITERATIVE TECHNIQUE. THE FINAL ITERATIONS PLRT 380
C ON EACH ROOT ARE PERFORMED USING THE ORIGINAL POLYNOMIAL PLRT 390
C RATHER THAN THE REDUCED POLYNOMIAL TO AVOID ACCUMULATED PLRT 400
C ERRORS IN THE REDUCED POLYNOMIAL. PLRT 410
C ..... PLRT 420
C ..... PLRT 430
C ..... PLRT 440
C ..... PLRT 450
C SUBROUTINE POLRT(XCOF,COF,M,ROOTR,ROOTI,IER) PLRT 460
C DIMENSION XCOF(L1),COF(L1),ROOTR(L1),ROOTI(L1) PLRT 470
C DOUBLE PRECISION XO,YO,X,Y,XPR,YPR,UX,UY,V,YT,XT,U,XT2,YT2,SUMSQ, PLRT 480
C I DX,DY,TEMP,ALPHA PLRT 490
C ..... PLRT 500
C ..... PLRT 510
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE PLRT 520
C C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION PLRT 530
C STATEMENT WHICH FOLLOWS. PLRT 540
C ..... PLRT 550
C DOUBLE PRECISION XCOF,COF,ROOTR,ROOTI PLRT 560
C ..... PLRT 570
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS PLRT 580
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS PLRT 590
C ROUTINE. PLRT 600

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```

145 DO 150 L=2,N
150 CDF(L+1)=CDF(L+1)+ALPHA*CDF(L)-SUMSQ*CDF(L-1)
155 ROOTI(NZ)=Y
      ROOTR(NZ)=X
      N2=N2+1
      IF(SUMSQ) 160,165,160
160 Y=-Y
      SUMSQ=0.0
      GO TO 155
165 IF(N) 20,20,45
      END

```

```

PLRT1890
PLRT1900
PLRT1910
PLRT1920
PLRT1930
PLRT1940
PLRT1950
PLRT1960
PLRT1970
PLRT1980
PLRT1990

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Subroutines PRQD and DPRQD

These subroutines find the roots of a real polynomial by means of the QD-algorithm with displacement. The progressive QD-algorithm is a fast device for calculation of all roots of a polynomial $P(x)$ with real coefficients when there are no approximations to the roots available.

The roots of $P(x) = 0$ are determined by solving for the poles of $Q(x)/P(x)$ where $Q(x)$ is some polynomial of smaller degree than $P(x)$. In the following, n is used as the symbol for the degree of $P(x)$. Using the derivative $P'(x)$ for $Q(x)$ has the advantage that the poles are simple even in case of multiple roots of $P(x)$.

Start of the QD-algorithm requires the continued S-fraction:

$$\frac{c}{x-q_1} \cfrac{1}{1-e_1} \cfrac{1}{x-q_2} \cfrac{1}{1-\dots} \cfrac{1}{q_n} \text{ of } P'(x)/P(x)$$

This calculation is performed using the Euclidean algorithm. By means of normalization such that the highest coefficient is 1, $Q_0(x)$ is obtained from $P(x)$, and $P_1(x)$ from $P'(x)$. Then e_k and q_k are calculated from the iteration scheme:

$$q_k Q_k(x) = x \cdot P_k(x) - Q_{k-1}(x), \quad k = 1, 2, \dots, n \quad (1)$$

$$e_k P_{k+1}(x) = Q_k(x) - P_k(x), \quad k = 1, 2, \dots, n-1 \quad (2)$$

using the fact that all elements $Q_i(x)$ and $P_i(x)$ are normalized by definition.

The following example is an illustration for this iteration scheme:

$$P(x) = 1 + 3x + 3x^2 + x^3, \quad n = 3$$

$$Q_0(x) = x^3 + 3x^2 + 3x + 1$$

$$P_1(x) = x^2 + 2x + 1, \quad q_1 Q_1(x) = -x^2 - 2x - 1, \quad q_1 = -1$$

$$Q_1(x) = x^2 + 2x + 1, \quad e_1 P_2(x) = 0, \quad e_1 = 0$$

where $Q_1(x)$ is a common divisor of $P'(x)/P(x)$ and $q_1 = -1$ is the value of the real root which factors out first.

The above iteration scheme breaks down if some intermediate value of q_i with $0 < i < n$ is equal or approximately equal to zero. In this case an error code is set to 4, which indicates that no S-fraction exists for $P'(x)/P(x)$.

If Q_0 and P_1 have a common divisor of degree j , this common divisor is obtained as Q_{n-j} , and necessarily $e_{n-j} P_{n-j+1} = 0$.

Due to roundoff errors, all coefficients of $e_{n-j} P_{n-j+1}$ cannot be expected to vanish exactly; therefore, allowance is made for coefficients of small absolute value.

If the highest coefficient of $e_{n-j} P_{n-j+1}$ is small in absolute value but some lower coefficient is not, the error code is set to 4, and the subroutine is abandoned.

The coefficients e_k, q_k obtained by the Euclidean algorithm form the first row of the QD-array indicated by superscript 0.

e_0	q_1	e_1	q_2	e_2	\dots	q_m	e_m
0	$q_1^{(0)}$	$e_1^{(0)}$	$q_2^{(0)}$	$e_2^{(0)}$	\dots	$q_m^{(0)}$	$e_m^{(0)}$
0	$q_1^{(1)}$	$e_1^{(1)}$	$q_2^{(1)}$	$e_2^{(1)}$	\dots	$q_m^{(1)}$	$e_m^{(1)}$
.....

Normally m is equal to n but it may be smaller if a common factor exists.

The following rows are obtained by means of the relationships:

$$q_i^{(v+1)} = q_i^{(v)} + e_i^{(v)} - e_{i-1}^{(v+1)}, \quad i = 1, \dots, m \quad (3)$$

$$e_i^{(v+1)} = \frac{e_i^{(v)} \cdot q_{i+1}^{(v)}}{q_i^{(v+1)}}, \quad i = 1, \dots, m-1 \quad (4)$$

together with $e_0^{(v)} = e_m^{(v)} = 0$.

Let x_i denote the roots of $P(x)$ ordered in decreasing absolute value. If $P(x)$ has only roots of different absolute value, there is convergence of the q_k -column to the value x_k . Complex roots are indicated by oscillation of certain q -values.

If x_k and x_{k+1} are of equal absolute value, then the roots of

$$x^2 - (q_k^{(v+1)} + q_{k+1}^{(v)})x + q_k^{(v)} q_{k+1}^{(v)} = 0 \quad (5)$$

converge to x_k and x_{k+1} . The same reasoning applies if the relation $|x_k| = |x_{k+1}|$ holds only approximately.

The QD-algorithm in the form (3), (4) suffers from the fact that convergence is rather slow. By means of displacement of the origin a form is obtained which is asymptotically of quadratic convergence.

The strategy is as follows. Start with displacement $t = 0$.

- I. As soon as convergence is indicated to a real root -- that is, $e_{m-1}^{(v)}$ is sufficiently small (internal test value 0.01) -- perform a displacement by the amount $q_m^{(v)}$.

Starting with $q_k^{(v)}, e_k^{(v)}$, use instead of (3), (4) the iteration scheme:

$$t = t + q_m^{(v)} \quad (6)$$

$$q_k^{(v+1)} = q_k^{(v)} + e_k^{(v)} - e_{k-1}^{(v+1)} - q_m^{(v)}, \quad k = 1, 2, \dots, m \quad (7)$$

$$e_k^{(v+1)} = q_{k+1}^{(v)} \cdot e_k^{(v)} / q_k^{(v+1)}, \quad k = 1, 2, \dots, m-1 \quad (8)$$

Values $e_0^{(v+1)}$ and $e_m^{(v)}$ are thereby set equal to zero.

- II. If convergence is indicated to a root pair -- that is, $e_{m-2}^{(v)}$ is less than $e_{m-1}^{(v)}$ and sufficiently small (internal test value 0.01) -- calculate the discriminant of the quadratic equation (5):

$$D = p * p - q_m^{(v)} * q_{m-1}^{(v)}$$

with

$$P = 0.5 (q_{m-1}^{(v)} + e_{m-1}^{(v)} + q_m^{(v)})$$

If D is positive, provide for a real displacement of amount $P - \sqrt{D}$ or $P + \sqrt{D}$, whichever has the smaller absolute value, and proceed according to (7), (8).

If D is negative, three complex displacements are applied in sequence: the first by amount $P + i\sqrt{|D|}$, the second by $-2i\sqrt{|D|}$, and the third by $V + i\sqrt{|D|}$, resulting in a total real displacement of amount P .

Instead of (6), (7), (8) the following iteration scheme is then obtained. Starting with:

$$t = t + P \quad (9)$$

$$q_1^* = q_1^{(v)} + e_1^{(v)} - P \quad (10)$$

$$P_1 = -D/q_1^{*2} \quad (11)$$

$$e_1^* = e_1^{(v)} q_2^{(v)} / \left[q_1^* (1 + p_1) \right] \quad (12)$$

$$q_1^{**} = q_1^* + e_1^* \quad (13)$$

calculate for $k = 2, 3, \dots, m$:

$$q_k^* = q_k^{(v)} + e_k^{(v)} - e_{k-1}^* - P \quad (14)$$

$$e_{k-1}^{**} = e_{k-1}^* q_k^* / q_{k-1}^{**} \quad (15)$$

$$p_k = p_{k-1} (q_{k-1}^{**} / q_k^*)^2 \quad (16)$$

$$q_{k-1}^{(v+3)} = q_{k-1}^{**} + e_{k-1}^{**} - e_{k-2}^{(v+3)} \quad (17)$$

$$e_k^* = q_{k+1}^{(v)} e_k^{(v)} / \left[q_k^* (1 + p_k) \right] \quad (18)$$

$$q_k^{**} = q_k^* + e_k^* - e_{k-1}^{**} \quad (19)$$

$$e_{k-1}^{(v+3)} = (e_{k-1}^{**} q_k^{**} / q_{k-1}^{(v+3)}) (1 + p_k) \quad (20)$$

Finally set:

$$q_m^{(v+3)} = q_m^{**} - e_{m-1}^{(v+3)} \quad (21)$$

Values $e_0^{(v+3)}$, $e_m^{(v)}$ and $q_{m+1}^{(v)}$ are thereby set equal to zero.

III. If none of the values $e_{m-1}^{(v)}$ and $e_{m-2}^{(v)}$ is sufficiently small, the relationship (3), (4) is used with no displacement at all.

Regarding termination of the iterative scheme given by I., II., III. there are two possibilities:

1. If $e_{m-1}^{(v)}$ is negligible (internal test value is 10^{-6} in single precision and 10^{-16} in double precision), a real root is factored out.

2. If $e_{m-2}^{(v)}$ is negligible (with the same internal test values), a pair of roots is factored out.

A maximum of ten times the number of coefficients using I., II. or III. is allowed. At every iteration step for one and the same root or root pair, the internal test value for convergence and the internal test value for acceptance of a displacement are increased by ten percent.

In case of convergence:

1. For a real root --

real part of root = $t + q_m$
complex part of root = 0

2. For a real root pair (characterized by $D > 0$) --

real part of first root = $t + P + \sqrt{D}$
complex part of first root = 0
real part of second root = $t + P - \sqrt{D}$
complex part of second root = 0

3. For a complex root pair (characterized by $D < 0$) --

real part of first root = $t + P$
complex part of first root = $\sqrt{-D}$
real part of second root = $t + P$
complex part of second root = $-\sqrt{-D}$

As soon as a root or root pair has been factored out, m is reduced by 1 or 2 respectively and the whole procedure I., II., III. is repeated with original values of internal test values, until $m = 0$ -- that is, all roots have been calculated -- or $m = 1$, when the last real root is factored immediately. If $P'(x)$, $P(x)$ have a common divisor, the whole process is repeated for this common divisor. Thus, the complete factorization of the original polynomial $P(x)$ is obtained.

Some remarks are in order:

1. The QD-algorithm is a nonlinear relationship and therefore sensitive to roundoff errors. Small intermediate q -values cause loss of accuracy. Therefore, all divisors are checked before division is actually performed. If a divisor is small in

absolute value due to loss of significant digits, the error parameter is set to 3 indicating possible instability of calculation, and further calculation is bypassed.

2. If a maximum of 10 * n iteration steps is insufficient for calculation of all roots, the error parameter is set to 1, indicating poor convergence. Further calculation is bypassed again.

3. If the original polynomial has a degree less than one, the error parameter is set to 2 indicating that no root exists.

4. If, in case of a complex displacement, q_m^{**} or q_m^* gets very small due to loss of significant digits, and the calculated $e^{(v+3)}_{m-2}$ is less than the internal test value TOL, a pair of roots is calculated from the quadratic equation:

$$x^2 - x \cdot (q_{n-1}^{**} + q_n^* - e_{n-2}^{(v+3)}) + (q_{n-1}^{**} - e_{n-1}^*)$$

$$\left[q_n^* - e_{n-1}^* p_{n-1} - q_n^* \frac{e_{n-2}^{**}}{(v+3)} (1 + p_{n-1}^*) \right] \quad (22)$$

which is easily obtained from (5).

5. A final test of accuracy is made after calculation of all roots of the given polynomial. The calculated roots are used for calculation of the corresponding coefficient vector. If this calculated coefficient vector has less than a specified number of correct digits (the maximal relative error must be less than TOL), the error parameter is set to -1 indicating that calculation of all roots was successful only with poor accuracy of results.

C	PRQD 10
C	PRQD 20
C	PRQD 30
C	PRQD 40
C	PRQD 50
C	PRQD 60
C	PRQD 70
C	PRQD 80
C	PRQD 90
C	PRQD 100
C	PRQD 110
C	PRQD 120
C	PRQD 130
C	PRQD 140
C	PRQD 150
C	PRQD 160
C	PRQD 170
C	PRQD 180
C	PRQD 190
C	PRQD 200
C	PRQD 210
C	PRQD 220
C	PRQD 230
C	PRQD 240
C	PRQD 250
C	PRQD 260
C	PRQD 270
C	PRQD 280
C	PRQD 290
C	PRQD 300
C	PRQD 310
C	PRQD 320
C	PRQD 330
C	PRQD 340
C	PRQD 350
C	PRQD 360
C	PRQD 370
C	PRQD 380
C	PRQD 390
C	PRQD 400

REMARKS
 THE REAL PART OF THE ROOTS IS STORED IN Q(I) UP TO Q(IR)
 CORRESPONDING COMPLEX PARTS ARE STORED IN E(I) UP TO E(IR).
 IER = 0 MEANS NO ERRORS
 IER = 1 MEANS NO CONVERGENCE WITH FEASIBLE TOLERANCE
 IER = 2 MEANS POLYNOMIAL IS DEGENERATE (CONSTANT OR ZERO)
 IER = 3 MEANS SUBROUTINE WAS ABANDONED DUE TO ZERO DIVISOR
 IER = 4 MEANS THERE EXISTS NO S-FRACTION

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IER --1 MEANS CALCULATED COEFFICIENT VECTOR REVEALS POOR ACCURACY OF THE CALCULATED ROOTS.
THE CALCULATED COEFFICIENT VECTOR HAS LESS THAN 3 CORRECT DIGITS.
THE FINAL COMPARISON BETWEEN GIVEN AND CALCULATED COEFFICIENT VECTOR IS PERFORMED ONLY IF ALL ROOTS HAVE BEEN CALCULATED.
THE MAXIMAL RELATIVE ERROR OF THE COEFFICIENT VECTOR IS RECORDED IN Q(IR+1).

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE

METHOD
THE ROOTS OF THE POLYNOMIAL ARE CALCULATED BY MEANS OF THE QUOTIENT-DIFFERENCE ALGORITHM WITH DISPLACEMENT.
REFERENCE
H.RUTISHAUSER, DER QUOTIENTEN-DIFFERENZ-ALGORITHMUS, BIRKHAUSER, BASEL/STUTTGART, 1957.

.....
SUBROUTINE PRQD(C,IC,Q,E,POL,IR,IER)
DIMENSIONED DUMMY VARIABLES
DIMENSION E(1),Q(1),C(1),POL(1)

NORMALIZATION OF GIVEN POLYNOMIAL
TEST OF DIMENSION
IR CONTAINS INDEX OF HIGHEST COEFFICIENT
IER=0
IR=IC
EPS=1.E-6
TOL=1.E-3
LIMIT=10*IC
KOUNT=0
1 IF(IR-1)79,79,2

DROP TRAILING ZERO COEFFICIENTS
2 IF(C(IR))4,3,4
3 IR=IR-1
GOTO 1

REARRANGEMENT OF GIVEN POLYNOMIAL
EXTRACTION OF ZERO ROOTS
4 O=1./C(IR)
IEND=IR-1
ISTA=1
NSAV=IR+1
JBEG=1

Q(J)=1.
Q(J+1)=C(IR-1)/C(IR)
Q(IR)=C(J)/C(IR)
WHERE J IS THE INDEX OF THE LOWEST NONZERO COEFFICIENT
DO 9 I=1,IR
J=NSAV-1
IF(C(I))7,5,7
5 GOTO(6,8),JBEG
6 NSAV=NSAV+1
Q(ISTA)=0.
E(ISTA)=0.
ISTA=ISTA+1
GOTO 9
7 JBEG=2
8 Q(J)=C(I)*O
C(I)=Q(J)
9 CONTINUE

INITIALIZATION
ESAV=0.
Q(ISTA)=0.
10 NSAV=IR

COMPUTATION OF DERIVATIVE
EXPT=IR-ISTA
E(ISTA)=EXPT
DO 11 I=ISTA,IEND
EXPT=EXPT-1.0
POL(I+1)=EPS*ABS(Q(I+1))+EPS
11 E(I+1)=Q(I+1)*EXPT

TEST OF REMAINING DIMENSION
IF(ISTA-IEND)12,20,60
12 IEND=IEND-1

COMPUTATION OF S-FRACTION
DO 19 I=ISTA,IEND
IF(I-ISTA)13,16,13
13 IF(ABS(E(I))-POL(I+1))14,14,16

THE GIVEN POLYNOMIAL HAS MULTIPLE ROOTS, THE COEFFICIENTS OF THE COMMON FACTOR ARE STORED FROM Q(NSAV) UP TO Q(IR)
14 NSAV=I
DO 15 K=I,IEND
IF(ABS(E(K))-POL(K+1))15,15,80
15 CONTINUE
GOTO 21

EUCLIDEAN ALGORITHM
16 DO 19 K=I,IEND
E(K+1)=E(K)/E(I)
Q(K+1)=E(K+1)-Q(K+1)
IF(K-1)18,17,18

TEST FOR SMALL DIVISOR
17 IF(ABS(Q(I+1))-POL(I+1))80,80,19
18 Q(K+1)=Q(K+1)/Q(I+1)
POL(K+1)=POL(K+1)/ABS(Q(I+1))
E(K)=Q(K+1)-E(K)
19 CONTINUE
20 Q(IR)=Q(IR)

PRQD(10)

THE DISPLACEMENT EXPT IS SET TO 0 AUTOMATICALLY.
E(ISTA)=0.,Q(ISTA+1),...,E(NSAV-1),Q(NSAV),E(NSAV)=0.
FORM A DIAGONAL OF THE QO-ARRAY.
INITIALIZATION OF BOUNDARY VALUES
21 E(ISTA)=0.
NRAN=NSAV-1
22 E(NRAN+1)=0.

TEST FOR LINEAR OR CONSTANT FACTOR
NRAN-ISTA IS DEGREE-1
IF(NRAN-ISTA)24,23,31

LINEAR FACTOR
23 Q(ISTA+1)=Q(ISTA+1)+EXPT
E(ISTA+1)=0.
  
```

```

C TEST FOR UNFACTORED COMMON DIVISOR
24 E(ISTA)=ESAV
IF(IR-NSAV)60,60,25
C
C INITIALIZE QD-ALGORITHM FOR COMMON DIVISOR
25 ISTA=NSAV
ESAV=E(ISTA)
GOTO 10
C
C COMPUTATION OF ROOT PAIR
26 P=P*EXPT
C
C TEST FOR REALITY
IF(O)27,28,28
C
C COMPLEX ROOT PAIR
27 Q(NRAN)=P
Q(NRAN+1)=P
E(NRAN)=T
E(NRAN+1)=-T
GOTO 29
C
C REAL ROOT PAIR
28 Q(NRAN)=T
Q(NRAN+1)=P+T
E(NRAN)=0.
C
C REDUCTION OF DEGREE BY 2 (DEFLATION)
29 NRAN=NRAN-2
GOTO 22
C
C COMPUTATION OF REAL ROOT
30 Q(NRAN+1)=EXPT+P
C
C REDUCTION OF DEGREE BY 1 (DEFLATION)
NRAN=NRAN-1
GOTO 22
C
C START QD-ITERATION
31 JBEG=ISTA+1
JEND=NRAN-1
TEPS=EPS
TOELT=1.E-2
32 KOUNT=KOUNT+1
P=Q(NRAN+1)
R=ABS(E(NRAN))
C
C TEST FOR CONVERGENCE
IF(R-TEPS)30,30,33
33 S=ABS(E(JEND))
C
C IS THERE A REAL ROOT NEXT
IF(S-R)36,38,34
C
C IS DISPLACEMENT SMALL ENOUGH
34 IF(R-TOELT)36,35,35
35 P=0.
36 D=P
DO 37 J=JBEG,NRAN
Q(J)=Q(J)+E(J)-E(J-1)-D
C
C TEST FOR SMALL DIVISOR
IF(ABS(Q(J))-POL(J))81,81,37
37 E(J)=Q(J)+E(J)-E(J-1)/Q(J)
Q(NRAN+1)=-E(NRAN)+Q(NRAN+1)-D
GOTO 54
C
C CALCULATE DISPLACEMENT FOR DOUBLE ROOTS
QUADRATIC EQUATION FOR DOUBLE ROOTS
X**2-(Q(NRAN)+Q(NRAN+1)+E(NRAN))*X+Q(NRAN)*Q(NRAN+1)=0
38 P=0.5*(Q(NRAN)+E(NRAN)+Q(NRAN+1))
D=P*P-Q(NRAN)*Q(NRAN+1)
T=SQRT(ABS(D))
C
C TEST FOR CONVERGENCE
IF(S-TEPS)26,26,39
C
C ARE THERE COMPLEX ROOTS
39 IF(O)43,40,40
40 IF(P)42,41,41
41 T=-T
42 P=P+T
R=S
GOTO 34
C
C MODIFICATION FOR COMPLEX ROOTS
IS DISPLACEMENT SMALL ENOUGH
43 IF(S-TOELT)44,35,35
C
C INITIALIZATION
44 D=Q(JBEG)+E(JBEG)-P
C
C TEST FOR SMALL DIVISOR
IF(ABS(D)-POL(JBEG))81,81,45
45 T=T/D**2
U=E(JBEG)+Q(JBEG+1)/(O*(1.+T))
V=D*U
KOUNT=KOUNT+2
C
C THREEFOLD LOOP FOR COMPLEX DISPLACEMENT
DO 53 J=JBEG,NRAN
D=Q(J+1)+E(J+1)-U-P
C
C TEST FOR SMALL DIVISOR
IF(ABS(V)-POL(J))46,46,49
46 IF(J-NRAN)81,47,81
47 EXPT=EXPT+P
IF(ABS(E(JEND))-TOL)48,48,81
48 P=0.5*(V+D-E(JEND))
D=P*P-(V+D)*D-U*(1.+T)/Q(JEND)
T=SQRT(ABS(D))
GOTO 26
C
C TEST FOR SMALL DIVISOR
49 IF(ABS(O)-POL(J+1))46,46,50
50 W=U*V
T=T*W/O**2
Q(J)=V+W-E(J-1)
U=0.
IF(J-NRAN)51,52,52
51 U=Q(J+2)*E(J+1)/(O*(1.+T))
52 V=D+U-W
C
C TEST FOR SMALL DIVISOR
IF(ABS(Q(J))-POL(J))81,81,53
53 E(J)=W*V*(1.+T)/Q(J)
Q(NRAN+1)=V-E(NRAN)
54 EXPT=EXPT+P
TEPS=TEPS*1.1

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PRQ01690
PRQ01700
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PRQ01720
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PRQ01990
PRQ02000
PRQ02010
PRQ02020
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PRQ02870
PRQ02880
PRQ02890
PRQ02900
PRQ02910
PRQ02920
PRQ02930
PRQ02940
PRQ02950
PRQ02960
PRQ02970

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TOELT=TOELT*1.1
IF(KOUNT-LIMIT)32,55,55
C
C NO CONVERGENCE WITH FEASIBLE TOLERANCE
C
C ERROR RETURN IN CASE OF UNSATISFACTORY CONVERGENCE
55 IER=1
C
C REARRANGE CALCULATED ROOTS
56 IEND=NSAV-NRAN-1
E(ISTA)=ESAV
IF(IEND)59,59,57
57 DO 58 I=1,IEND
J=ISTA+I
K=NRAN+1+I
E(J)=E(K)
58 Q(J)=Q(K)
59 IR=ISTA+IEND
C
C NORMAL RETURN
60 IR=IR-1
IF(IR)78,78,61
C
C REARRANGE CALCULATED ROOTS
61 DO 62 I=1,IR
Q(I)=Q(I+1)
62 E(I)=E(I+1)
C
C CALCULATE COEFFICIENT VECTOR FROM ROOTS
POL(IR+1)=1.
IEND=IR-1
JBEG=1
DO 69 J=1,IR
ISTA=IR+1-J
O=0.
P=Q(ISTA)
T=E(ISTA)
IF(T)65,63,65
C
C MULTIPLY WITH LINEAR FACTOR
63 DO 64 I=ISTA,IR
POL(I)=O-P*POL(I+1)
64 O=POL(I+1)
GOTO 69
65 GOTO(66,67),JBEG
66 JBEG=2
POL(ISTA)=0.
GOTO 69
C
C MULTIPLY WITH QUADRATIC FACTOR
67 JBEG=1
U=P*P+T
P=P+P
DO 68 I=ISTA,IEND
POL(I)=O-P*POL(I+1)+U*POL(I+2)
68 O=POL(I+1)
POL(IR)=O-P
69 CONTINUE
IF(IR)78,78,78
C
C COMPARISON OF COEFFICIENT VECTORS, IE. TEST OF ACCURACY
70 P=0.
DO 75 I=1,IR
IF(C(I))72,71,72
71 O=ABS(POL(I))
GOTO 73
72 O=ABS((POL(I)-C(I))/C(I))
73 IF(P-O)74,75,75
74 P=O
75 CONTINUE
IF(P-TOL)77,76,76
76 IER=1
77 Q(IR+1)=P
E(IR+1)=0.
78 RETURN
C
C ERROR RETURNS
C
C ERROR RETURN FOR POLYNOMIALS OF DEGREE LESS THAN 1
79 IER=2
IR=0
RETURN
C
C ERROR RETURN IF THERE EXISTS NO S-FRACTION
80 IER=4
IR=ISTA
GOTO 60
C
C ERROR RETURN IN CASE OF INSTABLE QD-ALGORITHM
81 IER=3
GOTO 56
END

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PRQ02980
PRQ02990
PRQ03000
PRQ03010
PRQ03020
PRQ03030
PRQ03040
PRQ03050
PRQ03060
PRQ03070
PRQ03080
PRQ03090
PRQ03100
PRQ03110
PRQ03120
PRQ03130
PRQ03140
PRQ03150
PRQ03160
PRQ03170
PRQ03180
PRQ03190
PRQ03200
PRQ03210
PRQ03220
PRQ03230
PRQ03240
PRQ03250
PRQ03260
PRQ03270
PRQ03280
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PRQ03850
PRQ03860
PRQ03870
DPRQ 10
DPRQ 20
DPRQ 30
DPRQ 40
DPRQ 50
DPRQ 60
DPRQ 70
DPRQ 80
DPRQ 90
DPRQ 100
DPRQ 110
DPRQ 120
DPRQ 130
DPRQ 140
DPRQ 150
DPRQ 160
DPRQ 170
DPRQ 180
DPRQ 190
DPRQ 200
DPRQ 210
DPRQ 220
DPRQ 230
DPRQ 240
DPRQ 250
DPRQ 260
DPRQ 270

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C          POLYNOMIAL WITH CALCULATED ROOTS                DPRQ 280
C          THIS RESULTING COEFFICIENT VECTOR HAS DIMENSION IR+1 DPRQ 290
C          COEFFICIENTS ARE ORDERED FROM LOW TO HIGH        DPRQ 300
C          DOUBLE PRECISION ARRAY                            DPRQ 310
C          IR - NUMBER OF CALCULATED ROOTS                  DPRQ 320
C          NORMALLY IR IS EQUAL TO DIMENSION IC MINUS ONE   DPRQ 330
C          IER - RESULTING ERROR PARAMETER. SEE REMARKS     DPRQ 340
C
C          REMARKS
C          THE REAL PART OF THE ROOTS IS STORED IN Q(1) UP TO Q(1R) DPRQ 360
C          CORRESPONDING COMPLEX PARTS ARE STORED IN E(1) UP TO E(1R). DPRQ 380
C          IER = 0 MEANS NO ERRORS                           DPRQ 390
C          IER = 1 MEANS NO CONVERGENCE WITH FEASIBLE TOLERANCE DPRQ 400
C          IER = 2 MEANS POLYNOMIAL IS DEGENERATE (CONSTANT OR ZERO) DPRQ 410
C          IER = 3 MEANS SUBROUTINE WAS ABANDONED DUE TO ZERO DIVISOR DPRQ 420
C          IER = 4 MEANS THERE EXISTS NO S-FRACTION        DPRQ 430
C          IER = -1 MEANS CALCULATED COEFFICIENT VECTOR REVEALS POOR DPRQ 440
C          ACCURACY OF THE CALCULATED ROOTS.                DPRQ 450
C          THE CALCULATED COEFFICIENT VECTOR HAS LESS THAN  DPRQ 460
C          6 CORRECT DIGITS.                                 DPRQ 470
C          THE FINAL COMPARISON BETWEEN GIVEN AND CALCULATED DPRQ 480
C          COEFFICIENT VECTOR IS PERFORMED ONLY IF ALL ROOTS HAVE BEEN DPRQ 490
C          CALCULATED.                                      DPRQ 500
C          THE MAXIMAL RELATIVE ERROR OF THE COEFFICIENT VECTOR IS DPRQ 510
C          RECORDED IN Q(1R+1).                              DPRQ 520
C
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          NONE
C
C          METHOD
C          THE ROOTS OF THE POLYNOMIAL ARE CALCULATED BY MEANS OF
C          THE QUOTIENT-DIFFERENCE ALGORITHM WITH DISPLACEMENT.
C          REFERENCE
C          H. RUTISHAUSER, DER QUOTIENTEN-DIFFERENZEN-ALGORITHMUS,
C          BIRKHAUSER, BASEL/STUTTGART, 1957.
C
C          -----
C          SUBROUTINE DPRODC(IC,Q,E,POL,IR,IER)
C          DIMENSIONED DUMMY VARIABLES
C          DIMENSION E(1),Q(1),C(1),POL(1)
C          DOUBLE PRECISION Q,E,O,P,T,EXPT,ESAV,U,V,W,C,POL,EPS
C
C          NORMALIZATION OF GIVEN POLYNOMIAL
C          TEST OF DIMENSION
C          IR CONTAINS INDEX OF HIGHEST COEFFICIENT
C          IR=IC
C          IER=0
C          EPS=1.D-16
C          TOL=1.E-6
C          LIMIT=10*IC
C          KOUNT=0
C          1 IF (IR-1)79,79,2
C
C          DROP TRAILING ZERO COEFFICIENTS
C          2 IF (C(IR))4,3,4
C          3 IR=IR-1
C          GOTO 1
C
C          REARRANGEMENT OF GIVEN POLYNOMIAL
C          EXTRACTION OF ZERO ROOTS
C          4 O=1.OOO/C(IR)
C          IEND=IR-1
C          ISTA=1
C          NSAV=IR+1
C          JBEG=1
C
C          Q(J)=1.
C          Q(J+1)=C(IR-1)/C(IR)
C          Q(1R)=C(1)/C(IR)
C          WHERE J IS THE INDEX OF THE LOWEST NONZERO COEFFICIENT
C          DO 9 I=1,IR
C          J=NSAV-1
C          IF (C(I))5,7
C          5 GOTO(6,8),JBEG
C          6 NSAV=NSAV+1
C          Q(ISTA)=0.00
C          E(ISTA)=0.00
C          ISTA=ISTA+1
C          GOTO 9
C          7 JBEG=2
C          8 Q(I)=C(I)*O
C          C(I)=Q(J)
C          9 CONTINUE
C
C          INITIALIZATION
C          ESAV=0.00
C          Q(ISTA)=0.00
C          10 NSAV=IR
C
C          COMPUTATION OF DERIVATIVE
C          EXPT=IR-ISTA
C          E(ISTA)=EXPT
C          DO 11 I=ISTA,IEND
C          EXPT=EXPT-1.OOO
C          POL(I+1)=EPS*DABS(Q(I+1))+EPS
C          11 E(I+1)=Q(I+1)*EXPT
C
C          TEST OF REMAINING DIMENSION
C          IF (ISTA-IEND)12,20,60
C          12 JEND=IEND-1
C
C          COMPUTATION OF S-FRACTION
C          DO 19 I=ISTA,JEND
C          IF (I-ISTA)13,16,13
C          13 IF (DABS(E(I))-POL(I+1))14,14,16
C
C          THE GIVEN POLYNOMIAL HAS MULTIPLE ROOTS. THE COEFFICIENTS OF
C          THE COMMON FACTOR ARE STORED FROM Q(NSAV) UP TO Q(1R)
C          14 NSAV=1
C          DO 15 K=1,JEND
C          IF (DABS(E(K))-POL(K+1))15,15,80
C          15 CONTINUE
C          GOTO 21
C
C          EUCLIDEAN ALGORITHM
C          16 DO 19 K=1,IEND
C          E(K+1)=E(K+1)/E(K)
C          Q(K+1)=E(K+1)-Q(K+1)
C          IF (K-1)18,17,18
C
C          TEST FOR SMALL DIVISOR
C          17 IF (DABS(Q(I+1))-POL(I+1))80,80,19
C          18 Q(K+1)=Q(K+1)/Q(I+1)
C          POL(K+1)=POL(K+1)/DABS(Q(I+1))
C          E(K)=Q(K+1)-E(K)
C          19 CONTINUE
C          20 Q(1R)=Q(1R)

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C          THE DISPLACEMENT EXPT IS SET TO 0 AUTOMATICALLY. DPRQ1570
C          E(ISTA)=0.,Q(ISTA+1),...,E(NSAV-1),Q(NSAV),E(NSAV)=0., DPRQ1580
C          FORM A DIAGONAL OF THE QD-ARRAY.                DPRQ1590
C          INITIALIZATION OF BOUNDARY VALUES                DPRQ1600
C          21 E(ISTA)=0.00                                     DPRQ1610
C          NRAN=NSAV-1                                       DPRQ1620
C          22 E(NRAN+1)=0.00                                  DPRQ1630
C
C          TEST FOR LINEAR OR CONSTANT FACTOR                DPRQ1640
C          NRAN=ISTA IS DEGREE-1                             DPRQ1650
C          IF (NRAN-ISTA)24,23,31                             DPRQ1660
C
C          LINEAR FACTOR                                      DPRQ1670
C          23 Q(ISTA+1)=Q(ISTA+1)*EXPT                       DPRQ1680
C          E(ISTA+1)=0.00                                     DPRQ1690
C
C          TEST FOR UNFACTORED COMMON DIVISOR                DPRQ1700
C          24 E(ISTA)=ESAV                                     DPRQ1710
C          IF (IR-NSAV)160,60,25                              DPRQ1720
C          INITIALIZE QD-ALGORITHM FOR COMMON DIVISOR        DPRQ1730
C          25 ISTA=NSAV                                       DPRQ1740
C          ESAV=E(ISTA)                                       DPRQ1750
C          GOTO 10                                             DPRQ1760
C
C          COMPUTATION OF ROOT PAIR                          DPRQ1770
C          26 P=P+EXPT                                         DPRQ1780
C
C          TEST FOR REALITY                                   DPRQ1790
C          IF (D)27,28,28                                     DPRQ1800
C
C          COMPLEX ROOT PAIR                                 DPRQ1810
C          27 Q(NRAN)=P                                         DPRQ1820
C          Q(NRAN+1)=P                                         DPRQ1830
C          E(NRAN)=T                                           DPRQ1840
C          E(NRAN+1)=-T                                         DPRQ1850
C          GOTO 29                                             DPRQ1860
C
C          REAL ROOT PAIR                                    DPRQ1870
C          28 Q(NRAN)=-P                                         DPRQ1880
C          Q(NRAN+1)=P+T                                         DPRQ1890
C          E(NRAN)=0.00                                         DPRQ1900
C
C          REDUCTION OF DEGREE BY 2 (DEFLATION)              DPRQ1910
C          29 NRAN=NRAN-2                                       DPRQ1920
C          GOTO 22                                             DPRQ1930
C
C          COMPUTATION OF REAL ROOT                          DPRQ1940
C          30 Q(NRAN+1)=EXPT+P                                   DPRQ1950
C
C          REDUCTION OF DEGREE BY 1 (DEFLATION)              DPRQ1960
C          NRAN=NRAN-1                                       DPRQ1970
C          GOTO 22                                             DPRQ1980
C
C          START QD-ITERATION                                 DPRQ1990
C          31 JBEG=ISTA+1                                       DPRQ2000
C          JEND=NRAN-1                                         DPRQ2010
C          TEPS=EPS                                             DPRQ2020
C          TDELT=1.E-2                                         DPRQ2030
C          32 KOUNT=KOUNT+1                                       DPRQ2040
C          P=Q(NRAN+1)                                         DPRQ2050
C          R=ABS(SNGL(E(NRAN)))                                  DPRQ2060
C
C          TEST FOR CONVERGENCE                              DPRQ2070
C          33 S=ABS(SNGL(E(JEND)))                                DPRQ2080
C          IF (R-TEPS)30,30,33                                  DPRQ2090
C
C          IS THERE A REAL ROOT NEXT                          DPRQ2100
C          34 IF (S-R)38,38,34                                  DPRQ2110
C
C          IS DISPLACEMENT SMALL ENOUGH                     DPRQ2120
C          35 P=0.00                                           DPRQ2130
C          36 O=P                                               DPRQ2140
C          DO 37 J=JBEG,NRAN                                    DPRQ2150
C          Q(J)=Q(J)+E(J)-E(J-1)-O                              DPRQ2160
C
C          TEST FOR SMALL DIVISOR                             DPRQ2170
C          37 E(J)=Q(J+1)*E(J)/Q(J)                               DPRQ2180
C          Q(NRAN+1)=-E(NRAN)+Q(NRAN+1)-O                       DPRQ2190
C          GOTO 54                                             DPRQ2200
C
C          CALCULATE DISPLACEMENT FOR DOUBLE ROOTS           DPRQ2210
C          QUADRATIC EQUATION FOR DOUBLE ROOTS              DPRQ2220
C          X**2-(Q(NRAN)+Q(NRAN+1))+E(NRAN)*Q(NRAN+1)=0     DPRQ2230
C          38 P=0.500*(Q(NRAN)+E(NRAN)+Q(NRAN+1))             DPRQ2240
C          O=P*P-Q(NRAN)*Q(NRAN+1)                             DPRQ2250
C          T=OSQRT(DABS(O))                                     DPRQ2260
C
C          TEST FOR CONVERGENCE                              DPRQ2270
C          39 IF (S-TEPS)126,26,39                             DPRQ2280
C
C          ARE THERE COMPLEX ROOTS                           DPRQ2290
C          40 IF (O)43,40,40                                     DPRQ2300
C          41 T=-T                                              DPRQ2310
C          42 P=P+T                                             DPRQ2320
C          R=S                                                 DPRQ2330
C          GOTO 34                                             DPRQ2340
C
C          MODIFICATION FOR COMPLEX ROOTS                    DPRQ2350
C          IS DISPLACEMENT SMALL ENOUGH                      DPRQ2360
C          43 IF (S-TDELT)44,35,35                             DPRQ2370
C
C          INITIALIZATION                                     DPRQ2380
C          44 O=Q(JBEG)*E(JBEG)-P                               DPRQ2390
C
C          TEST FOR SMALL DIVISOR                             DPRQ2400
C          45 IF (DABS(O)-POL(JBEG))81,81,45                   DPRQ2410
C          T=(1/T)*2                                           DPRQ2420
C          U=E(JBEG)*Q(JBEG+1)/(O*(1.OOO+T))                 DPRQ2430
C          V=O+U                                               DPRQ2440
C
C          THREEFOLD LOOP FOR COMPLEX DISPLACEMENT          DPRQ2450
C          DO 53 J=JBEG,NRAN                                    DPRQ2460
C          O=Q(J+1)+E(J+1)-U-P                                  DPRQ2470
C
C          TEST FOR SMALL DIVISOR                             DPRQ2480
C          46 IF (DABS(V)-POL(J))46,46,49                       DPRQ2490
C          47 EXPT=EXPT+P                                       DPRQ2500
C          IF (ABS(SNGL(E(JEND)))-TOL)48,48,81                 DPRQ2510
C          48 P=0.500*(V+O-E(JEND))                             DPRQ2520
C          O=P*P-(V+U)*O+U*T-O*W*(1.OOO+T)/Q(JEND)           DPRQ2530
C          T=OSQRT(DABS(O))                                     DPRQ2540
C          GOTO 26                                             DPRQ2550

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C
C      TEST FOR SMALL DIVISOR
49 IF(DABS(OI)-POL(J+1))46,46,50
50 W=U*O/V
   T=T*(V/O)**2
   Q(J)=W*E(J-1)
   U=O.DO
   IF(J-NRAN)51,52,52
51 U=Q(J+2)*E(J+1)/(O*(L.DO+T))
52 V=O+U-W
C
C      TEST FOR SMALL DIVISOR
   IF(DABS(QJ)-POL(J))81,81,53
53 E(J)=W*V*(L.DO+T)/Q(J)
   Q(NRAN+1)=V-E(NRAN)
54 EXPT=EXPT+P
   TEPS=TEPS*1.1
   TDELTA=TDELTA*1.1
   IF(KOUNT-LIMIT)32,55,55
C
C      NO CONVERGENCE WITH FEASIBLE TOLERANCE
C      ERROR RETURN IN CASE OF UNSATISFACTORY CONVERGENCE
55 IER=1
C
C      REARRANGE CALCULATED ROOTS
56 IEND=NSAV-NRAN-1
   E(ISTA)=ESAV
   IF(IEND)59,59,57
57 DO 58 I=1,IEND
   J=ISTA+I
   K=NRAN+I+1
   E(J)=E(K)
58 Q(J)=Q(K)
59 IR=ISTA+IEND
C
C      NORMAL RETURN
60 IR=IR-1
   IF(IR)78,78,61
C
C      REARRANGE CALCULATED ROOTS
61 DO 62 I=1,IR
   Q(I)=Q(I+1)
62 E(I)=E(I+1)
C
C      CALCULATE COEFFICIENT VECTOR FROM ROOTS
   POL(IR+1)=1.DO
   IEND=IR-1
   JBEG=1
   DO 69 J=1,IR
   ISTA=IR+1-J
   O=O.DO
   P=Q(ISTA)
   T=E(ISTA)
   IF(T)65,63,65
C
C      MULTIPLY WITH LINEAR FACTOR
63 DO 64 I=ISTA,IR
   POL(I)=O-P*POL(I+1)
64 O=POL(I+1)
   GOTO 69
65 GOTO(66,67),JBEG
66 JBEG=2
   POL(ISTA)=O.DO
   GOTO 69
C
C      MULTIPLY WITH QUADRATIC FACTOR
67 JBEG=1
   U=P*P+T*T
   P=P*P
   DO 68 I=ISTA,IEND
   POL(I)=O-P*POL(I+1)+U*POL(I+2)
68 O=POL(I+1)
   POL(IR)=O-P
69 CONTINUE
   IF(IR)76,70,78
C
C      COMPARISON OF COEFFICIENT VECTORS, IE. TEST OF ACCURACY
70 P=O.DO
   DO 75 I=1,IR
   IF(C(I))72,71,72
71 O=DABS(POL(I))
   GOTO 73
72 D=DABS((POL(I)-C(I))/C(I))
73 IF(P-O)74,75,75
74 P=O
75 CONTINUE
   IF(SNGL(P)-TOL)77,76,76
76 IER=1
77 Q(IR+1)=P
   E(IR+1)=O.DO
78 RETURN
C
C      ERROR RETURNS
C      ERROR RETURN FOR POLYNOMIALS OF DEGREE LESS THAN I
79 IER=2
   IR=O
   RETURN
C
C      ERROR RETURN IF THERE EXISTS NO S-FRACTION
80 IER=4
   IR=ISTA
   GOTO 60
C
C      ERROR RETURN IN CASE OF INSTABLE QD-ALGORITHM
81 IER=3
   GOTO 56
   END

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DPRQ2860
DPRQ2870
DPRQ2880
DPRQ2890
DPRQ2900
DPRQ2910
DPRQ2920
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DPRQ3000
DPRQ3010
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DPRQ3830
DPRQ3840
DPRQ3850
DPRQ3860
DPRQ3870
DPRQ3880
DPRQ3890
DPRQ3900
DPRQ3910
DPRQ3920

```

Subroutines PRBM and DPRBM

These subroutines compute the real and complex roots of a real polynomial

$$p(x) = c_1 + c_2 x + \dots + c_{n+1} x^n$$

using Bairstow's iterative method of quadratic factorization.

1. Mathematical background

Every real polynomial of degree greater than one can be factored in the form $p(x) = q(x)r(x)$ where $q(x) = x^2 + q_2x + q_1$ is quadratic. If $q(x)$ is reducible, that is, if $q(x)$ is a product of two real linear factors, $p(x)$ has a pair of real roots; and if $q(x)$ is irreducible, $p(x)$ has a complex conjugate pair of roots. If $r(x)$ has degree exceeding one, it too may be factored as above, and so on. The quadratic factors of $p(x)$ are determined by subroutines PQFB and DPQFB. See those routines for a detailed description of Bairstow's method.

2. Programming considerations

The subroutines need only the coefficient vector $C = (c_1, \dots, c_{IC})$ and the number of coefficients $IC = n+1$ as input. They give as output an error parameter IER , the number of computed roots IR , the real and complex parts of the computed roots in vectors RR and RC , and -- if all the roots have been computed -- the coefficients of the polynomial with the computed roots stored in the vector POL .

If $p(x)$ is a constant, that is, if $c_2 = c_3 = \dots = 0$, we set $IR = 0$, $IER = 2$, and return to the call program.

Otherwise, let $IR = \max \{ j \mid c_j \neq 0 \}$. Then we may write:

$$p(x) = c_{IR} \bar{p}(x) \bar{\bar{p}}(x)$$

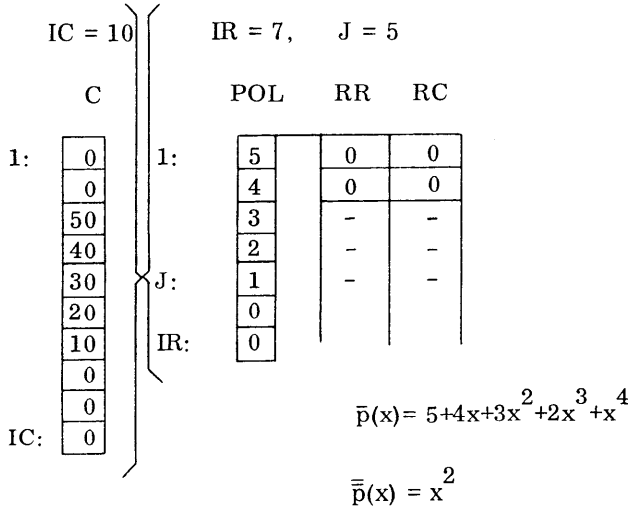
$$\bar{p}(x) = p_1 + p_2 x + \dots + p_J x^{J-1}$$

$$\bar{\bar{p}}(x) = x^K$$

where $K \geq 0$, $J = IR - K$, and $p_j = c_{K+j}/c_{IR}$, $j = 1, 2, \dots, J$, and $p_1 \neq 0$. The coefficients of \bar{p} are stored in $POL(1)$ up to $POL(J)$ and $POL(J+1)$ up to $POL(IR)$ are initialized to zero. If an exponential overflow occurs during the calculation of the p_j we again set $IR = 0$, $IER = 2$ and return control to the calling program.

The following example illustrates the procedure so far:

$$p(x) = 0+0 \cdot x+50 \cdot x^2 + 40 \cdot x^3 + 30 \cdot x^4 + 20 \cdot x^5 + 10 \cdot x^6 + 0 \cdot x^7 + 0 \cdot x^8 + 0 \cdot x^9$$



3. The Bairstow iteration

Upon entering the main part of the routine we assume

$$p(x) = c_{IR} \bar{p}(x) \bar{\bar{p}}(x)$$

where

$$\bar{p}(x) = p_1 + p_2x + \dots + p_jx^{j-1} \quad (p_j = 1)$$

is the polynomial with the unknown roots, and

$$\bar{\bar{p}}(x) = p_{j+1} + p_{j+2}x + \dots + p_{IR}x^{IR-j-1} + x^{IR-j}$$

is the polynomial generated from the computed roots. The coefficients p_1, p_2, \dots, p_{IR} are stored in $POL(1), POL(2), \dots, POL(IR)$. Now there are three possibilities:

(1) $j = 1$. All the roots have been computed. IR is decreased by 1 in order to record the number of computed roots and control is passed on to the last phase of the subroutine (the appendix).

(2) $j = 2$. The last root is $x = -p_1$. This is recorded by setting $RR(IR - 1) = -p_1$ and $RC(IR - 1) = 0$. The polynomial $\bar{p}(x)$ is multiplied by the linear factor $x + p_1$, occupying after multiplication the locations $POL(2)$ up to $POL(IR)$. IR is decreased by 1, thus recording the number of computed roots, and control is passed on to the appendix.

(3) $j \geq 3$. In this case the polynomial $\bar{p}(x)$ is factored by means of subroutine PQFB or DPQFB, where the quadratic factor $q_1 + q_2x + x^2$ of the previous step is used as the initial guess (in the first factorization x^2 is used). If factorization is not successful, it is restarted with the initial guesses $-q_1 + q_2x + x^2, -q_1 - q_2x + x^2$ and $q_1 - q_2x + x^2$. If none of these trials leads to a successful factorization, q_1 and q_2 are increased by 1 (at most nine times). If after a maximum of 40 trials factorization is still unsuccessful, IR is decreased by J , thus recording the number of computed roots, and the rest of the subroutine is bypassed giving the error message $IER = 3$.

If any one of these trials is successful, $\bar{p}(x)$ is divided by the determined quadratic factor, occupying after division the locations $POL(1)$ up to $POL(J-2)$. Then the polynomial $\bar{\bar{p}}(x)$ is multiplied by the same quadratic factor and occupies after multiplication the locations $POL(J-1)$ up to $POL(IR)$. At least the quadratic equation is solved, and the real and complex parts of the two roots are stored in the corresponding locations of RR and RC . After decreasing j by 2, the main part of the subroutine is reentered.

Assuming that all the roots of the polynomial have been computed, the coefficients of the polynomial $\bar{\bar{p}}(x)$ are shifted into the locations $POL(1)$ up to $POL(IR)$, and $POL(IR+1)$ is set to 1 (IR is the number of computed roots).

Furthermore, the absolutely greatest error of the coefficients of the resulting polynomial is generated using the formula

$$a = \max_i |\delta_i|$$

$$\text{where } \delta_i = \begin{cases} (p_i - c_i)/c_i & \text{if } c_i \neq 0 \\ p_i & \text{if } c_i = 0 \end{cases} \quad i = 1, \dots, IR$$

The number a is stored in $RR(IR+1)$ giving the user some indication of the accuracy reached by the subroutines. The warning $IER = -1$ is given if $a > \epsilon$ ($\epsilon = 10^{-3}$ in single precision and $\epsilon = 10^{-6}$ in double precision). The warning $IER = -1$ is overridden by the warning $IER = 1$, which is given if any quadratic factorization fails to converge. (See PQFB.)

For reference see J. H. Wilkinson, "The Evaluation of the Zeros of Ill-Conditioned Polynomials (Parts 1 and 2)", Numerische Mathematik, vol. 1 (1959), pp 150-180.


```

C -----DPRR 10
C                                     DPRR 20
C                                     DPRR 30
SUBROUTINE DPFRM          DPRR 40
C                                     DPRR 50
C                                     DPRR 60
PURPOSE                  DPRR 70
TO CALCULATE ALL REAL AND COMPLEX ROOTS OF A GIVEN
POLYNOMIAL WITH REAL COEFFICIENTS.   DPRR 80
C                                     DPRR 90
USAGE                    DPRR 100
CALL DPFRM (C,IC,RR,RC,POL,IR,IER)  DPRR 110
C                                     DPRR 120
DESCRIPTION OF PARAMETERS DPRR 130
C   - DOUBLE PRECISION INPUT VECTOR CONTAINING THE
COEFFICIENTS OF THE GIVEN POLYNOMIAL. COEFFICIENTS
ARE ORDERED FROM LGW TO HIGH. ON RETURN COEFFI-
CIENTS ARE DIVIDED BY THE LAST NONZERO TERM.   DPRR 140
REMARK #1.
C   - DIMENSION OF VECTORS C, RR, RC, AND POL.   DPRR 150
RR   - RESULTANT DOUBLE PRECISION VECTOR OF REAL PARTS
OF THE ROOTS.   DPRR 160
C   - RESULTANT DOUBLE PRECISION VECTOR OF COMPLEX PARTS
OF THE ROOTS.   DPRR 170
POL  - RESULTANT DOUBLE PRECISION VECTOR OF COEFFICIENTS
OF THE POLYNOMIAL WITH CALCULATED ROOTS.
COEFFICIENTS ARE ORDERED FROM LOW TO HIGH (SEE
REMARK #1).   DPRR 180
IC   - OUTPUT VALUE SPECIFYING THE NUMBER OF CALCULATED
ROOTS. NORMALLY IR IS EQUAL TO IC-1.   DPRR 190
IER  - RESULTANT ERROR PARAMETER CODED AS FOLLOWS
IER=0 - NO ERROR.
IER=1 - SUBROUTINE DPQFB RECORDS POOR CONVERGENCE
OR QUADRATIC FACTORIZATION WITHIN
100 ITERATION STEPS.
IER=2 - POLYNOMIAL IS DEGENERATE, I.E. ZERO OR
CONSTANT,
OR OVERFLOW IN NORMALIZATION OF GIVEN
POLYNOMIAL.
IER=3 - THE SUBROUTINE IS BYPASSED DUE TO
SUCCESSIVE ZERO DIVISORS OR OVERFLOWS
IN QUADRATIC FACTORIZATION OR DUE TO
COMPLETELY UNSATISFACTORY ACCURACY.
IER=-1 - CALCULATED COEFFICIENT VECTOR HAS LESS
THAN SIX CORRECT SIGNIFICANT DIGITS.
THIS REVEALS POOR ACCURACY OF CALCULATED
ROOTS.   DPRR 200
DPRR 210
DPRR 220
DPRR 230
DPRR 240
DPRR 250
DPRR 260
DPRR 270
DPRR 280
DPRR 290
DPRR 300
DPRR 310
DPRR 320
DPRR 330
DPRR 340
DPRR 350
DPRR 360
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DPRR 380
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DPRR 400
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DPRR 670
DPRR 680
DPRR 690
DPRR 700
DPRR 710
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DPRR 1000
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DPRR 1070
DPRR 1080
DPRR 1090
DPRR 1100
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DPRR 1140
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DPRR 1940
DPRR 1950
DPRR 1960
DPRR 1970
DPRR 1980
DPRR 1990
DPRR 2000
DPRR 2010
DPRR 2020
DPRR 2030
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DPRR 2460
DPRR 2470
DPRR 2480
DPRR 2490
DPRR 2500
DPRR 2510

```

Subroutines PQFB and DPQFB

These subroutines use Bairstow's iterative method to find an approximation to a quadratic factor of a given polynomial $p(x) = c_1 + c_2x + \dots + c_{n+1}x^n$ ($\text{deg } p(x) = n \geq 2, c_i \text{ real}$).

1. Mathematical background

Let $Q(x) = x^2 + Q_2x + Q_1$ be any quadratic polynomial with real coefficients. Then $p(x) = R(x)Q(x) + B(Q_1, Q_2)x + C(Q_1, Q_2)$, where $C(Q_1, Q_2) = a_1$, $B(Q_1, Q_2) = a_2$, $R(x) = a_3 + a_4x + \dots + a_{n+1}x^{n-2}$, and

$$a_i = \begin{cases} 0 & \text{if } i > n+1 \\ c_i - Q_2 a_{i+1} - Q_1 a_{i+2} & \text{if } i = n+1, \dots, 2 \\ c_1 - Q_1 a_3 & \text{if } i = 1 \end{cases}$$

Of course, if $q(x) = x^2 + q_2x + q_1$ is a factor of $p(x)$, then:

$$\text{and } \begin{cases} C(q_1, q_2) = 0 \\ B(q_1, q_2) = 0 \end{cases}$$

Suppose that $Q(x)$ is an approximation to $q(x)$; then Q_1 and Q_2 are approximations to q_1 and q_2 respectively, and if ΔQ_1 and ΔQ_2 are such that:

$$\text{and } \begin{cases} q_1 = Q_1 + \Delta Q_1 \\ q_2 = Q_2 + \Delta Q_2 \end{cases}$$

Then:

$$\text{and } \begin{cases} C(Q_1 + \Delta Q_1, Q_2 + \Delta Q_2) = 0 \\ B(Q_1 + \Delta Q_1, Q_2 + \Delta Q_2) = 0 \end{cases} \quad (1)$$

Instead of solving (1) for ΔQ_1 and ΔQ_2 , we solve:

$$\begin{cases} C(Q_1, Q_2) + \frac{\partial}{\partial Q_1} C(Q_1, Q_2) \Delta Q_1 + \frac{\partial}{\partial Q_2} C(Q_1, Q_2) \Delta Q_2 = 0 \\ \text{and } B(Q_1, Q_2) + \frac{\partial}{\partial Q_1} B(Q_1, Q_2) \Delta Q_1 + \frac{\partial}{\partial Q_2} B(Q_1, Q_2) \Delta Q_2 = 0 \end{cases} \quad (2)$$

for ΔQ_1 and ΔQ_2 . Equation (2) is the linearization of (1). To solve (2) we must find $\frac{\partial}{\partial Q_i} B(Q_1, Q_2)$ and $\frac{\partial}{\partial Q_i} C(Q_1, Q_2)$, $i = 1, 2$. To do this we define

$$r_i = \begin{cases} a_i & \text{if } i > 1 \\ a_1 - Q_2 B & \text{if } i = 1 \end{cases}$$

and then

$$s_i = \begin{cases} 0 & \text{if } i > n+1 \\ r_i - Q_2 s_{i+1} - Q_1 s_{i+2} & \text{if } i = n+1, n, n-1, \dots, 1 \end{cases}$$

Now:

$$\left. \frac{\partial r_i}{\partial Q_2} = -r_{i+1} - Q_2 \frac{\partial r_{i+1}}{\partial Q_2} - Q_1 \frac{\partial r_{i+2}}{\partial Q_2} \right\}$$

and

$$\left. \frac{\partial r_i}{\partial Q_1} = -r_{i+2} - Q_2 \frac{\partial r_{i+1}}{\partial Q_1} - Q_1 \frac{\partial r_{i+2}}{\partial Q_1} \right\}$$

By an easy induction on i it follows that:

$$\frac{\partial r_i}{\partial Q_2} = -S_{i+1} \quad \text{and} \quad \frac{\partial r_i}{\partial Q_1} = -S_{i+2}, \quad i = 1, \dots, n+1$$

In particular:

$$\left. \begin{aligned} \frac{\partial B}{\partial Q_1} &= \frac{\partial a_2}{\partial Q_1} = \frac{\partial r_2}{\partial Q_1} = -S_4 \\ \frac{\partial B}{\partial Q_2} &= \frac{\partial a_2}{\partial Q_2} = \frac{\partial r_2}{\partial Q_2} = -S_3 \\ \frac{\partial C}{\partial Q_1} &= \frac{\partial a_1}{\partial Q_1} = \frac{\partial r_1}{\partial Q_1} + Q_2 \frac{\partial r_2}{\partial Q_1} = \\ &\quad -S_3 - Q_2 S_4 \\ \frac{\partial C}{\partial Q_2} &= \frac{\partial a_1}{\partial Q_2} = \frac{\partial r_1}{\partial Q_2} + Q_2 \frac{\partial r_2}{\partial Q_2} + r_2 = \\ &\quad -S_2 - Q_2 S_3 + r_4 \end{aligned} \right\}$$

and if we let:

$$\left. \begin{aligned} C_1 &= s_4 \\ B_1 &= s_3 \\ A_1 &= s_2 - r_2 \\ A &= r_1 \end{aligned} \right\}$$

then we can rewrite (2) as:

$$\left. \begin{aligned} (B_1 + Q_2 C_1) \Delta Q_1 + (A_1 + Q_2 B_1) \Delta Q_2 &= A + Q_2 B \\ C_1 \Delta Q_1 + B_1 \Delta Q_2 &= B \end{aligned} \right\}$$

which simplifies to:

$$\left. \begin{aligned} B_1 \Delta Q_1 + A_1 \Delta Q_2 &= A \\ C_1 \Delta Q_1 + B_1 \Delta Q_2 &= B \end{aligned} \right\} \quad (3)$$

Solving (3) we find that:

$$\left. \begin{aligned} \Delta Q_1 &= \frac{A_1 B - B_1 A}{A_1 C_1 - B_1^2} \\ \Delta Q_2 &= \frac{C_1 A - B_1 B}{A_1 C_1 - B_1^2} \end{aligned} \right\}$$

We can now replace Q_i by $Q_i + \Delta Q_i$, $i = 1, 2$, and repeat the above procedure.

2. Programming considerations

The input consists of a vector C of polynomial coefficients (C(1) is the constant term), the dimension IC of C, a vector Q of dimension 4 with Q(1) and Q(2) containing initial guesses for the coefficients of a quadratic factor, and an upper bound LIM for the number of iterations to be performed.

First $J \leq IC$ is determined such that $C(J) \neq 0$, $C(K) = 0$ for $K > J$. If $J \leq 1$, there is no computation and the error parameter IER is set to -1. If $J > 1$, the polynomial is normalized by dividing all the coefficients of C by C(J), the coefficient of the leading term. If overflow occurs during the normalization, computation is terminated and IER is set to -1. If no overflow occurs, the degree (J-1)

of the polynomial p(x) is tested; if p is of degree 1, there is no further computation and IER is set to -2; if p is of degree 2, Q(1) and Q(2) are set to C(1) and C(2) respectively, Q(3) and Q(4) are set to zero, IER is set to zero, and computation is terminated; if p is of degree greater than 2, the main part of the subroutine--the Bairstow iterative procedure--is entered.

Every approximation $Q(x) = x^2 + Q_2 x + Q_1$ to a quadratic factor of p has associated with it a constant CC, called the norm of the modified linear remainder and hereafter referred to as the norm. It is given by $CC = CA \cdot |A| + CB \cdot |B|$ where:

$$CA = \begin{cases} 1 & \text{if } |C(1)| \leq |C(2)| \\ \left| \frac{C(2)}{C(1)} \right| & \text{if } |C(1)| > |C(2)| \end{cases}$$

and

$$CB = \begin{cases} \left| \frac{C(1)}{C(2)} \right| & \text{if } |C(1)| < |C(2)| \\ 1 & \text{if } |C(1)| \geq |C(2)| \end{cases}$$

Since there is no guarantee that the Bairstow method will converge, several accuracy tests are performed at the end of each iteration. Depending on the outcome of these tests, which in part involve CC, either the computation is terminated or another iteration is performed.

Letting:

$$EPS = \begin{cases} 10^{-6} & \text{in single precision} \\ 10^{-14} & \text{in double precision} \end{cases}$$

and:

$$EPS1 = \begin{cases} 10^{-3} & \text{in single precision} \\ 10^{-16} & \text{in double precision} \end{cases}$$

the tests are described below.

a. If $|A| \leq EPS * |C(1)|$ and $|B| \leq EPS * |C(2)|$, or if $|\Delta Q_1| \leq EPS * |Q_1|$ and $|\Delta Q_2| \leq EPS * |Q_2|$, computation is terminated after setting IER = 0, $Q(1) = Q_1$, $Q(2) = Q_2$, $Q(3) = A$, and $Q(4) = B$.

b. If $|\Delta Q_1| \leq EPS1 * |Q_1|$ and $|\Delta Q_2| \leq EPS1 * |Q_2|$, and if $|\Delta Q_1 / Q_1|$ or $|\Delta Q_2 / Q_2|$ is not smaller than its value for the previous iteration (this is generally due to roundoff errors), computation is terminated after setting IER = 0, $Q(1) = QQ_1$, $Q(2) = QQ_2$, $Q(3) = AA$, and $Q(4) = BB$ where QQ_1 , QQ_2 , AA , and BB are the values of Q_1 , Q_2 , A , and B belonging to

a previous iteration--the iteration with the smallest norm.

c. If no convergence occurs within LIM iterations and if the last norm is not greater than CD/10, where CD is the norm associated with the quadratic factor x^2 , results are generated as in b. with the exception that IER is set to 1. If the last norm is greater than CD/10:

- (1) If the initial guess for the quadratic factor was x^2 , the results are generated as in b. with the exception that IER is set to -3.
- (2) If the initial guess for the quadratic factor was not x^2 , the subroutine restarts with x^2 as the initial guess.

d. If exponential overflow or division by 0 occurs during any iteration, results are generated as in b. with the exception that IER is set to -3.

For reference see:

- (1) J. H. Wilkinson, "The Evaluation of the Zeros of Ill-Conditioned Polynomials (Part I and II)," Numerische Mathematik, vol. 1 (1959), pp. 150-180.
- (2) F. B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp. 472-476.

C		PQFB 10
C		PQFB 20
C	-----	PQFB 30
C	SUBROUTINE PQFB	PQFB 40
C	PURPOSE	PQFB 50
C	TO FIND AN APPROXIMATION Q(X)=Q1+Q2*X+X*X TO A QUADRATIC	PQFB 60
C	FACTOR OF A GIVEN POLYNOMIAL P(X) WITH REAL COEFFICIENTS.	PQFB 70
C		PQFB 80
C	USAGE	PQFB 90
C	CALL PQFB(C,IC,Q,LIM,IER)	PQFB 100
C		PQFB 110
C	DESCRIPTION OF PARAMETERS	PQFB 120
C	C - INPUT VECTOR CONTAINING THE COEFFICIENTS OF P(X) -	PQFB 130
C	C(1) IS THE CONSTANT TERM (DIMENSION IC)	PQFB 140
C	IC - DIMENSION OF C	PQFB 150
C	Q - VECTOR OF DIMENSION 4 - ON INPUT Q(1) AND Q(2) MUST	PQFB 160
C	CONTAIN INITIAL GUESSES FOR Q1 AND Q2 - ON RETURN Q(1)	PQFB 170
C	AND Q(2) CONTAIN THE REFINED COEFFICIENTS Q1 AND Q2 OF	PQFB 180
C	Q(X), WHILE Q(3) AND Q(4) CONTAIN THE COEFFICIENTS A	PQFB 190
C	AND B OF A+B*X, WHICH IS THE REMAINDER OF THE QUOTIENT	PQFB 200
C	OF P(X) BY Q(X)	PQFB 210
C	LIM - INPUT VALUE SPECIFYING THE MAXIMUM NUMBER OF	PQFB 220
C	ITERATIONS TO BE PERFORMED	PQFB 230
C	IER - RESULTING ERROR PARAMETER (SEE REMARKS)	PQFB 240
C	IER= 0 - NO ERROR	PQFB 250
C	IER= 1 - NO CONVERGENCE WITHIN LIM ITERATIONS	PQFB 260
C	IER=-1 - THE POLYNOMIAL P(X) IS CONSTANT OR UNDEFINED	PQFB 270
C	- OR OVERFLOW OCCURRED IN NORMALIZING P(X)	PQFB 280
C	IER=-2 - THE POLYNOMIAL P(X) IS OF DEGREE 1	PQFB 290
C	IER=-3 - NO FURTHER REFINEMENT OF THE APPROXIMATION	PQFB 300
C	TO PQFB 310	PQFB 310
C	A QUADRATIC FACTOR IS FEASIBLE, DUE TO EITHER	PQFB 320
C	DIVISION BY 0, OVERFLOW OR AN INITIAL GUESS	PQFB 330
C	THAT IS NOT SUFFICIENTLY CLOSE TO A FACTOR OF	PQFB 340
C	P(X)	PQFB 350
C		PQFB 360
C	REMARKS	PQFB 370
C	(1) IF IER=-1 THERE IS NO COMPUTATION OTHER THAN THE	PQFB 380
C	POSSIBLE NORMALIZATION OF C.	PQFB 390
C	(2) IF IER=-2 THERE IS NO COMPUTATION OTHER THAN THE	PQFB 400
C	NORMALIZATION OF C.	PQFB 410
C	(3) IF IER=-3 IT IS SUGGESTED THAT A NEW INITIAL GUESS	PQFB 420
C	MADE FOR A QUADRATIC FACTOR. Q, HOWEVER, WILL CONTAIN	PQFB 430
C	THE VALUES ASSOCIATED WITH THE ITERATION THAT YIELDED	PQFB 440
C	THE SMALLEST NORM OF THE MODIFIED LINEAR REMAINDER.	PQFB 450
C	(4) IF IER=1, THEN, ALTHOUGH THE NUMBER OF ITERATIONS LIM	PQFB 460
C	WAS TOO SMALL TO INDICATE CONVERGENCE, NO OTHER PROB-	PQFB 470
C	LEMS HAVE BEEN DETECTED, AND Q WILL CONTAIN THE VALUES	PQFB 480
C	ASSOCIATED WITH THE ITERATION THAT YIELDED THE SMALLEST	PQFB 490
C	NORM OF THE MODIFIED LINEAR REMAINDER.	PQFB 500
C	(5) FOR COMPLETE DETAIL SEE THE DOCUMENTATION FOR	PQFB 510
C	SUBROUTINES PQFB AND DPQFB.	PQFB 520
C		PQFB 530
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	PQFB 540
C	NONE	PQFB 550
C		PQFB 560
C	METHOD	PQFB 570
C	COMPUTATION IS BASED ON BAIRSTON'S ITERATIVE METHOD. (SEE	PQFB 580
C	WILKINSON, J.H., THE EVALUATION OF THE ZEROS OF ILL-CON-	PQFB 590
C	DITIONED POLYNOMIALS (PART ONE AND TWO), NUMERISCHE MATHE-	PQFB 600
C	MATIK, VOL. 1 (1959), PP. 150-180, OR HILDEBRAND, F.B.,	PQFB 610
C	INTRODUCTION TO NUMERICAL ANALYSIS, MC GRAW-HILL, NEW YORK,	PQFB 620
C	TORONTO/LONDON, 1956, PP. 472-476.)	PQFB 630
C		PQFB 640
C	-----	PQFB 650
C		PQFB 660

```

SUBROUTINE DPQFB(C,IC,Q,LIM,IER)
DIMENSION C(1),Q(1)
TEST ON LEADING ZERO COEFFICIENTS
IER=0
J=IC+1
1 J=J-1
IF(J-1)40,2
2 IF(C(J))3,1,3
NORMALIZATION OF REMAINING COEFFICIENTS
3 A=C(J)
IF(A=1,3,6,4
4 DO 5 I=1,J
C(I)=C(I)/A
CALL OVERFL(N)
IF(N-2)40,5,5
5 CONTINUE
TEST ON NECESSITY OF BAIRSTOW ITERATION
6 IF(J-1)1,38,7
PREPARE BAIRSTOW ITERATION
7 EPS=1.E-6
EPS1=1.E-3
L=0
LL=0
Q1=Q(1)
Q2=Q(2)
QQ1=0.
QQ2=0.
AA=C(1)
BB=C(2)
CB=ABS(AA)
CA=ABS(BB)
IF(CB-CA)8,9,10
8 CC=CB+CB
CB=CB/CA
CA=1.
GO TO 11
9 CC=CA+CA
CA=1.
CB=1.
GO TO 11
10 CC=CA+CA
CA=CA/CB
CB=1.
11 CD=CC*.1
START BAIRSTOW ITERATION
PREPARE NESTED MULTIPLICATION
12 A=0.
B=A
A1=A
B1=B
I=J
QQ01=01
QQ02=Q2
Q01=HH
Q02=H
START NESTED MULTIPLICATION
13 H=-Q1B-Q2A+CA/C(1)
CALL OVERFL(N)
IF(N-2)42,14,14
14 B=A
A=H
I=I-1
IF(I-1)118,15,16
15 H=0.
16 H=-Q1A1-Q2A1+H
CALL OVERFL(N)
IF(N-2)42,17,17
17 C1=B1
B1=A1
A1=H
GO TO 13
END OF NESTED MULTIPLICATION
TEST ON SATISFACTORY ACCURACY
18 H=CA*ABS(A1+CB*ABS(B1))
IF(LL)19,19,39
19 L=L+1
IF(ABS(A)-EPS*ABS(C(1)))20,20,21
20 IF(ABS(B)-EPS*ABS(C(2)))39,39,21
TEST ON LINEAR REMAINDER OF MINIMUM NORM
21 IF(H-CC)22,22,23
22 AA=A
BB=B
CC=H
QQ1=Q1
QQ2=Q2
TEST ON LAST ITERATION STEP
23 IF(L-LIM)28,28,24
TEST ON RESTART OF BAIRSTOW ITERATION WITH ZERO INITIAL GUESS
24 IF(H-CD)43,43,25
25 IF(Q(1))27,26,27
26 IF(Q(2))27,42,27
27 Q(1)=0.
Q(2)=0.
GO TO 7
PERFORM ITERATION STEP
28 HH=MAX1(ABS(A1),ABS(B1),ABS(C1))
IF(HH)42,42,29
29 A1=A1/HH
B1=B1/HH
C1=C1/HH
H=A1*C1-B1*Q1
IF(H)30,42,30
30 A=B/HH
B=H/HH
HH=(B*A1-A*B1)/H
H=(A*C1-B*Q1)/H
Q1=Q1/HH
Q2=Q2/H
END OF ITERATION STEP
TEST ON SATISFACTORY RELATIVE ERROR OF ITERATED VALUES
IF(ABS(HH)-EPS*ABS(Q1))31,31,33
31 IF(ABS(HH)-EPS*ABS(Q2))32,32,33
32 LL=L
GO TO 12

```

```

C 33 IF(L-1)12,17,34
C 34 IF(ABS(HH)-EPS1*ABS(Q1))35,35,12
C 35 IF(ABS(HH)-EPS1*ABS(Q2))36,36,12
C 36 IF(ABS(QQ1*HH)-ABS(Q1*QQ1))37,44,44
C 37 IF(ABS(QQ2*HH)-ABS(Q2*QQ2))12,44,44
C 38 END OF BAIRSTOW ITERATION
C 39 EXIT IN CASE OF QUADRATIC POLYNOMIAL
C 40 Q(1)=C(1)
C 41 Q(2)=C(2)
C 42 Q(3)=0.
C 43 Q(4)=0.
C 44 RETURN
C 45 EXIT IN CASE OF SUFFICIENT ACCURACY
C 46 Q(1)=Q1
C 47 Q(2)=Q2
C 48 Q(3)=A
C 49 Q(4)=B
C 50 RETURN
C 51 ERROR EXIT IN CASE OF ZERO OR CONSTANT POLYNOMIAL
C 52 IER=-1
C 53 RETURN
C 54 ERROR EXIT IN CASE OF LINEAR POLYNOMIAL
C 55 IER=-2
C 56 RETURN
C 57 ERROR EXIT IN CASE OF NONREFINED QUADRATIC FACTOR
C 58 IER=-3
C 59 GO TO 44
C 60 ERROR EXIT IN CASE OF UNSATISFACTORY ACCURACY
C 61 IER=1
C 62 Q(1)=QQ1
C 63 Q(2)=QQ2
C 64 Q(3)=AA
C 65 Q(4)=BB
C 66 RETURN
C 67 END
DPQF 10
DPQF 20
.....
SUBROUTINE DPQFB
DPQF 30
DPQF 40
DPQF 50
DPQF 60
PURPOSE
DPQF 70
TO FIND AN APPROXIMATION Q(X)=Q1+Q2*X*X TO A QUADRATIC
DPQF 80
FACTOR OF A GIVEN POLYNOMIAL P(X) WITH REAL COEFFICIENTS.
DPQF 90
DPQF 70
USAGE
DPQF 100
CALL DPQFB(C,IC,Q,LIM,IER)
DPQF 110
DESCRIPTION OF PARAMETERS
DPQF 120
C - DOUBLE PRECISION INPUT VECTOR CONTAINING THE
DPQF 130
COEFFICIENTS OF P(X) - C(1) IS THE CONSTANT TERM
DPQF 140
(IC DIMENSION IC)
DPQF 150
Q - DOUBLE PRECISION VECTOR OF DIMENSION 4 - ON INPUT Q(1)
DPQF 160
AND Q(2) CONTAIN INITIAL GUESSES FOR Q1 AND Q2 - ON
DPQF 170
RETURN Q(1) AND Q(2) CONTAIN THE REFINED COEFFICIENTS
DPQF 180
Q1 AND Q2 OF Q(X), WHILE Q(3) AND Q(4) CONTAIN THE
DPQF 190
COEFFICIENTS A AND B OF A+B*X, WHICH IS THE REMAINDER
DPQF 200
OF THE QUOTIENT OF P(X) BY Q(X)
DPQF 210
LIM - INPUT VALUE SPECIFYING THE MAXIMUM NUMBER OF
DPQF 220
ITERATIONS TO BE PERFORMED
DPQF 230
IER - RESULTING ERROR PARAMETER (SEE REMARKS)
DPQF 240
IER=0 - NO ERROR
DPQF 250
IER=1 - NO CONVERGENCE WITHIN LIM ITERATIONS
DPQF 260
IER=-1 - THE POLYNOMIAL P(X) IS CONSTANT OR UNDEFINED
DPQF 270
OR OVERFLOW OCCURRED IN NORMALIZING P(X)
DPQF 280
IER=-2 - THE POLYNOMIAL P(X) IS OF DEGREE 1
DPQF 290
IER=-3 - NO FURTHER REFINEMENT OF THE APPROXIMATION
DPQF 300
A QUADRATIC FACTOR IS FEASIBLE, DUE TO EITHER
DPQF 310
DIVISION BY 0, OVERFLOW OR AN INITIAL GUESS
DPQF 320
THAT IS NOT SUFFICIENTLY CLOSE TO A FACTOR OF
DPQF 330
P(X)
DPQF 340
REMARKS
DPQF 350
(1) IF IER=-1 THERE IS NO COMPUTATION OTHER THAN THE
DPQF 360
POSSIBLE NORMALIZATION OF C.
DPQF 370
(2) IF IER=-2 THERE IS NO COMPUTATION OTHER THAN THE
DPQF 380
NORMALIZATION OF C.
DPQF 390
(3) IF IER=-3 IT IS SUGGESTED THAT A NEW INITIAL GUESS
DPQF 400
MADE FOR A QUADRATIC FACTOR - Q, HOWEVER, WILL CONTAIN
DPQF 410
THE VALUES ASSOCIATED WITH THE ITERATION THAT YIELDED
DPQF 420
THE SMALLEST NORM OF THE MODIFIED LINEAR REMAINDER.
DPQF 430
(4) IF IER=1, THEN, ALTHOUGH THE NUMBER OF ITERATIONS LIM
DPQF 440
WAS TOO SMALL TO INDICATE CONVERGENCE, NO OTHER
DPQF 450
PROBLEMS HAVE BEEN DETECTED, AND Q WILL CONTAIN THE
DPQF 460
VALUES ASSOCIATED WITH THE ITERATION THAT YIELDED THE
DPQF 470
SMALLEST NORM OF THE MODIFIED LINEAR REMAINDER.
DPQF 480
(5) FOR COMPLETE DETAIL SEE THE DOCUMENTATION FOR
DPQF 490
SUBROUTINES DPFB AND DPQFB.
DPQF 500
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
DPQF 510
NONE
DPQF 520
METHOD
DPQF 530
COMPUTATION IS BASED ON BAIRSTOW'S ITERATIVE METHOD.
DPQF 540
(WILKINSON, J.H., THE EVALUATION OF THE ZEROS OF
DPQF 550
ILL-CONDITIONED POLYNOMIALS (PART ONE AND TWO),
DPQF 560
NUMERISCHE MATHEMATIK, VOL.1 (1959),
DPQF 570
PP. 150-180, OR HILDEBRAND, F.B.,
DPQF 580
INTRODUCTION TO NUMERICAL ANALYSIS,
DPQF 590
MC GRAW-HILL, NEW YORK/TORONTO/LONDON, 1956,
DPQF 600
PP. 472-476.)
DPQF 610
SUBROUTINE DPQFB(C,IC,Q,LIM,IER)
DPQF 620
DIMENSION C(1),Q(1)
DPQF 630
DOUBLE PRECISION A,B,AA,BB,CA,CB,CC,CD,A1,B1,C1,H,HH,Q1,Q2,QQ1,
DPQF 640
QQ2,QQ01,QQ02,D01,D02,EPS,EPS1,C,Q
DPQF 650
TEST ON LEADING ZERO COEFFICIENTS
DPQF 660
IER=0
DPQF 670
J=IC+1
DPQF 680
J=J-1
DPQF 690

```



```

IF(J-1)40,40,2
2 IF(C(J))3,1,3
C
C      NORMALIZATION OF REMAINING COEFFICIENTS
3 A=C(J)
IF(A-1.D)4,6,4
4 DO 5 I=1,J
C(I)=C(I)/A
CALL OVERFL(N)
IF(N-2)40,5,5
5 CONTINUE
C
C      TEST ON NECESSITY OF BAIRSTOW ITERATION
6 IF(J-3)41,38,7
C
C      PREPARE BAIRSTOW ITERATION
7 EPS=1.D-14
EPS1=1.D-6
L=0
LL=0
Q1=Q(1)
Q2=Q(2)
QQ1=0.DD
QQ2=0.DD
AA=C(1)
BB=C(2)
CB=DABS(AA)
CA=DABS(BB)
IF(CB-CA)8,9,10
8 CC=CB/CB
CB=CB/CA
CA=1.DD
GO TO 11
9 CC=CA/CA
CA=1.DD
CB=1.DD
GO TO 11
10 CG=CA/CA
CA=CA/CB
CB=1.DD
11 CD=CC*.1DD
C
C      START BAIRSTOW ITERATION
C      PREPARE NESTED MULTIPLICATION
12 A=0.DD
B=A
A1=A
B1=A
I=J
QQ1=Q1
QQ2=Q2
DQ1=HH
DQ2=H
C
C      START NESTED MULTIPLICATION
13 H=-Q1*B-Q2*A+C(I)
CALL OVERFL(N)
IF(N-2)42,14,14
14 B=A
A=H
I=I-1
IF(I-1)18,15,16
15 H=0.DD
16 H=-Q1*B1-Q2*A1+H
CALL OVERFL(N)
IF(N-2)42,17,17
17 C1=B1
B1=A1
A1=H
GO TO 13
C      END OF NESTED MULTIPLICATION
C
C      TEST ON SATISFACTORY ACCURACY
18 H=C1*DABS(A)+CB*DABS(B)
IF(LL)19,19,39
19 L=L+1
IF(DABS(A)-EPS*DABS(C(1)))20,20,21
20 IF(DABS(B)-EPS*DABS(C(2)))39,39,21
C
C      TEST ON LINEAR REMAINDER OF MINIMUM NORM
21 IF(H-C)22,22,23

```

```

DPQF 790
DPQF 800
DPQF 810
DPQF 820
DPQF 830
DPQF 840
DPQF 850
DPQF 860
DPQF 870
DPQF 880
DPQF 890
DPQF 900
DPQF 910
DPQF 920
DPQF 930
DPQF 940
DPQF 950
DPQF 960
DPQF 970
DPQF 980
DPQF 990
DPQF 1000
DPQF 1010
DPQF 1020
DPQF 1030
DPQF 1040
DPQF 1050
DPQF 1060
DPQF 1070
DPQF 1080
DPQF 1090
DPQF 1100
DPQF 1110
DPQF 1120
DPQF 1130
DPQF 1140
DPQF 1150
DPQF 1160
DPQF 1170
DPQF 1180
DPQF 1190
DPQF 1200
DPQF 1210
DPQF 1220
DPQF 1230
DPQF 1240
DPQF 1250
DPQF 1260
DPQF 1270
DPQF 1280
DPQF 1290
DPQF 1300
DPQF 1310
DPQF 1320
DPQF 1330
DPQF 1340
DPQF 1350
DPQF 1360
DPQF 1370
DPQF 1380
DPQF 1390
DPQF 1400
DPQF 1410
DPQF 1420
DPQF 1430
DPQF 1440
DPQF 1450
DPQF 1460
DPQF 1470
DPQF 1480
DPQF 1490
DPQF 1500
DPQF 1510
DPQF 1520
DPQF 1530
DPQF 1540
DPQF 1550
DPQF 1560
DPQF 1570
DPQF 1580
DPQF 1590

```

```

22 AA=A
BB=B
CC=H
QQ1=Q1
QQ2=Q2
C
C      TEST ON LAST ITERATION STEP
23 IF(L-1)M)28,28,24
C
C      TEST ON RESTART OF BAIRSTOW ITERATION WITH ZERO INITIAL GUESS
24 IF(H-CD)43,43,25
25 IF(Q(1))27,26,27
26 IF(Q(2))27,42,27
27 Q(1)=0.DD
Q(2)=0.DD
GO TO 7
C
C      PERFORM ITERATION STEP
28 HH=DMAX(DABS(A1),DABS(B1),DABS(C1))
IF(HH)42,42,29
29 A1=A1/HH
B1=B1/HH
C1=C1/HH
H=A1+C1-B1*B1
IF(H)30,42,30
30 A=A/HH
B=B/HH
HH=(B*A1-A*R1)/H
H=(A*C1-B*R1)/H
Q1=Q1+HH
Q2=Q2+H
C
C      END OF ITERATION STEP
C
C      TEST ON SATISFACTORY RELATIVE ERROR OF ITERATED VALUES
IF(DABS(HH)-EPS*DABS(Q1))31,31,33
31 IF(DABS(H)-EPS*DABS(Q2))32,32,33
32 LL=L
GO TO 12
C
C      TEST ON DECREASING RELATIVE ERRORS
33 IF(L-1)12,12,34
34 IF(DABS(HH)-EPS1*DABS(Q1))35,35,12
35 IF(DABS(H)-EPS1*DABS(Q2))36,36,12
36 IF(DABS(Q01+HH)-DABS(Q1+Q01))37,44,44
37 IF(DABS(Q02+H)-DABS(Q2+Q02))12,44,44
C      END OF BAIRSTOW ITERATION
C
C      EXIT IN CASE OF QUADRATIC POLYNOMIAL
38 Q(1)=C(1)
Q(2)=C(2)
Q(3)=0.DD
Q(4)=0.DD
RETURN
C
C      EXIT IN CASE OF SUFFICIENT ACCURACY
39 Q(1)=Q1
Q(2)=Q2
Q(3)=A
Q(4)=B
RETURN
C
C      ERROR EXIT IN CASE OF ZERO OR CONSTANT POLYNOMIAL
40 IER=-1
RETURN
C
C      ERROR EXIT IN CASE OF LINEAR POLYNOMIAL
41 IER=-2
RETURN
C
C      ERROR EXIT IN CASE OF NONREFINED QUADRATIC FACTOR
42 IER=-3
GO TO 44
C
C      ERROR EXIT IN CASE OF UNSATISFACTORY ACCURACY
43 IER=1
44 Q(1)=Q01
Q(2)=Q02
C(1)=A1
Q(4)=B
RETURN
END
DPQF 1600
DPQF 1610
DPQF 1620
DPQF 1630
DPQF 1640
DPQF 1650
DPQF 1660
DPQF 1670
DPQF 1680
DPQF 1690
DPQF 1700
DPQF 1710
DPQF 1720
DPQF 1730
DPQF 1740
DPQF 1750
DPQF 1760
DPQF 1770
DPQF 1780
DPQF 1790
DPQF 1800
DPQF 1810
DPQF 1820
DPQF 1830
DPQF 1840
DPQF 1850
DPQF 1860
DPQF 1870
DPQF 1880
DPQF 1890
DPQF 1900
DPQF 1910
DPQF 1920
DPQF 1930
DPQF 1940
DPQF 1950
DPQF 1960
DPQF 1970
DPQF 1980
DPQF 1990
DPQF 2000
DPQF 2010
DPQF 2020
DPQF 2030
DPQF 2040
DPQF 2050
DPQF 2060
DPQF 2070
DPQF 2080
DPQF 2090
DPQF 2100
DPQF 2110
DPQF 2120
DPQF 2130
DPQF 2140
DPQF 2150
DPQF 2160
DPQF 2170
DPQF 2180
DPQF 2190
DPQF 2200
DPQF 2210
DPQF 2220
DPQF 2230
DPQF 2240
DPQF 2250
DPQF 2260
DPQF 2270
DPQF 2280
DPQF 2290
DPQF 2300
DPQF 2310
DPQF 2320
DPQF 2330
DPQF 2340
DPQF 2350
DPQF 2360
DPQF 2370
DPQF 2380
DPQF 2390
DPQF 2400

```

Polynomials: Special Types

Subroutines CNP and DCNP

These subroutines compute the values of the Chebyshev polynomials for a given argument x and orders zero up to N. The Chebyshev polynomial $T_n(x)$ satisfies the recurrence equation

$$T_{n+1}(x) = 2x \cdot T_n(x) - T_{n-1}(x)$$

with starting values $T_0(x) = 1$, $T_1(x) = x$. From this equation it follows immediately that roundoff errors grow at worst linearly under the tacit assumption that the argument has an absolute value less than one.

If e_{n+r} is the error in $T_{n+r}(x)$ due to a single roundoff error e in $T_n(x)$:

$$e_{n+r+1} = 2x \cdot e_{n+r} - e_{n+r-1}$$

with initial conditions $e_n = e$, $e_{n-1} = 0$.

The solution of this difference equation has its maximum for $|x| = 1$:

$$e_{n-1} = 0, e_n = e, |e_{n+1}| = 2e, \dots, |e_{n+r}| = (r+1)e$$

The order is assumed to be zero for negative values of N.

```
C
C
C -----
C          DNP 10
C          DNP 20
C          DNP 30
C          DNP 40
C          DNP 50
C          DNP 60
C          DNP 70
C          DNP 80
C          DNP 90
C          DNP 100
C          DNP 110
C          DNP 120
C          DNP 130
C          DNP 140
C          DNP 150
C          DNP 160
C          DNP 170
C          DNP 180
C          DNP 190
C          DNP 200
C          DNP 210
C          DNP 220
C          DNP 230
C          DNP 240
C          DNP 250
C          DNP 260
C          DNP 270
C          DNP 280
C          DNP 290
C          DNP 300
C          DNP 310
C          DNP 320
C          DNP 330
C          DNP 340
C          DNP 350
C          DNP 360
C          DNP 370
C          DNP 380
C          DNP 390
C          DNP 400
C          DNP 410
C          DNP 420
C          DNP 430
C          DNP 440
C          DNP 450
C          DNP 460
C          DNP 470
C          DNP 480
C          DNP 490
C          DNP 500
C          DNP 510
C          DNP 520
C          DNP 530
C          DNP 540
C          DNP 550
C          DNP 560
C          DNP 570
C          DNP 580
C
C          SUBROUTINE DCNP
C
C          PURPOSE
C          COMPUTE THE VALUES OF THE CHEBYSHEV POLYNOMIALS T(N,X)
C          FOR ARGUMENT VALUE X AND ORDERS 0 UP TO N.
C
C          USAGE
C          CALL DCNP(Y,X,N)
C
C          DESCRIPTION OF PARAMETERS
C          Y - RESULT VECTOR OF DIMENSION N+1 CONTAINING THE VALUES
C          OF CHEBYSHEV POLYNOMIALS OF ORDER 0 UP TO N
C          FOR GIVEN ARGUMENT X.
C          DOUBLE PRECISION VECTOR.
C          VALUES ARE ORDERED FROM LOW TO HIGH ORDER
C          Y - RESULT VALUE
C          DOUBLE PRECISION VARIABLE.
C          X - ARGUMENT OF CHEBYSHEV POLYNOMIAL
C          N - ORDER OF CHEBYSHEV POLYNOMIAL
C
C          REMARKS
C          N LESS THAN 0 IS TREATED AS IF N WERE 0
C
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          NONE
C
C          METHOD
C          EVALUATION IS BASED ON THE RECURRENCE EQUATION FOR
C          CHEBYSHEV POLYNOMIALS T(N,X)
C          T(N+1,X)=2*X*T(N,X)-T(N-1,X),
C          WHERE THE FIRST TERM IN BRACKETS IS THE ORDER,
C          THE SECOND IS THE ARGUMENT.
C          STARTING VALUES ARE T(0,X)=1, T(1,X)=X.
C
C -----
C          SUBROUTINE DCNP(Y,X,N)
C          DIMENSION Y(1)
C          DOUBLE PRECISION Y,X,F
C
C          Y(1)=1.00
C          IF(N)1,1,2
C          1 RETURN
C
C          2 Y(2)=X
C          IF(N-1)1,1,3
C
C          INITIALIZATION
C          3 F=X*X
C
C          DO 4 I=2,N
C          4 Y(I+1)=F*Y(I)-Y(I-1)
C          RETURN
C          END
```

```
C
C          CNP 10
C          CNP 20
C          CNP 30
C          CNP 40
C          CNP 50
C          CNP 60
C          CNP 70
C          CNP 80
C          CNP 90
C          CNP 100
C          CNP 110
C          CNP 120
C          CNP 130
C          CNP 140
C          CNP 150
C          CNP 160
C          CNP 170
C          CNP 180
C          CNP 190
C          CNP 200
C          CNP 210
C          CNP 220
C          CNP 230
C          CNP 240
C          CNP 250
C          CNP 260
C          CNP 270
C          CNP 280
C          CNP 290
C          CNP 300
C          CNP 310
C          CNP 320
C          CNP 330
C          CNP 340
C          CNP 350
C          CNP 360
C          CNP 370
C          CNP 380
C          CNP 390
C          CNP 400
C          CNP 410
C          CNP 420
C          CNP 430
C          CNP 440
C          CNP 450
C          CNP 460
C          CNP 470
C          CNP 480
C          CNP 490
C          CNP 500
C          CNP 510
C          CNP 520
C          CNP 530
C          CNP 540
C
C          SUBROUTINE CNP
C
C          PURPOSE
C          COMPUTE THE VALUES OF THE CHEBYSHEV POLYNOMIALS T(N,X)
C          FOR ARGUMENT VALUE X AND ORDERS 0 UP TO N.
C
C          USAGE
C          CALL CNP(Y,X,N)
C
C          DESCRIPTION OF PARAMETERS
C          Y - RESULT VECTOR OF DIMENSION N+1 CONTAINING THE VALUES
C          OF CHEBYSHEV POLYNOMIALS OF ORDER 0 UP TO N
C          FOR GIVEN ARGUMENT X.
C          Y - RESULT VALUE
C          VALUES ARE ORDERED FROM LOW TO HIGH ORDER
C          X - ARGUMENT OF CHEBYSHEV POLYNOMIAL
C          N - ORDER OF CHEBYSHEV POLYNOMIAL
C
C          REMARKS
C          N LESS THAN 0 IS TREATED AS IF N WERE 0
C
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          NONE
C
C          METHOD
C          EVALUATION IS BASED ON THE RECURRENCE EQUATION FOR
C          CHEBYSHEV POLYNOMIALS T(N,X)
C          T(N+1,X)=2*X*T(N,X)-T(N-1,X),
C          WHERE THE FIRST TERM IN BRACKETS IS THE ORDER,
C          THE SECOND IS THE ARGUMENT.
C          STARTING VALUES ARE T(0,X)=1, T(1,X)=X.
C
C -----
C          SUBROUTINE CNP(Y,X,N)
C          DIMENSION Y(1)
C          Y(1)=1.
C          IF(N)1,1,2
C          1 RETURN
C
C          2 Y(2)=X
C          IF(N-1)1,1,3
C
C          INITIALIZATION
C          3 F=X*X
C
C          DO 4 I=2,N
C          4 Y(I+1)=F*Y(I)-Y(I-1)
C          RETURN
C          END
```

Subroutines CNPS and DCNPS

These subroutines compute the value of a series expansion in Chebyshev polynomials. The Chebyshev polynomial Tn(x) satisfies the recurrence equation

T_{n+1}(x) = 2x * T_n(x) - T_{n-1}(x)

with starting values T0(x) = 1, T1(x) = x.

An n-term expansion in Chebyshev polynomials with coefficient vector C = (c1, ..., cn) is evaluated by means of a backward iteration scheme:

Arg = 2x, H1 = 0, H0 = 0

H2 = H1

H1 = H0

H0 = Arg * H1 - H2 + c_{n-i+1}

Y = (c1 - H2 + H0) / 2.

for i = 1, ..., n

This gives result Y(x) = sum_{i=1}^n c_i T_{i-1}(x).

Calculation is bypassed in case of a nonpositive value of the dimension n.

```
C
C
C .....
C SUBROUTINE CNPS
C
C PURPOSE
C COMPUTES THE VALUE OF AN N-TERM EXPANSION IN CHEBYSHEV
C POLYNOMIALS WITH COEFFICIENT VECTOR C FOR ARGUMENT VALUE X.
C
C USAGE
C CALL CNPS(Y,X,C,N)
C
C DESCRIPTION OF PARAMETERS
C Y - RESULT VALUE
C X - ARGUMENT VALUE
C C - COEFFICIENT VECTOR OF GIVEN EXPANSION
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
C N - DIMENSION OF COEFFICIENT VECTOR C
C
C REMARKS
C OPERATION IS BYPASSED IN CASE N LESS THAN 1
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C
C METHOD
C DEFINITION
C Y=SUM(C(I)*T(I-1,X), SUMMED OVER I FROM 1 TO N).
C EVALUATION IS DONE BY MEANS OF BACKWARD RECURSION
C USING THE RECURRENCE EQUATION FOR CHEBYSHEV POLYNOMIALS
C T(N+1,X)=2*X*T(N,X)-T(N-1,X).
C .....
C SUBROUTINE CNPS(Y,X,C,N)
C
C DIMENSION C(1)
C
C TEST OF DIMENSION
C IF(N)1,1,2
C 1 RETURN
C
C 2 IF(N-2)3,4,4
C 3 Y=C(1)
C RETURN
C
C INITIALIZATION
C 4 ARG=X*X
C H1=0.0D0
C H0=0.0D0
C
C DO 5 I=1,N
C K=N-I
C H2=H1
C H1=H0
C 5 H0=ARG*H1-H2+C(K+1)
C Y=0.5*(C(1)-H2+H0)
C RETURN
C END
```

```
C .....
C SUBROUTINE DCNPS
C
C PURPOSE
C COMPUTES THE VALUE OF AN N-TERM EXPANSION IN CHEBYSHEV
C POLYNOMIALS WITH COEFFICIENT VECTOR C FOR ARGUMENT VALUE X.
C
C USAGE
C CALL DCNPS(Y,X,C,N)
C
C DESCRIPTION OF PARAMETERS
C Y - RESULT VALUE
C DOUBLE PRECISION VARIABLE
C X - ARGUMENT VALUE
C DOUBLE PRECISION VARIABLE
C C - COEFFICIENT VECTOR OF GIVEN EXPANSION
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
C DOUBLE PRECISION VECTOR
C N - DIMENSION OF COEFFICIENT VECTOR C
C
C REMARKS
C OPERATION IS BYPASSED IN CASE N LESS THAN 1
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C
C METHOD
C DEFINITION
C Y=SUM(C(I)*T(I-1,X), SUMMED OVER I FROM 1 TO N).
C EVALUATION IS DONE BY MEANS OF BACKWARD RECURSION
C USING THE RECURRENCE EQUATION FOR CHEBYSHEV POLYNOMIALS
C T(N+1,X)=2*X*T(N,X)-T(N-1,X).
C .....
C SUBROUTINE DCNPS(Y,X,C,N)
C
C DIMENSION C(1)
C DOUBLE PRECISION C,Y,X,H0,H1,H2,ARG
C
C TEST OF DIMENSION
C IF(N)1,1,2
C 1 RETURN
C
C 2 IF(N-2)3,4,4
C 3 Y=C(1)
C RETURN
C
C INITIALIZATION
C 4 ARG=X*X
C H1=0.0D0
C H0=0.0D0
C
C DO 5 I=1,N
C K=N-I
C H2=H1
C H1=H0
C 5 H0=ARG*H1-H2+C(K+1)
C Y=0.5D0*(C(1)-H2+H0)
C RETURN
C END
```

Subroutines TCNP and DTCNP

These subroutines transform a given series expansion in Chebyshev polynomials to a polynomial. The independent variable x of the given expansion is thereby substituted by the independent variable z of the resulting polynomial using the linear transformation $x = A * z + B$ or $z = (x - B)/A$.

$$\text{This means: } \sum_{i=1}^N C_i * T_{i-1}(A * z + B) = \sum_{i=1}^N \text{POL}_i * z^{i-1}$$

Calculation is bypassed in case of a nonpositive value of the dimension N .

The range $(-1, +1)$ in x is transformed to the range (z_1, z_R) in z with $z_1 = -(1+B)/A$ and $z_R = (1-B)/A$, or vice versa, $A = 2/(z_R - z_1)$ and $B = -(z_R + z_1)/(z_R - z_1)$.

The Chebyshev polynomial $T_N(x)$ satisfies the recurrence equation

$$T_{n+1}(x) = 2x \cdot T_n(x) - T_{n-1}(x)$$

with starting values $T_0(x) = 1$, $T_1(x) = x$. The transformation is performed by means of a forward iteration scheme:

1. The coefficient vector of the Chebyshev polynomial $T_i(x)$ is calculated from the coefficient vectors of $T_{i-1}(x)$, $T_{i-2}(x)$ using the recurrence equation, for $i = 3, \dots, N$.

2. The resulting polynomial coefficient vector is obtained by summation of c_i times coefficient vector of $T_{i-1}(x)$ over i , for $i = 1, \dots, N$.

```

C ..... TCNP 10
C SUBROUTINE TCNP TCNP 20
C A SERIES EXPANSION IN CHEBYSHEV POLYNOMIALS WITH INDEPENDENT TCNP 30
C VARIABLE X IS TRANSFORMED TO A POLYNOMIAL WITH INDEPENDENT TCNP 40
C VARIABLE Z, WHERE X=A*Z+B. TCNP 50
C
C PURPOSE TCNP 60
C CALL TCNP(A,B,POL,N,C,WORK) TCNP 70
C
C USAGE TCNP 110
C CALL TCNP(A,B,POL,N,C,WORK) TCNP 120
C
C DESCRIPTION OF PARAMETERS TCNP 140
C A - FACTOR OF LINEAR TERM IN GIVEN LINEAR TRANSFORMATION TCNP 150
C B - CONSTANT TERM IN GIVEN LINEAR TRANSFORMATION TCNP 160
C POL - COEFFICIENT VECTOR OF POLYNOMIAL (RESULTANT VALUE) TCNP 170
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH TCNP 180
C N - DIMENSION OF COEFFICIENT VECTORS POL AND C TCNP 190
C C - GIVEN COEFFICIENT VECTOR OF EXPANSION TCNP 200
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH TCNP 210
C POL AND C MAY BE IDENTICALLY LOCATED TCNP 220
C WORK - WORKING STORAGE OF DIMENSION 2*N TCNP 230
C
C REMARKS TCNP 240
C COEFFICIENT VECTOR C REMAINS UNCHANGED IF NOT COINCIDING TCNP 250
C WITH COEFFICIENT VECTOR POL. TCNP 260
C OPERATION IS BYPASSED IN CASE N LESS THAN 1. TCNP 270
C THE LINEAR TRANSFORMATION X=A*Z+B OR Z=(1/A)(X-B) TRANSFORMS TCNP 280
C THE RANGE (-1,+1) IN X TO THE RANGE (ZL,ZR) IN Z, WHERE TCNP 290
C ZL=(1+B)/A AND ZR=(1-B)/A. TCNP 300
C FOR GIVEN ZL, ZR WE HAVE A=2/(ZR-ZL) AND B=-(ZR+ZL)/(ZR-ZL) TCNP 310
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED TCNP 320
C NONE TCNP 330
C
C METHOD TCNP 340
C THE TRANSFORMATION IS BASED ON THE RECURRENCE EQUATION TCNP 350
C FOR CHEBYSHEV POLYNOMIALS T(N,X) TCNP 360
C T(N+1,X)=2*X*T(N,X)-T(N-1,X), TCNP 370
C WHERE THE FIRST TERM IN BRACKETS IS THE INDEX, TCNP 380
C THE SECOND IS THE ARGUMENT. TCNP 390
C STARTING VALUES ARE T(0,X)=1, T(1,X)=X. TCNP 400
C THE TRANSFORMATION IS IMPLICITLY DEFINED BY MEANS OF TCNP 410
C X = A*Z+B TOGETHER WITH TCNP 420
C SUM(POL(I)*Z**(I-1), SUMMED OVER I FROM 1 TO N) TCNP 430
C =SUM(C(I)*T(I-1,X), SUMMED OVER I FROM 1 TO N). TCNP 440
C

```

```

C ..... TCNP 490
C SUBROUTINE TCNP(A,B,POL,N,C,WORK) TCNP 500
C DIMENSION POL(1),C(1),WORK(1) TCNP 510
C TEST OF DIMENSION TCNP 520
C IF(N-1)2,1,3 TCNP 530
C DIMENSION LESS THAN 2 TCNP 540
C 1 POL(1)=C(1) TCNP 550
C 2 RETURN TCNP 560
C 3 POL(1)=C(1)+C(2)*B TCNP 570
C POL(2)=C(2)*A TCNP 580
C IF(N-2)2,2,4 TCNP 590
C INITIALIZATION TCNP 600
C 4 WORK(1)=1. TCNP 610
C WORK(2)=B TCNP 620
C WORK(3)=0. TCNP 630
C WORK(4)=A TCNP 640
C XD=A+A TCNP 650
C XO=B+B TCNP 660
C CALCULATE COEFFICIENT VECTOR OF NEXT CHEBYSHEV POLYNOMIAL TCNP 670
C AND ADD MULTIPLE OF THIS VECTOR TO POLYNOMIAL POL TCNP 740
C DO 6 J=3,N TCNP 750
C P=0. TCNP 760
C DO 5 K=2,J TCNP 770
C H=P-WORK(2*K-3)+XO*WORK(2*K-2) TCNP 780
C P=WORK(2*K-2) TCNP 790
C WORK(2*K-2)=H TCNP 800
C WORK(2*K-3)=P TCNP 810
C POL(K-1)=POL(K-1)+H*C(J) TCNP 820
C 5 P=XO*P TCNP 830
C WORK(2*J-1)=0. TCNP 840
C WORK(2*J)=P TCNP 850
C 6 POL(J)=C(J)*P TCNP 860
C RETURN TCNP 870
C END TCNP 880
C TCNP 890
C TCNP 900

```

```

C ..... DTCN 10
C SUBROUTINE DTCNP DTCN 20
C PURPOSE DTCN 30
C A SERIES EXPANSION IN CHEBYSHEV POLYNOMIALS WITH INDEPENDENT DTCN 40
C VARIABLE X IS TRANSFORMED TO A POLYNOMIAL WITH INDEPENDENT DTCN 50
C VARIABLE Z, WHERE X=A*Z+B. DTCN 60
C
C USAGE DTCN 70
C CALL DTCNP(A,B,POL,N,C,WORK) DTCN 80
C
C DESCRIPTION OF PARAMETERS DTCN 100
C A - FACTOR OF LINEAR TERM IN GIVEN LINEAR TRANSFORMATION DTCN 110
C B - CONSTANT TERM IN GIVEN LINEAR TRANSFORMATION DTCN 120
C POL - COEFFICIENT VECTOR OF POLYNOMIAL (RESULTANT VALUE) DTCN 130
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH DTCN 140
C DOUBLE PRECISION VECTOR DTCN 150
C N - DIMENSION OF COEFFICIENT VECTORS POL AND C DTCN 160
C C - GIVEN COEFFICIENT VECTOR OF EXPANSION DTCN 170
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH DTCN 180
C POL AND C MAY BE IDENTICALLY LOCATED DTCN 190
C DOUBLE PRECISION VECTOR DTCN 200
C WORK - WORKING STORAGE OF DIMENSION 2*N DTCN 210
C DTCN 220
C DTCN 230
C
C REMARKS DTCN 240
C COEFFICIENT VECTOR C REMAINS UNCHANGED IF NOT COINCIDING DTCN 250
C WITH COEFFICIENT VECTOR POL. DTCN 260
C OPERATION IS BYPASSED IN CASE N LESS THAN 1. DTCN 270
C THE LINEAR TRANSFORMATION X=A*Z+B OR Z=(1/A)(X-B) TRANSFORMS DTCN 280
C THE RANGE (-1,+1) IN X TO THE RANGE (ZL,ZR) IN Z, WHERE DTCN 290
C ZL=(1+B)/A AND ZR=(1-B)/A. DTCN 300
C FOR GIVEN ZL, ZR WE HAVE A=2/(ZR-ZL) AND B=-(ZR+ZL)/(ZR-ZL) DTCN 310
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DTCN 320
C NONE DTCN 330
C
C METHOD DTCN 340
C THE TRANSFORMATION IS BASED ON THE RECURRENCE EQUATION DTCN 350
C FOR CHEBYSHEV POLYNOMIALS T(N,X) DTCN 360
C T(N+1,X)=2*X*T(N,X)-T(N-1,X), DTCN 370
C WHERE THE FIRST TERM IN BRACKETS IS THE INDEX, DTCN 380
C THE SECOND IS THE ARGUMENT. DTCN 390
C STARTING VALUES ARE T(0,X)=1, T(1,X)=X. DTCN 400
C THE TRANSFORMATION IS IMPLICITLY DEFINED BY MEANS OF DTCN 410
C X = A*Z+B TOGETHER WITH DTCN 420
C SUM(POL(I)*Z**(I-1), SUMMED OVER I FROM 1 TO N) DTCN 430
C =SUM(C(I)*T(I-1,X), SUMMED OVER I FROM 1 TO N). DTCN 440
C
C SUBROUTINE DTCNP(A,B,POL,N,C,WORK) DTCN 450
C DIMENSION POL(1),C(1),WORK(1) DTCN 460
C DOUBLE PRECISION A,B,POL,C,WORK,H,P,XO,XD DTCN 470
C TEST OF DIMENSION DTCN 480
C IF(N-1)2,1,3 DTCN 490
C DIMENSION LESS THAN 2 DTCN 500
C 1 POL(1)=C(1) DTCN 510
C 2 RETURN DTCN 520
C 3 POL(1)=C(1)+C(2)*B DTCN 530
C POL(2)=C(2)*A DTCN 540
C IF(N-2)2,2,4 DTCN 550
C INITIALIZATION DTCN 560
C 4 WORK(1)=1.00 DTCN 570
C WORK(2)=B DTCN 580
C WORK(3)=0.00 DTCN 590
C WORK(4)=A DTCN 600
C XD=A+A DTCN 610
C XO=B+B DTCN 620
C

```

```

C      CALCULATE COEFFICIENT VECTOR OF NEXT CHEBYSHEV POLYNOMIAL
C      AND ADD MULTIPLE OF THIS VECTOR TO POLYNOMIAL POL
      DO 6 J=3,N
      P=0.00
C
      DO 5 K=2,J
      H=P-WORK(2*K-3)+X*WORK(2*K-2)
      P=WORK(2*K-2)
      WORK(2*K-2)=H
      WORK(2*K-3)=P
      POL(K-1)=POL(K-1)+H*C(J)
5     P=X*H
      WORK(2*J-1)=0.00
      WORK(2*J)=P
6     POL(J)=C(J)*P
      RETURN
      END

```

```

DTCN 800
DTCN 810
DTCN 820
DTCN 830
DTCN 840
DTCN 850
DTCN 860
DTCN 870
DTCN 880
DTCN 890
DTCN 900
DTCN 910
DTCN 920
DTCN 930
DTCN 940
DTCN 950
DTCN 960

```

Subroutines CSP and DCSP

These subroutines compute the values of the shifted Chebyshev polynomials for a given argument x and orders zero up to N . The shifted Chebyshev polynomial satisfies the recurrence equation.

$$T_{n+1}^S(x) = 2(2x-1)T_n^S(x) - T_{n-1}^S(x)$$

with starting values $T_0^S(x) = 1$, $T_1^S(x) = 2 \cdot x - 1$. From this equation, it follows immediately that roundoff errors grow at worst linearly under the tacit assumption that the argument values are between zero and one.

If e_{n+r} is the error in $T_{n+r}^S(x)$ due to a single rounding error e in $T_n^S(x)$:

$$e_{n+r+1} = 2(2x-1)e_{n+r} - e_{n+r-1}$$

with initial conditions $e_n = e$, $e_{n-1} = 0$.

The solution of this difference equation has its maximum for $x = 1$ or $x = 0$.

$$e_{n-1} = 0, e_n = e, |e_{n+1}| = 2e, \dots, |e_{n+r}| = (1+r)e.$$

The order is assumed to be zero for negative values of N .

```

C      .....CSP 10
C      .....CSP 20
C      .....CSP 30
C      SUBROUTINE CSP                                CSP 40
C      PURPOSE                                       CSP 50
C      COMPUTE THE VALUES OF THE SHIFTED CHEBYSHEV POLYNOMIALS
C      TS(N,X) FOR ARGUMENT X AND ORDERS 0 UP TO N.  CSP 60
C      .....CSP 70
C      USAGE                                         CSP 80
C      CALL CSP(Y,X,N)                               CSP 90
C      .....CSP 100
C      DESCRIPTION OF PARAMETERS                    CSP 110
C      Y      - RESULT VECTOR OF DIMENSION N+1 CONTAINING THE VALUES
C      OF SHIFTED CHEBYSHEV POLYNOMIALS OF ORDER 0 UP TO N
C      FOR GIVEN ARGUMENT X.                         CSP 120
C      X      - ARGUMENT OF SHIFTED CHEBYSHEV POLYNOMIAL
C      N      - ORDER OF SHIFTED CHEBYSHEV POLYNOMIAL
C      .....CSP 130
C      REMARKS                                       CSP 140
C      N LESS THAN 0 IS TREATED AS IF N WERE 0      CSP 150
C      .....CSP 160
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C      NONE                                          CSP 170
C      .....CSP 180
C      METHOD                                         CSP 190
C      EVALUATION IS BASED ON THE RECURRENCE EQUATION FOR
C      SHIFTED CHEBYSHEV POLYNOMIALS TS(N,X)
C      TS(N+1,X)=4*X*(X-1)*TS(N,X)-TS(N-1,X)
C      WHERE THE FIRST TERM IN BRACKETS IS THE ORDER,
C      THE SECOND IS THE ARGUMENT.
C      STARTING VALUES ARE TS(0,X)=1, TS(1,X)=2*X-1.
C      .....CSP 200
C      .....CSP 210
C      .....CSP 220
C      SUBROUTINE CSP(Y,X,N)                          CSP 230
C      DIMENSION Y(1)                                CSP 240
C      TEST OF ORDER                                 CSP 250
C      Y(1)=1.                                        CSP 260
C      IF(N)1,1,2                                    CSP 270
C      1 RETURN                                       CSP 280
C      2 Y(2)=X+X-1.                                  CSP 290
C      IF(N-1)1,1,3                                  CSP 300
C      .....CSP 310
C      INITIALIZATION                                CSP 320
C      3 F=Y(2)+Y(2)                                  CSP 330
C      .....CSP 340
C      DO 4 I=2,N                                    CSP 350
C      4 Y(I+1)=F*Y(I)-Y(I-1)                         CSP 360
C      RETURN                                         CSP 370
C      END                                           CSP 380
C      .....CSP 390
C      .....CSP 400
C      .....CSP 410
C      .....CSP 420
C      .....CSP 430
C      .....CSP 440
C      .....CSP 450
C      .....CSP 460
C      .....CSP 470
C      .....CSP 480
C      .....CSP 490
C      .....CSP 500
C      .....CSP 510
C      .....CSP 520
C      .....CSP 530
C      .....CSP 540
C      .....CSP 550

```

```

C ..... DSP 10
C SUBROUTINE DCSP ..... DSP 20
C ..... DSP 30
C SUBROUTINE DCSP ..... DSP 40
C ..... DSP 50
C PURPOSE ..... DSP 60
C COMPUTE THE VALUES OF THE SHIFTED CHEBYSHEV POLYNOMIALS ..... DSP 70
C TS(N,X) FOR ARGUMENT X AND ORDERS 0 UP TO N. ..... DSP 80
C ..... DSP 90
C USAGE ..... DSP 100
C CALL DCSP(Y,X,N) ..... DSP 110
C ..... DSP 120
C DESCRIPTION OF PARAMETERS ..... DSP 130
C Y ..... DSP 140
C - RESULT VECTOR OF DIMENSION N+1 CONTAINING THE VALUES ..... DSP 150
C OF SHIFTED CHEBYSHEV POLYNOMIALS OF ORDER 0 UP TO N ..... DSP 160
C FOR GIVEN ARGUMENT X. ..... DSP 170
C DOUBLE PRECISION VECTOR. ..... DSP 180
C VALUES ARE ORDERED FROM LOW TO HIGH ORDER ..... DSP 190
C X ..... DSP 200
C - ARGUMENT OF SHIFTED CHEBYSHEV POLYNOMIAL ..... DSP 210
C DOUBLE PRECISION VARIABLE. ..... DSP 220
C N ..... DSP 230
C - ORDER OF SHIFTED CHEBYSHEV POLYNOMIAL ..... DSP 240
C ..... DSP 250
C REMARKS ..... DSP 260
C N LESS THAN 0 IS TREATED AS IF N WERE 0 ..... DSP 270
C ..... DSP 280
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED ..... DSP 290
C NONE ..... DSP 300
C ..... DSP 310
C METHOD ..... DSP 320
C EVALUATION IS BASED ON THE RECURRENCE EQUATION FOR ..... DSP 330
C SHIFTED CHEBYSHEV POLYNOMIALS TS(N,X) ..... DSP 340
C TS(N+1,X)=(4*X-2)*TS(N,X)-TS(N-1,X). ..... DSP 350
C WHERE THE FIRST TERM IN BRACKETS IS THE ORDER, ..... DSP 360
C THE SECOND IS THE ARGUMENT. ..... DSP 370
C STARTING VALUES ARE TS(0,X)=1, TS(1,X)=2*X-1. ..... DSP 380
C ..... DSP 390
C SUBROUTINE DCSP(Y,X,N) ..... DSP 400
C ..... DSP 410
C DIMENSION Y(1) ..... DSP 420
C DOUBLE PRECISION Y,X,F ..... DSP 430
C ..... DSP 440
C TEST OF ORDER ..... DSP 450
C Y(1)=1,DO ..... DSP 460
C IF(N)1,1,2 ..... DSP 470
C 1 RETURN ..... DSP 480
C ..... DSP 490
C 2 Y(2)=X+X-1,DO ..... DSP 500
C IF(N-1)1,1,3 ..... DSP 510
C ..... DSP 520
C INITIALIZATION ..... DSP 530
C 3 F=Y(2)+Y(2) ..... DSP 540
C ..... DSP 550
C DO 4 I=2,N ..... DSP 560
C 4 Y(I+1)=F*Y(I)-Y(I-1) ..... DSP 570
C RETURN ..... DSP 580
C END ..... DSP 590

```

Subroutines CSPS and DCSPS

These subroutines compute the value of a series expansion in shifted Chebyshev polynomials. The shifted Chebyshev polynomial $T_n^S(x)$ satisfies the recurrence equation

$$T_{n+1}^S(x) = 2(2x-1)T_n^S(x) - T_{n-1}^S(x)$$

with starting values $T_0^S(x) = 1$, $T_1^S(x) = 2x - 1$.

An n-term expansion in shifted Chebyshev polynomials with coefficient vector $C = (c_1, \dots, c_n)$ is evaluated by means of a backward iteration scheme:

$$\text{Arg} = 4x - 2, H_1 = 0, H_0 = 0$$

$$H_2 = H_1$$

$$H_1 = H_0$$

$$H_0 = \text{Arg} \cdot H_1 - H_2 + c_{n-i+1}$$

$$Y = (c_1 - H_2 + H_0)/2.$$

} for $i = 1, \dots, n$

This gives the result $Y(x) = \sum_{i=1}^n c_i T_{i-1}^S(x)$.

Calculation is bypassed in case of a nonpositive value of the dimension n.

```

C ..... CSPS 10
C ..... CSPS 20
C SUBROUTINE CSPS ..... CSPS 30
C ..... CSPS 40
C ..... CSPS 50
C PURPOSE ..... CSPS 60
C COMPUTES THE VALUE OF AN N-TERM EXPANSION IN SHIFTED ..... CSPS 70
C CHEBYSHEV POLYNOMIALS WITH COEFFICIENT VECTOR C ..... CSPS 80
C FOR ARGUMENT VALUE X. ..... CSPS 90
C ..... CSPS 100
C USAGE ..... CSPS 110
C CALL CSPS(Y,X,C,N) ..... CSPS 120
C ..... CSPS 130
C DESCRIPTION OF PARAMETERS ..... CSPS 140
C Y ..... CSPS 150
C - RESULT VALUE ..... CSPS 160
C X ..... CSPS 170
C - ARGUMENT VALUE ..... CSPS 180
C C ..... CSPS 190
C - COEFFICIENT VECTOR OF GIVEN EXPANSION ..... CSPS 200
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH ..... CSPS 210
C N ..... CSPS 220
C - DIMENSION OF COEFFICIENT VECTOR C ..... CSPS 230
C ..... CSPS 240
C REMARKS ..... CSPS 250
C OPERATION IS BYPASSED IN CASE N LESS THAN 1 ..... CSPS 260
C ..... CSPS 270
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED ..... CSPS 280
C NONE ..... CSPS 290
C ..... CSPS 300
C METHOD ..... CSPS 310
C DEFINITION ..... CSPS 320
C Y=SUM(C(I))*TS(I-1,X), SUMMED OVER I FROM 1 TO N. ..... CSPS 330
C EVALUATION IS DONE BY MEANS OF BACKWARD RECURSION ..... CSPS 340
C USING THE RECURRENCE EQUATION FOR SHIFTED ..... CSPS 350
C CHEBYSHEV POLYNOMIALS ..... CSPS 360
C TS(N+1,X)=(4*X-2)*TS(N,X)-TS(N-1,X). ..... CSPS 370
C ..... CSPS 380
C SUBROUTINE CSPS(Y,X,C,N) ..... CSPS 390
C ..... CSPS 400
C DIMENSION C(1) ..... CSPS 410
C ..... CSPS 420
C TEST OF DIMENSION ..... CSPS 430
C IF(N)1,1,2 ..... CSPS 440
C 1 RETURN ..... CSPS 450
C ..... CSPS 460
C 2 IF(N-2)3,4,4 ..... CSPS 470
C 3 Y=C(1) ..... CSPS 480
C RETURN ..... CSPS 490
C ..... CSPS 500
C INITIALIZATION ..... CSPS 510
C 4 ARG=X+X-1. ..... CSPS 520
C ARG=ARG+ARG ..... CSPS 530
C H1=0. ..... CSPS 540
C H0=0. ..... CSPS 550
C ..... CSPS 560
C DO 5 I=1,N ..... CSPS 570
C K=N-I ..... CSPS 580
C H2=H1 ..... CSPS 590
C H1=H0 ..... CSPS 600
C 5 H0=ARG*H1-H2+C(K+1) ..... CSPS 610
C Y=0.5*(C(1)-H2+H0) ..... CSPS 620
C RETURN ..... CSPS 630
C END ..... CSPS 640

```

```

C          DSPS 10
C          ..... DSPS 20
C          SUBROUTINE DCSPS          DSPS 30
C          DSPS 40
C          DSPS 50
C          DSPS 60
C          PURPOSE
C          COMPUTES THE VALUE OF AN N-TERM EXPANSION IN SHIFTED
C          CHEBYSHEV POLYNOMIALS WITH COEFFICIENT VECTOR C
C          FOR ARGUMENT VALUE X.
C          DSPS 70
C          DSPS 80
C          DSPS 90
C          DSPS 100
C          USAGE
C          CALL DCSPS(Y,X,C,N)
C          DSPS 110
C          DSPS 120
C          DSPS 130
C          DESCRIPTION OF PARAMETERS
C          Y - RESULT VALUE
C          DSPS 140
C          X - DOUBLE PRECISION VARIABLE
C          DSPS 150
C          C - ARGUMENT VALUE
C          DSPS 160
C          N - DOUBLE PRECISION VARIABLE
C          DSPS 170
C          C - COEFFICIENT VECTOR OF GIVEN EXPANSION
C          COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
C          DSPS 180
C          N - DOUBLE PRECISION VECTOR
C          DSPS 190
C          N - DIMENSION OF COEFFICIENT VECTOR C
C          DSPS 200
C          DSPS 210
C          DSPS 220
C          REMARKS
C          OPERATION IS BYPASSED IN CASE N LESS THAN 1
C          DSPS 230
C          DSPS 240
C          DSPS 250
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          NONE
C          DSPS 260
C          DSPS 270
C          METHOD
C          DEFINITION
C          Y=SUM(C(I)*TS(I-1,X), SUMMED OVER I FROM 1 TO N).
C          EVALUATION IS DONE BY MEANS OF BACKWARD RECURSION
C          USING THE RECURRENCE EQUATION FOR SHIFTED
C          CHEBYSHEV POLYNOMIALS
C          TS(N+1,X)=(4*X-2)*TS(N,X)-TS(N-1,X).
C          DSPS 280
C          DSPS 290
C          DSPS 300
C          ..... DSPS 380
C          SUBROUTINE DCSPS(Y,X,C,N)
C          DSPS 390
C          DSPS 400
C          DSPS 410
C          DIMENSION C(1)
C          DOUBLE PRECISION C,Y,X,HC,H1,H2,ARG
C          DSPS 420
C          DSPS 430
C          DSPS 440
C          TEST OF DIMENSION
C          IF(N)1,2
C          1 RETURN
C          DSPS 450
C          DSPS 460
C          2 IF(N-2)3,4,4
C          3 Y=C(1)
C          RETURN
C          DSPS 470
C          DSPS 480
C          DSPS 490
C          DSPS 500
C          DSPS 510
C          DSPS 520
C          DSPS 530
C          DSPS 540
C          DSPS 550
C          DSPS 560
C          DSPS 570
C          DSPS 580
C          DSPS 590
C          DSPS 600
C          DSPS 610
C          DSPS 620
C          DSPS 630
C          DSPS 640
C          DSPS 650
C          END

```

Subroutines TCSP and DTCS

These subroutines transform a given series expansion in shifted Chebyshev polynomials to a polynomial. The independent variable x of the given expansion is thereby substituted by the independent variable z of the resulting polynomial using the linear transformation $x = A * z + B$ or $z = (x - B)/A$.

This means:
$$\sum_{i=1}^N C_i * T_{i-1}^S(A * z + B)$$

$$= \sum_{i=1}^N POL_i * z^{i-1}$$

Calculation is bypassed in case of a nonpositive value of the dimension N .

The range $(0, +1)$ in x is transformed to the range (z_L, z_R) in z with $z_L = -B/A$ and $z_R = (1-B)/A$ or vice versa, $A = 1/(z_R - z_L)$ and $B = -z_L/(z_R - z_L)$.

The shifted Chebyshev polynomial $T_n^S(x)$ satisfies the recurrence equation

$$T_{n+1}^S(x) = 4x T_n^S(x) - 2 T_n^S(x) - T_{n-1}^S(x)$$

with starting values $T_0^S(x) = 1$, $T_1^S(x) = 2x - 1$. The transformation is performed by means of a forward iteration scheme:

1. The coefficient vector of the shifted Chebyshev polynomial $T_i^S(x)$ is calculated from the coefficient vectors of $T_{i-1}^S(x)$, $T_{i-2}^S(x)$ using the recurrence equation, for $i = 3, \dots, N$.
2. The resulting polynomial coefficient vector is obtained by summation of c_i times $T_{i-1}^S(x)$ over i , for $i = 1, \dots, N$.

```

C          TCSP 10
C          ..... TCSP 20
C          SUBROUTINE TCSP          TCSP 30
C          TCSP 40
C          TCSP 50
C          PURPOSE
C          A SERIES EXPANSION IN SHIFTED CHEBYSHEV POLYNOMIALS WITH
C          INDEPENDENT VARIABLE X IS TRANSFORMED TO A POLYNOMIAL WITH
C          INDEPENDENT VARIABLE Z, WHERE X=A*Z+B.
C          TCSP 70
C          TCSP 80
C          TCSP 90
C          TCSP 100
C          USAGE
C          CALL TCSP(A,B,POL,N,C,WORK)
C          TCSP 110
C          TCSP 120
C          TCSP 130
C          DESCRIPTION OF PARAMETERS
C          A - FACTOR OF LINEAR TERM IN GIVEN LINEAR TRANSFORMATION
C          TCSP 140
C          B - CONSTANT TERM IN GIVEN LINEAR TRANSFORMATION
C          TCSP 150
C          POL - COEFFICIENT VECTOR OF POLYNOMIAL (RESULTANT VALUE)
C          TCSP 160
C          COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
C          TCSP 170
C          N - DIMENSION OF COEFFICIENT VECTORS POL AND C
C          TCSP 180
C          C - GIVEN COEFFICIENT VECTOR OF EXPANSION
C          COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
C          TCSP 190
C          POL AND C MAY BE IDENTICALLY LOCATED
C          TCSP 200
C          WORK - WORKING STORAGE OF DIMENSION 2*N
C          TCSP 210
C          TCSP 220
C          TCSP 230
C          TCSP 240
C          TCSP 250
C          TCSP 260
C          REMARKS
C          COEFFICIENT VECTOR C REMAINS UNCHANGED IF NOT COINCIDING
C          WITH COEFFICIENT VECTOR POL.
C          TCSP 270
C          OPERATION IS BYPASSED IN CASE N LESS THAN 1.
C          TCSP 280
C          THE LINEAR TRANSFORMATION X=A*Z+B OR Z=(1/A)(X-B) TRANSFORMS
C          THE RANGE (0,1) IN X TO THE RANGE (ZL,ZR) IN Z, WHERE
C          ZL=-B/A AND ZR=(1-B)/A.
C          TCSP 290
C          FOR GIVEN ZL, ZR WE HAVE A=1/(ZR-ZL) AND B=-ZL/(ZR-ZL).
C          TCSP 300
C          TCSP 310
C          TCSP 320
C          TCSP 330
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          NONE
C          TCSP 340
C          TCSP 350
C          TCSP 360
C          TCSP 370
C          METHOD
C          THE TRANSFORMATION IS BASED ON THE RECURRENCE EQUATION FOR
C          SHIFTED CHEBYSHEV POLYNOMIALS TS(N,X)
C          TS(N+1,X)=(4*X-2)*TS(N,X)-TS(N-1,X),
C          WHERE THE FIRST TERM IN BRACKETS IS THE INDEX,
C          TCSP 380
C          TCSP 390
C          TCSP 400
C          TCSP 410
C          TCSP 420

```

```

C          STARTING VALUES ARE TS(0,X)=1, TS(1,X)=2*X-1.
C          THE TRANSFORMATION IS IMPLICITLY DEFINED BY MEANS OF
C          X=A*Z+B TOGETHER WITH
C          SUM(POL(I)*Z***(I-1), SUMMED OVER I FROM 1 TO N)
C          =SUM(C(I)*TS(I-1,X), SUMMED OVER I FROM 1 TO N).
C          .....
C          SUBROUTINE TCSP(A,B,POL,N,C,WORK)
C          DIMENSION POL(1),C(1),WORK(1)
C          TEST OF DIMENSION
C          IF(N-1)2,1,3
C          DIMENSION LESS THAN 2
C          1 POL(1)=C(1)
C          2 RETURN
C          3 XD=A+A
C          XO=B+B-1.
C          POL(1)=C(1)+C(2)*XD
C          POL(2)=C(2)*XD
C          IF(N-2)2,2,4
C          INITIALIZATION
C          4 WORK(1)=1.
C          WORK(2)=XO
C          WORK(3)=0.
C          WORK(4)=XD
C          XD=XO*XD
C          XO=XO*XD
C          CALCULATE COEFFICIENT VECTOR OF NEXT SHIFTED CHEBYSHEV
C          POLYNOMIAL AND ADD MULTIPLE OF THIS VECTOR TO POLYNOMIAL POL
C          DO 6 J=3,N
C          P=0.
C          DO 5 K=2,J
C          H=P-WORK(2*K-3)+XO*WORK(2*K-2)
C          P=WORK(2*K-2)
C          WORK(2*K-2)=H
C          WORK(2*K-3)=P
C          POL(K-1)=POL(K-1)+H*C(J)
C          5 P=XO*P
C          WORK(2*J-1)=0.
C          WORK(2*J)=P
C          6 POL(J)=C(J)*P
C          RETURN
C          END
TCSP 430
TCSP 440
TCSP 450
TCSP 460
TCSP 470
TCSP 480
TCSP 490
TCSP 500
TCSP 510
TCSP 520
TCSP 530
TCSP 540
TCSP 550
TCSP 560
TCSP 570
TCSP 580
TCSP 590
TCSP 600
TCSP 610
TCSP 620
TCSP 630
TCSP 640
TCSP 650
TCSP 660
TCSP 670
TCSP 680
TCSP 690
TCSP 700
TCSP 710
TCSP 720
TCSP 730
TCSP 740
TCSP 750
TCSP 760
TCSP 770
TCSP 780
TCSP 790
TCSP 800
TCSP 810
TCSP 820
TCSP 830
TCSP 840
TCSP 850
TCSP 860
TCSP 870
TCSP 880
TCSP 890
TCSP 900
TCSP 910
TCSP 920

```

```

C          .....
C          SUBROUTINE DTCS
C          DTCS 10
C          .....
C          DTCS 20
C          DTCS 30
C          DTCS 40
C          DTCS 50
C          DTCS 60
C          DTCS 70
C          DTCS 80
C          DTCS 90
C          DTCS 100
C          DTCS 110
C          DTCS 120
C          DTCS 130
C          DTCS 140
C          DTCS 150
C          DTCS 160
C          DTCS 170
C          DTCS 180
C          DTCS 190
C          DTCS 200
C          DTCS 210
C          DTCS 220
C          DTCS 230
C          DTCS 240
C          DTCS 250
C          DTCS 260
C          DTCS 270
C          DTCS 280
C          DTCS 290
C          DTCS 300
C          DTCS 310
C          DTCS 320
C          DTCS 330
C          DTCS 340
C          DTCS 350
C          DTCS 360
C          DTCS 370
C          DTCS 380
C          DTCS 390
C          DTCS 400
C          DTCS 410
C          DTCS 420
C          DTCS 430
C          DTCS 440
C          DTCS 450
C          DTCS 460
C          DTCS 470
C          DTCS 480
C          DTCS 490
C          DTCS 500
C          DTCS 510
C          DTCS 520
C          DTCS 530
C          DTCS 540
C          DTCS 550
C          DTCS 560
C          DTCS 570
C          DTCS 580
C          DTCS 590
C          DTCS 600
C          DTCS 610
C          DTCS 620
C          DTCS 630
C          DTCS 640
C          DTCS 650
C          DTCS 660
C          DTCS 670
C          DTCS 680
C          DTCS 690
C          DTCS 700
C          DTCS 710
C          DTCS 720
C          DTCS 730
C          DTCS 740
C          DTCS 750
C          DTCS 760
C          DTCS 770
C          DTCS 780
C          DTCS 790
C          DTCS 800
C          DTCS 810
C          DTCS 820
C          DTCS 830
C          DTCS 840
C          DTCS 850
C          DTCS 860
C          DTCS 870
C          DTCS 880
C          DTCS 890
C          DTCS 900
C          DTCS 910
C          DTCS 920
C          DTCS 930
C          DTCS 940
C          DTCS 950
C          DTCS 960
C          DTCS 970
C          DTCS 980

```


Subroutines HEP and DHEP

These subroutines compute the values of the Hermite polynomials for a given argument x and orders zero up to N . The Hermite polynomial $H_n(x)$ satisfies the recurrence equation

$$H_{n+1}(x) = 2(x \cdot H_n(x) - n \cdot H_{n-1}(x))$$

with starting values $H_0(x) = 1$, $H_1(x) = 2x$.

The order is assumed to be zero for negative values of N .

```
C
C
C .....
C
C SUBROUTINE HEP
C
C PURPOSE
C   COMPUTE THE VALUES OF THE HERMITE POLYNOMIALS H(N,X)
C   FOR ARGUMENT VALUE X AND ORDERS 0 UP TO N.
C
C USAGE
C   CALL HEP(Y,X,N)
C
C DESCRIPTION OF PARAMETERS
C   Y - RESULT VECTOR OF DIMENSION N+1 CONTAINING THE VALUES
C     OF HERMITE POLYNOMIALS OF ORDER 0 UP TO N
C     FOR GIVEN ARGUMENT X.
C     VALUES ARE ORDERED FROM LOW TO HIGH ORDER
C   X - ARGUMENT OF HERMITE POLYNOMIAL
C   N - ORDER OF HERMITE POLYNOMIAL
C
C REMARKS
C   N LESS THAN 0 IS TREATED AS IF N WERE 0
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C   NONE
C
C METHOD
C   EVALUATION IS BASED ON THE RECURRENCE EQUATION FOR
C   HERMITE POLYNOMIALS H(N,X)
C   H(N+1,X)=2*(X*H(N,X)-N*H(N-1,X))
C   WHERE THE FIRST TERM IN BRACKETS IS THE INDEX,
C   THE SECOND IS THE ARGUMENT.
C   STARTING VALUES ARE H(0,X)=1, H(1,X)=2*X.
C .....
C
C SUBROUTINE HEP(Y,X,N)
C
C DIMENSION Y(1)
C
C TEST OF ORDER
C   Y(1)=1.
C   IF(N)1,1,2
C 1 RETURN
C
C 2 Y(2)=X+X
C   IF(N-1)1,1,3
C
C 3 DO 4, I=2,N
C   F=X*Y(I)-FLOAT(I-1)*Y(I-1)
C 4 Y(I+1)=F+F
C RETURN
C END
HEP 10
HEP 20
HEP 30
HEP 40
HEP 50
HEP 60
HEP 70
HEP 80
HEP 90
HEP 100
HEP 110
HEP 120
HEP 130
HEP 140
HEP 150
HEP 160
HEP 170
HEP 180
HEP 190
HEP 200
HEP 210
HEP 220
HEP 230
HEP 240
HEP 250
HEP 260
HEP 270
HEP 280
HEP 290
HEP 300
HEP 310
HEP 320
HEP 330
HEP 340
HEP 350
HEP 360
HEP 370
HEP 380
HEP 390
HEP 400
HEP 410
HEP 420
HEP 430
HEP 440
HEP 450
HEP 460
HEP 470
HEP 480
HEP 490
HEP 500
HEP 510
HEP 520
HEP 530
```

```
C
C .....
C
C SUBROUTINE DHEP
C
C PURPOSE
C   COMPUTE THE VALUES OF THE HERMITE POLYNOMIALS H(N,X)
C   FOR ARGUMENT VALUE X AND ORDERS 0 UP TO N.
C
C USAGE
C   CALL DHEP(Y,X,N)
C
C DESCRIPTION OF PARAMETERS
C   Y - RESULT VECTOR OF DIMENSION N+1 CONTAINING THE VALUES
C     OF HERMITE POLYNOMIALS OF ORDER 0 UP TO N
C     FOR GIVEN ARGUMENT X.
C     DOUBLE PRECISION VECTOR.
C     VALUES ARE ORDERED FROM LOW TO HIGH ORDER
C   X - ARGUMENT OF HERMITE POLYNOMIAL
C     DOUBLE PRECISION VARIABLE.
C   N - ORDER OF HERMITE POLYNOMIAL
C
C REMARKS
C   N LESS THAN 0 IS TREATED AS IF N WERE 0
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C   NONE
C
C METHOD
C   EVALUATION IS BASED ON THE RECURRENCE EQUATION FOR
C   HERMITE POLYNOMIALS H(N,X)
C   H(N+1,X)=2*(X*H(N,X)-N*H(N-1,X))
C   WHERE THE FIRST TERM IN BRACKETS IS THE INDEX,
C   THE SECOND IS THE ARGUMENT.
C   STARTING VALUES ARE H(0,X)=1, H(1,X)=2*X.
C .....
C
C SUBROUTINE DHEP(Y,X,N)
C
C DIMENSION Y(1)
C DOUBLE PRECISION Y,X,F
C
C TEST OF ORDER
C   Y(1)=1.00
C   IF(N)1,1,2
C 1 RETURN
C
C 2 Y(2)=X+X
C   IF(N-1)1,1,3
C
C 3 DO 4, I=2,N
C   F=X*Y(I)-DFLOAT(I-1)*Y(I-1)
C 4 Y(I+1)=F+F
C RETURN
C END
DHP 10
DHP 20
DHP 30
DHP 40
DHP 50
DHP 60
DHP 70
DHP 80
DHP 90
DHP 100
DHP 110
DHP 120
DHP 130
DHP 140
DHP 150
DHP 160
DHP 170
DHP 180
DHP 190
DHP 200
DHP 210
DHP 220
DHP 230
DHP 240
DHP 250
DHP 260
DHP 270
DHP 280
DHP 290
DHP 300
DHP 310
DHP 320
DHP 330
DHP 340
DHP 350
DHP 360
DHP 370
DHP 380
DHP 390
DHP 400
DHP 410
DHP 420
DHP 430
DHP 440
DHP 450
DHP 460
DHP 470
DHP 480
DHP 490
DHP 500
DHP 510
DHP 520
DHP 530
DHP 540
DHP 550
```

Subroutines HEPS and DHEPS

These subroutines compute the value of a series expansion in Hermite polynomials. The Hermite polynomial $H_n(x)$ satisfies the recurrence equation

$$H_{n+1}(x) = 2(x \cdot H_n(x) - n \cdot H_{n-1}(x))$$

with starting values $H_0(x) = 1$, $H_1(x) = 2x$.

An n-term expansion in Hermite polynomials with coefficient vector $C = (c_1, \dots, c_n)$ is evaluated by means of a forward iteration scheme:

$$\left. \begin{aligned} Y &= c_1, H_0 = 1, H_1 = 2 \cdot x \\ H_2 &= x \cdot H_1 - (i-1) H_0 \\ H_0 &= H_1 \\ H_1 &= H_2 + H_2 \\ Y &= Y + c_i \cdot H_0 \end{aligned} \right\} \text{ for } i=2, \dots, n$$

This gives the result $Y(x) = \sum_{i=1}^n c_i \cdot H_{i-1}(x)$.

Calculation is bypassed in case of a nonpositive value of the dimension n.

```

C                                     HEPS 10
C .....                             HEPS 20
C                                     HEPS 30
C SUBROUTINE HEPS                     HEPS 40
C                                     HEPS 50
C PURPOSE                             HEPS 60
C COMPUTES THE VALUE OF AN N-TERM EXPANSION IN HERMITE
C POLYNOMIALS WITH COEFFICIENT VECTOR C FOR ARGUMENT VALUE X. HEPS 70
C                                     HEPS 80
C USAGE                               HEPS 90
C CALL HEPS(Y,X,C,N)                 HEPS 100
C                                     HEPS 110
C DESCRIPTION OF PARAMETERS          HEPS 120
C Y - RESULT VALUE                   HEPS 130
C X - ARGUMENT VALUE                 HEPS 140
C C - COEFFICIENT VECTOR OF GIVEN EXPANSION HEPS 150
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH HEPS 170
C N - DIMENSION OF COEFFICIENT VECTOR C HEPS 180
C                                     HEPS 190
C REMARKS                             HEPS 200
C OPERATION IS BYPASSED IN CASE N LESS THAN 1 HEPS 210
C                                     HEPS 220
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED HEPS 230
C NONE                               HEPS 240
C                                     HEPS 250
C METHOD                               HEPS 260
C DEFINITION                         HEPS 270
C Y=SUM(C(I)*H(I-1,X), SUMMED OVER I FROM 1 TO N). HEPS 280
C EVALUATION IS DONE BY MEANS OF UPWARD RECURSION HEPS 290
C USING THE RECURRENCE EQUATION FOR HERMITE POLYNOMIALS HEPS 300
C H(N+1,X)=2*(X*H(N,X)-N*H(N-1,X)). HEPS 310
C                                     HEPS 320
C .....                             HEPS 330
C SUBROUTINE HEPS(Y,X,C,N)           HEPS 340
C                                     HEPS 350
C DIMENSION C(1)                     HEPS 360
C                                     HEPS 370
C TEST OF DIMENSION                 HEPS 380
C IF(N)1,1,2                         HEPS 390
C 1 RETURN                            HEPS 400
C                                     HEPS 410
C 2 Y=C(1)                            HEPS 420
C IF(N-2)1,3,3                       HEPS 430
C                                     HEPS 440
C INITIALIZATION                    HEPS 450
C 3 HO=1. DO                           HEPS 460
C H1=X+X                               HEPS 470
C                                     HEPS 480
C DO 4 I=2,N                          HEPS 490
C H2=X*H1-FLOAT(I-1)*HO               HEPS 500
C HO=H1                                HEPS 510
C H1=H2+H2                             HEPS 520
C 4 Y=Y+C(I)*HO                       HEPS 530
C RETURN                              HEPS 540
C END                                  HEPS 550
C                                     HEPS 560

```

```

C                                     DHPS 10
C .....                             DHPS 20
C                                     DHPS 30
C SUBROUTINE DHEPS                   DHPS 40
C                                     DHPS 50
C PURPOSE                             DHPS 60
C COMPUTES THE VALUE OF AN N-TERM EXPANSION IN HERMITE
C POLYNOMIALS WITH COEFFICIENT VECTOR C FOR ARGUMENT VALUE X. DHPS 70
C                                     DHPS 80
C USAGE                               DHPS 90
C CALL DHEPS(Y,X,C,N)               DHPS 100
C                                     DHPS 110
C DESCRIPTION OF PARAMETERS          DHPS 120
C Y - RESULT VALUE                   DHPS 130
C X - ARGUMENT VALUE                 DHPS 140
C C - COEFFICIENT VECTOR OF GIVEN EXPANSION DHPS 150
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH DHPS 170
C N - DIMENSION OF COEFFICIENT VECTOR C DHPS 180
C                                     DHPS 190
C REMARKS                             DHPS 200
C OPERATION IS BYPASSED IN CASE N LESS THAN 1 DHPS 210
C                                     DHPS 220
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DHPS 230
C NONE                               DHPS 240
C                                     DHPS 250
C METHOD                               DHPS 260
C DEFINITION                         DHPS 270
C Y=SUM(C(I)*H(I-1,X), SUMMED OVER I FROM 1 TO N). DHPS 280
C EVALUATION IS DONE BY MEANS OF UPWARD RECURSION DHPS 290
C USING THE RECURRENCE EQUATION FOR HERMITE POLYNOMIALS DHPS 300
C H(N+1,X)=2*(X*H(N,X)-N*H(N-1,X)). DHPS 310
C                                     DHPS 320
C .....                             DHPS 330
C SUBROUTINE DHEPS(Y,X,C,N)         DHPS 340
C                                     DHPS 350
C DIMENSION C(1)                     DHPS 360
C DOUBLE PRECISION C,Y,X,HO,H1,H2    DHPS 370
C                                     DHPS 380
C TEST OF DIMENSION                 DHPS 390
C IF(N)1,1,2                         DHPS 400
C 1 RETURN                            DHPS 410
C                                     DHPS 420
C 2 Y=C(1)                            DHPS 430
C IF(N-2)1,3,3                       DHPS 440
C                                     DHPS 450
C INITIALIZATION                    DHPS 460
C 3 HO=1. DO                           DHPS 470
C H1=X+X                               DHPS 480
C                                     DHPS 490
C DO 4 I=2,N                          DHPS 500
C H2=X*H1-DFLOAT(I-1)*HO             DHPS 510
C HO=H1                                DHPS 520
C H1=H2+H2                             DHPS 530
C 4 Y=Y+C(I)*HO                       DHPS 540
C RETURN                              DHPS 550
C END                                  DHPS 560

```

Subroutines THEP and DTHEP

These subroutines transform a given series expansion in Hermite polynomials to a polynomial. The independent variable x of the given expansion is thereby substituted by the independent variable z of the resulting polynomial using the linear transformation $x = A * z + B$ or $z = (x-B)/A$.

This means:
$$\sum_{i=1}^N C_i * H_{i-1} (A * z + B) = \sum_{i=1}^N POL_i * z^{i-1}$$

Calculation is bypassed in case of a nonpositive value of the dimension N.

The range (-c, + c) in x is transformed to the range (z_l, z_r) in z with z_l = - (c + B)/A and z_r = (c-B)/A, or vice versa, A = 2 c / (z_r - z_l) and B = - c (z_r + z_l) / (z_r - z_l).

The Hermite polynomial H_n(x) satisfies the recurrence equation

$$H_{n+1}(x) = 2 (x \cdot H_n(x) - n \cdot H_{n-1}(x))$$

with starting values H₀(x) = 1, H₁(x) = 2 x.

The transformation is performed by means of a forward iteration scheme:

1. The coefficient vector of the Hermite polynomial H_i(x) is calculated from the coefficient vectors of H_{i-1}(x), H_{i-2}(x) using the recurrence equation, for i = 3, . . . , N.
2. The resulting polynomial coefficient vector is obtained by summation of c_i times coefficient vector of H_{i-1}(x) over i, for i = 1, . . . , N.

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```

Subroutines LAP and DLAP

These subroutines compute the values of the normalized Laguerre polynomials for a given argument x and orders zero up to N. The polynomial $L_n(x)/n!$, termed $L_n(x)$ below, satisfies the recurrence equation

$$L_{n+1}(x) = \left[(2n+1-x)L_n(x) - nL_{n-1}(x) \right] / (n+1)$$

with starting values $L_0(x) = 1$, $L_1(x) = 1 - x$. For reasons of economy and numerical stability the recurrence equation is used in the form

$$L_{n+1}(x) = L_n(x) - L_{n-1}(x) + L_n(x) - \left[(1+x)L_n(x) - L_{n-1}(x) \right] / (n+1).$$

For large values of n the last term is negligible, giving the approximation

$$L_{n+1}(x) = 2L_n(x) - L_{n-1}(x).$$

This form shows that roundoff errors grow at worst linearly as long as x is small compared to n.

If e_{n+r} is the error in $L_{n+r}(x)$ due to a single rounding error e in $L_n(x)$, the approximation is:

$$e_{n+r+1} = 2 \cdot e_{n+r} - e_{n+r-1}$$

with initial conditions $e_n = e$, $e_{n-1} = 0$. This implies:

$$e_{n+1} = 2e, e_{n+2} = 3 \cdot e, \dots, e_{n+r} = (r+1)e$$

The order is assumed to be zero for negative values of N.

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```

```

SUBROUTINE LAP(Y,X,N)
DIMENSION Y(1)
TEST OF ORDER
Y(1)=1
IF(N)1,1,2
1 RETURN
2 Y(2)=1.-X
IF(N-1)1,1,3
INITIALIZATION
3 T=1.*X
DO 4 I=2,N
4 Y(I+1)=Y(I)-Y(I-1)+Y(I)-(T*Y(I)-Y(I-1))/FLOAT(I)
RETURN
END

```

```

LAP 370
LAP 380
LAP 390
LAP 400
LAP 410
LAP 420
LAP 430
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LAP 470
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LAP 500
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LAP 520
LAP 530
LAP 540
LAP 550

```

Subroutines LAPS and DLAPS

These subroutines compute the value of a series expansion in normalized Laguerre polynomials. The polynomial $L_n(x)/n!$, termed $L_n(x)$ below, satisfies the recurrence equation

$$L_{n+1}(x) = 2 \cdot L_n(x) - L_{n-1}(x) - \left[(1+x) \cdot L_n(x) - L_{n-1}(x) \right] / (n+1)$$

with starting values $L_0(x) = 1$, $L_1(x) = 1-x$.

An n -term expansion in Laguerre polynomials with coefficient vector $C = (c_1, \dots, c_n)$ is evaluated by means of a forward iteration scheme:

$$\begin{aligned}
 Y &= c_1, H_0 = 1, H_1 = 1-x, T = 1-x \\
 H_2 &= H_1 - H_0 + H_1 - (T \cdot H_1 - H_0)/i \\
 H_0 &= H_1 \\
 H_1 &= H_2 \\
 Y &= Y + c_i \cdot H_0
 \end{aligned}
 \left. \vphantom{\begin{aligned} Y \\ H_2 \\ H_0 \\ H_1 \\ Y \end{aligned}} \right\} \text{for } i=2, \dots, n$$

This gives the result $Y(x) = \sum_{i=1}^n c_i \cdot L_{i-1}(x)$.

Calculation is bypassed in case of a nonpositive value of the dimension n .

```

SUBROUTINE DLAP
PURPOSE
COMPUTE THE VALUES OF THE LAGUERRE POLYNOMIALS L(N,X)
FOR GIVEN ARGUMENT X AND ORDERS 0 UP TO N.
USAGE
CALL DLAP(Y,X,N)
DESCRIPTION OF PARAMETERS
Y - RESULT VECTOR OF DIMENSION N+1 CONTAINING THE VALUES
OF LAGUERRE POLYNOMIALS OF ORDER 0 UP TO N
FOR GIVEN ARGUMENT X.
X - ARGUMENT OF LAGUERRE POLYNOMIAL
N - ORDER OF LAGUERRE POLYNOMIAL
REMARKS
N LESS THAN 0 IS TREATED AS IF N WERE 0
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
EVALUATION IS BASED ON THE RECURRENCE EQUATION FOR
LAGUERRE POLYNOMIALS L(N,X)
L(N+1,X)=2*L(N,X)-L(N-1,X)-((1+X)*L(N,X)-L(N-1,X))/(N+1),
WHERE THE FIRST TERM IN BRACKETS IS THE ORDER,
THE SECOND IS THE ARGUMENT.
STARTING VALUES ARE L(0,X)=1, L(1,X)=1.-X.
SUBROUTINE DLAP(Y,X,N)
DIMENSION Y(1)
DOUBLE PRECISION Y,X,T
TEST OF ORDER
Y(1)=1.00
IF(N)1,1,2
1 RETURN
2 Y(2)=1.00-X
IF(N-1)1,1,3
INITIALIZATION
3 T=1.00*X
DO 4 I=2,N
4 Y(I+1)=Y(I)-Y(I-1)+Y(I)-(T*Y(I)-Y(I-1))/FLOAT(I)
RETURN
END

```

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C ..... DAPS 1000

```

Subroutines TLAP and DTLAP

These subroutines transform a given series expansion in Laguerre polynomials to a polynomial. The independent variable x of the given expansion is thereby substituted by the independent variable z of the resulting polynomial using the linear transformation $x = A * z + B$ or $z = (x-B)/A$.

$$\begin{aligned} \text{This means: } & \sum_{i=1}^N C_i * L_{i-1}(A * z + B) \\ & = \sum_{i=1}^N \text{POL}_i * z^{i-1} \end{aligned}$$

Calculation is bypassed in case of a nonpositive value of the dimension N .

The range $(0, c)$ in x is transformed to the range (z_1, z_T) in z with $z_1 = -B/A$ and $z_T = (c - B)/A$, or vice versa, $A = c/(z_T - z_1)$ and $B = -c * z_1/(z_T - z_1)$.

The Laguerre polynomial $L_n(x)$ satisfies the recurrence equation

$$\begin{aligned} L_{n+1}(x) = & x/(n+1) * L_n(x) + \left[2 - 1/(n+1) \right] L_n(x) - \\ & \left[1 - 1/(n+1) \right] L_{n-1}(x) \end{aligned}$$

with starting values $L_0(x) = 1$, $L_1(x) = 1 - x$.

The transformation is performed by means of a forward iteration scheme:

1. The coefficient vector of the Laguerre polynomial $L_i(x)$ is calculated from the coefficient vectors of $L_{i-1}(x)$, $L_{i-2}(x)$ using the recurrence equation, for $i = 3, \dots, N$.

2. The resulting polynomial coefficient vector is obtained by summation of c_i times $L_{i-1}(x)$ over i , for $i = 1, \dots, N$.

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SUBROUTINE TLAP
PURPOSE
A SERIES EXPANSION IN LAGUERRE POLYNOMIALS WITH INDEPENDENT
VARIABLE X IS TRANSFORMED TO A POLYNOMIAL WITH INDEPENDENT
VARIABLE Z, WHERE X=A*Z+B
USAGE
CALL TLAP(A,B,POL,N,C,WORK)
DESCRIPTION OF PARAMETERS
A - FACTOR OF LINEAR TERM IN GIVEN LINEAR TRANSFORMATION
B - CONSTANT TERM IN GIVEN LINEAR TRANSFORMATION
POL - COEFFICIENT VECTOR OF POLYNOMIAL (RESULTANT VALUE)
COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
N - DIMENSION OF COEFFICIENT VECTORS POL AND C
C - GIVEN COEFFICIENT VECTOR OF EXPANSION
COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
POL AND C MAY BE IDENTICALLY LOCATED
WORK - WORKING STORAGE OF DIMENSION 2*N
REMARKS
COEFFICIENT VECTOR C REMAINS UNCHANGED IF NOT COINCIDING
WITH COEFFICIENT VECTOR POL.
OPERATION IS BYPASSED IN CASE N LESS THAN 1.
THE LINEAR TRANSFORMATION X=A*Z+B OR Z=(1/A)(X-B) TRANSFORMS
THE RANGE (0,C) IN X TO THE RANGE (ZL,ZR) IN Z, WHERE
ZL=-B/A AND ZR=(C-B)/A.
FOR GIVEN ZL, ZR AND C WE HAVE A=C/(ZR-ZL) AND
B=-C*ZL/(ZR-ZL)
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
THE TRANSFORMATION IS BASED ON THE RECURRENCE EQUATION
FOR LAGUERRE POLYNOMIALS  $L(N,X)$ 
 $L(N+1,X)=2*L(N,X)-L(N-1,X)-((1+X)*L(N,X)-L(N-1,X))/(N+1)$ ,
WHERE THE FIRST TERM IN BRACKETS IS THE INDEX,
THE SECOND IS THE ARGUMENT.
STARTING VALUES ARE L(0,X)=1, L(1,X)=1-X.
THE TRANSFORMATION IS IMPLICITLY DEFINED BY MEANS OF
X=A*Z+B TOGETHER WITH
SUM(POL(I)*Z**(I-1), SUMMED OVER I FROM 1 TO N)
=SUM(C(I)*L(I-1,X), SUMMED OVER I FROM 1 TO N).
SUBROUTINE TLAP(A,B,POL,N,C,WORK)
DIMENSION POL(1),C(1),WORK(1)
TEST OF DIMENSION
IF(N-1)2,1,3
DIMENSION LESS THAN 2
1 POL(1)=C(1)
2 RETURN
3 POL(1)=C(1)+C(2)-B*C(2)
POL(2)=-C(2)*A
IF(N-2)2,2,4
INITIALIZATION
4 WORK(1)=1.
WORK(2)=1.00-B
WORK(3)=0.
WORK(4)=-A
FI=1.
CALCULATE COEFFICIENT VECTOR OF NEXT LAGUERRE POLYNOMIAL
AND ADD MULTIPLE OF THIS VECTOR TO POLYNOMIAL POL
DO 6 J=3,N
FI=FI+1.
Q1=Q-L.
Q2=1.-Q1-B*Q
Q=Q*A
P=0.
DO 5 K=2,J
H=-P*Q+WORK(2*K-2)*Q2+WORK(2*K-3)*Q1
P=WORK(2*K-2)
WORK(2*K-2)=H
WORK(2*K-3)=P
5 POL(K-1)=POL(K-1)+H*C(J)
WORK(2*J-1)=0.
WORK(2*J)=-Q*P
6 POL(J)=C(J)+WORK(2*J)
RETURN
END

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C ..... DTLA 160
C ..... DTLA 170
C ..... DTLA 180
C ..... DTLA 190
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C ..... DTLA 210
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C ..... DTLA 360
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C ..... DTLA 380
C ..... DTLA 390
C ..... DTLA 400
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C ..... DTLA 460
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C ..... DTLA 480
C ..... DTLA 490
C ..... DTLA 500
C ..... DTLA 510
C ..... DTLA 520
C ..... DTLA 530
C ..... DTLA 540
C ..... DTLA 550
C ..... DTLA 560
C ..... DTLA 570
C ..... DTLA 580
C ..... DTLA 590
C ..... DTLA 600
C ..... DTLA 610
C ..... DTLA 620
C ..... DTLA 630
C ..... DTLA 640
C ..... DTLA 650
C ..... DTLA 660
C ..... DTLA 670
C ..... DTLA 680
C ..... DTLA 690
C ..... DTLA 700
C ..... DTLA 710
C ..... DTLA 720
C ..... DTLA 730
C ..... DTLA 740
C ..... DTLA 750
C ..... DTLA 760
C ..... DTLA 770
C ..... DTLA 780
C ..... DTLA 790
C ..... DTLA 800
C ..... DTLA 810
C ..... DTLA 820
C ..... DTLA 830
C ..... DTLA 840
C ..... DTLA 850
C ..... DTLA 860
C ..... DTLA 870
C ..... DTLA 880
C ..... DTLA 890
C ..... DTLA 900
C ..... DTLA 910
C ..... DTLA 920
C ..... DTLA 930
C ..... DTLA 940
C ..... DTLA 950
C ..... DTLA 960
C ..... DTLA 970
C ..... DTLA 980
C ..... DTLA 990
C ..... DTLA1000
SUBROUTINE DTLAP
PURPOSE
A SERIES EXPANSION IN LAGUERRE POLYNOMIALS WITH INDEPENDENT
VARIABLE X IS TRANSFORMED TO A POLYNOMIAL WITH INDEPENDENT
VARIABLE Z, WHERE X=A*Z+B
USAGE
CALL DTLAP(A,B,POL,N,C,WORK)
DESCRIPTION OF PARAMETERS
A - FACTOR OF LINEAR TERM IN GIVEN LINEAR TRANSFORMATION
DOUBLE PRECISION VARIABLE
B - CONSTANT TERM IN GIVEN LINEAR TRANSFORMATION
DOUBLE PRECISION VARIABLE
POL - COEFFICIENT VECTOR OF POLYNOMIAL (RESULTANT VALUE)
COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
DOUBLE PRECISION VECTOR
N - DIMENSION OF COEFFICIENT VECTORS POL AND C
C - GIVEN COEFFICIENT VECTOR OF EXPANSION
COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
POL AND C MAY BE IDENTICALLY LOCATED
DOUBLE PRECISION VECTOR
WORK - WORKING STORAGE OF DIMENSION 2*N
DOUBLE PRECISION ARRAY
REMARKS
COEFFICIENT VECTOR C REMAINS UNCHANGED IF NOT COINCIDING
WITH COEFFICIENT VECTOR POL.
OPERATION IS BYPASSED IN CASE N LESS THAN 1.
THE LINEAR TRANSFORMATION X=A*Z+B OR Z=(1/A)(X-B) TRANSFORMS
THE RANGE (0,C) IN X TO THE RANGE (ZL,ZR) IN Z, WHERE
ZL=-B/A AND ZR=(C-B)/A.
FOR GIVEN ZL, ZR AND C WE HAVE A=C/(ZR-ZL) AND
B=-C*ZL/(ZR-ZL)
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
THE TRANSFORMATION IS BASED ON THE RECURRENCE EQUATION
FOR LAGUERRE POLYNOMIALS  $L(N,X)$ 
 $L(N+1,X)=2*L(N,X)-L(N-1,X)-((1+X)*L(N,X)-L(N-1,X))/(N+1)$ ,
WHERE THE FIRST TERM IN BRACKETS IS THE INDEX,
THE SECOND IS THE ARGUMENT.
STARTING VALUES ARE L(0,X)=1, L(1,X)=1-X.
THE TRANSFORMATION IS IMPLICITLY DEFINED BY MEANS OF
X=A*Z+B TOGETHER WITH
SUM(POL(I)*Z**(I-1), SUMMED OVER I FROM 1 TO N)
=SUM(C(I)*L(I-1,X), SUMMED OVER I FROM 1 TO N).
SUBROUTINE DTLAP(A,B,POL,N,C,WORK)
DIMENSION POL(1),C(1),WORK(1)
DOUBLE PRECISION A,B,POL,C,WORK,H,P,Q1,Q2,FI
TEST OF DIMENSION
IF(N-1)2,1,3
DIMENSION LESS THAN 2
1 POL(1)=C(1)
2 RETURN
3 POL(1)=C(1)+C(2)-B*C(2)
POL(2)=-C(2)*A
IF(N-2)2,2,4
INITIALIZATION
4 WORK(1)=1.00
WORK(2)=1.00-B
WORK(3)=0.00
WORK(4)=-A
FI=1.00
CALCULATE COEFFICIENT VECTOR OF NEXT LAGUERRE POLYNOMIAL
AND ADD MULTIPLE OF THIS VECTOR TO POLYNOMIAL POL
DO 6 J=3,N
FI=FI+1.00
Q1=1.00/FI
Q1=Q-L.00
Q2=1.00-Q1-B*Q
Q=Q*A
P=0.00
DO 5 K=2,J
H=-P*Q+WORK(2*K-2)*Q2+WORK(2*K-3)*Q1
P=WORK(2*K-2)
WORK(2*K-2)=H
WORK(2*K-3)=P
5 POL(K-1)=POL(K-1)+H*C(J)
WORK(2*J-1)=0.00
WORK(2*J)=-Q*P
6 POL(J)=C(J)+WORK(2*J)
RETURN
END

```

Subroutines LEP and DLEP

These subroutines compute the values of the Legendre polynomials for a given argument x and orders zero up to N . The Legendre polynomial $P_n(x)$ satisfies the recurrence equation

$$P_{n+1}(x) = ((2n+1) \cdot x \cdot P_n(x) - n \cdot P_{n-1}(x)) / (n+1)$$

with starting values $P_0(x) = 1$, $P_1(x) = x$.

For reasons of economy and numerical stability the recurrence equation is used in the form:

$$P_{n+1}(x) = x \cdot P_n(x) - P_{n-1}(x) + x \cdot P_n(x) - (x \cdot P_n(x) - P_{n-1}(x)) / (n+1)$$

For large values of n the last term is negligible, giving the approximation:

$$P_{n+1}(x) = 2 \cdot x \cdot P_n(x) - P_{n-1}(x)$$

This form shows that roundoff errors grow at worst linearly, assuming that the argument x is absolutely less than one.

If e_{n+r} is the error in $P_{n+r}(x)$ due to a single rounding error e in $P_n(x)$, the approximation is

$$e_{n+r+1} = 2x \cdot e_{n+r} - e_{n+r-1}$$

with initial conditions $e_n = e$, $e_{n-1} = 0$. The solution of this difference equation has its maximum for $|x| = 1$:

$$e_{n-1} = 0, e_n = e, |e_{n+1}| = 2e, \dots, |e_{n+r}| = (r+1)e$$

The order is assumed to be zero for negative values of N .

```

C
C
C .....LEP 10
C .....LEP 20
C .....LEP 30
C .....LEP 40
C .....LEP 50
C .....LEP 60
SUBROUTINE LEP
C .....LEP 70
C .....LEP 80
C .....LEP 90
PURPOSE
C .....LEP 100
C .....LEP 110
C .....LEP 120
C .....LEP 130
C .....LEP 140
C .....LEP 150
C .....LEP 160
C .....LEP 170
C .....LEP 180
C .....LEP 190
C .....LEP 200
C .....LEP 210
C .....LEP 220
C .....LEP 230
C .....LEP 240
C .....LEP 250
C .....LEP 260
C .....LEP 270
C .....LEP 280
C .....LEP 290
C .....LEP 300
C .....LEP 310
C .....LEP 320
C .....LEP 330
C .....LEP 340
C .....LEP 350
C .....LEP 360
C .....LEP 370
C .....LEP 380
C .....LEP 390
C .....LEP 400
C .....LEP 410
C .....LEP 420
C .....LEP 430
C .....LEP 440
C .....LEP 450
C .....LEP 460
C .....LEP 470
C .....LEP 480
C .....LEP 490
C .....LEP 500
C .....LEP 510
C .....LEP 520
C .....LEP 530
END

```

```

C
C
C .....DEP 10
C .....DEP 20
C .....DEP 30
C .....DEP 40
C .....DEP 50
C .....DEP 60
C .....DEP 70
C .....DEP 80
C .....DEP 90
C .....DEP 100
C .....DEP 110
C .....DEP 120
C .....DEP 130
C .....DEP 140
C .....DEP 150
C .....DEP 160
C .....DEP 170
C .....DEP 180
C .....DEP 190
C .....DEP 200
C .....DEP 210
C .....DEP 220
C .....DEP 230
C .....DEP 240
C .....DEP 250
C .....DEP 260
C .....DEP 270
C .....DEP 280
C .....DEP 290
C .....DEP 300
C .....DEP 310
C .....DEP 320
C .....DEP 330
C .....DEP 340
C .....DEP 350
C .....DEP 360
C .....DEP 370
C .....DEP 380
C .....DEP 390
C .....DEP 400
C .....DEP 410
C .....DEP 420
C .....DEP 430
C .....DEP 440
C .....DEP 450
C .....DEP 460
C .....DEP 470
C .....DEP 480
C .....DEP 490
C .....DEP 500
C .....DEP 510
C .....DEP 520
C .....DEP 530
C .....DEP 540
C .....DEP 550
C .....DEP 560
END

```


Subroutines LEPS and DLEPS

These subroutines compute the value of a series expansion in Legendre polynomials. The Legendre polynomial $P_n(x)$ satisfies the recurrence equation

$$P_{n+1}(x) = 2x \cdot P_n(x) - P_{n-1}(x) - (x \cdot P_n(x) - P_{n-1}(x))/(n+1)$$

with starting values $P_0(x) = 1$, $P_1(x) = x$.

An n-term expansion in Legendre polynomials with coefficient vector $C = (c_1, \dots, c_n)$ is evaluated by means of a forward iteration scheme:

$$\left. \begin{aligned} Y &= c_1, H_0 = 1, H_1 = x \\ H_2 &= x \cdot H_1 \\ H_2 &= H_2 - H_0 + H_2 - (H_2 - H_0)/i \\ H_0 &= H_1 \\ H_1 &= H_2 \\ Y &= Y + c_i \cdot H_0 \end{aligned} \right\} \text{for } i = 2, \dots, n$$

$$\text{This gives the result } Y(x) = \sum_{i=1}^n c_i \cdot P_{i-1}(x).$$

Calculation is bypassed in case of a nonpositive value of the dimension N.

```

C ..... LEPS 10
C ..... LEPS 20
C ..... LEPS 30
C ..... LEPS 40
C ..... LEPS 50
C ..... LEPS 60
C ..... LEPS 70
C ..... LEPS 80
C ..... LEPS 90
C ..... LEPS 100
C ..... LEPS 110
C ..... LEPS 120
C ..... LEPS 130
C ..... LEPS 140
C ..... LEPS 150
C ..... LEPS 160
C ..... LEPS 170
C ..... LEPS 180
C ..... LEPS 190
C ..... LEPS 200
C ..... LEPS 210
C ..... LEPS 220
C ..... LEPS 230
C ..... LEPS 240
C ..... LEPS 250
C ..... LEPS 260
C ..... LEPS 270
C ..... LEPS 280
C ..... LEPS 290
C ..... LEPS 300
C ..... LEPS 310
C ..... LEPS 320
C ..... LEPS 330
C ..... LEPS 340
C ..... LEPS 350
C ..... LEPS 360
C ..... LEPS 370
C ..... LEPS 380
C ..... LEPS 390
C ..... LEPS 400
C ..... LEPS 410
C ..... LEPS 420
C ..... LEPS 430
C ..... LEPS 440
C ..... LEPS 450
C ..... LEPS 460
C ..... LEPS 470
C ..... LEPS 480
C ..... LEPS 490
C ..... LEPS 500
C ..... LEPS 510
C ..... LEPS 520
C ..... LEPS 530
C ..... LEPS 540
C ..... LEPS 550
C ..... LEPS 560
C ..... LEPS 570

```

```

C ..... DEPS 10
C ..... DEPS 20
C ..... DEPS 30
C ..... DEPS 40
C ..... DEPS 50
C ..... DEPS 60
C ..... DEPS 70
C ..... DEPS 80
C ..... DEPS 90
C ..... DEPS 100
C ..... DEPS 110
C ..... DEPS 120
C ..... DEPS 130
C ..... DEPS 140
C ..... DEPS 150
C ..... DEPS 160
C ..... DEPS 170
C ..... DEPS 180
C ..... DEPS 190
C ..... DEPS 200
C ..... DEPS 210
C ..... DEPS 220
C ..... DEPS 230
C ..... DEPS 240
C ..... DEPS 250
C ..... DEPS 260
C ..... DEPS 270
C ..... DEPS 280
C ..... DEPS 290
C ..... DEPS 300
C ..... DEPS 310
C ..... DEPS 320
C ..... DEPS 330
C ..... DEPS 340
C ..... DEPS 350
C ..... DEPS 360
C ..... DEPS 370
C ..... DEPS 380
C ..... DEPS 390
C ..... DEPS 400
C ..... DEPS 410
C ..... DEPS 420
C ..... DEPS 430
C ..... DEPS 440
C ..... DEPS 450
C ..... DEPS 460
C ..... DEPS 470
C ..... DEPS 480
C ..... DEPS 490
C ..... DEPS 500
C ..... DEPS 510
C ..... DEPS 520
C ..... DEPS 530
C ..... DEPS 540
C ..... DEPS 550
C ..... DEPS 560
C ..... DEPS 570
C ..... DEPS 580
C ..... DEPS 590
C ..... DEPS 600
C ..... DEPS 610

```

Subroutines TLEP and DTLEP

These subroutines transform a given series expansion in Legendre polynomials to a polynomial. The independent variable x of the given expansion is thereby substituted by the independent variable z of the resulting polynomial using the linear transformation $x = A * z + B$ or $z = (x - B)/A$.

$$\begin{aligned} \text{This means: } & \sum_{i=1}^N C_i * P_{i-1}(A * z + B) \\ & = \sum_{i=1}^N \text{POL}_i * z^{i-1} \end{aligned}$$

Calculation is bypassed in case of a nonpositive value of the dimension N .

The range $(-1, +1)$ in x is transformed to the range (z_1, z_r) in z with $z_1 = -(1 + B)/A$ and $z_r = (1 - B)/A$, or vice versa, $A = 2/(z_r - z_1)$ and $B = -(z_r + z_1)/(z_r - z_1)$.

The Legendre polynomial $P_n(x)$ satisfies the recurrence equation

$$P_{n+1}(x) = x \left[2 - 1/(n+1) \right] P_n(x) - \left[1 - 1/(n+1) \right] P_{n-1}(x)$$

with starting values $P_0(x) = 1$, $P_1(x) = x$.

The transformation is performed by means of a forward iteration scheme:

1. The coefficient vector of the Legendre polynomial $P_i(x)$ is calculated from the coefficient vectors of $P_{i-1}(x)$, $P_{i-2}(x)$ using the recurrence equation, for $i = 3, \dots, N$.

2. The resulting polynomial coefficient vector is obtained by summation of c_i times coefficient vector of $P_{i-1}(x)$ over i , for $i = 1, \dots, N$.

```

C
C
C ..... TLEP 10
C ..... TLEP 20
C ..... TLEP 30
SUBROUTINE TLEP TLEP 40
C ..... TLEP 50
C ..... TLEP 60
C ..... TLEP 70
PURPOSE TLEP 70
C ..... TLEP 80
C ..... TLEP 90
C ..... TLEP 100
C ..... TLEP 110
C ..... TLEP 120
C ..... TLEP 130
C ..... TLEP 140
DESCRIPTION OF PARAMETERS TLEP 140
C ..... TLEP 150
C ..... TLEP 160
C ..... TLEP 170
C ..... TLEP 180
C ..... TLEP 190
C ..... TLEP 200
C ..... TLEP 210
C ..... TLEP 220
C ..... TLEP 230
C ..... TLEP 240
C ..... TLEP 250
C ..... TLEP 260
C ..... TLEP 270
C ..... TLEP 280
C ..... TLEP 290
C ..... TLEP 300
C ..... TLEP 310
C ..... TLEP 320
C ..... TLEP 330
C ..... TLEP 340
C ..... TLEP 350
C ..... TLEP 360
C ..... TLEP 370
C ..... TLEP 380
C ..... TLEP 390
C ..... TLEP 400
C ..... TLEP 410
C ..... TLEP 420
C ..... TLEP 430
C ..... TLEP 440
C ..... TLEP 450
C ..... TLEP 460
C ..... TLEP 470
C ..... TLEP 480
C ..... TLEP 490
C ..... TLEP 500
SUBROUTINE TLEP(A,B,POL,N,C,WORK) TLEP 510
C ..... TLEP 520
C ..... TLEP 530
C ..... TLEP 540
C ..... TLEP 550
C ..... TLEP 560
C ..... TLEP 570
C ..... TLEP 580
C ..... TLEP 590
C ..... TLEP 600
C ..... TLEP 610
C ..... TLEP 620
C ..... TLEP 630
C ..... TLEP 640
C ..... TLEP 650
C ..... TLEP 660
C ..... TLEP 670
C ..... TLEP 680
C ..... TLEP 690
C ..... TLEP 700
C ..... TLEP 710
C ..... TLEP 720
C ..... TLEP 730
C ..... TLEP 740
C ..... TLEP 750
C ..... TLEP 760
C ..... TLEP 770
C ..... TLEP 780
C ..... TLEP 790
C ..... TLEP 800
C ..... TLEP 810
C ..... TLEP 820
C ..... TLEP 830
C ..... TLEP 840
C ..... TLEP 850
C ..... TLEP 860
C ..... TLEP 870
C ..... TLEP 880
C ..... TLEP 890
C ..... TLEP 900
C ..... TLEP 910
END

```

```

C.....DTLE 10
C.....DTLE 20
C.....DTLE 30
C.....DTLE 40
C.....DTLE 50
C.....DTLE 60
C.....DTLE 70
C.....DTLE 80
C.....DTLE 90
C.....DTLE 100
C.....DTLE 110
C.....DTLE 120
C.....DTLE 130
C.....DTLE 140
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C.....DTLE 470
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C.....DTLE 600
C.....DTLE 610
C.....DTLE 620
C.....DTLE 630
C.....DTLE 640
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C.....DTLE 710
C.....DTLE 720
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C.....DTLE 820
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C.....DTLE 870
C.....DTLE 880
C.....DTLE 890
C.....DTLE 900
C.....DTLE 910
C.....DTLE 920
C.....DTLE 930
C.....DTLE 940
C.....DTLE 950
C.....DTLE 960
C.....DTLE 970
SUBROUTINE DTLEP
PURPOSE
A SERIES EXPANSION IN LEGENDRE POLYNOMIALS WITH INDEPENDENT
VARIABLE X IS TRANSFORMED TO A POLYNOMIAL WITH INDEPENDENT
VARIABLE Z, WHERE X=A*Z+B
USAGE
CALL DTLEP(A,B,POL,N,C,WORK)
DESCRIPTION OF PARAMETERS
A - FACTOR OF LINEAR TERM IN GIVEN LINEAR TRANSFORMATION
DOUBLE PRECISION VARIABLE
B - CONSTANT TERM IN GIVEN LINEAR TRANSFORMATION
DOUBLE PRECISION VARIABLE
POL - COEFFICIENT VECTOR OF POLYNOMIAL (RESULTANT VALUE)
COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
DOUBLE PRECISION VECTOR
N - DIMENSION OF COEFFICIENT VECTORS POL AND C
C - GIVEN COEFFICIENT VECTOR OF EXPANSION
COEFFICIENTS ARE ORDERED FROM LOW TO HIGH
POL AND C MAY BE IDENTICALLY LOCATED
DOUBLE PRECISION VECTOR
WORK - WORKING STORAGE OF DIMENSION 2*N
DOUBLE PRECISION ARRAY
REMARKS
COEFFICIENT VECTOR C REMAINS UNCHANGED IF NOT COINCIDING
WITH COEFFICIENT VECTOR POL.
OPERATION IS BYPASSED IN CASE N LESS THAN 1.
THE LINEAR TRANSFORMATION X=A*Z+B OR Z=(1/A)(X-B) TRANSFORMS
THE RANGE (-1,+1) IN X TO THE RANGE (ZL,ZR) IN Z, WHERE
ZL=-((1+B)/A) AND ZR=(1-B)/A.
FOR GIVEN ZL, ZR WE HAVE A=2/(ZR-ZL) AND B=-((ZR+ZL)/(ZR-ZL))
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
THE TRANSFORMATION IS BASED ON THE RECURRENCE EQUATION
FOR LEGENDRE POLYNOMIALS P(N,X)
P(N+1,X)=2*X*P(N,X)-P(N-1,X)/(X*P(N,X)-P(N-1,X))/(N+1),
WHERE THE FIRST TERM IN BRACKETS IS THE INDEX,
THE SECOND IS THE ARGUMENT.
STARTING VALUES ARE P(0,X)=1, P(1,X)=X.
THE TRANSFORMATION IS IMPLICITLY DEFINED BY MEANS OF
X=A*Z+B TOGETHER WITH
SUM(POL(I)*Z**I*(-1), SUMMED OVER I FROM 1 TO N)
=SUM(C(I)*P(I-1,X), SUMMED OVER I FROM 1 TO N).
SUBROUTINE DTLEP(A,B,POL,N,C,WORK)
DIMENSION POL(1),C(1),WORK(1)
DOUBLE PRECISION A,B,POL,C,WORK,H,P,Q,Q1,FI
TEST OF DIMENSION
IF(N-1)2,1,3
DIMENSION LESS THAN 2
1 POL(1)=C(1)
2 RETURN
3 POL(1)=C(1)+B*C(2)
POL(2)=A*C(2)
IF(N-2)2,2,4
INITIALIZATION
4 WORK(1)=1.00
WORK(2)=B
WORK(3)=0.00
WORK(4)=A
FI=1.00
CALCULATE COEFFICIENT VECTOR OF NEXT LEGENDRE POLYNOMIAL
AND ADD MULTIPLE OF THIS VECTOR TO POLYNOMIAL POL
DO 6 J=3,N
FI=FI+1.00
Q=1.00/FI-1.00
Q1=1.00-Q
P=0.00
DO 5 K=2,J
H=(A*P+B*WORK(2*K-2))*Q1+Q*WORK(2*K-3)
P=WORK(2*K-2)
WORK(2*K-2)=H
WORK(2*K-3)=P
5 POL(K-1)=POL(K-1)+H*C(J)
WORK(2*K-1)=0.00
WORK(2*K)=A*P*Q1
6 POL(J)=C(J)*WORK(2*K)
RETURN
END

```

Roots of Nonlinear Equations

Subroutines RTWI and DRTWI

These subroutines refine the initial guess x_0 of a root of the general nonlinear equation $x = f(x)$. Wegstein's iteration scheme is used in order to get accelerated convergence in case of a function $f(x)$, which has at least continuous first derivative in the range in which iteration moves.

Following Figure 14, set $x_1 = y_0 = f(x_0)$ and $y_1 = f(x_1)$.

Refinement of x_1 is done by determination of the intersection of the linear function $y = x$ and the secant through the points (x_0, y_0) and (x_1, y_1) , thus getting:

$$x_2 = x_1 + \frac{x_1 - x_0}{\frac{y_0 - y_1}{x_1 - y_1} - 1}$$

$$\text{and } y_2 = f(x_2)$$

The next step is done by starting at (x_2, y_2) and setting:

$$x_3 = x_2 + \frac{x_2 - x_1}{\frac{y_1 - y_2}{x_2 - y_2} - 1}$$

$$y_3 = f(x_3)$$

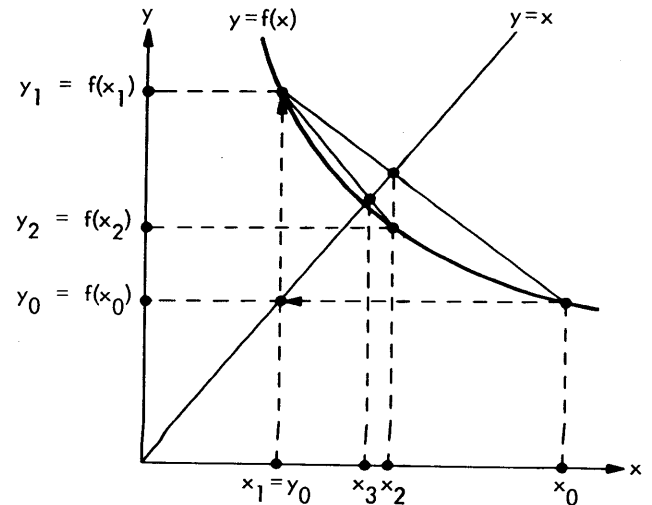


Figure 14. Wegstein's iterative method

It is easily seen that this determines the intersection between $y = x$ and the secant through the points (x_1, y_1) and (x_2, y_2) . Therefore Wegstein's iteration scheme is often called the secant modification of the normal iteration scheme $x_{i+1} = f(x_i)$.

Repeating these steps, the result is the iteration scheme:

$$x_{i+1} = x_i + \frac{x_i - x_{i-1}}{\frac{x_{i-1} - y_{i-1}}{x_i - y_i}} - 1 \quad (i = 1, 2, \dots) \quad (1)$$

$$y_{i+1} = f(x_{i+1})$$

Each step requires one evaluation of $f(x)$.

This iterative procedure is terminated if the following two conditions are satisfied:

$$\delta_1 \leq \epsilon \quad \text{and} \quad \delta_2 \leq 10 \cdot \epsilon$$

$$\text{with } \delta_1 = \begin{cases} \left| \frac{x_{i+1} - x_i}{x_{i+1}} \right| & \text{in case of } |x_{i+1}| > 1 \\ \left| x_{i+1} - x_i \right| & \text{in case of } |x_{i+1}| \leq 1 \end{cases} \quad (2)$$

$$\delta_2 = \begin{cases} \left| \frac{x_{i+1} - y_{i+1}}{x_{i+1}} \right| & \text{in case of } |x_{i+1}| > 1 \\ \left| x_{i+1} - y_{i+1} \right| & \text{in case of } |x_{i+1}| \leq 1 \end{cases}$$

and tolerance ϵ given by input.

The procedure described above may not converge within a specified number of iteration steps. Reasons for this behavior, which is indicated by an error message may be:

1. Too few iteration steps are specified.
2. The initial guess x_0 is too far away from any root.
3. The tolerance ϵ is too small with respect to roundoff errors.
4. The root to be determined is of multiplicity greater than one.

Furthermore, the procedure fails if at any iteration step the denominator of equation (1) becomes zero. This is also indicated by an error message. This failure may have two reasons:

1. The secant has the slope 1, either exactly or due to roundoff errors. In both cases it is probable that there is at least one point ξ in the range in which iteration moves with $f'(\xi) = 1$.

2. $x_i = x_{i-1}$ and $x_i \neq y_i = f(x_i)$. This case is possible due to roundoff errors or to a very steep slope of the secant.

For reference see G. N. Lance, Numerical Methods for High Speed Computers, Iliffe, London, 1960, pp. 134 - 138.

C	RTWI 10
C	SUBROUTINE RTWI	RTWI 20
C		RTWI 30
C	PURPOSE	RTWI 40
C	TO SOLVE GENERAL NONLINEAR EQUATIONS OF THE FORM X=FCT(X)	RTWI 50
C	BY MEANS OF WEGSTEIN-S ITERATION METHOD.	RTWI 60
C		RTWI 70
C	USAGE	RTWI 80
C	CALL RTWI (X,VAL,FCT,XST,EPS,IEND,IER)	RTWI 90
C	PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT.	RTWI 100
C		RTWI 110
C	DESCRIPTION OF PARAMETERS	RTWI 120
C	X - RESULTANT ROOT OF EQUATION X=FCT(X).	RTWI 130
C	VAL - RESULTANT VALUE OF X=FCT(X) AT ROOT X.	RTWI 140
C	FCT - NAME OF THE EXTERNAL FUNCTION SUBPROGRAM USED.	RTWI 150
C	XST - INPUT VALUE WHICH SPECIFIES THE INITIAL GUESS OF	RTWI 160
C	THE ROOT X.	RTWI 170
C	EPS - INPUT VALUE WHICH SPECIFIES THE UPPER BOUND OF THE	RTWI 180
C	ERROR OF RESULT X.	RTWI 190
C	IEND - MAXIMUM NUMBER OF ITERATION STEPS SPECIFIED.	RTWI 200
C	IER - RESULTANT ERROR PARAMETER CODED AS FOLLOWS	RTWI 210
C	IER=0 - NO ERROR,	RTWI 220
C	IER=1 - NO CONVERGENCE AFTER IEND ITERATION STEPS,	RTWI 230
C	IER=2 - AT ANY ITERATION STEP THE DENOMINATOR OF	RTWI 240
C	ITERATION FORMULA WAS EQUAL TO ZERO.	RTWI 250
C		RTWI 260
C	REMARKS	RTWI 270
C	THE PROCEDURE IS BYPASSED AND GIVES THE ERROR MESSAGE IER=2	RTWI 280
C	IF AT ANY ITERATION STEP THE DENOMINATOR OF ITERATION	RTWI 290
C	FORMULA WAS EQUAL TO ZERO. THAT MEANS THAT THERE IS AT	RTWI 300
C	LEAST ONE POINT IN THE RANGE IN WHICH ITERATION MOVES WITH	RTWI 310
C	DERIVATIVE OF FCT(X) EQUAL TO 1.	RTWI 320
C		RTWI 330
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	RTWI 340
C	THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED	RTWI 350
C	BY THE USER.	RTWI 360
C		RTWI 370
C	METHOD	RTWI 380
C	SOLUTION OF EQUATION X=FCT(X) IS DONE BY MEANS OF	RTWI 390
C	WEGSTEIN-S ITERATION METHOD, WHICH STARTS AT THE INITIAL	RTWI 400
C	GUESS XST OF A ROOT X. ONE ITERATION STEP REQUIRES ONE	RTWI 410
C	EVALUATION OF FCT(X). FOR TEST ON SATISFACTORY ACCURACY SEE	RTWI 420
C	FORMULAE (2) OF MATHEMATICAL DESCRIPTION.	RTWI 430
C	FOR REFERENCE, SEE	RTWI 440
C	(1) G. N. LANCE, NUMERICAL METHODS FOR HIGH SPEED COMPUTERS,	RTWI 450
C	ILIFFE, LONDON, 1960, PP.134-138.	RTWI 460
C	(2) J. WEGSTEIN, ALGORITHM 2, CACM, VOL.3, ISS.2 (1960),	RTWI 470
C	PP.74.	RTWI 480
C	(3) H.C. THACHER, ALGORITHM 15, CACM, VOL.3, ISS.8 (1960),	RTWI 490
C	PP.475.	RTWI 500
C	(4) J.G. HERRIOT, ALGORITHM 26, CACM, VOL.3, ISS.11 (1960),	RTWI 510
C	PP.603.	RTWI 520
C		RTWI 530
C	RTWI 540
C	SUBROUTINE RTWI(X,VAL,FCT,XST,EPS,IEND,IER)	RTWI 550
C		RTWI 560
C	PREPARE ITERATION	RTWI 570
C	IER=0	RTWI 580
C	TOL=XST	RTWI 590
C	X=FCT(TOL)	RTWI 600
C	A=X-XST	RTWI 610
C	B=-A	RTWI 620
C	TOL=X	RTWI 630
C	VAL=X-FCT(TOL)	RTWI 640
C		RTWI 650
C		RTWI 660
C		RTWI 670
C		RTWI 680
C		RTWI 690
C		RTWI 700
C	START ITERATION LOOP	RTWI 710
C	DO 6 I=1,IEND	RTWI 720
C	IF(VAL)1,7,1	RTWI 730
C		RTWI 740
C	EQUATION IS NOT SATISFIED BY X	RTWI 750
C	1 B=B/VAL-1.	RTWI 760
C	IF(B)2,B,2	RTWI 770
C		RTWI 780
C	ITERATION IS POSSIBLE	RTWI 790
C	2 A=A/B	RTWI 800
C	X=X+A	RTWI 810
C	B=VAL	RTWI 820
C	TOL=X	RTWI 830
C	VAL=X-FCT(TOL)	RTWI 840
C		RTWI 850
C	TEST ON SATISFACTORY ACCURACY	RTWI 860
C	TOL=EPS	RTWI 870
C	D=ABS(X)	RTWI 880
C	IF(D-1.74,4,3	RTWI 890
C	3 TOL=TOL*D	RTWI 900
C	4 IF(ABS(A)-TOL)5,5,6	RTWI 910
C	5 IF(ABS(VAL)-10.*TOL)7,7,6	RTWI 920
C	6 CONTINUE	RTWI 930
C	END OF ITERATION LOOP	RTWI 940
C		RTWI 950
C		RTWI 960
C	NO CONVERGENCE AFTER IEND ITERATION STEPS. ERROR RETURN.	RTWI 970
C	IER=1	RTWI 980
C	7 RETURN	RTWI 990
C		RTWI1000
C	ERROR RETURN IN CASE OF ZERO DIVISOR	RTWI1010
C	8 IER=2	RTWI1020
C	RETURN	RTWI1030
C	END	RTWI1040

```

C .....
C SUBROUTINE DRTMI
C TO SOLVE GENERAL NONLINEAR EQUATIONS OF THE FORM X=FCT(X)
C BY MEANS OF WEGSTEIN-S ITERATION METHOD.
C
C USAGE
C CALL DRTMI (X,VAL,FCT,XST,EPS,IEND,IER)
C PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT.
C
C DESCRIPTION OF PARAMETERS
C X - DOUBLE PRECISION RESULTANT ROOT OF EQUATION
C VAL - DOUBLE PRECISION RESULTANT VALUE OF X=FCT(X)
C FCT - NAME OF THE EXTERNAL DOUBLE PRECISION FUNCTION
C SUBPROGRAM USED.
C XST - DOUBLE PRECISION INPUT VALUE WHICH SPECIFIES THE
C INITIAL GUESS OF THE ROOT X.
C EPS - SINGLE PRECISION INPUT VALUE WHICH SPECIFIES THE
C UPPER BOUND OF THE ERROR OF RESULT X.
C IEND - MAXIMUM NUMBER OF ITERATION STEPS SPECIFIED.
C IER - RESULTANT ERROR PARAMETER CODED AS FOLLOWS
C IER=0 - NO ERROR,
C IER=1 - NO CONVERGENCE AFTER IEND ITERATION STEPS,
C IER=2 - AT ANY ITERATION STEP THE DENOMINATOR OF
C ITERATION FORMULA WAS EQUAL TO ZERO.
C
C REMARKS
C THE PROCEDURE IS BYPASSED AND GIVES THE ERROR MESSAGE IER=2
C IF AT ANY ITERATION STEP THE DENOMINATOR OF ITERATION
C FORMULA WAS EQUAL TO ZERO, THAT MEANS THAT THERE IS AT
C LEAST ONE POINT IN THE RANGE IN WHICH ITERATION MOVES WITH
C DERIVATIVE OF FCT(X) EQUAL TO 1.
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)
C MUST BE FURNISHED BY THE USER.
C
C METHOD
C SOLUTION OF EQUATION X=FCT(X) IS DONE BY MEANS OF
C WEGSTEIN-S ITERATION METHOD, WHICH STARTS AT THE INITIAL
C GUESS XST OF A ROOT X. ONE ITERATION STEP REQUIRES ONE
C EVALUATION OF FCT(X). FOR TEST ON SATISFACTORY ACCURACY SEE
C FORMULAE (2) OF MATHEMATICAL DESCRIPTION.
C FOR REFERENCE, SEE
C (1) G. N. LANCE, NUMERICAL METHODS FOR HIGH SPEED COMPUTERS,
C TLIFFE, LONDON, 1960, PP.134-138,
C (2) J. WEGSTEIN, ALGORITHM 2, CACM, VOL.3, ISS.2 (1960),
C PP.74,
C (3) H.C. THACHER, ALGORITHM 15, CACM, VOL.3, ISS.8 (1960),
C PP.475,
C (4) J.G. HERRIOT, ALGORITHM 26, CACM, VOL.3, ISS.11 (1960),
C PP.603.
C .....
C SUBROUTINE DRTMI(X,VAL,FCT,XST,EPS,IEND,IER)
C
C DOUBLE PRECISION X,VAL,FCT,XST,A,B,D,TOL
C
C PREPARE ITERATION
C IER=0
C TOL=XST
C X=FCT(TOL)
C A=X-XST
C B=A-XST
C D=A
C TOL=X
C VAL=X-FCT(TOL)
C
C START ITERATION LOOP
C DO 6 I=1,IEND
C IF(VAL)1,7,1
C
C EQUATION IS NOT SATISFIED BY X
C 1 B=B/VAL-1.00
C IF(B)2,0,2
C
C ITERATION IS POSSIBLE
C 2 A=A/B
C X=X+A
C B=VAL
C TOL=X
C VAL=X-FCT(TOL)
C
C TEST ON SATISFACTORY ACCURACY
C TOL=EPS
C D=DABS(X)
C IF(D-1.00)4,4,3
C 3 TOL=TOL*0
C 4 IF(DABS(A)-TOL)5,5,6
C 5 IF(DABS(VAL)-1.01*TOL)7,7,6
C 6 CONTINUE
C END OF ITERATION LOOP
C
C NO CONVERGENCE AFTER IEND ITERATION STEPS. ERROR RETURN.
C IER=1
C 7 RETURN
C
C ERROR RETURN IN CASE OF ZERO DIVISOR
C 8 IER=2
C RETURN
C END

```

Subroutines RTMI and DRTMI

These subroutines determine a root of the general nonlinear equation $f(x) = 0$ in the range of x from x_{l1} up to x_{r1} (x_{l1} , x_{r1} given by input) by means of Mueller's iteration scheme of successive bisection and inverse parabolic interpolation. The procedure assumes $f(x_{l1}) \cdot f(x_{r1}) \leq 0$.

Starting with $x_l = x_{l1}$ and $x_r = x_{r1}$ and following Fig. 15, one iteration step is described.

First, the middle of the interval $x_l \dots x_r$ is computed:

$$x_m = \frac{1}{2} (x_l + x_r).$$

In case $f(x_m) \cdot f(x_r) < 0$, x_l and x_r are interchanged to ensure that $f(x_m) \cdot f(x_r) > 0$.

In case

$$2 f(x_m) [f(x_m) - f(x_l)] - f(x_r) [f(x_r) - f(x_l)] \geq 0 \quad (1)$$

x_r is replaced by x_m and the bisection step is repeated. If, after a specified number of successive bisections, inequality (1) is still satisfied, the procedure is bypassed and an error message is given.

In Fig. 15, the second bisection step leads to a configuration which does not satisfy inequality (1). Thus by inverse parabolic interpolation:

$$\Delta x = f(x_l) \frac{x_m - x_l}{f(x_m) - f(x_l)}$$

$$\left\{ 1 + f(x_m) \frac{f(x_r) - 2f(x_m) + f(x_l)}{[f(x_r) - f(x_m)][f(x_r) - f(x_l)]} \right\} \quad (2)$$

$$\text{and } x = x_l - \Delta x$$

and x is sure to be situated between x_l and x_m .

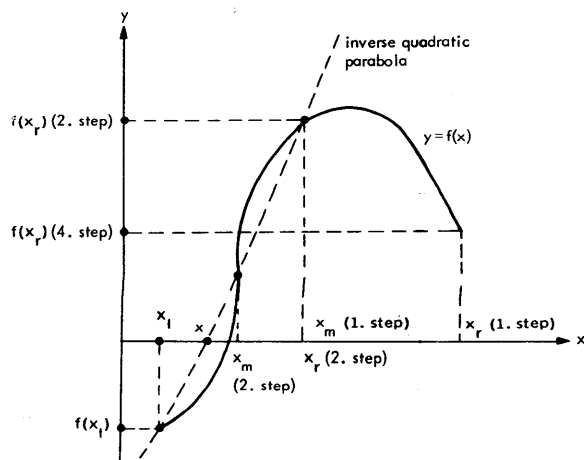


Figure 15. Mueller's iterative method

Now, for the next iteration step, x becomes x_l and x_m becomes x_r if $f(x) \cdot f(x_l) > 0$, or x becomes x_r if $f(x) \cdot f(x_l) < 0$.

Convergence is either quadratic or linear if the multiplicity of the root to be determined is equal to one or greater than one respectively, and if $f(x)$ can be differentiated continuously at least twice in the range $x_{l1} \dots x_{r1}$. Each iteration step requires two evaluations of $f(x)$.

This iterative procedure is terminated if either the two conditions (checked in bisection loop)

$$\text{and } \left. \begin{aligned} |x_r - x_l| &\leq \epsilon \cdot \max(1, |x_r|) \\ |f(x_r) - f(x_l)| &\leq 100 \cdot \epsilon \end{aligned} \right\} \quad (3)$$

or the two conditions (checked after inverse parabolic interpolation)

$$\text{and } \left. \begin{aligned} |\Delta x| &\leq \epsilon \cdot \max(1, |x|) \\ |f(x)| &\leq 100 \cdot \epsilon \end{aligned} \right\} \quad (4)$$

are satisfied, where tolerance ϵ is given by input.

The procedure described above may not converge within a specified number of iteration steps followed by the same number of successive bisections. Reasons for this behaviour, which is indicated by an error message, may be:

1. Too few iteration steps are specified.
2. The initial interval $x_{l1} \dots x_{r1}$ is too long.
3. The tolerance ϵ is too small with respect to roundoff errors.

Furthermore, the procedure is bypassed, also giving an error message, if the basic assumption $f(x_{l1}) \cdot f(x_{r1}) \leq 0$ is not satisfied.

For reference see G. K. Kristiansen, "Zero of Arbitrary Function", BIT, vol. 3 (1963), pp. 205-206.

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C       PROCEDURE IS BYPASSED AND GIVES THE ERROR MESSAGE IER=2.      RTM1 370
C       SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED                    RTM1 380
C       THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED    RTM1 390
C       BY THE USER.                                                 RTM1 400
C                                                                      RTM1 410
C       METHOD                                                          RTM1 420
C       SOLUTION OF EQUATION FCT(X)=0 IS DONE BY MEANS OF MUELLER-S   RTM1 430
C       ITERATION METHOD OF SUCCESSIVE BISECTIONS AND INVERSE         RTM1 440
C       PARABOLIC INTERPOLATION, WHICH STARTS AT THE INITIAL BOUNDS  RTM1 450
C       XLI AND XRI. CONVERGENCE IS QUADRATIC IF THE DERIVATIVE OF   RTM1 460
C       FCT(X) AT ROOT X IS NOT EQUAL TO ZERO. ONE ITERATION STEP   RTM1 470
C       REQUIRES TWO EVALUATIONS OF FCT(X). FOR TEST ON SATISFACTORY RTM1 480
C       ACCURACY SEE FORMULAE (3,4) OF MATHEMATICAL DESCRIPTION.     RTM1 490
C       FOR REFERENCE, SEE G. K. KRISTIENSEN, ZERO OF ARBITRARY     RTM1 500
C       FUNCTION, BIT, VOL. 3 (1963), PP.205-206.                   RTM1 520
C                                                                      RTM1 530
C       .....RTM1 540
C       SUBROUTINE RTM1(X,F,FCT,XLI,XRI,EPS,IEND,IER)                 RTM1 550
C                                                                      RTM1 560
C       PREPARE ITERATION                                             RTM1 570
C       IER=0                                                         RTM1 580
C       XL=XLI                                                         RTM1 590
C       XR=XRI                                                         RTM1 600
C       X=XL                                                           RTM1 610
C       TOL=X                                                           RTM1 620
C       F=FCT(TOL)                                                    RTM1 630
C       IF(F)1,16,1                                                    RTM1 640
C 1  FL=F                                                                RTM1 650
C       X=XR                                                            RTM1 660
C       TOL=X                                                           RTM1 670
C       F=FCT(TOL)                                                    RTM1 680
C       IF(F)2,16,2                                                    RTM1 690
C 2  FR=F                                                                RTM1 700
C       IF(SIGN(1.,FL)+SIGN(1.,FR))25,3,25                             RTM1 710
C                                                                      RTM1 720
C       BASIC ASSUMPTION FL*FR LESS THAN 0 IS SATISFIED.            RTM1 730
C       GENERATE TOLERANCE FOR FUNCTION VALUES.                    RTM1 740
C 3  I=0                                                                RTM1 750
C       TOLF=100.*EPS                                                 RTM1 760
C                                                                      RTM1 770
C       START ITERATION LOOP                                         RTM1 780
C 4  I=I+1                                                              RTM1 790
C                                                                      RTM1 800
C       START BISECTION LOOP                                         RTM1 810
C       DD 13 K=1,IEND                                               RTM1 820
C       X=.5*(XL+XR)                                                 RTM1 830
C       F=FCT(X)                                                      RTM1 840
C       IF(F)5,16,5                                                  RTM1 850
C 5  IF(SIGN(1.,F)+SIGN(1.,FR))7,6,7                                  RTM1 860
C                                                                      RTM1 870
C       INTERCHANGE XL AND XR IN ORDER TO GET THE SAME SIGN IN F AND RTM1 880
C 6  TOL=XL                                                            RTM1 890
C       XL=XR                                                           RTM1 900
C       XR=TOL                                                         RTM1 910
C       TOL=FL                                                         RTM1 920
C       FL=FR                                                           RTM1 930
C       FR=TOL                                                         RTM1 940
C 7  TOL=F-FL                                                         RTM1 950
C       A=F/TOL                                                         RTM1 960
C       A=A+A                                                            RTM1 970
C       IF(A-FR*(FR-FL))8,9,9                                           RTM1 980
C 8  IF(I-IEND)17,17,9                                               RTM1 990
C 9  XR=X                                                                RTM11000
C       FR=F                                                            RTM11010
C                                                                      RTM11020
C       TEST ON SATISFACTORY ACCURACY IN BISECTION LOOP             RTM11030
C       TOL=EPS                                                       RTM11040
C       A=ABS(XR)                                                       RTM11050
C       IF(A-1.)11,11,10                                              RTM11060
C 10 TOL=TOL*A                                                         RTM11070
C 11 IF(ABS(XR-XL)-TOL)12,12,13                                        RTM11080
C 12 IF(ABS(FR-FL)-TOLF)14,14,13                                       RTM11090
C 13 CONTINUE                                                         RTM11100
C       END OF BISECTION LOOP                                         RTM11110
C                                                                      RTM11120
C       NO CONVERGENCE AFTER IEND ITERATION STEPS FOLLOWED BY IEND  RTM11130
C       SUCCESSIVE STEPS OF BISECTION OR STEADILY INCREASING      RTM11140
C       VALUES AT RIGHT BOUNDS. ERROR RETURN.                       RTM11150
C       IER=1                                                           RTM11160
C 14 IF(ABS(FR)-ABS(FL))16,16,15                                       RTM11170
C 15 X=XL                                                               RTM11180
C       F=FL                                                            RTM11190
C 16 RETURN                                                            RTM11200
C                                                                      RTM11210
C       COMPUTATION OF ITERATED X-VALUE BY INVERSE PARABOLIC        RTM11220
C 17 X=FR-F                                                            RTM1270
C       DX=(X-XL)*FL*(1.+F*(A-TOL)/(A*(FR-FL)))/TOL                 RTM1280
C       XM=X                                                             RTM1290
C       FM=F                                                             RTM1300
C       X=XL-DX                                                         RTM1310
C       TOL=X                                                           RTM1320
C       F=FCT(TOL)                                                      RTM1330
C       IF(F)18,16,18                                                  RTM1340
C       END OF BISECTION LOOP                                         RTM1350
C       TEST ON SATISFACTORY ACCURACY IN ITERATION LOOP             RTM1360
C 18 TOL=EPS                                                            RTM1370
C       A=ABS(X)                                                         RTM1380
C       IF(A-1.)20,20,19                                               RTM1390
C 19 TOL=TOL*A                                                         RTM1400
C 20 IF(ABS(DX)-TOL)21,21,22                                           RTM1410
C 21 IF(ABS(F)-TOLF)16,16,22                                          RTM1420
C                                                                      RTM1430
C       PREPARATION OF NEXT BISECTION LOOP                           RTM1440
C 22 IF(SIGN(1.,F)+SIGN(1.,FL))24,23,24                                RTM1450
C 23 XR=X                                                                RTM1460
C       FR=F                                                            RTM1470
C       GO TO 4                                                         RTM1480
C 24 XL=X                                                                RTM1490
C       FL=F                                                            RTM1500
C       XR=XM                                                            RTM1510
C       FR=FM                                                            RTM1520
C       GO TO 4                                                         RTM1530
C       END OF ITERATION LOOP                                         RTM1540
C                                                                      RTM1550
C       ERROR RETURN IN CASE OF WRONG INPUT DATA                   RTM1560
C 25 IER=2                                                              RTM1570
C       RETURN                                                           RTM1580
C       END                                                              RTM1590
C                                                                      RTM1600

```

```

C       SUBROUTINE RTM1                                             RTM1 10
C       .....RTM1 20
C       PURPOSE                                                    RTM1 30
C       TO SOLVE GENERAL NONLINEAR EQUATIONS OF THE FORM FCT(X)=0  RTM1 40
C       BY MEANS OF MUELLER-S ITERATION METHOD.                    RTM1 50
C       USAGE                                                      RTM1 60
C       CALL RTM1(X,F,FCT,XLI,XRI,EPS,IEND,IER)                   RTM1 70
C       PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT.            RTM1 80
C       DESCRIPTION OF PARAMETERS                                  RTM1 90
C       X - RESULTANT ROOT OF EQUATION FCT(X)=0.                 RTM1 100
C       F - RESULTANT FUNCTION VALUE AT ROOT X.                  RTM1 110
C       FCT - NAME OF THE EXTERNAL FUNCTION SUBPROGRAM USED.     RTM1 120
C       XLI - INPUT VALUE WHICH SPECIFIES THE INITIAL LEFT BOUND RTM1 130
C       OF THE ROOT X.                                           RTM1 140
C       XRI - INPUT VALUE WHICH SPECIFIES THE INITIAL RIGHT BOUND RTM1 150
C       OF THE ROOT X.                                           RTM1 160
C       EPS - INPUT VALUE WHICH SPECIFIES THE UPPER BOUND OF THE RTM1 170
C       ERROR OF RESULT X.                                        RTM1 180
C       IEND - MAXIMUM NUMBER OF ITERATION STEPS SPECIFIED.     RTM1 190
C       IER - RESULTANT ERROR PARAMETER CODED AS FOLLOWS        RTM1 200
C       IER=0 - NO ERROR,                                         RTM1 210
C       IER=1 - NO CONVERGENCE AFTER IEND ITERATION STEPS      RTM1 220
C       FOLLOWED BY IEND SUCCESSIVE STEPS OF                    RTM1 230
C       BISECTION.                                               RTM1 240
C       IER=2 - BASIC ASSUMPTION FCT(XLI)*FCT(XRI) LESS        RTM1 250
C       THAN OR EQUAL TO ZERO IS NOT SATISFIED.                RTM1 260
C       REMARKS                                                    RTM1 270
C       THE PROCEDURE ASSUMES THAT FUNCTION VALUES AT INITIAL  RTM1 280
C       BOUNDS XLI AND XRI HAVE NOT THE SAME SIGN. IF THIS BASIC RTM1 290
C       ASSUMPTION IS NOT SATISFIED BY INPUT VALUES XLI AND XRI, THE RTM1 300
C       RTM1 310
C       RTM1 320
C       RTM1 330
C       RTM1 340
C       RTM1 350
C       RTM1 360

```

```

C
C ..... DRTM 10
C ..... DRTM 20
C ..... DRTM 30
C
C SUBROUTINE DRTM1
C ..... DRTM 40
C ..... DRTM 50
C
C PURPOSE
C TO SOLVE GENERAL NONLINEAR EQUATIONS OF THE FORM FCT(X)=0
C BY MEANS OF MUELLER-S ITERATION METHOD.
C ..... DRTM 70
C ..... DRTM 80
C ..... DRTM 90
C ..... DRTM 100
C
C USAGE
C CALL DRTM1 (X,F,FCT,XLI,XRI,EPS,IEND,IER)
C PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT.
C ..... DRTM 110
C ..... DRTM 120
C ..... DRTM 130
C
C DESCRIPTION OF PARAMETERS
C X - DOUBLE PRECISION RESULTANT ROOT OF EQUATION
C ..... DRTM 140
C ..... DRTM 150
C ..... DRTM 160
C F - DOUBLE PRECISION RESULTANT FUNCTION VALUE
C AT ROOT X.
C ..... DRTM 170
C ..... DRTM 180
C FCT - NAME OF THE EXTERNAL DOUBLE PRECISION FUNCTION
C SUBPROGRAM USED.
C ..... DRTM 190
C ..... DRTM 200
C XLI - DOUBLE PRECISION INPUT VALUE WHICH SPECIFIES THE
C INITIAL LEFT BOUND OF THE ROOT X.
C ..... DRTM 210
C ..... DRTM 220
C XRI - DOUBLE PRECISION INPUT VALUE WHICH SPECIFIES THE
C INITIAL RIGHT BOUND OF THE ROOT X.
C ..... DRTM 230
C ..... DRTM 240
C EPS - SINGLE PRECISION INPUT VALUE WHICH SPECIFIES THE
C UPPER BOUND OF THE ERROR OF RESULT X.
C ..... DRTM 250
C ..... DRTM 260
C IEND - MAXIMUM NUMBER OF ITERATION STEPS SPECIFIED.
C ..... DRTM 270
C ..... DRTM 280
C IER - RESULTANT ERROR PARAMETER CODED AS FOLLOWS
C IER=0 - NO ERROR,
C IER=1 - NO CONVERGENCE AFTER IEND ITERATION STEPS
C FOLLOWED BY IEND SUCCESSIVE STEPS OF
C BISECTION,
C IER=2 - BASIC ASSUMPTION FCT(XLI)*FCT(XRI) LESS
C THAN OR EQUAL TO ZERO IS NOT SATISFIED.
C ..... DRTM 290
C ..... DRTM 300
C ..... DRTM 310
C ..... DRTM 320
C ..... DRTM 330
C ..... DRTM 340
C ..... DRTM 350
C ..... DRTM 360
C
C REMARKS
C THE PROCEDURE ASSUMES THAT FUNCTION VALUES AT INITIAL
C BOUNDS XLI AND XRI HAVE NOT THE SAME SIGN. IF THIS BASIC
C ASSUMPTION IS NOT SATISFIED BY INPUT VALUES XLI AND XRI, THE
C PROCEDURE IS BYPASSED AND GIVES THE ERROR MESSAGE IER=2.
C ..... DRTM 370
C ..... DRTM 380
C ..... DRTM 390
C ..... DRTM 400
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)
C MUST BE FURNISHED BY THE USER.
C ..... DRTM 410
C ..... DRTM 420
C ..... DRTM 430
C ..... DRTM 440
C ..... DRTM 450
C ..... DRTM 460
C
C METHOD
C SOLUTION OF EQUATION FCT(X)=0 IS DONE BY MEANS OF MUELLER-S
C ITERATION METHOD OF SUCCESSIVE BISECTIONS AND INVERSE
C PARABOLIC INTERPOLATION, WHICH STARTS AT THE INITIAL BOUNDS
C XLI AND XRI. CONVERGENCE IS QUADRATIC IF THE DERIVATIVE OF
C FCT(X) AT ROOT X IS NOT EQUAL TO ZERO. ONE ITERATION STEP
C REQUIRES TWO EVALUATIONS OF FCT(X). FOR TEST ON SATISFACTORY
C ACCURACY SEE FORMULAE (3,4) OF MATHEMATICAL DESCRIPTION.
C FOR REFERENCE, SEE G. K. KRISTIANSEN, ZERO OF ARBITRARY
C FUNCTION, BIT, VOL. 3 (1963), PP.205-206.
C ..... DRTM 470
C ..... DRTM 480
C ..... DRTM 490
C ..... DRTM 500
C ..... DRTM 510
C ..... DRTM 520
C ..... DRTM 530
C ..... DRTM 540
C ..... DRTM 550
C ..... DRTM 560
C ..... DRTM 570
C ..... DRTM 580
C
C SUBROUTINE DRTM1(X,F,FCT,XLI,XRI,EPS,IEND,IER)
C ..... DRTM 590
C ..... DRTM 600
C
C DOUBLE PRECISION X,F,FCT,XLI,XRI,XL,XR,FL,FR,TOL,TOLF,A,DX,XM,FM
C ..... DRTM 610
C ..... DRTM 620
C ..... DRTM 630
C ..... DRTM 640
C ..... DRTM 650
C ..... DRTM 660
C ..... DRTM 670
C ..... DRTM 680
C ..... DRTM 690
C ..... DRTM 700
C ..... DRTM 710
C ..... DRTM 720
C ..... DRTM 730
C ..... DRTM 740
C ..... DRTM 750
C ..... DRTM 760
C ..... DRTM 770
C ..... DRTM 780
C ..... DRTM 790
C ..... DRTM 800
C ..... DRTM 810
C ..... DRTM 820
C ..... DRTM 830
C ..... DRTM 840
C ..... DRTM 850
C ..... DRTM 860
C ..... DRTM 870
C ..... DRTM 880
C ..... DRTM 890
C ..... DRTM 900
C ..... DRTM 910
C ..... DRTM 920
C ..... DRTM 930
C ..... DRTM 940
C ..... DRTM 950
C ..... DRTM 960
C ..... DRTM 970
C ..... DRTM 980
C ..... DRTM 990
C ..... DRTM1000
C ..... DRTM1010
C ..... DRTM1020
C ..... DRTM1030
C ..... DRTM1040
C ..... DRTM1050
C ..... DRTM1060
C ..... DRTM1070
C ..... DRTM1080
C ..... DRTM1090
C ..... DRTM1100
C ..... DRTM1110
C ..... DRTM1120
C ..... DRTM1130
C ..... DRTM1140
C ..... DRTM1150
C ..... DRTM1160
C ..... DRTM1170
C ..... DRTM1180
C ..... DRTM1190
C ..... DRTM1200
C ..... DRTM1210
C ..... DRTM1220
C ..... DRTM1230
C ..... DRTM1240
C ..... DRTM1250
C ..... DRTM1260
C ..... DRTM1270
C ..... DRTM1280
C ..... DRTM1290
C
C PREPARE ITERATION
C IER=0
C XL=XLI
C XR=XRI
C X=XL
C TOL=X
C F=FCT(TOL)
C IF(F)1,16,1
C 1 FL=F
C X=XR
C TOL=X
C F=FCT(TOL)
C IF(F)2,16,2
C 2 FR=F
C IF(DSIGN(1.00,FL)+DSIGN(1.00,FR))125,3,25
C ..... DRTM 780
C ..... DRTM 790
C
C BASIC ASSUMPTION FL*FR LESS THAN 0 IS SATISFIED.
C GENERATE TOLERANCE FOR FUNCTION VALUES.
C 3 I=0
C TOLF=100.*EPS
C ..... DRTM 800
C ..... DRTM 810
C ..... DRTM 820
C ..... DRTM 830
C ..... DRTM 840
C ..... DRTM 850
C ..... DRTM 860
C ..... DRTM 870
C ..... DRTM 880
C ..... DRTM 890
C ..... DRTM 900
C ..... DRTM 910
C ..... DRTM 920
C ..... DRTM 930
C ..... DRTM 940
C ..... DRTM 950
C ..... DRTM 960
C ..... DRTM 970
C ..... DRTM 980
C ..... DRTM 990
C ..... DRTM1000
C ..... DRTM1010
C ..... DRTM1020
C ..... DRTM1030
C ..... DRTM1040
C ..... DRTM1050
C ..... DRTM1060
C ..... DRTM1070
C ..... DRTM1080
C ..... DRTM1090
C ..... DRTM1100
C ..... DRTM1110
C ..... DRTM1120
C ..... DRTM1130
C ..... DRTM1140
C ..... DRTM1150
C ..... DRTM1160
C ..... DRTM1170
C ..... DRTM1180
C ..... DRTM1190
C ..... DRTM1200
C ..... DRTM1210
C ..... DRTM1220
C ..... DRTM1230
C ..... DRTM1240
C ..... DRTM1250
C ..... DRTM1260
C ..... DRTM1270
C ..... DRTM1280
C ..... DRTM1290
C
C START ITERATION LOOP
C 4 I=I+1
C ..... DRTM 870
C ..... DRTM 880
C ..... DRTM 890
C ..... DRTM 900
C ..... DRTM 910
C ..... DRTM 920
C ..... DRTM 930
C ..... DRTM 940
C ..... DRTM 950
C ..... DRTM 960
C ..... DRTM 970
C ..... DRTM 980
C ..... DRTM 990
C ..... DRTM1000
C ..... DRTM1010
C ..... DRTM1020
C ..... DRTM1030
C ..... DRTM1040
C ..... DRTM1050
C ..... DRTM1060
C ..... DRTM1070
C ..... DRTM1080
C ..... DRTM1090
C ..... DRTM1100
C ..... DRTM1110
C ..... DRTM1120
C ..... DRTM1130
C ..... DRTM1140
C ..... DRTM1150
C ..... DRTM1160
C ..... DRTM1170
C ..... DRTM1180
C ..... DRTM1190
C ..... DRTM1200
C ..... DRTM1210
C ..... DRTM1220
C ..... DRTM1230
C ..... DRTM1240
C ..... DRTM1250
C ..... DRTM1260
C ..... DRTM1270
C ..... DRTM1280
C ..... DRTM1290
C
C START BISECTION LOOP
C DO 13 K=1,IEND
C X=.500*(XL+XR)
C TOL=X
C F=FCT(TOL)
C IF(F)5,16,5
C 5 IF(DSIGN(1.00,F)+DSIGN(1.00,FR))7,6,7
C ..... DRTM 970
C ..... DRTM 980
C ..... DRTM 990
C ..... DRTM1000
C ..... DRTM1010
C ..... DRTM1020
C ..... DRTM1030
C ..... DRTM1040
C ..... DRTM1050
C ..... DRTM1060
C ..... DRTM1070
C ..... DRTM1080
C ..... DRTM1090
C ..... DRTM1100
C ..... DRTM1110
C ..... DRTM1120
C ..... DRTM1130
C ..... DRTM1140
C ..... DRTM1150
C ..... DRTM1160
C ..... DRTM1170
C ..... DRTM1180
C ..... DRTM1190
C ..... DRTM1200
C ..... DRTM1210
C ..... DRTM1220
C ..... DRTM1230
C ..... DRTM1240
C ..... DRTM1250
C ..... DRTM1260
C ..... DRTM1270
C ..... DRTM1280
C ..... DRTM1290
C
C INTERCHANGE XL AND XR IN ORDER TO GET THE SAME SIGN IN F AND FR
C 6 TOL=XL
C XL=XR
C XR=TOL
C TOL=FL
C FL=FR
C FR=TOL
C 7 TOL=FR-FL
C A=F*TOL
C A=A+A
C IF(A-FR*(FR-FL))8,9,9
C 8 IF(I-IEND)17,17,9
C 9 XR=X
C FR=F
C ..... DRTM 970
C ..... DRTM 980
C ..... DRTM 990
C ..... DRTM1000
C ..... DRTM1010
C ..... DRTM1020
C ..... DRTM1030
C ..... DRTM1040
C ..... DRTM1050
C ..... DRTM1060
C ..... DRTM1070
C ..... DRTM1080
C ..... DRTM1090
C ..... DRTM1100
C ..... DRTM1110
C ..... DRTM1120
C ..... DRTM1130
C ..... DRTM1140
C ..... DRTM1150
C ..... DRTM1160
C ..... DRTM1170
C ..... DRTM1180
C ..... DRTM1190
C ..... DRTM1200
C ..... DRTM1210
C ..... DRTM1220
C ..... DRTM1230
C ..... DRTM1240
C ..... DRTM1250
C ..... DRTM1260
C ..... DRTM1270
C ..... DRTM1280
C ..... DRTM1290
C
C TEST ON SATISFACTORY ACCURACY IN BISECTION LOOP
C TOL=EPS
C A=DABS(XR)
C IF(A-1.00)11,11,10
C 10 TOL=TOL*A
C 11 IF(DABS(XR-XL)-TOL)12,12,13
C 12 IF(DABS(FR-FL)-TOLF)14,14,13
C 13 CONTINUE
C END OF BISECTION LOOP
C ..... DRTM 970
C ..... DRTM 980
C ..... DRTM 990
C ..... DRTM1000
C ..... DRTM1010
C ..... DRTM1020
C ..... DRTM1030
C ..... DRTM1040
C ..... DRTM1050
C ..... DRTM1060
C ..... DRTM1070
C ..... DRTM1080
C ..... DRTM1090
C ..... DRTM1100
C ..... DRTM1110
C ..... DRTM1120
C ..... DRTM1130
C ..... DRTM1140
C ..... DRTM1150
C ..... DRTM1160
C ..... DRTM1170
C ..... DRTM1180
C ..... DRTM1190
C ..... DRTM1200
C ..... DRTM1210
C ..... DRTM1220
C ..... DRTM1230
C ..... DRTM1240
C ..... DRTM1250
C ..... DRTM1260
C ..... DRTM1270
C ..... DRTM1280
C ..... DRTM1290
C
C NO CONVERGENCE AFTER IEND ITERATION STEPS FOLLOWED BY IEND
C SUCCESSIVE STEPS OF BISECTION OR STEADILY INCREASING FUNCTION
C VALUES AT RIGHT BOUNDS. ERROR RETURN.
C IER=1
C 14 IF(DABS(FR)-DABS(FL))16,16,15
C 15 X=XL
C F=FL
C 16 RETURN
C ..... DRTM 970
C ..... DRTM 980
C ..... DRTM 990
C ..... DRTM1000
C ..... DRTM1010
C ..... DRTM1020
C ..... DRTM1030
C ..... DRTM1040
C ..... DRTM1050
C ..... DRTM1060
C ..... DRTM1070
C ..... DRTM1080
C ..... DRTM1090
C ..... DRTM1100
C ..... DRTM1110
C ..... DRTM1120
C ..... DRTM1130
C ..... DRTM1140
C ..... DRTM1150
C ..... DRTM1160
C ..... DRTM1170
C ..... DRTM1180
C ..... DRTM1190
C ..... DRTM1200
C ..... DRTM1210
C ..... DRTM1220
C ..... DRTM1230
C ..... DRTM1240
C ..... DRTM1250
C ..... DRTM1260
C ..... DRTM1270
C ..... DRTM1280
C ..... DRTM1290

```

Subroutines RTNI and DRTNI

These subroutines refine the initial guess x_0 of a root of the general nonlinear equation $f(x) = 0$. Newton's iteration scheme is used in the following form:

$$x_{i+1} = x_i - \frac{f(x_i)}{f'(x_i)} \quad (i = 0, 1, 2, \dots) \quad (1)$$

Convergence is quadratic or linear if the multiplicity of the root to be determined is equal to one or greater than one respectively, and if $f(x)$ can be differentiated continuously at least twice in the range in which iteration moves. Each iteration step requires one evaluation of $f(x)$ and one evaluation of $f'(x)$.

This iterative procedure is terminated if the following two conditions are satisfied:

$$\delta \leq \epsilon \text{ and } |f(x_{i+1})| \leq 100 \cdot \epsilon$$

$$\text{with } \delta = \left\{ \begin{array}{l} \left| \frac{x_{i+1} - x_i}{x_{i+1}} \right| \text{ in case of } |x_{i+1}| > 1 \\ |x_{i+1} - x_i| \text{ in case of } |x_{i+1}| \leq 1 \end{array} \right\} \quad (2)$$

and tolerance ϵ given by input.

The procedure described above may not converge within a specified number of iteration steps. Reasons for this behaviour, which is indicated by an error message, may be:

1. Too few iteration steps are specified.
2. The initial guess x_0 is too far away from any root.
3. The tolerance ϵ is too small with respect to roundoff errors.
4. The root to be determined is of multiplicity greater than one.

Furthermore, the procedure fails and is bypassed if at any iteration step the derivative $f'(x_i)$ becomes zero. This is also indicated by an error message.

For reference see:

- (1) F. B. Hildebrand, *Introduction to Numerical Analysis*, McGraw-Hill, New York/Toronto/London, 1956, pp. 447 - 450.
- (2) R. Zurmühl, *Praktische Mathematik für Ingenieure und Physiker*, Springer, Berlin/Göttingen/Heidelberg, 1963, pp. 12 - 17.

```

C      RTNI 10
C      RTNI 20
C      RTNI 30
C      SUBROUTINE RTNI
C      RTNI 40
C      PURPOSE
C      TO SOLVE GENERAL NONLINEAR EQUATIONS OF THE FORM F(X)=0
C      BY MEANS OF NEWTON-S ITERATION METHOD.
C      RTNI 50
C      RTNI 60
C      RTNI 70
C      RTNI 80
C      RTNI 90
C      USAGE
C      CALL RTNI (X,F,DERF,FCT,XST,EPS,IEND,IER)
C      PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT.
C      RTNI 100
C      RTNI 110
C      RTNI 120
C      DESCRIPTION OF PARAMETERS
C      RTNI 130
C      X - RESULTANT ROOT OF EQUATION F(X)=0.
C      RTNI 140
C      F - RESULTANT FUNCTION VALUE AT ROOT X.
C      RTNI 150
C      DERF - RESULTANT VALUE OF DERIVATIVE AT ROOT X.
C      RTNI 160
C      FCT - NAME OF THE EXTERNAL SUBROUTINE USED. IT COMPUTES
C      TO GIVEN ARGUMENT X FUNCTION VALUE F AND DERIVATIVE
C      RTNI 170
C      DERF. ITS PARAMETER LIST MUST BE X,F,DERF.
C      RTNI 180
C      XST - INPJT VALUE WHICH SPECIFIES THE INITIAL GUESS OF
C      THE ROOT X.
C      RTNI 190
C      EPS - INPJT VALUE WHICH SPECIFIES THE UPPER BOUND OF THE
C      ERROR OF RESULT X.
C      RTNI 200
C      IEND - MAXIMUM NUMBER OF ITERATION STEPS SPECIFIED.
C      RTNI 210
C      IER - RESULTANT ERROR PARAMETER CODED AS FOLLOWS
C      RTNI 220
C      IER=0 - NO ERROR,
C      RTNI 230
C      IER=1 - NO CONVERGENCE AFTER IEND ITERATION STEPS,
C      RTNI 240
C      IER=2 - AT ANY ITERATION STEP DERIVATIVE DERF WAS
C      EQUAL TO ZERO.
C      RTNI 250
C      RTNI 260
C      RTNI 270
C      RTNI 280
C      RTNI 290
C      RTNI 300
C      RTNI 310
C      RTNI 320
C      REMARKS
C      THE PROCEDURE IS BYPASSED AND GIVES THE ERROR MESSAGE IER=2
C      IF AT ANY ITERATION STEP DERIVATIVE OF F(X) IS EQUAL TO 0.
C      POSSIBLY THE PROCEDURE WOULD BE SUCCESSFUL IF IT IS STARTED
C      ONCE MORE WITH ANOTHER INITIAL GUESS XST.
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C      THE EXTERNAL SUBROUTINE FCT(X,F,DERF) MUST BE FURNISHED
C      BY THE USER.
C      METHOD
C      SOLUTION OF EQUATION F(X)=0 IS DONE BY MEANS OF NEWTON-S
C      ITERATION METHOD, WHICH STARTS AT THE INITIAL GUESS XST OF
C      A ROOT X. CONVERGENCE IS QUADRATIC IF THE DERIVATIVE OF
C      F(X) AT ROOT X IS NOT EQUAL TO ZERO. ONE ITERATION STEP
C      REQUIRES ONE EVALUATION OF F(X) AND ONE EVALUATION OF THE
C      DERIVATIVE OF F(X). FOR TEST ON SATISFACTORY ACCURACY SEE
C      FORMULAE (2) OF MATHEMATICAL DESCRIPTION.
C      FOR REFERENCE, SEE R. ZURMUEHL, PRAKTIISCHE MATHEMATIK FUER
C      INGENIEURE UND PHYSIKER, SPRINGER, BERLIN/GOETTINGEN/
C      HEIDELBERG, 1963, PP.12-17.
C      RTNI 330
C      RTNI 340
C      RTNI 350
C      RTNI 360
C      RTNI 370
C      RTNI 380
C      RTNI 390
C      RTNI 400
C      RTNI 410
C      RTNI 420
C      RTNI 430
C      RTNI 440
C      RTNI 450
C      RTNI 460
C      RTNI 470
C      RTNI 480
C      RTNI 490
C      RTNI 500
C      RTNI 510
C      RTNI 520
C      RTNI 530
C      RTNI 540
C      SUBROUTINE RTNI(X,F,DERF,FCT,XST,EPS,IEND,IER)
C      RTNI 550
C      RTNI 560
C      RTNI 570
C      RTNI 580
C      RTNI 590
C      RTNI 600
C      RTNI 610
C      RTNI 620
C      RTNI 630
C      RTNI 640
C      RTNI 650
C      RTNI 660
C      RTNI 670
C      RTNI 680
C      RTNI 690
C      RTNI 700
C      EQUATION IS NOT SATISFIED BY X
C      1 IF(DERF)2,8,2
C      RTNI 710
C      RTNI 720
C      RTNI 730
C      ITERATION IS POSSIBLE
C      2 DX=F/DERF
C      X=X-DX
C      TOL=X
C      CALL FCT(TOL,F,DERF)
C      RTNI 740
C      RTNI 750
C      RTNI 760
C      RTNI 770
C      RTNI 780
C      RTNI 790
C      TEST ON SATISFACTORY ACCURACY
C      TOL=EPS
C      A=ABS(X)
C      IF(A-1.)4,4,3
C      RTNI 800
C      RTNI 810
C      RTNI 820
C      RTNI 830
C      RTNI 840
C      RTNI 850
C      RTNI 850
C      RTNI 870
C      RTNI 880
C      RTNI 890
C      END OF ITERATION LOOP
C      RTNI 900
C      RTNI 910
C      NO CONVERGENCE AFTER IEND ITERATION STEPS. ERROR RETURN.
C      IER=1
C      RTNI 920
C      RTNI 930
C      7 RETURN
C      ERROR RETURN IN CASE OF ZERO DIVISOR
C      RTNI 940
C      RTNI 950
C      RTNI 960
C      RTNI 970
C      RTNI 980
C      RTNI 990
    
```



```

C ..... DRTN 10
C ..... DRTN 20
C ..... DRTN 30
C ..... DRTN 40
C ..... DRTN 50
C ..... DRTN 60
C ..... DRTN 70
C ..... DRTN 80
C ..... DRTN 90
C ..... DRTN 100
C ..... DRTN 110
C ..... DRTN 120
C ..... DRTN 130
C ..... DRTN 140
C ..... DRTN 150
C ..... DRTN 160
C ..... DRTN 170
C ..... DRTN 180
C ..... DRTN 190
C ..... DRTN 200
C ..... DRTN 210
C ..... DRTN 220
C ..... DRTN 230
C ..... DRTN 240
C ..... DRTN 250
C ..... DRTN 260
C ..... DRTN 270
C ..... DRTN 280
C ..... DRTN 290
C ..... DRTN 300
C ..... DRTN 310
C ..... DRTN 320
C ..... DRTN 330
C ..... DRTN 340
C ..... DRTN 350
C ..... DRTN 360
C ..... DRTN 370
C ..... DRTN 380
C ..... DRTN 390
C ..... DRTN 400
C ..... DRTN 410
C ..... DRTN 420
C ..... DRTN 430
C ..... DRTN 440
C ..... DRTN 450
C ..... DRTN 460
C ..... DRTN 470
C ..... DRTN 480
C ..... DRTN 490
C ..... DRTN 500
C ..... DRTN 510
C ..... DRTN 520
C ..... DRTN 530
C ..... DRTN 540
C ..... DRTN 550
C ..... DRTN 560
C ..... DRTN 570
C ..... DRTN 580
C ..... DRTN 590
C ..... DRTN 600
C ..... DRTN 610
C ..... DRTN 620
C ..... DRTN 630
C ..... DRTN 640
C ..... DRTN 650
C ..... DRTN 660
C ..... DRTN 670
C ..... DRTN 680
C ..... DRTN 690
C ..... DRTN 700
C ..... DRTN 710
C ..... DRTN 720
C ..... DRTN 730
C ..... DRTN 740
C ..... DRTN 750
C ..... DRTN 760
C ..... DRTN 770
C ..... DRTN 780
C ..... DRTN 790
C ..... DRTN 800
C ..... DRTN 810
C ..... DRTN 820
C ..... DRTN 830
C ..... DRTN 840
C ..... DRTN 850
C ..... DRTN 860
C ..... DRTN 870
C ..... DRTN 880
C ..... DRTN 890
C ..... DRTN 900
C ..... DRTN 910
C ..... DRTN 920
C ..... DRTN 930
C ..... DRTN 940
C ..... DRTN 950
C ..... DRTN 960
C ..... DRTN 970
C ..... DRTN 980
C ..... DRTN 990
C ..... DRTN1000
C ..... DRTN1010
C ..... DRTN1020
C ..... DRTN1030
SUBROUTINE DRTNI
PURPOSE
TO SOLVE GENERAL NONLINEAR EQUATIONS OF THE FORM F(X)=0
BY MEANS OF NEWTON-S ITERATION METHOD.
USAGE
CALL DRTNI (X,F,DERF,FCT,XST,EPS,IEND,IER)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT.
DESCRIPTION OF PARAMETERS
X - DOUBLE PRECISION RESULTANT ROOT OF EQUATION F(X)=0.
F - DOUBLE PRECISION RESULTANT FUNCTION VALUE AT
ROOT X.
DERF - DOUBLE PRECISION RESULTANT VALUE OF DERIVATIVE
AT ROOT X.
FCT - NAME OF THE EXTERNAL SUBROUTINE USED. IT COMPUTES
TO GIVEN ARGUMENT X FUNCTION VALUE F AND DERIVATIVE
DERF. ITS PARAMETER LIST MUST BE X,F,DERF, WHERE
ALL PARAMETERS ARE DOUBLE PRECISION.
XST - DOUBLE PRECISION INPUT VALUE WHICH SPECIFIES THE
INITIAL GUESS OF THE ROOT X.
EPS - SINGLE PRECISION INPUT VALUE WHICH SPECIFIES THE
UPPER BOUND OF THE ERROR OF RESULT X.
IEND - MAXIMUM NUMBER OF ITERATION STEPS SPECIFIED.
IER - RESULTANT ERROR PARAMETER CODED AS FOLLOWS
IER=0 - NO ERROR.
IER=1 - NO CONVERGENCE AFTER IEND ITERATION STEPS.
IER=2 - AT ANY ITERATION STEP DERIVATIVE DERF WAS
EQUAL TO ZERO.
REMARKS
THE PROCEDURE IS BYPASSED AND GIVES THE ERROR MESSAGE IER=2
IF AT ANY ITERATION STEP DERIVATIVE OF F(X) IS EQUAL TO 0.
POSSIBLY THE PROCEDURE WOULD BE SUCCESSFUL IF IT IS STARTED
ONCE MORE WITH ANOTHER INITIAL GUESS XST.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL SUBROUTINE FCT(X,F,DERF) MUST BE FURNISHED
BY THE USER.
METHOD
SOLUTION OF EQUATION F(X)=0 IS DONE BY MEANS OF NEWTON-S
ITERATION METHOD, WHICH STARTS AT THE INITIAL GUESS XST OF
A ROOT X. CONVERGENCE IS QUADRATIC IF THE DERIVATIVE OF
F(X) AT ROOT X IS NOT EQUAL TO ZERO. ONE ITERATION STEP
REQUIRES ONE EVALUATION OF F(X) AND ONE EVALUATION OF THE
DERIVATIVE OF F(X). FOR TEST ON SATISFACTORY ACCURACY SEE
FORMULAE (2) OF MATHEMATICAL DESCRIPTION.
FOR REFERENCE, SEE R. ZURMUEHL, PRAKTISCHE MATHEMATIK FUER
INGENIEURE UND PHYSIKER, SPRINGER, BERLIN/GOETTINGEN/
HEIDELBERG, 1963, PP. 12-17.
.....
SUBROUTINE DRTNI(X,F,DERF,FCT,XST,EPS,IEND,IER)
DOUBLE PRECISION X,F,DERF,XST,TOL,TOLF,DX,A
PREPARE ITERATION
IER=0
X=XST
TOL=X
CALL FCT(TOL,F,DERF)
TOLF=100.*EPS
START ITERATION LOOP
DO 6 I=1,IEND
IF(F)1,7,1
EQUATION IS NOT SATISFIED BY X
1 IF(DERF)2,8,2
ITERATION IS POSSIBLE
2 DX=F/DERF
X=X-DX
TOL=X
CALL FCT(TOL,F,DERF)
TEST ON SATISFACTORY ACCURACY
TOL=EPS
A=DABS(X)
IF(A-1.DD)4,4,3
3 TOL=TOL*A
4 IF(DABS(DX)-TOL)5,5,6
5 IF(DABS(F)-TOLF)7,7,6
6 CONTINUE
END OF ITERATION LOOP
NO CONVERGENCE AFTER IEND ITERATION STEPS. ERROR RETURN.
IER=1
7 RETURN
ERROR RETURN IN CASE OF ZERO DIVISOR
8 IER=2
RETURN
END

```

Extremum of Functions

Subroutines FMFP and DFMFP

These subroutines perform the calculation of an unconstrained minimum of a function of several variables using a method proposed by Davidon. The underlying method is described in the article by R. Fletcher and M.J.D. Powell, "A Rapidly Convergent Descent Method for Minimization", Computer Journal, vol. 6, iss. 2, 1963, pp. 163 - 168.

It is assumed that the function f of the n variables x_1, \dots, x_n (abbreviated as argument vector x) may be computed together with its gradient vector $g(x)$ for any point x . The generalized Taylor expansion for functions of several variables is

$$f(x+u) = f(x) + g(x) \cdot u + \frac{1}{2} u^T G(x)u + \text{higher terms}$$

where g is the gradient vector and G the matrix of second order partial derivatives. Vectors are assumed to be column vectors; u^T means transpose of vector u . It is assumed that in the neighborhood of the required minimum x_{\min} the function is approximated closely by the first three terms of its Taylor expansion, giving

$$f(x) = f(x_{\min}) + \frac{1}{2} (x - x_{\min})^T G(x_{\min}) (x - x_{\min})$$

since $g(x_{\min}) = 0$. Then the gradient is seen to be approximately $g(x) = G(x_{\min}) (x - x_{\min})$.

Assume now that the symmetric matrix G is positive definite. Then the following equation holds true:

$$x - x_{\min} = G^{-1} (x_{\min}) \cdot g(x)$$

which would allow x_{\min} to be calculated in one step if $G^{-1}(x_{\min})$ were available.

To approach $G^{-1}(x_{\min})$, a method of successive linear searches in G -conjugate directions is used. Starting with the identity matrix $G^{(0)} = I$, a sequence of symmetric matrices $G^{(i)}$ is generated which tends to G^{-1} . At the $(i+1)^{st}$ iteration step a linear search is made in direction $h^{(i)} = -G^{(i)}g^{(i)}$, where $g^{(i)}$ is an abbreviation for $g(x^{(i)})$. By means of the linear search the minimum of $y(t) = f(x^{(i)} + t \cdot h^{(i)})$ is determined, giving argument $x^{(i+1)} = x^{(i)} + t_j \cdot h^{(i)}$.

The argument of the minimum $x^{(i+1)}$ on the line through $x^{(i)}$ in direction $h^{(i)}$ is determined by the relation that scalar product $(g^{(i+1)}, h^{(i)}) = 0$.

Now:
$$x^{(n)} = x^{(j)} + \sum_{i=j}^{n-1} t_i h^{(i)}$$

and:
$$g^{(n)} = g^{(j)} + \sum_{i=j}^{n-1} t_i Gh^{(i)}$$

Therefore:

scalar product
$$(g^{(n)}, h^{(j)}) = \sum_{i=j+1}^{n-1} t_i (Gh^{(i)}, h^{(j)})$$

Suppose now that the vectors $h^{(0)}, h^{(1)}, \dots, h^{(n-1)}$ are G -conjugate, satisfying $(Gh^{(i)}, h^{(j)}) = 0$ for $i \neq j$. Then $(g^{(n)}, h^{(j)}) = 0$, and since $h^{(0)}, h^{(1)}, \dots, h^{(n-1)}$ form a basis, $g^{(n)} = 0$ and $x^{(n)} = x_{\min}$. This shows that the minimum is located at the n^{th} iteration for a quadratic function when using successive linear searches for G -conjugate directions.

For the generation of G-conjugate directions, start with $h^{(0)} = -g^{(0)}$ and calculate successive directions $h^{(i)}$ by means of $h^{(i)} = -G^{(i)}g^{(i)}$, where $G^{(i)}$ is modified to $G^{(i+1)}$ so that $h^{(i)}$ is an eigenvector of the matrix $G^{(i+1)}$ with eigenvalue 1. This ensures that $G^{(i)}$ approaches G^{-1} as $x^{(i)}$ approaches x_{\min} . An easy calculation shows:

$$G^{(i+1)} = G^{(i)} + \frac{dx \cdot dx^T}{dx^T \cdot dg} - \frac{G^{(i)} dg \cdot dg^T G^{(i)}}{dg^T G^{(i)} dg}$$

with $dg = g^{(i+1)} - g^{(i)}$

$$dx = x^{(i+1)} - x^{(i)}$$

where all vectors are regarded as column vectors, and superscript T means transpose of column vector--that is, row vector.

The strategy adopted for termination of the successive linear searches is as follows:

1. If the function value has not decreased in the last iteration step, the search for the minimum is terminated provided the gradient is already sufficiently small; otherwise, the next step is in the direction of steepest descent.

2. If the argument vector and the direction vector change by very small amounts, and at least n iterations are performed, the minimization is terminated again.

3. If the number of iterations exceeds an upper bound furnished by the user, further calculation is bypassed, and an error code is set to 1 indicating poor convergence.

4. If one of the successive linear searches indicates that no constrained minimum exists, further calculation is bypassed again, and the error code is set to 2 indicating that it is likely that no minimum exists.

The i^{th} term $G^{(i)}$ is reset to the identity matrix if there is indication that the current $G^{(i)}$ is not positive definite, or if the formula for $G^{(i+1)}$ breaks down due to zero divisors.

The linear search technique used in subroutines FMFP and DFMP is as follows. For a given argument vector x and vector h , defining a direction through x , a local minimum of the function $y(t) = f(x+th)$ must be found. This means that a value t_m must be determined for which

$$y'(t_m) = \text{scalar product } (g(x+t_m h), h) = 0$$

From $y'(0) = (g(x), h) < 0$ it is evident that a minimum $y(t_m) < y(0)$ should be found for positive values of t .

The calculation of the minimum is in three stages. The first estimates the magnitude of t_m , the second determines an interval containing t_m , and the third interpolates the value of t_m .

An estimate of the step-size may be obtained, assuming that the true value of the constrained minimum is equal to the estimated value EST of the unconstrained minimum and that $y(t)$ is closely represented by a quadratic polynomial passing through $(x, y(0))$ with derivative $y'(0)$:
step = 2 (EST - $y(0)$)/ $y'(0)$.

This equation tends to overestimate the step-size, since the unconstrained minimum will normally not lie on the line through x with direction h . Therefore, step is taken as step-size s only if it is positive and less than one. Otherwise, $s = 1$ is taken as step-size.

At the second stage $y(t)$ and $y'(t)$ are examined at the points $t = s, 2s, 4s, \dots, s_1, s_2$, where successive values are obtained by doubling the step-size.

This search is terminated at $t = s_2$ if:

$$y'(s_2) = 0, \text{ or } y'(s_2) > 0, \text{ or } y(s_2) \geq y(s_1)$$

$$\text{or if } s_2 \cdot \left(\sum_{i=1}^n |h_i| \right) > 10^{10}.$$

The last case (search argument runs out of range) is interpreted as an indication that no local minimum exists on the given line. In this case, the error indicator is set to (2) and further calculation is bypassed.

In case $y'(s_2) = 0$, t_m is set to s_2 and $x_m = x + s_2 h$ is used as the argument of a constrained minimum on the line through x with direction h .

In the second and third case ($y'(s_2) > 0$ and/or $y(s_2) \geq y(s_1)$) a minimum lies necessarily between s_1 and s_2 . Its argument value gets approximated using cubic interpolation.

The extrema of the cubic interpolation passing through $(s_1, y_1 = y(s_1), y'_1 = y'(s_1))$ and $(s_2, y_2 = y(s_2), y'_2 = y'(s_2))$ are given by solving a quadratic equation. The solution s_3 can be expressed as

$$s_3 = s_1 + (1-\alpha)(s_2-s_1) = s_2 - \alpha(s_2 - s_1) \text{ with}$$

$$\alpha = \frac{y'_2 - z + w}{y'_2 - y'_1 + 2W} = \frac{y'_2 + z - w}{y'_2 + y'_1 + 2z},$$

$$0 < \alpha < 1, \text{ and } z = y'_1 + y'_2 - 3 \frac{y_2 - y_1}{s_2 - s_1},$$

$$w = \pm (z^2 - y'_1 y'_2)^{1/2}.$$

The conditions on the problem guarantee a real value of w . The sign of w is so chosen that s_3 is in the interval (s_1, s_2) . If this condition is satisfied for the two possible values of s_3 , the value closer to s_1 is retained.

As written above, two equivalent formulas can provide α . The choice is based on numerical stability considerations.

If $y(s_3) \leq y(s_1)$ and $y(s_3) \leq y(s_2)$, then t_m is set equal to s_3 and $x_m = x + t_m h$ is used as argument of the desired minimum along the given line. Otherwise, the interval (s_1, s_2) is reduced by replacing s_1 by s_3 if $y(s_3) \leq y(s_1)$ and $y'(s_3) < 0$ and by replacing s_2 by s_3 in all other cases. The interpolation process is repeated for this new reduced interval.

```

C
C ..... FMPF 10
C ..... FMPF 20
C ..... FMPF 30
C ..... FMPF 40
C ..... FMPF 50
C ..... FMPF 60
C ..... FMPF 70
C ..... FMPF 80
C ..... FMPF 90
C ..... FMPF 100
C ..... FMPF 110
C ..... FMPF 120
C ..... FMPF 130
C ..... FMPF 140
C ..... FMPF 150
C ..... FMPF 160
C ..... FMPF 170
C ..... FMPF 180
C ..... FMPF 190
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C ..... FMPF 390
C ..... FMPF 400
C ..... FMPF 410
C ..... FMPF 420
C ..... FMPF 430
C ..... FMPF 440
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C ..... FMPF 950
C ..... FMPF 960
C ..... FMPF 970
C ..... FMPF 980
C ..... FMPF 990
C ..... FMPF1000
C ..... FMPF1010
C ..... FMPF1020
C ..... FMPF1030
C ..... FMPF1040
C ..... FMPF1050
C ..... FMPF1060
C ..... FMPF1070
C ..... FMPF1080
C ..... FMPF1090
C ..... FMPF1100
C ..... FMPF1110

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```

GC TC 8
? N=1
8 CENTIALE
5 F(LJ)=T
C
C CHECK WHETHER FUNCTION WILL DECREASE STEPPING ALONG H.
CY=C.
PARP=C.
GARP=C.
C
C CALCULATE DIRECTIONAL DERIVATIVE AND TESTVALUES FOR DIRECTION
VECTOR H AND GRADIENT VECTOR G.
CC IC J=1,N
PARP=PARP+ABS(F(J))
GARP=GARP+ABS(G(J))
IC CY=CY+F(LJ)*G(LJ)
C
C REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF DIRECTIONAL
DERIVATIVE APPEARS TO BE POSITIVE OR ZERO.
IF(CY)11,21,51
C
C REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF DIRECTION
VECTOR H IS SMALL COMPARED TO GRADIENT VECTOR G.
11 IF((GARP/GARP-EP5)15,15,12
C
C SEARCH FOR MINIMUM ALONG DIRECTION H
C
C SEARCH ALONG H FOR POSITIVE DIRECTIONAL DERIVATIVE
12 F=F+
ALFA=2*(EST-F)/CY
APRCA=1.
C
C USE ESTIMATE FOR STEP SIZE ONLY IF IT IS POSITIVE AND LESS THAN
1. OTHERWISE TAKE 1. AS STEP SIZE
IF(ALFA)15,15,13
13 IF(ALFA-APRCA)14,15,15
14 APRCA=ALFA
15 ALFA=C.
C
C SAVE FUNCTION AND DERIVATIVE VALUES FOR GLC ARGUMENT
16 F=F+
CY=C
C
C STEP ARGUMENT ALONG H
CC 17 J=1,N
17 X(J)=X(J)+APRCA*H(J)
C
C COMPLETE FUNCTION VALUE AND GRADIENT FOR NEW ARGUMENT
F=F+
CY=C
C
C COMPLETE DIRECTIONAL DERIVATIVE BY FOR NEW ARGUMENT. TERMINATE
SEARCH, IF CY IS POSITIVE. IF CY IS ZERO THE MINIMUM IS FOUND
CY=C.
CC 18 J=1,N
CY=C+G(LJ)*H(J)
IF(CY)15,36,22
C
C TERMINATE SEARCH ALSO IF THE FUNCTION VALUE INDICATES THAT
A MINIMUM HAS BEEN PASSED
15 IF(F-F)12C,22,22
C
C REPEAT SEARCH AND DOUBLE STEP SIZE FOR FURTHER SEARCHES
2C APRCA=APRCA*ALFA
ALFA=APRCA
END OF SEARCH LCCP
C
C TERMINATE IF THE CHANGE IN ARGUMENT GETS VERY LARGE
IF((N*APRCA-LE10)16,16,21
C
C LINEAR SEARCH TECHNIQUE INDICATES THAT NO MINIMUM EXISTS
21 IER=2
RETURN
C
C INTERPOLATE LINEARLY IN THE INTERVAL DEFINED BY THE SEARCH
ARGUE AND COMPUTE THE ARGUMENT X FOR WHICH THE INTERPOLATION
POLYNOMIAL IS MINIMIZED
22 T=C.
23 IF(APRCA)24,36,24
24 Z=3*(F-FY)/APRCA+CY+CY
ALFA=APRCA*(ABS(Z),ABS(OX),ABS(CY))
CALFA=Z/ALFA
CALFA=ALFA*CALFA-CY/ALFA+CY/ALFA
IF(CALFA)25,25,25
25 W=ALFA*SCAL(CALFA)
ALFA=CY-CX+W
IF(ALFA)25C,25,25C
25C ALFA=CY-2*W/ALFA
GC TC 25C
25I ALFA=(Z-CY-W)/(Z+CX+Z+CY)
252 ALFA=APRCA*ALFA
CC 26 J=1,N
26 X(J)=X(J)+ALFA*H(J)
C
C TERMINATE, IF THE VALUE OF THE ACTUAL FUNCTION AT X IS LESS
THAN THE FUNCTION VALUES AT THE INTERVAL ENDS. OTHERWISE REDUCE
THE INTERVAL BY CHOOSING THE END-POINT EQUAL TO X AND REPEAT
IF THE INTERPOLATION WHICH END-POINT IS CHOSEN DEPENDS ON THE
VALUE OF THE FUNCTION AND ITS GRADIENT AT X
CALL FUNCT(N,X,F,G)
IF(F-F)127,27,20
27 IF(F-F)13C,36,26
28 CALFA=C.
CC 25 J=1,N
25 CALFA=ALFA*G(LJ)+G(LJ)
IF(CALFA)30,33,33
30 IF(F-F)132,31,33
31 IF(CX-CALFA)32,36,32
32 F=F+
CX=CALFA
APRCA=ALFA
CC IC 22
33 IF(F-F)125,34,35
34 IF(CY-CALFA)15,36,35
35 F=F+
CY=CALFA
APRCA=APRCA-ALFA
GC TC 22
C
C TERMINATE, IF FUNCTION HAS ACT DECREASED DURING LAST ITERATION
36 IF(CY<F-4*EP5)51,36,36
C
C COMPLETE DIFFERENCE VECTORS OF ARGUMENT AND GRADIENT FROM
THE CONSECUTIVE ITERATIONS
3C CC 27 J=1,N
N=N+1
F(K)=G(LJ)+F(K)
K=K+K

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```

37 F(K)=F(J)-F(K)
C
C
C TEST LENGTH OF ARGUMENT VECTOR AND DIRECTION VECTOR
C IF AT LEAST N ITERATIONS HAVE BEEN EXECUTED, TERMINATE, IF
C NOT ARE LESS THAN EPS
C
C IER=C
C IF (K-LIMIT)/4.2>3.2
35 T=C.
C Z=C.
C EC 4C J=1,N
C N=N+J
C M=F(K)
C T=T+ZES(F(K))
C Z=Z+M*(K)
C IF (N-EPSS)4.1+4.42
41 IF (T-EPSS)5.6+5.42
C
C TERMINATE, IF NUMBER OF ITERATIONS WOULD EXCEED LIMIT
42 IF (K-LIMIT)/4.3>5.5
C
C PREPARE UPDATING OF MATRIX F
43 ALF=C.
C EC 47 J=1,N
C N=N+J
C M=C.
C EC 4C L=1,N
C KL=A+L
C N=N+L
C B=B+F*(K)
C IF (L-J)44+45+45
44 N=N+N
C EC IC 4E
45 N=N+1
46 C=CONTINUE
C N=N+J
C ALFA=ALFA+B*(K)
47 F(J)=B
C
C REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF RESULTS
C ARE NOT SATISFACTORY
C IF (Z/ALFA)46+1+40
C
C UPDATE MATRIX F
48 N=N+1
C EC 45 L=1,N
C KL=A+L
C EC 45 J=L,N
C NJ=N+J
C F(K)=F(K)+F(K)
C IF (L-J)44+45+45
45 N=N+1
C EC IC 5
C END OF ITERATION LCCP
C
C NO CONVERGENCE AFTER LIMIT ITERATIONS
50 IER=1
C RETURN
C
C RESERVE OLD VALUES OF FUNCTION AND ARGUMENTS
51 EC 52 J=1,N
C N=N+J
52 X(J)=F(K)
C CALL FUNCT(N,X,F,G)
C
C REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF DERIVATIVE
C FALLS TO BE SUFFICIENTLY SMALL
C IF (GARP-EPSS)55+55.53
C
C TEST FOR REPEATED FAILURE OF ITERATION
53 IF (IER)56.54+54
54 IER=-1
C EC IC 1
55 IER=C
56 RETURN
C
C
C
C
C .....
C SLERCLINE EPFPF
C
C PLFPESE
C TO FIND A LOCAL MINIMUM OF A FUNCTION OF SEVERAL VARIABLES
C BY THE METHOD OF FLETCHER AND POWELL
C
C LSAFE
C CALL EPFP(FUNCT,N,X,F,G,EST,EPS,LIMIT,IER,M)
C
C DESCRIPTION OF PARAMETERS
C FLACT - USER-WRITTEN SLERCLINE CONCERNING THE FUNCTION TO
C BE MINIMIZED, IT MUST BE OF THE FORM
C SLERCLINE FLACT(N,ARG,VAL,GRAD)
C AND MUST SERVE THE FOLLOWING PURPOSE
C FOR EACH N-DIMENSIONAL ARGUMENT VECTOR ARG,
C FUNCTION VALUE AND GRADIENT VECTOR MUST BE COMPUTED
C AND, ON RETURN, STORED IN VAL AND GRAD RESPECTIVELY
C ARG, VAL AND GRAD MUST BE OF DOUBLE PRECISION.
C N - NUMBER OF VARIABLES
C M - VECTOR OF DIMENSION N CONTAINING THE INITIAL
C ARGUMENT WHERE THE ITERATION STARTS, ON RETURN,
C X HELDS THE ARGUMENT CORRESPONDING TO THE
C COMPUTED MINIMUM FUNCTION VALUE
C DOUBLE PRECISION VECTOR.
C F - SINGLE VARIABLE CONTAINING THE MINIMUM FUNCTION
C VALUE ON RETURN, I.E. F=F(X).
C DOUBLE PRECISION VARIABLE.
C G - VECTOR OF DIMENSION N CONTAINING THE GRADIENT
C VECTOR CORRESPONDING TO THE MINIMUM ON RETURN,
C I.E. G=G(X).
C DOUBLE PRECISION VECTOR.
C EST - IS AN ESTIMATE OF THE MINIMUM FUNCTION VALUE.
C DOUBLE PRECISION VARIABLE.
C EPS - RESIDUAL REPRESENTING THE EXPECTED ABSOLUTE ERROR.
C A REASONABLE CHOICE IS 10**(-10), I.E.
C SCREEN+1 GREATER THAN 10**(-D), WHERE D IS THE
C NUMBER OF SIGNIFICANT DIGITS IN FLOATING POINT
C REPRESENTATION.
C DOUBLE PRECISION VARIABLE.
C LIMIT - MAXIMUM NUMBER OF ITERATIONS.
C IER - ERROR PARAMETER
C IER = C MEANS CONVERGENCE WAS OBTAINED
C IER = 1 MEANS NO CONVERGENCE IN LIMIT ITERATIONS
C IER = -1 MEANS ERRORS IN GRADIENT CALCULATION
C IER = 2 MEANS LINEAR SEARCH TECHNIQUE INDICATES
C IT IS LIKELY THAT THERE EXISTS A MINIMUM.
C F - WORKING STORAGE OF DIMENSION N*(N+7)/2.
C DOUBLE PRECISION ARRAY.
C
C REMARKS
C 1) THE SLERCLINE NAME REPLACING THE DUMMY ARGUMENT FUNCT
C MUST BE DECLARED AS EXTERNAL IN THE CALLING PROGRAM.
C 2) IER IS SET TO 2 IF, STEPPING IN ONE OF THE COMPUTED

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C      TERMINATE IF THE CHANGE IN ARGUMENT GETS VERY LARGE      DFMF1000
      IF (HARR-APBCA-1.E10)/16.16.21      DFMF1000
C
C      LINEAR SEARCH TECHNIQUE INDICATES THAT NO MINIMUM EXISTS      DFMF1000
      21 IER=2      DFMF1010
      RETURN      DFMF1020
C      INTERPOLATE QUADRATICALLY IN THE INTERVAL DEFINED BY THE SEARCH      DFMF1030
      ARGUMENT AND COMPLETE THE ARGUMENT X FOR WHICH THE INTERPOLATION      DFMF1040
      POLYNOMIAL IS MINIMIZED      DFMF1050
      22 T=C.EC      DFMF1060
      23 IF (APBCA) 24.36.24      DFMF1070
      24 Z=C.CC*(B-F)/APBDA+CX+CY      DFMF1080
      ALFA=C*ABS(CAES(2),C*ABS(CX),C*ABS(CY))      DFMF1090
      CALFA=Z/ALFA      DFMF1100
      CALFA=CALFA+CALFA-CX/ALFA+CY/ALFA      DFMF1110
      IF (CALFA) 25.25.25      DFMF1120
      25 N=ALFA*CSORT(CALFA)      DFMF1130
      ALFA=CY-EX+6*6      DFMF1140
      IF (ALFA) 25C.251.25C      DFMF1150
      25C ALFA=(CY-2*N)/ALFA      DFMF1160
      CC TC 252      DFMF1170
      251 ALFA=(Z+CY-N)/(Z+CX+2*CY)      DFMF1180
      252 ALFA=ALFA*APBCA      DFMF1190
      CC 26 1=1.N      DFMF1200
      26 X((I+1)*(1+(1-ALFA)**I))      DFMF1210
C
C      TERMINATE, IF THE VALUE OF THE ACTUAL FUNCTION AT X IS LESS      DFMF1220
      THAN THE FUNCTION VALUES AT THE INTERVAL ENDS. OTHERWISE REDUCE      DFMF1230
      THE INTERVAL BY CHOOSING ONE END-POINT EQUAL TO X AND REPEAT      DFMF1240
      THE INTERPOLATION. WHICH END-POINT IS CHOSEN DEPENDS ON THE      DFMF1250
      VALUE OF THE FUNCTION AND ITS GRADIENT AT X      DFMF1260
C
      CALL FUNCTA(N,F,G)      DFMF1270
      IF (F-FR) 27.27.28      DFMF1280
      27 IF (F-C) 28.28.28      DFMF1290
      28 CALFA=C.EC      DFMF1300
      CC 29 1=1.N      DFMF1310
      29 CALFA=CALFA+G((I+1)*I)      DFMF1320
      IF (CALFA) 30.33.33      DFMF1330
      30 IF (F-FR) 32.31.33      DFMF1340
      31 IF (CX-CALFA) 32.36.32      DFMF1350
      32 F=F+G      DFMF1360
      CX=CALFA      DFMF1370
      T=ALFA      DFMF1380
      APBCA=ALFA      DFMF1390
      CC TC 22      DFMF1400
      33 IF (FV-F) 35.24.35      DFMF1410
      34 IF (CY-CALFA) 35.36.35      DFMF1420
      35 FV=F      DFMF1430
      CY=CALFA      DFMF1440
      APBCA=APBCA-ALFA      DFMF1450
      CC TC 22      DFMF1460
C
C      TERMINATE, IF FUNCTA HAS ACT DECREASED DURING LAST ITERATION      DFMF1470
      36 IF (CCLF-F) 35.35.36.36      DFMF1480
C
C      COMPUTE DIFFERENCE VECTORS OF ARGUMENT AND GRADIENT FROM      DFMF1490
      THE CONSECUTIVE ITERATIONS      DFMF1500
      37 CC 37 J=1.N      DFMF1510
      K=N+J      DFMF1520
      F(K)=G(J)-G(K)      DFMF1530
      G(K)=G(J)      DFMF1540
      37 F(K)=X(J)-X(K)      DFMF1550
C
C      TEST LENGTH OF ARGUMENT DIFFERENCE VECTOR AND DIRECTION VECTOR      DFMF1560
      IF AT LEAST A ITERATIONS HAVE BEEN EXECUTED. TERMINATE, IF      DFMF1570
      BOTH ARE LESS THAN EPS      DFMF1580
      IER=C      DFMF1590
      IF (KCLAT-N) 42.35.42      DFMF1600
      35 T=C.EC      DFMF1610
      Z=C.EC      DFMF1620
      CC 4C J=1.N      DFMF1630
      K=N+J      DFMF1640
      K=N+K      DFMF1650
      F(K)=G(J)-G(K)      DFMF1660
      IF (C*CAES(I,K))      DFMF1670
      4C Z=Z+6*6*(K)      DFMF1680
      IF (HARR-EFS) 41.41.42      DFMF1690
      41 IF (T-EFS) 56.56.42      DFMF1700
C
C      TERMINATE, IF NUMBER OF ITERATIONS WOULD EXCEED LIMT      DFMF1710
      42 IF (KCLAT-LIMIT) 43.5C.5C      DFMF1720
C
C      PREPARE UPDATING OF MATRIX F      DFMF1730
      43 ALFA=C.EC      DFMF1740
      CC 4J J=1.N      DFMF1750
      N=N+2      DFMF1760
      W=C.EC      DFMF1770
      CC 4E L=1.N      DFMF1780
      KL=N+L      DFMF1790
      W=N+6*(KL)*6*(K)      DFMF1800
      IF (L-J) 44.45.45      DFMF1810
      44 N=N+L      DFMF1820
      CC TC 4E      DFMF1830
      45 N=N+1      DFMF1840
      46 CC(T) 4E      DFMF1850
      N=N+J      DFMF1860
      ALFA=ALFA+6*6*(K)      DFMF1870
      47 F(J)=6      DFMF1880
C
C      REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF RESULTS      DFMF1890
      ARE NOT SATISFACTORY      DFMF1900
      IF (Z*ALFA) 46.1.46      DFMF1910
C
C      UPDATE MATRIX F      DFMF1920
      48 N=N+1      DFMF1930
      CC 4S L=1.N      DFMF1940
      KL=N+L      DFMF1950
      CC 4S J=L.N      DFMF1960
      N=N+2      DFMF1970
      F(K)=F(J)+6*(KL)*6*(KJ)/2-H(L)*6*(J)/ALFA      DFMF1980
      45 N=N+1      DFMF1990
      CC TC 5      DFMF2000
C
C      END OF ITERATION LCCP      DFMF2010
C
C      NO CONVERGENCE AFTER LIMIT ITERATIONS      DFMF2020
      51 IER=1      DFMF2030
      RETURN      DFMF2040
C
C      RESTORE OLD VALUES OF FUNCTA AND ARGUMENTS      DFMF2050
      51 CC 52 J=1.N      DFMF2060
      N=N+J      DFMF2070
      52 F(J)=F(K)      DFMF2080
      CALL FUNCTA(N,F,G)      DFMF2090
C
C      REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF DERIVATIVE      DFMF2100
      FAILS TO BE SUFFICIENTLY SMALL      DFMF2110
      IF (GARR-EFS) 55.55.53

```

```

      TEST FOR REPEATED FAILURE OF ITERATION
      53 IF (IER) 56.54.54
      54 IER=1
      CC IC 1
      55 IER=C
      56 IER=A
      EAC

```

- DFMF3120
- DFMF3130
- DFMF3140
- DFMF3150
- DFMF3160
- DFMF3170
- DFMF3180
- DFMF3190

Subroutines FMCG and DFMCG

These subroutines perform the calculation of an unconstrained minimum of a function of several variables using conjugate gradients. The underlying method is described in the article by R. Fletcher and C. M. Reeves, "Function minimization by conjugate gradients", *Computer Journal*, vol. 7, no. 2, 1964, pp. 149-154.

It is assumed that the function $f(x)$ of the n variables x_1, \dots, x_n may be computed, together with its gradient $g(x)$ for any point $x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix}$. In the

neighborhood of the required minimum x_{\min} the function $f(x)$ is approximated closely by the first three terms of its Taylor expansion, giving

$$f(x) = f(x_{\min}) + \frac{1}{2} (x - x_{\min})^T G(x_{\min}) (x - x_{\min})$$

since $g(x_{\min}) = 0$. The quantity $G(x_{\min})$ means the matrix of second-order partial derivatives taken at the point x_{\min} .

From the Taylor expansion, the gradient is seen to be approximately:

$$g(x) = G(x_{\min}) \cdot (x - x_{\min})$$

The condition for the gradient to vanish is:

$$G(x_{\min}) \cdot x = G(x_{\min}) \cdot x_{\min}$$

For solution of these equations, directions $h^{(0)}, h^{(1)}, \dots$ are generated such that $h^{(i+1)}$ is a linear combination of $-g^{(i+1)}(x^{(i+1)})$ and $h^{(0)}, h^{(1)}, \dots, h^{(i)}$, so that G -orthogonality is satisfied, that is, $h^{(i)T} G h^{(j)} = 0$ for $i \neq j$.

An easy calculation gives the following results. If a sequence of successive linear searches in directions $h^{(0)} = -g^{(0)}, h^{(i+1)} = -g^{(i+1)} + \beta_i \cdot h^{(i)}$ is performed with:

$$\beta_i = \frac{(g^{(i+1)}, g^{(i+1)})}{(g^{(i)}, g^{(i)})}, \quad x^{(i+1)} = x^{(i)} + t_i h^{(i)} \quad \text{and}$$

$$(g^{(i+1)}, h^{(i)}) = 0$$

then this process is guaranteed to locate the minimum of a quadratic function in n iterations at most. For general functions the process is iterative rather than n -step. (This is true even for quadratic functions due to roundoff errors.)

Strategy for termination of the successive linear searches is as follows:

1. If the change of the argument is very small, and at least $n + 1$ iterations have been performed, the search for the minimum is terminated.
2. If the function value has not decreased in the last linear search, the minimization is terminated.
3. If the number of iterations exceeds an upper bound furnished by the user, further calculation is bypassed, and an error code is set to 1 indicating poor convergence.
4. If one of the successive linear searches indicates that no constrained minimum exists, further calculation is bypassed, and the error code is set to 2 indicating that it is likely that no minimum exists.
5. After each cycle of $n + 1$ iterations, the next iteration is in the direction of steepest descent.

The linear search technique used in subroutines FMCG and DFMCG is described in the writeup for subroutines FMFP and DFMFP.

```

C      FMCG 10
C      FMCG 20
C      FMCG 30
C      FMCG 40
C      FMCG 50
C      FMCG 60
C      FMCG 70
C      FMCG 80
C      FMCG 90
C      FMCG 100
C      FMCG 110
C      FMCG 120
C      FMCG 130
C      FMCG 140
C      FMCG 150
C      FMCG 160
C      FMCG 170
C      FMCG 180
C      FMCG 190
C      FMCG 200
C      FMCG 210
C      FMCG 220
C      FMCG 230
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C      FMCG 360
C      FMCG 370
C      FMCG 380
C      FMCG 390
C      FMCG 400
C      FMCG 410
C      FMCG 420
C      FMCG 430
C      FMCG 440
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C      FMCG 690
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C      FMCG 840
C      FMCG 850
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C      FMCG 960
C      FMCG 970
C      FMCG 980
C      FMCG 990
C      FMCG1000
C      FMCG1010
C      FMCG1020
C      FMCG1030
C      FMCG1040
C      FMCG1050
C      FMCG1060
C      FMCG1070
C      FMCG1080
C      FMCG1090
C      FMCG1100
C      FMCG1110
C      FMCG1120
C      FMCG1130
C      FMCG1140
C      FMCG1150
C      FMCG1160
C      FMCG1170
C      FMCG1180
C      FMCG1190
C      FMCG1200
C      FMCG1210
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C      FMCG1500
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C      FMCG1600
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C      FMCG2190
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C      FMCG2220
C      FMCG2230
C      FMCG2240
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C      FMCG2270
C      FMCG2280
C      FMCG2290
C      FMCG2300
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C      FMCG2350
C      FMCG2360
C      FMCG2370
C      FMCG2380
C      FMCG2390
C      FMCG2400
C      FMCG2410
C      FMCG2420
C      FMCG2430
C      FMCG2440

SUBROUTINE FMCG(FUNCT,N,X,F,C,EST,EPS,LIMIT,IER,H)
  DIMENSIONED DUMMY VARIABLES
  DIMENSION X(1),G(1),G1(1)
  ! COMPLETE FUNCTION VALUE AND GRADIENT VECTOR FOR INITIAL ARGUMENT
  CALL FUNCT(N,X,F,G)
  HSET ITERATION COUNTER
  IER=C
  N1=N+1
  ! START ITERATION CYCLE FOR EVERY N(1) ITERATIONS
  DO 43 I=1,N1
  ! STEP ITERATION COUNTER AND SAVE FUNCTION VALUE
  KCLAT=KCLAT+1
  CLCF=F
  ! COMPLETE SQUARE OF GRADIENT AND TERMINATE IF ZERO
  GNP=C
  DO 2 J=1,N
  CRR=CRR+C(J)*C(J)
  IF(GRR)46,46,3
  ! EACH TIME THE ITERATION LOOP IS ENDED, THE FIRST STEP WILL
  ! BE IN DIRECTION OF STEEPEST DESCENT
  DO 3 I=1,N1,4,4
  DO 5 J=1,N
  F(J)=G(J)
  DO TC E
  ! FURTHER DIRECTION VECTORS F WILL BE CHOSEN CORRESPONDING
  ! TO THE CONJUGATE GRADIENT METHOD
  ! APPECA=CONJUGATE
  DO 7 J=1,N
  F(J)=APPECA*(F(J)-G(J))
  ! COMPLETE TESTVALUE FOR DIRECTIONAL VECTOR AND DIRECTIONAL
  ! DERIVATIVE
  FV=F
  FRR=C
  DO 5 J=1,N
  R=J*N
  ! SAVE ARGUMENT VECTOR
  F(K)=X(J)
  FRR=F+H*RES(F(J))
  CY=CY+F(J)*C(J)
  ! CHECK WHETHER FUNCTION WILL DECREASE STEPPING ALONG H AND
  ! SKIP LINEAR SEARCH ROUTINE IF NOT
  IF(CY)10,42,42
  ! COMPLETE SCALE FACTOR USED IN LINEAR SEARCH SUBROUTINE
  LC=SRP=1./FRR
  ! SEARCH MINIMUM ALONG DIRECTION H
  FMCG1290
  ! SEARCH ALONG H FOR POSITIVE DIRECTIONAL DERIVATIVE
  FMCG1300
  FMCG1310
  FV=F
  ALFA=2.*(EST-F)/CY
  APPECA=SRP
  FMCG1320
  FMCG1330
  FMCG1340
  ! USE ESTIMATE FOR STEPSIZE ONLY IF IT IS POSITIVE AND LESS THAN
  ! SNRP, OTHERWISE TAKE SNRP AS STEPSIZE.
  FMCG1350
  FMCG1360
  IF(ALFA)13,13,11
  FMCG1370
  !1 IF(ALFA-APPECA)12,13,12
  FMCG1380
  !12 APPECA=ALFA
  FMCG1390
  !13 ALFA=C
  FMCG1400
  ! SAVE FUNCTION AND DERIVATIVE VALUES FOR OLD ARGUMENT
  FMCG1410
  FMCG1420
  FMCG1430
  FMCG1440
  FMCG1450
  FMCG1460
  ! STEP ARGUMENT ALONG H
  FMCG1470
  DO 15 I=1,N
  FMCG1480
  X(I)=X(I)+APPECA*F(I)
  FMCG1490
  ! COMPLETE FUNCTION VALUE AND GRADIENT FOR NEW ARGUMENT
  FMCG1500
  CALL FUNCT(N,X,F,G)
  FMCG1510
  FV=F
  FMCG1520
  ! COMPLETE DIRECTIONAL DERIVATIVE DV FOR NEW ARGUMENT, TERMINATE
  ! SEARCH, IF DV POSITIVE, IF DV IS ZERO THE MINIMUM IS FOUND
  FMCG1530
  FMCG1540
  FMCG1550
  FMCG1560
  ! ETC...
  FMCG1570
  DO 14 CY=CY+(I)*F(I)
  FMCG1580
  IF(CY)17,20,20
  FMCG1590
  ! TERMINATE SEARCH ALSO IF THE FUNCTION VALUE INDICATES THAT
  ! A MINIMUM HAS BEEN PASSED
  FMCG1600
  FMCG1610
  !17 IF(FY-F)16,20,20
  FMCG1620
  ! REPEAT SEARCH AND DOUBLE STEPSIZE FOR FURTHER SEARCHES
  FMCG1630
  !18 APPECA=APPECA*ALFA
  FMCG1640
  ALFA=APPECA
  FMCG1650
  ! TERMINATE IF THE CHANGE IN ARGUMENT GETS VERY LARGE
  FMCG1660
  !19 IF(ABS(APPECA-1.ETC)14,14,15
  FMCG1670
  ! LINEAR SEARCH TECHNIQUE INDICATES THAT NO MINIMUM EXISTS
  FMCG1680
  !15 IER=2
  FMCG1690
  FMCG1700
  ! RESTORE OLD VALUES OF FUNCTION AND ARGUMENTS
  FMCG1710
  FMCG1720
  F=CLCF
  FMCG1730
  DO 1CC J=1,N
  FMCG1740
  G(J)=G(J)
  FMCG1750
  R=N+J
  FMCG1760
  !1CC X(J)=H*(K)
  FMCG1770
  X(J)=R
  FMCG1780
  ! END OF SEARCH LOOP
  FMCG1790
  ! INTERPOLATE LINEARLY IN THE INTERVAL DEFINED BY THE SEARCH
  FMCG1800
  ! AND COMPUTE THE ARGUMENT X FOR WHICH THE INTERPOLATION
  ! POLYNOMIAL IS MINIMIZED
  FMCG1810
  FMCG1820
  !20 T=C
  FMCG1830
  !21 IF(APPECA)22,30,22
  FMCG1840
  !22 T=2.*(F-F)/APPECA+CY+CY
  FMCG1850
  ! ALFA=APPECA*(RES(2)+RES(1)+RES(1))
  FMCG1860
  CALFA=T/ALFA
  FMCG1870
  ! ALFA=CALFA+ALFA-CY/ALFA*CY/ALFA
  FMCG1880
  !10 CALFA=12,27,27
  FMCG1890
  ! RESTORE OLD VALUES OF FUNCTION AND ARGUMENTS
  FMCG1900
  DO 23 J=1,N
  FMCG1910
  X(N+J)=X(N+J)
  FMCG1920
  !23 X(J)=H*(K)
  FMCG1930
  CALL FUNCT(N,X,F,G)
  FMCG1940
  ! TEST FOR REPEATED FAILURE OF ITERATION
  FMCG1950
  !25 IF(IER)19,20,47
  FMCG1960
  !26 IER=1
  FMCG1970
  !27 H=ALFA*SGHT(CALFA)
  FMCG1980
  ! ALFA=CY-CX+H
  FMCG1990
  ! IF(ALFA)27C,27L,27C
  FMCG2000
  !27C ALFA=CY-CX+H/ALFA
  FMCG2010
  ! DO TC 27
  FMCG2011
  !27L ALFA=(ALFA-H)/(2+CX+CY)
  FMCG2012
  !27 ALFA=ALFA*APPECA
  FMCG2013
  DO 28 I=1,N
  FMCG2014
  X(I)=X(I)+H*(1+I*(ALFA)+I)
  FMCG2015
  FMCG2020
  FMCG2030
  FMCG2040
  ! TERMINATE, IF THE VALUE OF THE ACTUAL FUNCTION AT X IS LESS
  FMCG2050
  ! THAN THE FUNCTION VALUES AT THE INTERVAL ENDS, OTHERWISE REDUCE
  FMCG2060
  ! THE INTERVAL BY CHOOSING ONE END-POINT EQUAL TO X AND REPEAT
  FMCG2070
  ! THE INTERPOLATION, WHICH END-POINT IS CHOSEN DEPENDS ON THE
  FMCG2080
  ! VALUE OF THE FUNCTION AND ITS GRADIENT AT X
  FMCG2090
  CALL FUNCT(N,X,F,G)
  FMCG2100
  !19 F=F+J*25,25,30
  FMCG2110
  !25 IF(F-F)26,36,30
  FMCG2120
  FMCG2130
  FMCG2140
  ! COMPLETE DIRECTIONAL DERIVATIVE
  FMCG2150
  DO 3C CALFA=C
  FMCG2160
  DO 31 I=1,N
  FMCG2170
  !31 CALFA=CALFA+C(I)*F(I)
  FMCG2180
  ! IF(CALFA)32,35,35
  FMCG2190
  !32 IF(F-F)33,35,35
  FMCG2200
  !33 IF(CY-CALFA)34,36,34
  FMCG2210
  !34 F=F
  FMCG2220
  CX=CALFA
  FMCG2230
  TX=ALFA
  FMCG2240
  !35 CALFA=ALFA
  FMCG2250
  DO TC 21
  FMCG2260
  !35 IF(F-F)37,36,37
  FMCG2270
  !36 IF(CY-CALFA)37,36,37
  FMCG2280
  !37 F=F
  FMCG2290
  CY=CALFA
  FMCG2300
  !37 APPECA=APPECA-ALFA
  FMCG2310
  DO TC 2C
  FMCG2320
  ! TERMINATE, IF FUNCTION HAS ACT DECREASED DURING LAST ITERATION
  FMCG2330
  ! OTHERWISE SAVE GRADIENT VECTOR
  FMCG2340
  !38 IF(CY)25,25,35
  FMCG2350
  !35 CLCF=CRR
  FMCG2360
  ! COMPLETE DIFFERENCE OF NEW AND OLD ARGUMENT VECTOR
  FMCG2370
  FMCG2380
  T=C
  FMCG2390
  DO 4C J=1,N
  FMCG2400
  R=J*N
  FMCG2410
  !4C F(R)=F(H*(K))
  FMCG2420
  !4C T=T+RES(H*(K))
  FMCG2430
  FMCG2440

```

```

C
C TEST LENGTH OF DIFFERENCE VECTOR IF AT LEAST N+1 ITERATIONS
C HAVE BEEN EXECUTED. TERMINATE, IF LENGTH IS LESS THAN EPS
C IF (CLNT-N)142,41,41
41 IF (1-EPS)145,45,42
C
C TERMINATE, IF NUMBER OF ITERATIONS WOULD EXCEED LIMIT
42 IF (COUNT-LIMIT)143,44,44
43 IER=0
C END OF ITERATION CYCLE
C
C START NEXT ITERATION CYCLE
CC TC 1
C
C AC COVERAGE AFTER LIMIT ITERATIONS
44 IER=1
IF (GAMP-EPS)146,46,47
C
C TEST FOR SUFFICIENTLY SMALL GRADIENT
45 IF (GAMP-EPS)146,46,25
46 IER=0
47 RETURN
END

```

FMCG2450
FMCG2460
FMCG2470
FMCG2480
FMCG2490
FMCG2500
FMCG2510
FMCG2520
FMCG2530
FMCG2540
FMCG2550
FMCG2560
FMCG2570
FMCG2580
FMCG2590
FMCG2600
FMCG2610
FMCG2620
FMCG2630
FMCG2640
FMCG2650
FMCG2660
FMCG2670

```

C
C COMPUTE SCALE OF GRADIENT AND TERMINATE IF ZERO
C GRP=C*CC
CC 2 J=1,N
2 C=0
C=GRP*(1+G(J))
IF (C)146,46,3
C
C EACH TIME THE ITERATION LOOP IS EXECUTED, THE FIRST STEP WILL
C BE IN DIRECTION OF STEEPEST DESCENT
3 IF (1-J)14,4,4
4 CC 5 J=1,N
5 F(J)=G(J)
CC TC 1
C
C FURTHER DIRECTION VECTORS F WILL BE CHOSEN CORRESPONDING
C TO THE CONJUGATE GRADIENT METHOD
6 A=PEA=C*GRP/CLC
CC 7 J=1,N
7 F(J)=A*PEA*(1-J)-G(J)
C
C COMPUTE TEST VALUE FOR DIRECTIONAL VECTOR AND DIRECTIONAL
C DERIVATIVE
8 CV=C*CC
GRP=C*CC
CC 5 J=1,N
R=J*N
C
C SAVE ARGUMENT VECTOR
F(K)=X(J)
GRP=GRP+R*CAESIN(I*J)
5 CV=CV+R*(J)*G(J)
C
C CHECK WHETHER FUNCTION WILL DECREASE STEPPING ALONG H AND
C STOP IF LINEAR SEARCH ROUTINE IS NOT
IF (CV)112,12,12
C
C COMPUTE SCALE FACTOR USED IN LINEAR SEARCH SUBROUTINE
10 SAMP=1./CC/GRP
C
C SEARCH MINIMUM ALONG DIRECTION F
C
C SEARCH ALONG F FOR POSITIVE DIRECTIONAL DERIVATIVE
F=F+R
ALFA=2./CC*(1-EF)/CV
A=PEA=SAMP
C
C USE ESTIMATE FOR STEPSIZE ONLY IF IT IS POSITIVE AND LESS THAN
C SAMP. OTHERWISE TAKE SAMP AS STEPSIZE.
IF (ALFA)112,12,11
11 IF (ALFA-A*PEA)112,12,12
12 A=PEA*ALFA
13 ALFA=C*CC
C
C SAVE FUNCTION AND DERIVATIVE VALUES FOR OLD ARGUMENT
14 F=X*Y
EX=Y
C
C STEP ARGUMENT ALONG F
CC 15 I=1,N
C
15 X(I)=X(I)+A*PEA*(1-I)
C
C COMPUTE FUNCTION VALUE AND GRADIENT FOR NEW ARGUMENT
CALL FUNCT(X,F,G)
F=Y+R
C
C COMPUTE DIRECTIONAL DERIVATIVE CV FOR NEW ARGUMENT. TERMINATE
C SEARCH, IF CV POSITIVE. IF CV IS ZERO THE MINIMUM IS FOUND
CV=C*CC
CC 16 I=1,N
16 CV=CV+G(I)*X(I)
IF (CV)112,12,12
C
C TERMINATE SEARCH ALSO IF THE FUNCTION VALUE INDICATES THAT
C A MINIMUM HAS BEEN PASSED
17 IF (F-F)112,12,12
C
C REPEAT SEARCH AND DOUBLE STEPSIZE FOR FURTHER SEARCHES
18 A=PEA*A*PEA
ALFA=A*PEA
C
C TERMINATE IF THE CHANGE IN ARGUMENT GETS VERY LARGE
IF (A*GRP)112,12,12
C
C LINEAR SEARCH TECHNIQUE INDICATES THAT NO MINIMUM EXISTS
15 IER=2
C
C RESTORE OLD VALUES OF FUNCTION AND ARGUMENTS
F=CLC
CC 19 J=1,N
C(J)=X(J)
K=N+J
100 X(J)=F(K)
RETURN
C
C END OF SEARCH LOOP
C
C INTERPOLATE QUADRATICALLY IN THE INTERVAL DEFINED BY THE SEARCH
C AND COMPUTE THE ANGLE AT WHICH THE INTERPOLATION
C POLYNOMIAL IS MINIMIZED
20 Y=C
21 IF (A*PEA)122,12,12
22 Z=3.-CC*(1-F)/A*PEA*(1-F)
ALFA=C*CAESIN(1)+CAESIN(1)+CAESIN(1)
CALFA=Z/ALFA
CALFA=CALFA*(ALFA-CX)/ALFA+CV/ALFA
IF (CALFA)122,12,12
C
C RESTORE OLD VALUES OF FUNCTION AND ARGUMENTS
23 CC 24 J=1,N
R=N+J
24 X(J)=F(K)
CALL FUNCT(X,F,G)
C
C TEST FOR REPEATED FAILURE OF ITERATION
25 IF (IER)126,12,12
26 IER=1
CC TC 1
27 N=ALFA*CAESIN(CALFA)
ALFA=CX-CX*CAESIN(1)
IF (ALFA)126,12,12
27C ALFA=CX-2*N*ALFA
CC TC 272
271 ALFA=CX-CX*(1+Z*CAESIN(1)+Z*CV)
272 ALFA=ALFA*A*PEA
CC 28 I=1,N
28 X(I)=X(I)+X(I)-ALFA*(1-I)

```

DFMC 10
DFMC 20
DFMC 30
DFMC 40
DFMC 50
DFMC 60
DFMC 70
DFMC 80
DFMC 90
DFMC 100
DFMC 110
DFMC 120
DFMC 130
DFMC 140
DFMC 150
DFMC 160
DFMC 170
DFMC 180
DFMC 190
DFMC 200
DFMC 210
DFMC 220
DFMC 230
DFMC 240
DFMC 250
DFMC 260
DFMC 270
DFMC 280
DFMC 290
DFMC 300
DFMC 310
DFMC 320
DFMC 330
DFMC 340
DFMC 350
DFMC 360
DFMC 370
DFMC 380
DFMC 390
DFMC 400
DFMC 410
DFMC 420
DFMC 430
DFMC 440
DFMC 450
DFMC 460
DFMC 470
DFMC 480
DFMC 490
DFMC 500
DFMC 510
DFMC 520
DFMC 530
DFMC 540
DFMC 550
DFMC 560
DFMC 570
DFMC 580
DFMC 590
DFMC 600
DFMC 610
DFMC 620
DFMC 630
DFMC 640
DFMC 650
DFMC 660
DFMC 670
DFMC 680
DFMC 690
DFMC 700
DFMC 710
DFMC 720
DFMC 730
DFMC 740
DFMC 750
DFMC 760
DFMC 770
DFMC 780
DFMC 790
DFMC 800
DFMC 810
DFMC 820
DFMC 830
DFMC 840
DFMC 850
DFMC 860
DFMC 870
DFMC 880
DFMC 890
DFMC 900
DFMC 910
DFMC 920
DFMC 930
DFMC 940
DFMC 950
DFMC 960
DFMC 970

SUBROUTINE EFFCG
PURPOSE
TO FIND A LOCAL MINIMUM OF A FUNCTION OF SEVERAL VARIABLES
BY THE METHOD OF CONJUGATE GRADIENTS
USAGE
CALL EFFCG(FUNCT,N,X,F,C,EST,EPS,LIMIT,IER,H)
DESCRIPTION OF PARAMETERS
FUNCT - USER-WRITTEN SUBROUTINE CONCERNING THE FUNCTION TO
BE MINIMIZED. IT MUST BE OF THE FORM
SUBROUTINE FUNCT(N,ARG,VAL,GRAD)
AND MUST SERVE THE FOLLOWING PURPOSE
FOR EACH N-DIMENSIONAL ARGUMENT VECTOR ARG,
FUNCTION VALUE AND GRADIENT VECTOR MUST BE COMPUTED
AND, ON RETURN, STORED IN VAL AND GRAD RESPECTIVELY.
ARG, VAL AND GRAD MUST BE OF DOUBLE PRECISION.
N - NUMBER OF VARIABLES
X - VECTOR OF DIMENSION N CONTAINING THE INITIAL
ARGUMENT WHERE THE ITERATION STARTS. ON RETURN,
X POINTS THE ARGUMENT CORRESPONDING TO THE
COMPUTED MINIMUM FUNCTION VALUE
DOUBLE PRECISION VECTOR.
F - SINGLE VARIABLE CONTAINING THE MINIMUM FUNCTION
VALUE ON RETURN, I.E. F=F(X).
DOUBLE PRECISION VARIABLE.
C - VECTOR OF DIMENSION N CONTAINING THE GRADIENT
VECTOR CORRESPONDING TO THE MINIMUM ON RETURN,
I.E. C=G(F(X)).
DOUBLE PRECISION VECTOR.
EST - IS AN ESTIMATE OF THE MINIMUM FUNCTION VALUE.
SINGLE PRECISION VARIABLE.
EPS - TEST VALUE REPRESENTING THE EXPECTED ABSOLUTE ERROR.
A REASONABLE CHOICE IS 10**(-16), I.E.
SOMEWHAT GREATER THAN 10**(-17), WHERE D IS THE
NUMBER OF SIGNIFICANT DIGITS IN FLOATING POINT
REPRESENTATION.
LIMIT - MAXIMUM NUMBER OF ITERATIONS.
IER - ERROR PARAMETER
IER = 0 MEANS CONVERGENCE WAS OBTAINED
IER = 1 MEANS NO CONVERGENCE IN LIMIT ITERATIONS
IER = -1 MEANS ERRORS IN GRADIENT CALCULATION
IER = 2 MEANS LINEAR SEARCH TECHNIQUE INDICATES
IT IS LIKELY THAT THERE EXISTS NO MINIMUM.
H - WORKING STORAGE OF DIMENSION 2*N.
DOUBLE PRECISION ARRAY.
REMARKS
I) THE SUBROUTINE NAME REPLACING THE DUMMY ARGUMENT FUNCT
MUST BE DECLARED AS EXTERNAL IN THE CALLING PROGRAM.
II) IER IS SET TO 2 IF, STEPPING IN ONE OF THE COORDINATE
DIRECTIONS, THE FUNCTION WILL NEVER INCREASE WITHIN
A TOLERABLE RANGE OF ARGUMENT.
III) IER = 2 MAY OCCUR ALSO IF THE INTERVAL WHERE F
INCREASES IS SMALL AND THE INITIAL ARGUMENT WAS
RELATIVELY FAR AWAY FROM THE MINIMUM SUCH THAT THE
MINIMUM WAS OVERLEAPED. THIS IS DUE TO THE SEARCH
TECHNIQUE WHICH DROPPES THE STEPSIZE UNTIL A POINT
IS FOUND WHERE THE FUNCTION INCREASES.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
FUNCT
METHOD
THE METHOD IS DESCRIBED IN THE FOLLOWING ARTICLE
M. FLETCHER AND C. M. REEVES, FUNCTION MINIMIZATION BY
CONJUGATE GRADIENTS,
COMPUTER JOURNAL VOL. 7, ISS. 2, 1964, PP. 149-154.
SUBROUTINE EFFCG(FUNCT,N,X,F,C,EST,EPS,LIMIT,IER,H)
DIMENSION X(1),G(1),F(1)
DOUBLE PRECISION X,G,GRP,F,GRP,F,FX,FY,CLOF,CLDG,SAMP,AMBCA,
ALFA,CALFA,T,Z,N,EX,CY
C
C COMPUTE FUNCTION VALUE AND GRADIENT VECTOR FOR INITIAL ARGUMENT
CALL FUNCT(X,F,G)
C
C RESET ITERATION COUNTER
COUNT=C
IER=0
R=N+1
C
C START ITERATION CYCLE FOR EVERY N+1 ITERATIONS
1 CC 42 I=1,N
C
C STEP ITERATION COUNTER AND SAVE FUNCTION VALUE
COUNT=COUNT+1
CLCF=F


```

C      TERMINATE, IF THE VALUE OF THE ACTUAL FUNCTION AT X IS LESS DFMC2130
C      THAN THE FUNCTION VALUES AT THE INTERVAL ENDS, OTHERWISE REDUCE DFMC2140
C      THE INTERVAL BY CHOOSING ONE END-POINT EQUAL TO X AND REPEAT DFMC2150
C      THE INTERCALCULATION, WHICH END-POINT IS CHOSEN DEPENDS ON THE DFMC2160
C      VALUE OF THE FUNCTION AND ITS GRADIENT AT X DFMC2170
C      CALL FUNCT(A,X,F,G) DFMC2180
C      IF(F-F*125,25,30) DFMC2190
C      29 IF(F-F*130,30,30) DFMC2200
C      COMPLETE DIRECTIONAL DERIVATIVE DFMC2210
C      30 CALFAC=CC DFMC2220
C      CC 31 J=1,N DFMC2230
C      31 CALFA=CALFAC*(1/N) DFMC2240
C      IF(CALFA)32,35,35 DFMC2250
C      32 IF(F-F*130,30,30) DFMC2260
C      33 IF(CA-CALFA)34,30,34 DFMC2270
C      34 F=F DFMC2280
C      CA=CALFA DFMC2290
C      T=ALFA DFMC2300
C      #PCA=ALFA DFMC2310
C      CC TC 21 DFMC2320
C      35 IF(FY-F*130,30,30) DFMC2330
C      36 IF(CY-CALFA)37,30,37 DFMC2340
C      37 FY=F DFMC2350
C      CY=CALFA DFMC2360
C      #PCA=#PCA-ALFA DFMC2370
C      CC TC 20 DFMC2380
C      DFMC2390
C      DFMC2400
C      DFMC2410
C      TERMINATE, IF FUNCTION HAS NOT DECREASED DURING LAST ITERATION DFMC2420
C      OTHERWISE SAVE GRADIENT AND DFMC2430
C      38 IF(CALF-F*EPS)15,25,35 DFMC2440
C      39 CLDG=GARD DFMC2450
C      COMPLETE DIFFERENCE OF NEW AND OLD ARGUMENT VECTOR DFMC2460
C      T=C,CC DFMC2470
C      DFMC2480
C      CC 40 J=1,N DFMC2490
C      F=J,N DFMC2500
C      F(I)=X(I)-T(I) DFMC2510
C      40 T=T+C*ABS(F(I)) DFMC2520
C      TEST LENGTH OF DIFFERENCE VECTOR IF AT LEAST N+1 ITERATIONS DFMC2530
C      HAVE BEEN EXECUTED. TERMINATE, IF LENGTH IS LESS THAN EPS DFMC2540
C      41 IF(KLNT-N)42,41,41 DFMC2550
C      41 IF(T-EPS)43,45,42 DFMC2560
C      TERMINATE, IF NUMBER OF ITERATIONS WOULD EXCEED LIMIT DFMC2570
C      42 IF(KLNT-LIMIT)43,49,44 DFMC2580
C      43 IER=C DFMC2590
C      END OF ITERATION CYCLE DFMC2600
C      START NEXT ITERATION CYCLE DFMC2610
C      GC TC 1 DFMC2620
C      DFMC2630
C      DFMC2640
C      AC CONVERGENCE AFTER LIMIT ITERATIONS DFMC2650
C      44 IER=1 DFMC2660
C      IF(GARD-EPS)46,46,47 DFMC2670
C      DFMC2680
C      DFMC2690
C      TEST FOR SUFFICIENTLY SMALL GRADIENT DFMC2700
C      45 IF(GARD-EPS)46,46,25 DFMC2710
C      46 IER=C DFMC2720
C      47 RETURN DFMC2730
C      END DFMC2740
C      DFMC2750

```

PERMUTATIONS

Let n be a positive integer and let $N = \{1, \dots, n\}$. A permutation on N is a one-one function from N onto N . In what follows, all permutations will be on N .

Suppose P and Q are permutations. We define a new permutation $R = Q \cdot P$ by $R(j) = (Q \cdot P)(j) = Q(P(j))$ for $j \in N$. Note that in general $P \cdot Q \neq Q \cdot P$, although \cdot is associative. The operation \cdot is ordinary function composition. The identity permutation is the identity function I on N , defined by $I(j) = j$ for $j \in N$. An inverse of a permutation P is a permutation P^{-1} with the property that $P \cdot P^{-1} = P^{-1} \cdot P = I$. It is easily proved that every permutation has a unique inverse; indeed, if P is a permutation, its inverse P^{-1} is given by $P^{-1}(j) = s$ where s is such that $P(s) = j$, $j \in N$. Note also that if P and Q are permutations, $(Q \cdot P)^{-1} = P^{-1} \cdot Q^{-1}$. The conjugate of Q by P is the permutation $P \cdot Q \cdot P^{-1}$.

A transposition is a permutation that moves at most two elements of N ; that is, T is a transposition if and only if integers i and j exist such that $T(k) = k$ for $k \neq i, j$. It may easily be proved that every permutation can be written as a product $T_1 \cdot T_2 \cdot \dots \cdot T_n$ of transpositions where for $i = 1, \dots, n$ there exists $k_i \in N$ such that:

$$T_i(j) = \begin{cases} k_i & \text{if } j = i \\ i & \text{if } j = k_i \\ j & \text{if } j \neq i, k_i \end{cases}$$

Every transposition is its own inverse.

If P is a permutation, we will identify P and the symbol

$$\begin{pmatrix} 1 & 2 & \dots & n \\ p_1 & p_2 & \dots & p_n \end{pmatrix}$$

where

$$p_i = P(i) \text{ for } i = 1, \dots, n.$$

At times we will also identify the permutation P and the vector (p_1, \dots, p_n) . Whenever this is the case we will write "... permutation $P = (p_1, \dots, p_n)$...", or "permutation vector $P = (p_1, \dots, p_n)$ ".

Similarly, if T is the transposition given by:

$$T(j) = \begin{cases} j & \text{if } j \neq i, k \\ i & \text{if } j = k \\ k & \text{if } j = i \end{cases}$$

then we identify T and the symbol (i, k) . (This leads to no difficulty if $n = 2$, since in this case all permutations are also transpositions.)

We note above that any permutation P can be written as a product $T_1 \cdot \dots \cdot T_n$ of transpositions of a certain form. In the new notation we have $P = (1, t_1) \cdot \dots \cdot (n, t_n)$, $t_i \in N$, $i = 1, \dots, n$. The t_i are generally not distinct. At times we will identify the product $(1, t_1) \cdot \dots \cdot (n, t_n)$ and the vector (t_1, \dots, t_n) . Whenever this identification is meant we will write "...transposition vector $P = (t_1, \dots, t_n)$ ".

Permutations can be used to induce rearrangements of ordered collections of objects. The convention that we will use is illustrated by the following example. Suppose that A is an m by n matrix and C_i is the i^{th} column of A for $i = 1, \dots, n$. If the permutation $P = (p_1, \dots, p_n)$ is applied to the columns of A , there results the m by n matrix A' whose p_i^{th} column, C_{p_i} , is C_i for $i = 1, \dots, n$.

Examples

Suppose $n = 5$, and let P and Q be the permutations given by:

$$\begin{aligned} P(1) = 3 \quad P(2) = 1 \quad P(3) = 5 \quad P(4) = 2 \quad P(5) = 4 \\ \text{and} \\ Q(1) = 1 \quad Q(2) = 3 \quad Q(3) = 5 \quad Q(4) = 2 \quad Q(5) = 4 \end{aligned}$$

Then P and Q may also be written as:

$$P = \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 3 & 1 & 5 & 2 & 4 \end{pmatrix} \quad \text{and} \quad Q = \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 1 & 3 & 5 & 2 & 4 \end{pmatrix}$$

or as the permutation vectors:

$$P = (3, 1, 5, 2, 4) \quad \text{and} \quad Q = (1, 3, 5, 2, 4)$$

Now:

$$Q \cdot P = \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 1 & 3 & 5 & 2 & 4 \end{pmatrix} \cdot \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 3 & 1 & 5 & 2 & 4 \end{pmatrix} = \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 5 & 1 & 4 & 3 & 2 \end{pmatrix}$$

while:

$$P \cdot Q = \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 3 & 1 & 5 & 2 & 4 \end{pmatrix} \cdot \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 1 & 3 & 5 & 2 & 4 \end{pmatrix} = \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 3 & 5 & 4 & 1 & 2 \end{pmatrix}$$

P^{-1} is the permutation given by

$$P^{-1}(1) = 2 \quad P^{-1}(2) = 4 \quad P^{-1}(3) = 1 \quad P^{-1}(4) = 5$$

$$P^{-1}(5) = 3$$

or

$$P^{-1} = \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 2 & 4 & 1 & 5 & 3 \end{pmatrix}$$

or the permutation vector $P = (2, 4, 1, 5, 3)$.

We now write P as a product of transpositions in the standard form defined above. We have:

$$\begin{aligned} P &= \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 3 & 1 & 5 & 2 & 4 \end{pmatrix} = (1, 3) \cdot \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 1 & 3 & 5 & 2 & 4 \end{pmatrix} \\ &= (1, 3) \cdot \left[(2, 3) \cdot \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 1 & 2 & 5 & 3 & 4 \end{pmatrix} \right] \\ &= (1, 3) \cdot (2, 3) \cdot \\ &\quad \left[(3, 5) \cdot \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 1 & 2 & 3 & 5 & 4 \end{pmatrix} \right] \\ &= (1, 3) \cdot (2, 3) \cdot (3, 5) \cdot \\ &\quad \left[(4, 5) \cdot \begin{pmatrix} 1 & 2 & 3 & 4 & 5 \\ 1 & 2 & 3 & 4 & 5 \end{pmatrix} \right] \\ &= (1, 3) \cdot (2, 3) \cdot (3, 5) \cdot (4, 5) \cdot (5, 5). \end{aligned}$$

Hence P is equivalent to the transposition vector $(3, 3, 5, 5, 5)$.

Subroutine PPRCN

Subroutine PPRCN computes the permutation vector that is the composition of two given permutation vectors, and the permutation vector that is the conjugate of a given permutation vector by another permutation vector. (See the general discussion for definitions and notation.)

1. Mathematical background

Suppose that $IP1 = (p_1, \dots, p_n)$ and $IP2 = (q_1, \dots, q_n)$ are permutation vectors on $N = \{1, \dots, n\}$.

a. The composition $IP3 = IP2 \cdot IP1$ of $IP1$ and $IP2$ is given by $IP3 = (r_1, \dots, r_n)$ where $r_i = q_{p_i}$ for $i = 1, \dots, n$.

b. The conjugate $IP3 = IP1 \cdot IP2 \cdot IP1^{-1}$ of $IP2$ by $IP1$ is given by $IP3 = (r_1, \dots, r_n)$ where $r_{p_i} = q_i$ for $i = 1, \dots, n$.

2. Programming considerations

Depending on whether the input parameter $IPAR$ is nonnegative or negative, subroutine PPRCN computes either the composition of $IP1$ and $IP2$ or the conjugate of $IP2$ by $IP1$.

Subroutine PERM is used to check that n is positive and that $IP1$ and $IP2$ are permutation vectors on N . If n is not positive or if $IP1$ and $IP2$ are not both permutation vectors on N , computation is terminated as soon as the error is detected, and the error parameter IER is set to -1 or 1 , respectively. If there is no error, IER is set to zero.

The computation of the resulting vector $IP3$ proceeds as follows.

a. If $IPAR$ is nonnegative, for each i , $i = 1, \dots, n$, $IP3(i)$ is set to $IP2(IP1(i))$.

b. If $IPAR$ is negative, initially subroutine PERM is used to compute $IP1^{-1}$, which is stored in $IP3$. Then, for $i = 1, \dots, n$, $IP3(i)$ is set to $IP1(IP2(IP3(i)))$.

$IP3$ cannot have the same storage allocation as $IP1$ or $IP2$. $IP1$ and $IP2$ are returned unchanged.

```

C ..... PPRC 10
C ..... PPRC 20
C ..... PPRC 30
C SUBROUTINE PPRCN PPRC 40
C ..... PPRC 50
C PURPOSE PPRC 60
C TO COMPUTE, GIVEN TWO PERMUTATION VECTORS IP1 AND IP2, THE PPRC 70
C COMPOSITION IP2(IP1) AND THE CONJUGATE IP1(IP2(IP1 INVERSE)) PPRC 80
C OF IP2 BY IP1. (SEE THE GENERAL DISCUSSION FOR DEFINITIONS PPRC 90
C AND NOTATION.) PPRC 100
C ..... PPRC 110
C USAGE PPRC 120
C CALL PPRCN(IP1,IP2,IP3,N,IPAR,IER) PPRC 130
C ..... PPRC 140
C DESCRIPTION OF PARAMETERS PPRC 150
C IP1 - GIVEN PERMUTATION VECTOR (DIMENSION N) PPRC 160
C IP2 - GIVEN PERMUTATION VECTOR (DIMENSION N) PPRC 170
C IP3 - RESULTING PERMUTATION VECTOR (DIMENSION N) PPRC 180
C N - DIMENSION OF VECTORS IP1, IP2 AND IP3 PPRC 190
C IPAR - INPUT PARAMETER PPRC 200
C IPAR NON-NEGATIVE - COMPUTE IP2(IP1) PPRC 210
C IPAR NEGATIVE - COMPUTE IP1(IP2(IP1 INVERSE)) PPRC 220
C IER - RESULTING ERROR PARAMETER PPRC 230
C IER=-1 - N IS NOT POSITIVE PPRC 240
C IER=0 - NO ERROR PPRC 250
C IER=1 - IP1 AND IP2 ARE NOT BOTH PERMUTATION PPRC 260
C VECTORS ON 1,...,N PPRC 270
C ..... PPRC 280
C REMARKS PPRC 290
C (1) IF IER=-1 THERE HAS BEEN NO COMPUTATION. PPRC 300
C (2) IF IER=1, THEN COMPUTATION HAS BEEN UNSUCCESSFUL DUE TO PPRC 310
C ERROR AND THE PARTIAL RESULTS FOUND IN IP2 ARE USELESS. PPRC 320
C (3) IP3 CANNOT HAVE THE SAME STORAGE ALLOCATION AS IP1 OR PPRC 330
C IP2. PPRC 340
C ..... PPRC 350
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED PPRC 360
C PERM PPRC 370
C ..... PPRC 380
C METHOD PPRC 390
C SUBROUTINE PERM IS USED TO CHECK THAT IP1 AND IP2 ARE PERMUTATION PPRC 400
C VECTORS. IF IP2(IP1) IS COMPUTED, IP3(I) IS SET TO PPRC 410
C IP2(IP1(I)) FOR I=1,...,N. IF IP1(IP2(IP1 INVERSE)) IS PPRC 420
C COMPUTED, FIRST IP3 IS SET TO IP1 INVERSE BY SUBROUTINE PERM PPRC 430
C AND THEN IP3(I) IS SET TO IP1(IP2(IP3(I))) FOR I=1,...,N. PPRC 440
C ..... PPRC 450
C SUBROUTINE PPRCN(IP1,IP2,IP3,N,IPAR,IER) PPRC 460
C ..... PPRC 470
C DIMENSION IP1(1),IP2(1),IP3(1) PPRC 480
C ..... PPRC 490
C CHECK THAT N IS POSITIVE AND THAT IP2 IS A PERMUTATION VECTOR PPRC 500
C CALL PERM(IP2,IP3,N,-1,IER) PPRC 510
C ..... PPRC 520
C TEST IER TO SEE IF THERE IS AN ERROR PPRC 530
C IF(IER)7,1,7 PPRC 540
C ..... PPRC 550
C CHECK THAT IP1 IS A PERMUTATION VECTOR AND COMPUTE IP1 INVERSE PPRC 560
C CALL PERM(IP1,IP3,N,-1,IER) PPRC 570
C ..... PPRC 580
C TEST IER TO SEE IF THERE IS AN ERROR PPRC 590
C IF(IER)7,2,7 PPRC 600
C ..... PPRC 610
C ..... PPRC 620
C ..... PPRC 630
C ..... PPRC 640
C TEST IPAR FOR THE DESIRED OPERATION PPRC 650
C 2 IF(IPAR)3,5,5 PPRC 660
C ..... PPRC 670
C COMPUTE IP1(IP2(IP1 INVERSE)) PPRC 680
C DO 4 I=1,N PPRC 690
C K=IP3(I) PPRC 700
C J=IP2(K) PPRC 710
C 4 IP3(I)=IP1(J) PPRC 720
C RETURN PPRC 730
C ..... PPRC 740
C COMPUTE IP2(IP1) PPRC 750
C DO 6 I=1,N PPRC 760
C K=IP1(I) PPRC 770
C 6 IP3(I)=IP2(K) PPRC 780
C RETURN PPRC 790
C END PPRC 800

```

Subroutine PERM

Subroutine PERM computes the permutation vector that is the inverse of a given permutation vector, the permutation vector that is equivalent to a given transposition vector, and a transposition vector that is equivalent to a given permutation vector. (See the general discussion for definitions and notation.)

1. Mathematical background

Let $N = \{1, \dots, n\}$.

a. If $IP1 = (p_1, \dots, p_n)$ is a permutation vector on N , its inverse, $IP2$, is given by $IP2 = (r_1, \dots, r_n)$ where $r_{p_i} = i$ for $i = 1, \dots, n$.

b. Let $IP1 = (t_1, \dots, t_n)$ be a transposition vector on N . The computation of the permutation vector that is equivalent to $IP1$ is based on the identity:

$$\begin{pmatrix} 1 & \dots & n \\ s_1 & \dots & s_n \end{pmatrix} \cdot (i, v_i) = \begin{pmatrix} 1 & \dots & i & \dots & v_i & \dots & n \\ s_1 & \dots & s_{v_i} & \dots & s_i & \dots & s_n \end{pmatrix} \quad (1)$$

Applying (1) for $i = 1, \dots, n$ to the right-hand side of the identity

$$(1, t_1) \cdot \dots \cdot (n, t_n) = \begin{pmatrix} 1 & \dots & n \\ 1 & \dots & n \end{pmatrix} \cdot (1, t_1) \cdot \dots \cdot (n, t_n)$$

there results

$$(1, t_1) \cdot \dots \cdot (n, t_n) = \begin{pmatrix} 1 & \dots & n \\ q_1 & \dots & q_n \end{pmatrix}$$

The desired permutation vector, $IP2$, is $IP2 = (q_1, \dots, q_n)$.

c. Let $IP1 = (p_1, \dots, p_n)$ be a permutation vector on N . The computation of a transposition vector that is equivalent to $IP1$ is based on the identity:

$$\begin{pmatrix} 1 & \dots & n \\ s_1 & \dots & s_n \end{pmatrix} = (i, s_i) \cdot \begin{pmatrix} 1 & \dots & i & \dots & k & \dots & n \\ s_1 & \dots & i & \dots & s_i & \dots & s_n \end{pmatrix} \quad (2)$$

for $i = 1, \dots, n$ where for each i , k is such that $p_k = i$. Using (2) with i successively $1, \dots, n$ we may write:

$$\begin{aligned} \begin{pmatrix} 1 & \dots & n \\ p_1 & \dots & p_n \end{pmatrix} &= (1, t_1) \cdot \dots \cdot (n, t_n) \cdot \begin{pmatrix} 1 & \dots & n \\ 1 & \dots & n \end{pmatrix} \\ &= (1, t_1) \cdot \dots \cdot (n, t_n) \end{aligned}$$

Sequences: Sums and Limits

Subroutines TEAS and DTEAS

The problem is to assign a scalar value S to a given sequence x_1, x_2, x_3, \dots . In case of convergence of the sequence, S should be the limit. The Epsilon algorithm possibly increases the speed of convergence and determines an approximate value FIN of S in terms of the given members of the finite sequence $x_1, x_2, x_3, \dots, x_N$.

1. Theoretical background

The value FIN is calculated by means of the Epsilon algorithm (see Figure 16).

The first column (with superscript 1) is identical to the given sequence:

$$x_i^{(1)} = x_i \quad (i = 1, 2, 3, \dots)$$

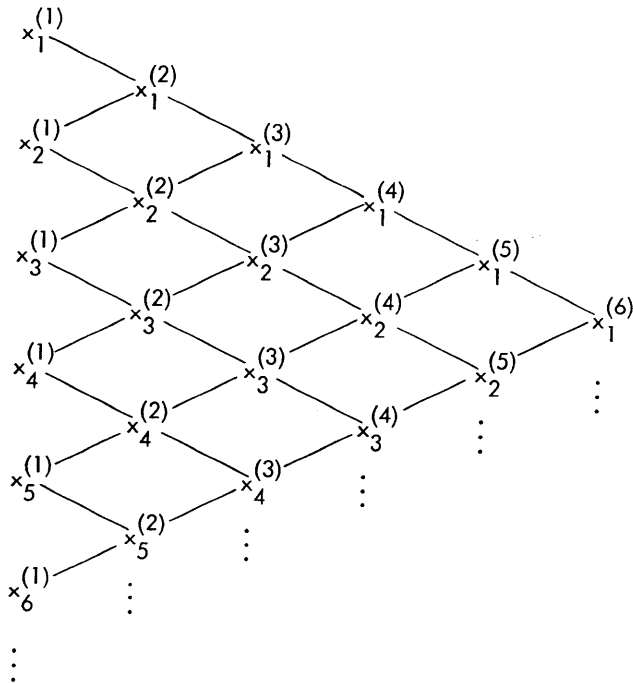


Figure 16. The complete Epsilon array

The values in the third column (with superscript 3) are derived from three consecutive members of the sequence; for example, $x_2^{(3)}$ is derived from $x_2^{(1)}$, $x_3^{(1)}$ and $x_4^{(1)}$. Generally, the column with superscript $2k + 1$ ($k = 1, 2, 3, \dots$) contains quantities derived from $2k + 1$ consecutive members of the sequence. The intermediate values with even superscripts are auxiliary quantities.

The Epsilon algorithm is based on the following relationship:

$$x_i^{(k)} = x_{i+1}^{(k-2)} + \frac{1}{x_{i+1}^{(k-1)} - x_i^{(k-1)}} \quad \begin{matrix} (k = 2, 3, 4, \dots) \\ (i = 1, 2, 3, \dots) \end{matrix} \quad (1)$$

$$x_i^{(0)} = 0$$

With this fundamental relationship the complete Epsilon array shown in Figure 16 is built up from left to right.

2. Programming considerations

Subroutines TEAS and DTEAS generate only the first five columns of the complete Epsilon array; this E-2 transformation is used in an iterative way. Within one iteration the quantities in the upward diagonals are computed in a DO-loop by means of the algorithmic relationship (1). This process requires six auxiliary storage boxes ($W1, W2, W3, W4, W5, W6$).

The values in the fifth column $x_1^{(5)}, x_2^{(5)}, \dots, x_{NEW-4}^{(5)}$ are successively stored in $x(1), x(2), \dots, x(NEW-4)$ as long as they are finite.

If a term $x_k^{(5)}$ in the fifth column becomes formally infinite, the values $x_1^{(5)}$ up to $x_k^{(5)}$ are cancelled and $x_{k+1}^{(5)}$ is stored in $x(1)$, $x_{k+2}^{(5)}$ in $x(2)$, and so on. Hence, after one iteration no component of the transformed vector x becomes infinite except possibly the last.

Consecutive equal terms in the column with superscript k ($k=1, 2, 3$) are reproduced in the column with superscript $k+2$. The basic mesh of the E-2 transformation is shown in Figure 17.

As a nonlinear algorithm the E-2 transformation is sensitive to roundoff errors; therefore special procedures are incorporated to avoid undue loss of accuracy:

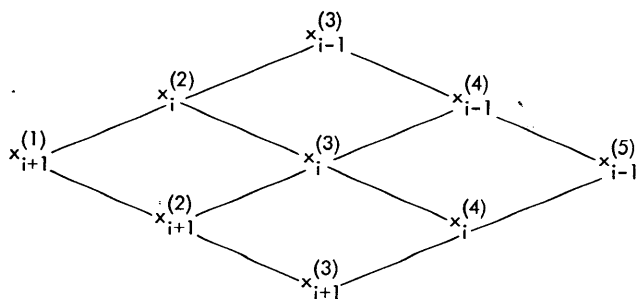


Figure 17. Basic mesh of the E-2 transformation

- a. If there is an intolerable loss of significance in the calculation of a term in the third or fifth column, TEAS or DTEAS transfers out of the diagonal loop and uses for further calculation only those components of vector x , which have already been transformed.
- b. If two consecutive quantities in the second column $x_i^{(2)}$ and $x_{i+1}^{(2)}$ (see Figure 17) are nearly equal, $x_i^{(3)}$ is large and ill-determined. Therefore, if:

$$\left. \begin{aligned} |x_{i+1}^{(2)} - x_i^{(2)}| &\leq 10^{-4} \cdot |x_{i+1}^{(2)}| \\ &\text{in single precision or} \\ |x_{i+1}^{(2)} - x_i^{(2)}| &\leq 10^{-12} \cdot |x_{i+1}^{(2)}| \\ &\text{in double precision} \end{aligned} \right\} (2)$$

subroutine TEAS or DTEAS calculates the iterated member of the sequence $x_{i-1}^{(5)}$ with a singular rule:

$$x_{i-1}^{(5)} = \frac{x_i^{(3)} \cdot W7}{1 + W7} \quad (3)$$

where
$$W7 = \frac{x_{i+1}^{(3)}}{x_i^{(3)} - x_{i+1}^{(3)}} + \frac{x_{i-1}^{(3)}}{x_i^{(3)} - x_{i-1}^{(3)}} - \frac{x_{i+1}^{(1)}}{x_i^{(3)} - x_{i+1}^{(1)}}$$

This requires two more auxiliary storage locations W7 and T.

- c. If $x_i^{(2)}$ and $x_{i+1}^{(2)}$ are exactly equal, $x_i^{(3)}$ becomes infinite, and the singular rule for the Epsilon algorithm is simply:

$$x_{i-1}^{(5)} = x_{i+1}^{(3)} + x_{i-1}^{(3)} - x_{i+1}^{(1)} \quad (4)$$

- d. If three or more consecutive terms in the second column are equal, singular rule (4) cannot be applied; the corresponding iterated members of the sequence in the fifth column become formally infinite.

Iteration is terminated if one of the following conditions holds true:

- a. Three times in succession the relative difference between neighboring transformed terms $X(i) = x_i$ is not greater than EPS; that is,

$$|x_i - x_{i+1}| \leq \text{EPS} \cdot |x_{i+1}| \quad (i = k, k+1, k+2) \quad (5)$$

In case $|x_{i+1}| \leq 1$, the relative difference (5) is replaced by the absolute

$$|x_i - x_{i+1}| \leq \text{EPS} \quad (i = k, k+1, k+2) \quad (6)$$

- b. The number of the transformed members of sequence (NEW-IMIN) is less than six.

In the first case x_{k+2} is returned as result value FIN, and IER = 0 as the error parameter. In the second case the values IER = 1 and FIN = x_1 are returned.

Some remarks are in order. First, the user must specify N--that is, the dimension of the input vector x --so that the character of the infinite sequence is recognizable. Second, subroutine TEAS or DTEAS works satisfactorily if the convergence of the given sequence is a geometric one; that is,

$$x_n - S = A \cdot \lambda^n + O(\lambda^n), \quad |\lambda| < 1 \quad (7)$$

For reference see:

- (1) Shanks, Algorithm 215, CACM 1963, no. 11, p. 662.
- (2) P. Wynn, "Singular Rules for certain nonlinear Algorithms," BIT vol. 3, 1963, pp. 175 - 195.

```

C
C ..... TEAS 13
C ..... TEAS 20
C ..... TEAS 30
C ..... TEAS 40
C ..... TEAS 50
C ..... TEAS 60
C ..... TEAS 70
C ..... TEAS 80
C ..... TEAS 90
C ..... TEAS 100
C ..... TEAS 110
C ..... TEAS 120
C ..... TEAS 130
C ..... TEAS 140
C ..... TEAS 150
C ..... TEAS 160
C ..... TEAS 170
C ..... TEAS 180
C ..... TEAS 190
C ..... TEAS 200
C ..... TEAS 210
C ..... TEAS 220
C ..... TEAS 230
C ..... TEAS 240
C ..... TEAS 250
C ..... TEAS 260
C ..... TEAS 270
C ..... TEAS 280
C ..... TEAS 290
C ..... TEAS 300
C ..... TEAS 310
C ..... TEAS 320
C ..... TEAS 330
C ..... TEAS 340
C ..... TEAS 350
C ..... TEAS 360
C ..... TEAS 370
C ..... TEAS 380
C ..... TEAS 390
C ..... TEAS 400
C ..... TEAS 410
C ..... TEAS 420
C ..... TEAS 430
C ..... TEAS 440
C ..... TEAS 450
C ..... TEAS 460
C ..... TEAS 470
C ..... TEAS 480
C ..... TEAS 490
C ..... TEAS 500
C ..... TEAS 510
C ..... TEAS 520
C ..... TEAS 530
C ..... TEAS 540
C ..... TEAS 550
C ..... TEAS 560
C ..... TEAS 570
C ..... TEAS 580
C ..... TEAS 590
C ..... TEAS 600
C ..... TEAS 610
C ..... TEAS 620
C ..... TEAS 630
C ..... TEAS 640
C ..... TEAS 650
C ..... TEAS 660
C ..... TEAS 670
C ..... TEAS 680
C ..... TEAS 690
C ..... TEAS 700
C ..... TEAS 710
C ..... TEAS 720
C ..... TEAS 730
C ..... TEAS 740
C ..... TEAS 750
C ..... TEAS 760
C ..... TEAS 770
C ..... TEAS 780
C ..... TEAS 790
C ..... TEAS 800
C ..... TEAS 810
C ..... TEAS 820
C ..... TEAS 830
C ..... TEAS 840
C ..... TEAS 850
C ..... TEAS 860
C ..... TEAS 870
C ..... TEAS 880
C ..... TEAS 890
C ..... TEAS 900
C ..... TEAS 910
C ..... TEAS 920
C ..... TEAS 930
C ..... TEAS 940
C ..... TEAS 950
C ..... TEAS 960
C ..... TEAS 970
C ..... TEAS 980
C ..... TEAS 990
C ..... TEAS1000
C ..... TEAS1010
C ..... TEAS1020
C ..... TEAS1030
C ..... TEAS1040
C ..... TEAS1050
C ..... TEAS1060
C ..... TEAS1070
C ..... TEAS1080
C ..... TEAS1090
C ..... TEAS1100
C ..... TEAS1110
C ..... TEAS1120
C ..... TEAS1130
C ..... TEAS1140
C ..... TEAS1150
C ..... TEAS1160
C ..... TEAS1170
C ..... TEAS1180
C ..... TEAS1190
C ..... TEAS1200
C ..... TEAS1210
C ..... TEAS1220
C ..... TEAS1230
C ..... TEAS1240
C ..... TEAS1250
C ..... TEAS1260
C ..... TEAS1270
C ..... TEAS1280
C ..... TEAS1290
C ..... TEAS1300

C FIRST TEST FOR LOSS OF SIGNIFICANCE
C
C IF(ABS(W5)-ABS(X(I-1)))*1.E-5123,24,24
23 IF(W5)36,24,36
C
24 W7=W5-W2
   IF(W7)27,25,27
25 W6=1.E38
26 ISW2=0
   X(IAUS)=W2
   GO TO 37
27 W6=W1+1./W7
28 IF(1/ISW1-1)33,29,29
C
C CALCULATE X(IAUS) WITH HELP OF SINGULAR RULE
C
29 IF(W2-1.E38)30,32,32
30 W7=W5/(W2-W5)+T/(W2-T)+X(I-2)/(X(I-2)-W2)
   IF(1./W7)31,38,31
31 X(IAUS)=W7*W2/(1.+W7)
   GO TO 39
C
32 X(IAUS)=W5+T-X(I-2)
   GO TO 39
C
33 W7=W6-W3
   IF(W7)34,38,34
34 X(IAUS)=W2+1./W7
C
C SECOND TEST FOR LOSS OF SIGNIFICANCE
C
C IF(ABS(X(IAUS))-ABS(W2)*1.E-5)35,37,37
35 IF(X(IAUS))36,37,36
C
36 NEW=IAUS-1
   ISW2=0
   GO TO 41
C
37 IF(W2-1.E38)39,38,38
38 X(IAUS)=1.E38
   IMIN=1
C
39 W1=W4
   T=W2
   W2=W5
   W3=W6
   ISW1=ISW2
40 ISW2=0
C
NEW=NEW-IMIN
C
C TEST FOR ACCURACY
C
41 IEND=NEW-1
   DO 47 I=1,IEND
   W1=ABS(X(I)-X(I+1))
   W2=ABS(X(I+1))
   IF(W1-EPS)44,44,42
42 IF(W2-1.)46,46,43
43 IF(W1-EPS*W2)44,44,46
44 ISW2=ISW2+1
   IF(3-ISW2)45,45,47
45 FIN=X(I)
   IER=0
   RETURN
C
46 ISW2=0
47 CONTINUE
C
IF(NEW-6)48,2,2
48 FIN=X(NEW)
   IER=1
   RETURN
   END
TEAS1310
TEAS1320
TEAS1330
TEAS1340
TEAS1350
TEAS1360
TEAS1370
TEAS1380
TEAS1390
TEAS1400
TEAS1410
TEAS1420
TEAS1430
TEAS1440
TEAS1450
TEAS1460
TEAS1470
TEAS1480
TEAS1490
TEAS1500
TEAS1510
TEAS1520
TEAS1530
TEAS1540
TEAS1550
TEAS1560
TEAS1570
TEAS1580
TEAS1590
TEAS1600
TEAS1610
TEAS1620
TEAS1630
TEAS1640
TEAS1650
TEAS1660
TEAS1670
TEAS1680
TEAS1690
TEAS1700
TEAS1710
TEAS1720
TEAS1730
TEAS1740
TEAS1750
TEAS1760
TEAS1770
TEAS1780
TEAS1790
TEAS1800
TEAS1810
TEAS1820
TEAS1830
TEAS1840
TEAS1850
TEAS1860
TEAS1870
TEAS1880
TEAS1890
TEAS1900
TEAS1910
TEAS1920
TEAS1930
TEAS1940
TEAS1950
TEAS1960
TEAS1970
TEAS1980
TEAS1990
TEAS2000
TEAS2010
TEAS2020
TEAS2030
TEAS2040

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C
C ..... DTEA 10
C DTEA 20
C DTEA 30
C SUBROUTINE DTEAS DTEA 40
C DTEA 50
C DTEA 60
C PURPOSE DTEA 70
C CALCULATE THE LIMIT OF A GIVEN SEQUENCE BY MEANS OF THE DTEA 80
C EPSILON-ALGORITHM. DTEA 90
C DTEA 100
C USAGE DTEA 110
C CALL DTEAS(X,N,FIN,EPS,IER) DTEA 120
C DTEA 130
C DESCRIPTION OF PARAMETERS DTEA 140
C X - DOUBLE PRECISION VECTOR WHOSE COMPONENTS ARE TERMS DTEA 150
C OF THE GIVEN SEQUENCE. ON RETURN THE COMPONENTS OF DTEA 160
C VECTOR X ARE DESTROYED. DTEA 170
C N - DIMENSION OF INPUT VECTOR X. DTEA 180
C FIN - RESULTANT SCALAR IN DOUBLE PRECISION CONTAINING ON DTEA 190
C RETURN THE LIMIT OF THE GIVEN SEQUENCE. DTEA 200
C EPS - SINGLE PRECISION INPUT VALUE, WHICH SPECIFIES THE DTEA 210
C UPPER BOUND OF THE RELATIVE (ABSOLUTE) ERROR IF THE DTEA 220
C COMPONENTS OF X ARE ABSOLUTELY GREATER (LESS) THAN DTEA 230
C ONE. DTEA 240
C CALCULATION IS TERMINATED AS SOON AS THREE TIMES IN DTEA 250
C SUCCESSION THE RELATIVE (ABSOLUTE) DIFFERENCE DTEA 260
C BETWEEN NEIGHBOURING TERMS IS NOT GREATER THAN EPS. DTEA 270
C IER - RESULTANT ERROR PARAMETER CODED IN THE FOLLOWING DTEA 280
C FORM DTEA 290
C IER=0 - NO ERROR DTEA 300
C IER=1 - REQUIRED ACCURACY NOT REACHED WITH DTEA 310
C MAXIMAL NUMBER OF ITERATIONS DTEA 320
C IER=-1 - INTEGER N IS LESS THAN TEN. DTEA 330
C DTEA 340
C REMARKS DTEA 350
C NO ACTION BESIDES ERROR MESSAGE IN CASE N LESS THAN TEN. DTEA 360
C THE CHARACTER OF THE GIVEN INFINITE SEQUENCE MUST BE DTEA 370
C RECOGNIZABLE BY THOSE N COMPONENTS OF THE INPUT VECTOR X. DTEA 380
C DTEA 390
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DTEA 400
C NONE DTEA 410
C DTEA 420
C METHOD DTEA 430
C THE CONVERGENCE OF THE GIVEN SEQUENCE IS ACCELERATED BY DTEA 440
C MEANS OF THE E(2)-TRANSFORMATION, USED IN AN ITERATIVE WAY. DTEA 450
C FOR REFERENCE, SEE DTEA 460
C ALGORITHM 215, SHANKS, CACM 1963, NO. 11, PP. 662. AND DTEA 470
C P. WYNN, SINGULAR RULES FOR CERTAIN NON-LINEAR ALGORITHMS DTEA 480
C BIT VOL. 3, 1963, PP. 175-195. DTEA 490
C ..... DTEA 500
C SUBROUTINE DTEAS(X,N,FIN,EPS,IER) DTEA 510
C DTEA 520
C DIMENSION X(1) DTEA 530
C DOUBLE PRECISION X,FIN,W1,W2,W3,W4,W5,W6,W7,T DTEA 540
C DTEA 550
C TEST ON WRONG INPUT PARAMETER N DTEA 560
C DTEA 570
C NEW=N DTEA 580
C IF(NEW-10)1,2,2 DTEA 590
C 1 IER=-1 DTEA 600
C RETURN DTEA 610
C DTEA 620
C CALCULATE INITIAL VALUES FOR THE EPSILON ARRAY DTEA 630
C DTEA 640
C 2 ISW1=0 DTEA 650
C ISW2=0 DTEA 660
C W1=1.038 DTEA 670
C W7=X(4)-X(3) DTEA 680
C IF(W7)3,4,3 DTEA 690
C 3 W1=1.00/W7 DTEA 700
C DTEA 710
C 4 W5=1.038 DTEA 720
C W7=X(2)-X(1) DTEA 730
C IF(W7)5,6,5 DTEA 740
C 5 W5=1.00/W7 DTEA 750
C DTEA 760
C 6 W4=X(3)-X(2) DTEA 770
C IF(W4)9,7,9 DTEA 780
C 7 W4=1.038 DTEA 790
C T=X(2) DTEA 800
C W2=X(3) DTEA 810
C W3=1.038 DTEA 820
C GO TO 17 DTEA 830
C DTEA 840
C 9 W4=1.00/W4 DTEA 850
C DTEA 860
C T=1.038 DTEA 870
C W7=W4-W5 DTEA 880
C IF(W7)10,11,13 DTEA 890
C 10 T=X(2)+1.00/W7 DTEA 900
C DTEA 910
C 11 W2=W1-W4 DTEA 920
C IF(W2)15,12,15 DTEA 930
C 12 W2=1.038 DTEA 940
C IF(T-1.038)13,14,14 DTEA 950
C 13 ISW2=1 DTEA 960
C W3=W4 DTEA 970
C GO TO 17 DTEA 980
C DTEA 990
C 15 W2=X(3)+1.00/W2 DTEA 1000
C W7=W2-T DTEA 1010
C IF(W7)16,8,16 DTEA 1020
C 16 W3=W4+1.00/W7 DTEA 1030
C DTEA 1040
C 17 ISW1=ISW2 DTEA 1050
C ISW2=0 DTEA 1060
C IMIN=4 DTEA 1070
C DTEA 1080
C CALCULATE DIAGONALS OF THE EPSILON ARRAY IN A DO-LOOP DTEA 1090
C DTEA 1100
C DTEA 1110
C DO 40 I=5,NEW DTEA 1120
C IAUS=I-IMIN DTEA 1130
C W4=1.038 DTEA 1140
C W5=X(I-1) DTEA 1150
C W7=X(I)-X(I-1) DTEA 1160
C IF(W7)18,24,18 DTEA 1170
C 18 W4=1.00/W7 DTEA 1180
C DTEA 1190
C IF(W1-1.038)19,25,25 DTEA 1200
C 19 W6=W4-W1 DTEA 1210
C DTEA 1220
C TEST FOR NECESSITY OF A SINGULAR RULE DTEA 1230
C DTEA 1240
C IF(DABS(W6)-DABS(W4))*1.0-12)20,20,22 DTEA 1250
C 20 ISW2=1 DTEA 1260
C IF(W6)22,21,22 DTEA 1270
C 21 W5=1.038 DTEA 1280
C W6=W1 DTEA 1290
C IF(W2-1.038)28,26,26 DTEA 1300
C 22 W5=X(I-1)+1.00/W6 DTEA 1310
C DTEA 1320
C FIRST TEST FOR LOSS OF SIGNIFICANCE DTEA 1330
C DTEA 1340
C IF(DABS(W5)-DABS(X(I-1)))*1.0-10)23,24,24 DTEA 1350
C 23 IF(W5)36,24,36 DTEA 1360
C DTEA 1370
C 24 W7=W5-W2 DTEA 1380
C IF(W7)27,25,27 DTEA 1390
C 25 W6=1.038 DTEA 1400
C 26 ISW2=0 DTEA 1410
C X(IAUS)=W2 DTEA 1420
C GO TO 37 DTEA 1430
C 27 W6=W1+1.00/W7 DTEA 1440
C 28 IF(1)33,29,29 DTEA 1450
C DTEA 1460
C CALCULATE X(IAUS) WITH HELP OF SINGULAR RULE DTEA 1470
C DTEA 1480
C 29 IF(W2-1.038)30,32,32 DTEA 1490
C 30 W7=W5/(W2-W5)+T/(W2-T)+X(I-2)/(X(I-2)-W2) DTEA 1500
C IF(1.00+W7)31,38,31 DTEA 1510
C 31 X(IAUS)=W7+W2/(1.00+W7) DTEA 1520
C GO TO 39 DTEA 1530
C DTEA 1540
C 32 X(IAUS)=W5+T-X(I-2) DTEA 1550
C GO TO 39 DTEA 1560
C DTEA 1570
C 33 W7=W6-W3 DTEA 1580
C IF(W7)34,38,34 DTEA 1590
C 34 X(IAUS)=W2+1.00/W7 DTEA 1600
C DTEA 1610
C SECOND TEST FOR LOSS OF SIGNIFICANCE DTEA 1620
C DTEA 1630
C IF(DABS(X(IAUS))-DABS(W2))*1.0-10)35,37,37 DTEA 1640
C 35 IF(X(IAUS))36,37,36 DTEA 1650
C DTEA 1660
C 36 NEW=IAUS DTEA 1670
C ISW2=0 DTEA 1680
C GO TO 41 DTEA 1690
C DTEA 1700
C 37 IF(W2-1.038)39,38,38 DTEA 1710
C 38 X(IAUS)=1.038 DTEA 1720
C IMIN=1 DTEA 1730
C DTEA 1740
C 39 W1=W4 DTEA 1750
C T=W2 DTEA 1760
C W2=W5 DTEA 1770
C W3=W6 DTEA 1780
C ISW1=ISW2 DTEA 1790
C 40 ISW2=0 DTEA 1800
C DTEA 1810
C NEW=NEW-IMIN DTEA 1820
C DTEA 1830
C TEST FOR ACCURACY DTEA 1840
C DTEA 1850
C 41 IEND=NEW-1 DTEA 1860
C DO 47 I=1,IEND DTEA 1870
C HE1=DABS(X(I)-X(I+1)) DTEA 1880
C HE2=DABS(X(I+1)) DTEA 1890
C IF(HE1-EPS)44,44,42 DTEA 1900
C 42 IF(HE2-1.146)46,43 DTEA 1910
C 43 IF(HE1-EPS*HE2)44,44,46 DTEA 1920
C 44 ISW2=ISW2+1 DTEA 1930
C IF(3-ISW2)45,45,47 DTEA 1940
C 45 FIN=X(I) DTEA 1950
C IER=0 DTEA 1960
C RETURN DTEA 1970
C DTEA 1980
C 46 ISW2=0 DTEA 1990
C 47 CONTINUE DTEA 2000
C DTEA 2010
C IF(NEW-6)48,2,2 DTEA 2020
C 48 FIN=X(NEW) DTEA 2030
C IER=1 DTEA 2040
C RETURN DTEA 2050
C END DTEA 2060

```

Subroutines TEUL and DTEUL

These subroutines calculate the sum value of the series $\sum_{k=1}^{\infty} F_k$ by means of a refined Euler transformation.

The following abbreviations are used:

$$\Delta^0 F_i = F_i$$

$$\Delta^1 F_i = \frac{1}{2} [F_i + F_{i+1}]$$

$$\Delta^2 F_i = \frac{1}{2} [\Delta F_i + \Delta F_{i+1}] = \frac{1}{4} [F_i + 2F_{i+1} + F_{i+2}]$$

$$\Delta^3 F_i = \frac{1}{2} [\Delta^2 F_i + \Delta^2 F_{i+1}] = \frac{1}{8} [F_i + 3F_{i+1} + 3F_{i+2} + F_{i+3}]$$

Generally:

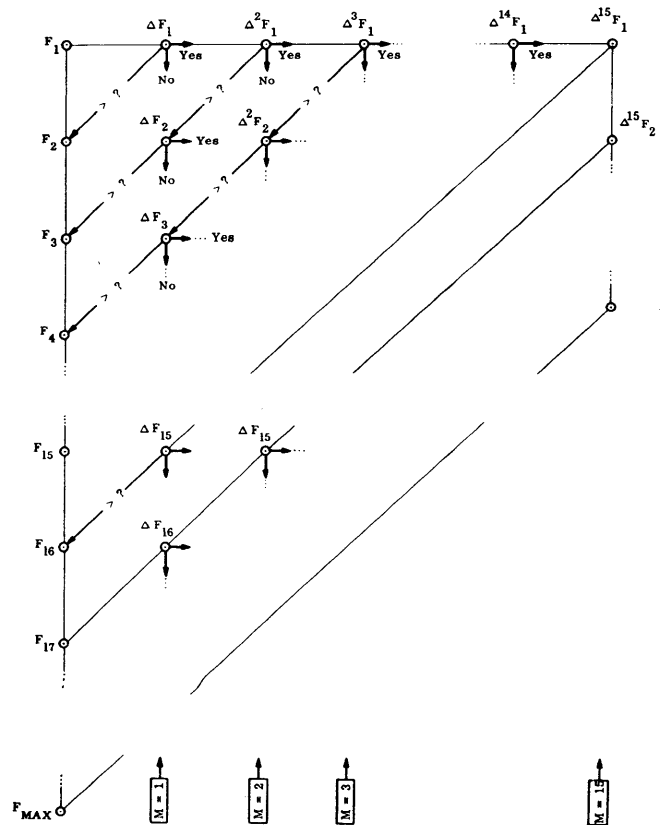
$$\Delta^m F_i = \frac{1}{2} [\Delta^{m-1} F_i + \Delta^{m-1} F_{i+1}] = \frac{1}{2^m} [F_i + \binom{m}{1} F_{i+1} + \binom{m}{2} F_{i+2} + \dots + \binom{m}{m-1} F_{i+m-1} + \binom{m}{m} F_{i+m}]$$

Euler transformation means that the given infinite series will be transformed as follows:

$$\sum_{k=1}^{\infty} F_k = \frac{1}{2} [F_1 + \Delta F_1 + \Delta^2 F_1 + \Delta^3 F_1 + \Delta^4 F_1 + \dots]$$

The transformed series will converge whenever the given series does, and to the same sum. It may even converge when the parent series does not; in this case the sum is called the Euler sum of the parent series.

A refined Euler transformation is explained by means of the following diagram.



The computation is done in this way. First the absolute value $|\Delta F_1|$ is compared with $|F_2|$ (see diagram). In case $|\Delta F_1| < |F_2|$, the value $\frac{1}{2}(\Delta F_1)$ is added to the initial value $\frac{1}{2}F_1$ (the beginning of the Euler transformation). Then $|\Delta^2 F_1|$ is compared with $|\Delta F_2|$ (see "YES" in diagram).

In case $|\Delta F_1| \geq |F_2|$, the value ΔF_1 is added to $\frac{1}{2}F_1$ and, as next $|\Delta F_2|$, is compared with $|F_3|$ (see "NO"). This means that F_1 is added unchanged, and the Euler transformation is delayed for one term, and so forth.

If in this sequence of comparisons $|\Delta^i F_k| < |\Delta^{i-1} F_{k+1}|$ is generally true, the value $\frac{1}{2}(\Delta^i F_k)$ is added to the current sum in the sense of the Euler transformation. If it is not true, the value $\Delta^i F_k$ is added and the Euler transformation is delayed for one term--that is, the terms F_1, F_2, \dots, F_k are added unchanged, and the transformation actually starts with term F_{k+1} .

The highest term in the scheme of calculation may be $\Delta^{15} F_i$ ($i = 1, 2, 3, \dots, \text{MAX}-15$), in case $\text{MAX} > 15$. Hence a maximum of fourteen terms of the series may be transformed in succession by Euler. If the procedure is not terminated up to this point, the index of the transformed terms is raised by 1, and a further unchanged term is added.

The last term of the parent series which may be used by the computation is F_{MAX} .

The procedure is terminated if with five successive terms of the series the relative change of the sum value is less than EPS, or if MAX terms of the series were used for calculation.

For reference see:

- (1.) F. B. Hildebrand, Introduction to Numerical Analysis, McGraw-Hill, New York/Toronto/London, 1956, pp. 155 - 160.
- (2.) P. Naur, "Report on the Algorithmic Language ALGOL 60", CACM, vol. 3, no. 5 (1960), pp. 311.

```

C      TEUL 15
C      TEUL 20
C      TEUL 30
C      SUBROUTINE TEUL          TEUL 40
C      TEUL 50
C      PURPOSE                  TEUL 60
C      COMPUTE THE SUM OF FCT(K) FOR K FROM ONE UP TO INFINITY. TEUL 70
C      TEUL 80
C      USAGE                    TEUL 90
C      CALL TEUL(FCT,SUM,MAX,EPS,IER)
C      PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT. TEUL 100
C      TEUL 110
C      TEUL 120
C      DESCRIPTION OF PARAMETERS TEUL 130
C      FCT - NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED. TEUL 140
C      IT COMPUTES THE K-TH TERM OF THE SERIES TO ANY TEUL 150
C      GIVEN INDEX K. TEUL 160
C      SUM - RESULTANT VALUE CONTAINING ON RETURN THE SUM OF TEUL 170
C      THE GIVEN SERIES. TEUL 180
C      MAX - INPUT VALUE, WHICH SPECIFIES THE MAXIMAL NUMBER TEUL 190
C      OF TERMS OF THE SERIES THAT ARE RESPECTED. TEUL 200
C      EPS - INPUT VALUE, WHICH SPECIFIES THE UPPER BOUND OF TEUL 210
C      THE RELATIVE ERROR. TEUL 220
C      SUMMATION IS STOPPED AS SOON AS FIVE TIMES IN TEUL 230
C      SUCCESSION THE ABSOLUTE VALUE OF THE TERMS OF THE TEUL 240
C      TRANSFORMED SERIES ARE FOUND TO BE LESS THAN TEUL 250
C      EPS*(ABSOLUTE VALUE OF CURRENT SUM). TEUL 250
C      IER - RESULTANT ERROR PARAMETER CODED IN THE FOLLOWING TEUL 270
C      FORM TEUL 280
C      IER=0 - NO ERROR TEUL 285
C      IER=1 - REQUIRED ACCURACY NOT REACHED WITH TEUL 300
C      MAXIMAL NUMBER OF TERMS TEUL 310
C      IER=-1 - THE INTEGER MAX IS LESS THAN ONE. TEUL 320
C      TEUL 330
C      REMARKS                  TEUL 340
C      NO ACTION BESIDES ERROR MESSAGE IN CASE MAX LESS THAN ONE. TEUL 350
C      TEUL 360
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED TEUL 370
C      THE EXTERNAL FUNCTION SUBPROGRAM FCT(K) MUST BE FURNISHED TEUL 380
C      BY THE USER. TEUL 390
C      TEUL 400
C      METHOD                   TEUL 410
C      EVALUATION IS DONE BY MEANS OF A SUITABLY REFINED EULER TEUL 420
C      TRANSFORMATION. FOR REFERENCE, SEE TEUL 430
C      F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS, TEUL 440
C      MCGRAW/HILL, NEW YORK/TORONTO/LONDON, 1956, PP.155-160, AND TEUL 450
C      P. NAUR, REPORT ON THE ALGORITHMIC LANGUAGE ALGOL 60, TEUL 460
C      CACM, VOL.3, ISS.5 (1960), PP.311. TEUL 470
C      TEUL 480
C      .....
C      SUBROUTINE TEUL (FCT,SUM,MAX,EPS,IER) TEUL 490
C      TEUL 500
C      DIMENSION Y(15) TEUL 510
C      TEUL 520
C      TEST ON WRONG INPUT PARAMETER MAX TEUL 530
C      TEUL 540
C      IF(MAX)1,1,2 TEUL 550
C      1 IER=-1 TEUL 560
C      GOTO 12 TEUL 570
C      TEUL 580
C      INITIALIZE EULER TRANSFORMATION TEUL 590
C      TEUL 600
C      2 IER=1 TEUL 610
C      I=1 TEUL 620
C      M=1 TEUL 630
C      N=1 TEUL 640
C      Y(1)=FCT(N) TEUL 650
C      SUM=Y(1)*.5 TEUL 660
C      TEUL 670
C      START EULER-LOOP TEUL 680
C      TEUL 690
C      3 J=0 TEUL 700
C      4 I=I+1 TEUL 710
C      IF(I=-MAX)5,5,12 TEUL 720
C      5 N=I TEUL 730
C      AMN=FCT(N) TEUL 740
C      DO 6 K=1,M TEUL 750
C      AMP=(AMN+Y(K))*5 TEUL 760
C      Y(K)=AMN TEUL 770
C      6 AMN=AMP TEUL 780
C      TEUL 790
C      CHECK EULER TRANSFORMATION TEUL 800
C      TEUL 810
C      IF(ABS(AMN)-ABS(Y(M)))7,9,9 TEUL 820
C      7 IF(M-15)8,9,9 TEUL 830
C      8 M=M+1 TEUL 840
C      Y(M)=AMN TEUL 850
C      AMN=.5*AMN TEUL 860
C      TEUL 870
C      UPDATE SUM TEUL 880
C      TEUL 890
C      9 SUM=SUM+AMN TEUL 900
C      IF(ABS(AMN)-EPS*ABS(SUM))10,10,3 TEUL 910
C      TEUL 920
C      TEST END OF PROCEDURE TEUL 930
C      TEUL 940
C      TEUL 950
C      10 J=J+1 TEUL 960
C      IF(J-5)4,11,11 TEUL 970
C      11 IER=0 TEUL 980
C      12 RETURN TEUL 990
C      END TEUL1000

```


Interpolation, Approximation, and Smoothing

Subroutines ALI and DALI

These subroutines perform an Aitken-Lagrange interpolation. Given the table x_i, y_i ($i = 1, 2, \dots, n$) of argument and function values stored in the two one-dimensional storage arrays ARG and VAL, the problem is to interpolate function value Y at the given point X. It is assumed that the table represents a single-valued function $y = y(x)$ which is suitable for approximation by a polynomial⁺, and that $|x_i - X| \geq |x_j - X|$ for $i > j$.⁺⁺

Then, using the following formulas:

$$y_{1,2} = \frac{1}{x_2 - x_1} \cdot \begin{vmatrix} y_1 & x_1 - X \\ y_2 & x_2 - X \end{vmatrix} ;$$

$$y_{1,3} = \frac{1}{x_3 - x_1} \cdot \begin{vmatrix} y_1 & x_1 - X \\ y_3 & x_3 - X \end{vmatrix} ,$$

$$y_{1,2,3} = \frac{1}{x_3 - x_2} \cdot \begin{vmatrix} y_{1,2} & x_2 - X \\ y_{1,3} & x_3 - X \end{vmatrix} ;$$

$$y_{1,4} = \frac{1}{x_4 - x_1} \cdot \begin{vmatrix} y_1 & x_1 - X \\ y_4 & x_4 - X \end{vmatrix} ,$$

$$y_{1,2,4} = \frac{1}{x_4 - x_2} \cdot \begin{vmatrix} y_{1,2} & x_2 - X \\ y_{1,4} & x_4 - X \end{vmatrix} ,$$

$$y_{1,2,3,4} = \frac{1}{x_4 - x_3} \cdot \begin{vmatrix} y_{1,2,3} & x_3 - X \\ y_{1,2,4} & x_4 - X \end{vmatrix} ;$$

..... ,

it is possible to generate by row the triangular Aitken scheme shown in Figure 18.

x_1	y_1				
x_2	y_2	$y_{1,2}$			
x_3	y_3	$y_{1,3}$	$y_{1,2,3}$		
x_4	y_4	$y_{1,4}$	$y_{1,2,4}$	$y_{1,2,3,4}$	
\vdots	\vdots	\vdots	\vdots		
x_n	y_n	$y_{1,n}$	$y_{1,2,n}$	$y_{1,2,3,n}$	$\dots y_{1,2,3,\dots,n}$

Figure 18. Aitken's scheme for Lagrange interpolation

All result values of row j can be stored in VAL(J). Thus, it is possible to generate the downward diagonal of Aitken's scheme in storage array VAL, using the machine-processable formula:

$$VAL(J) = \frac{VAL(I)*(X-ARG(J)) - VAL(J)*(X-ARG(I))}{ARG(I) - ARG(J)} \quad (I = 1, 2, \dots, J-1) \quad (1)$$

for $J = 2, 3, \dots, NDIM$.

The procedure stops under the following conditions: if the difference of two successive values in the downward diagonal is absolutely less than a given tolerance ϵ (test starts at step $J = 3$), or if the absolute value of this difference stops diminishing, thus showing the influence of rounding errors (test starts at step $J = 5$, or for double-precision, $J = 8$), or if the procedure has worked through the whole triangular Aitken scheme, or if it discovers two table points with identical arguments.

Finally, Y is set equal to VAL(J) in case of monotonically decreasing absolute differences, or equal to VAL(J-1) if these differences start oscillating.

For reference see F. B. Hildebrand, Introduction to Numerical Analysis, McGraw-Hill, New York/Toronto/London, 1956, pp. 49-50.

⁺This order in table x_i, y_i , ($i = 1, 2, \dots, n$) could be generated by subroutines ATSG, ATSM, ATSE, DATSG, DATSM, DATSE.

⁺⁺This means $y(x)$ should be closely approximated by a polynomial of low degree which has the table points with arguments next to x as nodes.

```

C ..... ALI 10
C ..... ALI 20
C ..... ALI 30
C ..... ALI 40
C ..... ALI 50
C ..... ALI 60
C ..... ALI 70
C ..... ALI 80
C ..... ALI 90
C ..... ALI 100
C ..... ALI 110
C ..... ALI 120
C ..... ALI 130
C ..... ALI 140
C ..... ALI 150
C ..... ALI 160
C ..... ALI 170
C ..... ALI 180
C ..... ALI 190
C ..... ALI 200
C ..... ALI 210
C ..... ALI 220
C ..... ALI 230
C ..... ALI 240
C ..... ALI 250
C ..... ALI 260
C ..... ALI 270
C ..... ALI 280
C ..... ALI 290
C ..... ALI 300
C ..... ALI 310
C ..... ALI 320
C ..... ALI 330
C ..... ALI 340
C ..... ALI 350
C ..... ALI 360
C ..... ALI 370
C ..... ALI 380
C ..... ALI 390
C ..... ALI 400
C ..... ALI 410
C ..... ALI 420
C ..... ALI 430
C ..... ALI 440
C ..... ALI 450
C ..... ALI 460
C ..... ALI 470
C ..... ALI 480
C ..... ALI 490
C ..... ALI 500
C ..... ALI 510
C ..... ALI 520
C ..... ALI 530
C ..... ALI 540
C ..... ALI 550
C ..... ALI 560
C ..... ALI 570
C ..... ALI 580
C ..... ALI 590
C ..... ALI 600
C ..... ALI 610
C ..... ALI 620
C ..... ALI 630
C ..... ALI 640
C ..... ALI 650
C ..... ALI 660
C ..... ALI 670
C ..... ALI 680
C ..... ALI 690
C ..... ALI 700
C ..... ALI 710
C ..... ALI 720
C ..... ALI 730
C ..... ALI 740
C ..... ALI 750
C ..... ALI 760
C ..... ALI 770
C ..... ALI 780
C ..... ALI 790
C ..... ALI 800
C ..... ALI 810
C ..... ALI 820
C ..... ALI 830
C ..... ALI 840
C ..... ALI 850
C ..... ALI 860
C ..... ALI 870
C ..... ALI 880
C ..... ALI 890
C ..... ALI 900
C ..... ALI 910
C ..... ALI 920
C ..... ALI 930
C ..... ALI 940
C ..... ALI 950
C ..... ALI 960
C ..... ALI 970
C ..... ALI 980
C ..... ALI 990
C ..... ALI 1000
C ..... ALI 1010
C ..... ALI 1020
C ..... ALI 1030
C ..... ALI 1040
C ..... ALI 1050
C ..... ALI 1060
C ..... ALI 1070
C ..... ALI 1080

```

```

C ..... DALI 10
C ..... DALI 20
C ..... DALI 30
C ..... DALI 40
C ..... DALI 50
C ..... DALI 60
C ..... DALI 70
C ..... DALI 80
C ..... DALI 90
C ..... DALI 100
C ..... DALI 110
C ..... DALI 120
C ..... DALI 130
C ..... DALI 140
C ..... DALI 150
C ..... DALI 160
C ..... DALI 170
C ..... DALI 180
C ..... DALI 190
C ..... DALI 200
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C ..... DALI 410
C ..... DALI 420
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C ..... DALI 470
C ..... DALI 480
C ..... DALI 490
C ..... DALI 500
C ..... DALI 510
C ..... DALI 520
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C ..... DALI 640
C ..... DALI 650
C ..... DALI 660
C ..... DALI 670
C ..... DALI 680
C ..... DALI 690
C ..... DALI 700
C ..... DALI 710
C ..... DALI 720
C ..... DALI 730
C ..... DALI 740
C ..... DALI 750
C ..... DALI 760
C ..... DALI 770
C ..... DALI 780
C ..... DALI 790
C ..... DALI 800
C ..... DALI 810
C ..... DALI 820
C ..... DALI 830
C ..... DALI 840
C ..... DALI 850
C ..... DALI 860
C ..... DALI 870
C ..... DALI 880
C ..... DALI 890
C ..... DALI 900
C ..... DALI 910
C ..... DALI 920
C ..... DALI 930
C ..... DALI 940
C ..... DALI 950
C ..... DALI 960
C ..... DALI 970
C ..... DALI 980
C ..... DALI 990
C ..... DALI 1000
C ..... DALI 1010
C ..... DALI 1020
C ..... DALI 1030
C ..... DALI 1040
C ..... DALI 1050
C ..... DALI 1060
C ..... DALI 1070
C ..... DALI 1080
C ..... DALI 1090
C ..... DALI 1100
C ..... DALI 1110

```

Subroutines AHI and DAHI

These subroutines perform an Aitken-Hermite interpolation. Given the table x_i, y_i, y'_i ($i = 1, 2, \dots, n$) of argument, function and derivative values, stored in the two one-dimensional storage arrays ARG and VAL, the problem is to interpolate function value Y at the given point X. It is assumed that the table represents a single-valued function $y = y(x)$ which is suitable for approximation by a polynomial⁺, and that it is stored as shown in Figure 19 (first and second column) with $|x_i - X| \geq |x_j - X|$ for $i > j$.⁺⁺

Before starting Aitken's iteration scheme, the components of vector VAL (that is, function and derivative values) are replaced by interpolation values z_i of first order (third column). This is done by the following machine-processable formulas:

$$\text{VAL}(I) = Y + \text{VAL}(I+1) * H_1$$

$$(I = 1, 3, 5, \dots, 2 * \text{NDIM}-1) \quad (1)$$

$$\text{VAL}(I+1) = Y + (\text{VAL}(I+2)-Y) \frac{H_1}{H_1 - H_2}$$

$$(I = 1, 3, 5, \dots, 2 * \text{NDIM}-3) \quad (2)$$

with

$$Y = \text{VAL}(I), \quad H_1 = X - \text{ARG}(J-1), \quad H_2 = X - \text{ARG}(J)$$

and

$$J = \frac{I+1}{2} + 1.$$

Now it is possible to generate successively the upward diagonals of the triangular Aitken scheme, using the following formulas:

⁺This order in table x_i, y_i, y'_i ($i = 1, 2, \dots, n$) could be generated by subroutines ATSG, ATSM, ATSE, DATSG, DATSM, DATSE.

⁺⁺This means $y(x)$ should be closely approximated by a polynomial of low degree which has the table points with arguments next to x as nodes and which has the specified derivative values in these nodes.

$$z_{1,2} = \frac{1}{x_2 - x_1} \cdot \begin{vmatrix} z_1 & x_1 - X \\ z_2 & x_2 - X \end{vmatrix};$$

$$z_{2,3} = \frac{1}{x_2 - x_1} \cdot \begin{vmatrix} z_2 & x_1 - X \\ z_3 & x_2 - X \end{vmatrix},$$

$$z_{1,2,3} = \frac{1}{x_2 - x_1} \cdot \begin{vmatrix} z_{1,2} & x_1 - X \\ z_{2,3} & x_2 - X \end{vmatrix};$$

$$z_{3,4} = \frac{1}{x_3 - x_2} \cdot \begin{vmatrix} z_3 & x_2 - X \\ z_4 & x_3 - X \end{vmatrix},$$

$$z_{2,3,4} = \frac{1}{x_3 - x_1} \cdot \begin{vmatrix} z_{2,3} & x_1 - X \\ z_{3,4} & x_3 - X \end{vmatrix};$$

$$z_{1,2,3,4} = \frac{1}{x_3 - x_1} \cdot \begin{vmatrix} z_{1,2,3} & x_1 - X \\ z_{2,3,4} & x_3 - X \end{vmatrix};$$

.....

All result values of an upward diagonal can be stored in positions of vector VAL with decreasing subscripts, using the machine-processable formula:

$$\text{VAL}(K) = \frac{\text{VAL}(K)*(X-H_1) - \text{VAL}(K+1)*(X-\text{ARG}(L))}{\text{ARG}(L) - H_1}$$

$$(J = 1, 2, \dots, I) \quad (3)$$

with

$$K = I + 1 - J, \quad M = \left\lceil \frac{I+3}{2} \right\rceil, \quad L = \left\lceil \frac{K+1}{2} \right\rceil$$

and

$$H_1 = \text{ARG}(M)$$

for $I = 1, 2, \dots, 2 * \text{NDIM}-2$.

The procedure stops under the following circumstances: if the difference between two successive interpolated values VAL(I) is absolutely less than a given tolerance ϵ or if the absolute value of this difference stops diminishing, thus showing the influence of rounding errors (test starts at step $i = 5$, or for double-precision, $i = 8$), or if the procedure has worked through the whole triangular Aitken scheme, or if it discovers two table points with identical arguments.

ARG(1) = x ₁	VAL(1) = y ₁	VAL(1) = z ₁	z _{1,2}	z _{1,2,3}	z _{1,2,3,4}
ARG(2) = x ₂	VAL(2) = y ₁	VAL(2) = z ₂	z _{2,3}	z _{2,3,4}	
...	VAL(3) = y ₂	VAL(3) = z ₃	z _{3,4}		
...	VAL(4) = y ₂	VAL(4) = z ₄			
...
ARG(NDIM) = x _n	VAL(2*NDIM-1) = y _n	VAL(2*NDIM-1) = z _{2n-1}			
	VAL(2*NDIM) = y _n				

```

C SUBROUTINE AHI(X,ARG,VAL,Y,NDIM,EPS,IER) AHI 730
C AHI 740
C AHI 750
C DIMENSION ARG(1),VAL(1) AHI 760
C IER=2 AHI 770
C H2=X-ARG(1) AHI 780
C IF(NDIM-1)2,1,3 AHI 790
C 1 Y=VAL(1)+VAL(2)*H2 AHI 800
C 2 RETURN AHI 810
C AHI 820
C VECTOR ARG HAS MORE THAN 1 ELEMENT. AHI 830
C THE FIRST STEP PREPARES VECTOR VAL SUCH THAT AITKEN SCHEME CAN BE AHI 840
C USED. AHI 850
C 3 I=1 AHI 860
C DO 5 J=2,NDIM AHI 870
C H1=H2 AHI 880
C H2=X-ARG(J) AHI 890
C Y=VAL(I) AHI 900
C VAL(I)=Y+VAL(I+1)*H1 AHI 910
C H1=H2 AHI 920
C IF(H1)4,13,4 AHI 930
C 4 VAL(I+1)=Y+(VAL(I+2)-Y)*H1/H AHI 940
C 5 I=I+2 AHI 950
C VAL(I)=VAL(I)+VAL(I+1)*H2 AHI 960
C END OF FIRST STEP AHI 970
C AHI 980
C PREPARE AITKEN SCHEME AHI 990
C DELT2=0. AHI 1000
C IEND=I-1 AHI 1010
C AHI 1020
C START AITKEN-LOOP AHI 1030
C DO 9 I=1,IEND AHI 1040
C DELT1=DELT2 AHI 1050
C Y=VAL(I) AHI 1060
C M=(I+3)/2 AHI 1070
C H1=ARG(M) AHI 1080
C DO 6 J=1,I AHI 1090
C K=I+1-J AHI 1100
C L=(K+1)/2 AHI 1110
C H=ARG(L)-H1 AHI 1120
C IF(H)6,14,6 AHI 1130
C 6 VAL(K)=(VAL(K)*(X-H1)-VAL(K+1)*(X-ARG(L)))/H AHI 1140
C DELT2=ABS(Y-VAL(1)) AHI 1150
C IF(DELT2-EPS)11,11,7 AHI 1160
C 7 IF(I-5)9,8,8 AHI 1170
C 8 IF(DELT2-DELT1)9,12,12 AHI 1180
C 9 CONTINUE AHI 1190
C END OF AITKEN-LOOP AHI 1200
C AHI 1210
C 10 Y=VAL(I) AHI 1220
C RETURN AHI 1230
C AHI 1240
C THERE IS SUFFICIENT ACCURACY WITHIN 2*NDIM-2 ITERATION STEPS AHI 1250
C IER=0 AHI 1260
C GOTO 10 AHI 1270
C AHI 1280
C TEST VALUE DELT2 STARTS OSCILLATING AHI 1290
C IER=1 AHI 1300
C RETURN AHI 1310
C THERE ARE TWO IDENTICAL ARGUMENT VALUES IN VECTOR ARG AHI 1320
C 13 Y=VAL(I) AHI 1330
C 14 IER=3 AHI 1340
C RETURN AHI 1350
C END AHI 1360
C AHI 1370
C AHI 1380
C AHI 1390
C AHI 1400
C SUBROUTINE DAHI AHI 1410
C DAHI 1420
C DAHI 1430
C DAHI 1440
C PURPOSE AHI 1450
C TO INTERPOLATE FUNCTION VALUE Y FOR A GIVEN ARGUMENT VALUE AHI 1460
C X USING A GIVEN TABLE (ARG,VAL) OF ARGUMENT, FUNCTION, AND AHI 1470
C DERIVATIVE VALUES. AHI 1480
C DAHI 1490
C USAGE AHI 1500
C CALL DAHI (X,ARG,VAL,Y,NDIM,EPS,IER) AHI 1510
C DAHI 1520
C DESCRIPTION OF PARAMETERS AHI 1530
C X - DOUBLE PRECISION ARGUMENT VALUE SPECIFIED BY INPUT. DAHI 1540
C ARG - DOUBLE PRECISION INPUT VECTOR (DIMENSION NDIM) OF DAHI 1550
C ARGUMENT VALUES OF THE TABLE (NOT DESTROYED). DAHI 1560
C VAL - DOUBLE PRECISION INPUT VECTOR (DIMENSION 2*NDIM) OF DAHI 1570
C FUNCTION AND DERIVATIVE VALUES OF THE TABLE (DESTROYED). DAHI 1580
C FUNCTION AND DERIVATIVE VALUES MUST BE STORED IN DAHI 1590
C STORED IN PAIRS, THAT MEANS BEGINNING WITH FUNCTION VALUE AT DAHI 1600
C VAL(J) AT POINT ARG(I) EVERY FUNCTION VALUE MUST BE FOLLOWED DAHI 1610
C BY THE VALUE OF DERIVATIVE AT THE SAME POINT. DAHI 1620
C Y - RESULTING INTERPOLATED DOUBLE PRECISION FUNCTION DAHI 1630
C VALUE. DAHI 1640
C NDIM - AN INPUT VALUE WHICH SPECIFIES THE NUMBER OF DAHI 1650
C POINTS IN TABLE (ARG,VAL). DAHI 1660
C EPS - SINGLE PRECISION INPUT CONSTANT WHICH IS USED AS DAHI 1670
C UPPER BOUND FOR THE ABSOLUTE ERROR. DAHI 1680
C IER - A RESULTING ERROR PARAMETER. DAHI 1690
C DAHI 1700
C REMARKS AHI 1710
C (1) TABLE (ARG,VAL) SHOULD REPRESENT A SINGLE-VALUED DAHI 1720
C FUNCTION AND SHOULD BE STORED IN SUCH A WAY, THAT THE DAHI 1730
C DISTANCES ABS(ARG(I)-X) INCREASE WITH INCREASING DAHI 1740
C SUBSCRIPT I. TO GENERATE THIS ORDER IN TABLE (ARG,VAL), DAHI 1750
C SUBROUTINES ATSG, ATSM OR ATSE COULD BE USED IN A DAHI 1760
C PREVIOUS STAGE. DAHI 1770
C (2) NO ACTION BESIDES ERROR MESSAGE IN CASE NDIM LESS DAHI 1780
C THAN 1. DAHI 1790
C (3) INTERPOLATION IS TERMINATED EITHER IF THE DIFFERENCE DAHI 1800
C BETWEEN TWO SUCCESSIVE INTERPOLATED VALUES IS DAHI 1810
C ABSOLUTELY LESS THAN TOLERANCE EPS, OR IF THE ABSOLUTE DAHI 1820
C VALUE OF THIS DIFFERENCE STOPS DIMINISHING, OR AFTER DAHI 1830
C (2*NDIM-2) STEPS. FURTHER IT IS TERMINATED IF THE DAHI 1840
C PROCEDURE DISCOVERS TWO ARGUMENT VALUES IN VECTOR ARG DAHI 1850
C WHICH ARE IDENTICAL, DEPENDENT ON THESE FOUR CASES, DAHI 1860
C ERROR PARAMETER IER IS CODED IN THE FOLLOWING FORM DAHI 1870
C IER=0 - IT WAS POSSIBLE TO REACH THE REQUIRED DAHI 1880
C ACCURACY (NO ERROR). DAHI 1890
C IER=1 - IT WAS IMPOSSIBLE TO REACH THE REQUIRED DAHI 1900
C ACCURACY BECAUSE OF ROUNDING ERRORS. DAHI 1910
C IER=2 - IT WAS IMPOSSIBLE TO CHECK ACCURACY BECAUSE DAHI 1920
C NDIM IS LESS THAN 2, OR THE REQUIRED ACCURACY DAHI 1930
C COULD NOT BE REACHED BY MEANS OF THE GIVEN DAHI 1940
C TABLE. NDIM SHOULD BE INCREASED. DAHI 1950
C IER=3 - THE PROCEDURE DISCOVERED TWO ARGUMENT VALUES DAHI 1960
C IN VECTOR ARG WHICH ARE IDENTICAL. DAHI 1970
C DAHI 1980
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED AHI 1990
C NONE AHI 2000
C AHI 2010
C METHOD AHI 2020
C INTERPOLATION IS DONE BY MEANS OF AITKEN'S SCHEME OF AHI 2030
C HERMITE INTERPOLATION. ON RETURN Y CONTAINS AN INTERPOLATED AHI 2040
C FUNCTION VALUE AT POINT X, WHICH IS IN THE SENSE OF REMARK AHI 2050
C (3) OPTIMAL WITH RESPECT TO GIVEN TABLE. FOR REFERENCE, SEE AHI 2060
C F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS, AHI 2070
C MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.314-317, AND AHI 2080
C GERSHINSKY/LEVINE, AITKEN-HERMITE INTERPOLATION, AHI 2090
C JACM, VOL.11, ISS.3 (1964), PP.352-356. AHI 2100
C AHI 2110
C AHI 2120
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED AHI 2130
C NONE AHI 2140
C AHI 2150

```

Figure 19. Aitken's scheme for Hermite interpolation

Finally, Y is set equal to VAL(1) in case of monotonically decreasing absolute differences, or to VAL(1) of the step before if these differences start oscillating.

For reference see:

- (1) F. B. Hildebrand, Introduction to Numerical Analysis, McGraw Hill, New York/Toronto, London, 1956, pp. 49-50, 352-356.
- (2) Gershinsky/Levine, "Aitken-Hermite Interpolation", JACM, vol. 11, iss. 3 (1964), pp. 352-356.

.....	AHI 10
.....	AHI 20
.....	AHI 30
SUBROUTINE AHI	AHI 40
PURPOSE	AHI 50
TO INTERPOLATE FUNCTION VALUE Y FOR A GIVEN ARGUMENT VALUE	AHI 60
X USING A GIVEN TABLE (ARG,VAL) OF ARGUMENT, FUNCTION, AND	AHI 80
DERIVATIVE VALUES.	AHI 90
USAGE	AHI 100
CALL AHI (X,ARG,VAL,Y,NDIM,EPS,IER)	AHI 110
DESCRIPTION OF PARAMETERS	AHI 120
X - THE ARGUMENT VALUE SPECIFIED BY INPUT.	AHI 130
ARG - THE INPUT VECTOR (DIMENSION NDIM) OF ARGUMENT	AHI 140
VALUES OF THE TABLE (NOT DESTROYED).	AHI 150
VAL - THE INPUT VECTOR (DIMENSION 2*NDIM) OF FUNCTION	AHI 160
AND DERIVATIVE VALUES OF THE TABLE (DESTROYED).	AHI 170
FUNCTION AND DERIVATIVE VALUES MUST BE STORED IN	AHI 180
PAIRS, THAT MEANS BEGINNING WITH FUNCTION VALUE AT	AHI 190
POINT ARG(I) EVERY FUNCTION VALUE MUST BE FOLLOWED	AHI 200
BY THE VALUE OF DERIVATIVE AT THE SAME POINT.	AHI 210
Y - THE RESULTING INTERPOLATED FUNCTION VALUE.	AHI 220
NDIM - AN INPUT VALUE WHICH SPECIFIES THE NUMBER OF	AHI 230
POINTS IN TABLE (ARG,VAL).	AHI 240
EPS - AN INPUT CONSTANT WHICH IS USED AS UPPER BOUND	AHI 250
FOR THE ABSOLUTE ERROR.	AHI 260
IER - A RESULTING ERROR PARAMETER.	AHI 270
REMARKS	AHI 280
(1) TABLE (ARG,VAL) SHOULD REPRESENT A SINGLE-VALUED	AHI 290
FUNCTION AND SHOULD BE STORED IN SUCH A WAY, THAT THE	AHI 300
DISTANCES ABS(ARG(I)-X) INCREASE WITH INCREASING	AHI 310
SUBSCRIPT I. TO GENERATE THIS ORDER IN TABLE (ARG,VAL),	AHI 320
SUBROUTINES ATSG, ATSM OR ATSE COULD BE USED IN A	AHI 330
PREVIOUS STAGE.	AHI 340
(2) NO ACTION BESIDES ERROR MESSAGE IN CASE NDIM LESS	AHI 350
THAN 1.	AHI 360
(3) INTERPOLATION IS TERMINATED EITHER IF THE DIFFERENCE	AHI 370
BETWEEN TWO SUCCESSIVE INTERPOLATED VALUES IS	AHI 380
ABSOLUTELY LESS THAN TOLERANCE EPS, OR IF THE ABSOLUTE	AHI 390
VALUE OF THIS DIFFERENCE STOPS DIMINISHING, OR AFTER	AHI 400
(2*NDIM-2) STEPS. FURTHER IT IS TERMINATED IF THE	AHI 410
PROCEDURE DISCOVERS TWO ARGUMENT VALUES IN VECTOR ARG	AHI 420
WHICH ARE IDENTICAL, DEPENDENT ON THESE FOUR CASES,	AHI 430
ERROR PARAMETER IER IS CODED IN THE FOLLOWING FORM	AHI 440
IER=0 - IT WAS POSSIBLE TO REACH THE REQUIRED	AHI 450
ACCURACY (NO ERROR).	AHI 460
IER=1 - IT WAS IMPOSSIBLE TO REACH THE REQUIRED	AHI 470
ACCURACY BECAUSE OF ROUNDING ERRORS.	AHI 480
IER=2 - IT WAS IMPOSSIBLE TO CHECK ACCURACY BECAUSE	AHI 490
NDIM IS LESS THAN 2, OR THE REQUIRED ACCURACY	AHI 500
COULD NOT BE REACHED BY MEANS OF THE GIVEN	AHI 510
TABLE. NDIM SHOULD BE INCREASED.	AHI 520
IER=3 - THE PROCEDURE DISCOVERED TWO ARGUMENT VALUES	AHI 530
IN VECTOR ARG WHICH ARE IDENTICAL.	AHI 540
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	AHI 550
NONE	AHI 560
METHOD	AHI 570
INTERPOLATION IS DONE BY MEANS OF AITKEN'S SCHEME OF	AHI 580
HERMITE INTERPOLATION. ON RETURN Y CONTAINS AN INTERPOLATED	AHI 590
FUNCTION VALUE AT POINT X, WHICH IS IN THE SENSE OF REMARK	AHI 600
(3) OPTIMAL WITH RESPECT TO GIVEN TABLE. FOR REFERENCE, SEE	AHI 610
F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS,	AHI 620
MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.314-317, AND	AHI 630
GERSHINSKY/LEVINE, AITKEN-HERMITE INTERPOLATION,	AHI 640
JACM, VOL.11, ISS.3 (1964), PP.352-356.	AHI 650
.....	AHI 700
.....	AHI 710
.....	AHI 720


```

C
C
C          METHOD
C          INTERPOLATION IS DONE BY MEANS OF AITKENS SCHEME OF
C          HERMITE INTERPOLATION. ON RETURN Y CONTAINS AN INTERPOLATED
C          FUNCTION VALUE AT POINT X, WHICH IS IN THE SENSE OF REMARK
C          (3) OPTIMAL WITH RESPECT TO GIVEN TABLE. FOR REFERENCE, SEE
C          F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS,
C          MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.314-317, AND
C          GERSHINSKY/LEVINE, AITKEN-HERMITE INTERPOLATION,
C          JACM, VOL.11, ISS.3 (1964), PP.352-356.
C
C          .....
C          SUBROUTINE DAHI(X,ARG,VAL,Y,NDIM,EPS,IER)
C
C          DIMENSION ARG(1),VAL(1)
C          DOUBLE PRECISION ARG,VAL,X,Y,H,HI,H2
C          IER=2
C          H2=X-ARG(1)
C          IF(NDIM=1,2,1,3
C          1 Y=VAL(1)+VAL(2)*H2
C          2 RETURN
C
C          VECTOR ARG HAS MORE THAN 1 ELEMENT.
C          THE FIRST STEP PREPARES VECTOR VAL SUCH THAT AITKEN SCHEME CAN BE
C          USED.
C          3 I=1
C          DO 5 J=2,NDIM
C          HI=H2
C          H2=X-ARG(J)
C          Y=VAL(I)
C          VAL(I)=Y+VAL(I+1)*HI
C          H=HI-H2
C          IF(H14,13,4
C          4 VAL(I+1)=Y+(VAL(I+2)-Y)*HI/H
C          5 I=I+2
C          VAL(I)=VAL(I)+VAL(I+1)*H2
C          END OF FIRST STEP
C
C          PREPARE AITKEN SCHEME
C          DELT2=0.
C          IEND=I-1
C
C          START AITKEN-LOOP
C          DO 9 I=1,IEND
C          DELT1=DELT2
C          Y=VAL(I)
C          H=(I+3)/2
C          HI=ARG(H)
C          DO 6 J=I,1
C          K=I+1-J
C          L=(K+1)/2
C          H=ARG(L)-HI
C          IF(H16,14,6
C          6 VAL(K)=(VAL(K)*(X-HI)-VAL(K+1)*(X-ARG(L)))/H
C          DELT2=DABS(Y-VAL(I))
C          IF(DELT2-EPS11,11,7
C          7 IF(I=819,8,8
C          8 IF(DELT2-DELT1)9,12,12
C          9 CONTINUE
C          END OF AITKEN-LOOP
C
C          10 Y=VAL(I)
C          RETURN
C
C          THERE IS SUFFICIENT ACCURACY WITHIN 2*NDIM-2 ITERATION STEPS
C          11 IER=0
C          GOTO 10
C
C          TEST VALUE DELT2 STARTS OSCILLATING
C          12 IER=1
C          RETURN
C
C          THERE ARE TWO IDENTICAL ARGUMENT VALUES IN VECTOR ARG
C          13 Y=VAL(1)
C          14 IER=3
C          RETURN
C          END

```

```

DAHI 620
DAHI 630
DAHI 640
DAHI 650
DAHI 660
DAHI 670
DAHI 680
DAHI 690
DAHI 700
DAHI 710
DAHI 720
DAHI 730
DAHI 740
DAHI 750
DAHI 760
DAHI 770
DAHI 780
DAHI 790
DAHI 800
DAHI 810
DAHI 820
DAHI 830
DAHI 840
DAHI 850
DAHI 860
DAHI 870
DAHI 880
DAHI 890
DAHI 900
DAHI 910
DAHI 920
DAHI 930
DAHI 940
DAHI 950
DAHI 960
DAHI 970
DAHI 980
DAHI 990
DAHI1000
DAHI1010
DAHI1020
DAHI1030
DAHI1040
DAHI1050
DAHI1060
DAHI1070
DAHI1080
DAHI1090
DAHI1100
DAHI1110
DAHI1120
DAHI1130
DAHI1140
DAHI1150
DAHI1160
DAHI1170
DAHI1180
DAHI1190
DAHI1200
DAHI1210
DAHI1220
DAHI1230
DAHI1240
DAHI1250
DAHI1260
DAHI1270
DAHI1280
DAHI1290
DAHI1300
DAHI1310
DAHI1320
DAHI1330
DAHI1340
DAHI1350
DAHI1360
DAHI1370
DAHI1380
DAHI1390
DAHI1400

```

Subroutines ACFI and DACFI

These subroutines perform a continued fraction interpolation. Given the table x_i, y_i ($i = 1, 2, \dots, n$) of argument and function values, stored in the two one-dimensional storage arrays ARG and VAL, the problem is to interpolate function value Y at the given point X. It is assumed that the table represents a single-valued function $y = y(x)$ which is suitable for approximation by a rational function⁺, and that $|x_i - X| \geq x_j - X$ for $i > j$.⁺⁺

Then, using the following formulas:

$$y_{1,2} = \frac{x_2 - x_1}{y_2 - y_1};$$

$$y_{1,3} = \frac{x_3 - x_1}{y_3 - y_1}; \quad y_{1,2,3} = \frac{x_3 - x_2}{y_{1,3} - y_{1,2}};$$

$$y_{1,4} = \frac{x_4 - x_1}{y_4 - y_1}; \quad y_{1,2,4} = \frac{x_4 - x_2}{y_{1,4} - y_{1,2}};$$

$$y_{1,2,3,4} = \frac{x_4 - x_3}{y_{1,2,4} - y_{1,2,3}};$$

the triangular scheme of inverted differences shown in Figure 20 can be generated by row for the given table x_i, y_i .

All result values of row i can be stored in VAL(I). Thus, it is possible to generate the downward diagonal of the inverted differences scheme in storage array VAL, using the machine-processable formula:

$$\text{VAL}(I) = \frac{\text{ARG}(I) - \text{ARG}(J)}{\text{VAL}(I) - \text{VAL}(J)} \quad (J = 1, 2, \dots, I-1) \quad (1)$$

for $I = 2, 3, \dots, \text{NDIM}$.

⁺This order in table x_i, y_i ($i = 1, 2, \dots, n$) could be generated by subroutines ATSG, ATSM, ATSE, DATSG, DATSM, DATSE.

⁺⁺This means $y(x)$ should be closely approximated by a rational function, with numerator and denominator of low degree, which has the table points with arguments next to x as nodes.

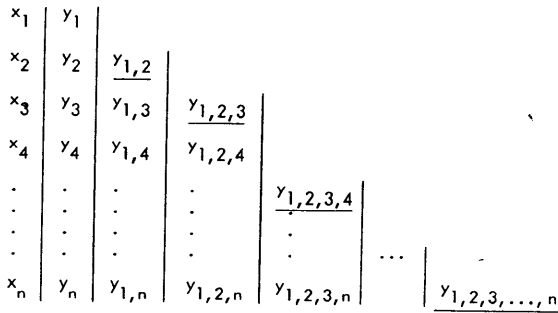


Figure 20. Triangular scheme for fraction interpolation

If for $J = I-1$, $VAL(I)$ is equal to the infinity element, table point $ARG(I)$, $VAL(I)$ (that is, x_i, y_i) gets interchanged with a table point ahead.

Now, after computation of each new component $VAL(I)$, continued fraction interpolation generates the following set of parameters:

$$P_3 = VAL(I) * P_2 + (X - ARG(I-1)) * P_1 \quad (2)$$

$$Q_3 = VAL(I) * Q_2 + (X - ARG(I-1)) * Q_1 \quad (3)$$

and

$$Y = P_3/Q_3 \quad (4)$$

starting with $P_1 = 1, P_2 = VAL(1), Q_1 = 0, Q_2 = 1$. After having done this, it sets $P_1 = P_2, P_2 = P_3, Q_1 = Q_2, Q_2 = Q_3$ after each step.

The procedure stops under the following conditions: if the difference between two successive values of Y is absolutely less than a given tolerance ϵ , or if the absolute value of this difference starts oscillating (test of oscillating differences starts at step $I = 8$, or for double-precision, $I = 10$), or if I has become $NDIM$, or if the procedure discovers two table points with identical argument values.

For reference see F. B. Hildebrand, Introduction to Numerical Analysis, McGraw-Hill, New York/Toronto/London, 1956, pp. 395-406.

```

C ..... ACFI 13
C ..... ACFI 20
C ..... ACFI 30
C ..... ACFI 43
C ..... ACFI 53
C ..... ACFI 60
C ..... ACFI 70
C ..... ACFI 80
C ..... ACFI 90
C ..... ACFI 100
C ..... ACFI 110
C ..... ACFI 120
C ..... ACFI 130
C ..... ACFI 140
C ..... ACFI 150
C ..... ACFI 160
C ..... ACFI 170
C ..... ACFI 180
C ..... ACFI 190
C ..... ACFI 200
C ..... ACFI 210
C ..... ACFI 220
C ..... ACFI 230
C ..... ACFI 240
C ..... ACFI 250
C ..... ACFI 260
SUBROUTINE ACFI
PURPOSE
TO INTERPOLATE FUNCTION VALUE Y FOR A GIVEN ARGUMENT VALUE
X USING A GIVEN TABLE (ARG,VAL) OF ARGUMENT AND FUNCTION
VALUES.
USAGE
CALL ACFI (X,ARG,VAL,Y,NDIM,EPS,IER)
DESCRIPTION OF PARAMETERS
X - THE ARGUMENT VALUE SPECIFIED BY INPUT.
ARG - THE INPUT VECTOR (DIMENSION NDIM) OF ARGUMENT
VALUES OF THE TABLE (POSSIBLY DESTROYED).
VAL - THE INPUT VECTOR (DIMENSION NDIM) OF FUNCTION
VALUES OF THE TABLE (DESTROYED).
Y - THE RESULTING INTERPOLATED FUNCTION VALUE.
NDIM - AN INPUT VALUE WHICH SPECIFIES THE NUMBER OF
POINTS IN TABLE (ARG,VAL).
EPS - AN INPUT CONSTANT WHICH IS USED AS UPPER BOUND
FOR THE ABSOLUTE ERROR.
IER - A RESULTING ERROR PARAMETER.

```

```

C ..... ACFI 270
C ..... ACFI 280
C ..... ACFI 290
C ..... ACFI 300
C ..... ACFI 310
C ..... ACFI 320
C ..... ACFI 330
C ..... ACFI 340
C ..... ACFI 350
C ..... ACFI 360
C ..... ACFI 370
C ..... ACFI 380
C ..... ACFI 390
C ..... ACFI 400
C ..... ACFI 410
C ..... ACFI 420
C ..... ACFI 430
C ..... ACFI 440
C ..... ACFI 450
C ..... ACFI 460
C ..... ACFI 470
C ..... ACFI 480
C ..... ACFI 490
C ..... ACFI 500
C ..... ACFI 510
C ..... ACFI 520
C ..... ACFI 530
C ..... ACFI 540
C ..... ACFI 550
C ..... ACFI 560
C ..... ACFI 570
C ..... ACFI 580
C ..... ACFI 590
C ..... ACFI 600
C ..... ACFI 610
C ..... ACFI 620
C ..... ACFI 630
C ..... ACFI 640
C ..... ACFI 650
C ..... ACFI 660
C ..... ACFI 670
C ..... ACFI 680
C ..... ACFI 690
C ..... ACFI 700
C ..... ACFI 710
C ..... ACFI 720
C ..... ACFI 730
C ..... ACFI 740
C ..... ACFI 750
C ..... ACFI 760
C ..... ACFI 770
C ..... ACFI 780
C ..... ACFI 790
C ..... ACFI 800
C ..... ACFI 810
C ..... ACFI 820
C ..... ACFI 830
C ..... ACFI 840
C ..... ACFI 850
C ..... ACFI 860
C ..... ACFI 870
C ..... ACFI 880
C ..... ACFI 890
C ..... ACFI 900
C ..... ACFI 910
C ..... ACFI 920
C ..... ACFI 930
C ..... ACFI 940
C ..... ACFI 950
C ..... ACFI 960
C ..... ACFI 970
C ..... ACFI 980
C ..... ACFI 990
C ..... ACFI1000
C ..... ACFI1010
C ..... ACFI1020
C ..... ACFI1030
C ..... ACFI1040
C ..... ACFI1050
C ..... ACFI1060
C ..... ACFI1070
C ..... ACFI1080
C ..... ACFI1090
C ..... ACFI1100
C ..... ACFI1110
C ..... ACFI1120
C ..... ACFI1130
C ..... ACFI1140
C ..... ACFI1150
C ..... ACFI1160
C ..... ACFI1170
C ..... ACFI1180
C ..... ACFI1190
C ..... ACFI1200
C ..... ACFI1210
C ..... ACFI1220
C ..... ACFI1230
C ..... ACFI1240
C ..... ACFI1250
C ..... ACFI1260
C ..... ACFI1270
C ..... ACFI1280
C ..... ACFI1290
C ..... ACFI1300
C ..... ACFI1310
C ..... ACFI1320
C ..... ACFI1330
C ..... ACFI1340
C ..... ACFI1350
C ..... ACFI1360
C ..... ACFI1370
C ..... ACFI1380
C ..... ACFI1390
C ..... ACFI1400
C ..... ACFI1410
C ..... ACFI1420
C ..... ACFI1430
C ..... ACFI1440
C ..... ACFI1450
C ..... ACFI1460
C ..... ACFI1470
C ..... ACFI1480
C ..... ACFI1490
C ..... ACFI1500
C ..... ACFI1510
C ..... ACFI1520
C ..... ACFI1530
C ..... ACFI1540
C ..... ACFI1550
C ..... ACFI1560
C ..... ACFI1570
C ..... ACFI1580
REMARKS
(1) TABLE (ARG,VAL) SHOULD REPRESENT A SINGLE-VALUED
FUNCTION AND SHOULD BE STORED IN SUCH A WAY, THAT THE
DISTANCES ABS(ARG(I)-X) INCREASE WITH INCREASING
SUBSCRIPT I. TO GENERATE THIS ORDER IN TABLE (ARG,VAL),
SUBROUTINES ATSG, ATSM OR ATSE COULD BE USED IN A
PREVIOUS STAGE.
(2) NO ACTION BESIDES ERROR MESSAGE IN CASE NDIM LESS
THAN 1.
(3) INTERPOLATION IS TERMINATED EITHER IF THE DIFFERENCE
BETWEEN TWO SUCCESSIVE INTERPOLATED VALUES IS
ABSOLUTELY LESS THAN TOLERANCE EPS, OR IF THE ABSOLUTE
VALUE OF THIS DIFFERENCE STOPS DIMINISHING, OR AFTER
(NDIM-1) STEPS (THE NUMBER OF POSSIBLE STEPS IS
DIMINISHED IF AT ANY STAGE INFINITY ELEMENT APPEARS IN
THE DOWNWARD DIAGONAL OF INVERTED-DIFFERENCES SCHEME
AND IF IT IS IMPOSSIBLE TO ELIMINATE THIS INFINITY
ELEMENT BY INTERCHANGING OF TABLE POINTS).
FURTHER IT IS TERMINATED IF THE PROCEDURE DISCOVERS TWO
ARGUMENT VALUES IN VECTOR ARG WHICH ARE IDENTICAL.
DEPENDENT ON THESE FOUR CASES, ERROR PARAMETER IER IS
CODED IN THE FOLLOWING FORM
IER=0 - IT WAS POSSIBLE TO REACH THE REQUIRED
ACCURACY (NO ERROR).
IER=1 - IT WAS IMPOSSIBLE TO REACH THE REQUIRED
ACCURACY BECAUSE OF ROUNDING ERRORS.
IER=2 - IT WAS IMPOSSIBLE TO CHECK ACCURACY BECAUSE
NDIM IS LESS THAN 2, OR THE REQUIRED ACCURACY
COULD NOT BE REACHED BY MEANS OF THE GIVEN
TABLE. NDIM SHOULD BE INCREASED.
IER=3 - THE PROCEDURE DISCOVERED TWO ARGUMENT VALUES
IN VECTOR ARG WHICH ARE IDENTICAL.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
INTERPOLATION IS DONE BY CONTINUED FRACTIONS AND INVERTED-
DIFFERENCES SCHEME. ON RETURN Y CONTAINS AN INTERPOLATED
FUNCTION VALUE AT POINT X, WHICH IS IN THE SENSE OF REMARK
(3) OPTIMAL WITH RESPECT TO GIVEN TABLE. FOR REFERENCE, SEE
F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS,
MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.395-406.
.....
SUBROUTINE ACFI(X,ARG,VAL,Y,NDIM,EPS,IER)
DIMENSION ARG(1),VAL(1)
IER=2
IF(NDIM)20,20,1
Y=VAL(1)
DELT2=0.
IF(NDIM-1)20,20,2
PREPARATIONS FOR INTERPOLATION LOOP
2 P2=1.
P3=Y
Q2=0.
Q3=1.
START INTERPOLATION LOOP
DO 16 I=2,NDIM
I1=0
P1=P2
P2=P3
Q1=Q2
Q2=Q3
Z=Y
DELT1=DELT2
JEND=I-1
COMPUTATION OF INVERTED DIFFERENCES
3 AUX=VAL(I)
DO 10 J=1,JEND
H=VAL(I)-VAL(J)
IF(ABS(H)-1.E-6*ABS(VAL(I)))4,4,9
4 IF(ABS(I)-ARG(J))15,17,5
5 IF(I-J)END16,6,6
INTERCHANGE ROW I WITH ROW I+1
6 I1=I+1
I1=I+1
IF(I1-NDIM)7,7,19
7 VAL(I1)=VAL(I1)
VAL(I1)=AUX
AUX=ARG(I1)
ARG(I1)=ARG(I1)
ARG(I1)=AUX
GOTO 3
COMPUTATION OF VAL(I) IN CASE VAL(I)-VAL(J) AND J LESS THAN I-1
8 VAL(I)=1.E75
GOTO 10
COMPUTATION OF VAL(I) IN CASE VAL(I) NOT EQUAL TO VAL(J)
9 VAL(I)=(ARG(I)-ARG(J))/H
10 CONTINUE
INVERTED DIFFERENCES ARE COMPUTED
COMPUTATION OF NEW Y
P3=VAL(I)*P2+(X-ARG(I-1))*P1
Q3=VAL(I)*Q2+(X-ARG(I-1))*Q1
IF(Q3)11,12,11
11 Y=P3/Q3
GOTO 13
12 Y=1.E75
13 DELT2=ABS(Z-Y)
IF(DELT2-EPS)19,19,14
14 IF(I-8)16,15,15
15 IF(DELT2-DELT1)16,18,18
16 CONTINUE
END OF INTERPOLATION LOOP
RETURN
THERE ARE TWO IDENTICAL ARGUMENT VALUES IN VECTOR ARG
17 IER=3
RETURN
TEST VALUE DELT2 STARTS OSCILLATING
18 Y=Z
IER=1
RETURN
THERE IS SATISFACTORY ACCURACY WITHIN NDIM-1 STEPS
19 IER=0
20 RETURN
END

```


Subroutines ATSG and DATSG

These subroutines perform a table selection out of a given general table.

Given a search argument x and a general table z_i, f_i ($i = 1, 2, \dots, \text{irow}$) stored in two vectors Z and F (in case $\text{icol} = 1$), or z_i, f_i, f'_i ($i = 1, 2, \dots, \text{irow}$) stored in vector Z and the two columns of matrix F (in case $\text{icol} = 2$); the problem is to select those n ($\leq \text{irow}$) points z_{i_j}, f_{i_j} or $z_{i_j}, f_{i_j}, f'_{i_j}$ ($j = 1, 2, \dots, n$), respectively, which are next to x and to store their coordinates in two vectors ARG and VAL so that the distances $|x - z_{i_j}|$ increase

with increasing subscript j . This problem may arise when using interpolation subroutines ALI, AHI, ACFI, DALL, DAHI, DACFI. The table for the case $\text{icol} = 1$ is shown in Figure 21, and that for case $\text{icol} = 2$ in Figure 22.

Selection is done in two parts. In the first part, auxiliary vector WORK with components $z_i - x$ ($i = 1, 2, \dots, \text{irow}$) is generated and its greatest component, $\max_i |z_i - x|$, is stored in an auxiliary storage location. In each of the n steps of the second part the subscript i_j of the smallest component of vector WORK is searched for. Afterwards this component is replaced by a number greater than

$\max_i |z_i - x|$. Then, z_{i_j} goes into the storage location $\text{ARG}(j)$ and:

In case $\text{icol} = 1$ -- f_{i_j} into the storage location $\text{VAL}(j)$

f_{i_j} into the storage location $\text{VAL}(2 * j - 1)$ and

In case $\text{icol} = 2$ -- f'_{i_j} into the storage location $\text{VAL}(2 * j)$

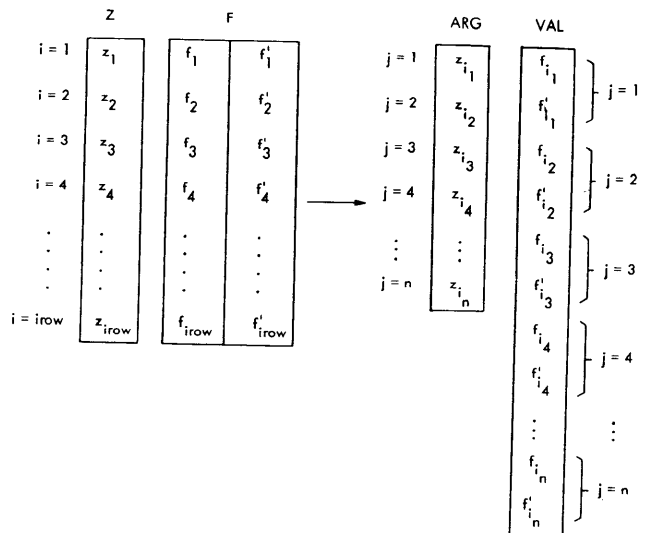


Figure 22. Table selection in case $\text{icol}=2$

If (by an error of the user) the dimension n of the table to be selected is greater than the dimension irow of the given table, the procedure selects only a maximum table of irow points. In order to avoid errors in further work with table (ARG, VAL) , the user ought to check the correspondence between the selected table and its dimension by comparison of n and irow . This test may be done before or after calling subroutine ATSG or DATSG .

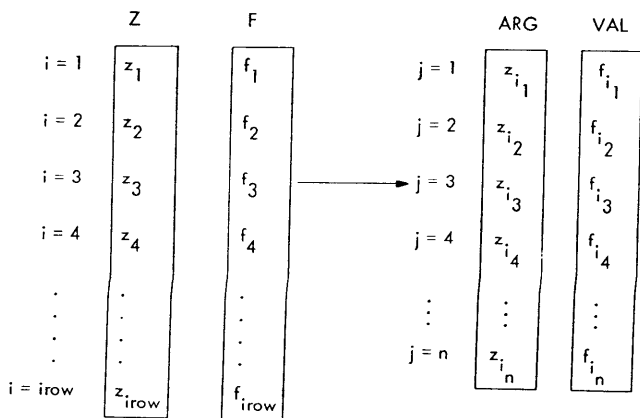


Figure 21. Table selection in case $\text{icol}=1$

```

C ..... ATSG 10
C ..... ATSG 20
C ..... ATSG 30
C ..... ATSG 40
C ..... ATSG 50
C ..... ATSG 60
C ..... ATSG 70
C ..... ATSG 80
C ..... ATSG 90
C ..... ATSG 100
C ..... ATSG 110
C ..... ATSG 120
C ..... ATSG 130
C ..... ATSG 140
C ..... ATSG 150
C ..... ATSG 160
C ..... ATSG 170
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C ..... ATSG 200
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C ..... ATSG 340
C ..... ATSG 350
C ..... ATSG 360
C ..... ATSG 370
C ..... ATSG 380
C ..... ATSG 390
C ..... ATSG 400
C ..... ATSG 410
C ..... ATSG 420
C ..... ATSG 430
C ..... ATSG 440
C ..... ATSG 450
C ..... ATSG 460
C ..... ATSG 470
C ..... ATSG 480
C ..... ATSG 490
C ..... ATSG 500
C ..... ATSG 510
C ..... ATSG 520
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C ..... ATSG 570
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C ..... ATSG 600
C ..... ATSG 610
C ..... ATSG 620
C ..... ATSG 630
C ..... ATSG 640
C ..... ATSG 650
C ..... ATSG 660
C ..... ATSG 670
C ..... ATSG 680
C ..... ATSG 690
C ..... ATSG 700
C ..... ATSG 710
C ..... ATSG 720
C ..... ATSG 730
C ..... ATSG 740
C ..... ATSG 750
C ..... ATSG 760
C ..... ATSG 770
C ..... ATSG 780
C ..... ATSG 790
C ..... ATSG 800
C ..... ATSG 810
C ..... ATSG 820
C ..... ATSG 830
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C ..... ATSG 850
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C ..... ATSG 890
C ..... ATSG 900
C ..... ATSG 910
C ..... ATSG 920
C ..... ATSG 930
C ..... ATSG 940
C ..... ATSG 950
C ..... ATSG 960
C ..... ATSG 970
C ..... ATSG 980
C ..... ATSG 990
C ..... ATSG 1000

```

```

C ..... ATSG 580
C ..... ATSG 590
C ..... ATSG 600
SUBROUTINE DATSG(X,Z,F,WORK,IROW,ICOL,ARG,VAL,NDIM) ATSG 610
C ..... ATSG 620
C ..... ATSG 630
C ..... ATSG 640
C ..... ATSG 650
C ..... ATSG 660
C ..... ATSG 670
C ..... ATSG 680
C ..... ATSG 690
C ..... ATSG 700
C ..... ATSG 710
C ..... ATSG 720
C ..... ATSG 730
C ..... ATSG 740
C ..... ATSG 750
C ..... ATSG 760
C ..... ATSG 770
C ..... ATSG 780
C ..... ATSG 790
C ..... ATSG 800
C ..... ATSG 810
C ..... ATSG 820
C ..... ATSG 830
C ..... ATSG 840
C ..... ATSG 850
C ..... ATSG 860
C ..... ATSG 870
C ..... ATSG 880
C ..... ATSG 890
C ..... ATSG 900
C ..... ATSG 910
C ..... ATSG 920
C ..... ATSG 930
C ..... ATSG 940
C ..... ATSG 950
C ..... ATSG 960
C ..... ATSG 970
END

```

```

C ..... DTSG 13
C ..... DTSG 20
C ..... DTSG 30
SUBROUTINE DATSG DTSG 40
C ..... DTSG 50
C ..... DTSG 60
C ..... DTSG 70
C ..... DTSG 80
C ..... DTSG 90
C ..... DTSG 100
C ..... DTSG 110
C ..... DTSG 120
C ..... DTSG 130
C ..... DTSG 140
C ..... DTSG 150
C ..... DTSG 160
C ..... DTSG 170
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C ..... DTSG 920
C ..... DTSG 930
C ..... DTSG 940
C ..... DTSG 950
C ..... DTSG 960
C ..... DTSG 970
C ..... DTSG 980
C ..... DTSG 990

```

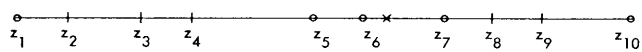
Subroutines ATSM and DATSM

These subroutines perform a table selection out of a given monotonic table. They have the same function as subroutines ATSG and DATSG with the difference that the given table is stored with monotonically increasing or decreasing arguments z_i .

Selection is done in two parts. In the first part, argument z_i next to search argument x is searched for by "binary search". This procedure (in case $irow = 10$) is shown in Figure 23.

The second part starts at z_{i_1} . At each of the n steps, the procedure decides by comparison of distances if the next step has to go to the right or to the left. Care must be taken that none of the selected subscripts i_j becomes greater than $irow$ or less than one. Thus, in case $n = 5$, the sequence of argument values becomes $z_{i_1} = z_6$, $z_{i_2} = z_7$, $z_{i_3} = z_5$, $z_{i_4} = z_8$, $z_{i_5} = z_9$. The selected table is stored in the same way as in subroutine ATSG or DATSG.

If (by an error of the user) the dimension n of the table to be selected is greater than the dimension $irow$ of the given table, the procedure selects only a maximum table of $irow$ points. In order to avoid errors in further work with table (ARG, VAL), the user ought to check the correspondence between the selected table and its dimension by comparison of n and $irow$. This test may be done before or after calling subroutine ATSM or DATSM.



- (1) x lies between z_1 and z_{10} .
- (2) x lies between z_5 and z_{10} .
- (3) x lies between z_5 and z_7 .
- (4) x lies between z_6 and z_7 .
- (5) Comparison of the two distances $|z_6 - x|$ and $|z_7 - x|$ shows that z_6 is next to x .

Figure 23. Binary search for argument z_i ($irow=10$)

```

C .....
C ..... ATSM 13
C ..... ATSM 20
C ..... SUBROUTINE ATSM ATSM 30
C ..... ATSM 40
C ..... ATSM 50
C ..... PURPOSE ATSM 60
C ..... NDIM POINTS OF A GIVEN TABLE WITH MONOTONIC ARGUMENTS ARE ATSM 70
C ..... SELECTED AND ORDERED SUCH THAT ATSM 80
C ..... ABS(ARG(I)-X).GE.ABS(ARG(J)-X) IF I.GT.J. ATSM 90
C ..... USAGE ATSM 100
C ..... CALL ATSM (X,Z,F,IROW,ICOL,ARG,VAL,NDIM) ATSM 110
C ..... ATSM 120
C ..... ATSM 130
C ..... DESCRIPTION OF PARAMETERS ATSM 140
C ..... X - THE SEARCH ARGUMENT. ATSM 150
C ..... Z - THE VECTOR OF ARGUMENT VALUES (DIMENSION IROW). ATSM 160
C ..... THE ARGUMENT VALUES MUST BE STORED IN INCREASING ATSM 170
C ..... OR DECREASING SEQUENCE. ATSM 180
C ..... F - IN CASE ICOL=1, F IS THE VECTOR OF FUNCTION VALUES ATSM 190
C ..... (DIMENSION IROW). ATSM 200
C ..... IN CASE ICOL=2, F IS AN IROW BY 2 MATRIX. THE FIRST ATSM 210
C ..... COLUMN SPECIFIES THE VECTOR OF FUNCTION VALUES AND ATSM 220
C ..... THE SECOND THE VECTOR OF DERIVATIVES. ATSM 230
C ..... IROW - THE DIMENSION OF VECTOR Z AND OF EACH COLUMN ATSM 240
C ..... IN MATRIX F. ATSM 250
C ..... ICOL - THE NUMBER OF COLUMNS IN F (I.E. 1 OR 2). ATSM 260
C ..... ARG - THE RESULTING VECTOR OF SELECTED AND ORDERED ATSM 270
C ..... ARGUMENT VALUES (DIMENSION NDIM). ATSM 280
C ..... VAL - THE RESULTING VECTOR OF SELECTED FUNCTION VALUES ATSM 290
C ..... (DIMENSION NDIM) IN CASE ICOL=1. IN CASE ICOL=2, ATSM 300
C ..... VAL IS THE VECTOR OF FUNCTION AND DERIVATIVE VALUES ATSM 310
C ..... (DIMENSION 2*NDIM) WHICH ARE STORED IN PAIRS (I.E. ATSM 320
C ..... EACH FUNCTION VALUE IS FOLLOWED BY ITS DERIVATIVE ATSM 330
C ..... VALUE). ATSM 340
C ..... NDIM - THE NUMBER OF POINTS WHICH MUST BE SELECTED OUT OF ATSM 350
C ..... THE GIVEN TABLE (Z,F). ATSM 360
C ..... ATSM 370
C ..... ATSM 380
C ..... REMARKS ATSM 390
C ..... NO ACTION IN CASE IROW LESS THAN 1. ATSM 400
C ..... IF INPUT VALUE NDIM IS GREATER THAN IROW, THE PROGRAM ATSM 410
C ..... SELECTS ONLY A MAXIMUM TABLE OF IROW POINTS. THEREFORE THE ATSM 420
C ..... AND ITS DIMENSION BY COMPARISON OF NDIM AND IROW. IN ORDER ATSM 430
C ..... TO GET CORRECT RESULTS IN FURTHER WORK WITH TABLE (ARG,VAL). ATSM 440
C ..... THIS TEST MAY BE DONE BEFORE OR AFTER CALLING ATSM 450
C ..... SUBROUTINE ATSM. ATSM 460
C ..... SUBROUTINE ATSM ESPECIALLY CAN BE USED FOR GENERATING THE ATSM 470
C ..... TABLE (ARG,VAL) NEEDED IN SUBROUTINES ALI, AHI, AND ACF1. ATSM 480
C ..... ATSM 490
C ..... SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED ATSM 500
C ..... NONE ATSM 510
C ..... ATSM 520
C ..... METHOD ATSM 530
C ..... SELECTION IS DONE BY SEARCHING THE SUBSCRIPT J OF THAT ATSM 540
C ..... ARGUMENT, WHICH IS NEXT TO X (BINARY SEARCH). ATSM 550
C ..... AFTERWARDS NEIGHBOURING ARGUMENT VALUES ARE TESTED AND ATSM 560
C ..... SELECTED IN THE ABOVE SENSE. ATSM 570
C ..... ATSM 580
C ..... ATSM 590
C ..... ATSM 600
C ..... SUBROUTINE ATSM(X,Z,F,IROW,ICOL,ARG,VAL,NDIM) ATSM 610
C ..... ATSM 620
C ..... ATSM 630
C ..... DIMENSION Z(1),F(1),ARG(1),VAL(1) ATSM 640
C ..... ATSM 650
C ..... CASE IROW=1 IS CHECKED OUT ATSM 660
C ..... IF(IROW-1)23,21,1 ATSM 670
C ..... 1 N=NDIM ATSM 680
C ..... ATSM 690
C ..... IF N IS GREATER THAN IROW, N IS SET EQUAL TO IROW. ATSM 700
C ..... IF(N-IROW)3,3,2 ATSM 710
C ..... 2 N=IROW ATSM 720
C ..... ATSM 730
C ..... CASE IROW.GE.2 ATSM 740
C ..... SEARCHING FOR SUBSCRIPT J SUCH THAT Z(J) IS NEXT TO X. ATSM 750
C ..... 3 IF(Z(IROW)-Z(1))5,4,4 ATSM 760
C ..... 4 J=IROW ATSM 770
C ..... I=1 ATSM 780
C ..... GOTO 6 ATSM 790
C ..... 5 I=IROW ATSM 800
C ..... J=1 ATSM 810
C ..... 6 K=(J+1)/2 ATSM 820
C ..... IF(X-Z(K))7,7,8 ATSM 830
C ..... 7 J=K ATSM 840
C ..... GOTO 9 ATSM 850
C ..... 8 I=K ATSM 860
C ..... 9 IF(ABS(J-I)-1)10,10,6 ATSM 870
C ..... 10 IF(ABS(Z(J)-X)-ABS(Z(I)-X))12,12,11 ATSM 880
C ..... 11 J=I ATSM 890
C ..... ATSM 900
C ..... TABLE SELECTION ATSM 910
C ..... 12 K=J ATSM 920
C ..... JL=0 ATSM 930
C ..... JR=0 ATSM 940
C ..... DO 20 I=1,N ATSM 950
C ..... ARG(I)=Z(K) ATSM 960
C ..... IF(ICOL-1)14,14,13 ATSM 970
C ..... 13 VAL(2*I-1)=F(K) ATSM 980
C ..... KK=K+IROW ATSM 990
C ..... VAL(2*I)=F(KK) ATSM1000
C ..... GOTO 15 ATSM1010
C ..... 14 VAL(I)=F(K) ATSM1020
C ..... 15 J=J+JR ATSM1030
C ..... IF(JJR-IROW)16,16,18 ATSM1040
C ..... 16 J=J-JL ATSM1050
C ..... 17 IF(J=1)19,19,17 ATSM1060
C ..... 18 IF(ABS(Z(JJR+1)-X)-ABS(Z(J-1)-X))19,19,18 ATSM1070
C ..... JL=JL+1 ATSM1080
C ..... K=J-JL ATSM1090
C ..... GOTO 20 ATSM1100
C ..... 19 JR=JR+1 ATSM1110
C ..... K=J+JR ATSM1120
C ..... 20 CONTINUE ATSM1130
C ..... RETURN ATSM1140
C ..... ATSM1150
C ..... CASE IROW=1 ATSM1160
C ..... 21 ARG(1)=Z(1) ATSM1170
C ..... VAL(1)=F(1) ATSM1180
C ..... IF(ICOL-2)23,22,23 ATSM1190
C ..... 22 VAL(2)=F(2) ATSM1200
C ..... 23 RETURN ATSM1210
C ..... END ATSM1220

```

```

C ..... DTSM 10
C SUBROUTINE DATSM DTSM 20
C DTSM 30
C DTSM 40
C DTSM 50
C DTSM 60
C DTSM 70
C DTSM 80
C DTSM 90
C DTSM 100
C DTSM 110
C DTSM 120
C DTSM 130
C DTSM 140
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C DTSM 990
C DTSML000
C DTSML010
C DTSML020
C DTSML030
C DTSML040
C DTSML050
C DTSML060
C DTSML070
C DTSML080
C DTSML090
C DTSML100
C DTSML110
C DTSML120
C DTSML130
C DTSML140
C DTSML150
C DTSML160
C DTSML170
C DTSML180
C DTSML190
C DTSML200
C DTSML210
C DTSML220
C DTSML230
C .....
SUBROUTINE DATSM
PURPOSE
NDIM POINTS OF A GIVEN TABLE WITH MONOTONIC ARGUMENTS ARE
SELECTED AND ORDERED SUCH THAT
ABS(ARG(I)-X).GE.ABS(ARG(J)-X) IF I.GT.J.
USAGE
CALL DATSM (X,Z,F,IROW,ICOL,ARG,VAL,NDIM)
DESCRIPTION OF PARAMETERS
X - DOUBLE PRECISION SEARCH ARGUMENT.
Z - DOUBLE PRECISION VECTOR OF ARGUMENT VALUES (DIMEN-
SION IROW). THE ARGUMENT VALUES MUST BE STORED IN
INCREASING OR DECREASING SEQUENCE.
F - IN CASE ICOL=1, F IS THE DOUBLE PRECISION VECTOR
OF FUNCTION VALUES (DIMENSION IROW).
IN CASE ICOL=2, F IS A DOUBLE PRECISION IROW BY 2
MATRIX. THE FIRST COLUMN SPECIFIES VECTOR OF FUNC-
TION VALUES AND THE SECOND VECTOR OF DERIVATIVES.
IROW - THE DIMENSION OF VECTOR Z AND OF EACH COLUMN
IN MATRIX F.
ICOL - THE NUMBER OF COLUMNS IN F (I.E. 1 OR 2).
ARG - RESULTING DOUBLE PRECISION VECTOR OF SELECTED AND
ORDERED ARGUMENT VALUES (DIMENSION NDIM).
VAL - RESULTING DOUBLE PRECISION VECTOR OF SELECTED
FUNCTION VALUES (DIMENSION NDIM) IN CASE ICOL=1.
IN CASE ICOL=2, VAL IS THE DOUBLE PRECISION VECTOR
OF FUNCTION AND DERIVATIVE VALUES (DIMENSION
2*NDIM) WHICH ARE STORED IN PAIRS (I.E. EACH FUNC-
TION VALUE IS FOLLOWED BY ITS DERIVATIVE VALUE).
NDIM - THE NUMBER OF POINTS WHICH MUST BE SELECTED OUT OF
THE GIVEN TABLE (Z,F).
REMARKS
NO ACTION IN CASE IROW LESS THAN 1.
IF INPUT VAL IS NDIM IS GREATER THAN IROW, THE PROGRAM
SELECTS ONLY A MAXIMUM TABLE OF IROW POINTS. THEREFORE THE
USER OUGHT TO CHECK CORRESPONDENCE BETWEEN TABLE (ARG,VAL)
AND ITS DIMENSION BY COMPARISON OF NDIM AND IROW, IN ORDER
TO GET CORRECT RESULTS IN FURTHER WORK WITH TABLE (ARG,VAL).
THIS TEST MAY BE DONE BEFORE OR AFTER CALLING
SUBROUTINE DATSM.
SUBROUTINE DATSM ESPECIALLY CAN BE USED FOR GENERATING THE
TABLE (ARG,VAL) NEEDED IN SUBROUTINES DALI, DAHI, AND DACFI.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
SELECTION IS DONE BY SEARCHING THE SUBSCRIPT J OF "HAT
ARGUMENT, WHICH IS NEXT TO X (BINARY SEARCH).
AFTERWARDS NEIGHBOURING ARGUMENT VALUES ARE TESTED AND
SELECTED IN THE ABOVE SENSE.
SUBROUTINE DATSM(X,Z,F,IROW,ICOL,ARG,VAL,NDIM)
DIMENSION Z(1),F(1),ARG(1),VAL(1)
DOUBLE PRECISION X,Z,F,ARG,VAL
CASE IROW=1 IS CHECKED OUT
IF(IROW-1)23,21,1
1 N=NDIM
IF N IS GREATER THAN IROW, N IS SET EQUAL TO IROW.
IF(N-IROW)3,3,2
2 N=IROW
CASE IROW.GE.2
SEARCHING FOR SUBSCRIPT J SUCH THAT Z(J) IS NEXT TO X.
3 IF(Z(IROW)-Z(1))5,4,4
4 J=IROW
I=1
GOTO 6
5 I=IROW
J=I
6 K=(J+1)/2
IF(X-Z(K))7,7,8
7 J=K
GOTO 9
8 I=K
9 IF(ABS(J-I)-1)10,10,6
10 IF(DABS(Z(J)-X)-DABS(Z(I)-X))12,12,11
11 J=I
TABLE SELECTION
12 K=J
JL=0
JR=0
DO 20 I=1,N
ARG(I)=Z(K)
IF(ICOL-1)14,14,13
13 VAL(2*I-1)=F(K)
KK=K+IROW
VAL(2*I)=F(KK)
GOTO 15
14 VAL(I)=F(K)
15 J=J+JR
IF(J=IROW)16,18,18
16 J=J-JL
IF(J=1)19,19,17
17 IF(DABS(Z(JR+1)-X)-DABS(Z(JL-1)-X))19,19,18
18 JL=JL+1
K=J-JL
GOTO 20
19 JR=JR+1
K=J+JR
20 CONTINUE
RETURN
CASE IROW=1
21 ARG(1)=Z(1)
VAL(1)=F(1)
IF(ICOL-1)23,22,23
22 VAL(2)=F(2)
23 RETURN
END

```

Subroutines ATSE and DATSE

These subroutines perform a table selection out of a given equidistant table. They have the same function as subroutines ATSG and DATSG with the difference that the given table is stored with equidistant arguments. Instead of vector Z of argument values, subroutines ATSE and DATSE need only the starting argument z_s and the increment of arguments dz .

Selection is done in two parts. In the first part, the subscript i_1 of the argument next to search argument x is computed, using the formula

$$i_1 = \left[\frac{x - z_s}{dz} + 1.5 \right]$$

where [a] means "integer part of a".

The second part starts at z_{i_1} and goes one step to the left (right), one to the right (left), and so on until all n arguments are selected. Care must be taken that none of the selected subscripts i_j becomes greater than $irow$ or less than one. In the example shown in Figure 24, the sequence (z_{i_j}) becomes

$$z_{i_1} = z_6, z_{i_2} = z_5, z_{i_3} = z_7, z_{i_4} = z_4, z_{i_5} = z_8, \\ z_{i_6} = z_3, z_{i_7} = z_2.$$

The selected table is stored in the same way as in subroutine ATSG or DATSG.

If, by a user error, the dimension n of the table to be selected is greater than the dimension $irow$ of the given table, the procedure selects only a maximum table of $irow$ points. In order to avoid errors in further work with table (ARG, VAL), the user ought to check the correspondence between the selected table and its dimension by comparison of n and $irow$. This test may be done before or after calling subroutine ATSE or DATSE.

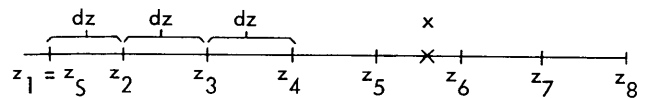


Figure 24. Generation of sequence (z_{i_j}) in case $irow=8, n=7$

```

C          ATSE 10
C          ATSE 20
C          SUBROUTINE ATSE          ATSE 30
C          ATSE 40
C          ATSE 50
C          ATSE 60
C          PURPOSE
C          NDIM POINTS OF A GIVEN TABLE WITH EQUIDISTANT ARGUMENTS ARE
C          SELECTED AND ORDERED SUCH THAT
C          ABS(ARG(I)-X).GE.ABS(ARG(J)-X) IF I.GT.J.          ATSE 70
C          ATSE 80
C          ATSE 90
C          ATSE 100
C          USAGE
C          CALL ATSE (X,ZS,DZ,F, IROW, ICOL, ARG, VAL, NDIM)
C          ATSE 110
C          ATSE 120
C          ATSE 130
C          DESCRIPTION OF PARAMETERS
C          X - THE SEARCH ARGUMENT.          ATSE 140
C          ZS - THE STARTING VALUE OF ARGUMENTS.          ATSE 150
C          DZ - THE INCREMENT OF ARGUMENTS.          ATSE 160
C          F - IN CASE ICOL=1, F IS THE VECTOR OF FUNCTION VALUES
C          (DIMENSION IROW).          ATSE 170
C          ATSE 180
C          IN CASE ICOL=2, F IS AN IROW BY 2 MATRIX. THE FIRSTATSE 190
C          COLJNM SPECIFIES THE VECTOR OF FUNCTION VALUES AND
C          THE SECOND THE VECTOR OF DERIVATIVES.          ATSE 200
C          ATSE 210
C          IROW - THE DIMENSION OF EACH COLUMN IN MATRIX F.          ATSE 220
C          ICOL - THE NUMBER OF COLUMNS IN F (I.E. 1 OR 2).          ATSE 230
C          ARG - THE RESULTING VECTOR OF SELECTED AND ORDERED
C          ARGUMENT VALUES (DIMENSION NDIM).          ATSE 240
C          VAL - THE RESULTING VECTOR OF SELECTED FUNCTION VALUES
C          (DIMENSION NDIM) IN CASE ICOL=1. IN CASE ICOL=2,
C          VAL IS THE VECTOR OF FUNCTION AND DERIVATIVE VALUES
C          (DIMENSION 2*NDIM) WHICH ARE STORED IN PAIRS (I.E. EACH
C          EACH FUNCTION VALUE IS FOLLOWED BY ITS DERIVATIVE
C          VALUE).          ATSE 250
C          ATSE 260
C          ATSE 270
C          ATSE 280
C          ATSE 290
C          ATSE 300
C          ATSE 310
C          ATSE 320
C          ATSE 330
C          NDIM - THE NUMBER OF POINTS WHICH MUST BE SELECTED OUT OF
C          THE GIVEN TABLE.          ATSE 340
C          ATSE 350
C          ATSE 360
C          REMARKS
C          NO ACTION IN CASE IROW LESS THAN 1.          ATSE 370
C          IF INPUT VALJE NDIM IS GREATER THAN IROW, THE PROGRAM
C          SELECTS ONLY A MAXIMUM TABLE OF IROW POINTS. THEREFORE THE
C          USER OUGHT TO CHECK CORRESPONDENCE BETWEEN TABLE (ARG,VAL)
C          AND ITS DIMENSION BY COMPARISON OF NDIM AND IROW, IN ORDER
C          TO GET CORRECT RESULTS IN FURTHER WORK WITH TABLE (ARG,VAL).
C          THIS TEST MAY BE DONE BEFORE OR AFTER CALLING
C          SUBROUTINE ATSE.          ATSE 430
C          SUBROUTINE ATSE ESPECIALLY CAN BE USED FOR GENERATING THE
C          TABLE (ARG,VAL) NEEDED IN SUBROUTINES ALI, AHI, AND ACFI.
C          ATSE 440
C          ATSE 450
C          ATSE 460
C          ATSE 470
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          NONE          ATSE 480
C          ATSE 490
C          ATSE 500
C          METHOD
C          SELECTION IS DONE BY COMPUTING THE SUBSCRIPT J OF THAT
C          ARGUMENT, WHICH IS NEXT TO X.
C          AFTERWARDS NEIGHBOURING ARGUMENT VALUES ARE TESTED AND
C          SELECTED IN THE ABOVE SENSE.          ATSE 510
C          ATSE 520
C          ATSE 530
C          ATSE 540
C          ATSE 550
C          ATSE 560
C          ATSE 570
C          SUBROUTINE ATSE(X,ZS,DZ,F, IROW, ICOL, ARG, VAL, NDIM)
C          ATSE 580
C          ATSE 590
C          ATSE 600
C          DIMENSION F(1),ARG(1),VAL(1)
C          IF(IROW-1)19,17,1
C          ATSE 610
C          ATSE 620
C          CASE DZ=0 IS CHECKED OUT
C          1 IF(DZ)2,17,2
C          2 N=NDIM
C          ATSE 630
C          ATSE 640
C          ATSE 650
C          IF N IS GREATER THAN IROW, N IS SET EQUAL TO IROW.
C          IF(N-IROW)4,4,3
C          3 N=IROW
C          ATSE 660
C          ATSE 670
C          ATSE 680
C          COMPUTATION OF STARTING SUBSCRIPT J.
C          4 J=(X-ZS)/DZ+1.5
C          IF(J)5,5,6
C          5 J=1
C          6 IF(J-IROW)8,8,7
C          7 J=IROW
C          ATSE 690
C          ATSE 700
C          ATSE 710
C          ATSE 720
C          ATSE 730
C          ATSE 740
C          ATSE 750
C          ATSE 760
C          ATSE 770
C          ATSE 780
C          ATSE 790
C          GENERATION OF TABLE ARG,VAL IN CASE DZ.NE.0.
C          8 II=J
C          JL=0
C          JR=0
C          DO 16 I=1,N
C          ARG(I)=ZS+FLOAT(II-1)*DZ
C          IF(ICOL-2)9,10,10
C          9 VAL(I)=F(II)
C          ATSE 800
C          ATSE 810
C          ATSE 820
C          ATSE 830
C          ATSE 840
C          ATSE 850
C          ATSE 860
C          ATSE 870
C          ATSE 880
C          ATSE 890
C          ATSE 900
C          ATSE 910
C          ATSE 920
C          ATSE 930
C          ATSE 940
C          ATSE 950
C          ATSE 960
C          ATSE 970
C          ATSE 980
C          ATSE 990
C          ATSE1000
C          ATSE1010
C          ATSE1020
C          ATSE1030
C          ATSE1040
C          ATSE1050
C          ATSE1060
C          ATSE1070
C          ATSE1080
C          ATSE1090
C          ATSE1090
C          END

```

```

C          DTSE 10
C          DTSE 20
C          SUBROUTINE DATSE          DTSE 30
C          DTSE 40
C          DTSE 50
C          DTSE 60
C          DTSE 70
C          DTSE 80
C          DTSE 90
C          DTSE 100
C          DTSE 110
C          DTSE 120
C          DTSE 130
C          DTSE 140
C          DTSE 150
C          DTSE 160
C          DTSE 170
C          DTSE 180
C          DTSE 190
C          DTSE 200
C          DTSE 210
C          DTSE 220
C          DTSE 230
C          DTSE 240
C          DTSE 250
C          DTSE 260
C          DTSE 270
C          DTSE 280
C          DTSE 290
C          DTSE 300
C          DTSE 310
C          DTSE 320
C          DTSE 330
C          DTSE 340
C          DTSE 350
C          DTSE 360
C          DTSE 370
C          DTSE 380
C          DTSE 390
C          DTSE 400
C          DTSE 410
C          DTSE 420
C          DTSE 430
C          DTSE 440
C          DTSE 450
C          DTSE 460
C          DTSE 470
C          DTSE 480
C          DTSE 490
C          DTSE 500
C          DTSE 510
C          DTSE 520
C          DTSE 530
C          DTSE 540
C          DTSE 550
C          DTSE 560
C          DTSE 570
C          DTSE 580
C          DTSE 590
C          DTSE 600
C          DTSE 610
C          DTSE 620
C          DTSE 630
C          DTSE 640
C          DTSE 650
C          DTSE 660
C          DTSE 670
C          DTSE 680
C          DTSE 690
C          DTSE 700
C          DTSE 710
C          DTSE 720
C          DTSE 730
C          DTSE 740
C          DTSE 750
C          DTSE 760
C          DTSE 770
C          DTSE 780
C          DTSE 790
C          DTSE 800
C          DTSE 810
C          DTSE 820
C          DTSE 830
C          DTSE 840
C          DTSE 850
C          DTSE 860
C          DTSE 870
C          DTSE 880
C          DTSE 890
C          DTSE 900
C          DTSE 910
C          DTSE 920
C          DTSE 930
C          DTSE 940
C          DTSE 950
C          DTSE 960
C          DTSE 970
C          DTSE 980
C          DTSE 990
C          DTSE1000
C          DTSE1010
C          DTSE1020
C          DTSE1030
C          DTSE1040
C          DTSE1050
C          DTSE1060
C          DTSE1070
C          DTSE1080
C          DTSE1090
C          DTSE1090
C          END

```


Subroutine SG13 and DSG13

These subroutines compute a vector $Z = (z_1, \dots, z_n)$ of smoothed function values, given vectors $X = (x_1, \dots, x_n)$ of argument values and $Y = (y_1, \dots, y_n)$ of corresponding function values. Except at the endpoints x_1 and x_n , each smoothed value z_i is obtained by evaluating at x_i the least-squares polynomial of degree 1 relevant to the three successive points (x_{i-1}, y_{i-1}) , (x_i, y_i) , and (x_{i+1}, y_{i+1}) .

1. Mathematical background

For $i = 3, \dots, n$ we must find m_i and b_i such that

$$w_i(x) = m_i x + b_i \tag{1}$$

gives the least-squares fit to the points (x_{i-1}, y_{i-2}) , (x_{i-1}, y_{i-1}) , and (x_i, y_i) . The problem, then, is to minimize

$$F(m_i, b_i) = \sum_{k=0}^2 [w_i(x_{i-k}) - y_{i-k}]^2$$

This minimum will occur when

$$\frac{\partial F}{\partial b_i} = 0 \text{ and } \frac{\partial F}{\partial m_i} = 0 \tag{2}$$

Now

$$\frac{\partial F}{\partial b_i} = 2 \sum_{k=0}^2 [w_i(x_{i-k}) - y_{i-k}]$$

and

$$\frac{\partial F}{\partial m_i} = 2 \sum_{k=0}^2 x_{i-k} [w_i(x_{i-k}) - y_{i-k}] \tag{3}$$

Solving equations (2) and (3) yields:

$$m_i = \frac{\sum_{k=0}^2 x_{i-k} y_{i-k} - 1/3 \left(\sum_{k=0}^2 x_{i-k} \right) \left(\sum_{k=0}^2 y_{i-k} \right)}{\sum_{k=0}^2 x_{i-k}^2 - 1/3 \left(\sum_{k=0}^2 x_{i-k} \right)^2} \tag{4}$$

and

$$b_i = \frac{1}{3} \sum_{k=0}^2 (y_{i-k} - m_i x_{i-k}) \tag{5}$$

Letting:

$$\left. \begin{aligned} \bar{y}_i &= \frac{1}{3} \sum_{k=0}^2 y_{i-k}, \quad \bar{x}_i = \frac{1}{3} \sum_{k=0}^2 x_{i-k}, \\ t_{i,k} &= x_{i-k} - \bar{x}_i \quad \text{and} \quad v_{i,k} = y_{i-k} - \bar{y}_i \end{aligned} \right\} \tag{6}$$

we may rewrite (4) and (5) as:

$$m_i = \frac{\sum_{k=0}^2 t_{i,k} v_{i,k}}{\sum_{k=0}^2 t_{i,k}^2} \tag{7}$$

and

$$b_i = \bar{y}_i - m_i \bar{x}_i \tag{8}$$

Using (8) in (1) gives

$$w_i(x) = m_i(x - \bar{x}_i) + \bar{y}_i$$

where m_i is as in (7).

The desired smoothed values z_i are given by:

$$z_i = \begin{cases} w_3(x_1) = m_3 t_{3,2} + \bar{y}_3 & \text{if } i=1 \\ w_{i+1}(x_i) = m_{i+1} t_{i+1,1} + \bar{y}_{i+1} & \text{if } i=2, \dots, n-1 \\ w_n(x_n) = m_n t_{n,0} + \bar{y}_n & \text{if } i=n \end{cases} \tag{9}$$

2. Programming considerations

The subroutines compute the z_i in serial order according to (9). If $n < 3$, there is no computation, and the error parameter IER is set to -1. Otherwise IER is set to zero at the end of the computation. The output vector Z can have the same storage allocation as X or Y.

For reference see Hildebrand, F. B., Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp 258-311.

```

C          SG13 12
C          SG13 20
C          SG13 30
C          SG13 40
C          SG13 50
C          SG13 60
C          SG13 70
C          SG13 80
C          SG13 90
C          SG13 100
C          SG13 110
C          SG13 120
C          SG13 130
C          SG13 140
C          SG13 150
C          SG13 160
C          SG13 170
C          SG13 180
C          SG13 190
C          SG13 200
C          SG13 210
C          SG13 220
C          SG13 230
C          SG13 240
C          SG13 250
C          SG13 260
C          SG13 270
C          SG13 280
C          SG13 290
C          SG13 300
C          SG13 310
C          SG13 320
C          SG13 330
C          SG13 340
C          SG13 350
C          SG13 360
C          SG13 370
C          SG13 380
C          SG13 390
C          SG13 400
C          SG13 410
C          SG13 420
C          SG13 430
C          SG13 440
C          SG13 450
C          SG13 460
C          SG13 470
C          SG13 480
C          SG13 490
C          SG13 500
C          SG13 510
C          SG13 520
C          SG13 530
C          SG13 540
C          SG13 550
C          SG13 560
C          SG13 570
C          SG13 580
C          SG13 590
C          SG13 600
C          SG13 610
C          SG13 620
C          SG13 630
C          SG13 640
C          SG13 650
C          SG13 660
C          SG13 670
C          SG13 680
C          SG13 690
C          SG13 700
C          SG13 710
C          SG13 720
C          SG13 730
C          SG13 740
C          SG13 750
C          SG13 760
C          SG13 770
C          SG13 780

```

```

C          DSG1 10
C          DSG1 20
C          DSG1 30
C          DSG1 40
C          DSG1 50
C          DSG1 60
C          DSG1 70
C          DSG1 80
C          DSG1 90
C          DSG1 100
C          DSG1 110
C          DSG1 120
C          DSG1 130
C          DSG1 140
C          DSG1 150
C          DSG1 160
C          DSG1 170
C          DSG1 180
C          DSG1 190
C          DSG1 200
C          DSG1 210
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C          DSG1 370
C          DSG1 380
C          DSG1 390
C          DSG1 400
C          DSG1 410
C          DSG1 420
C          DSG1 430
C          DSG1 440
C          DSG1 450
C          DSG1 460
C          DSG1 470
C          DSG1 480
C          DSG1 490
C          DSG1 500
C          DSG1 510
C          DSG1 520
C          DSG1 530
C          DSG1 540
C          DSG1 550
C          DSG1 560
C          DSG1 570
C          DSG1 580
C          DSG1 590
C          DSG1 600
C          DSG1 610
C          DSG1 620
C          DSG1 630
C          DSG1 640
C          DSG1 650
C          DSG1 660
C          DSG1 670
C          DSG1 680
C          DSG1 690
C          DSG1 700
C          DSG1 710
C          DSG1 720
C          DSG1 730
C          DSG1 740
C          DSG1 750
C          DSG1 760
C          DSG1 770
C          DSG1 780
C          DSG1 790
C          DSG1 800

```

Subroutines SE13 and DSE13

These subroutines compute a vector $Z = (z_1, \dots, z_n)$ of smoothed function values, given a vector $Y = (y_1, \dots, y_n)$ of function values whose entries y_i correspond to n equidistantly spaced argument values x_i , with $x_i - x_{i-1} = h$ for $i = 2, \dots, n$. Except at the endpoints x_1 and x_n , each smoothed value z_i is obtained by evaluating at x_i the least-squares polynomial of degree 1 relevant to the three successive points (x_{i+k}, y_{i+k}) , $k = -1, 0, 1$.

1. Mathematical background

The procedure is exactly that described for subroutines SG13 and DSG13, but here we have the additional relation $x_i - x_{i-1} = h$, a constant, for $i = 2, \dots, n$. This leads to the following expressions for the z_i :

$$z_i = \begin{cases} \frac{1}{6} (5y_1 + 2y_2 - y_3) & \text{if } i=1 \\ \frac{1}{3} (y_{i-1} + y_i + y_{i+1}) & \text{if } i=2, \dots, n-1 \\ \frac{1}{6} (-y_{n-2} + 2y_{n-1} + 5y_n) & \text{if } i=n \end{cases} \quad (1)$$

2. Programming considerations

The subroutines compute the z_i in serial order according to (1). If $n < 3$, there is no computation, and the error parameter IER is set to -1. Otherwise IER is set to zero at the end of the computation. The output vector Z can have the same storage allocation as Y .

For reference see F. B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp 295-302.

```

C                                     SE13 10
C .....                               SE13 20
C SUBROUTINE SE13                     SE13 30
C                                     SE13 40
C PURPOSE                             SE13 50
C TO COMPUTE A VECTOR OF SMOOTHED FUNCTION VALUES GIVEN A
C VECTOR OF FUNCTION VALUES WHOSE ENTRIES CORRESPOND TO
C EQUIDISTANTLY SPACED ARGUMENT VALUES. SE13 60
C                                     SE13 70
C USAGE                               SE13 80
C CALL SE13(Y,Z,NDIM,IER)             SE13 90
C                                     SE13 100
C DESCRIPTION OF PARAMETERS           SE13 110
C Y - GIVEN VECTOR OF FUNCTION VALUES (DIMENSION NDIM) SE13 120
C Z - RESULTING VECTOR OF SMOOTHED FUNCTION VALUES SE13 130
C (DIMENSION NDIM)                   SE13 140
C NDIM - DIMENSION OF VECTORS Y AND Z SE13 150
C IER - RESULTING ERROR PARAMETER     SE13 160
C IER = -1 - NDIM IS LESS THAN 3     SE13 170
C IER = 0 - NO ERROR                 SE13 180
C                                     SE13 190
C REMARKS                             SE13 200
C (1) IF IER=-1 THERE HAS BEEN NO COMPUTATION. SE13 210
C (2) Z CAN HAVE THE SAME STORAGE ALLOCATION AS Y. IF Y SE13 220
C IS DISTINCT FROM Z, THEN IT IS NOT DESTROYED. SE13 230
C                                     SE13 240
C SUBROUTINES AND SUBPROGRAMS REQUIRED SE13 250
C NONE                                SE13 260
C                                     SE13 270
C METHOD                               SE13 280
C IF X IS THE (SUPPRESSED) VECTOR OF ARGUMENT VALUES, THEN SE13 290
C EXCEPT AT THE ENDPPOINTS X(1) AND X(NDIM), EACH SMOOTHED SE13 300
C VALUE Z(I) IS OBTAINED BY EVALUATING AT X(I) THE LEAST- SE13 310
C SQUARES POLYNOMIAL OF DEGREE 1 RELEVANT TO THE 3 SUCCESSIVE SE13 320
C POINTS (X(I+K),Y(I+K)) K = -1,0,1. (SEE HILDEBRAND, F.B., SE13 330
C INTRODUCTION TO NUMERICAL ANALYSIS, MCGRAW-HILL, NEW YORK/ SE13 340
C TORONTO/LONDON, 1956, PP. 295-302.) SE13 350

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```

C                                     SE13 360
C .....                               SE13 370
C SUBROUTINE SE13(Y,Z,NDIM,IER)      SE13 380
C                                     SE13 390
C DIMENSION Y(1),Z(1)                SE13 400
C TEST OF DIMENSION                   SE13 410
C IF(NDIM-3)1,1                       SE13 420
C                                     SE13 430
C PREPARE LOOP                        SE13 440
C 1 B=.1666667*(5.*Y(1)+Y(2)+Y(3)) SE13 450
C   C=.1666667*(5.*Y(NDIM)+Y(NDIM-1)+Y(NDIM-1)-Y(NDIM-2)) SE13 460
C                                     SE13 470
C START LOOP                          SE13 480
C DO 2 I=3,NDIM                       SE13 490
C   A=B SE13 500
C   B=.3333333*(Y(I-2)+Y(I-1)+Y(I)) SE13 510
C 2 Z(I-2)=A SE13 520
C END OF LOOP                          SE13 530
C                                     SE13 540
C UPDATE LAST TWO COMPONENTS         SE13 550
C Z(NDIM-1)=B SE13 560
C Z(NDIM)=C SE13 570
C IER=0 SE13 580
C RETURN SE13 590
C                                     SE13 600
C ERROR EXIT IN CASE NDIM IS LESS THAN 3 SE13 610
C 3 IER=-1 SE13 620
C RETURN SE13 630
C END SE13 640

```

```

C .....                               DE13 10
C SUBROUTINE DSE13                   DE13 20
C                                     DE13 30
C PURPOSE                             DE13 40
C TO COMPUTE A VECTOR OF SMOOTHED FUNCTION VALUES GIVEN A
C VECTOR OF FUNCTION VALUES WHOSE ENTRIES CORRESPOND TO
C EQUIDISTANTLY SPACED ARGUMENT VALUES. DE13 50
C                                     DE13 60
C USAGE                               DE13 70
C CALL DSE13(Y,Z,NDIM,IER)          DE13 80
C                                     DE13 90
C DESCRIPTION OF PARAMETERS           DE13 100
C Y - GIVEN VECTOR OF DOUBLE PRECISION FUNCTION VALUES DE13 110
C (DIMENSION NDIM)                   DE13 120
C Z - RESULTING VECTOR OF DOUBLE PRECISION SMOOTHED DE13 130
C FUNCTION VALUES (DIMENSION NDIM) DE13 140
C NDIM - DIMENSION OF VECTORS Y AND Z DE13 150
C IER - RESULTING ERROR PARAMETER     DE13 160
C IER = -1 - NDIM IS LESS THAN 3     DE13 170
C IER = 0 - NO ERROR                 DE13 180
C                                     DE13 190
C REMARKS                             DE13 200
C (1) IF IER=-1 THERE HAS BEEN NO COMPUTATION. DE13 210
C (2) Z CAN HAVE THE SAME STORAGE ALLOCATION AS Y. IF Y DE13 220
C IS DISTINCT FROM Z, THEN IT IS NOT DESTROYED. DE13 230
C                                     DE13 240
C SUBROUTINES AND SUBPROGRAMS REQUIRED DE13 250
C NONE                                DE13 260
C                                     DE13 270
C METHOD                               DE13 280
C IF X IS THE (SUPPRESSED) VECTOR OF ARGUMENT VALUES, THEN DE13 290
C EXCEPT AT THE ENDPPOINTS X(1) AND X(NDIM), EACH SMOOTHED DE13 300
C VALUE Z(I) IS OBTAINED BY EVALUATING AT X(I) THE LEAST- DE13 310
C SQUARES POLYNOMIAL OF DEGREE 1 RELEVANT TO THE 3 SUCCESSIVE DE13 320
C POINTS (X(I+K),Y(I+K)) K = -1,0,1. (SEE HILDEBRAND, F.B., DE13 330
C INTRODUCTION TO NUMERICAL ANALYSIS, MCGRAW-HILL, NEW YORK/ DE13 340
C TORONTO/LONDON, 1956, PP. 295-302.) DE13 350
C                                     DE13 360
C .....                               DE13 370
C SUBROUTINE DSE13(Y,Z,NDIM,IER)     DE13 380
C DIMENSION Y(1),Z(1)                DE13 390
C DOUBLE PRECISION Y,Z,A,B,C          DE13 400
C TEST OF DIMENSION                   DE13 410
C IF(NDIM-3)1,1                       DE13 420
C PREPARE LOOP                        DE13 430
C 1 B=.1666666666666667*(5.*DO*(Y(1)+Y(2)+Y(3))) DE13 440
C   C=.1666666666666667*(5.*DO*(Y(NDIM)+Y(NDIM-1)+Y(NDIM-1)-Y(NDIM-2))) DE13 450
C                                     DE13 460
C START LOOP                          DE13 470
C DO 2 I=3,NDIM                       DE13 480
C   A=B DE13 490
C   B=.3333333333333333*(Y(I-2)+Y(I-1)+Y(I)) DE13 500
C 2 Z(I-2)=A DE13 510
C END OF LOOP                          DE13 520
C                                     DE13 530
C UPDATE LAST TWO COMPONENTS         DE13 540
C Z(NDIM-1)=B DE13 550
C Z(NDIM)=C DE13 560
C IER=0 DE13 570
C RETURN DE13 580
C                                     DE13 590
C ERROR EXIT IN CASE NDIM IS LESS THAN 3 DE13 600
C 3 IER=-1 DE13 610
C RETURN DE13 620
C END DE13 630

```

These subroutines compute a vector $Z = (z_1, \dots, z_n)$ of smoothed function values, given a vector $Y = (y_1, \dots, y_n)$ of function values whose entries y_i correspond to n equidistantly spaced argument values x_i with $x_i - x_{i-1} = h$ for $i = 2, \dots, n$. Except at the points x_1, x_2, x_{n-1} , and x_n , each smoothed value z_i is obtained by evaluating at x_i the least-squares polynomial of degree 1 relevant to the five successive points (x_{i+k}, y_{i+k}) , $k = -2, -1, \dots, 2$.

1. Mathematical background

For $i = 5, \dots, n$ we find m_i and b_i such that

$$w_i(x) = m_i x + b_i \tag{1}$$

gives the least-squares fit to the points (x_{i-k}, y_{i-k}) , $k=0, \dots, 4$. The problem, then, is to minimize

$$F(m_i, b_i) = \sum_{k=0}^4 \left[w_i(x_{i-k}) - y_{i-k} \right]^2$$

This minimum will occur when

$$\frac{\partial F}{\partial b_i} = 0 \text{ and } \frac{\partial F}{\partial m_i} = 0 \tag{2}$$

Now

$$\frac{\partial F}{\partial b_i} = 2 \sum_{k=0}^4 \left[w_i(x_{i-k}) - y_{i-k} \right]$$

and

$$\frac{\partial F}{\partial m_i} = 2 \sum_{k=0}^4 x_{i-k} \left[w_i(x_{i-k}) - y_{i-k} \right] \tag{3}$$

Solving equations (2) and (3) yields:

$$m_i = \frac{\sum_{k=0}^4 x_{i-k} y_{i-k} - \frac{1}{5} \left(\sum_{k=0}^4 x_{i-k} \right) \left(\sum_{k=0}^4 y_{i-k} \right)}{\sum_{k=0}^4 x_{i-k}^2 - \frac{1}{5} \left(\sum_{k=0}^4 x_{i-k} \right)^2} \tag{4}$$

and

$$b_i = \frac{1}{5} \sum_{k=0}^4 \left[y_{i-k} - m_i x_{i-k} \right] \tag{5}$$

Using the fact that $x_j - x_{j-1} = h$, a constant, for $j = 2, \dots, n$, (4) and (5) may be rewritten as

$$m_i = \frac{1}{10h} (2y_i + y_{i-1} - y_{i-3} - 2y_{i-4}) \tag{6}$$

and

$$b_i = \frac{1}{5} \sum_{k=0}^4 y_{i-k} - m_i x_{i-2} \tag{7}$$

Using (7) in (1) yields

$$w_i(x) = m_i(x - x_{i-2}) + \frac{1}{5} (y_{i-4} + \dots + y_i)$$

The desired smoothed function values z_i are given by:

$$z_i = \begin{cases} w_5(x_1) = \frac{1}{5} (3y_1 + 2y_2 + y_3 - y_5) & i=1 \\ w_5(x_2) = \frac{1}{10} (4y_1 + 3y_2 + 2y_3 + y_4) & i=2 \\ w_{i+2}(x_i) = \frac{1}{5} (y_{i-2} + y_{i-1} + y_i + y_{i+1} + y_{i+2}) & i=3, \dots, n-2 \\ w_n(x_{n-1}) = \frac{1}{10} (y_{n-3} + 2y_{n-2} + 3y_{n-1} + 4y_n) & i=n-1 \\ w_n(x_n) = \frac{1}{5} (-y_{n-4} + y_{n-2} + 2y_{n-1} + 3y_n) & i=n \end{cases} \tag{8}$$

2. Programming considerations

The subroutines compute the z_i in serial order according to (8). If $n < 5$, there is no computation, and the error parameter IER is set to -1. Otherwise IER is set to zero at the end of the computation. The output vector Z can have the same storage allocation as Y.

For reference see F. B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp 295-302.

C		SE15 10	C	DE15 10
C	-----	SE15 20	C	DE15 20
C		SE15 30	C	DE15 30
C	SUBROUTINE SE15	SE15 40	C	DE15 40
C		SE15 50	C	DE15 50
C	PURPOSE	SE15 60	C	DE15 60
C	TO COMPUTE A VECTOR OF SMOOTHED FUNCTION VALUES GIVEN A	SE15 70	C	DE15 70
C	VECTOR OF FUNCTION VALUES WHOSE ENTRIES CORRESPOND TO	SE15 80	C	DE15 80
C	EQUIDISTANTLY SPACED ARGUMENT VALUES.	SE15 90	C	DE15 90
C		SE15 100	C	DE15 100
C	USAGE	SE15 110	C	DE15 110
C	CALL SE15(Y,Z,NDIM,IER)	SE15 120	C	DE15 120
C		SE15 130	C	DE15 130
C	DESCRIPTION OF PARAMETERS	SE15 140	C	DE15 140
C	Y - GIVEN VECTOR OF FUNCTION VALUES (DIMENSION NDIM)	SE15 150	C	DE15 150
C	Z - RESULTING VECTOR OF SMOOTHED FUNCTION VALUES	SE15 160	C	DE15 160
C	(DIMENSION NDIM)	SE15 170	C	DE15 170
C	NDIM - DIMENSION OF VECTORS Y AND Z	SE15 180	C	DE15 180
C	IER - RESULTING ERROR PARAMETER	SE15 190	C	DE15 190
C	IER = -1 - NDIM IS LESS THAN 5	SE15 200	C	DE15 200
C	IER = 0 - NO ERROR	SE15 210	C	DE15 210
C		SE15 220	C	DE15 220
C	REMARKS	SE15 230	C	DE15 230
C	(1) IF IER=-1 THERE HAS BEEN NO COMPUTATION.	SE15 240	C	DE15 240
C	(2) Z CAN HAVE THE SAME STORAGE ALLOCATION AS Y. IF Y IS	SE15 250	C	DE15 250
C	DISTINCT FROM Z, THEN IT IS NOT DESTROYED.	SE15 260	C	DE15 260
C		SE15 270	C	DE15 270
C	SUBROUTINE AND FUNCTION SUBPROGRAMS REQUIRED	SE15 280	C	DE15 280
C	NONE	SE15 290	C	DE15 290
C		SE15 300	C	DE15 300
C	METHOD	SE15 310	C	DE15 310
C	IF X IS THE (SUPPRESSED) VECTOR OF ARGUMENT VALUES, THEN	SE15 320	C	DE15 320
C	EXCEPT AT THE POINTS X(1),X(2),X(NDIM-1) AND X(NDIM), EACH	SE15 330	C	DE15 330
C	SMOOTHED VALUE Z(I) IS OBTAINED BY EVALUATING AT X(I) THE	SE15 340	C	DE15 340
C	LEAST-SQUARES POLYNOMIAL OF DEGREE 1 RELEVANT TO THE 5	SE15 350	C	DE15 350
C	SUCCESSIVE POINTS (X(I+K),Y(I+K)) K = -2,-1,...,2. (SEE	SE15 360	C	DE15 360
C	HILDEBRAND, F.B., INTRODUCTION TO NUMERICAL ANALYSIS,	SE15 370	C	DE15 370
C	MC GRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP. 295-302.)	SE15 380	C	DE15 380
C		SE15 390	C	DE15 390
C	-----	SE15 400	C	DE15 400
C		SE15 410	C	DE15 410
C	SUBROUTINE SE15(Y,Z,NDIM,IER)	SE15 420	C	DE15 420
C		SE15 430	C	DE15 430
C		SE15 440	C	DE15 440
C		SE15 450	C	DE15 450
C	DIMENSION Y(1),Z(1)	SE15 460	C	DE15 460
C		SE15 470	C	DE15 470
C	TEST OF DIMENSION	SE15 480	C	DE15 480
C	IF(NDIM-5).LT.1	SE15 490	C	DE15 490
C		SE15 500	C	DE15 500
C	PREPARE LOOP	SE15 510	C	DE15 510
C	1 A=Y(1)+Y(1)	SE15 520	C	DE15 520
C	C=Y(2)+Y(2)	SE15 530	C	DE15 530
C	B=-2*(A+Y(1))+C+Y(3)-Y(5)	SE15 540	C	DE15 540
C	C=.100*(A+A+C+Y(2)+Y(3)+Y(4))	SE15 550	C	DE15 550
C		SE15 560	C	DE15 560
C	START LOOP	SE15 570	C	DE15 570
C	DO 2 I=5,NDIM	SE15 580	C	DE15 580
C	A=B	SE15 590	C	DE15 590
C	B=C	SE15 600	C	DE15 600
C	C=.2*(Y(I-4)+Y(I-3)+Y(I-2)+Y(I-1)+Y(I))	SE15 610	C	DE15 610
C	2 Z(I-4)=A	SE15 620	C	DE15 620
C		SE15 630	C	DE15 630
C	END OF LOOP	SE15 640	C	DE15 640
C		SE15 650	C	DE15 650
C	UPDATE LAST FOUR COMPONENTS	SE15 660	C	DE15 660
C	A=Y(NDIM)+Y(NDIM)	SE15 670	C	DE15 670
C	OA=-.1*(A+Y(NDIM-1)+Y(NDIM-1)+Y(NDIM-1)+Y(NDIM-2)+Y(NDIM-2))	SE15 680	C	DE15 680
C	1 Y(NDIM-3)=A	SE15 690	C	DE15 690
C	Z(NDIM-3)=B	SE15 700	C	DE15 700
C	Z(NDIM-2)=C	SE15 710	C	DE15 710
C	Z(NDIM-1)=A	SE15 720	C	DE15 720
C	Z(NDIM)=A+A-C	SE15 730	C	DE15 730
C	IER=0	SE15 740	C	DE15 740
C	RETURN	SE15 750	C	DE15 750
C		SE15 760	C	DE15 760
C	ERROR EXIT IN CASE NDIM IS LESS THAN 5	SE15 770	C	DE15 770
C	3 IER=-1	SE15 780	C	DE15 780
C	RETURN		C	DE15 790
C	END		C	DE15 800

C		DE15 10	C	DE15 10
C	-----	DE15 20	C	DE15 20
C		DE15 30	C	DE15 30
C	SUBROUTINE DSE15	DE15 40	C	DE15 40
C		DE15 50	C	DE15 50
C	PURPOSE	DE15 60	C	DE15 60
C	TO COMPUTE A VECTOR OF SMOOTHED FUNCTION VALUES GIVEN A	DE15 70	C	DE15 70
C	VECTOR OF FUNCTION VALUES WHOSE ENTRIES CORRESPOND TO	DE15 80	C	DE15 80
C	EQUIDISTANTLY SPACED ARGUMENT VALUES.	DE15 90	C	DE15 90
C		DE15 100	C	DE15 100
C	USAGE	DE15 110	C	DE15 110
C	CALL DSE15(Y,Z,NDIM,IER)	DE15 120	C	DE15 120
C		DE15 130	C	DE15 130
C	DESCRIPTION OF PARAMETERS	DE15 140	C	DE15 140
C	Y - GIVEN VECTOR OF DOUBLE PRECISION FUNCTION VALUES	DE15 150	C	DE15 150
C	(DIMENSION NDIM)	DE15 160	C	DE15 160
C	Z - RESULTING VECTOR OF DOUBLE PRECISION SMOOTHED	DE15 170	C	DE15 170
C	FUNCTION VALUES (DIMENSION NDIM)	DE15 180	C	DE15 180
C	NDIM - DIMENSION OF VECTORS Y AND Z	DE15 190	C	DE15 190
C	IER - RESULTING ERROR PARAMETER	DE15 200	C	DE15 200
C	IER = -1 - NDIM IS LESS THAN 5	DE15 210	C	DE15 210
C	IER = 0 - NO ERROR	DE15 220	C	DE15 220
C		DE15 230	C	DE15 230
C	REMARKS	DE15 240	C	DE15 240
C	(1) IF IER=-1 THERE HAS BEEN NO COMPUTATION.	DE15 250	C	DE15 250
C	(2) Z CAN HAVE THE SAME STORAGE ALLOCATION AS Y. IF Y IS	DE15 260	C	DE15 260
C	DISTINCT FROM Z, THEN IT IS NOT DESTROYED.	DE15 270	C	DE15 270
C		DE15 280	C	DE15 280
C	SUBROUTINE AND FUNCTION SUBPROGRAMS REQUIRED	DE15 290	C	DE15 290
C	NONE	DE15 300	C	DE15 300
C		DE15 310	C	DE15 310
C	METHOD	DE15 320	C	DE15 320
C	IF X IS THE (SUPPRESSED) VECTOR OF ARGUMENT VALUES, THEN	DE15 330	C	DE15 330
C	EXCEPT AT THE POINTS X(1),X(2),X(NDIM-1) AND X(NDIM), EACH	DE15 340	C	DE15 340
C	SMOOTHED VALUE Z(I) IS OBTAINED BY EVALUATING AT X(I) THE	DE15 350	C	DE15 350
C	LEAST-SQUARES POLYNOMIAL OF DEGREE 1 RELEVANT TO THE 5	DE15 360	C	DE15 360
C	SUCCESSIVE POINTS (X(I+K),Y(I+K)) K = -2,-1,...,2. (SEE	DE15 370	C	DE15 370
C	HILDEBRAND, F.B., INTRODUCTION TO NUMERICAL ANALYSIS,	DE15 380	C	DE15 380
C	MC GRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP. 295-302.)	DE15 390	C	DE15 390
C		DE15 400	C	DE15 400
C	-----	DE15 410	C	DE15 410
C		DE15 420	C	DE15 420
C	SUBROUTINE DSE15(Y,Z,NDIM,IER)	DE15 430	C	DE15 430
C		DE15 440	C	DE15 440
C		DE15 450	C	DE15 450
C	DIMENSION Y(1),Z(1)	DE15 460	C	DE15 460
C	DOUBLE PRECISION Y,Z,A,B,C	DE15 470	C	DE15 470
C		DE15 480	C	DE15 480
C	TEST OF DIMENSION	DE15 490	C	DE15 490
C	IF(NDIM-5).LT.1	DE15 500	C	DE15 500
C		DE15 510	C	DE15 510
C	PREPARE LOOP	DE15 520	C	DE15 520
C	1 A=Y(1)+Y(1)	DE15 530	C	DE15 530
C	C=Y(2)+Y(2)	DE15 540	C	DE15 540
C	B=-2.00*(A+Y(1))+C+Y(3)-Y(5)	DE15 550	C	DE15 550
C	C=.100*(A+A+C+Y(2)+Y(3)+Y(4))	DE15 560	C	DE15 560
C		DE15 570	C	DE15 570
C	START LOOP	DE15 580	C	DE15 580
C	DO 2 I=5,NDIM	DE15 590	C	DE15 590
C	A=B	DE15 600	C	DE15 600
C	B=C	DE15 610	C	DE15 610
C	C=.200*(Y(I-4)+Y(I-3)+Y(I-2)+Y(I-1)+Y(I))	DE15 620	C	DE15 620
C	2 Z(I-4)=A	DE15 630	C	DE15 630
C		DE15 640	C	DE15 640
C	END OF LOOP	DE15 650	C	DE15 650
C		DE15 660	C	DE15 660
C	UPDATE LAST FOUR COMPONENTS	DE15 670	C	DE15 670
C	A=Y(NDIM)+Y(NDIM)	DE15 680	C	DE15 680
C	OA=-.100*(A+Y(NDIM-1)+Y(NDIM-1)+Y(NDIM-1)+Y(NDIM-2)+Y(NDIM-2))	DE15 690	C	DE15 690
C	1 Y(NDIM-3)=A	DE15 700	C	DE15 700
C	Z(NDIM-3)=B	DE15 710	C	DE15 710
C	Z(NDIM-2)=C	DE15 720	C	DE15 720
C	Z(NDIM-1)=A	DE15 730	C	DE15 730
C	Z(NDIM)=A+A-C	DE15 740	C	DE15 740
C	IER=0	DE15 750	C	DE15 750
C	RETURN	DE15 760	C	DE15 760
C		DE15 770	C	DE15 770
C	ERROR EXIT IN CASE NDIM IS LESS THAN 5	DE15 780	C	DE15 780
C	3 IER=-1	DE15 790	C	DE15 790
C	RETURN	DE15 800	C	DE15 800
C	END		C	DE15 800

Subroutine SE35 and DSE35

These subroutines compute a vector $Z = (z_1, \dots, z_n)$ of smoothed function values, given a vector $Y = (y_1, \dots, y_n)$ of function values whose entries y_i correspond to n equidistantly spaced argument values x_i , with $x_i - x_{i-1} = h$ for $i = 2, \dots, n$. Except at the points x_1, x_2, x_{n-1} , and x_n , each smoothed value z_i is obtained by evaluating at x_i the least-squares polynomial of degree 3 relevant to the five successive points (x_{i+k}, y_{i+k}) , $k = -2, -1, \dots, 2$.

1. Mathematical background

For $i = 5, \dots, n$ we must find a_i, b_i, c_i , and d_i such that

$$w_i(x) = a_i x^3 + b_i x^2 + c_i x + d_i \quad (1)$$

gives the least-squares fit to the points (x_{i-k}, y_{i-k}) , $k = 0, \dots, 4$.

The problem, thus, is to minimize

$$F(a_i, b_i, c_i, d_i) = \sum_{k=0}^4 \left[w_i(x_{i-k}) - y_{i-k} \right]^2 \quad (2)$$

The minimum will occur when

$$\frac{\partial F}{\partial a_i} = \frac{\partial F}{\partial b_i} = \frac{\partial F}{\partial c_i} = \frac{\partial F}{\partial d_i} = 0$$

Now:

$$\left. \begin{aligned} \frac{\partial F}{\partial a_i} &= 2 \sum_{k=0}^4 x_{i-k}^3 \left[w_i(x_{i-k}) - y_{i-k} \right] \\ \frac{\partial F}{\partial b_i} &= 2 \sum_{k=0}^4 x_{i-k}^2 \left[w_i(x_{i-k}) - y_{i-k} \right] \\ \frac{\partial F}{\partial c_i} &= 2 \sum_{k=0}^4 x_{i-k} \left[w_i(x_{i-k}) - y_{i-k} \right] \\ \frac{\partial F}{\partial d_i} &= 2 \sum_{k=0}^4 \left[w_i(x_{i-k}) - y_{i-k} \right] \end{aligned} \right\} \quad (3)$$

Solving (2) and (3) for a_i, b_i, c_i , and d_i , with $x_i - x_{i-1} = h$, we get:

$$a_i = A_i$$

$$b_i = -3 A_i x_{i-2} + B_i$$

$$c_i = 3 A_i x_{i-2}^2 - 2 B_i x_{i-2} + C_i$$

$$d_i = -A_i x_{i-2}^3 + B_i x_{i-2}^2 - C_i x_{i-2} + D_i + \bar{y}_i$$

where:

$$\bar{y}_i = \frac{1}{5} \sum_{k=0}^4 y_{i-k}$$

$$A_i = -\frac{1}{12h} (y_{i-4} - 2y_{i-3} + 2y_{i-1} - y_i)$$

$$B_i = \frac{1}{14h^2} (4y_{i-4} + y_{i-3} + y_{i-1} + 4y_i - 10\bar{y}_i)$$

$$C_i = \frac{1}{12h} (y_{i-4} - 8y_{i-3} + 8y_{i-1} - y_i)$$

$$D_i = -\frac{1}{7} (4y_{i-4} + y_{i-3} + y_{i-1} + 4y_i - 10\bar{y}_i)$$

Finally, the desired smoothed values z_i are given by:

$$z_i = \left\{ \begin{aligned} w_5(x_1) &= y_1 - \frac{1}{70} \delta^4 y_3 \quad \text{if } i=1 \\ w_5(x_2) &= y_2 + \frac{2}{35} \delta^4 y_3 \quad \text{if } i=2 \\ w_{i+2}(x_i) &= y_i - \frac{3}{35} \delta^4 y_i \quad \text{if } i=3, \dots, n-2 \\ w_n(x_{n-1}) &= y_{n-1} + \frac{2}{35} \delta^4 y_{n-2} \quad \text{if } i=n-1 \\ w_n(x_n) &= y_n - \frac{1}{70} \delta^4 y_{n-2} \quad \text{if } i=n \end{aligned} \right\} \quad (4)$$

where

$$\delta^4 y_i = y_{i-2} - 4y_{i-1} + 6y_i - 4y_{i+1} + y_{i+2}$$

for $i=3, \dots, n-2$

2. Programming considerations

These subroutines compute the z_i in serial order according to (4). If $n < 5$, there is no computation, and the error parameter IER is set to -1. Otherwise IER is set to zero at the end of the computation. The output vector Z can have the same storage allocation as Y.

For reference see F. B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp. 295-302.

```

C ..... DSE3 10
C ..... DSE3 20
C ..... DSE3 30
C ..... DSE3 40
C ..... DSE3 50
C ..... DSE3 60
C ..... DSE3 70
C ..... DSE3 80
C ..... DSE3 90
C ..... DSE3 100
C ..... DSE3 110
C ..... DSE3 120
C ..... DSE3 130
C ..... DSE3 140
C ..... DSE3 150
C ..... DSE3 160
C ..... DSE3 170
C ..... DSE3 180
C ..... DSE3 190
C ..... DSE3 200
C ..... DSE3 210
C ..... DSE3 220
C ..... DSE3 230
C ..... DSE3 240
C ..... DSE3 250
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C ..... DSE3 280
C ..... DSE3 290
C ..... DSE3 300
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C ..... DSE3 320
C ..... DSE3 330
C ..... DSE3 340
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C ..... DSE3 370
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C ..... DSE3 390
C ..... DSE3 400
C ..... DSE3 410
C ..... DSE3 420
C ..... DSE3 430
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C ..... DSE3 460
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C ..... DSE3 480
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C ..... DSE3 500
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C ..... DSE3 520
C ..... DSE3 530
C ..... DSE3 540
C ..... DSE3 550
C ..... DSE3 560
C ..... DSE3 570
C ..... DSE3 580
C ..... DSE3 590
C ..... DSE3 600
C ..... DSE3 610
C ..... DSE3 620
C ..... DSE3 630
C ..... DSE3 640
C ..... DSE3 650
C ..... DSE3 660
C ..... DSE3 670
C ..... DSE3 680
C ..... DSE3 690
C ..... DSE3 700
C ..... DSE3 710
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C ..... DSE3 750
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C ..... DSE3 780
C ..... DSE3 790
C ..... DSE3 800
C ..... DSE3 810
C ..... DSE3 820
C ..... DSE3 830

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C ..... DSE3 10
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C ..... DSE3 40
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C ..... DSE3 750
C ..... DSE3 760
C ..... DSE3 770
C ..... DSE3 780
C ..... DSE3 790
C ..... DSE3 800
C ..... DSE3 810
C ..... DSE3 820
C ..... DSE3 830

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Subroutine APFS and DAPFS

These subroutines compute the solution of the normal equations set up by subroutines APLL and DAPLL. This is the second step in the procedure for determining the least-squares fit of a given discrete function.

1. Mathematical background

Let $f(x)$, $g_i(x)$, $i=1, 2, \dots, m$, and $w(x) > 0$ be functions defined for $x=x_1, x_2, \dots, x_n$.

The problem is to determine the coefficients c_i of the linear combination

$$p(x) = \sum_{i=1}^m c_i g_i(x)$$

such that

$$e_m = \sum_{k=1}^n w(x_k) (f(x_k) - p(x_k))^2 = \text{minimum} \quad (1)$$

The necessary conditions

$$\frac{\partial e_m}{\partial c_i} = 0, \quad i=1, 2, \dots, m \quad (2)$$

form a system of m linear equations in m unknowns c_i .

To simplify the notation we introduce the following matrices:

$$X = \begin{bmatrix} x_1 \\ x_2 \\ \cdot \\ \cdot \\ x_n \end{bmatrix}, \quad F = \begin{bmatrix} f(x_1) \\ \cdot \\ \cdot \\ \cdot \\ f(x_n) \end{bmatrix}, \quad W = \begin{bmatrix} w(x_1) & & & \\ & w(x_2) & & \\ & & \cdot & \\ & & & \cdot \\ & & & & w(x_n) \end{bmatrix},$$

$$c = \begin{bmatrix} c_1 \\ \cdot \\ \cdot \\ \cdot \\ c_m \end{bmatrix}, \quad G = \begin{bmatrix} g_1(x_1) & \cdot & \cdot & g_1(x_n) \\ \cdot & & & \cdot \\ \cdot & & & \cdot \\ \cdot & & & \cdot \\ g_m(x_1) & \cdot & \cdot & g_m(x_n) \end{bmatrix}$$

Then we have

$$e_m = (F^T - C^T G) W (F - G^T C)$$

or, with $e_o = F^T W F$,

$$e_m = e_o - 2C^T G W F + C^T G W G^T C \quad (1')$$

Using (1'), equations (2) may be written as

$$G W G^T C = G W F \quad (2')$$

Combining (1') and (2') gives

$$e_o - e_m = C^T G W G^T C \quad (3)$$

The normal equations (2') for the unknown vector C may be solved using Cholesky's method, since the coefficient matrix $A = G W G^T$ is obviously symmetric and is positive definite if all the fundamental functions $g_i(x)$ are linearly independent for the arguments x_i ; that is, if the rows of G are linearly independent. Let $R = G W F$. Using Cholesky's method, A and R are replaced without additional storage requirements by T and $(T^T)^{-1}R$, where $A = T^T T$, and T is upper triangular.

Using these facts, an easy calculation shows

$$e_o - e_m = \left\| (T^T)^{-1} R \right\|^2$$

Introducing additional fundamental functions in the linear combination $p(x)$ will not affect the first m rows and columns of A or the first m elements of R . Therefore, Cholesky's method gives a decomposition of $e_o - e_m$ into the separate components corresponding to individual degrees of freedom.

2. Programming considerations

All least-squares fits of dimension $1, 2, \dots, m$ may be computed from the reduced normal equations $TC = (T^T)^{-1}R$. If the solutions are generated in the storage locations of T , there is no additional storage requirement.

Using the decomposition of $e_o - e_m$, the factorization may be terminated with dimension k if $e_k < \eta e_o$, giving the least-squares fit of dimension k which satisfies the user-specified precision (relative tolerance η). Due to rounding errors this will work only if η is approximately between 1 and 10^{-6} in single precision, and between 1 and 10^{-15} in double precision. Nevertheless, the square sum of residuals corresponding to a least-squares fit calculated in single or double precision may be as small as $e_o 10^{-12}$ or $e_o 10^{-30}$, respectively.

Due to rounding errors the square root method may break down if very small or negative pivot elements indicate a loss of significance. Therefore, all pivot elements are tested against the absolute value of EPS multiplied by the first diagonal element of A. If the kth pivot element is not greater than this internal test value, the normal equations are treated as if they had dimension k-1 only.

Let N1, N2 denote the following numbers:

N1 = the largest number less than or equal to m for which there is no indication of loss of significance

N2 = the smallest number less than or equal to m for which

$$e_{N2} \leq \left| \eta e_0 \right|$$

Depending on the input parameter IOP, which specifies the operations to be performed, the dimension IRES (that is, the dimension of the subsystem of the normal equations used for calculation) is set to N1 if IOP is positive or zero, and to the smaller of the two numbers N1, N2 if IOP is negative.

The operations performed by APFS are:

IOP = 0 Compute the triangular factorization $A = T^T T$, $TC = (T^T)^{-1} R$ and e_{IRES} only.

IOP = ±1 In addition to the above, the least-squares fit of dimension IRES is computed and stored in column IRES of the triangular array WORK.

IOP = ±2 In addition to IOP = 0 calculations, all least-square fits of dimension 1 up to IRES are computed and stored in columns 1 up to IRES of the array WORK.

a. Storage allocation

Initially the symmetric coefficient matrix A is stored columnwise in compressed form in the triangular array WORK. It is followed immediately by the right-hand side vector R and a single location containing e_0 initially and e_{IRES} on return. This storage scheme is generated by subroutine APLL.

b. Errors

The error parameter IER is set to -1 if a non-positive dimension m has been specified.

If IOP is positive or zero, IER is set to 1 in case of an indication of a loss of significance.

If IOP is negative, IER is set to 1 if the specified accuracy could not be reached, even with a fit of dimension IRES.

For reference see A. T. Berztiss, "Least-squares fitting of polynomials to irregularly spaced data", *SIAM Review* (1964), vol. 6, no. 3, pp 203-227.

C		APFS 10
C		APFS 20
C		APFS 30
C		APFS 40
C		APFS 50
C		APFS 60
C	PURPOSE	APFS 70
C	PERFORM SYMMETRIC FACTORIZATION OF THE MATRIX OF THE NORMAL	APFS 80
C	EQUATIONS FOLLOWED BY CALCULATION OF THE LEAST SQUARES FIT	APFS 90
C	OPTIONALLY	APFS 100
C		APFS 110
C	USAGE	APFS 120
C	CALL APFS(WORK,IP,IRES,IOP,EPS,ETA,IER)	APFS 130
C		APFS 140
C	DESCRIPTION OF PARAMETERS	APFS 150
C	WORK - GIVEN SYMMETRIC COEFFICIENT MATRIX, STORED	APFS 160
C	COMPRESSED, I.E UPPER TRIANGULAR PART COLUMNWISE.	APFS 170
C	THE GIVEN RIGHT HAND SIDE OCCUPIES THE NEXT IP	APFS 180
C	LOCATIONS IN WORK. THE VERY LAST COMPONENT OF WORK	APFS 190
C	CONTAINS THE SQUARE SUM OF FUNCTION VALUES E0	APFS 200
C	THIS SCHEME OF STORAGE ALLOCATION IS PRODUCED E.G.	APFS 210
C	BY SUBROUTINE APLL.	APFS 220
C	THE GIVEN MATRIX IS FACTORED IN THE FORM	APFS 230
C	TRANSPPOSE(T)T AND THE GIVEN RIGHT HAND SIDE IS	APFS 240
C	DIVIDED BY TRANSPPOSE(T).	APFS 250
C	THE UPPER TRIANGULAR FACTOR T IS RETURNED IN WORK IF	APFS 260
C	IOP EQUALS ZERO.	APFS 270
C	IN CASE OF NONZERO IOP THE CALCULATED SOLUTIONS ARE	APFS 280
C	STORED IN THE COLUMNS OF TRIANGULAR ARRAY WORK OF	APFS 290
C	CORRESPONDING DIMENSION AND E0 IS REPLACED BY THE	APFS 300
C	SQUARE SUM OF THE ERRORS FOR FIT OF DIMENSION IRES.	APFS 310
C	THE TOTAL DIMENSION OF WORK IS (IP+1)*(IP+2)/2	APFS 320
C	IP - NUMBER OF FUNDAMENTAL FUNCTIONS USED FOR LEAST	APFS 330
C	SQUARES FIT	APFS 340
C	IRES - DIMENSION OF CALCULATED LEAST SQUARES FIT.	APFS 350
C	LET N1, N2, DENOTE THE FOLLOWING NUMBERS:	APFS 360
C	M1 = MAXIMAL DIMENSION FOR WHICH NO LOSS OF	APFS 370
C	SIGNIFICANCE WAS INDICATED DURING FACTORIZATION.	APFS 380
C	N2 = SMALLEST DIMENSION FOR WHICH THE SQUARE SUM OF	APFS 390
C	THE ERRORS DOES NOT EXCEED TEST=ABS(ETA*EPS)	APFS 400
C	THEN IRES=MIN(M1,N1) IF IOP IS NONNEGATIVE	APFS 410
C	AND IRES=MIN(M1,N2) IF IOP IS NEGATIVE	APFS 420
C	IOP - INPUT PARAMETER FOR SELECTION OF OPERATION	APFS 430
C	IOP = 0 MEANS TRIANGULAR FACTORIZATION, DIVISION OF	APFS 440
C	THE RIGHT HAND SIDE BY TRANSPPOSE(T) AND	APFS 450
C	CALCULATION OF THE SQUARE SUM OF ERRORS IS	APFS 460
C	PERFORMED ONLY	APFS 470
C	IOP = +1 OR -1 MEANS THE SOLUTION OF DIMENSION IRES	APFS 480
C	IS CALCULATED ADDITIONALLY	APFS 490
C	IOP = +2 OR -2 MEANS ALL SOLUTIONS FOR DIMENSION ONE ARE	APFS 500
C	UP TO IRES ARE CALCULATED ADDITIONALLY	APFS 510
C	EPS - RELATIVE TOLERANCE FOR TEST ON LOSS OF SIGNIFICANCE.	APFS 520
C	A SENSIBLE VALUE IS BETWEEN 1.E-3 AND 1.E-6	APFS 530
C	ETA - RELATIVE TOLERANCE FOR TOLERATED SQUARE SUM OF	APFS 540
C	ERRORS. A REALISTIC VALUE IS BETWEEN 1.E0 AND 1.E-6	APFS 550
C	IER - RESULTANT ERROR PARAMETER	APFS 560
C	IER = -1 MEANS NONPOSITIVE IP	APFS 570
C	IER = 0 MEANS NO LOSS OF SIGNIFICANCE DETECTED	APFS 580
C	AND SPECIFIED TOLERANCE OF ERRORS REACHED	APFS 590
C	IER = 1 MEANS LOSS OF SIGNIFICANCE DETECTED OR	APFS 600
C	SPECIFIED TOLERANCE OF ERRORS NOT REACHED	APFS 610
C		APFS 620
C	REMARKS	APFS 630
C	THE ABSOLUTE TOLERANCE USED INTERNALLY FOR TEST ON LOSS OF	APFS 640
C	SIGNIFICANCE IS TOL=ABS(EPS*WORK(1)).	APFS 650
C	THE ABSOLUTE TOLERANCE USED INTERNALLY FOR THE SQUARE SUM OF	APFS 660
C	ERRORS IS ABS(ETA*EPS).	APFS 670
C	IOP GREATER THAN 2 HAS THE SAME EFFECT AS IOP = 2.	APFS 680
C	IOP LESS THAN -2 HAS THE SAME EFFECT AS IOP = -2.	APFS 690
C	IRES = 0 MEANS THE ABSOLUTE VALUE OF EPS IS NOT LESS THAN	APFS 700
C	ONE AND/OR WORK(1) IS NOT POSITIVE AND/OR IP IS NOT POSITIVE	APFS 710
C		APFS 720
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	APFS 730
C	NONE	APFS 740
C		APFS 750
C	METHOD	APFS 760
C	CALCULATION OF THE LEAST SQUARES FITS IS DONE USING	APFS 770
C	CHOLESKY'S SQUARE ROOT METHOD FOR SYMMETRIC FACTORIZATION.	APFS 780
C	THE INCORPORATED TEST ON LOSS OF SIGNIFICANCE MEANS EACH	APFS 790
C	RADIAND MUST BE GREATER THAN THE INTERNAL ABSOLUTE	APFS 800
C	TOLERANCE TOL=ABS(EPS*WORK(1)).	APFS 810
C	IN CASE OF LOSS OF SIGNIFICANCE IN THE ABOVE SENSE ONLY A	APFS 820
C	SUBSYSTEM OF THE NORMAL EQUATIONS IS SOLVED.	APFS 830
C	IN CASE OF NEGATIVE IOP THE TRIANGULAR FACTORIZATION IS	APFS 840
C	TERMINATED PREMATURELY EITHER IF THE SQUARE SUM OF THE	APFS 850
C	ERRORS DOES NOT EXCEED ETA*EPS OR IF THERE IS INDICATION	APFS 860
C	FOR LOSS OF SIGNIFICANCE	APFS 870
C		APFS 880
C	-----	APFS 890
C	SUBROUTINE APFS(WORK,IP,IRES,IOP,EPS,ETA,IER)	APFS 900
C		APFS 910
C		APFS 920
C		APFS 930
C	DIMENSIONED DUMMY VARIABLES	APFS 940
C	DIMENSION WORK(1)	APFS 950
C	IRES=0	APFS 960
C		APFS 970
C	TEST OF SPECIFIED DIMENSION	APFS 980
C	IF(IP).1.2	APFS 990
C		APFS 1000
C	ERROR RETURN IN CASE OF ILLEGAL DIMENSION	APFS 1010
C	1 IER=-1	APFS 1020
C	RETURN	APFS 1030
C		APFS 1040
C	INITIALIZE FACTORIZATION PROCESS	APFS 1050
C	2 IPIV=0	APFS 1060
C	IPPL=IP+1	APFS 1070
C	IER=1	APFS 1080
C	ITE=IP+IP/2	APFS 1090
C	IEND=ITE+IP/2	APFS 1100
C	TOL=ABS(EPS*WORK(1))	APFS 1110
C	TEST=ABS(ETA*WORK(IEND))	APFS 1120
C		APFS 1130
C	START LOOP OVER ALL ROWS OF WORK	APFS 1140
C	DO 11 I=1,IP	APFS 1150
C	IPIV=IPIV+1	APFS 1160
C	JA=IPIV-IRES	APFS 1170
C	JE=IPIV-1	APFS 1180
C		APFS 1190
C	FORM SCALAR PRODUCT NEEDED TO MODIFY CURRENT ROW ELEMENTS	APFS 1200
C	JK=IPIV	APFS 1210

```

DO 9 K=1,IP01
SUM=0.
IF(IRES)5,5,3
3 JK=JK-IRES
DO 4 J=JA,JE
SUM=SUM+W0R(K,J)*W0R(K,J)
4 JK=JK+1
5 IF(JK-IP1V)6,6,8
C
C TEST FOR LOSS OF SIGNIFICANCE
6 SUM=W0R(K(IP1V)-SUM
IF(SUM-TOL)12,12,7
7 SUM=SQRT(SUM)
W0R(K(IP1V)=SUM
PIV=1./SUM
GOTO 9
C
C UPDATE OFF-DIAGONAL TERMS
8 SUM=(W0R(K(JK)-SUM)*PIV
W0R(K(JK)=SUM
9 JK=JK+K
C
C UPDATE SQUARE SUM OF ERRORS
W0R(K(IEND)=W0R(K(IEND)-SUM*SUM
C
C RECORD ADDRESS OF LAST PIVOT ELEMENT
IRES=IRES+1
IADR=IP1V
C
C TEST FOR TOLERABLE ERROR IF SPECIFIED
IF(IOP)10,11,11
10 IF(W0R(K(IEND)-TEST)13,13,11
11 CONTINUE
IF(IOP)12,22,12
C
C PERFORM BACK SUBSTITUTION IF SPECIFIED
12 IF(IOP)14,23,14
13 IER=0
14 IP1V=IRES
15 IF(IP1V)23,23,16
16 SUM=0.
JA=IE+IP1V
JJ=IADR
JK=IADR
K=IP1V
DO 19 I=1,IP1V
W0R(K(JK)=(W0R(JA)-SUM)/W0R(K(JJ)
IF(K-1)20,20,17
17 JE=JJ-1
SUM=0.
DO 18 J=K,IP1V
SUM=SUM+W0R(K(JK)*W0R(K(JE)
JK=JK+1
JE=JE+1
18 JK=JE-IP1V
JA=JA-1
JJ=JJ-K
19 K=K-1
20 IF(IOP/2)21,23,21
21 IADR=IADR-IP1V
IP1V=IP1V-1
GOTO 15
C
C NORMAL RETURN
22 IER=0
23 RETURN
END

```

Subroutine APCH and DAPCH

These subroutines set up the normal equations for a polynomial least-squares fit to a given discrete function. The solution of these equations is determined by subroutine APFS. The best fitting polynomial is computed in terms of its Chebyshev expansion.

1. Mathematical background

Let $f(x)$ be a function defined for $x=x_1, x_2, \dots, x_n$.

The problem is to determine the coefficients of the polynomial

$$p(x) = \sum_{i=1}^m c_i x^{i-1}, \text{ such that}$$

$$\sum_{i=1}^n (f(x_i) - p(x_i))^2 = \text{minimum}$$

This problem leads to a system of linear equations $AC = R$ where C is the vector of unknown coefficients, A is the m by m symmetric positive definite matrix with elements

$$a_{jk} = \sum_{i=1}^n x_i^{j-1} x_i^{k-1}$$

and R is the vector with elements

$$r_j = \sum_{i=1}^n f(x_i) x_i^{j-1}$$

If there is a weight w_i corresponding to each point $(x_i, f(x_i))$, the i^{th} term of the sums for the a_{jk} and r_j must be multiplied by w_i .

In practice the positive definite matrix A is badly ill-conditioned. Therefore, the straightforward method described above is feasible only for polynomials of low degree, about 3 or 4.

Use of Chebyshev polynomials instead of monomials results in a remarkable improvement of the condition of the normal equations, provided the arguments have a sensible distribution (for example, equidistant).

Let x_L and x_R denote the leftmost and rightmost arguments. By means of the linear transformation

$$t(x) = \frac{2x - (x_L + x_R)}{x_R - x_L} = x_D \cdot x + x_0$$

the argument range $x_L \leq x \leq x_R$ is reduced to the argument range $-1 \leq t \leq +1$.

The polynomial $p(x)$ is calculated in the form of its Chebyshev expansion $p(x) = b_1 T_0(t) + b_2 T_1(t) + \dots + b_m T_{m-1}(t)$, where $T_k(t)$ is the Chebyshev polynomial of degree k .

Then the vector B of the unknown coefficients b_i is a solution of the matrix equation $AB = R$, where A is an m by m symmetric positive definite matrix with elements

$$a_{jk} = \sum_{i=1}^n T_{j-1}(t(x_i)) T_{k-1}(t(x_i))$$

and R is a vector with elements

$$r_j = \sum_{i=1}^n T_{j-1}(t(x_i)) f(x_i)$$

The values of the Chebyshev polynomials for the argument t are calculated by means of the three-term recurrence equation:

$$T_k(t) = 2t \cdot T_{k-1}(t) - T_{k-2}(t); \quad k \geq 2$$

with starting values $T_0(t) = 1$, $T_1(t) = t$.

In setting up the matrix A , time is saved by using the identity $2T_j \cdot T_k = T_{j+k} + T_{j-k}$.

a. Remarks

The Chebyshev expansion of the polynomial $p(x)$ gives a much better indication of the accuracy of the approximation than the coefficient vector of the polynomial itself. If the specified degree of the polynomial is too high, the last terms of the Chebyshev expansion will be uniformly small compared to the coefficients in front. The degree may be reduced by the number of small trailing coefficients without unduly enlarging the overall error.

An upper bound for the error introduced by neglecting the last terms of the Chebyshev expansion is given by the sum of the absolute values of these terms. Normally, transformation of the Chebyshev expansions in $t(x)$ to ordinary polynomials in x results in severe loss of accuracy. Therefore, no attempt is made to return the polynomial expansions, which is no disadvantage since the Chebyshev expansion may be evaluated effectively for a specified argument x using subroutines CNPS and DCNPS with argument $t = x \cdot x_D + x_0$ and the calculated coefficient vector of the Chebyshev expansion.

The transformation of the calculated Chebyshev expansion to an ordinary polynomial may be accomplished using subroutines TCNP and DTCNP.

2. Programming considerations

Input arrays passed to subroutines APCH and DAPCH are DATI and WORK. DATI contains the given data set to be approximated, consisting of n argument values x_1, \dots, x_n followed by corresponding function values f_1, \dots, f_n and by corresponding weight values (if any). Constant weighting (value one) is implied if DATI ($2n + 1$) contains a nonpositive value.

Instead of arguments x_i , we use $t_i = x_i \cdot x_D + x_0$ for setting up the normal equations. The constants x_D and x_0 are returned as result values.

The normal equations are generated in the triangular array WORK. Only the upper triangular part of the symmetric coefficient matrix is generated and stored columnwise, followed immediately by the right-hand side and by the weighted square sum of function values.

This storage allocation scheme is required by subroutine APFS and DAPFS, which may be used for calculation of the solution of the normal equations. Exceptions are indicated by the error parameter IER, which is set to -1 if n and m are not both positive or if n is less than m , and to +1 if the arguments are coinciding; otherwise to zero, indicating successful operation.

C	APCH 10
C	APCH 20
C	SUBROUTINE APCH	APCH 30
C	APCH 40
C	PURPOSE	APCH 50
C	SET UP NORMAL EQUATIONS OF LEAST SQUARES FIT IN TERMS OF	APCH 60
C	CHEBYSHEV POLYNOMIALS FOR A GIVEN DISCRETE FUNCTION	APCH 70
C	APCH 80
C	USAGE	APCH 90
C	CALL DAPCH(DATI,N,IP,XD,XC,WCRK,IER)	APCH 100
C	APCH 110
C	DESCRIPTION OF PARAMETERS	APCH 120
C	DATI - VECTOR OF DIMENSION 3*N (OR DIMENSION 2*N+1)	APCH 130
C	CONTAINING THE GIVEN ARGUMENTS, FOLLOWED BY THE	APCH 140
C	FUNCTION VALUES AND N (RESPECTIVELY 1) WEIGHT	APCH 150
C	VALUES. THE CONTENT OF VECTOR DATI REMAINS	APCH 160
C	UNCHANGED.	APCH 170
C	DATI MUST BE OF DOUBLE PRECISION	APCH 180
C	N - NUMBER OF GIVEN POINTS	APCH 190
C	IP - DIMENSION OF LEAST SQUARES FIT, I.E. NUMBER OF	APCH 200
C	CHEBYSHEV POLYNOMIALS USED AS FUNDAMENTAL FUNCTIONS	APCH 210
C	IP SHOULD NOT EXCEED N	APCH 220
C	XC - RESULTANT MULTIPLICATIVE CONSTANT FOR LINEAR	APCH 230
C	TRANSFORMATION OF ARGUMENT RANGE	APCH 240
C	XC MUST BE DOUBLE PRECISION	APCH 250
C	XC - RESULTANT ADDITIVE CONSTANT FOR LINEAR	APCH 260
C	TRANSFORMATION OF ARGUMENT RANGE	APCH 270
C	XC MUST BE DOUBLE PRECISION	APCH 280
C	WCRK - WORKING STORAGE OF DIMENSION (IP+1)*(IP+2)/2	APCH 290
C	CA RETLNA WORK CONTAINS THE SYMMETRIC COEFFICIENT	APCH 300
C	MATRIX OF THE NORMAL EQUATIONS IN COMPRESSED FORM	APCH 310
C	FOLLOWS IMMEDIATELY BY RIGHT-HAND SIDE	APCH 320
C	AND SQUARE SUM OF FUNCTION VALUES	APCH 330
C	IER - RESULTING ERROR PARAMETER	APCH 340
C	IER = -1 MEANS FORMAL ERRORS IN DIMENSION	APCH 350
C	IER = 0 MEANS NO ERRORS	APCH 360
C	IER = 1 MEANS COINCIDING ARGUMENTS	APCH 370
C	APCH 380
C	REMARKS	APCH 390
C	AL WEIGHTS ARE USED IF THE VALUE OF DATI(2*N+1) IS	APCH 400
C	NOT POSITIVE	APCH 410
C	EXECUTION OF SUBROUTINE APCH IS A PREPARATORY STEP FOR	APCH 420
C	CALCULATION OF LEAST SQUARES FITS IN CHEBYSHEV POLYNOMIALS	APCH 430
C	IT SHOULD BE FOLLOWED BY EXECUTION OF SUBROUTINE APFS	APCH 440
C	APCH 450
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	APCH 460
C	APCH 470
C	PURPOSE	APCH 480
C	THE LEAST SQUARE FIT IS DETERMINED USING CHEBYSHEV	APCH 490
C	POLYNOMIALS AS FUNDAMENTAL FUNCTION SYSTEM.	APCH 500
C	THE METHOD IS DISCUSSED IN THE ARTICLE	APCH 510
C	P.T. BERTSIS, LEAST SQUARES FITTING TO IRREGULARLY SPACED	APCH 520
C	DATA, SIAM REVIEW, VOL. 6, ISS. 3, 1964, PP. 203-227.	APCH 530
C	APCH 540
C	SUBROUTINE APCH(DATI,N,IP,XD,XC,WCRK,IER)	APCH 550
C	APCH 560
C	APCH 570
C	APCH 580
C	APCH 590
C	APCH 600

C	APCH 610
C	APCH 620
C	APCH 630
C	APCH 640
C	APCH 650
C	APCH 660
C	APCH 670
C	APCH 680
C	APCH 690
C	APCH 700
C	APCH 710
C	APCH 720
C	APCH 730
C	APCH 740
C	APCH 750
C	APCH 760
C	APCH 770
C	APCH 780
C	APCH 790
C	APCH 800
C	APCH 810
C	APCH 820
C	APCH 830
C	APCH 840
C	APCH 850
C	APCH 860
C	APCH 870
C	APCH 880
C	APCH 890
C	APCH 900
C	APCH 910
C	APCH 920
C	APCH 930
C	APCH 940
C	APCH 950
C	APCH 960
C	APCH 970
C	APCH 980
C	APCH 990
C	APCH1000
C	APCH1010
C	APCH1020
C	APCH1030
C	APCH1040
C	APCH1050
C	APCH1060
C	APCH1070
C	APCH1080
C	APCH1090
C	APCH1100
C	APCH1110
C	APCH1120
C	APCH1130
C	APCH1140
C	APCH1150
C	APCH1160
C	APCH1170
C	APCH1180
C	APCH1190
C	APCH1200
C	APCH1210
C	APCH1220
C	APCH1230
C	APCH1240
C	APCH1250
C	APCH1260
C	APCH1270
C	APCH1280
C	APCH1290
C	APCH1300
C	APCH1310
C	APCH1320
C	APCH1330
C	APCH1340
C	APCH1350
C	APCH1360
C	APCH1370
C	APCH1380
C	APCH1390
C	APCH1400
C	APCH1410
C	APCH1420
C	APCH1430
C	APCH1440
C	APCH1450
C	APCH1460
C	APCH1470
C	APCH1480
C	APCH1490
C	APCH1500
C	APCH1510
C	APCH1520
C	APCH1530
C	APCH1540
C	APCH1550
C	APCH1560
C	APCH1570
C	APCH1580
C	DAPC 10
C	DAPC 20
C	DAPC 30
C	DAPC 40
C	DAPC 50
C	DAPC 60
C	DAPC 70
C	DAPC 80
C	DAPC 90
C	DAPC 100
C	DAPC 110
C	DAPC 120
C	DAPC 130
C	DAPC 140
C	DAPC 150
C	DAPC 160
C	DAPC 170
C	DAPC 180
C	DAPC 190
C	DAPC 200
C	DAPC 210
C	DAPC 220
C	DAPC 230
C	DAPC 240
C	DAPC 250
C	DAPC 260
C	DAPC 270
C	DAPC 280
C	DAPC 290
C	DAPC 300

```

C          ON RETURN WORK CONTAINS THE SYMMETRIC COEFFICIENT DAPC 310
C          MATRIX OF THE NORMAL EQUATIONS IN COMPRESSED FORM DAPC 320
C          FOLLOWED IMMEDIATELY BY RIGHT HAND SIDE DAPC 330
C          AND SQUARE SUM OF FUNCTION VALUES DAPC 340
C          WORK MUST BE OF DOUBLE PRECISION DAPC 350
C          IER - RESULTING ERROR PARAMETER DAPC 360
C          IER = -1 MEANS FORMAL ERRORS IN DIMENSION DAPC 370
C          IER = 0 MEANS NO ERRORS DAPC 380
C          IER = 1 MEANS COINCIDING ARGUMENTS DAPC 390
C
C          REMARKS DAPC 400
C          NO WEIGHTS ARE USED IF THE VALUE OF DAT1(2*N+1) IS DAPC 410
C          NOT POSITIVE. DAPC 420
C          EXECUTION OF SUBROUTINE DAPCH IS A PREPARATORY STEP FOR DAPC 430
C          CALCULATION OF LEAST SQUARES FITS IN CHEBYSHEV POLYNOMIALS DAPC 440
C          IT SHOULD BE FOLLOWED BY EXECUTION OF SUBROUTINE DAPFS DAPC 450
C
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DAPC 460
C          NONE DAPC 470
C
C          METHOD DAPC 480
C          THE LEAST SQUARE FIT IS DETERMINED USING CHEBYSHEV DAPC 490
C          POLYNOMIALS AS FUNDAMENTAL FUNCTION SYSTEM. DAPC 500
C          THE METHOD IS DISCUSSED IN THE ARTICLE DAPC 510
C          A.T.PERZISS, LEAST SQUARES FITTING TO IRREGULARLY SPACED DAPC 520
C          DATA, SIAM REVIEW, VOL.6, ISS.3, 1964, PP. 203-227. DAPC 530
C
C          ..... DAPC 540
C          SUBROUTINE DAPCH(DAT1,N,IP,XD,X0,XA,XE,XM,DF,T,SUM) DAPC 550
C
C          DIMENSIONED DUMMY VARIABLES DAPC 560
C          DIMENSION DAT1(11),WORK(1) DAPC 570
C          DOUBLE PRECISION DAT1,WORK,XD,X0,XA,XE,XM,DF,T,SUM DAPC 580
C
C          CHECK FOR FORMAL ERRORS IN SPECIFIED DIMENSIONS DAPC 590
C          IF(N-11)9,20,1 DAPC 600
C          1 IF(IP)19,19,2 DAPC 610
C
C          SEARCH SMALLEST AND LARGEST ARGUMENT DAPC 620
C          2 IF(IP-N)3,3,19 DAPC 630
C          3 XA=DAT1(1) DAPC 640
C          X0=XA DAPC 650
C          XE=0,00 DAPC 660
C          DO 7 I=1,N DAPC 670
C          XM=DAT1(I) DAPC 680
C          IF(XA-XM)5,5,4 DAPC 690
C          4 XA=XM DAPC 700
C          5 IF(XC-XM)6,7,7 DAPC 710
C          6 X0=XM DAPC 720
C          7 CONTINUE DAPC 730
C
C          INITIALIZE CALCULATION OF NORMAL EQUATIONS DAPC 740
C          XD=X0-XE DAPC 750
C          M=(IP*(IP+1))/2 DAPC 760
C          IEND=M+IP+1 DAPC 770
C          MT2=IP+IP DAPC 780
C          MT2M=MT2-1 DAPC 790
C
C          SET WORKING STORAGE AND RIGHT HAND SIDE TO ZERO DAPC 800
C          DO 8 I=1,IP DAPC 810
C          J=MT2-I DAPC 820
C          WORK(J)=0,00 DAPC 830
C          WORK(1)=0,00 DAPC 840
C          K=M+I DAPC 850
C          8 WORK(K)=0,00 DAPC 860
C
C          CHECK FOR DEGENERATE ARGUMENT RANGE DAPC 870
C          IF(XD)20,20,9 DAPC 880
C
C          CALCULATE CONSTANTS FOR REDUCTION OF ARGUMENTS DAPC 890
C          9 X0=(X0+XA)/XD DAPC 900
C          XD=2,00/XD DAPC 910
C          SUM=0,00 DAPC 920
C
C          START GREAT LOOP OVER ALL GIVEN POINTS DAPC 930
C          DO 15 I=1,N DAPC 940
C          T=DAT1(I)*XD+X0 DAPC 950
C          J=I+N DAPC 960
C          DF=DAT1(J) DAPC 970
C
C          CALCULATE AND STORE VALUES OF CHEBYSHEV POLYNOMIALS DAPC 980
C          FOR ARGUMENT T DAPC 990
C          XA=1,00 DAPC 1000
C          XM=T DAPC 1010
C          IF(ODAT1(2*N+1))11,11,10 DAPC 1020
C          10 J=J+N DAPC 1030
C          XA=DAT1(J) DAPC 1040
C          XM=T*XA DAPC 1050
C          11 T=T+T DAPC 1060
C          SUM=SUM+DF*DF*XA DAPC 1070
C          DF=DF*DF DAPC 1080
C          J=J-1 DAPC 1090
C          12 K=M+J DAPC 1100
C          WORK(K)=WORK(K)+DF*XA DAPC 1110
C          13 WORK(J)=WORK(J)+XA DAPC 1120
C          IF(J-MT2N)14,15,15 DAPC 1130
C          14 J=J-1 DAPC 1140
C          XE=T*XM-XA DAPC 1150
C          XA=XM DAPC 1160
C          XM=XE DAPC 1170
C          IF(J-IP)12,12,13 DAPC 1180
C          15 CONTINUE DAPC 1190
C          WORK(IEND)=SUM+SUM DAPC 1200
C
C          CALCULATE MATRIX OF NORMAL EQUATIONS DAPC 1210
C          LL=M DAPC 1220
C          KK=MT2M DAPC 1230
C          JJ=1 DAPC 1240
C          K=KK DAPC 1250
C          DO 18 J=1,M DAPC 1260
C          WORK(LL)=WORK(K)+WORK(JJ) DAPC 1270
C          LL=LL-1 DAPC 1280
C          IF(K-JJ)16,16,17 DAPC 1290
C          16 KK=KK-2 DAPC 1300
C          K=KK DAPC 1310
C          JJ=1 DAPC 1320
C          GOTO 18 DAPC 1330
C          17 JJ=JJ+1 DAPC 1340
C          K=K-1 DAPC 1350
C          18 CONTINUE DAPC 1360
C          IER=0 DAPC 1370
C          RETURN DAPC 1380
C
C          ERROR RETURN IN CASE OF FORMAL ERRORS DAPC 1390
C          19 IER=-1 DAPC 1400
C          RETURN DAPC 1410
C
C          ERROR RETURN IN CASE OF COINCIDING ARGUMENTS DAPC 1420
C          20 IER=1 DAPC 1430
C          RETURN DAPC 1440
C          END DAPC 1450

```

Subroutines ARAT and DARAT

These subroutines compute the best rational approximation $P(x)/Q(x)$ to a discrete function, $f(x)$, in the least-squares sense. The argument range should be the interval $[-1, +1]$.

Subroutines FRAT and DFRAT are an integral part of the procedure and have no independent meaning.

1. Mathematical background

Given positive integers ip , iq , and n , arguments x_i , function values f_i , and positive weights w_i , $i=1, 2, \dots, n$, the problem is to determine the coefficients of the polynomials

$$P(x) = p_1 + p_2x + \dots + p_{ip}x^{ip-1}$$

$$Q(x) = q_1 + q_2x + \dots + q_{iq}x^{iq-1}$$

such that

$$F = \sum_{i=1}^n w_i \left[f_i - \frac{P(x_i)}{Q(x_i)} \right]^2 = \text{minimum} \quad (1)$$

A direct approach to the problem (1) leads to a system of nonlinear equations. Therefore the problem is reformulated in the following way.

Let $P_0(x)$ and $Q_0(x)$ be an approximate solution to (1). The problem is then to determine increments $\Delta P_0(x)$ and $\Delta Q_0(x)$ such that

$$F = \sum_{i=1}^n w_i \left[f_i - \frac{P_0(x_i) + \Delta P_0(x_i)}{Q_0(x_i) + \Delta Q_0(x_i)} \right]^2 = \text{minimum} \quad (1')$$

Without loss of generality it may be assumed that the constant term of Q_0 remains unchanged, that is that the constant term of ΔQ_0 is zero, since numerator and denominator of the rational approximation are determined only up to a common factor.

Linearizing $\frac{P_0 + \Delta P_0}{Q_0 + \Delta Q_0}$ with respect to ΔP_0 and ΔQ_0 ,

$$\frac{P_0 + \Delta P_0}{Q_0 + \Delta Q_0} \approx \frac{P_0}{Q_0} \left[1 + \frac{\Delta P_0}{P_0} - \frac{\Delta Q_0}{Q_0} \right] \quad (2)$$

and using (2) in (1') gives the approximation $F \approx F_0$ where

$$F_o = \sum_{i=1}^n \frac{w_i}{Q_o(x_i)^2} \left[f_i Q_o(x_i) - P_o(x_i) - \Delta P_o(x_i) + \frac{P_o(x_i)}{Q_o(x_i)} \Delta Q_o(x_i) \right]^2$$

Defining

$$f_i^* = f_i Q_o(x_i) - P_o(x_i)$$

$$w_i^* = w_i / Q_o(x_i)^2$$

and a set of functions

$$g_k(x) = -\frac{P_o(x)}{Q_o(x)} x^k \quad k=1, 2, \dots, iq-1$$

$$g_k(x) = x^{k-iq} \quad k=iq, iq+1, \dots, iq+ip-1$$

we may write

$$F_o = \sum_{i=1}^n w_i^* \left[f_i^* - g(x_i) \right]^2$$

where

$$g(x) = \sum_{i=1}^m c_i g_i(x) \quad m=iq+ip-1$$

and the c_i are the coefficients of $\Delta Q_o(x)$ and $\Delta P_o(x)$:

$$\Delta Q_o(x) = \sum_{i=1}^{iq-1} c_i x^i$$

$$\Delta P_o(x) = \sum_{i=iq}^m c_i x^{i-iq}$$

Now the coefficients c_i are determined so that $F_o =$ minimum. This is a problem of the type discussed in APLL with function values f_i^* , weights w_i^* and fundamental functions $g_i(x)$, and leads to a system of linear equations

$$AC = R$$

with symmetric positive semi-definite coefficient matrix A (see APLL writeup for a description of A and R).

In subroutine ARAT, APLL is used to set up the normal equations $AC = R$, and APFS is used to solve the system for the coefficient vector C.

Given a solution ΔP_o and ΔQ_o to the problem $F_o =$ minimum, a new approximation is formed using

$$P_1 = P_o + \Delta P_o$$

$$Q_1 = Q_o + \Delta Q_o$$

In general, given approximations P_k and Q_k , increments ΔP_k and ΔQ_k are determined as indicated above, and the next approximations are

$$P_{k+1} = P_k + \Delta P_k$$

$$Q_{k+1} = Q_k + \Delta Q_k$$

(3)

This process is started with some initial approximation (usually with $P_o(x) \equiv 0$, $Q_o(x) \equiv 1$) and is stopped when there is indication of convergence (see below).

a. Refinement of the calculation procedure

The above approach has several defects:

(1) There is no guarantee for improvement of the rational fit obtained with successive iterations if the initial approximation is not close enough to a true solution.

(2) Zeros may come into the denominator, causing a complete breakdown of the procedure.

(3) The normal equations of the linearized problem are badly ill-conditioned if monomials are used as fundamental functions.

The first difficulty is resolved using an approach suggested by D. Braess in reference (1). Let

$$S_k = \sum_{i=1}^n w_i \left[f_i - \frac{P_k(x_i)}{Q_k(x_i)} \right]^2$$

Then instead of using the relations (3) we use

$$P_{k+1} = P_k + r \Delta P_k$$

$$Q_{k+1} = Q_k + r \Delta Q_k$$

where the relaxation factor r is chosen so that S_{k+1} is close to a minimum when regarded as a function of r , and $S_{k+1} \leq S_k$. If this cannot be done, the error parameter IER is set to IER = 1, and the process is stopped. Choosing r sufficiently small also prevents zeros from entering the denominator.

The condition of the normal equations is improved remarkably by using Chebyshev polynomials $T_k(x)$ instead of monomials x^k as fundamental functions; that is, the numerator and denominator are calculated in terms of their Chebyshev expansions. The argument range is assumed to be $(-1, +1)$.

If it turns out that the normal equations are still ill-conditioned, the diagonal elements of the coefficient matrix are slightly increased. This modification was suggested by D. W. Marquardt in reference (2). In this case again the calculated increment is modified by a relaxation factor r ; but now r may take on values even greater than 1 if this does not imply zeros coming into the denominator.

b. Convergence

Let T_k denote the sum of the absolute values of the coefficients of $P_k(x)$ and $Q_k(x)$. Then, assuming that the Marquardt modification was not needed, the process is stopped if either

$$\frac{S_k - S_{k+1}}{S_{k+1}} \leq r \epsilon$$

or

$$\frac{|T_k - T_{k+1}|}{T_{k+1}} \leq r \epsilon$$

or

$$S_{k+1} \leq \eta T_{k+1}$$

Here $\epsilon = 10^{-5}$ and $\eta = 10^{-11}$. If the diagonal terms of the coefficient matrix of the normal equations were increased, only the last test is applied. If none of these conditions is met, the process is repeated until the maximum number of iterations $k = \text{LIMIT}$ is reached (LIMIT is set to 20 in ARAT).

c. Remarks

(1) The user must specify the dimension of the denominator and of the numerator of the rational approximation he wants to calculate. The calculation procedure is somewhat sensitive to getting adequate dimensions. If the specified dimensions are

unrealistically high, the calculation procedure may break down due to a very poor convergence. In this case it is best to repeat the calculation with decreased dimensions.

(2) The initial approximation which the user has the option to specify must be such that the denominator is free of zeros over the range of approximation $(-1, +1)$. The standard initial approximation is $P(x) \equiv 0$ and $Q(x) \equiv 1$.

(3) The arguments of the given discrete functions should be reduced to the interval $(-1, +1)$. Arguments absolutely greater than 1 cause error propagation in the calculation of Chebyshev polynomials and may produce dubious results.

(4) Numerical experience has shown that the dimensions used in single precision should not exceed 5, and in double precision should not be above 10.

(5) Transformation of Chebyshev expansions to ordinary polynomials normally results in severe loss of accuracy. Therefore, no attempt is made to return the polynomial coefficients. This transformation may be easily accomplished through subroutines TCNP and DTCNP. The calculated Chebyshev expansions may be evaluated for a specified argument using subroutines CNPS and DCNPS.

2. Programming considerations

Arrays passed to subroutines ARAT and DARAT are DATI, WORK, and P. DATI contains the given data set to be approximated, consisting of n arguments x_1, \dots, x_n followed by the corresponding function values f_1, \dots, f_n and by weights w_1, \dots, w_n . Constant weighting (value one) is implied if DATI $(2n + 1)$ contains a nonpositive value.

WORK is used as working storage. On return it contains the values of the numerator in WORK $(n + 1)$ up to WORK $(2n)$ and the values of the denominator in WORK $(2n + 1)$ up to WORK $(3n)$. The storage positions WORK (1) up to WORK (n) and WORK $(3n + 1)$ up to WORK $(4n)$ are used to record the current nonmoderated values of change of numerator and denominator respectively. The remaining $(ip + iq)(ip + iq + 1) + 1$ storage locations of WORK are used to store the normal equations in compressed form twice, in a working area as well as in a save area. This is necessary to avoid recalculation of the normal equations in case of an ill-conditioned coefficient matrix.

P is a vector of dimension $ip + iq$ containing the calculated rational approximation on return. The coefficients of the Chebyshev expansion of the denominator are stored first, immediately followed by the coefficients of the Chebyshev expansion of the numerator. Coefficients are ordered from low to

high. P may also be used as an input array containing the initial approximation in terms of its Chebyshev expansions (with same ordering) optionally.

The normal equations are generated internally by means of subroutines APLL and DAPLL in the storage allocation scheme which is required by subroutines APFS and DAPFS. Subroutines FRAT and DFRAT are simply the interface between subroutines ARAT, DARAT and APLL, DAPLL used for handling the given data set and the specified fundamental functions.

The error parameter IER gives an indication of success or failure of the procedure.

- IER = 0 The process converged in the sense mentioned above.
- IER = -1 Formal error occurred in specified dimensions or initial approximations such as violation of any of the restrictions $n > 0$, $ip > 0$, $iq > 0$, $n \geq ip + iq$ or $Q_0(x) \neq 0$ on $(-1, 1)$. The latter could occur only if an optional initial approximation was used.
- IER = 1 The Marquardt modification was tried LIMIT times without success, or a suitable relaxation factor could not be found.
- IER = 2 The process has not converged after LIMIT steps.

In all cases where $IER \geq 0$ there is a calculated approximation available, but only in the case $IER = 0$ is there strong indication that this approximation is close to the best rational fit in the least-squares sense.

For reference see:

- (1) D. Braess, "Ueber Daempfung bei Minimalisierungsverfahren", Computing (1966) vol. 1, ed. 3, pp 264 - 272.
- (2) D. W. Marquardt, "An algorithm for least-squares estimation of non-linear parameters", JSIAM (1963), vol. II, ed. 2, pp. 431- 441.

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C ..... ARAT 10
C ..... ARAT 20
C ..... ARAT 30
C SUBROUTINE ARAT AFAT 40
C ..... ARAT 50
C PURPOSE AFAT 60
C CALCULATE BEST RATIONAL APPROXIMATION OF A DISCRETE AFAT 70
C FUNCTION IN THE LEAST SQUARES SENSE ARAT 80
C ..... ARAT 90
C USAGE AFAT 100
C CALL ARAT(DATI,N,WORK,P,IP,IQ,IER) ARAT 110
C ..... ARAT 120
C DESCRIPTION OF PARAMETERS ARAT 130
C DATI - INDDIMENSIONAL ARRAY WITH 3 COLUMNS AND N ROWS ARAT 140
C THE FIRST COLUMN MUST CONTAIN THE GIVEN ARGUMENTS, ARAT 150
C THE SECOND COLUMN THE GIVEN FUNCTION VALUES AND ARAT 160
C THE THIRD COLUMN THE GIVEN WEIGHTS IF ANY. ARAT 170
C IF NO WEIGHTS ARE TO BE USED THEN THE THIRD ARAT 180
C COLUMN MAY BE DROPPED, EXCEPT THE FIRST ELEMENT ARAT 190
C WHICH MUST CONTAIN A NONPOSITIVE VALUE ARAT 200
C N - NUMBER OF NODES OF THE GIVEN DISCRETE FUNCTION ARAT 210
C WORK - WORKING STORAGE WHICH IS OF DIMENSION ARAT 220
C (IP+IQ)*(IP+IQ+1)+4*N+1 AT LEAST. ARAT 230
C ON RETURN THE VALUES OF THE NUMERATOR ARE CONTAINED ARAT 240
C IN WORK(N+1) UP TO WORK(2*N), WHILE THE VALUES OF ARAT 250
C THE DENOMINATOR ARE STORED IN WORK(2*N+1) UP TO ARAT 260
C WORK(3*N) ARAT 270
C P - RESULTANT COEFFICIENT VECTOR OF DENOMINATOR AND ARAT 280
C NUMERATOR. THE DENOMINATOR IS STORED IN FIRST IQ ARAT 290
C LOCATIONS, THE NUMERATOR IN THE FOLLOWING IP ARAT 300
C LOCATIONS. ARAT 310
C COEFFICIENTS ARE ORDERED FROM LOW TO HIGH. ARAT 320
C IP - DIMENSION OF THE NUMERATOR (INPUT VALUE) ARAT 330

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C IO - DIMENSION OF THE DENOMINATOR (INPUT VALUE) ARAT 340
C IER - RESULTANT ERROR PARAMETER ARAT 350
C IER = -1 MEANS FORMAL ERRORS ARAT 360
C IER = 0 MEANS NO ERRORS ARAT 370
C IER = 1,2 MEANS POOR CONVERGENCE OF ITERATION ARAT 380
C IER IS ALSO USED AS INPUT VALUE AFAT 390
C A NONZERO INPUT VALUE INDICATES AVAILABILITY OF AN ARAT 400
C INITIAL APPROXIMATION STORED IN P ARAT 410
C ..... ARAT 420
C REMARKS ARAT 430
C THE COEFFICIENT VECTORS OF THE DENOMINATOR AND NUMERATOR ARAT 440
C OF THE RATIONAL APPROXIMATION ARE BOTH STORED IN P ARAT 450
C STARTING WITH LOW POWERS (DENOMINATOR FIRST). ARAT 460
C IP+IQ MUST NOT EXCEED N. ALL THREE VALUES MUST BE POSITIVE. ARAT 470
C SINCE CHEBYSHEV POLYNOMIALS ARE USED AS FUNDAMENTAL ARAT 480
C FUNCTIONS, THE ARGUMENTS SHOULD BE REDUCED TO THE INTERVAL ARAT 490
C (-1,1). THIS CAN ALWAYS BE ACCOMPLISHED BY MEANS OF A LINEAR ARAT 500
C TRANSFORMATION OF THE ORIGINALLY GIVEN ARGUMENTS. ARAT 510
C IF A FIT IN OTHER FUNCTIONS IS REQUIRED, CNP AND CNPS MUST ARAT 520
C BE REPLACED BY SUBROUTINES WHICH ARE OF ANALOGOUS DESIGN. ARAT 530
C ..... ARAT 540
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED ARAT 550
C APLL, APFS, FRAT, CNPS, CNP ARAT 560
C CNP IS REQUIRED WITHIN FRAT ARAT 570
C ..... ARAT 580
C METHOD ARAT 590
C THE ITERATIVE SCHEME USED FOR CALCULATION OF THE ARAT 600
C APPROXIMATION IS REPEATED SOLUTION OF THE NORMAL EQUATIONS ARAT 610
C WHICH ARE OBTAINED BY LINEARIZATION. ARAT 620
C A REFINED TECHNIQUE OF THIS LINEAR LEAST SQUARES APPROACH ARAT 630
C IS USED WHICH GUARANTEES THAT THE DENOMINATOR IS FREE OF ARAT 640
C ZERGES WITHIN THE APPROXIMATION INTERVAL. ARAT 650
C FOR REFERENCE SEE ARAT 660
C D. BRAESS, UEBER DAEMPFGUNG BEI MINIMALISIERUNGSVERFAHREN, ARAT 670
C COMPUTING(1966), VOL.1, ED.3, PP.264-272. ARAT 680
C D.W. MARQUARDT, AN ALGORITHM FOR LEAST-SQUARES ESTIMATION ARAT 690
C OF NONLINEAR PARAMETERS, ARAT 700
C JSIAM(1963), VOL.11, ED.2, PP.431-441. ARAT 710
C ..... ARAT 720
C SUBROUTINE ARAT(DATI,N,WORK,P,IP,IQ,IEF) ARAT 730
C ..... ARAT 740
C EXTERNAL FRAT ARAT 750
C ..... ARAT 760
C DIMENSIONED LOCAL VARIABLE ARAT 770
C DIMENSION IER(3) ARAT 780
C ..... ARAT 790
C DIMENSIONED DUMMY VARIABLES ARAT 800
C DIMENSION DATI(1),WORK(1),P(1) ARAT 810
C ..... ARAT 820
C INITIALIZE TESTVALUES ARAT 830
C LIMIT=20 ARAT 840
C ETA =1.E-11 ARAT 850
C EPS=1.E-5 ARAT 860
C ..... ARAT 870
C CHECK FOR FORMAL ERRORS ARAT 880
C IF(N)4,4,1 ARAT 890
C 1 IF(IP)4,4,2 ARAT 900
C 2 IF(IQ)4,4,3 ARAT 910
C 3 IPQ=IP+IQ ARAT 920
C IF(N-IPQ)4,5,5 ARAT 930
C ..... ARAT 940
C ERROR RETURN IN CASE OF FORMAL ERRORS ARAT 950
C 4 IER=-1 ARAT 960
C RETURN ARAT 970
C ..... ARAT 980
C INITIALIZE ITERATION PROCESS ARAT 990
C 5 KOUNT=0 ARAT 1000
C IERV(2)=IP ARAT 1010
C IERV(3)=IQ ARAT 1020
C NDP=N*IP ARAT 1030
C NNE=NDP+NDP ARAT 1040
C IX=IPQ-1 ARAT 1050
C IQP1=IQ+1 ARAT 1060
C IRHS=NNE+IPQ*IX/2 ARAT 1070
C IEND=IRHS+IX ARAT 1080
C ..... ARAT 1090
C TEST FOR AVAILABILITY OF AN INITIAL APPROXIMATION ARAT 1100
C IF(IER)6,6,8 ARAT 1110
C ..... ARAT 1120
C INITIALIZE NUMERATOR AND DENOMINATOR ARAT 1130
C 6 DO 7 I=2,IPQ ARAT 1140
C 7 P(I)=0. ARAT 1150
C P(I)=1. ARAT 1160
C ..... ARAT 1170
C CALCULATE VALUES OF NUMERATOR AND DENOMINATOR FOR INITIAL ARAT 1180
C APPROXIMATION ARAT 1190
C 8 DO 9 J=1,N ARAT 1200
C T=DATI(J) ARAT 1210
C I=J+N ARAT 1220
C CALL CNPS(WORK(I),T,P(IQP1),IP) ARAT 1230
C K=I*N ARAT 1240
C 9 CALL CNPS(WORK(K),T,P,IQ) ARAT 1250
C ..... ARAT 1260
C SET UP NORMAL EQUATIONS (MAIN LOOP OF ITERATION) ARAT 1270
C 10 CALL APLL(FRAT,N,IX,WORK,WORK(IEND+1),DATI,IERV) ARAT 1280
C ..... ARAT 1290
C CHECK FOR ZERO DENOMINATOR ARAT 1300
C IF(IEFV(1))14,11,4 ARAT 1310
C 11 INCR=0 ARAT 1320
C RELAX=.2. ARAT 1330
C ..... ARAT 1340
C RESTORE MATRIX IN WORKING STORAGE ARAT 1350
C 12 J=IEND ARAT 1360
C DO 13 I=NNE,IEND ARAT 1370
C J=J+1 ARAT 1380
C 13 WORK(I)=WORK(J) ARAT 1390
C IF(KOUNT)14,14,15 ARAT 1400
C ..... ARAT 1410
C SAVE SQUARE SUM OF ERRORS ARAT 1420
C 14 OSUM=WORK(IEND) ARAT 1430
C DIAG=OSUM*EPS ARAT 1440
C K=IQ ARAT 1450
C ..... ARAT 1460
C ADD CONSTANT TO DIAGONAL ARAT 1470
C IF(WORK(NNE))17,17,19 ARAT 1480
C 15 IF(INCR)19,19,16 ARAT 1490
C 16 K=IPQ ARAT 1500
C 17 J=NNE-1 ARAT 1510
C DO 18 I=1,K ARAT 1520
C WORK(J)=WORK(J)+DIAG ARAT 1530
C 18 J=J+1 ARAT 1540
C ..... ARAT 1550
C SOLVE NORMAL EQUATIONS ARAT 1560
C 19 CALL APFS(WORK(NNE),IX,IPES,1,EPS,ETA,IER) ARAT 1570
C ..... ARAT 1580
C CHECK FOR FAILURE OF EQUATION SOLVER ARAT 1590
C ..... ARAT 1600
C ..... ARAT 1610
C ..... ARAT 1620

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```

C          DATA 10          CALL DCNPS(WORK(I),T,P(IQI),IP)
C          DATA 20          K=I+N
C          DATA 30          9 CALL DCNPS(WORK(K),T,P,IC)
C          DATA 40          C
C          DATA 50          C          SET UP NORMAL EQUATIONS (MAIN LOOP OF ITERATION)
C          DATA 60          10 CALL DAPLL(DFRAT,N,IX,WURK,WORK(IEND+1),DAT,I,ERV)
C          DATA 70          C
C          DATA 80          C          CHECK FOR ZERO DENOMINATOR
C          DATA 90          IF(IERV(I))4,11,4
C          DATA 100         11 INCR=0
C          DATA 110         RELAX=2.00
C          DATA 120         C
C          DATA 130         C          RESTORE MATRIX IN WORKING STORAGE
C          DATA 140         12 J=IEND
C          DATA 150         DO 13 I=NE,IEND
C          DATA 160         DO 13 J=I
C          DATA 170         13 WGRK(I)=WGRK(J)
C          DATA 180         IF(KOUNT)14,14,15
C          DATA 190         C
C          DATA 200         C          SAVE SQUARE SUM OF ERRORS
C          DATA 210         14 OSUM=WGRK(IEND)
C          DATA 220         DIAG=OSUM*EPS
C          DATA 230         K=IQ
C          DATA 240         C
C          DATA 250         C          ADD CONSTANT TO DIAGONAL
C          DATA 260         IF(WGRK(NNE))17,17,19
C          DATA 270         15 IF(INCR)19,19,16
C          DATA 280         16 K=IPQ
C          DATA 290         17 J=NNE-1
C          DATA 300         DO 18 I=1,K
C          DATA 310         WGRK(J)=WGRK(J)+DIAG
C          DATA 320         18 J=J+1
C          DATA 330         C
C          DATA 340         C          SOLVE NORMAL EQUATIONS
C          DATA 350         19 CALL DAPFS(WORK(NNE),IX,IRES,1,EPS,ETA,IER)
C          DATA 360         C
C          DATA 370         C          CHECK FOR FAILURE OF EQUATION SOLVER
C          DATA 380         IF(IRES)4,4,20
C          DATA 390         C
C          DATA 400         C          TEST FOR DEFECTIVE NORMAL EQUATIONS
C          DATA 410         20 IF(IRES-IX)21,24,24
C          DATA 420         21 IF(INCR)22,22,23
C          DATA 430         22 DIAG=DIAG+0.125*DIAG
C          DATA 440         23 DIAG=DIAG+DIAG
C          DATA 450         INCR=INCR+1
C          DATA 460         C
C          DATA 470         C          START WITH OVER RELAXATION
C          DATA 480         RELAX=8.00
C          DATA 490         IF(INCF-LIMIT)12,45,45
C          DATA 500         C
C          DATA 510         C          CALCULATE VALUES OF CHANGE OF NUMERATOR AND DENOMINATOR
C          DATA 520         24 L=NDP
C          DATA 530         J=NNE+IRES*(IRES-1)/2-1
C          DATA 540         K=J+IQ
C          DATA 550         WGRK(J)=0.00
C          DATA 560         IRQ=IQ
C          DATA 570         IRP=IRES-IQ+1
C          DATA 580         IF(IQ)25,26,26
C          DATA 590         25 IRO=IRES+1
C          DATA 600         26 DO 29 I=1,N
C          DATA 610         T=DAT(I)
C          DATA 620         WGRK(I)=0.00
C          DATA 630         CALL DCNPS(WORK(I),T,WGRK(K),IRP)
C          DATA 640         M=L+N
C          DATA 650         CALL DCNPS(WORK(M),T,WGRK(J),IRQ)
C          DATA 660         IF(WORK(M)*WGRK(L))27,29,29
C          DATA 670         27 SUM=WGRK(L)+WGRK(M)
C          DATA 680         IF(RELAX+SUM)29,29,28
C          DATA 690         28 RELAX=SUM
C          DATA 700         29 L=L+1
C          DATA 710         C
C          DATA 720         C          MODIFY RELAXATION FACTOR IF NECESSARY
C          DATA 730         SSGE=OSUM
C          DATA 740         ITER=LIMIT
C          DATA 750         30 SUM=0.00
C          DATA 760         RELAX=RELAX*0.500
C          DATA 770         DO 32 I=1,N
C          DATA 780         M=I+N
C          DATA 790         K=M+N
C          DATA 800         L=K+N
C          DATA 810         SAVE=DAT(I)*M-(WGRK(M)+RELAX*WGRK(I))/(WGRK(K)+RELAX*WGRK(L))
C          DATA 820         SAVE=SAVE+SAVE
C          DATA 830         IF(DAT(I(NDP)))32,32,31
C          DATA 840         31 SAVE=SAVE+DAT(I)
C          DATA 850         32 SUM=SUM+SAVE
C          DATA 860         IF(ITER)45,33,33
C          DATA 870         33 ITER=ITER-1
C          DATA 880         IF(SUM-OSUM)34,37,35
C          DATA 890         34 CSUM=SUM
C          DATA 900         GOTO 30
C          DATA 910         C
C          DATA 920         C          TEST FOR IMPROVEMENT
C          DATA 930         35 IF(OSUM-SSGE)36,30,30
C          DATA 940         36 RELAX=RELAX+RELAX
C          DATA 950         37 T=0.
C          DATA 960         SAVE=0.00
C          DATA 970         K=IRES-1
C          DATA 980         DO 38 I=2,K
C          DATA 990         J=J+1
C          DATA 1000        T=T+DABS(P(I))
C          DATA 1010        P(I)=P(I)+RELAX*WGRK(J)
C          DATA 1020        38 SAVE=SAVE+DABS(P(I))
C          DATA 1030        C
C          DATA 1040        C          UPDATE CURRENT VALUES OF NUMERATOR AND DENOMINATOR
C          DATA 1050        DO 39 I=1,N
C          DATA 1060        J=I+N
C          DATA 1070        K=J+N
C          DATA 1080        L=K+N
C          DATA 1090        WGRK(J)=WGRK(J)+RELAX*WGRK(I)
C          DATA 1100        39 WGRK(K)=WGRK(K)+RELAX*WGRK(L)
C          DATA 1110        C
C          DATA 1120        C          TEST FOR CONVERGENCE
C          DATA 1130        IF(INCR)40,40,42
C          DATA 1140        40 IF(SSGE-OSUM-RELAX*OSUM+DBLE(EPS))46,46,41
C          DATA 1150        41 IF(DABS(T-SAVE)-RELAX*SAVE+DBLE(EPS))46,46,42
C          DATA 1160        42 IF(OSUM-SAVE+DBLE(ETA))46,46,43
C          DATA 1170        43 KOUNT=KOUNT+1
C          DATA 1180        IF(KOUNT-LIMIT)10,44,44
C          DATA 1190        C
C          DATA 1200        C          ERROP RETURN IN CASE OF POOR CONVERGENCE
C          DATA 1210        44 IER=2
C          DATA 1220        RETURN
C          DATA 1230        45 IER=1
C          DATA 1240        RETURN
C          DATA 1250        C
C          DATA 1260        C          NORMAL RETURN
C          DATA 1270        46 IER=0
C          DATA 1280        RETURN
C          DATA 1290        END

```

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C ..... DFRA 10
C ..... DFRA 20
C ..... DFRA 30
C ..... DFRA 40
C ..... DFRA 50
C ..... DFRA 60
C ..... DFRA 70
C ..... DFRA 80
C ..... DFRA 90
C ..... DFRA 100
C ..... DFRA 110
C ..... DFRA 120
C ..... DFRA 130
C ..... DFRA 140
C ..... DFRA 150
C ..... DFRA 160
C ..... DFRA 170
C ..... DFRA 180
C ..... DFRA 190
C ..... DFRA 200
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C ..... DFRA 390
C ..... DFRA 400
C ..... DFRA 410
C ..... DFRA 420
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C ..... DFRA 600
C ..... DFRA 610
C ..... DFRA 620
C ..... DFRA 630
C ..... DFRA 640
C ..... DFRA 650
C ..... DFRA 660
C ..... DFRA 670
C ..... DFRA 680
C ..... DFRA 690
C ..... DFRA 700
C ..... DFRA 710
C ..... DFRA 720
C ..... DFRA 730
C ..... DFRA 740
C ..... DFRA 750
C ..... DFRA 760
C ..... DFRA 770
C ..... DFRA 780
C ..... DFRA 790
C ..... DFRA 800
C ..... DFRA 810
C ..... DFRA 820
C ..... DFRA 830
C ..... DFRA 840
C ..... DFRA 850
C ..... DFRA 860
C ..... DFRA 870
C ..... DFRA 880
C ..... DFRA 890
C ..... DFRA 900
C ..... DFRA 910
C ..... DFRA 920
C ..... DFRA 930
C ..... DFRA 940
C ..... DFRA 950
C ..... DFRA 960
C ..... DFRA 970
C ..... DFRA 980
C ..... DFRA 990
C ..... DFRA1000
C ..... DFRA1010
C ..... DFRA1020
C ..... DFRA1030
C ..... DFRA1040
SUBROUTINE DFRAT
PURPOSE
  DFRAT IS USED FOR HANDLING OF DATA AND FUNDAMENTAL FUNCTIONS
  WITH RATIONAL APPROXIMATION. IT IS A SUBSTANTIAL PART OF
  RATIONAL APPROXIMATION AND HAS NO MEANING INDEPENDENTLY
USAGE
  CALL DFRAT(I,N,M,P,DATI,WGT,IER)
DESCRIPTION OF PARAMETERS
  I - SUBSCRIPT OF CURRENT DATA POINT
  N - NUMBER OF ALL DATA POINTS
  M - NUMBER OF FUNDAMENTAL FUNCTIONS USED
  P - ARRAY OF DIMENSION M*1 AT LEAST, WHICH CONTAINS
  ON RETURN THE VALUES OF THE M FUNDAMENTAL
  FUNCTIONS, FOLLOWED BY CURRENT FUNCTION VALUE
  P MUST BE OF DOUBLE PRECISION
  DATI - ARRAY CONTAINING GIVEN N ARGUMENTS, FOLLOWED
  BY N FUNCTION VALUES AND FINALLY BY 1 RESPECTIVELY
  N WEIGHT VALUES
  DATI MUST BE OF DOUBLE PRECISION
  WGT - RESULTANT WEIGHT FACTOR USED FOR I-TH TERM
  WGT MUST BE OF DOUBLE PRECISION
  IER - RESULTANT ERROR PARAMETER, COMBINED WITH INPUT
  VALUES FFP CONTROL
  IER(2) MEANS DIMENSION OF NUMERATOR
  IER(3) MEANS DIMENSION OF DENOMINATOR
  IER(1) IS USED AS RESULTANT ERROR PARAMETER,
  IER(1) = 0 IN CASE OF NO ERRORS
  IER(1) = 1 OTHERWISE (ZERO DENOMINATOR)
REMARKS
  VECTOR IER IS USED FOR COMMUNICATION BETWEEN DFRAT AND DFRAT
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  DCOMP
METHOD
  CF. MATHEMATICAL DESCRIPTION OF SUBROUTINE ARAT
.....
SUBROUTINE DFRAT(I,N,M,P,DATI,WGT,IER)
  DIMENSIONED DUMMY VARIABLES
  DIMENSION P(1),DATI(1),IER(1)
  DOUBLE PRECISION P,DATI,WGT,T,F,FNUM,FDEN
  INITIALIZATION
  IP=IER(2)
  IQ=IER(3)
  IQM1=IQ-1
  IPQ=IP+IQ
  LOOK UP ARGUMENT, FUNCTION VALUE AND WEIGHT
  LOOK UP NUMERATOR AND DENOMINATOR
  T=DATI(I)
  J=I+N
  F=DATI(J)
  FNUM=P(J)
  J=J+N
  WGT=1.00
  IF(DATI(2*N+1))2,2,1
1 WGT=DATI(J)
2 FDEN=P(J)
  CALCULATE FUNCTION VALUE USED
  F=F*FDEN-FNUM
  CHECK FOR ZERO DENOMINATOR
  IF(FDEN)4,3,4
  ERROR RETURN IN CASE OF ZERO DENOMINATOR
3 IER(1)=1
  RETURN
  CALCULATE WEIGHT FACTORS USED
4 WGT=WGT/(FDEN*FDEN)
  FNUM=-FNUM/FDEN
  CALCULATE FUNDAMENTAL FUNCTIONS
  J=IQM1
  IF(IP=10)6,5,5
  J=IP-1
6 CALL DCOMP(IQ,IQ,T,J)
  STORE VALUES OF DENOMINATOR FUNDAMENTAL FUNCTIONS
7 IF(IQM1)10,10,8
8 DO 9 II=1,IQM1
  J=II+IQ
9 P(II)=P(J)*FNUM
  STORE FUNCTION VALUE
10 P(IPQ)=F
  NORMAL RETURN
  IER(1)=0
  RETURN
END

```

Subroutines APLL and DAPLL

These subroutines set up the normal equations for a linear least-squares fit to a given discrete function. APLL is a preparatory step for the calculation of the least-squares fit. Normally it is followed by subroutine APFS.

A user-coded external subroutine must be supplied to compute the values of the fundamental functions.

1. Mathematical background

Let $f(x)$, $g_i(x)$, $i = 1, 2, \dots, m$, and $w(x) > 0$ be functions defined for $x = x_1, x_2, \dots, x_n$ (the x_i

may be vectors as well as scalars). The problem is to determine the coefficients c_i of the linear combination

$$p(x) = \sum_{i=1}^m c_i g_i(x)$$

such that

$$\sum_{k=1}^n w(x_k) (f(x_k) - p(x_k))^2 = \text{minimum}$$

This problem leads to a system of linear equations $AC = R$, where C is the vector of unknown coefficients, A is the m by m symmetric positive definite matrix with elements

$$a_{jk} = \sum_{i=1}^n w(x_i) g_j(x_i) g_k(x_i)$$

and R is an m -dimensional vector with elements

$$r_j = \sum_{i=1}^n w(x_i) f(x_i) g_j(x_i)$$

(See APFS for details.)

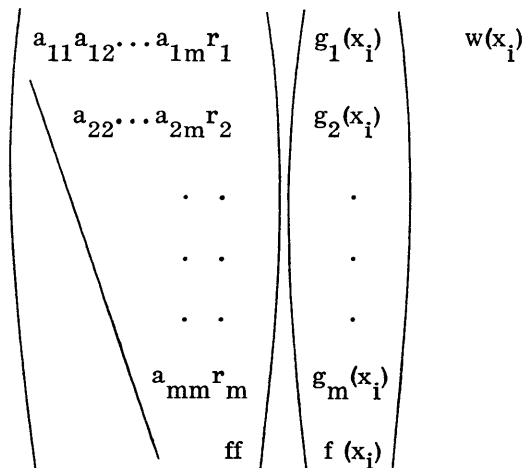
Some remarks regarding polynomial approximation are in order. Use of monomials $g_i(x) = x^{i-1}$ as fundamental functions results in a badly ill-conditioned coefficient matrix A . If Chebyshev or Legendre polynomials are used instead, the condition of the normal equations is improved remarkably, provided the arguments have a sensible distribution (for example, are equidistant in the interval -1 to $+1$).

2. Programming considerations

To allow for full flexibility in data handling, the user must provide an external subroutine that returns the values $g_1(x_i), g_2(x_i), \dots, g_m(x_i), f(x_i)$ stored in a vector P together with the weight value $w(x_i)$. Input values to this subroutine are the current subscript value i, a number of points n, and -- for ease of communication between main line and external -- a dummy array named DATI.

Coefficient matrix A and right-hand side R are allocated adjacently. A is stored columnwise in compressed form, and R is augmented by one element ff in which the weighted square sum of function values is returned. The coefficient matrix A, right-hand side R, and square sum of function values ff are generated in a loop over i from 1 to n. Initially they are set to zero.

Storage allocation scheme:



Triangular array WORK of dimension $m+1$ by $m+1$ Vector P of dimension $m+1$ Weight WGT

For updating of the j^{th} column of the triangular array WORK, the j^{th} element of vector P is multiplied by the weight WGT, giving AUX and then P(i). AUX is added to the i^{th} element in the j^{th} column of WORK for i equal 1 up to j.

In this way the coefficient matrix A, the right-hand side R, and the square sum of function values are generated quite naturally by one and the same scheme.

a. External subroutine for data handling

The error parameter IER may be declared as scalar (that is, vector with one element) or vector in the user's main line. Within APLL it is treated as a vector with one element.

IER(1) is used for control purposes. If IER(1) is set to a nonzero value within the external subroutine, APLL returns to the calling program (main line), with an unchanged value of IER(1).

APLL sets the error parameter IER(1) to zero at the beginning. An error return with IER(1) = -1 is activated if n and m are not both positive or if n is less than m.

The user has full flexibility for handling of the data $x_i, f(x_i), w(x_i), g_1(x_i), \dots, g_m(x_i)$.

(1) If he wishes to allocate $x_i, f(x_i), w(x_i), g_1(x_i), \dots, g_m(x_i)$ in main storage, he may use an array the name of which replaces the dummy DATI.

Integer values needed for addressing may be inserted as additional components in the vector IER.

(2) Use of COMMON is another possibility for data exchange between the main line and the data handling external subroutine.

(3) Calculation of some or all of the required quantities as functions of the subscript or as functions of the argument x_i is another convenient choice.

(4) The needed data may be read in sequentially from one or more external devices, for example, $x_i, f(x_i), w(x_i)$ from card unit, and/or $g_1(x_i), \dots, g_m(x_i)$ from tape unit.

The four cases listed above may occur in any sensible combination.

		APLL 10
		APLL 20
		APLL 30
		APLL 40
		APLL 50
		APLL 60
		APLL 70
		APLL 80
		APLL 90
		APLL 100
		APLL 110
		APLL 120
		APLL 130
		APLL 140
		APLL 150
		APLL 160
		APLL 170
		APLL 180
		APLL 190
		APLL 200
		APLL 210
		APLL 220
		APLL 230
		APLL 240
		APLL 250
		APLL 260
		APLL 270
		APLL 280
		APLL 290
		APLL 300
		APLL 310
		APLL 320
		APLL 330
		APLL 340
		APLL 350
		APLL 360
		APLL 370
		APLL 380
		APLL 390
		APLL 400
		APLL 410
		APLL 420
		APLL 430
		APLL 440
		APLL 450
		APLL 460
		APLL 470
		APLL 480
		APLL 490
		APLL 500
		APLL 510
		APLL 520
		APLL 530
		APLL 540
		APLL 550
		APLL 560
		APLL 570
		APLL 580
		APLL 590
		APLL 600
		APLL 610
		APLL 620
		APLL 630
		APLL 640

```

C AND HEIGHTS) IS COMPLETELY LEFT TO THE USER APLL 640
C ESSENTIALLY HE HAS THREE CHOICES APLL 650
C (1) THE I-TH VALUES OF ARGUMENT, FUNCTION VALUE AND WEIGHT APLL 660
C ARE CALCULATED WITHIN SUBROUTINE FFCT FOR GIVEN I. APLL 670
C (2) THE I-TH VALUES OF ARGUMENT, FUNCTION VALUE AND WEIGHT APLL 680
C ARE DETERMINED BY TABLE LOOK UP. THE STORAGE LOCATIONS APLL 690
C REQUIRED ARE ALLOCATED WITHIN THE DUMMY ARRAY DAT1 APLL 700
C (POSSIBLY IN P TOO, IN EXCESS OF THE SPECIFIED IP + 1 APLL 710
C LOCATIONS). APLL 720
C ANOTHER POSSIBILITY WOULD BE TO USE COMMON AS INTERFACE APLL 730
C BETWEEN MAIN LINE AND SUBROUTINE FFCT AND TO ALLOCATE APLL 740
C STORAGE FOR THE DATA SET IN COMMON. APLL 750
C (3) THE I-TH VALUES OF ARGUMENT, FUNCTION VALUE AND WEIGHT APLL 760
C ARE READ IN FROM AN EXTERNAL DEVICE. THIS MAY BE EASILY APLL 770
C ACCOMPLISHED SINCE I IS USED STRICTLY INCREASING FROM APLL 780
C ONE UP TO N WITHIN APLL APLL 790
C
C ..... APLL 800
C SUBROUTINE APLL(FFCT,N,IP,P,WORK,DAT1,IER) APLL 810
C
C DIMENSIONED DUMMY VARIABLES APLL 820
C DIMENSION P(1),WORK(1),DAT1(1),IER(1) APLL 830
C
C CHECK FOR FORMAL ERRORS IN SPECIFIED DIMENSIONS APLL 840
C 1 IF(N)10,1 APLL 850
C 2 IF(IP)10,2 APLL 860
C 3 IF(N-IP)10,3 APLL 870
C
C SET WORKING STORAGE AND RIGHT HAND SIDE TO ZERO APLL 880
C 3 IPP1=IP+1 APLL 890
C M=IPP1*(IP+2)/2 APLL 900
C IEP(1)=0 APLL 910
C DO 4 I=1,M APLL 920
C 4 WORK(I)=0. APLL 930
C
C START GREAT LOOP OVER ALL GIVEN POINTS APLL 940
C DO 8 I=1,N APLL 950
C CALL FFCT(I,N,IP,P,DAT1,WGT,IER) APLL 960
C IF(IER(1))9,5,9 APLL 970
C 5 J=0 APLL 980
C DO 7 K=1,IP+1 APLL 990
C AUX=PKI*WGT APLL 1000
C DO 6 L=1,K APLL 1010
C J=J+1 APLL 1020
C 6 WORK(J)=WORK(J)+P(L)*AUX APLL 1030
C 7 CONTINUE APLL 1040
C 8 CONTINUE APLL 1050
C
C NORMAL RETURN APLL 1060
C 9 RETURN APLL 1070
C
C ERROR RETURN IN CASE OF FORMAL ERRORS APLL 1080
C 10 IER(1)=-1 APLL 1090
C RETURN APLL 1100
C END APLL 1110

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C ..... DAPL 640
C METHOD DAPL 650
C HANDLING OF THE GIVEN DATA SET (ARGUMENTS,FUNCTION VALUES DAPL 660
C AND HEIGHTS) IS COMPLETELY LEFT TO THE USER DAPL 670
C ESSENTIALLY HE HAS THREE CHOICES DAPL 680
C (1) THE I-TH VALUES OF ARGUMENT, FUNCTION VALUE AND WEIGHT DAPL 690
C ARE CALCULATED WITHIN SUBROUTINE FFCT FOR GIVEN I. DAPL 700
C (2) THE I-TH VALUES OF ARGUMENT, FUNCTION VALUE AND WEIGHT DAPL 710
C ARE DETERMINED BY TABLE LOOK UP. THE STORAGE LOCATIONS DAPL 720
C REQUIRED ARE ALLOCATED WITHIN THE DUMMY ARRAY DAT1 DAPL 730
C (POSSIBLY IN P TOO, IN EXCESS OF THE SPECIFIED IP + 1 DAPL 740
C LOCATIONS). DAPL 750
C ANOTHER POSSIBILITY WOULD BE TO USE COMMON AS INTERFACE DAPL 760
C BETWEEN MAIN LINE AND SUBROUTINE FFCT AND TO ALLOCATE DAPL 770
C STORAGE FOR THE DATA SET IN COMMON. DAPL 780
C (3) THE I-TH VALUES OF ARGUMENT, FUNCTION VALUE AND WEIGHT DAPL 790
C ARE READ IN FROM AN EXTERNAL DEVICE. THIS MAY BE EASILY DAPL 800
C ACCOMPLISHED SINCE I IS USED STRICTLY INCREASING FROM DAPL 810
C ONE UP TO N WITHIN APLL DAPL 820
C
C ..... DAPL 830
C SUBROUTINE DAPL(FFCT,N,IP,P,WORK,DAT1,IER) DAPL 840
C
C DIMENSIONED DUMMY VARIABLES DAPL 850
C DIMENSION P(1),WORK(1),DAT1(1),IER(1) DAPL 860
C DOUBLE PRECISION P,WORK,DAT1,WGT,AUX DAPL 870
C
C CHECK FOR FORMAL ERRORS IN SPECIFIED DIMENSIONS DAPL 880
C 1 IF(N)10,1 DAPL 890
C 2 IF(IP)10,2 DAPL 900
C 3 IF(N-IP)10,3 DAPL 910
C
C SET WORKING STORAGE AND RIGHT HAND SIDE TO ZERO DAPL 920
C 3 IPP1=IP+1 DAPL 930
C M=IPP1*(IP+2)/2 DAPL 940
C IEP(1)=0 DAPL 950
C DO 4 I=1,M DAPL 960
C 4 WORK(I)=0.00 DAPL 970
C
C START GREAT LOOP OVER ALL GIVEN POINTS DAPL 980
C DO 8 I=1,N DAPL 990
C CALL FFCT(I,N,IP,P,DAT1,WGT,IER) DAPL 1000
C IF(IER(1))9,5,9 DAPL 1010
C 5 J=0 DAPL 1020
C DO 7 K=1,IPP1 DAPL 1030
C AUX=PKI*WGT DAPL 1040
C DO 6 L=1,K DAPL 1050
C J=J+1 DAPL 1060
C 6 WORK(J)=WORK(J)+P(L)*AUX DAPL 1070
C 7 CONTINUE DAPL 1080
C 8 CONTINUE DAPL 1090
C
C NORMAL RETURN DAPL 1100
C 9 RETURN DAPL 1110
C
C ERROR RETURN IN CASE OF FORMAL ERRORS DAPL 1120
C 10 IER(1)=-1 DAPL 1130
C RETURN DAPL 1140
C END DAPL 1150

```

```

C ..... DAPL 10
C SUBROUTINE DAPL DAPL 20
C PURPOSE DAPL 30
C SET UP NORMAL EQUATIONS FOR A LINEAR LEAST SQUARES FIT DAPL 40
C TO A GIVEN DISCRETE FUNCTION DAPL 50
C
C USAGE DAPL 60
C CALL DAPL(FFCT,N,IP,P,WORK,DAT1,IER) DAPL 70
C SUBROUTINE FFCT REQUIRES AN EXTERNAL STATEMENT DAPL 80
C
C DESCRIPTION OF PARAMETERS DAPL 90
C FFCT - USER CODED SUBROUTINE WHICH MUST BE DECLARED DAPL 100
C EXTERNAL IN THE MAIN PROGRAM. IT IS CALLED DAPL 110
C CALL FFCT(I,N,IP,P,DAT1,WGT,IER) AND RETURNS DAPL 120
C THE VALUES OF THE FUNDAMENTAL FUNCTIONS FOR DAPL 130
C THE I-TH ARGUMENT IN P(I) UP TO P(IP) DAPL 140
C FOLLOWED BY THE I-TH FUNCTION VALUE IN P(IP+1) DAPL 150
C N IS THE NUMBER OF ALL POINTS DAPL 160
C P,DAT1,WGT MUST BE OF DOUBLE PRECISION. DAPL 170
C DAT1 IS A DUMMY PARAMETER WHICH IS USED AS ARRAY DAPL 180
C NAME. THE GIVEN DATA SET MAY BE ALLOCATED IN DAT1 DAPL 190
C WGT IS THE WEIGHT FACTOR FOR THE I-TH POINT DAPL 200
C IER IS USED AS RESULTANT ERROR PARAMETER IN FFCT DAPL 210
C
C N - NUMBER OF GIVEN POINTS DAPL 220
C IP - NUMBER OF FUNDAMENTAL FUNCTIONS USED FOR LEAST DAPL 230
C SQUARES FIT DAPL 240
C IP SHOULD NOT EXCEED N DAPL 250
C P - WORKING STORAGE OF DIMENSION IP+1, WHICH DAPL 260
C IS USED AS INTERFACE BETWEEN APLL AND THE USER DAPL 270
C CODED SUBROUTINE FFCT DAPL 280
C P MUST BE OF DOUBLE PRECISION. DAPL 290
C WORK - WORKING STORAGE OF DIMENSION (IP+1)*(IP+2)/2. DAPL 300
C ON RETURN WORK CONTAINS THE SYMMETRIC COEFFICIENT DAPL 310
C MATRIX OF THE NORMAL EQUATIONS IN COMPRESSED FORM, DAPL 320
C I.E. UPPER TRIANGULAR PART ONLY STORED COLUMNWISE. DAPL 330
C THE FOLLOWING IP POSITIONS CONTAIN THE RIGHT DAPL 340
C HAND SIDE AND WORK((IP+1)*(IP+2)/2) CONTAINS DAPL 350
C THE WEIGHTED SQUARE SUM OF THE FUNCTION VALUES DAPL 360
C WORK MUST BE OF DOUBLE PRECISION. DAPL 370
C DAT1 - DUMMY ENTRY TO COMMUNICATE AN ARRAY NAME BETWEEN DAPL 380
C MAIN LINE AND SUBROUTINE FFCT. DAPL 390
C DAT1 MUST BE OF DOUBLE PRECISION. DAPL 400
C IEP - RESULTING ERROR PARAMETER DAPL 410
C IER = -1 MEANS FORMAL ERRORS IN SPECIFIED DIMENSIONS DAPL 420
C IER = 0 MEANS NO ERRORS DAPL 430
C IER = 1 MEANS ERROR IN EXTERNAL SUBROUTINE FFCT DAPL 440
C
C REMARKS DAPL 450
C TO ALLOW FOR EASY COMMUNICATION OF INTEGER VALUES DAPL 460
C BETWEEN MAINLINE AND EXTERNAL SUBROUTINE FFCT, THE ERROR DAPL 470
C PARAMETER IER IS TREATED AS A VECTOR OF DIMENSION 1 WITHIN DAPL 480
C SUBROUTINE DAPL. ADDITIONAL COMPONENTS OF IER MAY BE DAPL 490
C INTRODUCED BY THE USER FOR COMMUNICATION BACK AND FORTH. DAPL 500
C IN THIS CASE, HOWEVER, THE USER MUST SPECIFY IER AS A DAPL 510
C VECTOR IN HIS MAINLINE. DAPL 520
C EXECUTION OF SUBROUTINE DAPL IS A PREPARATORY STEP FOR DAPL 530
C CALCULATION OF THE LINEAR LEAST SQUARES FIT. DAPL 540
C NORMALLY IT IS FOLLOWED BY EXECUTION OF SUBROUTINE DAPFS DAPL 550
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DAPL 560
C THE EXTERNAL SUBROUTINE FFCT MUST BE FURNISHED BY THE USER DAPL 570

```

Subroutine FORIF

This subroutine produces the Fourier coefficients for a given periodic function.

Given:

1. A function $f(x)$ for values of x between 0 and 2π
2. N - the spacing desired such that the interval is $2\pi/(2N + 1)$
3. M - the desired order of the Fourier coefficients, $0 \leq M \leq N$

the coefficients of the Fourier series that approximate the given function are calculated as follows:

$$C_1 = \cos \left(\frac{2\pi}{2N+1} \right) \quad (1)$$

$$S_1 = \sin \left(\frac{2\pi}{2N+1} \right) \quad (2)$$

$$U_2 = 0$$

$$U_1 = 0$$

$$C = 1$$

$$S = 0$$

$$J = 1$$

The following recursive sequence is used to compute U_0 , U_1 , and U_2 :

$$U_0 = f\left(\frac{2m\pi}{2N+1}\right) + 2CU_1 - U_2 \quad (3)$$

$$U_2 = U_1$$

$$U_1 = U_0$$

for values of $m = 2N, 2N-1, \dots, 1$

The coefficients are then:

$$A_J = \frac{2}{2N+1} \left(f(0) + CU_1 - U_2 \right) \quad (4)$$

$$B_J = \frac{2}{2N+1} S U_1 \quad (5)$$

The values of C and S are updated to:

$$Q = C_1 C - S_1 S$$

$$S = C_1 S + S_1 C$$

$$C = Q$$

J is stepped by 1 and the sequence starting at equation (3) is now repeated until $M+1$ pairs of coefficients have been computed.

```

C ..... FRIF 10
C ..... FRIF 20
C ..... FRIF 30
C ..... FRIF 40
C ..... FRIF 50
C ..... FRIF 60
C ..... FRIF 70
C ..... FRIF 80
C ..... FRIF 90
C ..... FRIF 100
C ..... FRIF 110
C ..... FRIF 120
C ..... FRIF 130
C ..... FRIF 140
C ..... FRIF 150
C ..... FRIF 160
C ..... FRIF 170
C ..... FRIF 180
C ..... FRIF 190
C ..... FRIF 200
C ..... FRIF 210
C ..... FRIF 220
C ..... FRIF 230
C ..... FRIF 240
C ..... FRIF 250
C ..... FRIF 260
C ..... FRIF 270
C ..... FRIF 280
C ..... FRIF 290
C ..... FRIF 300
C ..... FRIF 310
C ..... FRIF 320
C ..... FRIF 330
C ..... FRIF 340
C ..... FRIF 350
C ..... FRIF 360
C ..... FRIF 370
C ..... FRIF 380
C ..... FRIF 390
C ..... FRIF 400
C ..... FRIF 410
C ..... FRIF 420
C ..... FRIF 430
C ..... FRIF 440
C ..... FRIF 450
C ..... FRIF 460
C ..... FRIF 470
C ..... FRIF 480
C ..... FRIF 490
C ..... FRIF 500
C ..... FRIF 510
C ..... FRIF 520
C ..... FRIF 530
C ..... FRIF 540
C ..... FRIF 550
C ..... FRIF 560
C ..... FRIF 570
C ..... FRIF 580
C ..... FRIF 590
C ..... FRIF 600
C ..... FRIF 610
C ..... FRIF 620
C ..... FRIF 630
C ..... FRIF 640
C ..... FRIF 650
C ..... FRIF 660
C ..... FRIF 670
C ..... FRIF 680
C ..... FRIF 690
C ..... FRIF 700
C ..... FRIF 710
C ..... FRIF 720
C ..... FRIF 730
C ..... FRIF 740
C ..... FRIF 750
C ..... FRIF 760
C ..... FRIF 770
C ..... FRIF 780
C ..... FRIF 790
C ..... FRIF 800
C ..... FRIF 810
C ..... FRIF 820
C ..... FRIF 830
C ..... FRIF 840
C ..... FRIF 850
C ..... FRIF 860
C ..... FRIF 870
C ..... FRIF 880
C ..... FRIF 890
C ..... FRIF 900
C ..... FRIF 910
C ..... FRIF 920
C ..... FRIF 930
C ..... FRIF 940
C ..... FRIF 950
C ..... FRIF 960
C ..... FRIF 970
C ..... FRIF 980
C ..... FRIF 990
C ..... FRIF1000
C ..... FRIF1010

SUBROUTINE FORIF
PURPOSE
FOURIER ANALYSIS OF A GIVEN PERIODIC FUNCTION IN THE
RANGE 0-2PI
COMPUTES THE COEFFICIENTS OF THE DESIRED NUMBER OF TERMS
IN THE FOURIER SERIES F(X)=A(0)+SUM(A(K)COS KX+B(K)SIN KX)
WHERE K=1,2,...,M TO APPROXIMATE THE COMPUTED VALUES OF A
GIVEN FUNCTION-SUBPROGRAM
USAGE
CALL FORIF(FUN,N,M,A,B,IER)
DESCRIPTION OF PARAMETERS
FUN-NAME OF FUNCTION SUBPROGRAM TO BE USED FOR COMPUTING
DATA POINTS
N -DEFINES THE INTERVAL SUCH THAT 2N+1 POINTS ARE TAKEN
OVER THE INTERVAL (0,2PI). THE SPACING IS THUS 2PI/2N+1
M -THE MAXIMUM ORDER OF THE HARMONICS TO BE FITTED
A -RESULTANT VECTOR OF FOURIER COSINE COEFFICIENTS OF
LENGTH M+1
A SUB 0, A SUB 1,..., A SUB M
B -RESULTANT VECTOR OF FOURIER SINE COEFFICIENTS OF
LENGTH M+1
B SUB 0, B SUB 1,..., B SUB M
IER-RESULTANT ERROR CODE WHERE
IER=0 NO ERROR
IER=1 M NOT GREATER OR EQUAL TO M
IER=2 M LESS THAN 0
REMARKS
M MUST BE GREATER THAN OR EQUAL TO ZERO
N MUST BE GREATER THAN OR EQUAL TO M
THE FIRST ELEMENT IN VECTOR B IS ZERO IN ALL CASES
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
FUN-NAME OF USER FUNCTION SUBPROGRAM USED FOR COMPUTING
DATA POINTS
CALLING PROGRAM MUST HAVE FORTRAN EXTERNAL STATEMENT
CONTAINING NAMES OF FUNCTION SUBPROGRAMS LISTED IN CALL TO
FORIF
METHOD
USES RECURSIVE TECHNIQUE DESCRIBED IN A. RALSTON, M. WILF,
'MATHEMATICAL METHODS FOR DIGITAL COMPUTERS', JOHN WILEY
AND SONS, NEW YORK, 1963, CHAPTER 24. THE METHOD OF
INDEXING THROUGH THE PROCEDURE HAS BEEN MODIFIED TO
SIMPLIFY THE COMPUTATION.
SUBROUTINE FORIF(FUN,N,M,A,B,IER)
DIMENSION A(1),B(1)
CHECK FOR PARAMETER ERRORS
IER=0
20 IF(M) 30,40,40
30 IER=2
RETURN
40 IF(M-N) 60,60,50
50 IER=1
RETURN
COMPUTE AND PRESET CONSTANTS
60 AN=N
COEF=2.0/(2.0*AN+1.0)
CONST=3.141593*COEF
S1=SIN(CONST)
C1=COS(CONST)
C=1.0
S=0.0
J=1
FUNZ=FUN(0.0)
70 U2=0.0
U1=0.0
A1=2*AN
FORM FOURIER COEFFICIENTS RECURSIVELY
75 X=A1*CONST
U0=FUN(X)+2.0*C*U1-U2
U2=U1
U1=U0
A1=A1-1.0
IF(A1) 80,80,75
80 A(J)=COEF*(FUNZ+C*U1-U2)
B(J)=COEF*S*U1
IF(J-(M+1)) 90,100,100
90 Q=C1*C-S1*S
S=C1*S+S1*C
C=Q
J=J+1
GO TO 70
100 A(1)=A1*0.5
RETURN
END

```

Subroutine FORIT

This subroutine produces the Fourier coefficients of a tabulated function.

Given:

1. Tabulated values of a function f(x) for x between 0 and 2π in steps of 2π/(2N+1)

2. N such that there are 2N+1 tabulated data points: 2Kπ/(2N+1), K = 0, 1, 2, ..., 2N

3. M - the desired order of the Fourier coefficients where 0 ≤ M ≤ N

the coefficients of the Fourier series which approximate the given function are calculated as follows:

C1 = cos(2π/(2N+1)) (1)

S1 = sin(2π/(2N+1)) (2)

U2 = 0

U1 = 0

C = 1

S = 0

J = 1

The following recursive sequence is used to compute U0, U1, and U2

U0 = f(2mπ/(2N+1)) + 2 C U1 - U2 (3)

U2 = U1

U1 = U0

for values of m = 2N, 2N-1, ..., 1

The coefficients are then:

AJ = 2/(2N+1) * (f(0) + C U1 - U2) (4)

Bj = 2/(2N+1) * S U1 (5)

The values of C and S are updated to:

Q = C1 C - S1 S

S = C1 S + S1 C

C = Q

j is stepped by 1 and the sequence starting at equation (3) is now repeated until M+1 pairs of coefficients have been computed.

```
C C C C ..... FRITE 10
C C C SUBROUTINE FORIT FRITE 20
C C C C FRITE 30
C C C C FRITE 40
C C C C FRITE 50
C C C C FRITE 60
C C C C FRITE 70
C C C C FRITE 80
C C C C FRITE 90
C C C C FRITE 100
C C C C FRITE 110
C C C C FRITE 120
C C C C FRITE 130
C C C C FRITE 140
C C C C FRITE 150
C C C C FRITE 160
C C C C FRITE 170
C C C C FRITE 180
C C C C FRITE 190
C C C C FRITE 200
C C C C FRITE 210
C C C C FRITE 220
C C C C FRITE 230
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C C C C FRITE 380
C C C C FRITE 390
C C C C FRITE 400
C C C C FRITE 410
C C C C FRITE 420
C C C C FRITE 430
C C C C FRITE 440
C C C C FRITE 450
C C C C FRITE 460
C C C C FRITE 470
C C C C FRITE 480
C C C C FRITE 490
C C C C FRITE 500
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C C C C FRITE 520
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C C C C FRITE 680
C C C C FRITE 690
C C C C FRITE 700
C C C C FRITE 710
C C C C FRITE 720
C C C C FRITE 730
C C C C FRITE 740
C C C C FRITE 750
C C C C FRITE 760
C C C C FRITE 770
C C C C FRITE 780
C C C C FRITE 790
C C C C FRITE 800
C C C C FRITE 810
C C C C FRITE 820
C C C C FRITE 830
C C C C FRITE 840
C C C C FRITE 850
C C C C FRITE 860
C C C C FRITE 870
C C C C FRITE 880
C C C C FRITE 890
C C C C FRITE 900
C C C C FRITE 910
C C C C FRITE 920
C C C C FRITE 930
C C C C FRITE 940
```

Subroutines HARM and DHARM

Given three integers $M_\nu, \nu = 1, 2, 3$ and a three-dimensional array of complex numbers $A(k_1, k_2, k_3)$ where $k_\nu = 0, 1, \dots, N_\nu - 1$ and $N_\nu = 2^{M_\nu}$, this subroutine computes the three-dimensional, complex Fourier series:

$$X(j_1, j_2, j_3) = \sum_{k_1=0}^{N_1-1} \sum_{k_2=0}^{N_2-1} \sum_{k_3=0}^{N_3-1} A(k_1, k_2, k_3) e^{2\pi i \left(\frac{j_1 \cdot k_1}{N_1} + \frac{j_2 \cdot k_2}{N_2} + \frac{j_3 \cdot k_3}{N_3} \right)} \quad (1)$$

where

$$j_\nu = 0, 1, \dots, N_\nu - 1 \text{ and } \nu = 1, 2, 3.$$

The inverse series may also be computed:

$$A(k_1, k_2, k_3) = \frac{1}{N_1 \cdot N_2 \cdot N_3} \sum_{j_1=0}^{N_1-1} \sum_{j_2=0}^{N_2-1} \sum_{j_3=0}^{N_3-1} X(j_1, j_2, j_3) e^{-2\pi i \left(\frac{j_1 \cdot k_1}{N_1} + \frac{j_2 \cdot k_2}{N_2} + \frac{j_3 \cdot k_3}{N_3} \right)} \quad (2)$$

For one dimension, the algorithm for the complex Fourier transform of complex numbers $A(k)$ is:

$$X(j) = \sum_{k=0}^{N-1} A(k) w^{jk} \quad (3)$$

where $w = e^{\frac{2\pi i}{N}}$, $N = 2^M$, $j = 0, 1, 2, \dots, N - 1$ expresses $X(j)$ as a function of the M arguments $j_{M-1}, j_{M-2}, \dots, j_1, j_0$ of the binary representation of j :

$$j = j_{M-1} \cdot 2^{M-1} + \dots + j_1 \cdot 2 + j_0, \quad j_\nu = 0 \text{ or } 1$$

Then (3) can be written:

$$X(j_{M-1}, \dots, j_1, j_0) = \sum_{k_0=0}^1 \sum_{k_1=0}^1 \dots \sum_{k_{M-1}=0}^1 A(k_{M-1}, \dots, k_0) w^j \cdot k_{M-1} \cdot 2^{M-1} \dots w^{j \cdot k_0 \cdot 2^0} \quad (4)$$

Then $w^{j k_{M-1} 2^{M-1}} = w^{j \cdot k_{M-1} 2^{M-1}}$ since $e^{2\pi i} = 1$, and the innermost sum in (4) yields an array:

$$A_1(j_0, k_{M-2}, \dots, k_0) = \sum_{k_{M-1}=0}^1 A(k_{M-1}, \dots, k_0) w^{j_0 \cdot k_{M-1} \cdot 2^{M-1}} \quad (5)$$

Successive arrays A_2, \dots, A_M obtained by summing over k_{M-2}, \dots, k_0 respectively are computed. The general formula is:

$$A_L(j_0, \dots, j_{L-1}, k_{M-L-1}, \dots, k_0) = \sum_{k_{M-L}=0}^1 A_{L-1}(j_0, \dots, j_{L-2}, k_{M-L}, \dots, k_0) w^{(j_{L-1} \cdot 2^{L-1} + \dots + j_0) k_{M-L} 2^{M-L}} \quad (6)$$

The final array will be the desired X . The storage indexing convention used is to let the M arguments of $A_L(j_0, \dots, k_0)$ be the binary representation of the index of the storage location for $A_L(j_0, \dots, k_0)$. In this way, each step of the algorithm involves fetching from two storage locations and returning results in the same two locations, thereby saving storage. However, the elements of the final array:

$$X(j_{M-1}, \dots, j_1, j_0) = A_M(j_0, k_1, \dots, j_{M-1})$$

are in the wrong order. The program reverses the order of bits in bit representations to compensate.

A modification of the above algorithm is made for three dimensions, and another modification is made in the L-loop to save computations.

```

C -----
C HARM 10
C HARM 20
C HARM 30
C HARM 40
C HARM 50
C HARM 60
C HARM 70
C HARM 80
C HARM 90
C HARM 100
C HARM 110
C HARM 120
C HARM 130
C HARM 140
C HARM 150
C HARM 160
C HARM 170
C HARM 180
C HARM 190
C HARM 200
C HARM 210
C HARM 220
C HARM 230
C HARM 240
C HARM 250
C HARM 260
C HARM 270
C HARM 280
C HARM 290
C HARM 300
C HARM 310
C HARM 320
C HARM 330
C HARM 340
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C HARM 510
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C HARM 540
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C HARM 560
C HARM 570
C HARM 580
C HARM 590
C HARM 600
C HARM 610
C HARM 620
C HARM 630
C HARM 640
C HARM 650
C HARM 660
C HARM 670
C HARM 680
C HARM 690
C HARM 700
C HARM 710
C HARM 720
C HARM 730
C HARM 740
C HARM 750
C HARM 760
C HARM 770
C HARM 780
C HARM 790
C HARM 800
C HARM 810
C HARM 820
C HARM 830
C HARM 840
C HARM 850
C HARM 860
C HARM 870
C HARM 880
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C HARM 900
C HARM 910
C HARM 920
C HARM 930
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C HARM 950
C HARM 960
C HARM 970
C HARM 980
C HARM 990
C HARM1000
C HARM1010
C HARM1020
C HARM1030
C HARM1040
C HARM1050
C HARM1060
C HARM1070
C HARM1080
C HARM1090
C HARM1100
C HARM1110
C HARM1120
C HARM1130
C HARM1140
C HARM1150
C HARM1160
C HARM1170
C HARM 10
C HARM 20
C HARM 30
C HARM 40
C HARM 50
C HARM 60
C HARM 70
C HARM 80
C HARM 90
C HARM 100
C HARM 110
C HARM 120
C HARM 130
C HARM 140
C HARM 150
C HARM 160
C HARM 170
C HARM 180
C HARM 190
C HARM 200
C HARM 210
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C HARM 390
C HARM 400
C HARM 410
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C HARM 470
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C HARM 500
C HARM 510
C HARM 520
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C HARM 540
C HARM 550
C HARM 560
C HARM 570
C HARM 580
C HARM 590
C HARM 600
C HARM 610
C HARM 620
C HARM 630
C HARM 640
C HARM 650
C HARM 660
C HARM 670
C HARM 680
C HARM 690
C HARM 700
C HARM 710
C HARM 720
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C HARM1000
C HARM1010
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C HARM1080
C HARM1090
C HARM1100
C HARM1110
C HARM1120
C HARM1130
C HARM1140
C HARM1150
C HARM1160
C HARM1170
C HARM 10
C HARM 20
C HARM 30
C HARM 40
C HARM 50
C HARM 60
C HARM 70
C HARM 80
C HARM 90
C HARM 100
C HARM 110
C HARM 120
C HARM 130
C HARM 140
C HARM 150
C HARM 160
C HARM 170
C HARM 180
C HARM 190
C HARM 200
C HARM 210
C HARM 220
C HARM 230
C HARM 240
C HARM 250
C HARM 260
C HARM 270
C HARM 280
C HARM 290
C HARM 300
C HARM 310
C HARM 320
C HARM 330
C HARM 340
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C HARM 420
C HARM 430
C HARM 440
C HARM 450
C HARM 460
C HARM 470
C HARM 480
C HARM 490
C HARM 500
C HARM 510
C HARM 520
C HARM 530
C HARM 540
C HARM 550
C HARM 560
C HARM 570
C HARM 580
C HARM 590
C HARM 600
C HARM 610
C HARM 620
C HARM 630
C HARM 640
C HARM 650
C HARM 660
C HARM 670
C HARM 680
C HARM 690
C HARM 700
C HARM 710
C HARM 720
C HARM 730
C HARM 740
C HARM 750
C HARM 760
C HARM 770
C HARM 780
C HARM 790
C HARM 800
C HARM 810
C HARM 820
C HARM 830
C HARM 840
C HARM 850
C HARM 860
C HARM 870
C HARM 880
C HARM 890
C HARM 900
C HARM 910
C HARM 920
C HARM 930
C HARM 940
C HARM 950
C HARM 960
C HARM 970
C HARM 980
C HARM 990
C HARM1000
C HARM1010
C HARM1020
C HARM1030
C HARM1040
C HARM1050
C HARM1060
C HARM1070
C HARM1080
C HARM1090
C HARM1100
C HARM1110
C HARM1120
C HARM1130
C HARM1140
C HARM1150
C HARM1160
C HARM1170

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IF (PI125C,25C,3C
3C ICIF=AF(1C)
  NIT=AF(1C)
  PEV = 24(PI1/2)
  IF (PI - PEV 16C,6C,40
C
C P IS CCC, CC L=1 CASE
4C WEIT=1/2
  KL=WEIT
  CC 5C I=1,IL1,ICIF
  KLAST=KL+1
  CC 5C R=1,KLAST,2
  KL=KWEIT
C
C CC CASE STEP WITH L=1,J=C
C A(K1)=A(K1)+A(KC)
C A(KC)=A(K1)-A(KC)
C
C T=A(KC)
  A(KC)=A(K1)-T
  A(K1)=A(K1)+T
  T=A(KC1)
  A(KC1)=A(K1)-T
  A(K1)=A(K1)+T
5C A(K1)=A(K1)+T
  IF (PI - 125C,25C,52
52 LFINST = 3
C
C EE = JLAST + 2*(L-2) - 1
  JLAST=1
  CC IC 7C
C
C P IS EVEN
C LFINST = 2
  JLAST=C
7C CC 24C L=LFINST,PI,2
  JJCIF=KEIT
  WEIT=KEIT/2
  KL=KEIT-2
C
C CC FOR J=C
  CC BC I=1,IL1,ICIF
  KLAST=KL
  CC BC R=1,KLAST,2
  K1=KWEIT
  K2=K1+KEIT
  K3=K2+KEIT
C
C CC INC STEPS WITH J=C
  A(K1)=A(K1)+A(K2)
  A(K2)=A(K1)-A(K2)
  A(K1)=A(K1)+A(K3)
  A(K3)=A(K1)-A(K3)
C
C A(K1)=A(K1)+A(K1)
  A(K2)=A(K2)+A(K2)+1
  A(K3)=A(K2)-A(K3)+1
C
C T=A(K2)
  A(K2)=A(K1)-T
  A(K1)=A(K1)+T
  T=A(K2+1)
  A(K2+1)=A(K1)+T
  A(K1)=A(K1)+T
C
C T=A(K3)
  A(K3)=A(K1)-T
  A(K1)=A(K1)+T
  T=A(K3+1)
  A(K3+1)=A(K1)+T
  A(K1)=A(K1)+T
C
C T=A(K1)
  A(K1)=A(K1)-T
  A(K1)=A(K1)+T
  T=A(K1+1)
  A(K1+1)=A(K1)+T
  A(K1)=A(K1)+T
C
C R=-A(K3+1)
  T = A(K3)
  A(K3)=A(K2)-R
  A(K2)=A(K2)+R
  A(K3+1)=A(K2+1)-T
  A(K2+1)=A(K2+1)+1
8C IF (JLAST) 235,235,82
  JJ=JJCIF +1
C
C CC FOR J=1
  ILAST = IL + JJ
  CC 65 I = JJ,ILAST,ICIF
  KLAST = KL+1
  CC 85 R=1,KLAST,2
  K1 = KWEIT
  K2 = K1+KEIT
  K3 = K2+KEIT
C
C LETTING W=(1+I)/ROOT2,W3=(1-I)/ROOT2,W2=1-I
  A(K1)=A(K1)+A(K2)+1
  A(K2)=A(K1)-A(K2)+1
  A(K1)=A(K1)+A(K3)+1
  A(K3)=A(K1)-A(K3)+1
C
C A(K1)=A(K1)+A(K1)
  A(K1)=A(K1)-A(K1)
  A(K2)=A(K2)+A(K3)+1
  A(K3)=A(K2)-A(K3)+1
C
C R = -A(K2+1)
  T = A(K2)
  A(K2) = A(K1)-R
  A(K1) = A(K1)+R
  A(K2+1)=A(K1)+T
  A(K1)=A(K1)+T
C
C A(K1)=A(K1)-A(K1+1)
  A(K1)=A(K1)+A(K1)
  R=-A(K3)-A(K3+1)
  T=A(K3)-A(K3+1)
  A(K3)=A(K3)+R/RCCT2
  A(K3+1)=A(K3)-T/RCCT2
  A(K1)=A(K3)+R/RCCT2
  A(K1+1)=A(K1+1)+R/RCCT2
  T = A(K1)
  A(K1)=A(K1)-T
  A(K1)=A(K1)+T
  T=A(K1+1)
  A(K1+1)=A(K1+1)-T
  A(K1)=A(K1)+T
  R=-A(K3+1)

```

T=A(K3)
A(K3)=A(K2)-R
A(K2)=A(K1)+R
A(K3)=A(K2)+1-T
85 A(K2+1)=A(K2)+1+T
95 IF(JLAST-1) 235,235,S,C
95 JJ=JJ+JJCIF
C
C ACN CC THE REPAIRING J'S
C EC 23C JJ=JLAST
C
C FETCF W'S
C DEF- W=H*INV(JJ), W2=H*W2, W3=H*W3
96 I=INV(J+1)
96 IC=AT-I
W(1)=S(1C)
W(2)=S(1)
I2=2*I
I2C=AT-I2
IF(I2C)I2C,110,1CC
C
C 2*I IS IN FIRST QUADRANT
1CC W(1)=S(12C)
W(2)=S(12)
CC TC 12C
11C W(1)=C.
W(2)=1.
CC TC 12C
C
C 2*I IS IN SECCND QUADRANT
12C I2C--I2C+AT
I2C--I2C
W(1)=S(12C)
W(2)=S(12CC)
12C I3=1+I2
I2C=AT-I3
IF(I3C)I3C,13C,14C
C
C I3 IN FIRST QUADRANT
14C W(1)=S(13C)
W(3(2))=S(12)
CC TC 2CC
15C W(1)=C.
W(2)=1.
CC TC 2CC
C
C I3CC=I3C+AT
16C IF(I3CC)I3CC,18C,17C
C
C I3 IN SECCND QUADRANT
17C I3C--I3C
W(1)=S(13C)
W(3(2))=S(13CC)
CC TC 2CC
18C W(1)=C.
W(2)=1.
CC TC 2CC
C
C 2*I IN THIR QUADRANT
19C I3CCC=AT+I3CC
I3CC -- I3CC
W(1)=S(13CCC)
W(2)=S(13CC)
20C ILAS=IL+JJ
CC 23C I=JJ, IL JCIF
KLAST=KL+I
CC 22C W=I, KLAST,2
K1=K*KEIT
K2=K+KEIT
K3=K+KEIT
C
C EC TWO STEPS WITH J ACT C
A(K1)=A(K1)+R2*W2
A(K2)=A(K1)-A(K2)+W2
A(K1)=A(K1)+W3*(K3)+W3
A(K2)=A(K1)+W3*(K2)+W3
C
C A(K1)=A(K1)+A(K1)
A(K1)=A(K1)+A(K1)
A(K2)=A(K2)+A(K2)+1
A(K3)=A(K2)-A(K3)+1
C
C R=A(K2)+W2(1)-A(K2+1)+W2(2)
T=A(K2)+W2(2)+A(K2+1)+W2(1)
A(K2)=A(K1)+R
A(K1)=A(K1)+R
A(K2+1)=A(K1)+1
A(K+1)=A(K+1)+T
C
C R=A(K2)+W3(1)-A(K2+1)+W3(2)
T=A(K2)+W3(2)+A(K2+1)+W3(1)
A(K2)=A(K1)+R
A(K1)=A(K1)+R
A(K2+1)=A(K1)+1
A(K+1)=A(K+1)+T
A(K1)=A(K1)+T
A(K2)=A(K2)+1
A(K3)=A(K2)-A(K3)+1
T=A(K3)
A(K1)=A(K2)+R
A(K2)=A(K1)+R
A(K3)=A(K2)+1-T
22C A(K2+1)=A(K2)+1+T
END CF I AND K LCCPS
C
C 23C JJ=JJEIF+JJ
END CF J LCCF
C
C 235 JLAST=J+JLAST+3
24C CCNTALE
END CF L LCCP
C
C 25C CCNTALE
END CF LC LCCP
C
C WE ACN HAVE THE COMPLEX FOURIER SLPs BUT THEIR ADDRESSES ARE
BIT-REVERSE. THE FOLLOWING ROUTINE PLTS THEM IN ORDER
ATSC=AT*AT
P3PT=P3-PT
35C IF(P3PT) 37C,36C,36C
C
C P3 GF. CF EC. PT
36C IGC2=1
A3VAT=A2/AT

HARM2480
HARM2490
HARM2500
HARM2510
HARM2520
HARM2530
HARM2540
HARM2550
HARM2560
HARM2570
HARM2580
HARM2590
HARM2600
HARM2610
HARM2620
HARM2630
HARM2640
HARM2650
HARM2660
HARM2670
HARM2680
HARM2690
HARM2700
HARM2710
HARM2720
HARM2730
HARM2740
HARM2750
HARM2760
HARM2770
HARM2780
HARM2790
HARM2800
HARM2810
HARM2820
HARM2830
HARM2840
HARM2850
HARM2860
HARM2870
HARM2880
HARM2890
HARM2900
HARM2910
HARM2920
HARM2930
HARM2940
HARM2950
HARM2960
HARM2970
HARM2980
HARM2990
HARM3000
HARM3010
HARM3020
HARM3030
HARM3040
HARM3050
HARM3060
HARM3070
HARM3080
HARM3090
HARM3100
HARM3110
HARM3120
HARM3130
HARM3140
HARM3150
HARM3160
HARM3170
HARM3180
HARM3190
HARM3200
HARM3210
HARM3220
HARM3230
HARM3240
HARM3250
HARM3260
HARM3270
HARM3280
HARM3290
HARM3300
HARM3310
HARM3320
HARM3330
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HARM3350
HARM3360
HARM3370
HARM3380
HARM3390
HARM3400
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HARM3570
HARM3580
HARM3590
HARM3600
HARM3610
HARM3620
HARM3630
HARM3640
HARM3650
HARM3660
HARM3670
HARM3680
HARM3690
HARM3700
HARM3710
HARM3720
HARM3730
HARM3740
HARM3750
HARM3760
HARM3770

PIAA3=A1
CC TC 36C
C
C P2 LESS THAN PT
37C IGC2=1
A3VA1=A2
ATVA3=AT/A3
PIAA3=A3
36C JJC3 = ATSC/A3
P3PT=P3-PT
45C IF (P3PT)I47C,46C,46C
C
C P2 GF. CF EC. PT
46C IGC2=1
A2VAT=A2/AT
PIAA2=A1
CC TC 46C
C
C P2 LESS THAN PT
47C IGC2 = 2
A2VAT=A1
ATVA2=AT/A2
PIAA2=A2
46C JJC2=N1SC/A2
P3PT=P3-PT
55C IF(P3PT)57C,56C,56C
C
C P1 GF. CF EC. PT
56C ICC1=1
A1VAT=A1/AT
PIAA1=A1
CC TC 56C
C
C P1 LESS THAN PT
57C ICC1=2
A1VAT=A1
ATVA1=AT/A1
PIAA1=A1
56C JJC1=N1SC/A1
60C JJ3=1
J=1
CC EC JFF3=1,A3VAT
JFF3=INV(JJ3)
CC EC JF3=1,PIAA3
CC TC (161C,42C),1CC2
61C IF3=INV(JF3)+A3VAT
CC TC 62C
62C IF3=INV(JF3)/A1VA3
63C I3=I1FF3+I3+K2
70C JJC2=1
CC EC JFF2=1,A2VAT
JFF2=INV(JJ2)+I3
CC EC JF2=1,PIAA2
CC TC (71C,72C),1CC2
71C IF2=INV(JF2)+A2VAT
CC TC 72C
72C IF2=INV(JF2)/A1VA2
73C I2=I1FF2+I2+K1
60C JJ1=1
CC EC JFF1=1,A1VAT
JFF1=INV(JJ1)+I2
CC EC JF1=1,PIAA1
CC TC (61C,62C),1CC1
61C IF1=INV(JF1)+A1VAT
CC TC 62C
62C IF1=INV(JF1)/A1VA1
63C I1=I1FF1+I1+K1
IF IJ-I1 E4C,E5C,85C
64C T=A(I)
A(I)=A(I)
A(J)=T
T=A(I+1)
A(I)=A(I+1)
A(I+1)=A(I)
C
C 55C JJ=JJ+JJ
60C JJ=JJ+JJ
END CF JFF1 AND JF2
C
C JJC=JJ2+JJ2
END CF JFF2 AND JF3 LCCPS
C
C 60C JJC = JJ2+JJ2
END CF JFF3 LCCP
C
C 65C IF(1FFSET)651,655,655
651 CC 85C
652 A(2*I) = -A(2*I)
655 SETURA
C
C THE FOLLOWING PROGRAM COMPUTES THE SIN AND INV TABLES.
C
C CC PT=MAX(I(1),P(2),P(3)) -2
PT = MAX(I2,PT1)
54C IF (PT-1E) 55C,55C,1E
56C IFERR=C
AT=2*PI
ATV2=AT/2
C
C SET LF SIN TABLE
C IFLT=AFIE(2*PI/11) FCR L=1
51C IFLT=AT-.7653581634
C
C JSTEP=2*PI*(PT-L+1) FCR L=1
JSTEP=AT
C
C JEIF=2*PI*(PT-L) FCR L=1
JEIF=ATV2
S(IJEIF)=SIN(I*ETA)
CC 55C L=2,PT
IETA=IFLT/AT2.
JSTEP=JSTEP
JSTEP=JEIF
JEIF=JEIF/2
S(IJEIF)=SIN(I*ETA)
JCI=AT-JEIF
S(IJCI)=COS(I*ETA)
JLAST=AT-JSTEP2
IF(JLAST - JSTEP) 55C,52C,52C
52C CC 54C J=JSTEP,JLAST,JSTEP
JC=AT-J
JC=J+JEIF
54C S(IJCI)=S(IJCI)+S(IJEIF)*S(IJCI)
55C CCNTALE
C
C SET LF [INVJ] TABLE
C
C 56C PILEXP=ATV2
C
C PILEXP=2*PI*(PT-L). FCR L=1
LP1L2F=1

HARM3780
HARM3790
HARM3800
HARM3810
HARM3820
HARM3830
HARM3840
HARM3850
HARM3860
HARM3870
HARM3880
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HARM3970
HARM3980
HARM3990
HARM4000
HARM4010
HARM4020
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HARM4100
HARM4110
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HARM4970
HARM4980
HARM4990
HARM5000
HARM5010
HARM5020
HARM5030
HARM5040
HARM5050
HARM5060
HARM5070
HARM5080
HARM5090
HARM5100
HARM5110

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C
C LPIERF=2*PI*(L-1), FOR L=1
C INV(L)=C
C CC SEC L=1,PT
C INV(LPIERF+1) = P*LEXP
C CC SEC J=2,LPIERF
C J=4,LPIERF
C 57C INV(JJ)=INV(JJ)+P*LEXP
C P*LEXP=P*LEXP/2
C SEC LPIERF=LPIERF/2
C 58C IF(1FSET)12,655,12
C ETC
HARMS120
HARMS130
HARMS140
HARMS150
HARMS160
HARMS170
HARMS180
HARMS190
HARMS200
HARMS210
HARMS220
HARMS230
10 IF(1FSET) 10,16,20
1E N= N1+N2+N3
FA = A
CC 15 I = 1,N
A(2*I-1) = A(2*I-1)/FA
15 A(2*I) = -A(2*I)/FA
2C A(1)=A(1)+A(1)*N2
A(3)=A(3)+A(1)*N2
CC 25C I(1),3
IL = A(2)-A(1)*I
IL1 = IL+1
PI = P*(I)
IF (PI)25C,25C,20
3C I(1)=A(1)*I
R(1)=A(1)*I
PEV = 2*(PI/2)
IF (PI - PEV) 16C,6C,4C
C
C P IS CCC, CC L=1 CASE
C 4C R(1)=R(1)/2
R=K(1)-2
CC 5C I=1,IL1,ICIF
K(1)=K(1)+1
CC 5C R=1,K(1)+2
K=K+K(1)
C
C CC CASE STEP WITH L=1,J=C
C A(K)=A(K)+A(K)
C A(K)=2(K)-A(K)
C
C T=A(K)
A(K)=A(K)-T
A(K)=A(K)+T
T=A(K)+1
A(K)=A(K)+1
5C A(N+1)=A(N)+1
IF (PI - 1)25C,25C,52
52 LFIRST = 2
C
C CEF = JLAST = 2*(L-2) - 1
JLAST=1
CC TC TC
C
C P IS EVEN
C 6C LFIRST = 2
JLAST=1
7C CC 2AC L=LFIRST,PI/2
J(1)=K(1)
R(1)=K(1)/4
R(1)=K(1)-2
C
C CC FOR J=C
C CC EC I=1,IL1,ICIF
K(1)=K(1)+1
CC BC R=1,K(1)+2
K1=K(1)+1
K2=K1+K(1)
K3=K2+K(1)
C
C EC THE STEPS WITH J=C
C A(K1)=A(K1)+A(K2)
C A(K2)=A(K1)+A(K2)
C A(K3)=A(K1)+A(K2)
C A(K3)=A(K1)-A(K2)
C
C A(K)=A(K)+A(K)
C A(K1)=A(K1)+A(K1)
C A(K2)=A(K2)+A(K2)+1
C A(K3)=A(K2)-A(K3)+1
C
C T=A(K2)
A(K2)=A(K)-T
A(K)=A(K)+T
T=A(K)+1
A(K2)=A(K)+1
A(K)=A(K)+1
C
C T=A(K2)
A(K3)=A(K1)-T
A(K1)=A(K1)+T
T=A(K)+1
A(K3)=A(K1)+1
A(K1)=A(K1)+1
C
C T=A(K1)
A(K1)=A(K)-T
A(K1)=A(K)+T
T=A(K)+1
A(K1)=A(K)+1
A(K4)=A(K)+1
C
C P=A(K2+1)
T = A(K2)
A(K3)=A(K2)+P
A(K2)=A(K2)+P
A(K3)=A(K2)+1
BC A(K2)=A(K2)+1
IF (JLAST) 235,235,82
E2 J=J(1)+1
C
C CC FOR J=1
ILAST= IL+J
CC E5 I = J,ILAST,ICIF
K(1)= K(1)+1
CC E5 R=1,K(1)+2
K1 = K+K(1)
K2 = K1+K(1)
K3 = K2+K(1)
C
C LETTING N=(1+I)/RCCT2,N3=(1+I)/K(1)+N2*P
C A(K)=A(K)+A(K2)*P
C A(K2)=A(K)-A(K2)*P
C A(K1)=A(K1)+A(K2)*N3
C A(K3)=A(K1)+A(K2)*N3
C
C A(K)=A(K)+A(K)
C A(K1)=A(K)+A(K)
C A(K2)=A(K2)+A(K3)+1
C A(K3)=A(K2)-A(K3)+1
C
C P = -A(K2+1)
T = A(K2)
A(K2) = A(K)+P
A(K3) = A(K)+P
A(K2)=A(K)+1
A(K1)=A(K)+1
C
C A(N)=A(K1)-A(K1+1)
HARMS1270
HARMS1280
HARMS1290
HARMS1300
HARMS1310
HARMS1320
HARMS1330
HARMS1340
HARMS1350
HARMS1360
HARMS1370
HARMS1380
HARMS1390
HARMS1400
HARMS1410
HARMS1420
HARMS1430
HARMS1440
HARMS1450
HARMS1460
HARMS1470
HARMS1480
HARMS1490
HARMS1500
HARMS1510
HARMS1520
HARMS1530
HARMS1540
HARMS1550
HARMS1560
HARMS1570
HARMS1580
HARMS1590
HARMS1600
HARMS1610
HARMS1620
HARMS1630
HARMS1640
HARMS1650
HARMS1660
HARMS1670
HARMS1680
HARMS1690
HARMS1700
HARMS1710
HARMS1720
HARMS1730
HARMS1740
HARMS1750
HARMS1760
HARMS1770
HARMS1780
HARMS1790
HARMS1800
HARMS1810
HARMS1820
HARMS1830
HARMS1840
HARMS1850
HARMS1860
HARMS1870
HARMS1880
HARMS1890
HARMS1900
HARMS1910
HARMS1920
HARMS1930
HARMS1940
HARMS1950
HARMS1960
HARMS1970
HARMS1980
HARMS1990
HARMS2000
HARMS2010
HARMS2020
HARMS2030
HARMS2040
HARMS2050
HARMS2060
HARMS2070
HARMS2080
HARMS2090
HARMS2100
HARMS2110
HARMS2120
HARMS2130
HARMS2140
HARMS2150
HARMS2160
HARMS2170
HARMS2180
HARMS2190
HARMS2200
HARMS2210
HARMS2220
HARMS2230
HARMS2240
HARMS2250
HARMS2260
HARMS2270
HARMS2280
HARMS2290
HARMS2300
HARMS2310
HARMS2320
HARMS2330
HARMS2340
HARMS2350

```

... A(K1)+A(K1)*A(K1) ... A(K2)+A(K2)*A(K2) ... A(K3)+A(K3)*A(K3) ... A(K1)+A(K2)+A(K3)+A(K1)*A(K2)+A(K2)*A(K3)+A(K1)*A(K3) ...

```

JCI=NT-JCIF
S(JCI)=CCCS(THETA)
JLAST=NT-JSTEP2
IF(JLAST - JSTEP) 95C,52C,92C
920 CC 94C J=JSTEP,JLAST,JSTEP
JC=NT-J
JC=J+JCIF
94C S(JD)=S(J)*S(JCI)+S(JCIF)*S(JCI)
95C CONTINUE
C
C SET UP INV(J) TABLE
C
94C NLEXP=NTV2
C
C NLEXP=2*(NT-L). FOR L=1
LNIEXP=1
C
C LNIEXP=2*(L-1). FOR L=1
INV(L)=0
CC 980 L=1,NT
INV(LNIEXP+1) = NLEXP
DO 970 J=2,LNIEXP
JJ=J+LNIEXP
970 INV(JJ)=INV(JJ)+NLEXP
NLEXP=NLEXP/2
980 LNIEXP=LNIEXP+2
982 IF(IIFSET)12,895,12
EAC

```

```

DHAR4970
DHAR4980
DHAR4990
DHAR5000
DHAR5010
DHAR5020
DHAR5030
DHAR5040
DHAR5050
DHAR5060
DHAR5070
DHAR5080
DHAR5090
DHAR5100
DHAR5110
DHAR5120
DHAR5130
DHAR5140
DHAR5150
DHAR5160
DHAR5170
DHAR5180
DHAR5190
DHAR5200
DHAR5210
DHAR5220
DHAR5230
DHAR5240

```

Subroutines RHARM and DRHARM

Given $2N$ real numbers $X_0, X_1, \dots, X_{2N-1}$, the subroutine computes Fourier coefficients $a_0, a_1, b_1, a_2, b_2, \dots, a_{N-1}, b_{N-1}, a_N$ in the equation:

$$X_j = \frac{1}{2} a_0 + \sum_{k=1}^{N-1} (a_k \cos\left(\frac{\pi \cdot j \cdot k}{N}\right) + b_k \sin\left(\frac{\pi \cdot j \cdot k}{N}\right)) + \frac{1}{2} a_N (-1)^j$$

where

$$j = 0, 1, \dots, 2N-1$$

The subroutine HARM is called to compute the complex coefficients:

$$A_k = \frac{1}{N} \sum_{j=0}^{N-1} (X_{2j} - iX_{2j+1}) e^{\frac{2\pi i}{N} \cdot j \cdot k},$$

$$k = 0, 1, 2, \dots, N-1$$

Then for $k = 1, 2, \dots, \frac{N}{2} - 1, \frac{N}{2}$ (the bar is conjugation):

$$A'_k = \frac{1}{2} (\bar{A}_k + A_{N-k})$$

$$A''_k = \frac{1}{2} (\bar{A}_{N-k} - A_k)$$

and:

$$C_k = \frac{1}{2} (A'_k + \bar{A}''_k e^{(\frac{\pi}{2} - \frac{\pi}{N} k)i})$$

for $k = 1, 2, \dots, \frac{N}{2} - 1, \frac{N}{2}$

$$C_{N-k} = \frac{1}{2} (\bar{A}'_k - A''_k e^{(\frac{\pi}{N-k} - \frac{\pi}{2})i})$$

for $k = 1, 2, \dots, \frac{N}{2} - 1$

Let:

$$C_o = \frac{1}{2} (\text{Re } A_o - \text{Im } A_o)$$

$$C_N = \frac{1}{2} (\text{Re } A_o + \text{Im } A_o)$$

Finally:

$$a_0 = 2 \operatorname{Re}(C_0)$$

$$a_k = 2 \operatorname{Re}(C_k)$$

$$b_k = -2 \operatorname{Im}(C_k)$$

$$a_N = 2 \operatorname{Re}(C_N)$$

```

AP2RE=A(K6)*CO+A(K6+1)*SI
AP2IM=-A(K6)*SI+A(K6+1)*CO
CIRE=-.5*(A(2*I-1)+AP2RE)
CIIM=-.5*(A(2*I)+AP2IM)
CNIRE=-.5*(A(2*I-1)-AP2RE)
CNIIM=-.5*(A(2*I)-AP2IM)
A(2*I-1)=CIRE
A(2*I)=CIIM
A(K6)=CNIRE
A(K6+1)=-CNIIM
SIS=SI
SI1=SC*CO*SS
116 CO=CO*SC-SIS*SS
C
C SHIFT C(J)S FOR J=N/2+1 TO J=N UP ONE SLOT
DO I17 I=1,NTOT/2
K8=NTOT/4+I
A(K8-2)=A(K8+1)
117 A(K8-1)=A(K8+1)
DO I50 I=3,NTOT/2
A(I)=2.*A(I)
500 A(I+1)=-2.*A(I+1)
RETURN
END
RHR100C
RHR1010
RHR1020
RHR1030
RHR1040
RHR1050
RHR1060
RHR1070
RHR1080
RHR1090
RHR110C
RHR1110
RHR1120
RHR1130
RHR1140
RHR1150
RHR1160
RHR1170
RHR1180
RHR1190
RHR1200
RHR1210
RHR1220
RHR1230

```

```

C
C ..... RHR 10
C
C SUBROUTINE RHARM RHR 20
C
C PURPOSE RHR 40
C FINDS THE FOURIER COEFFICIENTS OF ONE DIMENSIONAL REAL DATA RHR 50
C
C USAGE RHR 60
C CALL RHARM(A,M,INV,S,IFERR) RHR 70
C
C DESCRIPTION OF PARAMETERS RHR 80
C A - AS INPUT, CONTAINS ONE DIMENSIONAL REAL DATA. A IS RHR 90
C 2*N+4 CORE LOCATIONS, WHERE N = 2**M, 2*N REAL RHR 100
C NUMBERS ARE PUT INTO THE FIRST 2*N CORE LOCATIONS RHR 110
C OF A RHR 120
C AS OUTPUT, A CONTAINS THE FOURIER COEFFICIENTS RHR 130
C A0/2,B0=0,A1,B1,A2,B2,...,AN/2,BN=0 RESPECTIVELY IN RHR 140
C THE FIRST 2N+2 CORE LOCATIONS OF A RHR 150
C M - AN INTEGER WHICH DETERMINES THE SIZE OF THE VECTOR RHR 160
C A. THE SIZE OF A IS 2*(2**M) + 4. RHR 170
C INV - A VECTOR WORK AREA FOR BIT AND INDEX MANIPULATION OF RHR 180
C DIMENSION ONE EIGHTH THE NUMBER OF REAL INPUT, VIZ., RHR 190
C (1/8)*2*(2**M) RHR 200
C S - A VECTOR WORK AREA FOR SINE TABLES WITH DIMENSION RHR 210
C THE SAME AS INV RHR 220
C IFERR - A RETURNED VALUE OF 1 MEANS THAT M IS LESS THAN 3 OR RHR 230
C GREATER THAN 20. OTHERWISE IFERR IS SET = 0 RHR 240
C
C REMARKS RHR 250
C THIS SUBROUTINE GIVES THE FOURIER COEFFICIENTS OF 2*(2**M) RHR 260
C REAL POINTS. SEE SUBROUTINE HARM FOR THREE DIMENSIONAL, RHR 270
C COMPLEX FOURIER TRANSFORMS. RHR 280
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED RHR 290
C HARM RHR 300
C
C METHOD RHR 310
C THE FOURIER COEFFICIENTS A0,B0=0,A1,B1,...,AN,BN=0 ARE RHR 320
C OBTAINED FOR INPUT XJ, J=0,1,2,...,2N-1 FOR THE FOLLOWING RHR 330
C EQUATION (PI = 3.14159...) RHR 340
C
C N-1 RHR 350
C XJ=(1/2)A0+SUM (AK*COS(PI*J*K/N)+BK*SIN(PI*J*K/N))+(1/2)AN(-1) RHR 360
C K=1 RHR 370
C
C SEE REFERENCE UNDER SUBROUTINE HARM RHR 380
C
C ..... RHR 390
C
C SUBROUTINE RHARM(A,M,INV,S,IFERR) RHR 400
C DIMENSION A(1),L(3),INV(1),S(1) RHR 410
C IFSET=1 RHR 420
C L(1)=M RHR 430
C L(2)=0 RHR 440
C L(3)=0 RHR 450
C NTOT=2**M RHR 460
C FN = NTOT RHR 470
C DO 3 I = 2,NTOT/2 RHR 480
C A(I) = -A(I) RHR 490
C DO 6 I = 1,NTOT/2 RHR 500
C A(I) = A(I)/FN RHR 510
C CALL HARM(A,L,INV,S,IFSET,IFERR) RHR 520
C
C MOVE LAST HALF OF A(I)S DOWN ONE SLOT AND ADD A(N) AT BOTTOM TO RHR 530
C GIVE ARRAY FOR A1PRIME AND A2PRIME CALCULATION RHR 540
C
C 21 DO 52 I=1,NTOT/2 RHR 550
C JO=NTOT/2-I RHR 560
C A(IJO)=A(IJO-2) RHR 570
C 52 A(IJO+1)=A(IJO-1) RHR 580
C A(NTOT/2+3)=A(1) RHR 590
C A(NTOT/2+4)=A(2) RHR 600
C
C CALCULATE A1PRIMES AND STORE IN FIRST N SLOTS RHR 610
C CALCULATE A2PRIMES AND STORE IN SECOND N SLOTS IN REVERSE ORDER RHR 620
C KO=NTOT/4 RHR 630
C DO 104 I=1,KO,2 RHR 640
C KI=NTOT/2-I+4 RHR 650
C A1IRE=-.5*(A(I)+A(KI)) RHR 660
C AP2RE=-.5*(A(I+1)+A(KI+1)) RHR 670
C A1IM=.5*(A(I)-A(KI+1)) RHR 680
C AP2IM=-.5*(A(I)-A(KI)) RHR 690
C A(I)=A1IRE RHR 700
C A(I+1)=A1IM RHR 710
C A(KI)=AP2RE RHR 720
C A(KI+1)=AP2IM RHR 730
C NTOT = NTOT/2 RHR 740
C 110 NT=NTOT/4 RHR 750
C DEL=3.1415927/FLOAT(NTOT) RHR 760
C SS=SIGN(DEI) RHR 770
C SC=CO*SS RHR 780
C SI=0.0 RHR 790
C CO=1.0 RHR 800
C
C COMPUTE C(J)S FOR J=0 THRU J=N RHR 810
C 114 DO I16 I=1,NT RHR 820
C K6=NTOT/2-2*I+5 RHR 830

```

```

C
C ..... DRAR 10
C
C SUBROUTINE DRHARM DRAR 20
C
C PURPOSE DRAR 40
C FINDS THE FOURIER COEFFICIENTS OF ONE DIMENSIONAL DOUBLE DRAR 50
C PRECISION REAL DATA DRAR 60
C
C USAGE DRAR 80
C CALL DRHARM(A,M,INV,S,IFERR) DRAR 90
C
C DESCRIPTION OF PARAMETERS DRAR 100
C A - A DOUBLE PRECISION VECTOR DRAR 110
C AS INPUT, CONTAINS ONE DIMENSIONAL REAL DATA. A IS DRAR 120
C 2*N+4 CORE LOCATIONS, WHERE N = 2**M, 2*N REAL DRAR 130
C NUMBERS ARE PUT INTO THE FIRST 2*N CORE LOCATIONS DRAR 140
C OF A DRAR 150
C AS OUTPUT, A CONTAINS THE FOURIER COEFFICIENTS DRAR 160
C A0/2,B0=0,A1,B1,A2,B2,...,AN/2,BN=0 RESPECTIVELY IN DRAR 170
C THE FIRST 2N+2 CORE LOCATIONS OF A DRAR 180
C M - AN INTEGER WHICH DETERMINES THE SIZE OF THE VECTOR DRAR 190
C A. THE SIZE OF A IS 2*(2**M) + 4. DRAR 200
C INV - A VECTOR WORK AREA FOR BIT AND INDEX MANIPULATION OF DRAR 210
C DIMENSION ONE EIGHTH THE NUMBER OF REAL INPUT, VIZ., DRAR 220
C (1/8)*2*(2**M) DRAR 230
C S - A DOUBLE PRECISION VECTOR WORK AREA FOR SINE TABLES DRAR 240
C WITH DIMENSION THE SAME AS INV DRAR 250
C IFERR - A RETURNED VALUE OF 1 MEANS THAT M IS LESS THAN 3 OR DRAR 260
C GREATER THAN 20. OTHERWISE IFERR IS SET = 0 DRAR 270
C
C REMARKS DRAR 280
C THIS SUBROUTINE GIVES THE FOURIER COEFFICIENTS OF 2*(2**M) DRAR 290
C REAL POINTS. SEE SUBROUTINE DHARM FOR THREE DIMENSIONAL, DRAR 300
C DOUBLE PRECISION, COMPLEX FOURIER TRANSFORMS. DRAR 310
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DRAR 320
C DHARM DRAR 330
C
C METHOD DRAR 340
C THE FOURIER COEFFICIENTS A0,B0=0,A1,B1,...,AN,BN=0 ARE DRAR 350
C OBTAINED FOR INPUT XJ, J=0,1,2,...,2N-1 FOR THE FOLLOWING DRAR 360
C EQUATION (PI = 3.14159...) DRAR 370
C
C N-1 DRAR 380
C XJ=(1/2)A0+SUM (AK*COS(PI*J*K/N)+BK*SIN(PI*J*K/N))+(1/2)AN(-1) DRAR 390
C K=1 DRAR 400
C
C SEE REFERENCE UNDER SUBROUTINE DHARM DRAR 410
C
C ..... DRAR 420
C
C SUBROUTINE DRHARM(A,M,INV,S,IFERR) DRAR 430
C DIMENSION A(1),L(3),INV(1),S(1) DRAR 440
C DOUBLE PRECISION A,SI,APIIM,FN,CO,CIRE,AP2IM,S,SS,DEL,CIIM,APIRE, DRAR 450
C I,CNIRE,SC,SIS,AP2RE,CNIIM DRAR 460
C IFSET=1 DRAR 470
C L(1)=M DRAR 480
C L(2)=0 DRAR 490
C L(3)=0 DRAR 500
C NTOT=2**M DRAR 510
C FN = NTOT DRAR 520
C DO 3 I = 2,NTOT/2 DRAR 530
C A(I) = -A(I) DRAR 540
C DO 6 I = 1,NTOT/2 DRAR 550
C A(I) = A(I)/FN DRAR 560
C CALL DHARM(A,L,INV,S,IFSET,IFERR) DRAR 570
C
C MOVE LAST HALF OF A(I)S DOWN ONE SLOT AND ADD A(N) AT BOTTOM TO DRAR 580
C GIVE ARRAY FOR A1PRIME AND A2PRIME CALCULATION DRAR 590
C
C 21 DO 52 I=1,NTOT/2 DRAR 600
C JO=NTOT/2-I DRAR 610
C A(IJO)=A(IJO-2) DRAR 620
C 52 A(IJO+1)=A(IJO-1) DRAR 630
C A(NTOT/2+3)=A(1) DRAR 640
C A(NTOT/2+4)=A(2) DRAR 650
C
C CALCULATE A1PRIMES AND STORE IN FIRST N SLOTS DRAR 660
C CALCULATE A2PRIMES AND STORE IN SECOND N SLOTS IN REVERSE ORDER DRAR 670
C KO=NTOT/4 DRAR 680
C DO 104 I=1,KO,2 DRAR 690
C KI=NTOT/2-I+4 DRAR 700
C APIRE=-.5*(A(I)+A(KI)) DRAR 710
C AP2RE=-.5*(A(I+1)+A(KI+1)) DRAR 720
C APIIM=.5*(A(I)-A(KI+1)) DRAR 730
C AP2IM=-.5*(A(I)-A(KI)) DRAR 740
C A(I)=APIRE DRAR 750
C A(I+1)=APIIM DRAR 760
C A(KI)=AP2RE DRAR 770
C A(KI+1)=AP2IM DRAR 780
C NTOT = NTOT/2 DRAR 790
C 110 NT=NTOT/4 DRAR 800
C DEL=3.141592653589793/DFLOAT(NTOT) DRAR 810
C SS=DSIGN(DEI) DRAR 820
C SC=DCOS(DEI) DRAR 830
C SI=0.0 DRAR 840
C CO=1.0 DRAR 850

```

```

C      COMPUTE C(J)S FOR J=0 THRU J=N
C      DD 116 I=1,NT
      K6=NTOT2-2*I+5
      AP2RE=A(K6)*CO+A(K6+1)*SI
      AP2IM=-A(K6)*SI+A(K6+1)*CO
      CIRE=-.5*(A(2*I-1)+AP2RE)
      CIIM=.5*(A(2*I)+AP2IM)
      CNIRE=.5*(A(2*I-1)-AP2RE)
      CNIIM=.5*(A(2*I)-AP2IM)
      A(2*I-1)=CIRE
      A(2*I)=CIIM
      A(K6)=CNIRE
      A(K6+1)=CNIIM
      SIS=SI
      SI=SI*SC+CO*SS
116 CD=CO*SC-SIS*SS
C      SHIFT C(J)S FOR J=N/2+1 TO J=N UP ONE SLOT
C      DD 117 I=1,NTOT,2
      KB=NTOT+4+I
      A(KB-2)=A(KB)
117 A(KB-1)=A(KB+1)
      DO 500 I=3,NTOT2,2
      A(I) = 2. * A(I)
500 A(I + 1) = -2. * A(I + 1)
      RETURN
      END

```

```

DRAR1000
DRAR1010
DRAR1020
DRAR1030
DRAR1040
DRAR1050
DRAR1060
DRAR1070
DRAR1080
DRAR1090
DRAR1100
DRAR1110
DRAR1120
DRAR1130
DRAR1140
DRAR1150
DRAR1160
DRAR1170
DRAR1180
DRAR1190
DRAR1200
DRAR1210
DRAR1220
DRAR1230
DRAR1240
DRAR1250
DRAR1260
DRAR1270

```

Subroutines APMM and DAPMM

These subroutines determine a linear combination of M linearly independent given continuous real functions, which constitute the Chebyshev approximation of a given real function over a discrete range.

1. Mathematical background

Let us consider a set of discrete data $\{x_k, f_k = f(x_k)\}$, $k = 1, \dots, N$, which defines a real valued function $f(x)$ over a discrete range, and M real continuous given functions $\{\varphi_i(x)\}$, $i = 1, \dots, M$, on an interval containing $[x_1, x_N]$.

The problem is to determine a set of M real coefficients $\{a_i\}$ that minimizes

$$w = \text{Max}_{1 \leq k \leq N} \left| \varphi(x_k) - f_k \right|, \text{ where } \varphi(x) = \sum_{i=1}^M a_i \varphi_i(x)$$

This problem can be expressed in terms of linear programming. At first, let us shift the unknowns so that the resulting ones are nonnegative:

$$b_i = a_i + b_{M+1}, \quad i = 1, \dots, M,$$

where

$$b_{M+1} = -\text{Min} [0, a_1, \dots, a_M]$$

At each point, the error of approximation is given by

$$e_k = \varphi(x_k) - f_k$$

or

$$e_k = \sum_{i=1}^{M+1} b_i \varphi_i(x_k) - f_k$$

where

$$\varphi_{M+1}(x) = -\sum_{i=1}^M \varphi_i(x)$$

By definition

$$w = \text{Max}_{1 \leq k \leq N} \left| e_k \right|$$

If we put $\varphi_{ik} = \varphi_i(x_k)$, the original problem can be expressed as: Minimize w , subject to:

$$w + \sum_{i=1}^{M+1} \varphi_{ik} b_i \geq f_k$$

$$w - \sum_{i=1}^{M+1} \varphi_{ik} b_i \geq f_k$$

$$b_i \geq 0 \text{ for } i = 1, \dots, M+1$$

$$w \geq 0$$

In practice, it is more convenient to solve the following dual problem in the nonnegative variables $\{s_k, t_k\}$, $k = 1, \dots, N$:

$$\text{Maximize } \sum_{k=1}^N f_k (s_k - t_k), \text{ subject to:}$$

$$\sum_{k=1}^N (s_k + t_k) \leq 1$$

$$\sum_{k=1}^N \varphi_{ik} (s_k - t_k) \leq 0, \quad i = 1, \dots, M+1$$

$$s_k \geq 0, \quad t_k \geq 0, \quad \text{for } k = 1, \dots, N$$

Using the variables of the dual problem as slacks, these $n + 2$ constraints can be written as equalities:

$$w + \sum_{k=1}^N (s_k + t_k) = 1$$

$$b_i + \sum_{k=1}^N \varphi_{ik} (s_k - t_k) = 0$$

The dual problem is solved by means of a revised simplex method (inverse matrix algorithm) using the following initial simplex tableau where w, b_1, \dots, b_{M+1} are basic variables:

Note that the entries in the transformed top row under w, b_1, \dots, b_{M+1} will be the optimal solution to the primal, that is, w and the b_i 's.

A condensed tableau is used for calculation. The correspondence between the subscripts of the full tableau and these of the condensed one is given by means of the index vector IHE.

When the procedure has reached the optimum, the top row contains on return:

w	Maximum error of approximation
$b_i, \quad i = 1, \dots, M+1$	Coefficients from which we can get the unknowns by $a_i = b_i - b_{M+1}$ for $i = 1, \dots, M$
$s_k, \quad k = 1, \dots, N$	The error at the given points, according to $e_k = s_k - w$

	Variables	$s_1 \dots s_N$	$t_1 \dots t_N$	w	b_1	b_2	\dots	b_{M+1}
Top Row	Maximize	$f_1 \dots f_N$	$-f_1 \dots -f_N$	0	0	0	\dots	0
	1	$= 1 \dots 1$	$1 \dots 1$	1	0	0	\dots	0
	0	$= \varphi_{11} \dots \varphi_{1N}$	$-\varphi_{11} \dots -\varphi_{1N}$	0	1	0	\dots	0
	0	$= \varphi_{21} \dots \varphi_{2N}$	$-\varphi_{21} \dots -\varphi_{2N}$	0	0	1	\dots	0
	0	$= \varphi_{M+1,1} \dots \varphi_{M+1,N}$	$-\varphi_{M+1,1} \dots -\varphi_{M+1,N}$	0	0	\dots		1

2. Programming considerations

For economy of storage requirements, the full simplex tableau is not stored, but only the top row at any iteration step. Therefore, we must update an inverse matrix T which allows us to generate the needed pivot column at any iteration step from the corresponding initial column. The procedure terminates for the following reasons:

a. An optimal top row is reached, indicated by the resultant error parameter IER, which is set to zero. All the relevant data are contained in this top row. The corresponding subscripts are stored in a part of the integer vector IHE.

b. No suitable pivot can be found. The resultant error parameter IER is set to -1.

c. The number of iterations ITER has reached the internal maximum N+M. The error parameter IER is set to 1 as a warning.

The subroutines APMM and DAPMM contain two tests for loss of significance:

a. The first test is made when an initial column is multiplied by the rows of matrix T. The corresponding result DSUM is set equal to zero if the following inequality is valid:

$$|DSUM| \leq HELP * EPS$$

where HELP is the absolutely greatest intermediate sum formed during calculation of the scalar product-sum DSUM, and EPS is an internal tolerance:

$$EPS = \begin{cases} 10^{-5} & \text{in APMM} \\ 10^{-14} & \text{in DAPMM} \end{cases}$$

b. The second test is made when a new element in the top row TOP is generated. The new element \overline{TOP}_i is calculated from the previous value \overline{TOP}_i by the addition

$$\overline{TOP}_i = \overline{TOP}_i + DSUM_i$$

The new value \overline{TOP}_i is replaced by zero if

$$|\overline{TOP}_i + DSUM_i| \leq |DSUM_i| * EPS$$

where EPS is the above-mentioned internal tolerance. Some remarks are in order:

a. In cases where the given approximating functions are polynomials, APMM and DAPMM are more efficient when used with orthogonal polynomials than with ordinary polynomials. The number of iterations required usually decreases with orthogonal functions,

and the magnitude of the roundoff errors may be significantly reduced. When using an ordinary polynomial approximating function it seems that the roundoff errors are due to the wide range of values of the elements $\phi_{i,k}$ in the initial tableau.

b. If approximation by normal Chebyshev polynomials, shifted Chebyshev polynomials, Legendre polynomials, Laguerre polynomials, or Hermite polynomials is desired, the subroutines CNP, CSP, LEP, LAP, or HEP, respectively from the SSP (Scientific Subroutine Package) can be used as the external subroutine FCT.

For reference see:

1. I. Barrodale and A. Young, "Algorithms for Best L_1 and L_∞ , Linear Approximations on a Discrete Set", Numerische Mathematik, vol. 8, iss. 3 (1966), pp. 295-306.
2. S. Vajda, Mathematical Programming, Addison-Wesley Publishing Company, Inc., London, 1961.

C	APMM	10
C	APMM	20
C	APMM	30
C	APMM	40
C	APMM	50
C	APMM	60
C	APMM	70
C	APMM	80
C	APMM	90
C	APMM	100
C	APMM	110
C	APMM	120
C	APMM	130
C	APMM	140
C	APMM	150
C	APMM	160
C	APMM	170
C	APMM	180
C	APMM	190
C	APMM	200
C	APMM	210
C	APMM	220
C	APMM	230
C	APMM	240
C	APMM	250
C	APMM	260
C	APMM	270
C	APMM	280
C	APMM	290
C	APMM	300
C	APMM	310
C	APMM	320
C	APMM	330
C	APMM	340
C	APMM	350
C	APMM	360
C	APMM	370
C	APMM	380
C	APMM	390
C	APMM	400
C	APMM	410
C	APMM	420
C	APMM	430
C	APMM	440
C	APMM	450
C	APMM	460
C	APMM	470
C	APMM	480
C	APMM	490
C	APMM	500
C	APMM	510
C	APMM	520
C	APMM	530
C	APMM	540
C	APMM	550
C	APMM	560
C	APMM	570
C	APMM	580
C	APMM	590
C	APMM	600
C	APMM	610
C	APMM	620
C	APMM	630
C	APMM	640
C	APMM	650
C	APMM	660
C	APMM	670
C	APMM	680
C	APMM	690
C	APMM	700
C	APMM	710
C	APMM	720
C	APMM	730
C	APMM	740

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C      L-SUB-INFINITY, LINEAR APPROXIMATIONS ON A DISCRETE SET,  APMM 750
C      NUMERISCHE MATHEMATIK, VOL.8, ISS.3 (1966), PP.295-306.  APMM 760
C      .....  APMM 770
C      .....  APMM 780
C      .....  APMM 790
C      SUBROUTINE APMMFCT,N,M,TOP,THE,PIV,T,ITER,IER)  APMM 800
C      .....  APMM 810
C      DIMENSION TOP(1),THE(1),PIV(1),T(1)  APMM 830
C      DOUBLE PRECISION DSUM  APMM 840
C      TEST ON WRONG INPUT PARAMETERS N AND M  APMM 850
C      IER=0  APMM 860
C      IF (N-1) 81,81.1  APMM 870
C      1 IF(M) 81,81.2  APMM 880
C      INITIALIZE CHARACTERISTIC VECTORS FOR THE TABLEAU  APMM 890
C      2 IER=0  APMM 900
C      PREPARE TOP-ROW TOP  APMM 910
C      DO 3 I=1,N  APMM 920
C      K=I+N  APMM 930
C      J=K+N  APMM 940
C      TOP(J)=TOP(K)  APMM 950
C      3 TOP(K)=TOP(I)  APMM 960
C      PREPARE INVERSE TRANSFORMATION MATRIX T  APMM 1000
C      L=1  APMM 1010
C      LL=L+L  APMM 1020
C      DO 4 I=1,LL  APMM 1030
C      T(I)=0.  APMM 1040
C      K=I  APMM 1050
C      J=L+1  APMM 1060
C      DO 5 I=1,L  APMM 1070
C      T(K)=1.  APMM 1080
C      5 K=K+J  APMM 1090
C      PREPARE INDEX-VECTOR IHE  APMM 1100
C      DO 6 I=1,L  APMM 1110
C      K=I+L  APMM 1120
C      J=K+L  APMM 1130
C      IHE(I)=I  APMM 1140
C      IHE(K)=I  APMM 1150
C      6 IHE(J)=I-I  APMM 1160
C      N=N+N  APMM 1170
C      K=K+L  APMM 1180
C      J=K+N  APMM 1190
C      DO 7 I=1,N  APMM 1200
C      K=I+1  APMM 1210
C      IHE(K)=I  APMM 1220
C      J=J+1  APMM 1230
C      7 IHE(J)=I  APMM 1240
C      SET COUNTER IER FOR ITERATION-STEPS  APMM 1250
C      IER=1  APMM 1260
C      8 IER=1+IER  APMM 1270
C      TEST FOR MAXIMUM ITERATION-STEPS  APMM 1280
C      IF (N=IER) 9,9,10  APMM 1290
C      9 IER=1  APMM 1300
C      GO TO 6  APMM 1310
C      DETERMINE THE COLUMN WITH THE MOST POSITIVE ELEMENT IN TOP  APMM 1320
C      10 ISE=0  APMM 1330
C      TP=0  APMM 1340
C      K=L+L+L  APMM 1350
C      SAVE=0.  APMM 1360
C      START TOP-LOOP  APMM 1370
C      DO 14 I=1,N  APMM 1380
C      IDO=K+I  APMM 1390
C      HELP=TOP(I)  APMM 1400
C      IF (HELP > SAVE) 12,12,11  APMM 1410
C      11 SAVE=HELP  APMM 1420
C      IPIV=I  APMM 1430
C      12 IF (IHE(IDO)) 14,13,15  APMM 1440
C      13 ISE=I  APMM 1450
C      14 CONTINUE  APMM 1460
C      END OF TOP-LOOP  APMM 1470
C      IS OPTIMAL TABLEAU REACHED?  APMM 1480
C      IF (IPIV) 49,49,15  APMM 1490
C      DETERMINE THE PIVOT-ELEMENT FOR THE COLUMN CHOSEN ABOVE  APMM 1500
C      15 ILAB=1  APMM 1510
C      IND=0  APMM 1520
C      J=ISE  APMM 1530
C      IF (J) 21,21,34  APMM 1540
C      TRANSFER K-TH COLUMN FROM T TO PIV  APMM 1550
C      16 K=(K-1)*L  APMM 1560
C      DO 17 I=1,L  APMM 1570
C      J=L+I  APMM 1580
C      K=K+1  APMM 1590
C      17 PIV(J)=T(K)  APMM 1600
C      IS ANOTHER COLUMN NEEDED FOR SEARCH FOR PIVOT-ELEMENT  APMM 1610
C      18 IF (ISE) 22,22,19  APMM 1620
C      19 ISE=ISE  APMM 1630
C      TRANSFER COLUMNS IN PIV  APMM 1640
C      J=L+1  APMM 1650
C      IDO=L+L  APMM 1660
C      DO 20 I=J,IND  APMM 1670
C      K=I+L  APMM 1680
C      20 PIV(K)=PIV(I)  APMM 1690
C      21 J=PIV  APMM 1700
C      GO TO 34  APMM 1710
C      SEARCH PIVOT-ELEMENT PIV(IND)  APMM 1720
C      22 SAVE=1.E38  APMM 1730
C      IDO=0  APMM 1740
C      K=L+1  APMM 1750
C      LL=L+L  APMM 1760
C      IND=0  APMM 1770
C      START PIVOT-LOOP  APMM 1780
C      DO 29 I=K,LL  APMM 1790
C      J=I+L  APMM 1800
C      HELP=PIV(I)  APMM 1810
C      IF (HELP) 29,29,23  APMM 1820
C      23 HELP=HELP  APMM 1830
C      IF (ISE) 26,24,26  APMM 1840
C      24 IF (IHE(J)) 27,25,27  APMM 1850
C      25 IDO=I  APMM 1860
C      GO TO 29  APMM 1870
C      26 HELP=PIV(J)/HELP  APMM 1880
C      27 IF (HELP > SAVE) 28,25,29  APMM 1890
C      28 SAVE=HELP  APMM 1900

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IND=I  APMM 2040
29 CONTINUE  APMM 2050
END OF PIVOT-LOOP  APMM 2060
TEST FOR SUITABLE PIVOT-ELEMENT  APMM 2070
IF (IND) 30,30,32  APMM 2080
30 IF (IDO) 68,58,31  APMM 2090
31 IND=IDO  APMM 2100
PIVOT-ELEMENT IS STORED IN PIV(IND)  APMM 2110
COMPUTE THE RECIPROCAL OF THE PIVOT-ELEMENT REPI  APMM 2120
32 REPI=1./PIV(IND)  APMM 2130
IND=IND-L  APMM 2140
UPDATE THE TOP-ROW TOP OF THE TABLEAU  APMM 2150
ILAB=0  APMM 2160
SAVE=TOP(PIV)*REPI  APMM 2170
TOP(PIV)=SAVE  APMM 2180
INITIALIZE J AS COUNTER FOR TOP-LOOP  APMM 2190
J=NAN  APMM 2200
33 IF (J-IPIV) 34,53,34  APMM 2210
34 K=0  APMM 2220
SEARCH COLUMN IN TRANSFORMATION-MATRIX T  APMM 2230
DO 36 I=1,L  APMM 2240
IF (IHE(I)-J) 35,35,36  APMM 2250
35 K=I  APMM 2260
IF (ILAB) 50,50,15  APMM 2270
36 CONTINUE  APMM 2280
GENERATE COLUMN USING SUBROUTINE FCT AND TRANSFORMATION-MATRIX  APMM 2290
I=L+L+NAN*J  APMM 2300
I=IHE(I)-N  APMM 2310
IF (I) 37,37,39  APMM 2320
37 I=I+N  APMM 2330
K=1  APMM 2340
38 I=I+NAN  APMM 2350
CALL SUBROUTINE FCT  APMM 2360
CALL FCT(PIV,TOP(I),M-1)  APMM 2370
PREPARE THE CALLED VECTOR PIV  APMM 2380
DSUM=0.0  APMM 2390
IDO=M  APMM 2400
DO 41 I=1,M  APMM 2410
HELP=PIV(IDO)  APMM 2420
IF (K) 35,39,40  APMM 2430
39 HELP=HELP  APMM 2440
40 DSUM=DSUM+DBLE(HELP)  APMM 2450
PIV(IDO-1)=HELP  APMM 2460
41 IDO=IDO-1  APMM 2470
PIV(L)=DSUM  APMM 2480
PIV(I)=1.  APMM 2490
TRANSFORM VECTOR PIV WITH ROWS OF MATRIX T  APMM 2500
IDO=IND  APMM 2510
IF (ILAB) 44,44,42  APMM 2520
42 K=1  APMM 2530
43 IDO=K  APMM 2540
44 DSUM=C.L  APMM 2550
HELP=0.  APMM 2560
START MULTIPLICATION-LOOP  APMM 2570
DO 46 I=1,L  APMM 2580
DSUM=DSUM+DBLE(PIV(I)*T(IDO))  APMM 2590
TOL=ABS(SNGL(DSUM))  APMM 2600
IF (TOL-HELP) 46,46,45  APMM 2610
45 HELP=TOL  APMM 2620
45 IDO=IDOL  APMM 2630
END OF MULTIPLICATION-LOOP  APMM 2640
TOL=1.E-5*HELP  APMM 2650
IF (ABS(SNGL(DSUM))-TOL) 47,47,48  APMM 2660
47 DSUM=0.0  APMM 2670
48 IF (ILAB) 51,51,49  APMM 2680
49 I=K+L  APMM 2690
PIV(I)=DSUM  APMM 2700
TEST FOR LAST COLUMN-TERM  APMM 2710
K=K+1  APMM 2720
IF (K-L) 43,43,18  APMM 2730
50 I=(K-1)*L+IND  APMM 2740
DSUM=I  APMM 2750
COMPUTE NEW TOP-ELEMENT  APMM 2760
51 DSUM=DSUM+DBLE(SAVE)  APMM 2770
TOL=1.E-5*ABS(SNGL(DSUM))  APMM 2780
TOP(J)=TOP(J)+SNGL(DSUM)  APMM 2790
IF (ABS(TOP(J))-TOL) 52,52,53  APMM 2800
52 TOP(J)=0.  APMM 2810
TEST FOR LAST TOP-TERM  APMM 2820
53 J=J-1  APMM 2830
IF (J) 54,54,33  APMM 2840
END OF TOP-LOOP  APMM 2850
TRANSFER K PIVOT-COLUMN  APMM 2860
54 I=IND+L  APMM 2870
PIV(I)=1.  APMM 2880
DO 55 I=1,L  APMM 2890
J=I+L  APMM 2900
55 PIV(I)=PIV(J)*REPI  APMM 2910
UPDATE TRANSFORMATION-MATRIX T  APMM 2920
J=0  APMM 2930
DO 57 I=1,L  APMM 2940
IDO=J+IND  APMM 2950
SAVE=T(IDO)  APMM 2960
T(IDO)=0.  APMM 2970
DO 56 K=1,L  APMM 2980
ISE=K+J  APMM 2990
56 T(ISE)=T(ISE)+SAVE*PIV(K)  APMM 3000
57 J=J+L  APMM 3010
UPDATE INDEX-VECTOR IHE  APMM 3020
INITIALIZE CHARACTERISTICS  APMM 3030
J=0  APMM 3040
K=0  APMM 3050
IDO=0  APMM 3060
START QUESTION-LOOP  APMM 3070
DO 61 I=1,L  APMM 3080
LL=I+L  APMM 3090
ILAB=IHE(LL)  APMM 3100
IF (IHE(I)-IPIV) 59,58,59  APMM 3110
59 ISE=I  APMM 3120
J=ILAB  APMM 3130

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59 IF(I148-IND) 61,60,61
60 IOD=I
K=IHE(I)
61 CONTINUE
END OF QUESTION-LOOP
START MODIFICATION
IF(K) 52,62+63
IHE(100)=IPIV
IF(ISE) 67,67,65
63 IF(IND-J) 64,66,64
64 LL=L+L+L+4*N
K=K+LL
I=IPIV+LL
ILAB=IHE(K)
IHE(K)=IHE(I)
IHE(I)=ILAB
IF(ISE) 67,67,65
65 IOD=IOD+L
I=I+L
IHE(100)=J
IHE(I)=IND
66 IHE(ISE)=0
67 LL=L+L
J=LL+IND
I=LL+IPIV
ILAB=IHE(I)
IHE(I)=IHE(J)
IHE(J)=ILAB
END OF MODIFICATION
GO TO B
SET ERROR PARAMETER IER=-1 SINCE NO SUITABLE PIVOT IS FOUND
68 IER=-1
EVALUATE FINAL TABLEU
COMPUTE AND SAVE AS MAXIMUM ERROR OF APPROXIMATION AND
HELP AS ADDITIVE CONSTANT FOR RESULTING COEFFICIENTS
69 SAVE=C
HELP=0.
K=L+L+L
DO 73 I=1,NAN
IOD=K+I
J=IHE(100)
IF(J) 71,70,73
70 SAVE=-TOP(I)
71 IF(M+J+1) 73,72,73
72 HELP=TOP(I)
73 CONTINUE
PREPARE T, TOP, PIV
T(I)=SAVE
IOD=NAN+I
J=NAN+N
DO 74 I=1,IOD
74 TOP(I)=SAVE
DO 75 I=1,M
75 PIV(I)=HELP
COMPUTE COEFFICIENTS OF RESULTING POLYNOMIAL IN PIV(I) UP TO PIV(M)
AND CALCULATE ERRORS AT GIVEN NODES IN TOP(I) UP TO TOP(N)
DO 79 I=1,NAN
IOD=K+I
J=IHE(100)
IF(J) 75,79,77
76 J=J
PIV(J)=HELP-TOP(I)
GO TO 79
77 IF(IJ-N) 78,79,79
78 J=J+NAN
TOP(J)=SAVE+TOP(I)
79 CONTINUE
DO 80 I=1,N
IOD=NAN+I
80 TOP(I)=TOP(100)
81 RETURN
END

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APMM3330
APMM3340
APMM3350
APMM3360
APMM3370
APMM3380
APMM3390
APMM3400
APMM3410
APMM3420
APMM3430
APMM3440
APMM3450
APMM3460
APMM3470
APMM3480
APMM3490
APMM3500
APMM3510
APMM3520
APMM3530
APMM3540
APMM3550
APMM3560
APMM3570
APMM3580
APMM3590
APMM3600
APMM3610
APMM3620
APMM3630
APMM3640
APMM3650
APMM3660
APMM3670
APMM3680
APMM3690
APMM3700
APMM3710
APMM3720
APMM3730
APMM3740
APMM3750
APMM3760
APMM3770
APMM3780
APMM3790
APMM3800
APMM3810
APMM3820
APMM3830
APMM3840
APMM3850
APMM3860
APMM3870
APMM3880
APMM3890
APMM3900
APMM3910
APMM3920
APMM3930
APMM3940
APMM3950
APMM3960
APMM3970
APMM3980
APMM3990
APMM4000
APMM4010
APMM4020
APMM4030
APMM4040
APMM4050
APMM4060
APMM4070
APMM4080
APMM4090
APMM4100

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C PIV - DOUBLE PRECISION VECTOR OF DIMENSION 3*M+6. DAPM 450
C ON RETURN PIV CONTAINS AT PIV(I) UP TO PIV(M) THE DAPM 460
C RESULTING COEFFICIENTS OF LINEAR APPROXIMATION. DAPM 470
C T - DOUBLE PRECISION AUXILIARY VECTOR OF DIMENSION DAPM 480
C (M+2)*(M+2) DAPM 490
C ITER - RESULTANT INTEGER WHICH SPECIFIES THE NUMBER OF DAPM 500
C ITERATIONS NEEDED DAPM 510
C IER - RESULTANT ERROR PARAMETER CODED IN THE FOLLOWING DAPM 520
C FORM DAPM 530
C IER=0 - NO ERROR DAPM 540
C IER=1 - THE NUMBER OF ITERATIONS HAS REACHED DAPM 550
C THE INTERNAL MAXIMUM M+M DAPM 560
C IER=-1 - NO RESULT BECAUSE OF WRONG INPUT PARA- DAPM 570
C METER M OR N OR SINCE AT SOME ITERATION DAPM 580
C NO SUITABLE PIVOT COULD BE FOUND DAPM 590
C REMARKS DAPM 600
C NO ACTION BESIDES ERROR MESSAGE IN CASE M LESS THAN 1 OR DAPM 610
C N LESS THAN 2. DAPM 620
C SURROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DAPM 630
C THE EXTERNAL SUBROUTINE FCT MUST BE FURNISHED BY THE USER. DAPM 640
C METHOD DAPM 650
C THE PROBLEM OF APPROXIMATION A TABULATED FUNCTION BY ANY DAPM 660
C LINEAR COMBINATION OF GIVEN FUNCTIONS IN THE SENSE OF DAPM 670
C CHERYSHEV (I.E. TO MINIMIZE THE MAXIMUM ERROR) IS TRANS- DAPM 710
C FORMED INTO A LINEAR PROGRAMMING PROBLEM. DAPMM USES A DAPM 720
C REVISED SIMPLEX METHOD TO SOLVE A CORRESPONDING DUAL DAPM 730
C PROBLEM. FOR REFERENCE, SEE DAPM 740
C I. BARRODALE/A. YOUNG, ALGORITHMS FOR BEST L-SUB-ONE AND DAPM 750
C L-SUB-INFINITY, LINEAR APPROXIMATIONS ON A DISCRETE SET, DAPM 760
C NUMERISCHE MATHEMATIK, VOL. 4, ISS. 3 (1966), PP. 295-306. DAPM 773
C DAPM 780
C DAPM 790
C SURROUTINE DAPMM(FCT,N,M,TOP,IHE,PIV,T,ITER,IER) DAPM 800
C DAPM 810
C DAPM 820
C DIMENSION TOP(1),IHE(1),PIV(1),T(1) DAPM 830
C DOUBLE PRECISION DSUM,TOP,PIV,T,SAVE,HELP,REPI,TOL DAPM 840
C DAPM 850
C TEST ON WRONG INPUT PARAMETERS N AND M DAPM 860
C IER=-1 DAPM 870
C IF (N-1) 81,81,1 DAPM 880
C 1 IF(M) 81,31,2 DAPM 890
C DAPM 900
C INITIALIZE CHARACTERISTIC VECTORS FOR THE TABLEU DAPM 910
C 2 IER=0 DAPM 920
C DAPM 930
C PREPARE TOP-ROW TOP DAPM 940
C DO 3 I=1,N DAPM 950
C K=I+N DAPM 960
C J=K+M DAPM 970
C TOP(I)=TOP(K) DAPM 980
C 3 TOP(K)=-TOP(I) DAPM 990
C DAPM 1000
C PREPARE INVERSE TRANSFORMATION MATRIX T DAPM 1010
C L=M+2 DAPM 1020
C LL=L+L DAPM 1030
C DO 4 I=1,LL DAPM 1040
C T(I)=0,0 DAPM 1050
C K=I DAPM 1060
C J=L+1 DAPM 1070
C DO 5 I=1,L DAPM 1080
C T(K)=1,0 DAPM 1090
C 5 K=K+J DAPM 1100
C DAPM 1110
C PREPARE INDEX-VECTOR IHE DAPM 1120
C DO 6 I=1,L DAPM 1130
C K=I+L DAPM 1140
C J=K+L DAPM 1150
C IHE(I)=0 DAPM 1160
C IHE(K)=I DAPM 1170
C 6 IHE(J)=I-I DAPM 1180
C NAN=NAN DAPM 1190
C K=L+L+L DAPM 1200
C J=K+NAN DAPM 1210
C DO 7 I=1,NAN DAPM 1220
C K=K+1 DAPM 1230
C IHE(K)=I DAPM 1240
C J=J+1 DAPM 1250
C 7 IHE(J)=I DAPM 1260
C DAPM 1270
C SET COUNTER ITER FOR ITERATION-STEPS DAPM 1280
C ITER=-1 DAPM 1290
C 8 ITER=ITER+1 DAPM 1300
C TEST FOR MAXIMUM ITERATION-STEPS DAPM 1310
C IF(NM-ITER) 9,9,10 DAPM 1320
C 9 IER=1 DAPM 1330
C GO TO 6 DAPM 1340
C DAPM 1350
C DAPM 1360
C DAPM 1370
C DETERMINE THE COLUMN WITH THE MOST POSITIVE ELEMENT IN TOP DAPM 1380
C 10 ISE=0 DAPM 1390
C IPIV=0 DAPM 1400
C K=L+L+L DAPM 1410
C SAVE=0,0 DAPM 1420
C START TOP-LOOP DAPM 1430
C DO 14 I=1,NAN DAPM 1440
C IOD=K+I DAPM 1450
C HELP=TOP(I) DAPM 1460
C IF(HELP-SAVE) 12,12,11 DAPM 1470
C 11 SAVE=HELP DAPM 1480
C IPIV=I DAPM 1490
C 12 IF(IHE(100)) 14,13,14 DAPM 1500
C 13 ISE=I DAPM 1510
C 14 CONTINUE DAPM 1520
C END OF TOP-LOOP DAPM 1530
C DAPM 1540
C IS OPTIMAL TABLEU REACHED DAPM 1550
C IF(PIV) 69,69,15 DAPM 1560
C DAPM 1570
C DETERMINE THE PIVOT-ELEMENT FOR THE COLUMN CHOSEN ABOVE DAPM 1580
C 15 ILAB=1 DAPM 1590
C IND=0 DAPM 1600
C J=ISE DAPM 1610
C IF(J) 21,21,34 DAPM 1620
C DAPM 1630
C TRANSFER K-TH COLUMN FROM T TO PIV DAPM 1640
C 16 K=(K-1)+L DAPM 1650
C DO 17 I=1,L DAPM 1660
C J=L+I DAPM 1670
C K=K+1 DAPM 1680
C 17 PIV(J)=T(K) DAPM 1690
C DAPM 1700
C IS ANOTHER COLUMN NEEDED FOR SEARCH FOR PIVOT-ELEMENT DAPM 1710
C 18 IF(ISE) 22,22,19 DAPM 1720
C DAPM 1730

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19 ISE=-ISE
C
C TRANSFER COLUMNS IN PIV
J=L+1
IDD=L+L
DO 20 I=J,100
K=I+L
20 PIV(K)=PIV(I)
21 J=IPIV
GO TO 34
C
C SEARCH PIVOT-ELEMENT PIV(IND)
22 SAVE=1.038
IDD=0
K=L+1
LL=L+L
IND=0
C
C START PIVOT-LOOP
DO 29 I=K,LL
J=I+L
HELP=PIV(I)
IF(HELP) 29,29,23
23 HELP=HELP
IF(ISE) 26,24,26
24 IF(HELP) 27,25,27
25 IDD=I
GO TO 29
26 HELP=-PIV(J)/HELP
27 IF(HELP-SAVE) 28,29,29
28 SAVE=HELP
IND=I
29 CONTINUE
END OF PIVOT-LOOP
C
C TEST FOR SUITABLE PIVOT-ELEMENT
IF(IND) 30,30,32
30 IF(IND) 68,68,31
31 IND=IDU
PIVOT-ELEMENT IS STORED IN PIV(IND)
C
C COMPUTE THE RECIPROCAL OF THE PIVOT-ELEMENT REPI
32 REPI=1.00/PIV(IND)
IND=IND-L
C
C UPDATE THE TOP-ROW TOP OF THE TABLEAU
ILAB=0
SAVE=-TOP(IPIV)*REPI
TOP(IPIV)=SAVE
C
C INITIALIZE J AS COUNTER FOR TOP-LOOP
J=NaN
33 IF(J-[PIV] 54,53,34
34 K=0
C
C SEARCH COLUMN IN TRANSFORMATION-MATRIX T
DO 36 I=1,L
IF(HE(I)-J) 36,35,36
35 K=I
IF(ILAB) 50,50,10
36 CONTINUE
C
C GENERATE COLUMN USING SUBROUTINE FCT AND TRANSFORMATION-MATRIX
I=L+L+L+NaN+J
I=HE(I)-N
IF(I) 37,37,38
37 I=I+N
K=I
38 I=I+NaN
C
C CALL SUBROUTINE FCT
CALL FCT(PIV,TOP(I),M-1)
C
C PREPARE THE CALLED VECTOR PIV
DSUM=0.00
IDD=M
DO 41 I=1,M
HELP=PIV(IDD)
IF(K) 39,39,40
39 HELP=HELP
40 DSUM=DSUM+HELP
PIV(IDD+1)=HELP
41 IDD=IDD-1
PIV(L)=DSUM
PIV(1)=1.00
C
C TRANSFORM VECTOR PIV WITH ROWS OF MATRIX T
IDD=IND
IF(ILAB) 44,44,42
42 K=I
43 IDD=K
44 DSUM=0.00
HELP=0.00
C
C START MULTIPLICATION-LOOP
DO 46 I=1,L
DSUM=DSUM+PIV(I)*F(IDD)
TOL=DABS(DSUM)
IF(TOL-HELP) 46,46,45
45 HELP=TOL
46 IDD=IDD+L
END OF MULTIPLICATION-LOOP
C
C TOL=1.0-14*HELP
IF(DABS(DSUM)-TOL) 47,47,48
47 DSUM=0.00
48 IF(ILAB) 51,51,49
49 I=K+L
PIV(I)=DSUM
C
C TEST FOR LAST COLUMN-TERM
K=K+1
IF(K-L) 43,43,18
50 I=K-1;L+1;IND
DSUM=T(I)
C
C COMPUTE NEW TOP-ELEMENT
51 DSUM=DSUM*SAVE
TOL=1.0-14*DABS(DSUM)
TOP(J)=TOP(J)+DSUM
IF(DABS(TOP(J))-TOL) 52,52,53
52 TOP(J)=0.00
C
C TEST FOR LAST TOP-TERM
53 J=J-1
IF(J) 54,54,33
END OF TOP-LOOP
C
C TRANSFORM PIVOT-COLUMN
DAPM1740
DAPM1750
DAPM1760
DAPM1770
DAPM1780
DAPM1790
DAPM1800
DAPM1810
DAPM1820
DAPM1830
DAPM1840
DAPM1850
DAPM1860
DAPM1870
DAPM1880
DAPM1890
DAPM1900
DAPM1910
DAPM1920
DAPM1930
DAPM1940
DAPM1950
DAPM1960
DAPM1970
DAPM1980
DAPM1990
DAPM2000
DAPM2010
DAPM2020
DAPM2030
DAPM2040
DAPM2050
DAPM2060
DAPM2070
DAPM2080
DAPM2090
DAPM2100
DAPM2110
DAPM2120
DAPM2130
DAPM2140
DAPM2150
DAPM2160
DAPM2170
DAPM2180
DAPM2190
DAPM2200
DAPM2210
DAPM2220
DAPM2230
DAPM2240
DAPM2250
DAPM2260
DAPM2270
DAPM2280
DAPM2290
DAPM2300
DAPM2310
DAPM2320
DAPM2330
DAPM2340
DAPM2350
DAPM2360
DAPM2370
DAPM2380
DAPM2390
DAPM2400
DAPM2410
DAPM2420
DAPM2430
DAPM2440
DAPM2450
DAPM2460
DAPM2470
DAPM2480
DAPM2490
DAPM2500
DAPM2510
DAPM2520
DAPM2530
DAPM2540
DAPM2550
DAPM2560
DAPM2570
DAPM2580
DAPM2590
DAPM2600
DAPM2610
DAPM2620
DAPM2630
DAPM2640
DAPM2650
DAPM2660
DAPM2670
DAPM2680
DAPM2690
DAPM2700
DAPM2710
DAPM2720
DAPM2730
DAPM2740
DAPM2750
DAPM2760
DAPM2770
DAPM2780
DAPM2790
DAPM2800
DAPM2810
DAPM2820
DAPM2830
DAPM2840
DAPM2850
DAPM2860
DAPM2870
DAPM2880
DAPM2890
DAPM2900
DAPM2910
DAPM2920
DAPM2930
DAPM2940
DAPM2950
DAPM2960
DAPM2970
DAPM2980
DAPM2990
DAPM3000
DAPM3010
DAPM3020
54 I=IND+L
PIV(I)=1.00
DO 55 I=1,L
J=I+L
55 PIV(I)=PIV(J)*REPI
C
C UPDATE TRANSFORMATION-MATRIX T
J=0
DO 57 I=1,L
IDD=J+1;IDD
SAVE=T(IDD)
T(IDD)=0.00
DO 56 K=1,L
ISE=K+J
56 T(ISE)=T(ISE)+SAVE*PIV(K)
57 J=J+L
C
C UPDATE INDEX-VECTOR IMF
INITIALIZE CHARACTERISTICS
J=0
K=0
ISE=0
IDD=0
C
C START QUESTION-LOOP
DO 61 I=1,L
LL=I+L
ILAB=HE(LL)
IF(HE(I)-IPIV) 59,58,59
58 ISE=I
J=I+L
59 IF(ILAB-IND) 61,60,61
60 IDD=I
K=HE(I)
51 CONTINUE
END OF QUESTION-LOOP
C
C START MODIFICATION
IF(K) 62,62,63
62 HE(IND)=IPIV
IF(ISE) 67,67,65
63 IF(IND-J) 64,66,64
64 LL=L+L+NaN
K=K+LL
I=IPIV+LL
ILAB=HE(K)
HE(K)=HE(I)
HE(I)=ILAB
IF(HE(I)-IPIV) 67,67,65
65 IDD=IDD+L
I=ISE+I
HE(IND)=J
HE(I)=IND
66 HE(ISE)=IPIV
67 LL=LL+L
J=LL+IND
I=LL+IPIV
ILAB=HE(I)
HE(I)=HE(J)
HE(J)=ILAB
HE(I)=ILAB
END OF MODIFICATION
C
C GO TO R
C
C SET ERROR PARAMETER IERR=-1 SINCE NO SUITABLE PIVOT IS FOUND
42 IERR=-1
C
C EVALUATE FINAL TABLEAU
COMPUTE SAVE AS MAXIMUM ERROR OF APPROXIMATION AND
HELP AS ADDITIVE CONSTANT FOR RESULTING COEFFICIENTS
68 SAVE=0.00
HELP=0.00
K=L+L
DO 73 I=1,NaN
IDD=K+I
J=HE(IDD)
IF(J) 71,70,73
70 SAVE=-TOP(I)
71 IF(M+J+1) 73,73,73
72 HELP=TOP(I)
73 CONTINUE
C
C PREPARE T,TOP,PIV
T(I)=SAVE
IDD=NaN+I
J=NaN+I
DO 74 I=1;IDD,J
TOP(I)=SAVE
DO 75 I=1,M
75 PIV(I)=HELP
C
C COMPUTE COEFFICIENTS OF RESULTING POLYNOMIAL IN PIV(I) UP TO TOP(I)
END AND CALCULATE ERRORS AT GIVEN NODES IN TOP(I) OR TO TOP(N)
DO 76 I=1,NaN
IDD=K+I
J=HE(IDD)
IF(J) 76,79,77
76 J=J
PIV(J)=HELP-TOP(I)
GO TO 79
77 IF(J-N) 78,78,79
78 J=J+NaN
TOP(J)=SAVE+TOP(I)
79 CONTINUE
DO 80 I=L,N
IDD=NaN+I
TOP(I)=TOP(IDD)
81 RETURN
END
DAPM3030
DAPM3040
DAPM3050
DAPM3060
DAPM3070
DAPM3080
DAPM3090
DAPM3100
DAPM3110
DAPM3120
DAPM3130
DAPM3140
DAPM3150
DAPM3160
DAPM3170
DAPM3180
DAPM3190
DAPM3200
DAPM3210
DAPM3220
DAPM3230
DAPM3240
DAPM3250
DAPM3260
DAPM3270
DAPM3280
DAPM3290
DAPM3300
DAPM3310
DAPM3320
DAPM3330
DAPM3340
DAPM3350
DAPM3360
DAPM3370
DAPM3380
DAPM3390
DAPM3400
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DAPM3480
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DAPM3670
DAPM3680
DAPM3690
DAPM3700
DAPM3710
DAPM3720
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DAPM3750
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DAPM3770
DAPM3780
DAPM3790
DAPM3800
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DAPM3860
DAPM3870
DAPM3880
DAPM3890
DAPM3900
DAPM3910
DAPM3920
DAPM3930
DAPM3940
DAPM3950
DAPM3960
DAPM3970
DAPM3980
DAPM3990
DAPM4000
DAPM4010
DAPM4020
DAPM4030
DAPM4040
DAPM4050
DAPM4060
DAPM4070
DAPM4080
DAPM4090
DAPM4100
DAPM4110

```

Numerical Quadrature

Subroutines QTFG and DQTFG

These subroutines perform the integration of a monotonically tabulated function by trapezoidal rule.

To compute the vector of integral values:

$$z_i = z(x_i) = \int_{x_1}^{x_i} y(x) dx \quad (i = 1, 2, \dots, n)$$

for a given table $(x_i, y_i; i = 1, 2, \dots, n)$ of monotonic arguments and their function values, the trapezoidal rule is used. It is assumed that the function to be integrated is continuous and can be differentiated at least twice. Starting with integral value $z_1 = 0$, successive integral values z_i ($i = 2, 3, \dots, n$) are computed, using the trapezoidal rule in the following form:

$$z_i = z_{i-1} + \frac{x_i - x_{i-1}}{2} (y_i + y_{i-1}) \quad (i = 2, 3, \dots, n)$$

Local truncation error at each step is:

$$R_i = -\frac{1}{12}(x_i - x_{i-1})^3 \cdot y''(\xi_i) \quad (\xi_i \in [x_{i-1}, x_i])$$

However, these truncation errors may accumulate.

For reference see F. B. Hildebrand, Introduction to Numerical Analysis, McGraw-Hill, New York/Toronto/London, 1956, pp. 75.

```

C
C
C ..... QTFG 10
C ..... QTFG 20
C SUBROUTINE QTFG ..... QTFG 30
C ..... QTFG 40
C ..... QTFG 50
C PURPOSE ..... QTFG 60
C TO COMPUTE THE VECTOR OF INTEGRAL VALUES FOR A GIVEN
C GENERAL TABLE OF ARGUMENT AND FUNCTION VALUES. ..... QTFG 70
C ..... QTFG 80
C ..... QTFG 90
C USAGE ..... QTFG 100
C CALL QTFG (X,Y,Z,NDIM) ..... QTFG 110
C ..... QTFG 120
C DESCRIPTION OF PARAMETERS ..... QTFG 130
C X - THE INPUT VECTOR OF ARGUMENT VALUES. ..... QTFG 140
C Y - THE INPUT VECTOR OF FUNCTION VALUES. ..... QTFG 150
C Z - THE RESULTING VECTOR OF INTEGRAL VALUES. Z MAY BE
C IDENTICAL WITH X OR Y. ..... QTFG 160
C NDIM - THE DIMENSION OF VECTORS X,Y,Z. ..... QTFG 170
C ..... QTFG 180
C REMARKS ..... QTFG 190
C NO ACTION IN CASE NDIM LESS THAN 1. ..... QTFG 200
C ..... QTFG 210
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED ..... QTFG 220
C NONE ..... QTFG 230
C ..... QTFG 240
C METHOD ..... QTFG 250
C BEGINNING WITH Z(1)=0. EVALUATION OF VECTOR Z IS DONE BY
C MEANS OF TRAPEZOIDAL RULE (SECOND ORDER FORMULA). ..... QTFG 260
C FOR REFERENCE, SEE ..... QTFG 270
C F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS,
C MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.75. ..... QTFG 280
C ..... QTFG 290
C ..... QTFG 300
C ..... QTFG 310
C ..... QTFG 320
C ..... QTFG 330
C ..... QTFG 340
C SUBROUTINE QTFG(X,Y,Z,NDIM) ..... QTFG 350
C ..... QTFG 360
C ..... QTFG 370
C DIMENSION X(1),Y(1),Z(1) ..... QTFG 380
C ..... QTFG 390
C SUM2=0. ..... QTFG 400
C IF(NDIM-1)4,3,1 ..... QTFG 410
C ..... QTFG 420
C INTEGRATION LOOP ..... QTFG 430
C 1 DO 2 I=2,NDIM ..... QTFG 440
C SUM1=SUM2 ..... QTFG 450
C SUM2=SUM2+.5*(X(I)-X(I-1))*(Y(I)+Y(I-1)) ..... QTFG 460
C 2 Z(I-1)=SUM1 ..... QTFG 470
C 3 Z(NDIM)=SUM2 ..... QTFG 480
C 4 RETURN ..... QTFG 490
C END ..... QTFG 500

```

```

C
C ..... DTFG 10
C ..... DTFG 20
C SUBROUTINE DQTFG ..... DTFG 30
C ..... DTFG 40
C ..... DTFG 50
C PURPOSE ..... DTFG 60
C TO COMPUTE THE VECTOR OF INTEGRAL VALUES FOR A GIVEN
C GENERAL TABLE OF ARGUMENT AND FUNCTION VALUES. ..... DTFG 70
C ..... DTFG 80
C ..... DTFG 90
C USAGE ..... DTFG 100
C CALL DQTFG (X,Y,Z,NDIM) ..... DTFG 110
C ..... DTFG 120
C DESCRIPTION OF PARAMETERS ..... DTFG 130
C X - DOUBLE PRECISION INPUT VECTOR OF ARGUMENT VALUES. ..... DTFG 140
C Y - DOUBLE PRECISION INPUT VECTOR OF FUNCTION VALUES. ..... DTFG 150
C Z - RESULTING DOUBLE PRECISION VECTOR OF INTEGRAL
C VALUES. Z MAY BE IDENTICAL WITH X OR Y. ..... DTFG 160
C NDIM - THE DIMENSION OF VECTORS X,Y,Z. ..... DTFG 170
C ..... DTFG 180
C REMARKS ..... DTFG 190
C NO ACTION IN CASE NDIM LESS THAN 1. ..... DTFG 200
C ..... DTFG 210
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED ..... DTFG 220
C NONE ..... DTFG 230
C ..... DTFG 240
C METHOD ..... DTFG 250
C BEGINNING WITH Z(1)=0. EVALUATION OF VECTOR Z IS DONE BY
C MEANS OF TRAPEZOIDAL RULE (SECOND ORDER FORMULA). ..... DTFG 260
C FOR REFERENCE, SEE ..... DTFG 270
C F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS,
C MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.75. ..... DTFG 280
C ..... DTFG 290
C ..... DTFG 300
C ..... DTFG 310
C ..... DTFG 320
C ..... DTFG 330
C ..... DTFG 340
C SUBROUTINE DQTFG(X,Y,Z,NDIM) ..... DTFG 350
C ..... DTFG 360
C ..... DTFG 370
C DIMENSION X(1),Y(1),Z(1) ..... DTFG 380
C DOUBLE PRECISION X,Y,Z,SUM1,SUM2 ..... DTFG 390
C ..... DTFG 400
C SUM2=0.00 ..... DTFG 410
C IF(NDIM-1)4,3,1 ..... DTFG 420
C ..... DTFG 430
C INTEGRATION LOOP ..... DTFG 440
C 1 DO 2 I=2,NDIM ..... DTFG 450
C SUM1=SUM2 ..... DTFG 460
C SUM2=SUM2+.500*(X(I)-X(I-1))*(Y(I)+Y(I-1)) ..... DTFG 470
C 2 Z(I-1)=SUM1 ..... DTFG 480
C 3 Z(NDIM)=SUM2 ..... DTFG 490
C 4 RETURN ..... DTFG 500
C END ..... DTFG 510

```


Subroutines QSF and DQSF

These subroutines perform the integration of an equidistantly tabulated function by Simpson's rule. To compute the vector of integral values:

$$z_i = z(x_i) = \int_a^{x_i} y(x) dx \quad (i=1, 2, \dots, n)$$

with $x_i = a + (i-1)h$

for a table of function values $y_i (i=1, 2, \dots, n)$, given at equidistant points $x_i = a + (i-1)h (i=1, 2, \dots, n)$, Simpson's rule together with Newton's 3/8 rule or a combination of these two rules is used. Local truncation error is of the order h^5 in all cases with more than three points in the given table. Only z_2 has a truncation error of the order h^4 if there are only three points in the given table. No action takes place if the table consists of less than three sample points.

The function to be integrated is assumed to be continuous and differentiable (three or four times, depending on the rule used).

Formulas used in this subroutine (z_j are integral values, y_j function values) are:

$$z_j = z_{j-1} + \frac{h}{3} (1.25 y_{j-1} + 2y_j + 0.25 y_{j+1}) \quad (1)$$

$$z_j = z_{j-2} + \frac{h}{3} (y_{j-2} + 4y_{j-1} + y_j) \quad (\text{Simpson's rule}) \quad (2)$$

$$z_j = z_{j-3} + \frac{3}{8} h (y_{j-3} + 3y_{j-2} + 3y_{j-1} + y_j) \quad (3)$$

(Newton's 3/8 rule)

$$z_j = z_{j-5} + \frac{h}{3} (y_{j-5} + 3.875 y_{j-4} + 2.625 y_{j-3} + 2.625 y_{j-2} + 3.875 y_{j-1} + y_j) \quad (4)$$

[combination of (2) and (3)]

Sometimes formula (2) is used in the following form:

$$z_j = z_{j+2} - \frac{h}{3} (y_j + 4 y_{j+1} + y_{j+2}) \quad (5)$$

Local truncation errors of formulas (1) ... (4) are, respectively:

$$R_1 = \frac{1}{24} h^4 y'''' (\xi_1) \quad (\xi_1 \in [x_{j-1}, x_{j+1}])$$

$$R_2 = -\frac{1}{90} h^5 y'''' (\xi_2) \quad (\xi_2 \in [x_{j-2}, x_j])$$

$$R_3 = -\frac{3}{80} h^5 y'''' (\xi_3) \quad (\xi_3 \in [x_{j-3}, x_j])$$

$$R_4 = -\frac{1}{144} h^5 y'''' (\xi_4) \quad (\xi_4 \in [x_{j-5}, x_j])$$

However, these truncation errors may accumulate.

For reference see:

- (1) F. B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp. 71-76.
- (2) R. Zurmühl, Praktische Mathematik für Ingenieure und Physiker. Springer, Berlin/Göttingen/Heidelberg, 1963, pp. 214-221.

```

C
C
C ..... QSF 10
C ..... QSF 20
C ..... QSF 30
C ..... QSF 40
C ..... QSF 50
C ..... QSF 60
C ..... QSF 70
C ..... QSF 80
C ..... QSF 90
C ..... QSF 100
C ..... QSF 110
C ..... QSF 120
C ..... QSF 130
C ..... QSF 140
C ..... QSF 150
C ..... QSF 160
C ..... QSF 170
C ..... QSF 180
C ..... QSF 190
C ..... QSF 200
C ..... QSF 210
C ..... QSF 220
C ..... QSF 230
C ..... QSF 240
C ..... QSF 250
C ..... QSF 260
C ..... QSF 270
C ..... QSF 280
C ..... QSF 290
C ..... QSF 300
C ..... QSF 310
C ..... QSF 320
C ..... QSF 330
C ..... QSF 340
C ..... QSF 350
C ..... QSF 360
C ..... QSF 370
C ..... QSF 380
C ..... QSF 390
C ..... QSF 400
C ..... QSF 410
C ..... QSF 420
C ..... QSF 430
C ..... QSF 440
C ..... QSF 450
C ..... QSF 460
C ..... QSF 470
C ..... QSF 480
C ..... QSF 490
C ..... QSF 500
C ..... QSF 510
C ..... QSF 520
C ..... QSF 530
C ..... QSF 540
C ..... QSF 550
C ..... QSF 560
C ..... QSF 570
C ..... QSF 580
C ..... QSF 590
C ..... QSF 600
C ..... QSF 610
C ..... QSF 620
C ..... QSF 630
C ..... QSF 640
C ..... QSF 650
C ..... QSF 660
C ..... QSF 670
C ..... QSF 680
C ..... QSF 690
C ..... QSF 700
C ..... QSF 710
C ..... QSF 720
C ..... QSF 730
C ..... QSF 740
C ..... QSF 750
C ..... QSF 760
C ..... QSF 770
C ..... QSF 780
C ..... QSF 790
C ..... QSF 800
C ..... QSF 810
C ..... QSF 820
C ..... QSF 830
C ..... QSF 840
C ..... QSF 850
C ..... QSF 860
C ..... QSF 870

```

```
C 7 IF(NCIP-3)I2,I1,E
C      NCIP IS EQUAL TO A C F 5
C      SLP1=1.125+(Y(1)+Y(2)+Y(2)+Y(2)+Y(3)+Y(3)+Y(4))
C      SLP1=Y(2)+Y(2)
C      SLP1=SLP1+SLP1
C      SLP1=Y(1)+Y(1)+SLP1+Y(2)
C      Z(1)=C.
C      ALX1=Y(2)+Y(2)
C      ALX1=ALX1+ALX1
C      Z(2)=SLP2+10*(Y(2)+ALX1+Y(4))
C      IF(NCIP-5)IC,S,S
C      S      ALX1=Y(4)+Y(4)
C      ALX1=ALX1+ALX1
C      Z(5)=SLP1+10*(Y(2)+ALX1+Y(5))
C      Z(3)=SLP1
C      Z(4)=SUM2
C      RETURN
C
C      NDIM IS EQUAL TO 3
C      SUM1=HT*(1.25*(Y(1)+Y(2)+Y(2)--.25*(Y(3))
C      SUM2=Y(2)+Y(2)
C      SLP2=SLP2+SLP2
C      Z(3)=HT*(Y(1)+SLP2+Y(3))
C      Z(1)=0.
C      Z(2)=SLP1
C      12 RETURN
C      END
```

```
6 Z(NDIM-1)=SUM2
Z(NDIM)=AUX1
RETURN
END OF INTEGRATION LOOP
C
C 7 IF(NDIM-3)I2,I1,8
C      NDIM IS EQUAL TO 4 OR 5
C      8 SUM2=1.12500*HT*(Y(1)+Y(2)+Y(2)+Y(2)+Y(3)+Y(3)+Y(4))
C      SUM1=Y(2)+Y(2)
C      SUM1=SUM1+SUM1
C      SUM1=HT*(Y(1)+SUM1+Y(3))
C      Z(1)=0.00
C      AUX1=Y(3)+Y(3)
C      AUX1=AUX1+AUX1
C      Z(2)=SUM2-HT*(Y(2)+AUX1+Y(4))
C      IF(NDIM-5)I0,9,9
C      9 AUX1=Y(4)+Y(4)
C      AUX1=AUX1+AUX1
C      Z(5)=SUM1+HT*(Y(3)+AUX1+Y(5))
C      Z(3)=SUM1
C      Z(4)=SUM2
C      RETURN
C
C      NDIM IS EQUAL TO 3
C      11 SUM1=HT*(1.2500*(Y(1)+Y(2)+Y(2)--.2500*(Y(3))
C      SUM2=Y(2)+Y(2)
C      SUM2=SUM2+SUM2
C      Z(3)=HT*(Y(1)+SUM2+Y(3))
C      Z(1)=0.00
C      Z(2)=SUM1
C      12 RETURN
C      END
```

DQSF 850
DQSF 860
DQSF 870
DQSF 880
DQSF 890
DQSF 900
DQSF 910
DQSF 920
DQSF 930
DQSF 940
DQSF 950
DQSF 960
DQSF 970
DQSF 980
DQSF 990
DQSF1000
DQSF1010
DQSF1020
DQSF1030
DQSF1040
DQSF1050
DQSF1060
DQSF1070
DQSF1080
DQSF1090
DQSF1100
DQSF1110
DQSF1120
DQSF1130
DQSF1140
DQSF1150
DQSF1160
DQSF1170

```
..... DQSF 10
DQSF 20
DQSF 30
SUBROUTINE DQSF DQSF 40
DQSF 50
PURPOSE DQSF 60
TO COMPUTE THE VECTOR OF INTEGRAL VALUES FOR A GIVEN
EQUIDISTANT TABLE OF FUNCTION VALUES. DQSF 70
DQSF 80
DQSF 90
DQSF 100
DQSF 110
DQSF 120
DQSF 130
DESCRIPTION OF PARAMETERS DQSF 140
H - DOUBLE PRECISION INCREMENT OF ARGUMENT VALUES. DQSF 150
Y - DOUBLE PRECISION INPUT VECTOR OF FUNCTION VALUES. DQSF 160
Z - RESULTING DOUBLE PRECISION VECTOR OF INTEGRAL DQSF 170
VALUES. Z MAY BE IDENTICAL WITH Y.
NDIM - THE DIMENSION OF VECTORS Y AND Z. DQSF 180
REMARKS DQSF 190
NO ACTION IN CASE NDIM LESS THAN 3. DQSF 200
DQSF 210
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DQSF 220
NONE DQSF 230
DQSF 240
METHOD DQSF 250
BEGINNING WITH Z(1)=0, EVALUATION OF VECTOR Z IS DONE BY DQSF 260
MEANS OF SIMPSONS RULE TOGETHER WITH NEWTONS 3/8 RULE OR A DQSF 270
COMBINATION OF THESE TWO RULES. TRUNCATION ERROR IS OF DQSF 280
ORDER *H*5 I.E. FOURTH ORDER METHOD01. ONLY IN CASE NDIM=3 DQSF 290
TRUNCATION ERROR OF Z(2) IS OF ORDER *H*4. DQSF 300
FOR REFERENCE, SEE DQSF 310
(1) F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS, DQSF 320
MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.71-76. DQSF 330
(2) R.ZURMUHLE, PRAKTISCHE MATHEMATIK FUER INGENIEURE UND DQSF 340
PHYSIKER, SPRINGER, BERLIN/GOETTINGEN/HEIDELBERG, 1963, DQSF 350
PP.214-221. DQSF 360
DQSF 370
..... DQSF 380
SUBROUTINE DQSF(H,Y,Z,NDIM) DQSF 390
DQSF 400
DQSF 410
DQSF 420
DQSF 430
DQSF 440
DIMENSION Y(1),Z(1) DQSF 450
DOUBLE PRECISION Y,Z,H,HT,SUM1,SUM2,AUX,AUX1,AUX2 DQSF 460
HT=.333333333333333333333333D0*H DQSF 470
IF(NDIM-5)7,8,1 DQSF 480
DQSF 490
DQSF 500
NDIM IS GREATER THAN 5. PREPARATIONS OF INTEGRATION LOOP DQSF 510
1 SUM1=Y(2)+Y(2) DQSF 520
SUM1=SUM1+SUM1 DQSF 530
SUM1=HT*(Y(1)+SUM1+Y(3)) DQSF 540
AUX1=Y(4)+Y(4) DQSF 550
AUX1=AUX1+AUX1 DQSF 560
AUX1=SUM1+HT*(Y(3)+AUX1+Y(5)) DQSF 570
AUX2=HT*(Y(1)+3.*87500*(Y(2)+Y(5))+2.62500*(Y(3)+Y(4))+Y(6)) DQSF 580
SUM2=Y(5)+Y(5) DQSF 590
SUM2=SUM2+SUM2 DQSF 600
SUM2=AUX2-HT*(Y(4)+SUM2+Y(6)) DQSF 610
Z(1)=0.00 DQSF 620
AUX=Y(3)+Y(3) DQSF 630
AUX=AUX+AUX DQSF 640
Z(2)=SUM2-HT*(Y(2)+AUX+Y(4)) DQSF 650
Z(3)=SUM1 DQSF 660
Z(4)=SUM2 DQSF 670
IF(NDIM-6)5,5,2 DQSF 680
DQSF 690
INTEGRATION LOOP DQSF 700
2 DO 4 I=7,NDIM,2 DQSF 710
SUM1=AUX1 DQSF 720
SUM2=AUX2 DQSF 730
AUX1=Y(I-1)+Y(I-1) DQSF 740
AUX1=AUX1+AUX1 DQSF 750
AUX1=SUM1+HT*(Y(I-2)+AUX1+Y(I)) DQSF 760
Z(I-2)=SUM1 DQSF 770
IF(I-NDIM)3,6,6 DQSF 780
3 AUX2=Y(I)+Y(I) DQSF 790
AUX2=AUX2+AUX2 DQSF 800
AUX2=SUM2+HT*(Y(I-1)+AUX2+Y(I+1)) DQSF 810
4 Z(I-1)=SUM2 DQSF 820
5 Z(NDIM-1)=AUX1 DQSF 830
Z(NDIM)=AUX2 DQSF 840
RETURN
```


Subroutines QHFG and DQHFG

These subroutines perform the integration of a monotonically tabulated function with first derivative by a Hermitian formula of first order. To compute the vector of integral values:

$$z_i = z(x_i) = \int_{x_1}^{x_i} y(x) dx \quad (i = 1, 2, \dots, n)$$

for a given table x_i, y_i, y_i' ($i = 1, 2, \dots, n$) of monotonic arguments and their function and derivative values, a first-order Hermitian formula is used. It is assumed that the function to be integrated is continuous and can be differentiated at least four times. Starting with the integral value $z_1 = 0$, successive integral values z_i ($i = 2, 3, \dots, n$) are computed by means of the following formula:

$$z_i = z_{i-1} + \frac{x_i - x_{i-1}}{2} \left[y_{i-1} + y_i + \frac{x_i - x_{i-1}}{6} (y_{i-1}' - y_i') \right]$$

($i = 2, 3, \dots, n$)

Local truncation error at each step is:

$$R_i = \frac{(x_i - x_{i-1})^5}{720} \cdot y^{(4)}(\xi_i) \quad (\xi_i \in [x_{i-1}, x_i])$$

However, these truncation errors may accumulate.

For reference see:

- (1) F. B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp. 314-319.
- (2) R. Zurmühl, Praktische Mathematik für Ingenieure und Physiker. Springer, Berlin/Göttingen/Heidelberg, 1963, pp. 227-230.

```

C ..... QHFG 10
C ..... QHFG 20
C ..... QHFG 30
C ..... QHFG 40
C ..... QHFG 50
C ..... QHFG 60
C ..... QHFG 70
C ..... QHFG 80
C ..... QHFG 90
C ..... QHFG 100
C ..... QHFG 110
C ..... QHFG 120
C ..... QHFG 130
C ..... QHFG 140
C ..... QHFG 150
C ..... QHFG 160
C ..... QHFG 170
C ..... QHFG 180
C ..... QHFG 190
C ..... QHFG 200
C ..... QHFG 210
C ..... QHFG 220
C ..... QHFG 230
C ..... QHFG 240
C ..... QHFG 250
C ..... QHFG 260
C ..... QHFG 270
C ..... QHFG 280
C ..... QHFG 290
C ..... QHFG 300
C ..... QHFG 310
C ..... QHFG 320
C ..... QHFG 330
C ..... QHFG 340
C ..... QHFG 350
C ..... QHFG 360
C ..... QHFG 370

```

```

C ..... QHFG 380
C ..... QHFG 390
C ..... QHFG 400
C ..... QHFG 410
C ..... QHFG 420
C ..... QHFG 430
C ..... QHFG 440
C ..... QHFG 450
C ..... QHFG 460
C ..... QHFG 470
C ..... QHFG 480
C ..... QHFG 490
C ..... QHFG 500
C ..... QHFG 510
C ..... QHFG 520
C ..... QHFG 530
C ..... QHFG 540
C ..... QHFG 550

```

```

C ..... DQHG 10
C ..... DQHG 20
C ..... DQHG 30
C ..... DQHG 40
C ..... DQHG 50
C ..... DQHG 60
C ..... DQHG 70
C ..... DQHG 80
C ..... DQHG 90
C ..... DQHG 100
C ..... DQHG 110
C ..... DQHG 120
C ..... DQHG 130
C ..... DQHG 140
C ..... DQHG 150
C ..... DQHG 160
C ..... DQHG 170
C ..... DQHG 180
C ..... DQHG 190
C ..... DQHG 200
C ..... DQHG 210
C ..... DQHG 220
C ..... DQHG 230
C ..... DQHG 240
C ..... DQHG 250
C ..... DQHG 260
C ..... DQHG 270
C ..... DQHG 280
C ..... DQHG 290
C ..... DQHG 300
C ..... DQHG 310
C ..... DQHG 320
C ..... DQHG 330
C ..... DQHG 340
C ..... DQHG 350
C ..... DQHG 360
C ..... DQHG 370
C ..... DQHG 380
C ..... DQHG 390
C ..... DQHG 400
C ..... DQHG 410
C ..... DQHG 420
C ..... DQHG 430
C ..... DQHG 440
C ..... DQHG 450
C ..... DQHG 460
C ..... DQHG 470
C ..... DQHG 480
C ..... DQHG 490
C ..... DQHG 500
C ..... DQHG 510
C ..... DQHG 520
C ..... DQHG 530
C ..... DQHG 540
C ..... DQHG 550
C ..... DQHG 560
C ..... DQHG 570

```

Subroutines QHFE and DQHFE

These subroutines perform the integration of an equidistantly tabulated function with first derivative by a Hermitian formula of first order. To compute the vector of integral values:

z_i = z(x_i) = integral from a to x_i of y(x) dx (i = 1, 2, ..., n)

with x_i = a + (i-1)h

for a table of function and first derivative values y_i, y_i'(i = 1, 2, ..., n), given at equidistant points x_i = a + (i - 1) h, a first-order Hermitian formula is used. It is assumed that the function to be integrated is continuous and can be differentiated at least four times. Starting with the integral value z_1 = 0, successive integral values z_i (i = 2, 3, ..., n) are computed by means of the following formula:

z_i = z_{i-1} + h/2 * [y_{i-1} + y_i + h/6 * (y'_{i-1} - y'_i)] (i = 1, 2, ..., n)

with a given increment h of argument values. As the local truncation error at each step is:

R_i = h^5/720 * y^{(4)}(xi) (xi in [x_{i-1}, x_i])

the global truncation error R in z_n appears as follows:

R = 1/720 * (n-1) h^5 y^{(4)}(xi) (xi in [x_1, x_n])

or

R = l/720 h^4 y^{(4)}(xi)

where l is the length of the whole integration interval.

For reference see:

- (1) F.B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp. 314-319.
(2) R. Zurmühl, Praktische Mathematik für Ingenieure und Physiker. Springer, Berlin/Göttingen/Heidelberg, 1963, pp. 227-230.

QHFE 10
QHFE 20
SUBROUTINE QHFE
PURPOSE
TO COMPUTE THE VECTOR OF INTEGRAL VALUES FOR A GIVEN
EQUIDISTANT TABLE OF FUNCTION AND DERIVATIVE VALUES.
USAGE
CALL QHFE (H,Y,DERY,Z,NDIM)
DESCRIPTION OF PARAMETERS
H - THE INCREMENT OF ARGUMENT VALUES.
Y - THE INPUT VECTOR OF FUNCTION VALUES.
DERY - THE INPUT VECTOR OF DERIVATIVE VALUES.
Z - THE RESULTING VECTOR OF INTEGRAL VALUES. Z MAY BE
IDENTICAL WITH Y OR DERY.
NDIM - THE DIMENSION OF VECTORS Y,DERY,Z.
REMARKS
NO ACTION IN CASE NDIM LESS THAN 1.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
BEGINNING WITH Z(1)=0, EVALUATION OF VECTOR Z IS DONE BY
MEANS OF HERMITEAN FOURTH ORDER INTEGRATION FORMULA.
FOR REFERENCE, SEE
(1) F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS,
MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.314-319.
(2) R.ZURMUEHL, PRAKTISCHE MATHEMATIK FUER INGENIEURE UND
PHYSIKER, SPRINGER, BERLIN/GOETTINGEN/HEIDELBERG, 1963,
PP.227-230.

DQHE 10
DQHE 20
SUBROUTINE DQHE
PURPOSE
TO COMPUTE THE VECTOR OF INTEGRAL VALUES FOR A GIVEN
EQUIDISTANT TABLE OF FUNCTION AND DERIVATIVE VALUES.
USAGE
CALL DQHE (H,Y,DERY,Z,NDIM)
DESCRIPTION OF PARAMETERS
H - DOUBLE PRECISION INCREMENT OF ARGUMENT VALUES.
Y - DOUBLE PRECISION INPUT VECTOR OF FUNCTION VALUES.
DERY - DOUBLE PRECISION INPUT VECTOR OF DERIVATIVE VALUES.
Z - RESULTING DOUBLE PRECISION VECTOR OF INTEGRAL
VALUES. Z MAY BE IDENTICAL WITH Y OR DERY.
NDIM - THE DIMENSION OF VECTORS Y,DERY,Z.
REMARKS
NO ACTION IN CASE NDIM LESS THAN 1.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE
METHOD
BEGINNING WITH Z(1)=0, EVALUATION OF VECTOR Z IS DONE BY
MEANS OF HERMITEAN FOURTH ORDER INTEGRATION FORMULA.
FOR REFERENCE, SEE
(1) F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS,
MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.314-319.
(2) R.ZURMUEHL, PRAKTISCHE MATHEMATIK FUER INGENIEURE UND
PHYSIKER, SPRINGER, BERLIN/GOETTINGEN/HEIDELBERG, 1963,
PP.227-230.

Subroutines QHSG and DQHSG

These subroutines perform the integration of a monotonically tabulated function with first and second derivatives by a Hermitian formula of second order. To compute the vector of integral values:

$$z_i = z(x_i) = \int_{x_1}^{x_i} y(x) dx \quad (i = 1, 2, \dots, n)$$

for a given table x_i, y_i, y_i', y_i'' ($i=1, 2, \dots, n$) of monotonic arguments and their function and first and second derivative values, a second-order Hermitian formula is used. It is assumed that the function to be integrated is continuous and can be differentiated at least six times. Starting with the integral value $z_1 = 0$, successive integral values z_i ($i = 2, 3, \dots, n$) are computed by means of the following formula:

$$z_i = z_{i-1} + \frac{x_i - x_{i-1}}{2} \left\{ y_{i-1}' + y_i' + \frac{x_i - x_{i-1}}{5} [y_{i-1}'' - y_i''] \right. \\ \left. + \frac{x_i - x_{i-1}}{12} (y_{i-1}'' + y_i'') \right\} \quad (i=2, 3, \dots, n)$$

Local truncation error at each step is:

$$R_i = - \frac{(x_i - x_{i-1})^7}{100800} y^{(6)}(\xi_i) \quad (\xi_i \in [x_{i-1}, x_i])$$

However, these truncation errors may accumulate.

For reference see R. Zurmühl, Praktische Mathematik für Ingenieure und Physiker. Springer, Berlin/Göttingen/Heidelberg, 1963, pp. 227-230.

```

C
C
C ..... QHSG 10
C           QHSG 20
C           QHSG 30
C           QHSG 40
C           QHSG 50
C           QHSG 60
C           QHSG 70
C           QHSG 80
C           QHSG 90
C           QHSG 100
C           QHSG 110
C           QHSG 120
C           QHSG 130
C           QHSG 140
C           QHSG 150
C           QHSG 160
C           QHSG 170
C           QHSG 180
C           QHSG 190
C           QHSG 200
C           QHSG 210
C           QHSG 220
C           QHSG 230
C           QHSG 240
C           QHSG 250
C           QHSG 260
C           QHSG 270
C           QHSG 280
C           QHSG 290
C           QHSG 300
C           QHSG 310
C           QHSG 320
C           QHSG 330
C           QHSG 340
C           QHSG 350
C           QHSG 360
C ..... QHSG 370
C           QHSG 380
C           QHSG 390
C           QHSG 400
C           QHSG 410
C           QHSG 420
C           QHSG 430
C           QHSG 440
C           QHSG 450
C           QHSG 460
C           QHSG 470
C           QHSG 480
C           QHSG 490
C           QHSG 500
C           QHSG 510
C           QHSG 520
C           QHSG 530
C           QHSG 540
C           QHSG 550
C           QHSG 560
C           QHSG 570
C
C
C ..... QHSG 10
C           QHSG 20
C           QHSG 30
C           QHSG 40
C           QHSG 50
C           QHSG 60
C           QHSG 70
C           QHSG 80
C           QHSG 90
C           QHSG 100
C           QHSG 110
C           QHSG 120
C           QHSG 130
C           QHSG 140
C           QHSG 150
C           QHSG 160
C           QHSG 170
C           QHSG 180
C           QHSG 190
C           QHSG 200
C           QHSG 210
C           QHSG 220
C           QHSG 230
C           QHSG 240
C           QHSG 250
C           QHSG 260
C           QHSG 270
C           QHSG 280
C           QHSG 290
C           QHSG 300
C           QHSG 310
C           QHSG 320
C           QHSG 330
C           QHSG 340
C           QHSG 350
C           QHSG 360
C ..... QHSG 370
C           QHSG 380
C           QHSG 390
C           QHSG 400
C           QHSG 410
C           QHSG 420
C           QHSG 430
C           QHSG 440
C           QHSG 450
C           QHSG 460
C           QHSG 470
C           QHSG 480
C           QHSG 490
C           QHSG 500
C           QHSG 510
C           QHSG 520
C           QHSG 530
C           QHSG 540
C           QHSG 550
C           QHSG 560
C           QHSG 570

```

```

C
C
C ..... DQHS 10
C           DQHS 20
C           DQHS 30
C           DQHS 40
C           DQHS 50
C           DQHS 60
C           DQHS 70
C           DQHS 80
C           DQHS 90
C           DQHS 100
C           DQHS 110
C           DQHS 120
C           DQHS 130
C           DQHS 140
C           DQHS 150
C           DQHS 160
C           DQHS 170
C           DQHS 180
C           DQHS 190
C           DQHS 200
C           DQHS 210
C           DQHS 220
C           DQHS 230
C           DQHS 240
C           DQHS 250
C           DQHS 260
C           DQHS 270
C           DQHS 280
C           DQHS 290
C           DQHS 300
C           DQHS 310
C           DQHS 320
C           DQHS 330
C           DQHS 340
C           DQHS 350
C           DQHS 360
C ..... DQHS 370
C           DQHS 380
C           DQHS 390
C           DQHS 400
C           DQHS 410
C           DQHS 420
C           DQHS 430
C           DQHS 440
C           DQHS 450
C           DQHS 460
C           DQHS 470
C           DQHS 480
C           DQHS 490
C           DQHS 500
C           DQHS 510
C           DQHS 520
C           DQHS 530
C           DQHS 540
C           DQHS 550
C           DQHS 560
C           DQHS 570

```

Subroutines QHSE and DQHSE

These subroutines perform the integration of an equidistantly tabulated function with first and second derivatives by a Hermitian formula of second order.

To compute the vector of integral values:

$$z_i = z(x_i) = \int_a^{x_i} y(x) dx \quad \left. \vphantom{\int_a^{x_i} y(x) dx} \right\} (i=1, 2, \dots, n)$$

with $x_i = a + (i-1)h$

for a table of function and first and second derivative values y_i, y'_i, y''_i ($i=1, 2, \dots, n$), given at equidistant points $x_i = a + (i-1)h$, a second-order Hermitian formula is used. It is assumed that the function to be integrated is continuous and can be differentiated at least six times. Starting with the integral value $z_1 = 0$, successive integral values z_i ($i=2, 3, \dots, n$) are computed by means of the following formula:

$$z_i = z_{i-1} + \frac{h}{2} \left\{ y_{i-1} + y_i + \frac{h}{5} \left[y'_{i-1} - y'_i + \frac{h}{12} (y''_{i-1} + y''_i) \right] \right\} \quad (i=2, 3, \dots, n)$$

with a given increment h of argument values.

As the local truncation error at each step is:

$$R_i = -\frac{h^7}{100800} y^{(6)}(\xi_i) \quad (\xi_i \in [x_{i-1}, x_i]),$$

the global truncation error R in z_n appears as follows:

$$R = -\frac{1}{100800} (n-1) h^7 y^{(6)}(\xi) \quad (\xi \in [x_1, x_n])$$

or

$$R = -\frac{\ell}{100800} h^6 y^{(6)}(\xi)$$

where ℓ is the length of the whole integration interval.

For reference see R. Zurmühl, Praktische Mathematik für Ingenieure und Physiker. Springer, Berlin/Göttingen/Heidelberg, 1963, pp. 227-230.

```

C
C ..... QHSE 10
C ..... QHSE 20
C ..... QHSE 30
C ..... QHSE 40
C ..... QHSE 50
C ..... QHSE 60
C ..... QHSE 70
C ..... QHSE 80
C ..... QHSE 90
C ..... QHSE 100
C ..... QHSE 110
C ..... QHSE 120
C ..... QHSE 130
C ..... QHSE 140
C ..... QHSE 150
C ..... QHSE 160
C ..... QHSE 170
C ..... QHSE 180
C ..... QHSE 190
C ..... QHSE 200
C ..... QHSE 210
C ..... QHSE 220
C ..... QHSE 230
C ..... QHSE 240
C ..... QHSE 250
C ..... QHSE 260
C ..... QHSE 270
C ..... QHSE 280
C ..... QHSE 290
C ..... QHSE 300
C ..... QHSE 310
C ..... QHSE 320
C ..... QHSE 330
C ..... QHSE 340
C ..... QHSE 350
C ..... QHSE 360
C ..... QHSE 370
C ..... QHSE 380
C ..... QHSE 390
C ..... QHSE 400
C ..... QHSE 410
C ..... QHSE 420
C ..... QHSE 430
C ..... QHSE 440
C ..... QHSE 450
C ..... QHSE 460
C ..... QHSE 470
C ..... QHSE 480
C ..... QHSE 490
C ..... QHSE 500
C ..... QHSE 510
C ..... QHSE 520
C ..... QHSE 530
C ..... QHSE 540
C ..... QHSE 550
C ..... QHSE 560
C ..... QHSE 570
C ..... QHSE 580
C ..... QHSE 590
C ..... QHSE 600
C ..... QHSE 610
C ..... QHSE 620
C ..... QHSE 630
C ..... QHSE 640
C ..... QHSE 650
C ..... QHSE 660
C ..... QHSE 670
C ..... QHSE 680
C ..... QHSE 690
C ..... QHSE 700
C ..... QHSE 710
C ..... QHSE 720
C ..... QHSE 730
C ..... QHSE 740
C ..... QHSE 750
C ..... QHSE 760
C ..... QHSE 770
C ..... QHSE 780
C ..... QHSE 790
C ..... QHSE 800
C ..... QHSE 810
C ..... QHSE 820
C ..... QHSE 830
C ..... QHSE 840
C ..... QHSE 850
C ..... QHSE 860
C ..... QHSE 870
C ..... QHSE 880
C ..... QHSE 890
C ..... QHSE 900
C ..... QHSE 910
C ..... QHSE 920
C ..... QHSE 930
C ..... QHSE 940
C ..... QHSE 950
C ..... QHSE 960
C ..... QHSE 970
C ..... QHSE 980
C ..... QHSE 990
C ..... QHSE 1000

```

```

C
C ..... DQHS 10
C ..... DQHS 20
C ..... DQHS 30
C ..... DQHS 40
C ..... DQHS 50
C ..... DQHS 60
C ..... DQHS 70
C ..... DQHS 80
C ..... DQHS 90
C ..... DQHS 100
C ..... DQHS 110
C ..... DQHS 120
C ..... DQHS 130
C ..... DQHS 140
C ..... DQHS 150
C ..... DQHS 160
C ..... DQHS 170
C ..... DQHS 180
C ..... DQHS 190
C ..... DQHS 200
C ..... DQHS 210
C ..... DQHS 220
C ..... DQHS 230
C ..... DQHS 240
C ..... DQHS 250
C ..... DQHS 260
C ..... DQHS 270
C ..... DQHS 280
C ..... DQHS 290
C ..... DQHS 300
C ..... DQHS 310
C ..... DQHS 320
C ..... DQHS 330
C ..... DQHS 340
C ..... DQHS 350
C ..... DQHS 360
C ..... DQHS 370
C ..... DQHS 380
C ..... DQHS 390
C ..... DQHS 400
C ..... DQHS 410
C ..... DQHS 420
C ..... DQHS 430
C ..... DQHS 440
C ..... DQHS 450
C ..... DQHS 460
C ..... DQHS 470
C ..... DQHS 480
C ..... DQHS 490
C ..... DQHS 500
C ..... DQHS 510
C ..... DQHS 520
C ..... DQHS 530
C ..... DQHS 540
C ..... DQHS 550
C ..... DQHS 560
C ..... DQHS 570
C ..... DQHS 580
C ..... DQHS 590
C ..... DQHS 600
C ..... DQHS 610
C ..... DQHS 620
C ..... DQHS 630
C ..... DQHS 640
C ..... DQHS 650
C ..... DQHS 660
C ..... DQHS 670
C ..... DQHS 680
C ..... DQHS 690
C ..... DQHS 700
C ..... DQHS 710
C ..... DQHS 720
C ..... DQHS 730
C ..... DQHS 740
C ..... DQHS 750
C ..... DQHS 760
C ..... DQHS 770
C ..... DQHS 780
C ..... DQHS 790
C ..... DQHS 800
C ..... DQHS 810
C ..... DQHS 820
C ..... DQHS 830
C ..... DQHS 840
C ..... DQHS 850
C ..... DQHS 860
C ..... DQHS 870
C ..... DQHS 880
C ..... DQHS 890
C ..... DQHS 900
C ..... DQHS 910
C ..... DQHS 920
C ..... DQHS 930
C ..... DQHS 940
C ..... DQHS 950
C ..... DQHS 960
C ..... DQHS 970
C ..... DQHS 980
C ..... DQHS 990
C ..... DQHS 1000

```

Subroutines QATR and DQATR

These subroutines perform the integration of a given function by the trapezoidal rule together with Romberg's extrapolation method in order to compute an approximation for:

$$y = \int_a^b f(x) dx \tag{1}$$

Successively dividing the interval [a, b] into 2^i equidistant subintervals ($i = 0, 1, 2, \dots$) and using the following notations:

$$h_i = \frac{b-a}{2^i}; x_{i,k} = a + k \cdot h_i; f_{i,k} = f(x_{i,k})$$

($k=0, 1, 2, \dots, 2^i$)

the trapezoidal rule gives approximations $T_{0,i}$ to the integral value y:

$$T_{0,i} = h_i \left\{ \sum_{k=0}^{2^i} f_{i,k} - \frac{1}{2} (f(a) + f(b)) \right\} \tag{2}$$

Then the following can be written:

$$T_{0,i} = y + \sum_{r=1}^{\infty} C_{0,2r} \cdot h_i^{2r}$$

with unknown coefficients $C_{0,2r}$ which do not depend on i . Thus there is a truncation error of the order h_i^2 .

Knowing two successive approximations, $T_{0,i}$ and $T_{0,i+1}$, an extrapolated value can be generated:

$$T_{1,i} = T_{0,i+1} + \frac{T_{0,i+1} - T_{0,i}}{2^2 - 1} \tag{3}$$

This is a better approximation to y because:

$$T_{1,i} = y + \frac{1}{2^2 - 1} \sum_{r=2}^{\infty} C_{0,2r} (2^{2r} h_{i+1}^{2r} - h_i^{2r})$$

Noting that $2^{2r} h_{i+1}^{2r} - h_i^{2r} = 0$ and setting:

$$C_{1,2r} = \frac{1}{2^{2r} - 2^{2r-2}} (2^{2r} - 2^{2r-2}) \cdot C_{0,2r}$$

$T_{1,i}$ becomes:

$$T_{1,i} = y + \sum_{r=2}^{\infty} C_{1,2r} h_{i+1}^{2r}$$

This gives a truncation error of the order h_{i+1}^4 .

Knowing $T_{0,i+2}$ also, $T_{1,i+1}$ can be generated (formula 3), and:

$$T_{2,i} = T_{1,i+1} + \frac{T_{1,i+1} - T_{1,i}}{2^4 - 1} \tag{4}$$

Thus:

$$T_{2,i} = y + \sum_{r=3}^{\infty} C_{2,2r} \cdot h_{i+2}^{2r}$$

$$\text{with } C_{2,2r} = \frac{1}{2^4 - 1} (2^4 - 2^{2r}) C_{1,2r}$$

with a truncation error of the order h_{i+2}^6 . Observe that the order of truncation error increases by 2 at each new extrapolation step.

The subroutine uses the scheme shown in Figure 25 for computation of T-values and generates the upward diagonal in the one-dimensional storage array AUX, using the general formula:

$$T_{k,j} = T_{k-1,j+1} + \frac{T_{k-1,j+1} - T_{k-1,j}}{2^{2k-1}} \quad (k+j=i, j = i-1, i-2, \dots, 2, 1, 0) \tag{5}$$

and storing:

- $T_{0,i}$ into AUX (i+1)
- $T_{1,i-1}, \dots$ into AUX (i)
- $T_{k,0}$ into AUX (1)

Truncation error		$O(h_i^2)$	$O(h_i^4)$	$O(h_i^6)$	$O(h_i^8) \dots$
step length	j	0	1	2	3 ...
h_i	i				
$b-a$	0	$T_{0,0}$	$T_{1,0}$	$T_{2,0}$	$T_{3,0} \dots$
$\frac{b-a}{2}$	1	$T_{0,1}$	$T_{1,1}$	$T_{2,1}$	\vdots
$\frac{b-a}{4}$	2	$T_{0,2}$	$T_{1,2}$	\vdots	
$\frac{b-a}{8}$	3	$T_{0,3}$	\vdots		
\vdots	\vdots	\vdots			

Figure 25. Computation of T-values (QATR)

The procedure stops if the difference between two successive values of AUX (1) is less than a given tolerance, or if the values of AUX (1) start oscillating, thus showing the influence of rounding errors.

For reference see S. Filippi, "Das Verfahren von Romberg-Stiefel-Bauer als Spezialfall des allgemeinen Prinzips von Richardson", Mathematik-Technik-Wirtschaft, vol. 11, iss. 2 (1964), pp. 49 - 54.

```

C ..... QATR 10
C ..... QATR 20
C ..... QATR 30
C ..... QATR 40
C ..... QATR 50
C ..... QATR 60
C ..... QATR 70
C ..... QATR 80
C ..... QATR 90
C ..... QATR 100
C ..... QATR 110
C ..... QATR 120
C ..... QATR 130
C ..... QATR 140
C ..... QATR 150
C ..... QATR 160
C ..... QATR 170
C ..... QATR 180
C ..... QATR 190
C ..... QATR 200
C ..... QATR 210
C ..... QATR 220
C ..... QATR 230
C ..... QATR 240
C ..... QATR 250
C ..... QATR 260
C ..... QATR 270
C ..... QATR 280
C ..... QATR 290
C ..... QATR 300
C ..... QATR 310
C ..... QATR 320
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C ..... QATR 370
C ..... QATR 380
C ..... QATR 390
C ..... QATR 400
C ..... QATR 410
C ..... QATR 420
C ..... QATR 430
C ..... QATR 440
C ..... QATR 450
C ..... QATR 460
C ..... QATR 470
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C ..... QATR 490
C ..... QATR 500
C ..... QATR 510
C ..... QATR 520
C ..... QATR 530
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C ..... QATR 690
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C ..... QATR 710
C ..... QATR 720
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C ..... QATR 760
C ..... QATR 770
C ..... QATR 780
C ..... QATR 790
C ..... QATR 800
C ..... QATR 810
C ..... QATR 820
C ..... QATR 830
C ..... QATR 840
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C ..... QATR 970
C ..... QATR 980
C ..... QATR 990
C ..... QATR1000
C ..... QATR1010
C ..... QATR1020
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C ..... QATR1060
C ..... QATR1070
C ..... QATR1080
C ..... QATR1090
C ..... QATR1100
C ..... QATR1110
C ..... QATR1120
C ..... QATR1130
C ..... QATR1140
C ..... QATR1150
C ..... QATR1160
C ..... QATR1170
C ..... QATR1180
C ..... QATR1190

```

```

11 IER=1
Y=H*Y
RETURN
END
QATR1100
QATR1110
QATR1120
QATR1130

C ..... QDQAT 10
C ..... QDQAT 20
C ..... QDQAT 30
C ..... QDQAT 40
C ..... QDQAT 50
C ..... QDQAT 60
C ..... QDQAT 70
C ..... QDQAT 80
C ..... QDQAT 90
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C ..... QDQAT1000
C ..... QDQAT1010
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C ..... QDQAT1060
C ..... QDQAT1070
C ..... QDQAT1080
C ..... QDQAT1090
C ..... QDQAT1100
C ..... QDQAT1110
C ..... QDQAT1120
C ..... QDQAT1130
C ..... QDQAT1140
C ..... QDQAT1150
C ..... QDQAT1160
C ..... QDQAT1170
C ..... QDQAT1180
C ..... QDQAT1190

SUBROUTINE DQATR
PURPOSE
TO COMPUTE AN APPROXIMATION FOR INTEGRAL(FCT(X), SUMMED
OVER X FROM XL TO XU).
USAGE
CALL DQATR (XL,XU,EPS,NDIM,FCT,Y,IER,AUX)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT.
DESCRIPTION OF PARAMETERS
XL - DOUBLE PRECISION LOWER BOUND OF THE INTERVAL.
XU - DOUBLE PRECISION UPPER BOUND OF THE INTERVAL.
EPS - SINGLE PRECISION UPPER BOUND OF THE ABSOLUTE ERROR.
NDIM - THE DIMENSION OF THE AUXILIARY STORAGE ARRAY AUX.
NDIM-1 IS THE MAXIMAL NUMBER OF BISECTIONS OF
THE INTERVAL (XL,XU).
FCT - THE NAME OF THE EXTERNAL DOUBLE PRECISION FUNCTION
SUBPROGRAM USED.
Y - RESULTING DOUBLE PRECISION APPROXIMATION FOR THE
INTEGRAL VALUE.
IER - A RESULTING ERROR PARAMETER.
AUX - AUXILIARY DOUBLE PRECISION STORAGE ARRAY WITH
DIMENSION NDIM.
REMARKS
ERROR PARAMETER IER IS CODED IN THE FOLLOWING FORM
IER=0 - IT WAS POSSIBLE TO REACH THE REQUIRED ACCURACY.
NO ERROR.
IER=1 - IT IS IMPOSSIBLE TO REACH THE REQUIRED ACCURACY
BECAUSE OF ROUNDING ERRORS.
IER=2 - IT WAS IMPOSSIBLE TO CHECK ACCURACY BECAUSE NDIM
IS LESS THAN 5, OR THE REQUIRED ACCURACY COULD NOT
BE REACHED WITHIN NDIM-1 STEPS. NDIM SHOULD BE
INCREASED.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)
MUST BE CODED BY THE USER. ITS DOUBLE PRECISION ARGUMENT X
SHOULD NOT BE DESTROYED.
METHOD
EVALUATION OF Y IS DONE BY MEANS OF TRAPEZOIDAL RULE IN
CONNECTION WITH ROMBERGS PRINCIPLE. ON RETURN Y CONTAINS
THE BEST POSSIBLE APPROXIMATION OF THE INTEGRAL VALUE AND
VECTOR AUX THE UPWARD DIAGONAL OF ROMBERG SCHEME.
COMPONENTS AUX(I) (I=1,2,...,IEND), WITH IEND LESS THAN OR
EQUAL TO NDIM) BECOME APPROXIMATIONS TO INTEGRAL VALUE WITH
DECREASING ACCURACY BY MULTIPLICATION WITH (XU-XL).
FOR REFERENCE, SEE
(1) FILIPPI, DAS VERFAHREN VON ROMBERG-STIEFEL-BAUER ALS
SPEZIALFALL DES ALLGEMEINEN PRINZIPI VON RICHARDSON,
MATHEMATIK-TECHNIK-WIRTSCHAFT, VOL.11, ISS.2 (1964),
PP.49-54.
(2) BAUER, ALGORITHM 60, CACM, VOL.4, ISS.6 (1961), PP.255.
..... QDQAT 610
..... QDQAT 620
..... QDQAT 630
..... QDQAT 640
..... QDQAT 650
..... QDQAT 660
..... QDQAT 670
..... QDQAT 680
..... QDQAT 690
..... QDQAT 700
..... QDQAT 710
..... QDQAT 720
..... QDQAT 730
..... QDQAT 740
..... QDQAT 750
..... QDQAT 760
..... QDQAT 770
..... QDQAT 780
..... QDQAT 790
..... QDQAT 800
..... QDQAT 810
..... QDQAT 820
..... QDQAT 830
..... QDQAT 840
..... QDQAT 850
..... QDQAT 860
..... QDQAT 870
..... QDQAT 880
..... QDQAT 890
..... QDQAT 900
..... QDQAT 910
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..... QDQAT 930
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..... QDQAT1070
..... QDQAT1080
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..... QDQAT1100
..... QDQAT1110
..... QDQAT1120
..... QDQAT1130
..... QDQAT1140
..... QDQAT1150
..... QDQAT1160
..... QDQAT1170
..... QDQAT1180
..... QDQAT1190

SUBROUTINE DQATR(XL,XU,EPS,NDIM,FCT,Y,IER,AUX)
DIMENSION AUX(1)
DOUBLE PRECISION AUX,XL,XU,X,Y,H,HH,HD,P,Q,SM,FCT
PREPARATIONS OF ROMBERG-LOOP
AUX(1)=.500*(FCT(XL)+FCT(XU))
H=XU-XL
IF(NDIM<=1),8,1
1 IF(H/2,10,2
NDIM IS GREATER THAN 1 AND H IS NOT EQUAL TO 0.
2 HH=H
E=EPS/ABS(H)
DELTA=0.
P=1.
JJ=1
DO 7 I=2,NDIM
Y=AUX(1)
DELTA=DELTA/2
HD=HH
HH=.500*HH
P=.500*P
X=XL+HH
SM=0.0
DO 3 J=1,JJ
SM=SM+FCT(X)
3 X=X+HD
AUX(1)=.500*AUX(1)+P*SM
A NEW APPROXIMATION OF INTEGRAL VALUE IS COMPUTED BY MEANS OF
TRAPEZOIDAL RULE.
START OF ROMBERGS EXTRAPOLATION METHOD.
Q=1.00
JI=1
DO 4 J=1,JJ
I=1-J
Q=Q+Q
Q=Q*Q
4 AUX(1)=AUX(1+1)+(AUX(1+1)-AUX(1))/(Q-1.00)
END OF ROMBERG-STEP
..... QDQAT 1050
DELTA=ABS(Y-AUX(1))
IF(I<=5),5,5
5 IF(DELTA<=E),10,10,6
6 IF(DELTA<=DELTA/7,11,11
7 JJ=JJ+JJ
8 IER=2
9 Y=H*AUX(1)
RETURN
10 IER=0
GO TO 9
11 IER=1
Y=H*Y
RETURN
END
..... QDQAT 1060
..... QDQAT 1070
..... QDQAT 1080
..... QDQAT 1090
..... QDQAT 1100
..... QDQAT 1110
..... QDQAT 1120
..... QDQAT 1130
..... QDQAT 1140
..... QDQAT 1150
..... QDQAT 1160
..... QDQAT 1170
..... QDQAT 1180
..... QDQAT 1190

```

Subroutines QG2, QG3, ..., QG10, DQG4, DQG8, DQG12, DQG16, DQG24, DQG32

These subroutines perform the integration of a given function by Gaussian quadrature formulas.

To compute:

$$y = \int_a^b f(x) dx$$

Gaussian quadrature formulas with $n = 2, 3, \dots, 10$ (or $n = 4, 8, 12, 16, 24, 32$) points are used. Transforming the range $x = a \dots b$ into $t = -1 \dots 1$ by:

$$t = \frac{2x - (a+b)}{b-a}, \quad x = \frac{b-a}{2}t + \frac{b+a}{2}$$

the result is:

$$y = \frac{b-a}{2} \int_{-1}^1 \varphi(t) dt \quad \text{with } \varphi(t) = f\left(\frac{b-a}{2}t + \frac{b+a}{2}\right)$$

Using:

$$\int_{-1}^1 \varphi(t) dt = \sum_{k=1}^n \left[A_k^{(n)} \varphi(t_k^{(n)}) \right] \quad (n = 2, 3, \dots)$$

with coefficients $A_k^{(n)}$ and nodes $t_k^{(n)}$ (note that $t_k^{(n)}$ are the roots of Legendre polynomials of degree n), the result is the approximations:

$$y_n = (b-a) \cdot \sum_{k=1}^n \left\{ \frac{A_k^{(n)}}{2} \cdot f \left[(b-a) \cdot \frac{t_k^{(n)}}{2} + \frac{b+a}{2} \right] \right\} \quad (n = 2, 3, \dots), \quad (1)$$

which are exact whenever $f(x)$ is a polynomial up to the degree $2n-1$.

The $A_k^{(n)}$ and $t_k^{(n)}$ are symmetric with respect to $t = 0$:

$$A_k^{(n)} = A_{n-k+1}^{(n)}, \quad t_k^{(n)} = -t_{n-k+1}^{(n)}$$

For reference see: V.J. Krylov, Approximate Calculation of Integrals. Macmillan, New York/London, 1962, pp. 100-111 and 337-340.

```

C
C ..... QG2 10
C QG2 20
C SUBROUTINE QG2 QG2 30
C QG2 40
C PURPOSE QG2 50
C TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU) QG2 70
C QG2 80
C USAGE QG2 90
C CALL QG2 (XL,XU,FCT,Y) QG2 100
C PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT QG2 110
C QG2 120
C DESCRIPTION OF PARAMETERS QG2 130
C XL - THE LOWER BOUND OF THE INTERVAL. QG2 140
C XU - THE UPPER BOUND OF THE INTERVAL. QG2 150
C FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED. QG2 160
C Y - THE RESULTING INTEGRAL VALUE. QG2 170
C QG2 180
C REMARKS QG2 190
C NONE QG2 200
C QG2 210
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED QG2 220
C THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED QG2 230
C BY THE USER. QG2 240
C QG2 250
C METHOD QG2 260
C EVALUATION IS DONE BY MEANS OF 2-POINT GAUSS QUADRATURE QG2 270
C FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 3. QG2 280
C EXACTLY. QG2 290
C FOR REFERENCE, SEE QG2 300
C V.I. KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, QG2 310
C MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-338. QG2 320
C QG2 330
C ..... QG2 340
C QG2 350
C SUBROUTINE QG2(XL,XU,FCT,Y) QG2 360
C QG2 370
C QG2 380
C A=.5*(XU+XL) QG2 390
C B=XU-XL QG2 400
C Y=.2086751*B QG2 410
C Y=.5*B*(FCT(A+Y)+FCT(A-Y)) QG2 420
C RETURN QG2 430
C END QG2 440

```

```

C
C ..... QG3 10
C QG3 20
C SUBROUTINE QG3 QG3 30
C QG3 40
C PURPOSE QG3 50
C TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU) QG3 70
C QG3 80
C USAGE QG3 100
C CALL QG3 (XL,XU,FCT,Y) QG3 110
C PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT QG3 120
C QG3 130
C DESCRIPTION OF PARAMETERS QG3 140
C XL - THE LOWER BOUND OF THE INTERVAL. QG3 150
C XU - THE UPPER BOUND OF THE INTERVAL. QG3 160
C FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED. QG3 170
C Y - THE RESULTING INTEGRAL VALUE. QG3 180
C QG3 190
C REMARKS QG3 200
C NONE QG3 210
C QG3 220
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED QG3 230
C THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED QG3 240
C BY THE USER. QG3 250
C QG3 260
C METHOD QG3 270
C EVALUATION IS DONE BY MEANS OF 3-POINT GAUSS QUADRATURE QG3 280
C FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 5 QG3 290
C EXACTLY. QG3 300
C FOR REFERENCE, SEE QG3 310
C V.I. KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, QG3 320
C MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-338. QG3 330
C QG3 340
C ..... QG3 350
C QG3 360
C SUBROUTINE QG3(XL,XU,FCT,Y) QG3 370
C QG3 380
C QG3 390
C A=.5*(XU+XL) QG3 400
C B=XU-XL QG3 410
C Y=.3872983*B QG3 420
C Y=.2777778*(FCT(A+Y)+FCT(A-Y)) QG3 430
C Y=.4444444*(FCT(A)) QG3 440
C RETURN QG3 450
C END

```

```

C          QG4 10
C          QG4 20
C          QG4 30
C          QG4 40
C          QG4 50
C          QG4 60
C          QG4 70
C          QG4 80
C          QG4 90
C          QG4 100
C          QG4 110
C          QG4 120
C          QG4 130
C          QG4 140
C          QG4 150
C          QG4 160
C          QG4 170
C          QG4 180
C          QG4 190
C          QG4 200
C          QG4 210
C          QG4 220
C          QG4 230
C          QG4 240
C          QG4 250
C          QG4 260
C          QG4 270
C          QG4 280
C          QG4 290
C          QG4 300
C          QG4 310
C          QG4 320
C          QG4 330
C          QG4 340
C          QG4 350
C          QG4 360
C          QG4 370
C          QG4 380
C          QG4 390
C          QG4 400
C          QG4 410
C          QG4 420
C          QG4 430
C          QG4 440
C          QG4 450
C          QG4 460
C
C          SUBROUTINE QG4(XL,XU,FCT,Y)
C
C          A= .5*(XU+XL)
C          B=XU-XL
C          C=.4305682*B
C          Y=.1739274*(FCT(A+C)+FCT(A-C))
C          C=.1699905*B
C          Y=B*(Y+.3260726*(FCT(A+C)+FCT(A-C)))
C          RETURN
C          END

```

```

C          QG5 10
C          QG5 20
C          QG5 30
C          QG5 40
C          QG5 50
C          QG5 60
C          QG5 70
C          QG5 80
C          QG5 90
C          QG5 100
C          QG5 110
C          QG5 120
C          QG5 130
C          QG5 140
C          QG5 150
C          QG5 160
C          QG5 170
C          QG5 180
C          QG5 190
C          QG5 200
C          QG5 210
C          QG5 220
C          QG5 230
C          QG5 240
C          QG5 250
C          QG5 260
C          QG5 270
C          QG5 280
C          QG5 290
C          QG5 300
C          QG5 310
C          QG5 320
C          QG5 330
C          QG5 340
C          QG5 350
C          QG5 360
C          QG5 370
C          QG5 380
C          QG5 390
C          QG5 400
C          QG5 410
C          QG5 420
C          QG5 430
C          QG5 440
C          QG5 450
C          QG5 460
C          QG5 470
C
C          SUBROUTINE QG5(XL,XU,FCT,Y)
C
C          A= .5*(XU+XL)
C          B=XU-XL
C          C=.4530899*B
C          Y=.1184634*(FCT(A+C)+FCT(A-C))
C          C=.2692347*B
C          Y=Y+.2393143*(FCT(A+C)+FCT(A-C))
C          Y=B*(Y+.2844444*FCT(A))
C          RETURN
C          END

```

```

C          DQG4 10
C          DQG4 20
C          DQG4 30
C          DQG4 40
C          DQG4 50
C          DQG4 60
C          DQG4 70
C          DQG4 80
C          DQG4 90
C          DQG4 100
C          DQG4 110
C          DQG4 120
C          DQG4 130
C          DQG4 140
C          DQG4 150
C          DQG4 160
C          DQG4 170
C          DQG4 180
C          DQG4 190
C          DQG4 200
C          DQG4 210
C          DQG4 220
C          DQG4 230
C          DQG4 240
C          DQG4 250
C          DQG4 260
C          DQG4 270
C          DQG4 280
C          DQG4 290
C          DQG4 300
C          DQG4 310
C          DQG4 320
C          DQG4 330
C          DQG4 340
C          DQG4 350
C          DQG4 360
C          DQG4 370
C          DQG4 380
C          DQG4 390
C          DQG4 400
C          DQG4 410
C          DQG4 420
C          DQG4 430
C          DQG4 440
C          DQG4 450
C          DQG4 460
C          DQG4 470
C          DQG4 480
C
C          SUBROUTINE DQG4(XL,XU,FCT,Y)
C
C          DOUBLE PRECISION XL,XU,Y,A,B,C,FCT
C
C          A=.500*(XU+XL)
C          B=XU-XL
C          C=.4305681557970262900*B
C          Y=.1739274225687269300*(FCT(A+C)+FCT(A-C))
C          C=.1699905217924281300*B
C          Y=B*(Y+.3260725774312730700*(FCT(A+C)+FCT(A-C)))
C          RETURN
C          END

```

```

C          QG6 10
C          QG6 20
C          QG6 30
C          QG6 40
C          QG6 50
C          QG6 60
C          QG6 70
C          QG6 80
C          QG6 90
C          QG6 100
C          QG6 110
C          QG6 120
C          QG6 130
C          QG6 140
C          QG6 150
C          QG6 160
C          QG6 170
C          QG6 180
C          QG6 190
C          QG6 200
C          QG6 210
C          QG6 220
C          QG6 230
C          QG6 240
C          QG6 250
C          QG6 260
C          QG6 270
C          QG6 280
C          QG6 290
C          QG6 300
C          QG6 310
C          QG6 320
C          QG6 330
C          QG6 340
C          QG6 350
C          QG6 360
C          QG6 370
C          QG6 380
C          QG6 390
C          QG6 400
C          QG6 410
C          QG6 420
C          QG6 430
C          QG6 440
C          QG6 450
C          QG6 460
C          QG6 470
C          QG6 480
C
C          SUBROUTINE QG6(XL,XU,FCT,Y)
C
C          A=.5*(XU+XL)
C          B=XU-XL
C          C=.4662348*B
C          Y=.08566225*(FCT(A+C)+FCT(A-C))
C          C=.3306047*B
C          Y=Y+.1803808*(FCT(A+C)+FCT(A-C))
C          C=.1193096*B
C          Y=B*(Y+.2339570*(FCT(A+C)+FCT(A-C)))
C          RETURN
C          END

```



```

C          QG7 10
C          ..... QG7 20
C          SUBROUTINE QG7          QG7 30
C          QG7 40
C          PURPOSE          QG7 50
C          TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU)  QG7 60
C          QG7 80
C          USAGE          QG7 90
C          CALL QG7 (XL,XU,FCT,Y)  QG7 100
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT  QG7 110
C          QG7 120
C          DESCRIPTION OF PARAMETERS  QG7 130
C          XL - THE LOWER BOUND OF THE INTERVAL.  QG7 140
C          XU - THE UPPER BOUND OF THE INTERVAL.  QG7 150
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.  QG7 160
C          Y - THE RESULTING INTEGRAL VALUE.  QG7 170
C          QG7 180
C          REMARKS  QG7 190
C          NONE  QG7 200
C          QG7 210
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED  QG7 220
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED  QG7 230
C          BY THE USER.  QG7 240
C          QG7 250
C          METHOD  QG7 260
C          EVALUATION IS DONE BY MEANS OF 7-POINT GAUSS QUADRATURE  QG7 270
C          FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 13  QG7 280
C          EXACTLY.  QG7 290
C          FOR REFERENCE, SEE  QG7 300
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,  QG7 310
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-338.  QG7 320
C          QG7 330
C          ..... QG7 340
C          SUBROUTINE QG7(XL,XU,FCT,Y)  QG7 350
C          QG7 360
C          QG7 370
C          QG7 380
C          QG7 390
C          QG7 400
C          QG7 410
C          QG7 420
C          C=.3707656*B  QG7 430
C          Y=Y+.1398527*(FCT(A+C)+FCT(A-C))  QG7 440
C          C=.2029226*B  QG7 450
C          Y=Y+.1909150*(FCT(A+C)+FCT(A-C))  QG7 460
C          Y=B*(Y+.2089796*FCT(A))  QG7 470
C          RETURN  QG7 480
C          END  QG7 490

```

```

C          ..... QG8 10
C          SUBROUTINE QG8          QG8 20
C          QG8 30
C          PURPOSE          QG8 40
C          TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU)  QG8 50
C          QG8 60
C          USAGE          QG8 70
C          CALL QG8 (XL,XU,FCT,Y)  QG8 80
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT  QG8 90
C          QG8 100
C          QG8 110
C          QG8 120
C          DESCRIPTION OF PARAMETERS  QG8 130
C          XL - DOUBLE PRECISION LOWER BOUND OF THE INTERVAL.  QG8 140
C          XU - DOUBLE PRECISION UPPER BOUND OF THE INTERVAL.  QG8 150
C          FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION  QG8 160
C          SUBPROGRAM USED.  QG8 170
C          Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.  QG8 180
C          QG8 190
C          REMARKS  QG8 200
C          NONE  QG8 210
C          QG8 220
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED  QG8 230
C          THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)  QG8 240
C          MUST BE FURNISHED BY THE USER.  QG8 250
C          QG8 260
C          METHOD  QG8 270
C          EVALUATION IS DONE BY MEANS OF 8-POINT GAUSS QUADRATURE  QG8 280
C          FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 15  QG8 290
C          EXACTLY. FOR REFERENCE, SEE  QG8 300
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,  QG8 310
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-340.  QG8 320
C          QG8 330
C          ..... QG8 340
C          SUBROUTINE QG8(XL,XU,FCT,Y)  QG8 350
C          QG8 360
C          QG8 370
C          QG8 380
C          QG8 390
C          QG8 400
C          QG8 410
C          QG8 420
C          C=.4801449282487681200*B  QG8 430
C          Y=.506142681451881300-1*(FCT(A+C)+FCT(A-C))  QG8 440
C          C=.398332387068133700*B  QG8 450
C          Y=Y-.1111905172266872400*(FCT(A+C)+FCT(A-C))  QG8 460
C          C=.2627662049981644900*B  QG8 470
C          Y=Y+.1568533229389436400*(FCT(A+C)+FCT(A-C))  QG8 480
C          C=.91717321247824900-1*B  QG8 490
C          Y=B*(Y+.1813418916891809900*(FCT(A+C)+FCT(A-C)))  QG8 500
C          RETURN  QG8 510
C          END  QG8 520

```

```

C          ..... QG9 10
C          SUBROUTINE QG9          QG9 20
C          QG9 30
C          PURPOSE          QG9 40
C          TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU)  QG9 50
C          QG9 60
C          USAGE          QG9 70
C          CALL QG9 (XL,XU,FCT,Y)  QG9 80
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT  QG9 90
C          QG9 100
C          QG9 110
C          QG9 120
C          DESCRIPTION OF PARAMETERS  QG9 130
C          XL - THE LOWER BOUND OF THE INTERVAL.  QG9 140
C          XU - THE UPPER BOUND OF THE INTERVAL.  QG9 150
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.  QG9 160
C          Y - THE RESULTING INTEGRAL VALUE.  QG9 170
C          QG9 180
C          REMARKS  QG9 190
C          NONE  QG9 200
C          QG9 210
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED  QG9 220
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED  QG9 230
C          BY THE USER.  QG9 240
C          QG9 250
C          METHOD  QG9 260
C          EVALUATION IS DONE BY MEANS OF 9-POINT GAUSS QUADRATURE  QG9 270
C          FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 17  QG9 280
C          EXACTLY.  QG9 290
C          FOR REFERENCE, SEE  QG9 300
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,  QG9 310
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-338.  QG9 320
C          QG9 330
C          ..... QG9 340
C          SUBROUTINE QG9(XL,XU,FCT,Y)  QG9 350
C          QG9 360
C          QG9 370
C          QG9 380
C          QG9 390
C          QG9 400
C          QG9 410
C          QG9 420
C          C=.4801449*B  QG9 430
C          Y=.04063719*(FCT(A+C)+FCT(A-C))  QG9 440
C          C=.4180156*B  QG9 450
C          Y=Y+.09032408*(FCT(A+C)+FCT(A-C))  QG9 460
C          C=.3066857*B  QG9 470
C          Y=Y+.1303053*(FCT(A+C)+FCT(A-C))  QG9 480
C          C=.1621267*B  QG9 490
C          Y=Y+.1561735*(FCT(A+C)+FCT(A-C))  QG9 500
C          Y=B*(Y+.1651197*FCT(A))  QG9 510
C          RETURN  QG9 520
C          END  QG9 530

```

```

C          ..... QG8 10
C          SUBROUTINE QG8          QG8 20
C          QG8 30
C          PURPOSE          QG8 40
C          TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU)  QG8 50
C          QG8 60
C          USAGE          QG8 70
C          CALL QG8 (XL,XU,FCT,Y)  QG8 80
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT  QG8 90
C          QG8 100
C          QG8 110
C          QG8 120
C          DESCRIPTION OF PARAMETERS  QG8 130
C          XL - THE LOWER BOUND OF THE INTERVAL.  QG8 140
C          XU - THE UPPER BOUND OF THE INTERVAL.  QG8 150
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.  QG8 160
C          Y - THE RESULTING INTEGRAL VALUE.  QG8 170
C          QG8 180
C          REMARKS  QG8 190
C          NONE  QG8 200
C          QG8 210
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED  QG8 220
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED  QG8 230
C          BY THE USER.  QG8 240
C          QG8 250
C          METHOD  QG8 260
C          EVALUATION IS DONE BY MEANS OF 8-POINT GAUSS QUADRATURE  QG8 270
C          FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 13  QG8 280
C          EXACTLY.  QG8 290
C          FOR REFERENCE, SEE  QG8 300
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,  QG8 310
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-338.  QG8 320
C          QG8 330
C          ..... QG8 340
C          SUBROUTINE QG8(XL,XU,FCT,Y)  QG8 350
C          QG8 360
C          QG8 370
C          QG8 380
C          QG8 390
C          QG8 400
C          QG8 410
C          QG8 420
C          C=.4801449*B  QG8 430
C          Y=.05061427*(FCT(A+C)+FCT(A-C))  QG8 440
C          C=.3983332*B  QG8 450
C          Y=Y+.1111905*(FCT(A+C)+FCT(A-C))  QG8 460
C          C=.2627662*B  QG8 470
C          Y=Y+.1568533*(FCT(A+C)+FCT(A-C))  QG8 480
C          C=.09171732*B  QG8 490
C          Y=B*(Y+.1813419*(FCT(A+C)+FCT(A-C)))  QG8 500
C          RETURN  QG8 510
C          END  QG8 520

```

QG10 10
.....QG10 20
C QG10 30
C QG10 40
C QG10 50
C QG10 60
C QG10 70
C QG10 80
C QG10 90
C QG10 100
C QG10 110
C QG10 120
C QG10 130
C QG10 140
C QG10 150
C QG10 160
C QG10 170
C QG10 180
C QG10 190
C QG10 200
C QG10 210
C QG10 220
C QG10 230
C QG10 240
C QG10 250
C QG10 260
C QG10 270
C QG10 280
C QG10 290
C QG10 300
C QG10 310
C QG10 320
C QG10 330
C QG10 340
C QG10 350
C QG10 360
C QG10 370
C QG10 380
C QG10 390
C QG10 400
C QG10 410
C QG10 420
C QG10 430
C QG10 440
C QG10 450
C QG10 460
C QG10 470
C QG10 480
C QG10 490
C QG10 500
C QG10 510
C QG10 520

SUBROUTINE QG10

PURPOSE
TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU)

USAGE

CALL QG10(XL,XU,FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT

DESCRIPTION OF PARAMETERS

XL - THE LOWER BOUND OF THE INTERVAL.
XU - THE UPPER BOUND OF THE INTERVAL.
FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
Y - THE RESULTING INTEGRAL VALUE.

REMARKS

NONE

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED BY THE USER.

METHOD

EVALUATION IS DONE BY MEANS OF 10-POINT GAUSS QUADRATURE FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 19 EXACTLY. FOR REFERENCE, SEE V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-338.

SUBROUTINE QG10(XL,XU,FCT,Y)

A=.5*(XU+XL)
B=XU-XL
C=.4869533*B
Y=.0333567*(FCT(A+C)+FCT(A-C))
C=.4325317*B
Y=Y+.07472567*(FCT(A+C)+FCT(A-C))
C=.339704*B
Y=Y+.1095432*(FCT(A+C)+FCT(A-C))
C=.2166977*B
Y=Y+.1346334*(FCT(A+C)+FCT(A-C))
C=.0744371*B
Y=B*(Y+.1477621*(FCT(A+C)+FCT(A-C)))
RETURN
END

DG16 10
.....DG16 20
C DG16 30
C DG16 40
C DG16 50
C DG16 60
C DG16 70
C DG16 80
C DG16 90
C DG16 100
C DG16 110
C DG16 120
C DG16 130
C DG16 140
C DG16 150
C DG16 160
C DG16 170
C DG16 180
C DG16 190
C DG16 200
C DG16 210
C DG16 220
C DG16 230
C DG16 240
C DG16 250
C DG16 260
C DG16 270
C DG16 280
C DG16 290
C DG16 300
C DG16 310
C DG16 320
C DG16 330
C DG16 340
C DG16 350
C DG16 360
C DG16 370
C DG16 380
C DG16 390
C DG16 400
C DG16 410
C DG16 420
C DG16 430
C DG16 440
C DG16 450
C DG16 460
C DG16 470
C DG16 480
C DG16 490
C DG16 500
C DG16 510
C DG16 520
C DG16 530
C DG16 540
C DG16 550
C DG16 560
C DG16 570
C DG16 580
C DG16 590
C DG16 600

SUBROUTINE DQG16

PURPOSE
TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU)

USAGE

CALL DQG16 (XL,XU,FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT

DESCRIPTION OF PARAMETERS

XL - DOUBLE PRECISION LOWER BOUND OF THE INTERVAL.
XU - DOUBLE PRECISION UPPER BOUND OF THE INTERVAL.
FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM USED.
Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.

REMARKS

NONE

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED BY THE USER.

METHOD

EVALUATION IS DONE BY MEANS OF 16-POINT GAUSS QUADRATURE FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 31 EXACTLY. FOR REFERENCE, SEE V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-340.

SUBROUTINE DQG16(XL,XU,FCT,Y)

DOUBLE PRECISION XL,XU,Y,A,B,C,FCT
A=.500*(XU+XL)
B=XU-XL
C=.494700674958249700*B
Y=.1357622970587704-1*(FCT(A+C)+FCT(A-C))
C=.4722875115366162900*B
Y=Y+.31126761969329960-1*(FCT(A+C)+FCT(A-C))
C=.4328156011939158700*B
Y=Y+.475792558412463920-1*(FCT(A+C)+FCT(A-C))
C=.3777022041775015200*B
Y=Y+.6231444856277669360-1*(FCT(A+C)+FCT(A-C))
C=.3089381222013218700*B
Y=Y+.74797944082889370-1*(FCT(A+C)+FCT(A-C))
C=.2290083888286136900*B
Y=Y+.84578259697501270-1*(FCT(A+C)+FCT(A-C))
C=.1408017753896294600*B
Y=Y+.91301707522461790-1*(FCT(A+C)+FCT(A-C))
C=.475062549188187200-1*B
Y=B*(Y+.94725305227534250-1*(FCT(A+C)+FCT(A-C)))
RETURN
END

DG12 10
.....DG12 20
C DG12 30
C DG12 40
C DG12 50
C DG12 60
C DG12 70
C DG12 80
C DG12 90
C DG12 100
C DG12 110
C DG12 120
C DG12 130
C DG12 140
C DG12 150
C DG12 160
C DG12 170
C DG12 180
C DG12 190
C DG12 200
C DG12 210
C DG12 220
C DG12 230
C DG12 240
C DG12 250
C DG12 260
C DG12 270
C DG12 280
C DG12 290
C DG12 300
C DG12 310
C DG12 320
C DG12 330
C DG12 340
C DG12 350
C DG12 360
C DG12 370
C DG12 380
C DG12 390
C DG12 400
C DG12 410
C DG12 420
C DG12 430
C DG12 440
C DG12 450
C DG12 460
C DG12 470
C DG12 480
C DG12 490
C DG12 500
C DG12 510
C DG12 520
C DG12 530
C DG12 540
C DG12 550
C DG12 560

SUBROUTINE DQG12

PURPOSE
TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU)

USAGE

CALL DQG12 (XL,XU,FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT

DESCRIPTION OF PARAMETERS

XL - DOUBLE PRECISION LOWER BOUND OF THE INTERVAL.
XU - DOUBLE PRECISION UPPER BOUND OF THE INTERVAL.
FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM USED.
Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.

REMARKS

NONE

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED BY THE USER.

METHOD

EVALUATION IS DONE BY MEANS OF 12-POINT GAUSS QUADRATURE FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 23 EXACTLY. FOR REFERENCE, SEE V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-340.

SUBROUTINE DQG12(XL,XU,FCT,Y)

DOUBLE PRECISION XL,XU,Y,A,B,C,FCT
A=.500*(XU+XL)
B=XU-XL
C=.4907803171233596300*B
Y=.235876681932559140-1*(FCT(A+C)+FCT(A-C))
C=.4520586281852374300*B
Y=Y+.534696629976592150-1*(FCT(A+C)+FCT(A-C))
C=.3849513370971523400*B
Y=Y+.80039164271673110-1*(FCT(A+C)+FCT(A-C))
C=.2936589771433087200*B
Y=Y+.1015837133615329600*(FCT(A+C)+FCT(A-C))
C=.18391574949901000*B
Y=Y+.1167462682691774000*(FCT(A+C)+FCT(A-C))
C=.626167042557344580-1*B
Y=B*(Y+.124535229067013900*(FCT(A+C)+FCT(A-C)))
RETURN
END

DG24 10
.....DG24 20
C DG24 30
C DG24 40
C DG24 50
C DG24 60
C DG24 70
C DG24 80
C DG24 90
C DG24 100
C DG24 110
C DG24 120
C DG24 130
C DG24 140
C DG24 150
C DG24 160
C DG24 170
C DG24 180
C DG24 190
C DG24 200
C DG24 210
C DG24 220
C DG24 230
C DG24 240
C DG24 250
C DG24 260
C DG24 270
C DG24 280
C DG24 290
C DG24 300
C DG24 310
C DG24 320
C DG24 330
C DG24 340
C DG24 350
C DG24 360
C DG24 370
C DG24 380
C DG24 390
C DG24 400
C DG24 410
C DG24 420
C DG24 430
C DG24 440
C DG24 450
C DG24 460
C DG24 470
C DG24 480
C DG24 490
C DG24 500
C DG24 510
C DG24 520
C DG24 530
C DG24 540
C DG24 550
C DG24 560
C DG24 570
C DG24 580
C DG24 590
C DG24 600

SUBROUTINE DQG24

PURPOSE
TO COMPUTE INTEGRAL(FCT(X), SUMMED OVER X FROM XL TO XU)

USAGE

CALL DQG24 (XL,XU,FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT

DESCRIPTION OF PARAMETERS

XL - DOUBLE PRECISION LOWER BOUND OF THE INTERVAL.
XU - DOUBLE PRECISION UPPER BOUND OF THE INTERVAL.
FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM USED.
Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.

REMARKS

NONE

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED BY THE USER.

METHOD

EVALUATION IS DONE BY MEANS OF 24-POINT GAUSS QUADRATURE FORMULA, WHICH INTEGRATES POLYNOMIALS UP TO DEGREE 47 EXACTLY. FOR REFERENCE, SEE V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, MACMILLAN, NEW YORK/LONDON, 1962, PP.100-111 AND 337-340.

SUBROUTINE DQG24(XL,XU,FCT,Y)

DOUBLE PRECISION XL,XU,Y,A,B,C,FCT
A=.500*(XU+XL)
B=XU-XL
C=.4975936099995106800*B
Y=.617061489999359980-2*(FCT(A+C)+FCT(A-C))
C=.4873642779856547500*B
Y=Y+.142656943144668320-1*(FCT(A+C)+FCT(A-C))
C=.4691372760013663800*B
Y=Y+.22138719408709930-1*(FCT(A+C)+FCT(A-C))
C=.4432077635022005200*B
Y=Y+.296492924577183900-1*(FCT(A+C)+FCT(A-C))
C=.4100099929869514600*B
Y=Y+.366732407055491530-1*(FCT(A+C)+FCT(A-C))
C=.370062095789271800*B
Y=Y+.430950807659766380-1*(FCT(A+C)+FCT(A-C))
C=.3240468259684877800*B
Y=Y+.488093260520569440-1*(FCT(A+C)+FCT(A-C))
C=.272710735694419700*B
Y=Y+.537221350579828170-1*(FCT(A+C)+FCT(A-C))
C=.2168967538130225700*B
Y=Y+.577528340268628010-1*(FCT(A+C)+FCT(A-C))
C=.1575213398480816900*B
Y=Y+.608352364639016960-1*(FCT(A+C)+FCT(A-C))
C=.9559433736808150-1*B
Y=Y+.629187281734144800-1*(FCT(A+C)+FCT(A-C))
C=.320284464313028130-1*B
Y=B*(Y+.639690976733760780-1*(FCT(A+C)+FCT(A-C)))
RETURN
END


```

C      QL3  10
C      .....
C      SUBROUTINE QL3
C      .....
C      PURPOSE
C      TO COMPUTE INTEGRAL(EXP(-X)*FCT(X), SUMMED OVER X FROM 0
C      TO INFINITY).
C      .....
C      USAGE
C      CALL QL3 (FCT,Y)
C      PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C      .....
C      DESCRIPTION OF PARAMETERS
C      FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
C      Y   - THE RESULTING INTEGRAL VALUE.
C      .....
C      REMARKS
C      NONE
C      .....
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C      THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
C      BY THE USER.
C      .....
C      METHOD
C      EVALUATION IS DONE BY MEANS OF 3-POINT GAUSSIAN-LAGUERRE
C      QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER
C      FCT(X) IS A POLYNOMIAL UP TO DEGREE 5.
C      FOR REFERENCE, SEE
C      V.I. KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,
C      MACMILLAN, NEW YORK/LONDON, 1962, PP.130-132 AND 347-352.
C      .....
C      SUBROUTINE QL3(FCT,Y)
C      .....
C      X=6.289945
C      Y=.01038926*FCT(X)
C      X=2.294280
C      Y=Y+.2785177*FCT(X)
C      X=-.4157746
C      Y=Y+.7110930*FCT(X)
C      RETURN
C      END

```

```

C      DQL4 10
C      .....
C      SUBROUTINE DQL4
C      .....
C      PURPOSE
C      TO COMPUTE INTEGRAL(EXP(-X)*FCT(X), SUMMED OVER X
C      FROM 0 TO INFINITY).
C      .....
C      USAGE
C      CALL DQL4 (FCT,Y)
C      PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C      .....
C      DESCRIPTION OF PARAMETERS
C      FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION
C      SUBPROGRAM USED.
C      Y   - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.
C      .....
C      REMARKS
C      NONE
C      .....
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C      THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)
C      MUST BE FURNISHED BY THE USER.
C      .....
C      METHOD
C      EVALUATION IS DONE BY MEANS OF 4-POINT GAUSSIAN-LAGUERRE
C      QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY,
C      WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 7.
C      FOR REFERENCE, SEE
C      SHAO/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF
C      CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED
C      GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT
C      TROO.1100 (MARCH 1964), PP.24-29.
C      .....
C      SUBROUTINE DQL4(FCT,Y)
C      .....
C      DOUBLE PRECISION X,Y,FCT
C      .....
C      X=.939507091230113301
C      Y=.539294705561327450-3*FCT(X)
C      X=.4536620296921128001
C      Y=Y+.388879085150053840-1*FCT(X)
C      X=.1745761101158346601
C      Y=Y+.3574186924377986900*FCT(X)
C      X=.3225476896193923100
C      Y=Y+.6031541043416336000*FCT(X)
C      RETURN
C      END

```

```

C      QL4  10
C      .....
C      SUBROUTINE QL4
C      .....
C      PURPOSE
C      TO COMPUTE INTEGRAL(EXP(-X)*FCT(X), SUMMED OVER X FROM 0
C      TO INFINITY).
C      .....
C      USAGE
C      CALL QL4 (FCT,Y)
C      PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C      .....
C      DESCRIPTION OF PARAMETERS
C      FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
C      Y   - THE RESULTING INTEGRAL VALUE.
C      .....
C      REMARKS
C      NONE
C      .....
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C      THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
C      BY THE USER.
C      .....
C      METHOD
C      EVALUATION IS DONE BY MEANS OF 4-POINT GAUSSIAN-LAGUERRE
C      QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER
C      FCT(X) IS A POLYNOMIAL UP TO DEGREE 7.
C      FOR REFERENCE, SEE
C      V.I. KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,
C      MACMILLAN, NEW YORK/LONDON, 1962, PP.130-132 AND 347-352.
C      .....
C      SUBROUTINE QL4(FCT,Y)
C      .....
C      X=9.395071
C      Y=.5392947E-3*FCT(X)
C      X=.4536620
C      Y=Y+.03888791*FCT(X)
C      X=1.745761
C      Y=Y+.3574187*FCT(X)
C      X=.3225477
C      Y=Y+.6031541*FCT(X)
C      RETURN
C      END

```

```

C      QL5  10
C      .....
C      SUBROUTINE QL5
C      .....
C      PURPOSE
C      TO COMPUTE INTEGRAL(EXP(-X)*FCT(X), SUMMED OVER X FROM 0
C      TO INFINITY).
C      .....
C      USAGE
C      CALL QL5 (FCT,Y)
C      PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C      .....
C      DESCRIPTION OF PARAMETERS
C      FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
C      Y   - THE RESULTING INTEGRAL VALUE.
C      .....
C      REMARKS
C      NONE
C      .....
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C      THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
C      BY THE USER.
C      .....
C      METHOD
C      EVALUATION IS DONE BY MEANS OF 5-POINT GAUSSIAN-LAGUERRE
C      QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER
C      FCT(X) IS A POLYNOMIAL UP TO DEGREE 9.
C      FOR REFERENCE, SEE
C      V.I. KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,
C      MACMILLAN, NEW YORK/LONDON, 1962, PP.130-132 AND 347-352.
C      .....
C      SUBROUTINE QL5(FCT,Y)
C      .....
C      X=12.64080
C      Y=.2336997E-4*FCT(X)
C      X=7.085810
C      Y=Y+.3611759E-2*FCT(X)
C      X=3.596426
C      Y=Y+.07596245*FCT(X)
C      X=1.413403
C      Y=Y+.3986668*FCT(X)
C      X=.2635603
C      Y=Y+.5217556*FCT(X)
C      RETURN
C      END

```

```

C
C ..... QL6 10
C ..... QL6 20
C ..... QL6 30
C ..... QL6 40
C ..... QL6 50
C ..... QL6 60
C ..... QL6 70
C ..... QL6 80
C ..... QL6 90
C ..... QL6 100
C ..... QL6 110
C ..... QL6 120
C ..... QL6 130
C ..... QL6 140
C ..... QL6 150
C ..... QL6 160
C ..... QL6 170
C ..... QL6 180
C ..... QL6 190
C ..... QL6 200
C ..... QL6 210
C ..... QL6 220
C ..... QL6 230
C ..... QL6 240
C ..... QL6 250
C ..... QL6 260
C ..... QL6 270
C ..... QL6 280
C ..... QL6 290
C ..... QL6 300
C ..... QL6 310
C ..... QL6 320
C ..... QL6 330
C ..... QL6 340
C ..... QL6 350
C ..... QL6 360
C ..... QL6 370
C ..... QL6 380
C ..... QL6 390
C ..... QL6 400
C ..... QL6 410
C ..... QL6 420
C ..... QL6 430
C ..... QL6 440
C ..... QL6 450
C ..... QL6 460
C ..... QL6 470
C ..... QL6 480
C ..... QL6 490
C ..... QL6 500
C ..... QL6 510
C
SUBROUTINE QL6(FCT,Y)
C
X=15.98287
Y=-.8985479E-6*FCT(X)
X=9.837467
Y=Y+.2610172E-3*FCT(X)
X=5.775144
Y=Y+.01339520*FCT(X)
X=2.92136
Y=Y+.113373*FCT(X)
X=1.188732
Y=Y+.4170908*FCT(X)
X=.2228466
Y=Y+.4589647*FCT(X)
RETURN
END

```

```

C ..... QLB 10
C ..... QLB 20
C ..... QLB 30
C ..... QLB 40
C ..... QLB 50
C ..... QLB 60
C ..... QLB 70
C ..... QLB 80
C ..... QLB 90
C ..... QLB 100
C ..... QLB 110
C ..... QLB 120
C ..... QLB 130
C ..... QLB 140
C ..... QLB 150
C ..... QLB 160
C ..... QLB 170
C ..... QLB 180
C ..... QLB 190
C ..... QLB 200
C ..... QLB 210
C ..... QLB 220
C ..... QLB 230
C ..... QLB 240
C ..... QLB 250
C ..... QLB 260
C ..... QLB 270
C ..... QLB 280
C ..... QLB 290
C ..... QLB 300
C ..... QLB 310
C ..... QLB 320
C ..... QLB 330
C ..... QLB 340
C ..... QLB 350
C ..... QLB 360
C ..... QLB 370
C ..... QLB 380
C ..... QLB 390
C ..... QLB 400
C ..... QLB 410
C ..... QLB 420
C ..... QLB 430
C ..... QLB 440
C ..... QLB 450
C ..... QLB 460
C ..... QLB 470
C ..... QLB 480
C ..... QLB 490
C ..... QLB 500
C ..... QLB 510
C ..... QLB 520
C ..... QLB 530
C ..... QLB 540
C ..... QLB 550
C
SUBROUTINE QLB(FCT,Y)
C
X=.22.86313
Y=-.1049001E-8*FCT(X)
X=15.74068
Y=Y+.8485747E-6*FCT(X)
X=10.75852
Y=Y+.9076509E-4*FCT(X)
X=7.045995
Y=Y+.2794536E-2*FCT(X)
X=4.266700
Y=Y+.0334349*FCT(X)
X=2.251087
Y=Y+.1757950*FCT(X)
X=.9037018
Y=Y+.4187868*FCT(X)
X=.1702796
Y=Y+.3691886*FCT(X)
RETURN
END

```

```

C ..... QL7 10
C ..... QL7 20
C ..... QL7 30
C ..... QL7 40
C ..... QL7 50
C ..... QL7 60
C ..... QL7 70
C ..... QL7 80
C ..... QL7 90
C ..... QL7 100
C ..... QL7 110
C ..... QL7 120
C ..... QL7 130
C ..... QL7 140
C ..... QL7 150
C ..... QL7 160
C ..... QL7 170
C ..... QL7 180
C ..... QL7 190
C ..... QL7 200
C ..... QL7 210
C ..... QL7 220
C ..... QL7 230
C ..... QL7 240
C ..... QL7 250
C ..... QL7 260
C ..... QL7 270
C ..... QL7 280
C ..... QL7 290
C ..... QL7 300
C ..... QL7 310
C ..... QL7 320
C ..... QL7 330
C ..... QL7 340
C ..... QL7 350
C ..... QL7 360
C ..... QL7 370
C ..... QL7 380
C ..... QL7 390
C ..... QL7 400
C ..... QL7 410
C ..... QL7 420
C ..... QL7 430
C ..... QL7 440
C ..... QL7 450
C ..... QL7 460
C ..... QL7 470
C ..... QL7 480
C ..... QL7 490
C ..... QL7 500
C ..... QL7 510
C ..... QL7 520
C ..... QL7 530
C
SUBROUTINE QL7(FCT,Y)
C
X=19.39573
Y=-.3170315E-7*FCT(X)
X=12.73418
Y=Y+.1586546E-4*FCT(X)
X=8.182153
Y=Y+.1074010E-2*FCT(X)
X=4.900353
Y=Y+.02063351*FCT(X)
X=.2567877
Y=Y+.1471263*FCT(X)
X=1.026665
Y=Y+.4218313*FCT(X)
X=.1930437
Y=Y+.4093190*FCT(X)
RETURN
END

```

```

C ..... DQL8 10
C ..... DQL8 20
C ..... DQL8 30
C ..... DQL8 40
C ..... DQL8 50
C ..... DQL8 60
C ..... DQL8 70
C ..... DQL8 80
C ..... DQL8 90
C ..... DQL8 100
C ..... DQL8 110
C ..... DQL8 120
C ..... DQL8 130
C ..... DQL8 140
C ..... DQL8 150
C ..... DQL8 160
C ..... DQL8 170
C ..... DQL8 180
C ..... DQL8 190
C ..... DQL8 200
C ..... DQL8 210
C ..... DQL8 220
C ..... DQL8 230
C ..... DQL8 240
C ..... DQL8 250
C ..... DQL8 260
C ..... DQL8 270
C ..... DQL8 280
C ..... DQL8 290
C ..... DQL8 300
C ..... DQL8 310
C ..... DQL8 320
C ..... DQL8 330
C ..... DQL8 340
C ..... DQL8 350
C ..... DQL8 360
C ..... DQL8 370
C ..... DQL8 380
C ..... DQL8 390
C ..... DQL8 400
C ..... DQL8 410
C ..... DQL8 420
C ..... DQL8 430
C ..... DQL8 440
C ..... DQL8 450
C ..... DQL8 460
C ..... DQL8 470
C ..... DQL8 480
C ..... DQL8 490
C ..... DQL8 500
C ..... DQL8 510
C ..... DQL8 520
C ..... DQL8 530
C ..... DQL8 540
C ..... DQL8 550
C
SUBROUTINE DQL8(FCT,Y)
C
X=-.2286313173688926402
Y=-.104800117481151040E-8*FCT(X)
X=-.1574067864127800502
Y=Y+.84857467162725320E-6*FCT(X)
X=-.1075851601018099502
Y=Y+.90765087733582130E-4*FCT(X)
X=-.7045905402393465701
Y=Y+.279453623522567250E-2*FCT(X)
X=-.4266700170287658001
Y=Y+.333434922612156520E-1*FCT(X)
X=.2251086629866130701
Y=Y+.1757949866371718100E*FCT(X)
X=.903701776799379900
Y=Y+.4187867808143429600E*FCT(X)
X=-.1702796323051010000
Y=Y+.3691885893416375300E*FCT(X)
RETURN
END

```

```

C ..... QL9 10
C ..... QL9 20
C ..... QL9 30
C ..... QL9 40
C ..... QL9 50
C ..... QL9 60
C ..... QL9 70
C ..... QL9 80
C ..... QL9 90
C ..... QL9 100
C ..... QL9 110
C ..... QL9 120
C ..... QL9 130
C ..... QL9 140
C ..... QL9 150
C ..... QL9 160
C ..... QL9 170
C ..... QL9 180
C ..... QL9 190
C ..... QL9 200
C ..... QL9 210
C ..... QL9 220
C ..... QL9 230
C ..... QL9 240
C ..... QL9 250
C ..... QL9 260
C ..... QL9 270
C ..... QL9 280
C ..... QL9 290
C ..... QL9 300
C ..... QL9 310
C ..... QL9 320
C ..... QL9 330
C ..... QL9 340
C ..... QL9 350
C ..... QL9 360
C ..... QL9 370
C ..... QL9 380
C ..... QL9 390
C ..... QL9 400
C ..... QL9 410
C ..... QL9 420
C ..... QL9 430
C ..... QL9 440
C ..... QL9 450
C ..... QL9 460
C ..... QL9 470
C ..... QL9 480
C ..... QL9 490
C ..... QL9 500
C ..... QL9 510
C ..... QL9 520
C ..... QL9 530
C ..... QL9 540
C ..... QL9 550
C ..... QL9 560
C ..... QL9 570

```

SUBROUTINE QL9

PURPOSE
TO COMPUTE INTEGRAL($\text{EXP}(-X)\text{FCT}(X)$), SUMMED OVER X FROM 0 TO INFINITY).

USAGE
CALL QL9 (FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT

DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
Y - THE RESULTING INTEGRAL VALUE.

REMARKS
NONE

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED BY THE USER.

METHOD
EVALUATION IS DONE BY MEANS OF 9-POINT GAUSSIAN-LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 17.
FOR REFERENCE, SEE
V.I. KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, MACMILLAN, NEW YORK/LONDON, 1962, PP.130-132 AND 347-352.

```

C ..... QL9 340
C ..... QL9 350
C ..... QL9 360
C ..... QL9 370
C ..... QL9 380
C ..... QL9 390
C ..... QL9 400
C ..... QL9 410
C ..... QL9 420
C ..... QL9 430
C ..... QL9 440
C ..... QL9 450
C ..... QL9 460
C ..... QL9 470
C ..... QL9 480
C ..... QL9 490
C ..... QL9 500
C ..... QL9 510
C ..... QL9 520
C ..... QL9 530
C ..... QL9 540
C ..... QL9 550
C ..... QL9 560
C ..... QL9 570

```

SUBROUTINE QL9(FCT,Y)

X=.2637407
Y=.3290874E-10*FCT(X)
X=.18.83360
Y=Y+.4110769E-7*FCT(X)
X=.13.46624
Y=Y+.6592123E-5*FCT(X)
X=.9.372985
Y=Y+.3052498E-3*FCT(X)
X=.6.204957
Y=Y+.00559627*FCT(X)
X=.3.783474
Y=Y+.04746056*FCT(X)
X=.2.005135
Y=Y+.1992875*FCT(X)
X=.8072200
Y=Y+.4112140*FCT(X)
X=.1523222
Y=Y+.3361264*FCT(X)
RETURN
END

```

C ..... QL10 10
C ..... QL10 20
C ..... QL10 30
C ..... QL10 40
C ..... QL10 50
C ..... QL10 60
C ..... QL10 70
C ..... QL10 80
C ..... QL10 90
C ..... QL10 100
C ..... QL10 110
C ..... QL10 120
C ..... QL10 130
C ..... QL10 140
C ..... QL10 150
C ..... QL10 160
C ..... QL10 170
C ..... QL10 180
C ..... QL10 190
C ..... QL10 200
C ..... QL10 210
C ..... QL10 220
C ..... QL10 230
C ..... QL10 240
C ..... QL10 250
C ..... QL10 260
C ..... QL10 270
C ..... QL10 280
C ..... QL10 290
C ..... QL10 300
C ..... QL10 310
C ..... QL10 320
C ..... QL10 330
C ..... QL10 340
C ..... QL10 350
C ..... QL10 360
C ..... QL10 370
C ..... QL10 380
C ..... QL10 390
C ..... QL10 400
C ..... QL10 410
C ..... QL10 420
C ..... QL10 430
C ..... QL10 440
C ..... QL10 450
C ..... QL10 460
C ..... QL10 470
C ..... QL10 480
C ..... QL10 490
C ..... QL10 500
C ..... QL10 510
C ..... QL10 520
C ..... QL10 530
C ..... QL10 540
C ..... QL10 550
C ..... QL10 560
C ..... QL10 570
C ..... QL10 580
C ..... QL10 590

```

SUBROUTINE QL10

PURPOSE
TO COMPUTE INTEGRAL($\text{EXP}(-X)\text{FCT}(X)$), SUMMED OVER X FROM 0 TO INFINITY).

USAGE
CALL QL10(FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT

DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
Y - THE RESULTING INTEGRAL VALUE.

REMARKS
NONE

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED BY THE USER.

METHOD
EVALUATION IS DONE BY MEANS OF 10-POINT GAUSSIAN-LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 19.
FOR REFERENCE, SEE
V.I. KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, MACMILLAN, NEW YORK/LONDON, 1962, PP.130-132 AND 347-352.

```

C ..... QL10 340
C ..... QL10 350
C ..... QL10 360
C ..... QL10 370
C ..... QL10 380
C ..... QL10 390
C ..... QL10 400
C ..... QL10 410
C ..... QL10 420
C ..... QL10 430
C ..... QL10 440
C ..... QL10 450
C ..... QL10 460
C ..... QL10 470
C ..... QL10 480
C ..... QL10 490
C ..... QL10 500
C ..... QL10 510
C ..... QL10 520
C ..... QL10 530
C ..... QL10 540
C ..... QL10 550
C ..... QL10 560
C ..... QL10 570
C ..... QL10 580
C ..... QL10 590

```

SUBROUTINE QL10(FCT,Y)

X=.29.92070
Y=.9911827E-12*FCT(X)
X=.21.99659
Y=Y+.1839565E-8*FCT(X)
X=.16.27926
Y=Y+.4249314E-6*FCT(X)
X=.11.84379
Y=Y+.2825923E-4*FCT(X)
X=.8.330153
Y=Y+.7530084E-3*FCT(X)
X=.5.552496
Y=Y+.009501517*FCT(X)
X=.3.401434
Y=Y+.06209746*FCT(X)
X=.1.808343
Y=Y+.2180683*FCT(X)
X=.7294545
Y=Y+.4011199*FCT(X)
X=.1377935
Y=Y+.3084411*FCT(X)
RETURN
END

```

C ..... DQ12 10
C ..... DQ12 20
C ..... DQ12 30
C ..... DQ12 40
C ..... DQ12 50
C ..... DQ12 60
C ..... DQ12 70
C ..... DQ12 80
C ..... DQ12 90
C ..... DQ12 100
C ..... DQ12 110
C ..... DQ12 120
C ..... DQ12 130
C ..... DQ12 140
C ..... DQ12 150
C ..... DQ12 160
C ..... DQ12 170
C ..... DQ12 180
C ..... DQ12 190
C ..... DQ12 200
C ..... DQ12 210
C ..... DQ12 220
C ..... DQ12 230
C ..... DQ12 240
C ..... DQ12 250
C ..... DQ12 260
C ..... DQ12 270
C ..... DQ12 280
C ..... DQ12 290
C ..... DQ12 300
C ..... DQ12 310
C ..... DQ12 320
C ..... DQ12 330
C ..... DQ12 340
C ..... DQ12 350
C ..... DQ12 360
C ..... DQ12 370
C ..... DQ12 380
C ..... DQ12 390
C ..... DQ12 400
C ..... DQ12 410
C ..... DQ12 420
C ..... DQ12 430
C ..... DQ12 440
C ..... DQ12 450
C ..... DQ12 460
C ..... DQ12 470
C ..... DQ12 480
C ..... DQ12 490
C ..... DQ12 500
C ..... DQ12 510
C ..... DQ12 520
C ..... DQ12 530
C ..... DQ12 540
C ..... DQ12 550
C ..... DQ12 560
C ..... DQ12 570
C ..... DQ12 580
C ..... DQ12 590
C ..... DQ12 600

```

SUBROUTINE DQ12

PURPOSE
TO COMPUTE INTEGRAL($\text{EXP}(-X)\text{FCT}(X)$), SUMMED OVER X FROM 0 TO INFINITY).

USAGE
CALL DQ12 (FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT

DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM USED.
Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.

REMARKS
NONE

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED BY THE USER.

METHOD
EVALUATION IS DONE BY MEANS OF 12-POINT GAUSSIAN-LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY, WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 23.
FOR REFERENCE, SEE
SHAU/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT TR00.1100 (MARCH 1964), PP.24-25.

```

C ..... DQ12 360
C ..... DQ12 370
C ..... DQ12 380
C ..... DQ12 390
C ..... DQ12 400
C ..... DQ12 410
C ..... DQ12 420
C ..... DQ12 430
C ..... DQ12 440
C ..... DQ12 450
C ..... DQ12 460
C ..... DQ12 470
C ..... DQ12 480
C ..... DQ12 490
C ..... DQ12 500
C ..... DQ12 510
C ..... DQ12 520
C ..... DQ12 530
C ..... DQ12 540
C ..... DQ12 550
C ..... DQ12 560
C ..... DQ12 570
C ..... DQ12 580
C ..... DQ12 590
C ..... DQ12 600

```

SUBROUTINE DQ12(FCT,Y)

DOUBLE PRECISION X,Y,FCT

X=.370991210446692002
Y=.81430774674262420-15*FCT(X)
X=.284879672509840002
Y=Y+.306160163503502080-11*FCT(X)
X=.2215109037939700602
Y=Y+.134239103051500410-8*FCT(X)
X=.1711685518746225602
Y=Y+.1166849387654091030-6*FCT(X)
X=.1300605499330634802
Y=Y+.83650558568197990-5*FCT(X)
X=.962131684245686701
Y=Y+.203231592662999390-3*FCT(X)
X=.6844525453115177301
Y=Y+.266397354186531590-2*FCT(X)
X=.4599227639418348501
Y=Y+.201023811546340970-1*FCT(X)
X=.2833751337743507201
Y=Y+.904492222211680930-1*FCT(X)
X=.1512610269776418801
Y=Y+.2440820113198775600*FCT(X)
X=.6117574845151306700
Y=Y+.3777592758731379800*FCT(X)
X=.1157221173580206800
Y=Y+.2647313710554431900*FCT(X)
RETURN
END

```

C ..... DQ16 10
C ..... DQ16 20
C ..... DQ16 30
C ..... DQ16 40
C ..... DQ16 50
C ..... DQ16 60
C ..... DQ16 70
C ..... DQ16 80
C ..... DQ16 90
C ..... DQ16 100
C ..... DQ16 110
C ..... DQ16 120
C ..... DQ16 130
C ..... DQ16 140
C ..... DQ16 150
C ..... DQ16 160
C ..... DQ16 170
C ..... DQ16 180
C ..... DQ16 190
C ..... DQ16 200
C ..... DQ16 210
C ..... DQ16 220
C ..... DQ16 230
C ..... DQ16 240
C ..... DQ16 250
C ..... DQ16 260
C ..... DQ16 270
C ..... DQ16 280
C ..... DQ16 290
C ..... DQ16 300
C ..... DQ16 310
C ..... DQ16 320
C ..... DQ16 330
C ..... DQ16 340
C ..... DQ16 350
C ..... DQ16 360
C ..... DQ16 370
C ..... DQ16 380
C ..... DQ16 390
C ..... DQ16 400
C ..... DQ16 410
C ..... DQ16 420
C ..... DQ16 430
C ..... DQ16 440
C ..... DQ16 450
C ..... DQ16 460
C ..... DQ16 470
C ..... DQ16 480
C ..... DQ16 490
C ..... DQ16 500
C ..... DQ16 510
C ..... DQ16 520
C ..... DQ16 530
C ..... DQ16 540
C ..... DQ16 550
C ..... DQ16 560
C ..... DQ16 570
C ..... DQ16 580
C ..... DQ16 590
C ..... DQ16 600

```

SUBROUTINE DQ16

PURPOSE
TO COMPUTE INTEGRAL($\text{EXP}(-X)\text{FCT}(X)$), SUMMED OVER X FROM 0 TO INFINITY).

USAGE
CALL DQ16 (FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT

DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM USED.
Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.

REMARKS
NONE

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED BY THE USER.

METHOD
EVALUATION IS DONE BY MEANS OF 16-POINT GAUSSIAN-LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY, WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 31.
FOR REFERENCE, SEE
SHAU/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT TR00.1100 (MARCH 1964), PP.24-25.

```

C ..... DQ16 360
C ..... DQ16 370
C ..... DQ16 380
C ..... DQ16 390
C ..... DQ16 400
C ..... DQ16 410
C ..... DQ16 420
C ..... DQ16 430
C ..... DQ16 440
C ..... DQ16 450
C ..... DQ16 460
C ..... DQ16 470
C ..... DQ16 480
C ..... DQ16 490
C ..... DQ16 500
C ..... DQ16 510
C ..... DQ16 520
C ..... DQ16 530
C ..... DQ16 540
C ..... DQ16 550
C ..... DQ16 560
C ..... DQ16 570
C ..... DQ16 580
C ..... DQ16 590
C ..... DQ16 600

```

SUBROUTINE DQ16(FCT,Y)

DOUBLE PRECISION X,Y,FCT

X=.5170116033954331802
Y=.41646237037285520-21*FCT(X)
X=.4194045264768833302
Y=Y+.505047370003551280-17*FCT(X)
X=.3458339870228662602
Y=Y+.62979670251786780-14*FCT(X)
X=.2857872974288214002
Y=Y+.21270790322410300-11*FCT(X)
X=.2351590569399190902
Y=Y+.286235024297388160-9*FCT(X)
X=.1918015685675313502
Y=Y+.188102484107967320-7*FCT(X)

```

X=-.1544152736878161 702
Y=Y+.68283193308119960-6*FCT(X)
X=.1221422336856615902
Y=Y+.148445868739812990-4*FCT(X)
X=.943831433639193901
Y=Y+.204271915308278660-3*FCT(X)
X=.7070338535048234101
Y=Y+.184907094352631090-2*FCT(X)
X=.5078018614549767801
Y=Y+.11299900803394530-1*FCT(X)
X=.3437086633893206601
Y=Y+.473289286941252190-1*FCT(X)
X=.21292836459880601
Y=Y+.1362769342963775400*FCT(X)
X=.1151057774931226901
Y=Y+.2657957776442141500*FCT(X)
X=.4626963289150808300
Y=Y+.3310578549508841700*FCT(X)
X=.87649410478927840-1
Y=Y+.2061517149578009900*FCT(X)
RETURN
END

```

C DL10 550 C
C DL16 560 C
C DL16 570 C
C DL16 580 C
C DL16 590 C
C DL16 600 C
C DL16 610 C
C DL16 620 C
C DL16 630 C
C DL16 640 C
C DL16 650 C
C DL16 660 C
C DL16 670 C
C DL16 680 C
C DL16 690 C
C DL16 700 C
C DL16 710 C
C DL16 720 C
C DL16 730 C
C DL16 740 C
C DL16 750 C
C DL16 760 C

```

C DL24 10 C  

C DL24 20 C  

C DL24 30 C  

C DL24 40 C  

C DL24 50 C  

C DL24 60 C  

C DL24 70 C  

C DL24 80 C  

C DL24 90 C  

C DL24 100 C  

C DL24 110 C  

C DL24 120 C  

C DL24 130 C  

C DL24 140 C  

C DL24 150 C  

C DL24 160 C  

C DL24 170 C  

C DL24 180 C  

C DL24 190 C  

C DL24 200 C  

C DL24 210 C  

C DL24 220 C  

C DL24 230 C  

C DL24 240 C  

C DL24 250 C  

C DL24 260 C  

C DL24 270 C  

C DL24 280 C  

C DL24 290 C  

C DL24 300 C  

C DL24 310 C  

C DL24 320 C  

C DL24 330 C  

C DL24 340 C  

C DL24 350 C  

C DL24 360 C  

C DL24 370 C  

C DL24 380 C  

C DL24 390 C  

C DL24 400 C  

C DL24 410 C  

C DL24 420 C  

C DL24 430 C  

C DL24 440 C  

C DL24 450 C  

C DL24 460 C  

C DL24 470 C  

C DL24 480 C  

C DL24 490 C  

C DL24 500 C  

C DL24 510 C  

C DL24 520 C  

C DL24 530 C  

C DL24 540 C  

C DL24 550 C  

C DL24 560 C  

C DL24 570 C  

C DL24 580 C  

C DL24 590 C  

C DL24 600 C  

C DL24 610 C  

C DL24 620 C  

C DL24 630 C  

C DL24 640 C  

C DL24 650 C  

C DL24 660 C  

C DL24 670 C  

C DL24 680 C  

C DL24 690 C  

C DL24 700 C  

C DL24 710 C  

C DL24 720 C  

C DL24 730 C  

C DL24 740 C  

C DL24 750 C  

C DL24 760 C  

C DL24 770 C  

C DL24 780 C  

C DL24 790 C  

C DL24 800 C  

C DL24 810 C  

C DL24 820 C  

C DL24 830 C  

C DL24 840 C  

C DL24 850 C  

C DL24 860 C  

C DL24 870 C  

C DL24 880 C  

C DL24 890 C  

C DL24 900 C  

C DL24 910 C  

C DL24 920 C

```

SUBROUTINE DQL24
PURPOSE
TO COMPUTE INTEGRAL(EXP(-X)*FCT(X), SUMMED OVER X
FROM 0 TO INFINITY).
USAGE
CALL DQL24 (FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION
SUBPROGRAM USED.
Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.
REMARKS
NONE
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)
MUST BE FURNISHED BY THE USER.
METHOD
EVALUATION IS DONE BY MEANS OF 24-POINT GAUSSIAN-LAGUERRE
QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY,
WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 47.
FOR REFERENCE, SEE
SHAD/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF
CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED
GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT
TR00.1100 (MARCH 1964), PP.24-25.

```

C DL32 10 C  

C DL32 20 C  

C DL32 30 C  

C DL32 40 C  

C DL32 50 C  

C DL32 60 C  

C DL32 70 C  

C DL32 80 C  

C DL32 90 C  

C DL32 100 C  

C DL32 110 C  

C DL32 120 C  

C DL32 130 C  

C DL32 140 C  

C DL32 150 C  

C DL32 160 C  

C DL32 170 C  

C DL32 180 C  

C DL32 190 C  

C DL32 200 C  

C DL32 210 C  

C DL32 220 C  

C DL32 230 C  

C DL32 240 C  

C DL32 250 C  

C DL32 260 C  

C DL32 270 C  

C DL32 280 C  

C DL32 290 C  

C DL32 300 C  

C DL32 310 C  

C DL32 320 C  

C DL32 330 C  

C DL32 340 C  

C DL32 350 C  

C DL32 360 C  

C DL32 370 C  

C DL32 380 C  

C DL32 390 C  

C DL32 400 C  

C DL32 410 C  

C DL32 420 C  

C DL32 430 C  

C DL32 440 C  

C DL32 450 C  

C DL32 460 C  

C DL32 470 C  

C DL32 480 C  

C DL32 490 C  

C DL32 500 C  

C DL32 510 C  

C DL32 520 C  

C DL32 530 C  

C DL32 540 C  

C DL32 550 C  

C DL32 560 C  

C DL32 570 C  

C DL32 580 C  

C DL32 590 C  

C DL32 600 C  

C DL32 610 C  

C DL32 620 C  

C DL32 630 C  

C DL32 640 C  

C DL32 650 C  

C DL32 660 C  

C DL32 670 C  

C DL32 680 C  

C DL32 690 C  

C DL32 700 C  

C DL32 710 C  

C DL32 720 C  

C DL32 730 C  

C DL32 740 C  

C DL32 750 C  

C DL32 760 C  

C DL32 770 C  

C DL32 780 C  

C DL32 790 C  

C DL32 800 C  

C DL32 810 C  

C DL32 820 C  

C DL32 830 C  

C DL32 840 C  

C DL32 850 C  

C DL32 860 C  

C DL32 870 C  

C DL32 880 C  

C DL32 890 C  

C DL32 900 C  

C DL32 910 C  

C DL32 920 C  

C DL32 930 C  

C DL32 940 C  

C DL32 950 C  

C DL32 960 C  

C DL32 970 C  

C DL32 980 C  

C DL32 990 C  

C DL32100 C  

C DL321010 C  

C DL321020 C  

C DL321030 C  

C DL321040 C  

C DL321050 C  

C DL321060 C  

C DL321070 C  

C DL321080 C

```

SUBROUTINE DQL32
PURPOSE
TO COMPUTE INTEGRAL(EXP(-X)*FCT(X), SUMMED OVER X
FROM 0 TO INFINITY).
USAGE
CALL DQL32 (FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION
SUBPROGRAM USED.
Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.
REMARKS
NONE
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)
MUST BE FURNISHED BY THE USER.
METHOD
EVALUATION IS DONE BY MEANS OF 32-POINT GAUSSIAN-LAGUERRE
QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY,
WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 63.
FOR REFERENCE, SEE
SHAD/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF
CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED
GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT
TR00.1100 (MARCH 1964), PP.24-25.

```

C DL32 10 C  

C DL32 20 C  

C DL32 30 C  

C DL32 40 C  

C DL32 50 C  

C DL32 60 C  

C DL32 70 C  

C DL32 80 C  

C DL32 90 C  

C DL32 100 C  

C DL32 110 C  

C DL32 120 C  

C DL32 130 C  

C DL32 140 C  

C DL32 150 C  

C DL32 160 C  

C DL32 170 C  

C DL32 180 C  

C DL32 190 C  

C DL32 200 C  

C DL32 210 C  

C DL32 220 C  

C DL32 230 C  

C DL32 240 C  

C DL32 250 C  

C DL32 260 C  

C DL32 270 C  

C DL32 280 C  

C DL32 290 C  

C DL32 300 C  

C DL32 310 C  

C DL32 320 C  

C DL32 330 C  

C DL32 340 C  

C DL32 350 C  

C DL32 360 C  

C DL32 370 C  

C DL32 380 C  

C DL32 390 C  

C DL32 400 C  

C DL32 410 C  

C DL32 420 C  

C DL32 430 C  

C DL32 440 C  

C DL32 450 C  

C DL32 460 C  

C DL32 470 C  

C DL32 480 C  

C DL32 490 C  

C DL32 500 C  

C DL32 510 C  

C DL32 520 C  

C DL32 530 C  

C DL32 540 C  

C DL32 550 C  

C DL32 560 C  

C DL32 570 C  

C DL32 580 C  

C DL32 590 C  

C DL32 600 C  

C DL32 610 C  

C DL32 620 C  

C DL32 630 C  

C DL32 640 C  

C DL32 650 C  

C DL32 660 C  

C DL32 670 C  

C DL32 680 C  

C DL32 690 C  

C DL32 700 C  

C DL32 710 C  

C DL32 720 C  

C DL32 730 C  

C DL32 740 C  

C DL32 750 C  

C DL32 760 C  

C DL32 770 C  

C DL32 780 C  

C DL32 790 C  

C DL32 800 C  

C DL32 810 C  

C DL32 820 C  

C DL32 830 C  

C DL32 840 C  

C DL32 850 C  

C DL32 860 C  

C DL32 870 C  

C DL32 880 C  

C DL32 890 C  

C DL32 900 C  

C DL32 910 C  

C DL32 920 C  

C DL32 930 C  

C DL32 940 C  

C DL32 950 C  

C DL32 960 C  

C DL32 970 C  

C DL32 980 C  

C DL32 990 C  

C DL32100 C  

C DL321010 C  

C DL321020 C  

C DL321030 C  

C DL321040 C  

C DL321050 C  

C DL321060 C  

C DL321070 C  

C DL321080 C

```

SUBROUTINE DQL32(FCT,Y)
DOUBLE PRECISION X,Y,FCT
X=.1117513980979377003
X=.988295428682839702
Y=Y+.13861694210625630-4*(FCT(X)
X=.887353404178924002
Y=Y+.26715121924013700-37*FCT(X)
X=.801874669779135202
Y=Y+.119224876009822240-33*FCT(X)
X=.726876290006627102
Y=Y+.49133754944522430-30*FCT(X)
X=.6597537728793505302
Y=Y+.141856054546303690-27*FCT(X)
X=.5989250916213601802
Y=Y+.566129413039735990-25*FCT(X)
X=.5433372133336690702
Y=Y+.134698253663739520-22*FCT(X)
X=.4922439498730863902
Y=Y+.205442967378804540-20*FCT(X)
X=.445092799575493802
Y=Y+.21197229016361860-18*FCT(X)
X=.4014571977153944202
Y=Y+.15421338339382340-16*FCT(X)
X=.3610049480575197402
Y=Y+.81718234434207190-15*FCT(X)
X=.3234662915396473702
Y=Y+.323780165772926650-13*FCT(X)
X=.2886210181632347502
Y=Y+.9199379288727040-12*FCT(X)
X=.2562863602245924802
Y=Y+.230589949189133610-10*FCT(X)
X=.2263088901319677402
Y=Y+.428138297104092890-9*FCT(X)
X=.198558609403360502
Y=Y+.63506222662580670-8*FCT(X)
X=.1729245433671531502
Y=Y+.76045678791207410-7*FCT(X)
X=.149311397552255702
Y=Y+.74164045786675520-6*FCT(X)
X=.127636979867427502
Y=Y+.593454161286863290-5*FCT(X)
X=.1078301863253997202
Y=Y+.39203419679874720-4*FCT(X)
X=.898294092421259601
Y=Y+.214864918801364190-3*FCT(X)
X=.735812673318624101
Y=Y+.9808030661495510-3*FCT(X)
X=.590395850417424301
Y=Y+.373881629461152480-2*FCT(X)
X=.4616456769749767401
Y=Y+.119182148348385570-1*FCT(X)
X=.3492213273021994501
Y=Y+.317609125091750700-1*FCT(X)
X=.2528336706425794901
Y=Y+.705786238657174420-1*FCT(X)
X=.172408877644445401
Y=Y+.1299837862860717600*FCT(X)
X=.1072448753817817601
Y=Y+.1959033359728810400*FCT(X)
X=.5768846293018864300
Y=Y+.23521322966984800*FCT(X)
X=.2345261095196185400
Y=Y+.2106431079388132300*FCT(X)
X=.44489365832670180-1
Y=Y+.1092183419523849700*FCT(X)
RETURN
END


```

C          QM4 10
C          .....QM4 20
C          SUBROUTINE QM4          QM4 30
C          QM4 40
C          PURPOSE          QM4 50
C          TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM QM4 60
C          -INFINITY TO +INFINITY). QM4 70
C          QM4 80
C          USAGE          QM4 90
C          CALL QM4 (FCT,Y) QM4 100
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT QM4 110
C          QM4 120
C          DESCRIPTION OF PARAMETERS QM4 130
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED. QM4 140
C          Y - THE RESULTING INTEGRAL VALUE. QM4 150
C          QM4 160
C          REMARKS QM4 170
C          NONE QM4 180
C          QM4 190
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED QM4 200
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED QM4 210
C          BY THE USER. QM4 220
C          QM4 230
C          METHOD QM4 240
C          EVALUATION IS DONE BY MEANS OF 4-POINT GAUSSIAN-HERMITE QM4 250
C          QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER QM4 260
C          FCT(X) IS A POLYNOMIAL UP TO DEGREE 7. QM4 270
C          FOR REFERENCE, SEE QM4 280
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, QM4 290
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.129-130 AND 343-346. QM4 300
C          QM4 310
C          .....QM4 320
C          SUBROUTINE QM4(FCT,Y) QM4 330
C          QM4 340
C          QM4 350
C          QM4 360
C          QM4 370
C          QM4 380
C          QM4 390
C          QM4 400
C          QM4 410
C          QM4 420
C          QM4 430
C          QM4 440
C          QM4 450
C
X=1.650680
Z=-X
Y=-.08131284*(FCT(X)+FCT(Z))
X=-.5246476
Z=-X
Y=Y+.8049141*(FCT(X)+FCT(Z))
RETURN
END

```

```

C          QM6 10
C          .....QM6 20
C          SUBROUTINE QM6          QM6 30
C          QM6 40
C          PURPOSE          QM6 50
C          TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM QM6 60
C          -INFINITY TO +INFINITY). QM6 70
C          QM6 80
C          USAGE          QM6 90
C          CALL QM6 (FCT,Y) QM6 100
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT QM6 110
C          QM6 120
C          DESCRIPTION OF PARAMETERS QM6 130
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED. QM6 140
C          Y - THE RESULTING INTEGRAL VALUE. QM6 150
C          QM6 160
C          REMARKS QM6 170
C          NONE QM6 180
C          QM6 190
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED QM6 200
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED QM6 210
C          BY THE USER. QM6 220
C          QM6 230
C          METHOD QM6 240
C          EVALUATION IS DONE BY MEANS OF 6-POINT GAUSSIAN-HERMITE QM6 250
C          QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER QM6 260
C          FCT(X) IS A POLYNOMIAL UP TO DEGREE 11. QM6 270
C          FOR REFERENCE, SEE QM6 280
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, QM6 290
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.129-130 AND 343-346. QM6 300
C          QM6 310
C          .....QM6 320
C          SUBROUTINE QM6(FCT,Y) QM6 330
C          QM6 340
C          QM6 350
C          QM6 360
C          QM6 370
C          QM6 380
C          QM6 390
C          QM6 400
C          QM6 410
C          QM6 420
C          QM6 430
C          QM6 440
C          QM6 450
C          QM6 460
C          QM6 470
C          QM6 480
C
X=2.390605
Z=-X
Y=-.004530010*(FCT(X)+FCT(Z))
X=1.335849
Z=-X
Y=Y+.1570673*(FCT(X)+FCT(Z))
X=-.6360774
Z=-X
Y=Y+.7246296*(FCT(X)+FCT(Z))
RETURN
END

```

```

C          QM5 10
C          .....QM5 20
C          SUBROUTINE QM5          QM5 30
C          QM5 40
C          PURPOSE          QM5 50
C          TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM QM5 60
C          -INFINITY TO +INFINITY). QM5 70
C          QM5 80
C          USAGE          QM5 90
C          CALL QM5 (FCT,Y) QM5 100
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT QM5 110
C          QM5 120
C          DESCRIPTION OF PARAMETERS QM5 130
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED. QM5 140
C          Y - THE RESULTING INTEGRAL VALUE. QM5 150
C          QM5 160
C          REMARKS QM5 170
C          NONE QM5 180
C          QM5 190
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED QM5 200
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED QM5 210
C          BY THE USER. QM5 220
C          QM5 230
C          METHOD QM5 240
C          EVALUATION IS DONE BY MEANS OF 5-POINT GAUSSIAN-HERMITE QM5 250
C          QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER QM5 260
C          FCT(X) IS A POLYNOMIAL UP TO DEGREE 9. QM5 270
C          FOR REFERENCE, SEE QM5 280
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, QM5 290
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.129-130 AND 343-346. QM5 300
C          QM5 310
C          .....QM5 320
C          SUBROUTINE QM5(FCT,Y) QM5 330
C          QM5 340
C          QM5 350
C          QM5 360
C          QM5 370
C          QM5 380
C          QM5 390
C          QM5 400
C          QM5 410
C          QM5 420
C          QM5 430
C          QM5 440
C          QM5 450
C          QM5 460
C          QM5 470
C
X=2.020103
Z=-X
Y=-.01995324*(FCT(X)+FCT(Z))
X=-.9585725
Z=-X
Y=Y+.3936193*(FCT(X)+FCT(Z))
X=0.
Y=Y+.9453087*(FCT(X))
RETURN
END

```

```

C          QM7 10
C          .....QM7 20
C          SUBROUTINE QM7          QM7 30
C          QM7 40
C          PURPOSE          QM7 50
C          TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM QM7 60
C          -INFINITY TO +INFINITY). QM7 70
C          QM7 80
C          USAGE          QM7 90
C          CALL QM7 (FCT,Y) QM7 100
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT QM7 110
C          QM7 120
C          DESCRIPTION OF PARAMETERS QM7 130
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED. QM7 140
C          Y - THE RESULTING INTEGRAL VALUE. QM7 150
C          QM7 160
C          REMARKS QM7 170
C          NONE QM7 180
C          QM7 190
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED QM7 200
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED QM7 210
C          BY THE USER. QM7 220
C          QM7 230
C          METHOD QM7 240
C          EVALUATION IS DONE BY MEANS OF 7-POINT GAUSSIAN-HERMITE QM7 250
C          QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER QM7 260
C          FCT(X) IS A POLYNOMIAL UP TO DEGREE 13. QM7 270
C          FOR REFERENCE, SEE QM7 280
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS, QM7 290
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.129-130 AND 343-346. QM7 300
C          QM7 310
C          .....QM7 320
C          SUBROUTINE QM7(FCT,Y) QM7 330
C          QM7 340
C          QM7 350
C          QM7 360
C          QM7 370
C          QM7 380
C          QM7 390
C          QM7 400
C          QM7 410
C          QM7 420
C          QM7 430
C          QM7 440
C          QM7 450
C          QM7 460
C          QM7 470
C          QM7 480
C          QM7 490
C          QM7 500
C
X=2.651961
Z=-X
Y=-.0009717812*(FCT(X)+FCT(Z))
X=1.673552
Z=-X
Y=Y+.05451558*(FCT(X)+FCT(Z))
X=-.8162879
Z=-X
Y=Y+-.4256073*(FCT(X)+FCT(Z))
X=0.
Y=Y+.8102646*(FCT(X))
RETURN
END

```

```

C          QH8 10
C          .....
C          QH8 20
C          QH8 30
C          SUBROUTINE QH8
C          QH8 40
C          QH8 50
C          PURPOSE
C          QH8 60
C          TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM
C          QH8 70
C          -INFINITY TO +INFINITY).
C          QH8 80
C          QH8 90
C          USAGE
C          QH8 100
C          CALL QH8 (FCT,Y)
C          QH8 110
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C          QH8 120
C          QH8 130
C          DESCRIPTION OF PARAMETERS
C          QH8 140
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
C          QH8 150
C          Y - THE RESULTING INTEGRAL VALUE.
C          QH8 160
C          QH8 170
C          REMARKS
C          QH8 180
C          NONE
C          QH8 190
C          QH8 200
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          QH8 210
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
C          QH8 220
C          BY THE USER.
C          QH8 230
C          QH8 240
C          METHOD
C          QH8 250
C          EVALUATION IS DONE BY MEANS OF 8-POINT GAUSSIAN-HERMITE
C          QH8 260
C          QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER
C          QH8 270
C          FCT(X) IS A POLYNOMIAL UP TO DEGREE 15.
C          QH8 280
C          FOR REFERENCE, SEE
C          QH8 290
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,
C          QH8 300
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.129-130 AND 343-346.
C          QH8 310
C          QH8 320
C          QH8 330
C          .....
C          QH8 340
C          SUBROUTINE QH8(FCT,Y)
C          QH8 350
C          QH8 360
C          QH8 370
C          QH8 380
C          Z=-X
C          QH8 390
C          Y=-.001996041*(FCT(X)+FCT(Z))
C          QH8 400
C          X=1.981657
C          QH8 410
C          Z=-X
C          QH8 420
C          Y=Y+.01707798*(FCT(X)+FCT(Z))
C          QH8 430
C          X=1.157194
C          QH8 440
C          Z=-X
C          QH8 450
C          Y=Y+.2078023*(FCT(X)+FCT(Z))
C          QH8 460
C          X=.3811870
C          QH8 470
C          Z=-X
C          QH8 480
C          Y=Y+.6611470*(FCT(X)+FCT(Z))
C          QH8 490
C          RETURN
C          QH8 500
C          END
C          QH8 510

```

```

C          QH9 10
C          .....
C          QH9 20
C          QH9 30
C          SUBROUTINE QH9
C          QH9 40
C          QH9 50
C          PURPOSE
C          QH9 60
C          TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM
C          QH9 70
C          -INFINITY TO +INFINITY).
C          QH9 80
C          QH9 90
C          USAGE
C          QH9 100
C          CALL QH9 (FCT,Y)
C          QH9 110
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C          QH9 120
C          QH9 130
C          DESCRIPTION OF PARAMETERS
C          QH9 140
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
C          QH9 150
C          Y - THE RESULTING INTEGRAL VALUE.
C          QH9 160
C          QH9 170
C          REMARKS
C          QH9 180
C          NONE
C          QH9 190
C          QH9 200
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          QH9 210
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
C          QH9 220
C          BY THE USER.
C          QH9 230
C          QH9 240
C          METHOD
C          QH9 250
C          EVALUATION IS DONE BY MEANS OF 9-POINT GAUSSIAN-HERMITE
C          QH9 260
C          QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER
C          QH9 270
C          FCT(X) IS A POLYNOMIAL UP TO DEGREE 17.
C          QH9 280
C          FOR REFERENCE, SEE
C          QH9 290
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,
C          QH9 300
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.129-130 AND 343-346.
C          QH9 310
C          QH9 320
C          QH9 330
C          .....
C          QH9 340
C          SUBROUTINE QH9(FCT,Y)
C          QH9 350
C          QH9 360
C          QH9 370
C          X=3.190993
C          QH9 380
C          Z=-X
C          QH9 390
C          Y=.3960698E-4*(FCT(X)+FCT(Z))
C          QH9 400
C          X=2.266581
C          QH9 410
C          Z=-X
C          QH9 420
C          Y=Y+.004943624*(FCT(X)+FCT(Z))
C          QH9 430
C          X=1.468553
C          QH9 440
C          Z=-X
C          QH9 450
C          Y=Y+.08847453*(FCT(X)+FCT(Z))
C          QH9 460
C          X=.7235510
C          QH9 470
C          Z=-X
C          QH9 480
C          Y=Y+.4326516*(FCT(X)+FCT(Z))
C          QH9 490
C          X=0.
C          QH9 500
C          Y=Y+.7202352*(FCT(X))
C          QH9 510
C          RETURN
C          QH9 520
C          END
C          QH9 530

```

```

C          DQH8 10
C          .....
C          DQH8 20
C          DQH8 30
C          SUBROUTINE DQH8
C          DQH8 40
C          DQH8 50
C          PURPOSE
C          DQH8 60
C          TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM
C          DQH8 70
C          -INFINITY TO +INFINITY).
C          DQH8 80
C          DQH8 90
C          USAGE
C          DQH8 100
C          CALL DQH8 (FCT,Y)
C          DQH8 110
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C          DQH8 120
C          DQH8 130
C          DESCRIPTION OF PARAMETERS
C          DQH8 140
C          FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION
C          DQH8 150
C          SUBPROGRAM USED.
C          DQH8 160
C          Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.
C          DQH8 170
C          DQH8 180
C          REMARKS
C          DQH8 190
C          NONE
C          DQH8 200
C          DQH8 210
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          DQH8 220
C          THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)
C          DQH8 230
C          MUST BE FURNISHED BY THE USER.
C          DQH8 240
C          DQH8 250
C          METHOD
C          DQH8 260
C          EVALUATION IS DONE BY MEANS OF 8-POINT GAUSSIAN-HERMITE
C          DQH8 270
C          QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER
C          DQH8 280
C          FCT(X) IS A POLYNOMIAL UP TO DEGREE 15.
C          DQH8 290
C          FOR REFERENCE, SEE
C          DQH8 300
C          SHAO/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF
C          DQH8 310
C          CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED
C          DQH8 320
C          GENERALIZED HERMITE POLYNOMIALS; IBM TECHNICAL REPORT
C          DQH8 330
C          TR00.1100 (MARCH 1964), PP.213-214.
C          DQH8 340
C          .....
C          DQH8 350
C          SUBROUTINE DQH8(FCT,Y)
C          DQH8 360
C          DQH8 370
C          DQH8 380
C          DOUBLE PRECISION X,Y,Z,FCT
C          DQH8 390
C          X=.2930637420257244001
C          DQH8 400
C          Z=-X
C          DQH8 410
C          Y=-.19960407221136762D-3*(FCT(X)+FCT(Z))
C          DQH8 420
C          X=.1981656756695842901
C          DQH8 430
C          Z=-X
C          DQH8 440
C          Y=Y+.17077983007413475D-1*(FCT(X)+FCT(Z))
C          DQH8 450
C          X=.1157193712446780201
C          DQH8 460
C          Z=-X
C          DQH8 470
C          Y=Y+.20780232581489188D0*(FCT(X)+FCT(Z))
C          DQH8 480
C          X=.3811869902073221200
C          DQH8 490
C          Z=-X
C          DQH8 500
C          Y=Y+.66114701255824290D0*(FCT(X)+FCT(Z))
C          DQH8 510
C          RETURN
C          DQH8 520
C          END
C          DQH8 530
C          DQH8 540
C          DQH8 550
C          DQH8 560

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```

C          QH10 10
C          .....
C          QH10 20
C          QH10 30
C          SUBROUTINE QH10
C          QH10 40
C          QH10 50
C          PURPOSE
C          QH10 60
C          TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM
C          QH10 70
C          -INFINITY TO +INFINITY).
C          QH10 80
C          QH10 90
C          USAGE
C          QH10 100
C          CALL QH10(FCT,Y)
C          QH10 110
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C          QH10 120
C          QH10 130
C          DESCRIPTION OF PARAMETERS
C          QH10 140
C          FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
C          QH10 150
C          Y - THE RESULTING INTEGRAL VALUE.
C          QH10 160
C          QH10 170
C          REMARKS
C          QH10 180
C          NONE
C          QH10 190
C          QH10 200
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          QH10 210
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
C          QH10 220
C          BY THE USER.
C          QH10 230
C          QH10 240
C          METHOD
C          QH10 250
C          EVALUATION IS DONE BY MEANS OF 10-POINT GAUSSIAN-HERMITE
C          QH10 260
C          QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER
C          QH10 270
C          FCT(X) IS A POLYNOMIAL UP TO DEGREE 19.
C          QH10 280
C          FOR REFERENCE, SEE
C          QH10 290
C          V.I.KRYLOV, APPROXIMATE CALCULATION OF INTEGRALS,
C          QH10 300
C          MACMILLAN, NEW YORK/LONDON, 1962, PP.129-130 AND 343-346.
C          QH10 310
C          QH10 320
C          .....
C          QH10 330
C          SUBROUTINE QH10(FCT,Y)
C          QH10 340
C          QH10 350
C          QH10 360
C          X=3.436159
C          QH10 370
C          Z=-X
C          QH10 380
C          Y=-.7640433E-5*(FCT(X)+FCT(Z))
C          QH10 390
C          X=2.532732
C          QH10 400
C          Z=-X
C          QH10 410
C          Y=Y+.001343646*(FCT(X)+FCT(Z))
C          QH10 420
C          X=1.756684
C          QH10 430
C          Z=-X
C          QH10 440
C          Y=Y+.03387439*(FCT(X)+FCT(Z))
C          QH10 450
C          X=1.036611
C          QH10 460
C          Z=-X
C          QH10 470
C          Y=Y+.2401386*(FCT(X)+FCT(Z))
C          QH10 480
C          X=.3429013
C          QH10 490
C          Z=-X
C          QH10 500
C          Y=Y+.6108626*(FCT(X)+FCT(Z))
C          QH10 510
C          RETURN
C          QH10 520
C          END
C          QH10 530
C          QH10 540

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```

C                                     DH16 10
C .....
C SUBROUTINE DQH16                    DH16 20
C                                     DH16 30
C                                     DH16 40
C PURPOSE                              DH16 50
C TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM DH16 60
C -INFINITY TO +INFINITY).           DH16 70
C                                     DH16 80
C USAGE                                DH16 90
C CALL DQH16 (FCT,Y)                 DH16 100
C PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT DH16 110
C                                     DH16 120
C DESCRIPTION OF PARAMETERS           DH16 130
C FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION DH16 140
C SUBPROGRAM USED.                   DH16 150
C Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.       DH16 160
C                                     DH16 170
C REMARKS                              DH16 180
C NONE                                DH16 190
C                                     DH16 200
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DH16 210
C THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) DH16 220
C MUST BE FURNISHED BY THE USER.     DH16 230
C                                     DH16 240
C METHOD                                DH16 250
C EVALUATION IS DONE BY MEANS OF 16-POINT GAUSSIAN-HERMITE DH16 260
C QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER DH16 270
C FCT(X) IS A POLYNOMIAL UP TO DEGREE 31. DH16 280
C FOR REFERENCE, SEE                  DH16 290
C SHAD/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF DH16 300
C CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED DH16 310
C GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT DH16 320
C TROO.1100 (MARCH 1964), PP.213-214. DH16 330
C                                     DH16 340
C .....
C SUBROUTINE DQH16(FCT,Y)             DH16 350
C                                     DH16 360
C DOUBLE PRECISION X,Y,Z,FCT          DH16 370
C                                     DH16 380
C X=.4688738939305818401             DH16 390
C Z=-X                                DH16 400
C Y=.265480747401118220-9*(FCT(X)+FCT(Z)) DH16 410
C X=.3869447904860122701             DH16 420
C Z=-X                                DH16 430
C Y=Y+.232098084486521070-6*(FCT(X)+FCT(Z)) DH16 440
C X=.3176999161979956001             DH16 450
C Z=-X                                DH16 460
C Y=Y+.271186009253788150-4*(FCT(X)+FCT(Z)) DH16 470
C X=.2546202157847481401             DH16 480
C Z=-X                                DH16 490
C Y=Y+.93228400862418050-3*(FCT(X)+FCT(Z)) DH16 500
C X=.1951787990916254001             DH16 510
C Z=-X                                DH16 520
C Y=Y+.128803115355099740-1*(FCT(X)+FCT(Z)) DH16 530
C X=.1380258539198880801             DH16 540
C Z=-X                                DH16 550
C Y=Y+.83810041398985830-1*(FCT(X)+FCT(Z)) DH16 560
C X=.822951449144655900              DH16 570
C Z=-X                                DH16 580
C Y=Y+.2806474585285336800*(FCT(X)+FCT(Z)) DH16 590
C X=.2734810461381524500             DH16 600
C Z=-X                                DH16 610
C Y=Y+.5079294790166137400*(FCT(X)+FCT(Z)) DH16 620
C RETURN                              DH16 630
C END                                  DH16 640

```

```

C                                     DH24 10
C .....
C SUBROUTINE DQM24                    DH24 20
C                                     DH24 30
C PURPOSE                              DH24 40
C TO COMPUTE INTEGRAL(EXP(-X*X)*FCT(X), SUMMED OVER X FROM DH24 50
C -INFINITY TO +INFINITY).           DH24 60
C                                     DH24 70
C USAGE                                DH24 80
C CALL DQM24 (FCT,Y)                 DH24 90
C PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT DH24 100
C                                     DH24 110
C DESCRIPTION OF PARAMETERS           DH24 120
C FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION DH24 130
C SUBPROGRAM USED.                   DH24 140
C Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.       DH24 150
C                                     DH24 160
C REMARKS                              DH24 170
C NONE                                DH24 180
C                                     DH24 190
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DH24 200
C THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) DH24 210
C MUST BE FURNISHED BY THE USER.     DH24 220
C                                     DH24 230
C METHOD                                DH24 240
C EVALUATION IS DONE BY MEANS OF 24-POINT GAUSSIAN-HERMITE DH24 250
C QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER DH24 260
C FCT(X) IS A POLYNOMIAL UP TO DEGREE 47. DH24 270
C FOR REFERENCE, SEE                  DH24 280
C SHAD/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF DH24 290
C CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED DH24 300
C GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT DH24 310
C TROO.1100 (MARCH 1964), PP.213-214. DH24 320
C                                     DH24 330
C .....
C SUBROUTINE DQM24(FCT,Y)             DH24 340
C                                     DH24 350
C DOUBLE PRECISION X,Y,Z,FCT          DH24 360
C                                     DH24 370
C X=.6015925561425739701             DH24 380
C Z=-X                                DH24 390
C Y=.166436849648910890-15*(FCT(X)+FCT(Z)) DH24 400
C X=.5259382927668044401             DH24 410
C Z=-X                                DH24 420
C Y=Y+.658462024307817010-12*(FCT(X)+FCT(Z)) DH24 430
C X=.4625662756423787301             DH24 440
C Z=-X                                DH24 450
C Y=Y+.304625426998756390-9*(FCT(X)+FCT(Z)) DH24 460
C X=.4053664402448149501             DH24 470
C Z=-X                                DH24 480
C Y=Y+.40189711749142970-7*(FCT(X)+FCT(Z)) DH24 490
C X=.3520006813034524701             DH24 500
C Z=-X                                DH24 510
C Y=Y+.215824570490233340-5*(FCT(X)+FCT(Z)) DH24 520
C X=.3012546137565564801             DH24 530
C Z=-X                                DH24 540
C Y=Y+.568869163640437980-4*(FCT(X)+FCT(Z)) DH24 550
C X=.2523881017011427001             DH24 560
C Z=-X                                DH24 570
C Y=Y+.82349248268841750-3*(FCT(X)+FCT(Z)) DH24 580
C X=.2049003573661698901             DH24 590
C Z=-X                                DH24 600
C Y=Y+.704835581007267100-2*(FCT(X)+FCT(Z)) DH24 610
C X=.1584250010961694101             DH24 620
C Z=-X                                DH24 630
C Y=Y+.374456705032307460-1*(FCT(X)+FCT(Z)) DH24 640
C X=.1126760817611245101             DH24 650
C Z=-X                                DH24 660
C Y=Y+.1277396217845591600*(FCT(X)+FCT(Z)) DH24 670
C X=.6741711070372122400             DH24 680
C Z=-X                                DH24 690
C Y=Y+.2861795353464430200*(FCT(X)+FCT(Z)) DH24 700
C X=.2244145474725155900             DH24 710
C Z=-X                                DH24 720
C Y=Y+.4269311638686992500*(FCT(X)+FCT(Z)) DH24 730
C RETURN                              DH24 740
C END                                  DH24 750

```


C		DH64 10	Y=+.1084983493061868400*(FCT(X)+FCT(Z))	DH641300
C	DH64 20	X=-.6919223058100445800	DH641300
C		DH64 30	Z=-X	DH641310
C	SUBROUTINE DQH64	DH64 40	Y=+.4149888241210786800*(FCT(X)+FCT(Z))	DH641320
C	PURPOSE	DH64 50	X=-.4149888241210786800	DH641330
C	TO COMPUTE INTEGRAL(EXP(-X**2))*FCT(X), SUMMED OVER X FROM	DH64 60	Z=-X	DH641340
C	-INFINITY TO +INFINITY).	DH64 70	Y=+.2329947860626780500*(FCT(X)+FCT(Z))	DH641350
C		DH64 80	X=.1383022449870097200	DH641360
C	USAGE	DH64 90	Z=-X	DH641370
C	CALL DQH64 (FCT,Y)	DH64 100	Y=+.2713774249413039800*(FCT(X)+FCT(Z))	DH641380
C	PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT	DH64 110	RETURN	DH641390
C		DH64 120	END	DH641400
C	DESCRIPTION OF PARAMETERS	DH64 130		
C	FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION	DH64 140		
C	SUBPROGRAM USED.	DH64 150		
C	Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.	DH64 160		
C	REMARKS	DH64 170		
C	NONE	DH64 180		
C		DH64 190		
C		DH64 200		
C		DH64 210		
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	DH64 220		
C	THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)	DH64 230		
C	MUST BE FURNISHED BY THE USER.	DH64 240		
C		DH64 250		
C	METHOD	DH64 260		
C	EVALUATION IS DONE BY MEANS OF 64-POINT GAUSSIAN-HERMITE	DH64 270		
C	QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY WHENEVER	DH64 280		
C	FCT(X) IS A POLYNOMIAL UP TO DEGREE 127.	DH64 290		
C	FOR REFERENCE, SEE	DH64 300		
C	SHAO/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF	DH64 310		
C	CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED	DH64 320		
C	GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT	DH64 330		
C	TROO.1100 (MARCH 1964), PP.213-214.	DH64 340		
C		DH64 350		
C	DH64 360		
C	SUBROUTINE DQH64(FCT,Y)	DH64 370		
C		DH64 380		
C		DH64 390		
C	DOUBLE PRECISION X,Y,Z,FCT	DH64 400		
C		DH64 410		
C		DH64 420		
C		DH64 430		
C	X=-.1052612316796054602	DH64 440		
C	Z=-X	DH64 450		
C	Y=.553570653585694280-48*(FCT(X)+FCT(Z))	DH64 460		
C	X=.989528758682953901	DH64 470		
C	Z=-X	DH64 480		
C	Y=+.167974799010815920-42*(FCT(X)+FCT(Z))	DH64 490		
C	X=.937315954964672101	DH64 500		
C	Z=-X	DH64 510		
C	Y=+.342113801125574050-38*(FCT(X)+FCT(Z))	DH64 520		
C	X=.890724909996477001	DH64 530		
C	Z=-X	DH64 540		
C	Y=+.155739062462976380-34*(FCT(X)+FCT(Z))	DH64 550		
C	X=.847752908337986301	DH64 560		
C	Z=-X	DH64 570		
C	Y=+.254966089911299930-31*(FCT(X)+FCT(Z))	DH64 580		
C	X=.807368728501022501	DH64 590		
C	Z=-X	DH64 600		
C	Y=+.192910359546496690-28*(FCT(X)+FCT(Z))	DH64 610		
C	X=.788954016404069701	DH64 620		
C	Z=-X	DH64 630		
C	Y=+.78617977889259100-26*(FCT(X)+FCT(Z))	DH64 640		
C	X=.732101303278094901	DH64 650		
C	Z=-X	DH64 660		
C	Y=+.191170688330064280-23*(FCT(X)+FCT(Z))	DH64 670		
C	X=.6965241120551107501	DH64 680		
C	Z=-X	DH64 690		
C	Y=+.298286278427985120-21*(FCT(X)+FCT(Z))	DH64 700		
C	X=.6620112262636027401	DH64 710		
C	Z=-X	DH64 720		
C	Y=+.315225456650378140-19*(FCT(X)+FCT(Z))	DH64 730		
C	X=.6284011228774828201	DH64 740		
C	Z=-X	DH64 750		
C	Y=+.235188471067581910-17*(FCT(X)+FCT(Z))	DH64 760		
C	X=.5955666326799486001	DH64 770		
C	Z=-X	DH64 780		
C	Y=+.128009339132243800-15*(FCT(X)+FCT(Z))	DH64 790		
C	X=.5634052164349972101	DH64 800		
C	Z=-X	DH64 810		
C	Y=+.521862372659084750-14*(FCT(X)+FCT(Z))	DH64 820		
C	X=.5318325224633270901	DH64 830		
C	Z=-X	DH64 840		
C	Y=+.162834073070972040-12*(FCT(X)+FCT(Z))	DH64 850		
C	X=.5007779602198768201	DH64 860		
C	Z=-X	DH64 870		
C	Y=+.3959177769672390-11*(FCT(X)+FCT(Z))	DH64 880		
C	X=.4701815647407499801	DH64 890		
C	Z=-X	DH64 900		
C	Y=+.76152172501454510-10*(FCT(X)+FCT(Z))	DH64 910		
C	X=.4399917168228137601	DH64 920		
C	Z=-X	DH64 930		
C	Y=+.117361674232154930-8*(FCT(X)+FCT(Z))	DH64 940		
C	X=.401634474566656701	DH64 950		
C	Z=-X	DH64 960		
C	Y=+.146512531647610940-7*(FCT(X)+FCT(Z))	DH64 970		
C	X=.3806571513945360501	DH64 980		
C	Z=-X	DH64 990		
C	Y=+.149553293672724710-6*(FCT(X)+FCT(Z))	DH641000		
C	X=.3514375935740906201	DH641010		
C	Z=-X	DH641020		
C	Y=+.125834025103118460-5*(FCT(X)+FCT(Z))	DH641030		
C	X=.3224731291992035701	DH641040		
C	Z=-X	DH641050		
C	Y=+.87884992308503590-5*(FCT(X)+FCT(Z))	DH641060		
C	X=.2937350823004621801	DH641070		
C	Z=-X	DH641080		
C	Y=+.512592913578627470-4*(FCT(X)+FCT(Z))	DH641090		
C	X=.2651972435430635001	DH641100		
C	Z=-X	DH641110		
C	Y=+.250983698513062690-3*(FCT(X)+FCT(Z))	DH641120		
C	X=.2368354588632401401	DH641130		
C	Z=-X	DH641140		
C	Y=+.103632909950757770-2*(FCT(X)+FCT(Z))	DH641150		
C	X=.2086272879881762001	DH641160		
C	Z=-X	DH641170		
C	Y=+.362258697853445880-2*(FCT(X)+FCT(Z))	DH641180		
C	X=.1805517171465544901	DH641190		
C	Z=-X	DH641200		
C	Y=+.107560405098791370-1*(FCT(X)+FCT(Z))	DH641210		
C	X=.1525889140209863701	DH641220		
C	Z=-X	DH641230		
C	Y=+.272031289536889180-1*(FCT(X)+FCT(Z))	DH641240		
C	X=.1247200156943117901	DH641250		
C	Z=-X	DH641260		
C	Y=+.587399819640994350-1*(FCT(X)+FCT(Z))	DH641270		
C	X=.969269423071178000	DH641280		
C	Z=-X	DH641280		

Subroutines QA2, QA3, ..., QA10, DQA4, DQA8, DQA12, DQA16, DQA24, DQA32

These subroutines perform the integration of a given function by associated Gaussian-Laguerre quadrature formulas:

To compute:

$$y = \int_0^{\infty} \frac{e^{-x} f(x)}{\sqrt{x}} dx$$

generalized Gaussian-Laguerre quadrature formulas with n = 2, 3, ..., 10 (or n = 4, 8, 12, 16, 24, 32) points are used to get approximations:

$$y_n = \sum_{k=1}^n A_k^{(n)} f(x_k^{(n)}) \quad (n = 2, 3, \dots) \quad (1)$$

which are exact whenever f(x) is a polynomial up to the degree 2n-1. Note that the nodes x_k^{(n)} are the roots of the associated Laguerre polynomials L_n^{(-1)}(x) of degree n.

For reference see:

(1) Concus/Cassatt/Jaehrig/Melby, "Tables for

the Evaluation of $\int_0^{\infty} x^{\beta} \cdot e^{-x} \cdot f(x) \cdot dx$ by Gauss-

Laguerre Quadrature", MTAC, vol. 17, No. 83 (1963), pp. 245-256.

(2) Shao/Chen/Frank, "Tables of Zeros and Gaussian Weights of Certain Associated Laguerre Polynomials and the Related Generalized Hermite Polynomials", IBM Technical Report TR 00.1100 (March 1964), pp. 15-16.

QA2 10
QA2 20
QA2 30
SUBROUTINE QA2
QA2 40
PURPOSE
TO COMPUTE INTEGRAL(EXP(-X)*FCT(X)/SQRT(X), SUMMED OVER X
FROM 0 TO INFINITY).
QA2 70
QA2 80
QA2 90
USAGE
CALL QA2 (FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
QA2 110
QA2 120
QA2 130
DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
Y - THE RESULTING INTEGRAL VALUE.
QA2 150
QA2 160
QA2 170
REMARKS
NONE
QA2 180
QA2 190
QA2 200
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
BY THE USER.
QA2 210
QA2 220
QA2 230
METHOD
EVALUATION IS DONE BY MEANS OF 2-POINT GENERALIZED GAUSSIAN-
LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY,
WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 3.
FOR REFERENCE, SEE
CONCUS/CASSATT/JAEHNIG/MELBY, TABLES FOR THE EVALUATION OF
INTEGRAL(X**BETA*EXP(-X)*F(X), SUMMED OVER X FROM 0 TO
INFINITY) BY GAUSS-LAGUERRE QUADRATURE, MTAC, VOL.17,
ISS.83 (1963), PP.245-256.
QA2 250
QA2 260
QA2 270
QA2 280
QA2 290
QA2 300
QA2 310
QA2 320
QA2 330
QA2 340
QA2 350
SUBROUTINE QA2(FCT,Y)
QA2 360
QA2 370
QA2 380
QA2 390
QA2 400
X=2.724745
Y=.1626257*FCT(X)
X=.2752551
Y=Y+1.609828*FCT(X)
RETURN
END
QA2 440
QA2 450

QA3 10
QA3 20
QA3 30
SUBROUTINE QA3
QA3 40
PURPOSE
TO COMPUTE INTEGRAL(EXP(-X)*FCT(X)/SQRT(X), SUMMED OVER X
FROM 0 TO INFINITY).
QA3 60
QA3 70
QA3 80
QA3 90
USAGE
CALL QA3 (FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
QA3 100
QA3 110
QA3 120
QA3 130
QA3 140
DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
Y - THE RESULTING INTEGRAL VALUE.
QA3 150
QA3 160
QA3 170
REMARKS
NONE
QA3 180
QA3 190
QA3 200
QA3 210
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
BY THE USER.
QA3 220
QA3 230
QA3 240
METHOD
EVALUATION IS DONE BY MEANS OF 3-POINT GENERALIZED GAUSSIAN-
LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY,
WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 5.
FOR REFERENCE, SEE
CONCUS/CASSATT/JAEHNIG/MELBY, TABLES FOR THE EVALUATION OF
INTEGRAL(X**BETA*EXP(-X)*F(X), SUMMED OVER X FROM 0 TO
INFINITY) BY GAUSS-LAGUERRE QUADRATURE, MTAC, VOL.17,
ISS.83 (1963), PP.245-256.
QA3 250
QA3 260
QA3 270
QA3 280
QA3 290
QA3 300
QA3 310
QA3 320
QA3 330
QA3 340
QA3 350
SUBROUTINE QA3(FCT,Y)
QA3 360
QA3 370
QA3 380
QA3 390
QA3 400
X=5.525344
Y=.009060020*FCT(X)
X=1.784493
Y=Y+.3141346*FCT(X)
X=.1901635
Y=Y+1.449259*FCT(X)
RETURN
END
QA3 410
QA3 420
QA3 430
QA3 440
QA3 450
QA3 460
QA3 470

QA4 10
QA4 20
QA4 30
SUBROUTINE QA4
QA4 40
PURPOSE
TO COMPUTE INTEGRAL(EXP(-X)*FCT(X)/SQRT(X), SUMMED OVER X
FROM 0 TO INFINITY).
QA4 70
QA4 80
QA4 90
USAGE
CALL QA4 (FCT,Y)
PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
QA4 100
QA4 110
QA4 120
QA4 130
DESCRIPTION OF PARAMETERS
FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
Y - THE RESULTING INTEGRAL VALUE.
QA4 150
QA4 160
QA4 170
REMARKS
NONE
QA4 180
QA4 190
QA4 200
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
BY THE USER.
QA4 210
QA4 220
QA4 230
QA4 240
QA4 250
METHOD
EVALUATION IS DONE BY MEANS OF 4-POINT GENERALIZED GAUSSIAN-
LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY,
WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 7.
FOR REFERENCE, SEE
CONCUS/CASSATT/JAEHNIG/MELBY, TABLES FOR THE EVALUATION OF
INTEGRAL(X**BETA*EXP(-X)*F(X), SUMMED OVER X FROM 0 TO
INFINITY) BY GAUSS-LAGUERRE QUADRATURE, MTAC, VOL.17,
ISS.83 (1963), PP.245-256.
QA4 260
QA4 270
QA4 280
QA4 290
QA4 300
QA4 310
QA4 320
QA4 330
QA4 340
QA4 350
SUBROUTINE QA4(FCT,Y)
QA4 360
QA4 370
QA4 380
QA4 390
QA4 400
X=.588636
Y=.0003992081*FCT(X)
X=3.926964
Y=Y+.03415597*FCT(X)
X=1.339097
Y=Y+.4156047*FCT(X)
X=.1453035
Y=Y+1.322294*FCT(X)
RETURN
END
QA4 410
QA4 420
QA4 430
QA4 440
QA4 450
QA4 460
QA4 470
QA4 480
QA4 490

```

C
C
C .....
C                DQA4 10
C                DQA4 20
C                DQA4 30
C                DQA4 40
C                DQA4 50
C                DQA4 60
C                DQA4 70
C                DQA4 80
C                DQA4 90
C                DQA4 100
C                DQA4 110
C                DQA4 120
C                DQA4 130
C                DQA4 140
C                DQA4 150
C                DQA4 160
C                DQA4 170
C                DQA4 180
C                DQA4 190
C                DQA4 200
C                DQA4 210
C                DQA4 220
C                DQA4 230
C                DQA4 240
C                DQA4 250
C                DQA4 260
C                DQA4 270
C                DQA4 280
C                DQA4 290
C                DQA4 300
C                DQA4 310
C                DQA4 320
C                DQA4 330
C                DQA4 340
C                DQA4 350
C                DQA4 360
C                DQA4 370
C                DQA4 380
C                DQA4 390
C                DQA4 400
C                DQA4 410
C                DQA4 420
C                DQA4 430
C                DQA4 440
C                DQA4 450
C                DQA4 460
C                DQA4 470
C                DQA4 480
C                DQA4 490
C                DQA4 500
C                DQA4 510
C                DQA4 520
C .....
C SUBROUTINE DQA4(FCT,Y)
C .....
C DOUBLE PRECISION X,Y,FCT
C .....
C X=.858863568901203401
C Y=.399208164422735240-3*FCT(X)
C X=.3926963501358287201
C Y=Y+.34155966014826951D-1*FCT(X)
C X=.133907288126361401
C Y=Y+.4156046516297837600*FCT(X)
C X=.1453035215033170900
C Y=Y+.13222940251164826D1*FCT(X)
C RETURN
C END

```

```

C .....
C                QA6 10
C                QA6 20
C                QA6 30
C                QA6 40
C                QA6 50
C                QA6 60
C                QA6 70
C                QA6 80
C                QA6 90
C                QA6 100
C                QA6 110
C                QA6 120
C                QA6 130
C                QA6 140
C                QA6 150
C                QA6 160
C                QA6 170
C                QA6 180
C                QA6 190
C                QA6 200
C                QA6 210
C                QA6 220
C                QA6 230
C                QA6 240
C                QA6 250
C                QA6 260
C                QA6 270
C                QA6 280
C                QA6 290
C                QA6 300
C                QA6 310
C                QA6 320
C                QA6 330
C                QA6 340
C                QA6 350
C                QA6 360
C                QA6 370
C                QA6 380
C                QA6 390
C                QA6 400
C                QA6 410
C                QA6 420
C                QA6 430
C                QA6 440
C                QA6 450
C                QA6 460
C                QA6 470
C                QA6 480
C                QA6 490
C                QA6 500
C                QA6 510
C                QA6 520
C                QA6 530
C .....
C SUBROUTINE QA6(FCT,Y)
C .....
C X=15.12996
C Y=.5317103E-6*FCT(X)
C X=.126248
C Y=Y+.0001714737*FCT(X)
C X=.5196153
C Y=Y+.007810781*FCT(X)
C X=.2552590
C Y=Y+.1032160*FCT(X)
C X=.8993028
C Y=Y+.5209866*FCT(X)
C X=.09874701
C Y=Y+.140270*FCT(X)
C RETURN
C END

```

```

C .....
C                QA5 10
C                QA5 20
C                QA5 30
C                QA5 40
C                QA5 50
C                QA5 60
C                QA5 70
C                QA5 80
C                QA5 90
C                QA5 100
C                QA5 110
C                QA5 120
C                QA5 130
C                QA5 140
C                QA5 150
C                QA5 160
C                QA5 170
C                QA5 180
C                QA5 190
C                QA5 200
C                QA5 210
C                QA5 220
C                QA5 230
C                QA5 240
C                QA5 250
C                QA5 260
C                QA5 270
C                QA5 280
C                QA5 290
C                QA5 300
C                QA5 310
C                QA5 320
C                QA5 330
C                QA5 340
C                QA5 350
C                QA5 360
C                QA5 370
C                QA5 380
C                QA5 390
C                QA5 400
C                QA5 410
C                QA5 420
C                QA5 430
C                QA5 440
C                QA5 450
C                QA5 460
C                QA5 470
C                QA5 480
C                QA5 490
C                QA5 500
C                QA5 510
C .....
C SUBROUTINE QA5(FCT,Y)
C .....
C X=11.80719
C Y=.1528087E-4*FCT(X)
C X=6.414730
C Y=Y+.002687291*FCT(X)
C X=.3.085937
C Y=Y+.06774879*FCT(X)
C X=.1.074562
C Y=Y+.4802772*FCT(X)
C X=.1175813
C Y=Y+.1.221725*FCT(X)
C RETURN
C END

```

```

C .....
C                QA7 10
C                QA7 20
C                QA7 30
C                QA7 40
C                QA7 50
C                QA7 60
C                QA7 70
C                QA7 80
C                QA7 90
C                QA7 100
C                QA7 110
C                QA7 120
C                QA7 130
C                QA7 140
C                QA7 150
C                QA7 160
C                QA7 170
C                QA7 180
C                QA7 190
C                QA7 200
C                QA7 210
C                QA7 220
C                QA7 230
C                QA7 240
C                QA7 250
C                QA7 260
C                QA7 270
C                QA7 280
C                QA7 290
C                QA7 300
C                QA7 310
C                QA7 320
C                QA7 330
C                QA7 340
C                QA7 350
C                QA7 360
C                QA7 370
C                QA7 380
C                QA7 390
C                QA7 400
C                QA7 410
C                QA7 420
C                QA7 430
C                QA7 440
C                QA7 450
C                QA7 460
C                QA7 470
C                QA7 480
C                QA7 490
C                QA7 500
C                QA7 510
C                QA7 520
C                QA7 530
C                QA7 540
C                QA7 550
C .....
C SUBROUTINE QA7
C .....
C PURPOSE
C TO COMPUTE INTEGRAL(EXP(-X)*FCT(X)/SQRT(X), SUMMED OVER X
C FROM 0 TO INFINITY).
C .....
C USAGE
C CALL QA7 (FCT,Y)
C PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C .....
C DESCRIPTION OF PARAMETERS
C FCT - THE NAME OF AN EXTERNAL FUNCTION SUBPROGRAM USED.
C Y - THE RESULTING INTEGRAL VALUE.
C .....
C REMARKS
C NONE
C .....
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C THE EXTERNAL FUNCTION SUBPROGRAM FCT(X) MUST BE FURNISHED
C BY THE USER.
C .....
C METHOD
C EVALUATION IS DONE BY MEANS OF 7-POINT GENERALIZED GAUSSIAN-
C LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY,
C WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 13.
C FOR REFERENCE, SEE
C CONCUS/CASSATT/JAEHNIG/MELBY, TABLES FOR THE EVALUATION OF
C INTEGRAL(X**BETA*EXP(-X)*F(X), SUMMED OVER X FROM 0 TO
C INFINITY) BY GAUSS-LAGUERRE QUADRATURE, MTAC, VOL.17,
C ISS.83 (1963), PP.245-256.
C .....
C SUBROUTINE QA7(FCT,Y)
C .....
C X=18.52828
C Y=.1725718E-7*FCT(X)
C X=11.99999
C Y=Y+.9432969E-5*FCT(X)
C X=.7.554091
C Y=Y+.0007101852*FCT(X)
C X=.4.389793
C Y=Y+.01570011*FCT(X)
C X=.2.180592
C Y=Y+.1370111*FCT(X)
C X=.7721379
C Y=Y+.5462112*FCT(X)
C X=.08511544
C Y=Y+.1.072812*FCT(X)
C RETURN
C END

```



```

C          DA12 10
C          DA12 20
C          DA12 30
C          SUBROUTINE DQA12
C          DA12 40
C          DA12 50
C          PURPOSE
C          TO COMPUTE INTEGRAL  $(\text{EXP}(-X) * \text{FCT}(X) / \text{SQRT}(X))$ , SUMMED OVER X
C          FROM 0 TO INFINITY).
C          DA12 60
C          DA12 70
C          DA12 80
C          DA12 90
C          USAGE
C          CALL DQA12 (FCT,Y)
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C          DA12 100
C          DA12 110
C          DA12 120
C          DA12 130
C          DA12 140
C          DESCRIPTION OF PARAMETERS
C          FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION
C          SUBPROGRAM USED.
C          Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE.
C          DA12 150
C          DA12 160
C          DA12 170
C          DA12 180
C          REMARKS
C          NONE
C          DA12 190
C          DA12 200
C          DA12 210
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X)
C          MUST BE FURNISHED BY THE USER.
C          DA12 220
C          DA12 230
C          DA12 240
C          DA12 250
C          METHOD
C          EVALUATION IS DONE BY MEANS OF 12-POINT GENERALIZED GAUSS-
C          LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY
C          WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 23.
C          FOR REFERENCE, SEE
C          SMAO/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF
C          CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED
C          GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT
C          TR00.1100 (MARCH 1964), PP.15-16.
C          DA12 260
C          DA12 270
C          DA12 280
C          DA12 290
C          DA12 300
C          DA12 310
C          DA12 320
C          DA12 330
C          DA12 340
C          DA12 350
C          DA12 360
C          DA12 370
C          SUBROUTINE DQA12(FCT,Y)
C          DA12 380
C          DA12 390
C          DA12 400
C          DA12 410
C          DA12 420
C          DA12 430
C          DA12 440
C          DA12 450
C          DA12 460
C          DA12 470
C          DA12 480
C          DA12 490
C          DA12 500
C          DA12 510
C          DA12 520
C          DA12 530
C          DA12 540
C          DA12 550
C          DA12 560
C          DA12 570
C          DA12 580
C          DA12 590
C          DA12 600
C          DA12 610
C          DA12 620
C          DA12 630
C          DA12 640
C          DA12 650
C          DA12 660
C          DA12 670
C          DA12 680
C          DOUBLE PRECISION X,Y,FCT
C          X=.36191360360615602D2
C          Y=.33287369929782177D-15*FCT(X)
C          X=.27661108779846090D2
C          Y=Y+.13169240486156340D-11*FCT(X)
C          X=.21396755936166109D2
C          Y=Y+.60925085399751278D-9*FCT(X)
C          X=.16432195087675313D2
C          Y=Y+.8037942349882859D-7*FCT(X)
C          X=.12390447963809471D2
C          Y=Y+.43164914098046673D-5*FCT(X)
C          X=.9075434230961203D1
C          Y=Y+.11377383272808760D-3*FCT(X)
C          X=.6369753880306349D1
C          Y=Y+.16473849653768349D-2*FCT(X)
C          X=.41984156448784132D1
C          Y=Y+.14096711620145342D-1*FCT(X)
C          X=.2509848097321280D1
C          Y=Y+.7489094100646149D-1*FCT(X)
C          X=.12695899401039615D1
C          Y=Y+.25547924336911832D0*FCT(X)
C          X=.454506468156378028D0
C          Y=Y+.57235907069288604D0*FCT(X)
C          X=.5036188911729395D-1
C          Y=Y+.8538623277373985D0*FCT(X)
C          RETURN
C          END

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```

C          DA16 10
C          DA16 20
C          DA16 30
C          SUBROUTINE DQA16
C          DA16 40
C          DA16 50
C          DA16 60
C          DA16 70
C          DA16 80
C          DA16 90
C          DA16 100
C          DA16 110
C          DA16 120
C          DA16 130
C          DA16 140
C          DA16 150
C          DA16 160
C          DA16 170
C          DA16 180
C          DA16 190
C          DA16 200
C          DA16 210
C          DA16 220
C          DA16 230
C          DA16 240
C          DA16 250
C          DA16 260
C          DA16 270
C          DA16 280
C          DA16 290
C          DA16 300
C          DA16 310
C          DA16 320
C          DA16 330
C          DA16 340
C          DA16 350
C          DA16 360
C          DA16 370
C          DA16 380
C          DA16 390
C          DA16 400
C          DA16 410
C          DA16 420
C          DA16 430
C          DA16 440
C          DA16 450
C          DA16 460
C          DA16 470
C          DA16 480
C          DA16 490
C          DA16 500
C          DA16 510
C          DA16 520
C          DA16 530
C          DA16 540
C          DA16 550
C          DA16 560
C          DA16 570
C          DA16 580
C          DA16 590
C          DA16 600
C          DA16 610
C          DA16 620
C          DA16 630
C          DA16 640
C          DA16 650
C          DA16 660
C          DA16 670
C          DA16 680
C          DA16 690
C          DA16 700
C          DA16 710
C          DA16 720
C          DA16 730
C          DA16 740
C          DA16 750
C          DA16 760
C          DA16 770
C          DA16 780
C          DA16 790
C          DA16 800
C          DA16 810
C          DA16 820
C          DA16 830
C          DA16 840
C          DA16 850
C          DA16 860
C          DA16 870
C          DA16 880
C          DA16 890
C          DA16 900
C          DA16 910
C          DA16 920
C          DA16 930
C          DA16 940
C          DA16 950
C          DA16 960
C          DA16 970
C          DA16 980
C          DA16 990
C          DA16 1000
C          SUBROUTINE DQA16(FCT,Y)
C          DOUBLE PRECISION X,Y,FCT
C          X=.5077722387753708D2
C          Y=.1662135285476832D-21*FCT(X)
C          X=.4108166652549120D2
C          Y=Y+.18463473073036584D-17*FCT(X)
C          X=.3378197048822616D2
C          Y=Y+.23966880341856973D-14*FCT(X)
C          X=.27831438211328676D2
C          Y=Y+.8430020422652895D-12*FCT(X)
C          X=.2282130069352520D2
C          Y=Y+.11866582926793277D-9*FCT(X)
C          X=.18537743178606694D2
C          Y=Y+.8197664329541793D-8*FCT(X)
C          X=.1485143134180125D2
C          Y=Y+.31483355850911881D-6*FCT(X)
C          X=.1167703367397595D2
C          Y=Y+.7301170259124752D-5*FCT(X)
C          X=.6642215179741444D1
C          Y=Y+.1083168123639965D-3*FCT(X)
C          X=.895500133723390D1
C          Y=Y+.4706726707667587D1
C          X=.7309780653308856D-2*FCT(X)
C          X=.3124601050702144D1
C          Y=Y+.3510685766314686D1-1*FCT(X)
C          X=.1877931507696074D1
C          Y=Y+.12091626191182523D0*FCT(X)
C          X=.953553155390865D0
C          Y=Y+.30253946815328497D0*FCT(X)
C          X=.34220015601094768D0
C          Y=Y+.5549162844059598D0*FCT(X)
C          X=.3796291457531345D-1
C          Y=Y+.7504767051856048D0*FCT(X)
C          RETURN
C          END

```

```

C          DA24 10
C          .....DA24 20
C          DA24 30
C          SUBROUTINE DQA24 DA24 40
C          DA24 50
C          DA24 60
C          PURPOSE DA24 70
C          TO COMPUTE INTEGRAL(EXP(-X)*FCT(X)/SQRT(X), SUMMED OVER X
C          FROM 0 TO INFINITY). DA24 80
C          DA24 90
C          USAGE DA24 100
C          CALL DQA24 (FCT,Y) DA24 110
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT DA24 120
C          DA24 130
C          DESCRIPTION OF PARAMETERS DA24 140
C          FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION DA24 150
C          SUBPROGRAM USED. DA24 160
C          Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE. DA24 170
C          DA24 180
C          REMARKS DA24 190
C          NONE DA24 200
C          DA24 210
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DA24 220
C          THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) DA24 230
C          MUST BE FURNISHED BY THE USER. DA24 240
C          DA24 250
C          METHOD DA24 260
C          EVALUATION IS DONE BY MEANS OF 24-POINT GENERALIZED GAUSS-
C          LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY
C          WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 47. DA24 270
C          FOR REFERENCE, SEE DA24 280
C          SMOO/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF
C          CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED
C          GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT
C          TR00.1100 (MARCH 1964), PP.15-16. DA24 290
C          DA24 300
C          .....DA24 360
C          SUBROUTINE DQA24(FCT,Y) DA24 370
C          DA24 380
C          DA24 390
C          DA24 400
C          DOUBLE PRECISION X,Y,FCT DA24 410
C          DA24 420
C          X=.8055628081995041D2 DA24 430
C          Y=.158711029215479940-34*FCT(X) DA24 440
C          X=.69068601975304369D2 DA24 450
C          Y=Y+.1169225386627757D-29*FCT(X) DA24 460
C          X=.6020666696305723D2 DA24 470
C          Y=Y+.7370072160301340D-26*FCT(X) DA24 480
C          X=.5279943252728363D2 DA24 490
C          Y=Y+.11129154937804570D-22*FCT(X) DA24 500
C          X=.4637697955754013D2 DA24 510
C          Y=Y+.63767746470102769D-20*FCT(X) DA24 520
C          X=.40711598185543107D2 DA24 530
C          Y=Y+.17460319202373353D-17*FCT(X) DA24 540
C          X=.3565370351632821D2 DA24 550
C          Y=Y+.26303192453168170D-15*FCT(X) DA24 560
C          X=.31106464709046565D2 DA24 570
C          Y=Y+.23951797309583587D-13*FCT(X) DA24 580
C          X=.27001406056472356D2 DA24 590
C          Y=Y+.14093865163091778D-11*FCT(X) DA24 600
C          X=.23287932824879917D2 DA24 610
C          Y=Y+.56305930756763382D-10*FCT(X) DA24 620
C          X=.1992742587524462D2 DA24 630
C          Y=Y+.15860934990330765D-8*FCT(X) DA24 640
C          X=.1689671928527108D2 DA24 650
C          Y=Y+.32450282717915397D-7*FCT(X) DA24 660
C          X=.14150586187285759D2 DA24 670
C          Y=Y+.49373179873395010D-6*FCT(X) DA24 680
C          X=.1169065926056073D2 DA24 690
C          Y=Y+.5699513834696962D-5*FCT(X) DA24 700
C          X=.9494095330026488D1 DA24 710
C          Y=Y+.50571980554969778D-4*FCT(X) DA24 720
C          X=.7547704680023454D1 DA24 730
C          Y=Y+.35030086360234566D-3*FCT(X) DA24 740
C          X=.5840733271323608D1 DA24 750
C          Y=Y+.19127846396380306D-2*FCT(X) DA24 760
C          X=.4364283076933306D1 DA24 770
C          Y=Y+.8306009823955105D-2*FCT(X) DA24 780
C          X=.3111052455147713D1 DA24 790
C          Y=Y+.28889923149962199D-1*FCT(X) DA24 800
C          X=.20751129098523806D1 DA24 810
C          Y=Y+.8095935396920770D-1*FCT(X) DA24 820
C          X=.12517406323627464D1 DA24 830
C          Y=Y+.18364459415857036D0*FCT(X) DA24 840
C          X=.63729027873266879D0 DA24 850
C          Y=Y+.33840894389128221D0*FCT(X) DA24 860
C          X=.2291023164926243D0 DA24 870
C          Y=Y+.50792308532951820D0*FCT(X) DA24 880
C          X=.2543796585689359D-1 DA24 890
C          Y=Y+.62200206075592616D0*FCT(X) DA24 900
C          RETURN DA24 910
C          END DA24 920

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```

C          DA32 10
C          .....DA32 20
C          DA32 30
C          SUBROUTINE DQA32 DA32 40
C          DA32 50
C          DA32 60
C          PURPOSE DA32 70
C          TO COMPUTE INTEGRAL(EXP(-X)*FCT(X)/SQRT(X), SUMMED OVER X
C          FROM 0 TO INFINITY). DA32 80
C          DA32 90
C          USAGE DA32 100
C          CALL DQA32 (FCT,Y) DA32 110
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT DA32 120
C          DA32 130
C          DESCRIPTION OF PARAMETERS DA32 140
C          FCT - THE NAME OF AN EXTERNAL DOUBLE PRECISION FUNCTION DA32 150
C          SUBPROGRAM USED. DA32 160
C          Y - THE RESULTING DOUBLE PRECISION INTEGRAL VALUE. DA32 170
C          DA32 180
C          REMARKS DA32 190
C          NONE DA32 200
C          DA32 210
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DA32 220
C          THE EXTERNAL DOUBLE PRECISION FUNCTION SUBPROGRAM FCT(X) DA32 230
C          MUST BE FURNISHED BY THE USER. DA32 240
C          DA32 250
C          METHOD DA32 260
C          EVALUATION IS DONE BY MEANS OF 32-POINT GENERALIZED GAUSS-
C          LAGUERRE QUADRATURE FORMULA, WHICH INTEGRATES EXACTLY
C          WHENEVER FCT(X) IS A POLYNOMIAL UP TO DEGREE 63. DA32 270
C          FOR REFERENCE, SEE DA32 280
C          SMOO/CHEN/FRANK, TABLES OF ZEROS AND GAUSSIAN WEIGHTS OF
C          CERTAIN ASSOCIATED LAGUERRE POLYNOMIALS AND THE RELATED
C          GENERALIZED HERMITE POLYNOMIALS, IBM TECHNICAL REPORT
C          TR00.1100 (MARCH 1964), PP.15-16. DA32 290
C          DA32 300
C          .....DA32 360
C          SUBROUTINE DQA32(FCT,Y) DA32 370
C          DA32 380
C          DA32 390
C          DA32 400
C          DOUBLE PRECISION X,Y,FCT DA32 410
C          DA32 420
C          X=.11079926894707576D3 DA32 430
C          Y=.11071413071713886D-47*FCT(X) DA32 440
C          X=.9791671642606276D2 DA32 450
C          Y=Y+.33594959802163184D-42*FCT(X) DA32 460
C          X=.8785611994313352D2 DA32 470
C          Y=Y+.6842276022511681D-38*FCT(X) DA32 480
C          X=.793390658288200D2 DA32 490
C          Y=Y+.31147812492595276D-34*FCT(X) DA32 500
C          X=.7186849935955142D2 DA32 510
C          Y=Y+.50993217982259985D-31*FCT(X) DA32 520
C          X=.6518442637613578D2 DA32 530
C          Y=Y+.38582071909299337D-28*FCT(X) DA32 540
C          X=.5912902793439195D2 DA32 550
C          Y=Y+.15723595577851821D-25*FCT(X) DA32 560
C          X=.5359723182614851D2 DA32 570
C          Y=Y+.38234137666012857D-23*FCT(X) DA32 580
C          X=.4851458386741604D2 DA32 590
C          Y=Y+.59652755685597023D-21*FCT(X) DA32 600
C          X=.4382588636990390D2 DA32 610
C          Y=Y+.63045091330075628D-19*FCT(X) DA32 620
C          X=.3948879112336812D2 DA32 630
C          Y=Y+.47037694213516382D-17*FCT(X) DA32 640
C          X=.3566996139617328D2 DA32 650
C          Y=Y+.25601867826448761D-15*FCT(X) DA32 660
C          X=.3174254379061660D2 DA32 670
C          Y=Y+.10437247453181695D-13*FCT(X) DA32 680
C          X=.2828453194970531D2 DA32 690
C          Y=Y+.32566814616194407D-12*FCT(X) DA32 700
C          X=.2507785654419805D2 DA32 710
C          Y=Y+.7918355533895448D-11*FCT(X) DA32 720
C          X=.2210707038220600D2 DA32 730
C          Y=Y+.15230434500290903D-9*FCT(X) DA32 740
C          X=.1935921087268714D2 DA32 750
C          Y=Y+.23472334644903987D-8*FCT(X) DA32 760
C          X=.16923405362953694D2 DA32 770
C          Y=Y+.293020506329522187D-7*FCT(X) DA32 780
C          X=.14489986690780274D2 DA32 790
C          Y=Y+.29910658734544941D-6*FCT(X) DA32 800
C          X=.1235083821771477D2 DA32 810
C          Y=Y+.25166805020623692D-5*FCT(X) DA32 820
C          X=.1039891905552624D2 DA32 830
C          Y=Y+.17576998641700718D-4*FCT(X) DA32 840
C          X=.8628029857405929D1 DA32 850
C          Y=Y+.10251858271572549D-3*FCT(X) DA32 860
C          X=.7032957798283893D1 DA32 870
C          Y=Y+.50196739702612497D-3*FCT(X) DA32 880
C          X=.5609103457496151D1 DA32 890
C          Y=Y+.20726581996151553D-2*FCT(X) DA32 900
C          X=.4352534529330140D1 DA32 910
C          Y=Y+.7245173957068918D-2*FCT(X) DA32 920
C          X=.32598922564569419D1 DA32 930
C          Y=Y+.21512081019758274D-1*FCT(X) DA32 940
C          X=.23283376682103970D1 DA32 950
C          Y=Y+.54406257907377837D-1*FCT(X) DA32 960
C          X=.155508231478938D1 DA32 970
C          Y=Y+.11747996392819887D0*FCT(X) DA32 980
C          X=.9394832145007343D0 DA32 990
C          Y=Y+.21699669861237368D0*FCT(X) DA321000
C          X=.47875647727748885D0 DA321010
C          Y=Y+.3433716846981674D0*FCT(X) DA321020
C          X=.1722157241453958D0 DA321030
C          Y=Y+.46598957212535609D0*FCT(X) DA321040
C          X=.19127510968446856D-1 DA321050
C          Y=Y+.54275484988260796D0*FCT(X) DA321060
C          RETURN DA321070
C          END DA321080

```

Numerical Differentiation

Subroutines DGT3 and DDGT3

These subroutines compute a vector $Z = (z_1, \dots, z_n)$ of derivative values, given vectors $X = (x_1, \dots, x_n)$ of argument values and $Y = (y_1, \dots, y_n)$ of corresponding function values. Except at the endpoints x_1 and x_n , z_i is the derivative at x_i of the Lagrangian interpolation polynomial of degree 2 relevant to the three successive points (x_{i-1}, y_{i-1}) , (x_i, y_i) and (x_{i+1}, y_{i+1}) .

1. Mathematical background

For $i = 1, \dots, n-2$ we must find a_i , b_i , and c_i such that

$$\bar{y}_i(x) = a_i x^2 + b_i x + c_i$$

passes through (x_i, y_i) , (x_{i+1}, y_{i+1}) , and (x_{i+2}, y_{i+2}) .

The desired derivative values z_i are given by:

$$z_i = \begin{cases} y_1'(x_1) = 2a_1 x_1 + b_1 & \text{if } i=1 \\ y_{i-1}'(x_i) = 2a_{i-1} x_i + b_{i-1} & \text{if } i=2, \dots, n-1 \\ y_{n-2}'(x_n) = 2a_{n-2} x_n + b_{n-2} & \text{if } i=n \end{cases}$$

An easy computation yields:

$$z_i = \begin{cases} \frac{y_2 - y_1}{x_2 - x_1} + \frac{y_3 - y_1}{x_3 - x_1} - \frac{y_3 - y_2}{x_3 - x_2} & \text{if } i=1 \\ \frac{y_i - y_{i-1}}{x_i - x_{i-1}} + \frac{y_{i+1} - y_i}{x_{i+1} - x_i} - \frac{y_{i+1} - y_{i-1}}{x_{i+1} - x_{i-1}} & \text{if } i=2, \dots, n-1 \\ \frac{y_n - y_{n-1}}{x_n - x_{n-1}} + \frac{y_n - y_{n-2}}{x_n - x_{n-2}} - \frac{y_{n-1} - y_{n-2}}{x_{n-1} - x_{n-2}} & \text{if } i=n \end{cases} \quad (1)$$

Assuming that the vectors X and Y represent a portion of a three-times differentiable function, z_i involves a truncation error T_i where:

$$T_i = \begin{cases} \frac{1}{6} (x_1 - x_2)(x_1 - x_3)y'''(\xi_1) & \text{if } i=1 \\ \frac{1}{6} (x_i - x_{i-1})(x_i - x_{i+1})y'''(\xi_i) & \text{if } i=2, \dots, n-1 \\ \frac{1}{6} (x_n - x_{n-1})(x_n - x_{n-2})y'''(\xi_n) & \text{if } i=n \end{cases}$$

and ξ_i is in the closed interval determined by the three argument values used in computing z_i , $i = 1, \dots, n$.

2. Programming considerations

The subroutines compute the z_i in serial order according to (1). If $n < 3$, there is no computation, and the error parameter is set to -1. If two of the three arguments x_{j-2} , x_{j-1} , x_j are identical, $j=3, \dots, n$, the computation is prematurely terminated, and the error parameter IER is set to j . However, z_1, \dots, z_{j-1} are returned if $j > 3$. In this case z_{j-1} is computed treating x_{j-1} as the right-hand endpoint. If there is no error, IER is set to zero at the end of the computation. The output vector Z can have the same storage allocation as X or Y .

For reference see F. B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp. 64-68.

```

C ..... DGT3 10
C ..... DGT3 20
C ..... DGT3 30
C SUBROUTINE DGT3 DGT3 40
C ..... DGT3 50
C ..... DGT3 60
C PURPOSE DGT3 70
C TO COMPUTE A VECTOR OF DERIVATIVE VALUES GIVEN VECTORS OF
C ARGUMENT VALUES AND CORRESPONDING FUNCTION VALUES. DGT3 80
C ..... DGT3 90
C USAGE DGT3 100
C CALL DGT3(X,Y,Z,NDIM,IER) DGT3 110
C ..... DGT3 120
C DESCRIPTION OF PARAMETERS DGT3 130
C X - GIVEN VECTOR OF ARGUMENT VALUES (DIMENSION NDIM) DGT3 140
C Y - GIVEN VECTOR OF FUNCTION VALUES CORRESPONDING TO X DGT3 150
C (DIMENSION NDIM) DGT3 160
C Z - RESULTING VECTOR OF DERIVATIVE VALUES (DIMENSION DGT3 170
C NDIM) DGT3 180
C NDIM - DIMENSION OF VECTORS X,Y AND Z DGT3 190
C IER - RESULTING ERROR PARAMETER DGT3 200
C IER = -1 - NDIM IS LESS THAN 3 DGT3 210
C IER = 0 - NO ERROR DGT3 220
C IER POSITIVE - X(IER) = X(IER-1) OR X(IER) = DGT3 230
C X(IER-2) DGT3 240
C ..... DGT3 250
C REMARKS DGT3 260
C (1) IF IER = -1,2,3, THEN THERE IS NO COMPUTATION. DGT3 270
C (2) IF IER = 4,.....,N, THEN THE DERIVATIVE VALUES Z(1) DGT3 280
C ..... Z(IER-1) HAVE BEEN COMPUTED. DGT3 290
C (3) Z CAN HAVE THE SAME STORAGE ALLOCATION AS X OR Y. IF DGT3 300
C X OR Y IS DISTINCT FROM Z, THEN IT IS NOT DESTROYED. DGT3 310
C ..... DGT3 320
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DGT3 330
C NONE DGT3 340
C ..... DGT3 350
C METHOD DGT3 360
C EXCEPT AT THE ENDPOINTS X(1) AND X(NDIM), Z(I) IS THE DGT3 370
C DERIVATIVE AT X(I) OF THE LAGRANGIAN INTERPOLATION DGT3 380
C POLYNOMIAL OF DEGREE 2 RELEVANT TO THE 3 SUCCESSIVE POINTS DGT3 390
C (X(I)*Y(I+K)) K = -1,0,1. (SEE HILDEBRAND, F.B., DGT3 400
C INTRODUCTION TO NUMERICAL ANALYSIS, MC GRAW-HILL, NEW YORK/ DGT3 410
C TORONTO/LONDON, 1956, PP. 64-68.) DGT3 420
C ..... DGT3 430
C ..... DGT3 440
C SUBROUTINE DGT3(X,Y,Z,NDIM,IER) DGT3 450
C ..... DGT3 460
C ..... DGT3 470
C DIMENSION X(1),Y(1),Z(1) DGT3 480
C ..... DGT3 490
C TEST OF DIMENSION AND ERROR EXIT IN CASE NDIM IS LESS THAN 3 DGT3 500
C IER=-1 DGT3 510
C IF(NDIM<3),1 DGT3 520
C ..... DGT3 530
C PREPARE DIFFERENTIATION LOOP DGT3 540
C 1 A=X(1) DGT3 550
C B=Y(1) DGT3 560
C I=2 DGT3 570
C DY2=X(2)-A DGT3 580
C IF(DY2)2,9,2 DGT3 590
C 2 DY2=(Y(2)-B)/DY2 DGT3 600
C ..... DGT3 610
C START DIFFERENTIATION LOOP DGT3 620
C DO 6 I=3,NDIM DGT3 630
C A=X(I)-A DGT3 640
C IF(A)3,9,3 DGT3 650
C 3 A=(Y(I)-B)/A DGT3 660
C B=X(I)-X(I-1) DGT3 670
C IF(B)4,9,4 DGT3 680
C 4 DY1=DY2 DGT3 690
C DY2=(Y(I)-Y(I-1))/B DGT3 700
C DY3=A DGT3 710
C A=X(I-1) DGT3 720
C B=Y(I-1) DGT3 730
C IF(I-3)5,5,6 DGT3 740
C ..... DGT3 750
C 5 Z(I)=DY1+DY3-DY2 DGT3 760
C 6 Z(I-1)=DY1+DY2-DY3 DGT3 770
C END DIFFERENTIATION LOOP DGT3 780
C ..... DGT3 790
C NORMAL EXIT DGT3 800
C IER=0 DGT3 810
C I=NDIM DGT3 820
C 7 Z(I)=DY2+DY3-DY1 DGT3 830
C 8 RETURN DGT3 840
C ..... DGT3 850
C EPROP EXIT IN CASE OF IDENTICAL ARGUMENTS DGT3 860
C 9 IER=I DGT3 870
C I=I-1 DGT3 880
C IF(I-2)8,8,7 DGT3 890
C END DGT3 900

```

```

C ..... DDGT 10
C SUBROUTINE DDGT3 DDGT 20
C DDGT 30
C DDGT 40
C DDGT 50
C DDGT 60
C DDGT 70
C DDGT 80
C DDGT 90
C DDGT 100
C DDGT 110
C DDGT 120
C DDGT 130
C DDGT 140
C DDGT 150
C DDGT 160
C DDGT 170
C DDGT 180
C DDGT 190
C DDGT 200
C DDGT 210
C DDGT 220
C DDGT 230
C DDGT 240
C DDGT 250
C DDGT 260
C DDGT 270
C DDGT 280
C DDGT 290
C DDGT 300
C DDGT 310
C DDGT 320
C DDGT 330
C DDGT 340
C DDGT 350
C DDGT 360
C DDGT 370
C DDGT 380
C DDGT 390
C DDGT 400
C DDGT 410
C DDGT 420
C DDGT 430
C DDGT 440
C DDGT 450
C DDGT 460
C DDGT 470
C DDGT 480
C DDGT 490
C DDGT 500
C DDGT 510
C DDGT 520
C DDGT 530
C DDGT 540
C DDGT 550
C DDGT 560
C DDGT 570
C DDGT 580
C DDGT 590
C DDGT 600
C DDGT 610
C DDGT 620
C DDGT 630
C DDGT 640
C DDGT 650
C DDGT 660
C DDGT 670
C DDGT 680
C DDGT 690
C DDGT 700
C DDGT 710
C DDGT 720
C DDGT 730
C DDGT 740
C DDGT 750
C DDGT 760
C DDGT 770
C DDGT 780
C DDGT 790
C DDGT 800
C DDGT 810
C DDGT 820
C DDGT 830
C DDGT 840
C DDGT 850
C DDGT 860
C DDGT 870
C DDGT 880
C DDGT 890
C DDGT 900
C DDGT 910
C DDGT 920
C .....
SUBROUTINE DDGT3(X,Y,Z,NDIM,IER)
C
C DESCRIPTION OF PARAMETERS
C X - GIVEN VECTOR OF DOUBLE PRECISION ARGUMENT VALUES
C (DIMENSION NDIM)
C Y - GIVEN VECTOR OF DOUBLE PRECISION FUNCTION VALUES
C CORRESPONDING TO X (DIMENSION NDIM)
C Z - RESULTING VECTOR OF DOUBLE PRECISION DERIVATIVE
C VALUES (DIMENSION NDIM)
C NDIM - DIMENSION OF VECTORS X,Y AND Z
C IER - RESULTING ERROR PARAMETER
C IER = -1 - NDIM IS LESS THAN 3
C IER = 0 - NO ERROR
C IER POSITIVE - X(IER) = X(IER-1) OR X(IER) =
C X(IER-2)
C
C REMARKS
C (1) IF IER = -1,2,3, THEN THERE IS NO COMPUTATION.
C (2) IF IER = 4,...,N, THEN THE DERIVATIVE VALUES Z(I)
C +...+ Z(IER-1) HAVE BEEN COMPUTED.
C (3) Z CAN HAVE THE SAME STORAGE ALLOCATION AS X OR Y. IF
C X OF Y IS DISTINCT FROM Z, THEN IT IS NOT DESTROYED.
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C
C METHOD
C EXCEPT AT THE ENPOINTS X(1) AND X(NDIM), Z(I) IS THE
C DERIVATIVE AT X(I) OF THE LAGRANGIAN INTERPOLATION
C POLYNOMIAL OF DEGREE 2 RELEVANT TO THE 3 SUCCESSIVE POINTS
C (X(I+K),Y(I+K)) K = -1,0,1. (SEE HILDEBRAND, F.B.,
C INTRODUCTION TO NUMERICAL ANALYSIS, MC GRAW-HILL, NEW YORK/
C TORONTO/LONDON, 1956, PP. 64-68.)
C .....
SUBROUTINE DDGT3(X,Y,Z,NDIM,IER)
C
C DIMENSION X(1),Y(1),Z(1)
C DOUBLE PRECISION X,Y,Z,DY1,DY2,DY3,A,B
C
C TEST OF DIMENSION AND ERROR EXIT IN CASE NDIM IS LESS THAN 3
C IER=-1
C IF(NDIM-3)8,1,1
C
C PREPARE DIFFERENTIATION LOOP
C 1 A=X(1)
C B=Y(1)
C I=2
C DY2=X(2)-A
C IF(DY2)2,9,2
C 2 DY2=(Y(2)-B)/DY2
C
C START DIFFERENTIATION LOOP
C DO 4 I=3,NDIM
C A=X(I)-A
C IF(A)3,9,3
C 3 A=(Y(I)-B)/A
C B=X(I)-X(I-1)
C IF(B)4,9,4
C 4 DY1=DY2
C DY2=(Y(I)-Y(I-1))/B
C DY3=A
C A=X(I-1)
C B=Y(I-1)
C IF(I-3)5,5,6
C 5 Z(I)=DY1+DY3-DY2
C 6 Z(I-1)=DY1+DY2-DY3
C END OF DIFFERENTIATION LOOP
C
C NORMAL EXIT
C IER=0
C I=NDIM
C 7 Z(I)=DY2+DY3-DY1
C 8 RETURN
C
C ERROR EXIT IN CASE OF IDENTICAL ARGUMENTS
C 9 IER=1
C I=I-1
C IF(I-2)8,8,7
C END

```

Subroutines DET3 and DDET3

These subroutines compute a vector $Z = (z_1, \dots, z_n)$ of derivative values, given a vector $Y = (y_1, \dots, y_n)$ of function values whose entries y_i correspond to n equidistantly spaced argument values x_i , with $x_i - x_{i-1} = h$ for $i = 2, \dots, n$. Except at the end-points x_1 and x_n , z_i is the derivative at x_i of the Lagrangian interpolation polynomial of degree 2 relevant to the three successive points (x_{i-1}, y_{i-1}) , (x_i, y_i) , and (x_{i+1}, y_{i+1}) .

1. Mathematical background

The procedure is that described for subroutines DGT3 and DDGT3, but here we have the additional relation $x_i - x_{i-1} = h$, a constant, for $i = 2, \dots, n$. This leads to the following expression for the z_i :

$$z_i = \begin{cases} \frac{1}{2h} (-y_3 + 4y_2 - 3y_1) & \text{if } i=1 \\ \frac{1}{2h} (y_{i+1} - y_{i-1}) & \text{if } i=2, \dots, n-1 \\ \frac{1}{2h} (3y_n - 4y_{n-1} + y_{n-2}) & \text{if } i=n \end{cases} \quad (1)$$

Assuming that the vector Y represents the function values of a portion of a three-times differentiable function, z_i involves a truncation error T_i where:

$$T_i = \begin{cases} \frac{h^2}{3} y'''(\xi_1), \quad \xi_1 \in [x_1, x_3] & \text{if } i=1 \\ -\frac{h^2}{6} y'''(\xi_i), \quad \xi_i \in [x_{i-1}, x_{i+1}] & \text{if } i=2, \dots, n-1 \\ \frac{h^2}{3} y'''(\xi_n), \quad \xi_n \in [x_{n-2}, x_n] & \text{if } i=n \end{cases}$$

In addition to these truncation errors, roundoff errors may be of considerable magnitude. Supposing that each of the ordinates y_i can be in error by $\pm \epsilon$, $\epsilon > 0$, the magnitude $|R_i|$ of the corresponding error R_i in the calculation of z_i can be as large as:

$$|R_i| = \begin{cases} \frac{4\epsilon}{|h|} & \text{if } i=1, n \\ \frac{\epsilon}{|h|} & \text{if } i=2, \dots, n-1 \end{cases}$$

Since small truncation errors generally require small $|h|$, while small roundoff errors generally require large $|h|$, it is reasonable to choose h so that $|T_i| \approx |R_i|$.

If $M = \sup y'''(\xi)$, where $\xi \in [x_1, x_n]$, and if we regard only the inner points x_2, \dots, x_{n-1} , we find that

$$h_{\text{optimum}} \approx \pm 1.8 \sqrt[3]{\epsilon/M}$$

and the magnitude $|E_i|$ of the total possible error E_i in z_i is given by:

$$|E_i| \approx \begin{cases} 3.3 \sqrt[3]{\epsilon^2 M} & \text{if } i=1, n \\ 1.1 \sqrt[3]{\epsilon^2 M} & \text{if } i=2, \dots, n-1 \end{cases}$$

2. Programming considerations

The subroutines compute the z_i in serial order according to (1). If $n < 3$ or if $h = 0$, there is no computation, and the error parameter IER is set to -1 or 1 respectively. Otherwise IER is set to zero at the end of the computation. The output vector Z can have the same storage allocation as Y.

For reference see F. B. Hildebrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp. 82-84.

```

C ..... DET3 10
C ..... DET3 20
C ..... DET3 30
C ..... DET3 40
C ..... DET3 50
C ..... DET3 60
C ..... DET3 70
C ..... DET3 80
C ..... DET3 90
C ..... DET3 100
C ..... DET3 110
C ..... DET3 120
C ..... DET3 130
C ..... DET3 140
C ..... DET3 150
C ..... DET3 160
C ..... DET3 170
C ..... DET3 180
C ..... DET3 190
C ..... DET3 200
C ..... DET3 210
C ..... DET3 220
C ..... DET3 230
C ..... DET3 240
C ..... DET3 250
C ..... DET3 260
C ..... DET3 270
C ..... DET3 280
C ..... DET3 290
C ..... DET3 300
C ..... DET3 310
C ..... DET3 320
C ..... DET3 330
C ..... DET3 340
C ..... DET3 350
C ..... DET3 360
C ..... DET3 370
C ..... DET3 380
C ..... DET3 390
C ..... DET3 400
C ..... DET3 410
C ..... DET3 420
C ..... DET3 430
C ..... DET3 440
C ..... DET3 450
C ..... DET3 460
C ..... DET3 470
C ..... DET3 480
C ..... DET3 490
C ..... DET3 500
C ..... DET3 510
C ..... DET3 520
C ..... DET3 530
C ..... DET3 540
C ..... DET3 550
C ..... DET3 560
C ..... DET3 570
C ..... DET3 580
C ..... DET3 590
C ..... DET3 600
C ..... DET3 610
C ..... DET3 620
C ..... DET3 630
C ..... DET3 640
C ..... DET3 650
C ..... DET3 660
C ..... DET3 670
C ..... DET3 680
C ..... DET3 690
C ..... DET3 700
C ..... DET3 710
C ..... DET3 720
C ..... DET3 730
C ..... DET3 740
C ..... DET3 750
C ..... DET3 760
C ..... DET3 770
C ..... DET3 780
C ..... DET3 790
C ..... DET3 800
C ..... DET3 810
C ..... DET3 820
C ..... DET3 830
C ..... DET3 840
C ..... DET3 850
C ..... DET3 860

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C ..... DET3 690
C ..... DET3 700
C ..... DET3 710
C ..... DET3 720
C ..... DET3 730
C ..... DET3 740
C ..... DET3 750
C ..... DET3 760
C ..... DET3 770
C ..... DET3 780
C ..... DET3 790
C ..... DET3 800
C ..... DET3 810
C ..... DET3 820
C ..... DET3 830
C ..... DET3 840

```

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C ..... DET3 10
C ..... DET3 20
C ..... DET3 30
C ..... DET3 40
C ..... DET3 50
C ..... DET3 60
C ..... DET3 70
C ..... DET3 80
C ..... DET3 90
C ..... DET3 100
C ..... DET3 110
C ..... DET3 120
C ..... DET3 130
C ..... DET3 140
C ..... DET3 150
C ..... DET3 160
C ..... DET3 170
C ..... DET3 180
C ..... DET3 190
C ..... DET3 200
C ..... DET3 210
C ..... DET3 220
C ..... DET3 230
C ..... DET3 240
C ..... DET3 250
C ..... DET3 260
C ..... DET3 270
C ..... DET3 280
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C ..... DET3 300
C ..... DET3 310
C ..... DET3 320
C ..... DET3 330
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C ..... DET3 400
C ..... DET3 410
C ..... DET3 420
C ..... DET3 430
C ..... DET3 440
C ..... DET3 450
C ..... DET3 460
C ..... DET3 470
C ..... DET3 480
C ..... DET3 490
C ..... DET3 500
C ..... DET3 510
C ..... DET3 520
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C ..... DET3 540
C ..... DET3 550
C ..... DET3 560
C ..... DET3 570
C ..... DET3 580
C ..... DET3 590
C ..... DET3 600
C ..... DET3 610
C ..... DET3 620
C ..... DET3 630
C ..... DET3 640
C ..... DET3 650
C ..... DET3 660
C ..... DET3 670
C ..... DET3 680
C ..... DET3 690
C ..... DET3 700
C ..... DET3 710
C ..... DET3 720
C ..... DET3 730
C ..... DET3 740
C ..... DET3 750
C ..... DET3 760
C ..... DET3 770
C ..... DET3 780
C ..... DET3 790
C ..... DET3 800
C ..... DET3 810
C ..... DET3 820
C ..... DET3 830
C ..... DET3 840
C ..... DET3 850
C ..... DET3 860

```

Subroutines DET5 and DDET5

These subroutines compute a vector $Z = (z_1, \dots, z_n)$ of derivative values, given a vector $Y = (y_1, \dots, y_n)$ of function values whose entries y_i correspond to n equidistantly spaced argument values x_i , with $x_i - x_{i-1} = h$ for $i = 2, \dots, n$. Except at the points x_1, x_2, x_{n-1} , and x_n , z_i is the derivative at x_i of the Lagrangian interpolation polynomial of degree 4 relevant to the five successive points (x_{i+k}, y_{i+k}) , $k = -2, -1, \dots, 2$.

1. Mathematical background

For $i = 1, \dots, n-4$ we must find a_i, b_i, c_i, d_i , and e_i such that

$$\bar{y}_i(x) = a_i x^4 + b_i x^3 + c_i x^2 + d_i x + e_i$$

passes through (x_{i+k}, y_{i+k}) for $k = 0, \dots, 4$.

The desired derivative values z_i are given by:

$$z_i = \begin{cases} \bar{y}'_1(x_i) = 4a_1 x_i^3 + 3b_1 x_i^2 + 2c_1 x_i + d_1 & \text{if } i = 1, 2 \\ \bar{y}'_{i-2}(x_i) = 4a_{i-2} x_i^3 + 3b_{i-2} x_i^2 + 2c_{i-2} x_i + d_{i-2} & \text{if } i = 3, \dots, n-2 \\ \bar{y}'_{n-4}(x_i) = 4a_{n-4} x_i^3 + 3b_{n-4} x_i^2 + 2c_{n-4} x_i + d_{n-4} & \text{if } i = n-1, n \end{cases}$$

Using the fact that $x_i - x_{i-1} = h$, a constant, for $i = 2, \dots, n$, we get:

$$z_i = \begin{cases} \frac{1}{12h} (-25y_1 + 48y_2 - 36y_3 + 16y_4 - 3y_5) & \text{if } i = 1 \\ \frac{1}{12h} (-3y_1 - 10y_2 + 18y_3 - 6y_4 + y_5) & \text{if } i = 2 \\ \frac{1}{12h} (y_{i-2} - 8y_{i-1} + 8y_{i+1} - y_{i+2}) & \text{if } i = 3, \dots, n-2 \\ \frac{1}{12h} (-y_{n-4} + 6y_{n-3} - 18y_{n-2} + 10y_{n-1} + 3y_n) & \text{if } i = n-1 \\ \frac{1}{12h} (3y_{n-4} - 16y_{n-3} + 36y_{n-2} - 48y_{n-1} + 25y_n) & \text{if } i = n \end{cases} \quad (1)$$

Assuming that the vector Y represents the function values of a portion of a five-times differentiable function, z_i involves a truncation error T_i where:

$$T_i = \begin{cases} \frac{h^4}{5} y^v(\xi_1), \quad \xi_1 \in [x_1, x_5] & \text{if } i = 1 \\ -\frac{h^4}{20} y^v(\xi_2), \quad \xi_2 \in [x_1, x_5] & \text{if } i = 2 \\ \frac{h^4}{30} y^v(\xi_i), \quad \xi_i \in [x_{i-2}, x_{i+2}] & \text{if } i = 3, \dots, n-2 \\ -\frac{h^4}{20} y^v(\xi_{n-1}), \quad \xi_{n-1} \in [x_{n-4}, x_n] & \text{if } i = n-1 \\ \frac{h^4}{5} y^v(\xi_n), \quad \xi_n \in [x_{n-4}, x_n] & \text{if } i = n \end{cases}$$

In addition to the truncation errors, roundoff errors may be of considerable magnitude. Supposing that the ordinates y_i can be in error by $\pm \epsilon$, $\epsilon > 0$, the magnitude $|R_i|$ of the corresponding error R_i in the computation of z_i can be as large as:

$$|R_i| = \begin{cases} \frac{32\epsilon}{3|h|} & \text{if } i = 1, n \\ \frac{19\epsilon}{6|h|} & \text{if } i = 2, n-1 \\ \frac{3\epsilon}{2|h|} & \text{if } i = 3, \dots, n-2 \end{cases}$$

Since small truncation errors generally require small $|h|$, while small roundoff errors generally require large $|h|$, it is reasonable to choose h so that $|T_i| \approx |R_i|$.

If $M = \sup_{\xi \in [x_1, x_n]} y'(\xi)$, and if we regard only the inner points x_3, \dots, x_{n-2} , we find that

$$h_{\text{optimum}} \approx 2.1 \sqrt[5]{\epsilon/M}$$

and the magnitude $|E_i|$ of the total possible error E_i in z_i is given by:

$$|E_i| \approx \begin{cases} 9 \sqrt[5]{\epsilon^4 M} & \text{if } i=1, n \\ 2.5 \sqrt[5]{\epsilon^4 M} & \text{if } i=2, n-1 \\ 1.4 \sqrt[5]{\epsilon^4 M} & \text{if } i=3, \dots, n-2 \end{cases}$$

2. Programming considerations

The subroutines compute the z_i in serial order according to (1). If $n < 5$ or if $h = 0$, there is no computation, and the error parameter IER is set to -1 or 1, respectively. Otherwise IER is set to zero at the end of the computation. The output vector Z may have the same storage allocation as Y .

For reference see F. B. Hilderbrand, Introduction to Numerical Analysis. McGraw-Hill, New York/Toronto/London, 1956, pp. 82-84.

```

C .....DETS 10
C .....DETS 20
C .....DETS 30
C .....DETS 40
C .....DETS 50
C .....DETS 60
C .....DETS 70
C .....DETS 80
C .....DETS 90
C .....DETS 100
C .....DETS 110
C .....DETS 120
C .....DETS 130
C .....DETS 140
C .....DETS 150
C .....DETS 160
C .....DETS 170
C .....DETS 180
C .....DETS 190
C .....DETS 200
C .....DETS 210
C .....DETS 220
C .....DETS 230
C .....DETS 240
C .....DETS 250
C .....DETS 260
C .....DETS 270
C .....DETS 280
C .....DETS 290
C .....DETS 300
C .....DETS 310
C .....DETS 320
C .....DETS 330
C .....DETS 340
C .....DETS 350
C .....DETS 360
C .....DETS 370
C .....DETS 380
C .....DETS 390
C .....DETS 400
C .....DETS 410
C .....DETS 420
C .....DETS 430
C .....DETS 440
C .....DETS 450
C .....DETS 460
C .....DETS 470
C .....DETS 480
C .....DETS 490
C .....DETS 500
C .....DETS 510
C .....DETS 520
C .....DETS 530

```

```

C TEST OF STEPSIZE
C 1 IF(H)2,5,2
C .....DETS 540
C .....DETS 550
C .....DETS 560
C .....DETS 570
C .....DETS 580
C .....DETS 590
C .....DETS 600
C .....DETS 610
C .....DETS 620
C .....DETS 630
C .....DETS 640
C .....DETS 650
C .....DETS 660
C .....DETS 670
C .....DETS 680
C .....DETS 690
C .....DETS 700
C .....DETS 710
C .....DETS 720
C .....DETS 730
C .....DETS 740
C .....DETS 750
C .....DETS 760
C .....DETS 770
C .....DETS 780
C .....DETS 790
C .....DETS 800
C .....DETS 810
C .....DETS 820
C .....DETS 830
C .....DETS 840
C .....DETS 850
C .....DETS 860
C .....DETS 870
C .....DETS 880

```

```

C .....DETS 10
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C .....DETS 160
C .....DETS 170
C .....DETS 180
C .....DETS 190
C .....DETS 200
C .....DETS 210
C .....DETS 220
C .....DETS 230
C .....DETS 240
C .....DETS 250
C .....DETS 260
C .....DETS 270
C .....DETS 280
C .....DETS 290
C .....DETS 300
C .....DETS 310
C .....DETS 320
C .....DETS 330
C .....DETS 340
C .....DETS 350
C .....DETS 360
C .....DETS 370
C .....DETS 380
C .....DETS 390
C .....DETS 400
C .....DETS 410
C .....DETS 420
C .....DETS 430
C .....DETS 440
C .....DETS 450
C .....DETS 460
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C .....DETS 480
C .....DETS 490
C .....DETS 500
C .....DETS 510
C .....DETS 520
C .....DETS 530
C .....DETS 540
C .....DETS 550
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C .....DETS 570
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C .....DETS 590
C .....DETS 600
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C .....DETS 820
C .....DETS 830
C .....DETS 840
C .....DETS 850
C .....DETS 860
C .....DETS 870
C .....DETS 880
C .....DETS 890
C .....DETS 900
C .....DETS 910

```

Subroutines DCAR and DDCAR

Suppose that $y = y(t)$ is eleven-times differentiable in a neighborhood of radius $R > 0$ of the point x . These subroutines compute an approximation Z to $y'(x)$ by applying Richardson's and Romberg's extrapolation method to successively computed central divided differences, using function values in a closed interval of radius $|h|$ about the point x , $0 < |h| < R$.

1. Mathematical background

Suppose, first, that $y = y(t)$ is analytic at x ; that is, y has a Taylor series expansion about the point x with radius of convergence $R > 0$. Let h be such that $0 < |h| < R$. For each positive integer n a step size h_1 with $0 < h_1 \leq |h|$ is computed as described below, and a sequence h_k of increments is generated, where

$$h_k = \frac{n-k+1}{n} h_1 \quad \text{for } k=2, \dots, n.$$

From the sequence $(x-h_k, x+h_k)$ of point pairs ($k=1, \dots, n$), the sequence of central divided differences

$$T_{0,k} = \frac{y(x+h_k) - y(x-h_k)}{2h_k} \quad \text{for } k=1, \dots, n \quad (1)$$

is computed, which forms the first column of the triangular Romberg scheme. The central divided differences $T_{0,k}$ represent the slopes of the secants s_k in Figure 26.

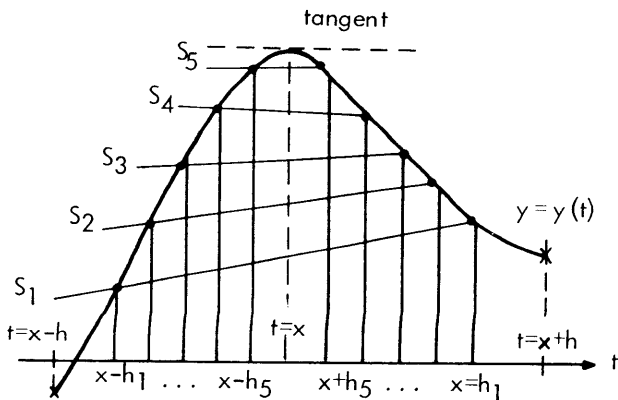


Figure 26. A sequence of secants for a given function $y = y(t)$ and a given argument $t = x$ for the case $n = 5, h > 0$

From the Taylor series expansions of $y(x+h_k)$ and $y(x-h_k)$ it follows that

$$T_{0,k} = y'(x) + \frac{h_k^2}{3!} y'''(x) + \frac{h_k^4}{5!} y^{(5)}(x) + \dots \quad \text{for } k=1, \dots, n$$

so that, as an approximation to $y'(x)$, $T_{0,k}$ involves a truncation error of order h_k^2 .

Knowing the two divided differences $T_{0,k}$ and $T_{0,k+1}$, we are able to generate the extrapolated value

$$T_{1,k} = T_{0,k+1} + \frac{T_{0,k+1} - T_{0,k}}{a_{1,k} - 1}$$

where (2)

$$a_{1,k} = \left(1 + \frac{1}{n-k}\right)^2$$

$T_{1,k}$ is a better approximation to $y'(x)$ since

$$T_{1,k} = y'(x) - \frac{1}{5!} \frac{1}{a_{1,k}} h_k^4 y^{(5)}(x)$$

$$- \frac{1}{7!} \frac{1}{a_{1,k}} \left(1 + \frac{1}{a_{1,k}}\right) h_k^6 y^{(7)}(x)$$

\dots , which involves a truncation error of order h_k^4 .

If we also know $T_{0,k+2}$, then we can generate $T_{1,k+1}$ using formula (2), and further, we can compute the extrapolated value

$$T_{2,k} = T_{1,k+1} + \frac{T_{1,k+1} - T_{1,k}}{a_{2,k} - 1}$$

where (3)

$$a_{2,k} = \left(1 + \frac{2}{n-(k+1)}\right)^2$$

which involves a truncation error of order h_k^6 .

Generally, the order of the truncation error is increased by 2 with each new extrapolation step; in particular, $T_{i,j}$ will involve a truncation error of order

$$h_j^{2i+2}, \quad i = 0, \dots, n-1, \quad j = 1, \dots, n.$$

Figure 27 shows the arrangement of the T -values in the triangular Romberg scheme. The T -values are computed following the upward diagonals, using the general formula:

$$T_{m, k-m} = T_{m-1, k-m+1} + \frac{T_{m-1, k-m+1} - T_{m-1, k-m}}{\frac{m}{n-(k+1)} \left(2 + \frac{m}{n-(k+1)}\right)}$$

for $m = 1, \dots, k-1$ for fixed $k, k = 2, \dots, n$

(4)

Truncation error		$O(h_k^2)$	$O(h_k^4)$	$O(h_k^6)$	$O(h_k^8)$	$O(h_k^{10})$
Stepsize	m k	0	1	2	3	4
		h_1	1	$T_{0,1}$	$T_{1,1}$	$T_{2,1}$
$h_2 = 0.8h_1$	2	$T_{0,2}$	$T_{1,2}$	$T_{2,2}$	$T_{3,2}$	
$h_3 = 0.6h_1$	3	$T_{0,3}$	$T_{1,3}$	$T_{2,3}$		
$h_4 = 0.4h_1$	4	$T_{0,4}$	$T_{1,4}$			
$h_5 = 0.2h_1$	5	$T_{0,5}$				

Figure 27. The triangular Romberg scheme of T-values for the case $n = 5$

Numerical experience shows that the accuracy of the results depends heavily on roundoff errors in the central divided differences $T_{0,k}$. Therefore, the choice of the absolutely smallest step size, h_n , is based on the following considerations.

Let

$$v = \begin{cases} 1 & \text{in single-precision computation} \\ 3 & \text{in double-precision computation} \end{cases}$$

$$h_0 = \min(n \cdot 10^{-v}, |h|)$$

Set

$$Y = \frac{1}{2}(y(x+h_0) + y(x-h_0))$$

and

$$T = \frac{1}{2}(y(x+h_0) - y(x-h_0))/h_0$$

Y and T are approximations to $y(x)$ and $y'(x)$, respectively.

Assuming that the errors in the function values $y(t)$ for $t \in [x-h, x+h]$ are bounded by

$$\epsilon = \begin{cases} Y \cdot 10^{-D} & \text{if } |Y| > 1 \\ 10^{-D} & \text{if } |Y| \leq 1 \end{cases}$$

formula (1) shows that the roundoff error in the computation of $T_{0,n}$ is bounded by

$$R(T_{0,n}) = \frac{\epsilon}{h_n} = \begin{cases} \frac{Y \cdot 10^{-D}}{h_n} & \text{if } |Y| > 1 \\ \frac{10^{-D}}{h_n} & \text{if } |Y| \leq 1 \end{cases}$$

where D is the number of significant digits in the floating-point representation of numbers. Suppose, also, that we are willing to tolerate a roundoff error

$$R'(T_{0,n}) = \begin{cases} T \cdot 10^{-D+v} & \text{if } |T| > 1 \\ 10^{-D+v} & \text{if } |T| \leq 1 \end{cases}$$

Then we must have $R(T_{0,n}) \leq R'(T_{0,n})$, which is satisfied when

$$h_n = \frac{\max(1, |Y|)}{\max(1, |T|)} \cdot 10^{-v} \quad (5)$$

Finally we set

$$h_1 = \min(n \cdot h_n, |h|) \quad (6)$$

guaranteeing that the evaluation of the function $y = y(t)$ is restricted to the closed interval $[x-h, x+h]$.

2. Programming considerations

Numerical experience shows that, because of increasing roundoff errors, it is generally fruitless to perform more than five extrapolations. Thus, the subroutines use $n = 5$, and consequently it is only necessary that $y = y(t)$ be eleven-times differentiable, rather than analytic. It is easy to see that in the case $n = 5$, $y = y(t)$ must be evaluated at twelve points in the closed interval $[x-h, x+h]$.

The parameter lists of both subroutines contain the decision parameter IH. If the user wants the maximum step size to equal $|h|$, he must set $IH = 0$. In all other cases ($IH \neq 0$) the procedure determines the maximum step size by itself, using formulas (5) and (6) with $n = 5$. Step size h_1 and all the other step sizes h_k ($k = 2, \dots, 5$) are successively stored in the single storage location HH.

As previously explained, the computation of the T-values is performed along the upward diagonals of the triangular Romberg scheme. Therefore, only a one-dimensional internal storage vector,

named AUX, with five storage locations is necessary. Figure 28 shows the storage administration and the sequence of computations (numbers in parentheses).

AUX(1)	T _{0,5} (11)				
AUX(2)	T _{0,4} (7)	T _{1,4} (12)			
AUX(3)	T _{0,3} (4)	T _{1,3} (8)	T _{2,3} (13)		
AUX(4)	T _{0,2} (2)	T _{1,2} (5)	T _{2,2} (9)	T _{3,2} (14)	
AUX(5)	T _{0,1} (1)	T _{1,1} (3)	T _{2,1} (6)	T _{3,1} (10)	T _{4,1} (15)

Figure 28. Storage administration and order of computation

Each extrapolation loop, the computation of the elements on an upward diagonal, is terminated as soon as the absolute values of the differences between adjacent diagonal elements stop decreasing, showing the influence of roundoff errors. The computed T-value that differs least in absolute value from its immediately preceding diagonal neighbor is the desired value Z.

3. Accuracy of results

Tests of the single-precision (double-precision) subroutine on the functions $y(t) = t^2$, $1/t$, e^t , $\tan t$, and $\sin t$ showed that the accuracy obtained using the step size determined by the subroutine was 3-4 (11-12) significant digits near poles, 5-6(13-14) decimal places near points with horizontal tangents, and 5-6(13-14) significant digits otherwise.

For reference see S. Fillipi and H. Engels, "Altes und Neues zur numerischen Differentiation," *Elektronische Datenverarbeitung*, iss. 2(1966) pp. 57-65.

```

C
C
C
C -----
C          SUBROUTINE DCAR
C          DCAR 17
C          DCAR 20
C          DCAR 30
C          DCAR 40
C          DCAR 50
C          DCAR 60
C          DCAR 70
C          DCAR 80
C          DCAR 90
C          DCAR 100
C          DCAR 110
C          DCAR 120
C          DCAR 130
C          DCAR 140
C          DCAR 150
C          DCAR 160
C          DCAR 170
C          DCAR 180
C          DCAR 190
C          DCAR 200
C          DCAR 210
C          DCAR 220
C          DCAR 230
C          DCAR 240
C          DCAR 250
C          DCAR 260
C          DCAR 270
C          DCAR 280
C          DCAR 290
C          DCAR 300
C          DCAR 310
C          DCAR 320
C          DCAR 330
C          DCAR 340
C          DCAR 350
C          DCAR 360
C          DCAR 370
C          DCAR 380
C          DCAR 390
C          DCAR 400
C          DCAR 410
C          DCAR 420
C          DCAR 430
C          DCAR 440
C          DCAR 450
C          DCAR 460
C          DCAR 470
C          DCAR 480
C          DCAR 490
C          DCAR 500
C          DCAR 510
C          DCAR 520
C          DCAR 530
C          DCAR 540
C          DCAR 550
C          DCAR 560
C          DCAR 570
C          DCAR 580
C          DCAR 590
C          DCAR 600
C          DCAR 610
C          DCAR 620
C          DCAR 630
C          DCAR 640
C          DCAR 650
C          DCAR 660
C          DCAR 670
C          DCAR 680
C          DCAR 690
C          DCAR 700
C          DCAR 710
C          DCAR 720
C          DCAR 730
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C          DCAR 750
C          DCAR 760
C          DCAR 770
C          DCAR 780
C          DCAR 790
C          DCAR 800
C          DCAR 810
C          DCAR 820
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C          DCAR 840
C          DCAR 850
C          DCAR 860
C          DCAR 870
C          DCAR 880
C          DCAR 890
C          DCAR 900
C          DCAR 910
C          DCAR 920
C          DCAR 930
C          DCAR 940
C          DCAR 950
C          DCAR 960
C          DCAR 970
C          DCAR 980
C          DCAR 990
C          DCAR1000
C          DCAR1010
C          DCAR1020
C          DCAR1030
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C          DCAR1050
C          DCAR1060
C          DCAR1070
C          DCAR1080
C          DCAR1090
C          DCAR1100
C          DCAR1110
C          DCAR1120
C          DCAR1130
C          DCAR1140
C          DCAR1150
C          DCAR1160
C          DCAR1170
C          DCAR1180
C          DCAR1190
C          DCAR1200
C          DCAR1210
C          DCAR1220
C          DCAR1230
C          DCAR1240
C
C          PURPOSE
C          TO COMPUTE, AT A GIVEN POINT X, AN APPROXIMATION Z TO THE
C          DERIVATIVE OF AN ANALYTICALLY GIVEN FUNCTION FCT THAT IS 11-
C          TIMES DIFFERENTIABLE IN A DOMAIN CONTAINING A CLOSED, 2-SIDED
C          SYMMETRIC INTERVAL OF RADIUS ABSOLUTE H ABOUT X, USING FUNCTION
C          VALUES ONLY ON THAT CLOSED INTERVAL.
C
C          USAGE
C          CALL DCAR (X,H,HH,FCT,Z)
C          PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
C
C          DESCRIPTION OF PARAMETERS
C          X - THE POINT AT WHICH THE DERIVATIVE IS TO BE COMPUTED
C          H - THE NUMBER WHOSE ABSOLUTE VALUE DEFINES THE CLOSED,
C          SYMMETRIC 2-SIDED INTERVAL ABOUT X (SEE PURPOSE)
C          HH - INPUT PARAMETER (SEE REMARKS AND METHOD)
C          HH NON-ZERO - THE SUBROUTINE GENERATES THE INTERNAL
C          VALUE HH
C          HH = 0 - THE INTERNAL VALUE HH IS SET TO ABSOLUTE H
C          FCT - THE NAME OF THE EXTERNAL FUNCTION SUBPROGRAM THAT WILL
C          GENERATE THE NECESSARY FUNCTION VALUES
C          Z - RESULTING DERIVATIVE VALUE
C
C          REMARKS
C          (1) IF H = 0, THEN THERE IS NO COMPUTATION.
C          (2) THE INTERNAL VALUE HH, WHICH IS DETERMINED ACCORDING TO
C          THE CENTRAL DIVIDED DIFFERENCES (SEE METHOD.) IF HH IS
C          NON-ZERO, THEN THE SUBROUTINE GENERATES HH ACCORDING TO
C          CRITERIA THAT BALANCE ROUND-OFF AND TRUNCATION ERROR. HH
C          IS ALWAYS LESS THAN OR EQUAL TO ABSOLUTE H IN ABSOLUTE
C          VALUE, SO THAT ALL COMPUTATION OCCURS WITHIN A RADIUS
C          ABSOLUTE H OF X.
C
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C          THE EXTERNAL FUNCTION SUBPROGRAM FCT(I) MUST BE FURNISHED BY
C          THE USER.
C
C          METHOD
C          THE COMPUTATION OF Z IS BASED ON RICHARDSON'S AND ROMBERG'S
C          EXTRAPOLATION METHOD AS APPLIED TO THE SEQUENCE OF CENTRAL
C          DIVIDED DIFFERENCES ASSOCIATED WITH THE POINT PAIRS
C          (X-(K*HH)/5, X+(K*HH)/5) K=1,...,5. (SEE FILLIPI, S., AND
C          ENGELS, H., ALTES UND NEUES ZUR NUMERISCHEN DIFFERENTIATION,
C          ELEKTRONISCHE DATENVERARBEITUNG, ISS. 2 (1966), PP. 57-65.)
C
C          SUBROUTINE DCAR(X,H,HH,FCT,Z)
C
C          DIMENSION AUX(5)
C
C          NO ACTION IN CASE OF ZERO INTERVAL LENGTH
C          IF(H)17,17
C
C          GENERATE STEPSIZE HH FOR DIVIDED DIFFERENCES
C          1 C=ABS(H)
C          IF(C)2,9,2
C          2 HH=.5
C          IF(C-HH)3,4,4
C          3 HH=C
C          4 A=FCT(X+HH)
C          B=FCT(X-HH)
C          Z=ABS((A-B)/(HH+HH))
C          A=.5*ABS(A+B)
C          HH=.5
C          IF(A-.1,16,6,6,5
C          5 HH=HH*A
C          6 IF(Z-.1,18,8,7
C          7 HH=HH/Z
C          8 IF(HH-C)10,10,9
C          9 HH=C
C
C          INITIALIZE DIFFERENTIATION LOOP
C          10 Z=(FCT(X+HH)-FCT(X-HH))/(HH+HH)
C          J=5
C          JJ=J-1
C          AUX(J)=Z
C          DH=HH/FL(OAT(J))
C          DZ=1.E75
C
C          START DIFFERENTIATION LOOP
C          11 J=J-1
C          C=J
C          HH=C*DH
C          AUX(J)=(FCT(X+HH)-FCT(X-HH))/(HH+HH)
C
C          INITIALIZE EXTRAPOLATION LOOP
C          DZ=1.E75
C          B=0.
C          A=1./C
C
C          START EXTRAPOLATION LOOP
C          DO 12 I=J,JJ
C          D1=DZ
C          B=B+A
C          HH=(AUX(I)-AUX(I+1))/(B*(2.+B))
C          AUX(I+1)=AUX(I)+HH
C
C          TEST ON OSCILLATING INCREMENTS
C          DZ=ABS(HH)
C          IF(DZ-D1)12,13,13
C          12 CONTINUE
C          END OF EXTRAPOLATION LOOP
C          UPDATE RESULT VALUE Z
C          I=JJ+1
C          GO TO 14
C          13 DZ=D1
C          JJ=I
C          14 IF(DZ-D1)15,16,16
C          15 DZ=D2
C          Z=AUX(I)
C          16 IF(J-1)17,17,11
C          END OF DIFFERENTIATION LOOP
C
C          17 RETURN
C          END

```

```

C          DDCA 10
C          ----- DDCA 20
C          DDCA 30
C          DDCA 40
C          DDCA 50
C          DDCA 60
C          DDCA 70
C          DDCA 80
C          DDCA 90
C          DDCA 100
C          DDCA 110
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```

Subroutines DBAR and DDBAR

Suppose that $y = y(t)$ is eleven-times differentiable in a neighborhood of radius $R > 0$ of the point x . These subroutines compute an approximation Z to $y'(x)$ by applying Richardson's and Romberg's extrapolation method to successively computed one-sided divided differences, using function values in a closed interval $[x, x+h]$, $0 < |h| < R$.

1. Mathematical background

Suppose, first, that $y = y(t)$ is analytic at x ; that is, y has a Taylor series expansion about the point x with radius of convergence $R > 0$. Let h be such that $0 < |h| < R$. For each positive integer n , a step size h_1 with $0 < |h_1| \leq |h|$ is computed as described below, and a sequence h_k of increments is generated, where

$$h_k = \frac{n-k+1}{n} h_1$$

for $k = 2, \dots, n$.

From the sequence $(x, x+h_k)$ of point pairs ($k = 1, \dots, n$), the sequence of one-sided divided differences

$$T_{0,k} = \frac{y(x+h_k) - y(x)}{h_k} \quad \text{for } k = 1, \dots, n \quad (1)$$

is computed, which forms the first column of the triangular Romberg scheme. These one-sided divided differences $T_{0,k}$ represent the slopes of the secants s_k in Figure 29, in the case $h > 0$.

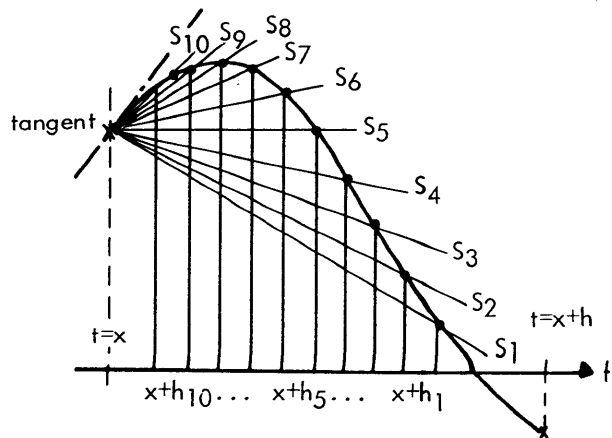


Figure 29. A sequence of secants for a given function $y = y(t)$ and a given argument $t = x$ for the case $n = 10$, $h > 0$

From the Taylor series expansion of $y(x+h_k)$ it follows that

$$T_{0,k} = y'(x) + \frac{h_k}{2!} y''(x) + \frac{h_k^2}{3!} y'''(x) + \dots \text{ for } k=1, \dots, n$$

so that, as an approximation to $y'(x)$, $T_{0,k}$ involves a truncation error of order h_k . Knowing the two divided differences $T_{0,k}$ and $T_{0,k+1}$, we are able to generate the extrapolated value

$$T_{1,k} = T_{0,k+1} + \frac{T_{0,k+1} - T_{0,k}}{a_{1,k} - 1}$$

where

$$a_{1,k} = \left(1 + \frac{1}{n-k}\right)$$

$T_{1,k}$ is a better approximation to $y'(x)$ since

$$T_{1,k} = y'(x) = \frac{1}{3!} \frac{1}{a_{1,k} - 1} h_k^2 y'''(x)$$

$$- \frac{1}{4!} \frac{1}{a_{1,k}} \left(1 + \frac{1}{a_{1,k}}\right) h_k^3 y^{iv}(x)$$

..., which involves a truncation error of order h_k^2 .

If we also know $T_{0,k+2}$, then we can generate

$T_{1,k+1}$ using formula (2), and further, we can compute the extrapolated value

$$T_{2,k} = T_{1,k+1} + \frac{T_{1,k+1} - T_{1,k}}{a_{2,k} - 1}$$

where

$$a_{2,k} = \left(1 + \frac{2}{n-(k+1)}\right)$$

which involves a truncation error of order h_k^3 .

Generally, the order of the truncation error is increased by 1 with each new extrapolation step; in particular, $T_{i,j}$ will involve a truncation error of order

$$h_j^{i+1}, \quad i = 0, \dots, n-1, \quad j = 1, \dots, n.$$

Figure 30 shows the arrangement of the T-values in the triangular Romberg scheme. The T-values are computed following the upward diagonals, using the general formula

$$T_{m,k-m} = T_{m-1,k-m+1} + \frac{T_{m-1,k-m+1} - T_{m-1,k-m}}{\frac{m}{n-k+1}}$$

for $m = 1, \dots, k-1$ for fixed k , $k = 2, \dots, n$

(3)

Truncation error		$O(h_k)$	$O(h_k^2)$	$O(h_k^3)$	$O(h_k^4)$	$O(h_k^5)$	$O(h_k^6)$	$O(h_k^7)$	$O(h_k^8)$	$O(h_k^9)$	$O(h_k^{10})$
Stepsize	m	0	1	2	3	4	5	6	7	8	9
	k										
h_1	1	$T_{0,1}$	$T_{1,1}$	$T_{2,1}$	$T_{3,1}$	$T_{4,1}$	$T_{5,1}$	$T_{6,1}$	$T_{7,1}$	$T_{8,1}$	$T_{9,1}$
$h_2=0.9h_1$	2	$T_{0,2}$	$T_{1,2}$	$T_{2,2}$	$T_{3,2}$	$T_{4,2}$	$T_{5,2}$	$T_{6,2}$	$T_{7,2}$	$T_{8,2}$	
$h_3=0.8h_1$	3	$T_{0,3}$	$T_{1,3}$	$T_{2,3}$	$T_{3,3}$	$T_{4,3}$	$T_{5,3}$	$T_{6,3}$	$T_{7,3}$		
$h_4=0.7h_1$	4	$T_{0,4}$	$T_{1,4}$	$T_{2,4}$	$T_{3,4}$	$T_{4,4}$	$T_{5,4}$	$T_{6,4}$			
$h_5=0.6h_1$	5	$T_{0,5}$	$T_{1,5}$	$T_{2,5}$	$T_{3,5}$	$T_{4,5}$	$T_{5,5}$				
$h_6=0.5h_1$	6	$T_{0,6}$	$T_{1,6}$	$T_{2,6}$	$T_{3,6}$	$T_{4,6}$					
$h_7=0.4h_1$	7	$T_{0,7}$	$T_{1,7}$	$T_{2,7}$	$T_{3,7}$						
$h_8=0.3h_1$	8	$T_{0,8}$	$T_{1,8}$	$T_{2,8}$							
$h_9=0.2h_1$	9	$T_{0,9}$	$T_{1,9}$								
$h_{10}=0.1h_1$	10	$T_{0,10}$									

Figure 30. The triangular Romberg scheme of T-values for the case $n = 10$

Numerical experience shows that the accuracy of the results depends heavily on roundoff errors in the one-sided divided differences $T_{0,k}$. Therefore, the choice of the absolutely smallest step size, h_n , is based on the following considerations.

Let

$$v = \begin{cases} 1 & \text{in single-precision computation} \\ 3 & \text{in double-precision computation} \end{cases}$$

Set

$$n_0 = \text{sgn}(h) \cdot \min\left(\frac{n}{2} \cdot 10^{-v}, |h|\right)$$

$$T = (y(x+h_0) - y(x))/h_0.$$

T is an approximation to $y'(x)$.

Assuming that the errors in the function values $y(t)$ for $t \in [x, x+h]$ are bounded by

$$\epsilon = \begin{cases} |y(x)| \cdot 10^{-D} & \text{if } |y(x)| > 1 \\ 10^{-D} & \text{if } |y(x)| \leq 1 \end{cases}$$

formula (1) shows that the roundoff error in the computation of $T_{0,n}$ is bounded by

$$R(T_{0,n}) = \frac{2\epsilon}{|h_n|} = \begin{cases} \frac{2|y(x)| \cdot 10^{-D}}{|h_n|} & \text{if } |y(x)| > 1 \\ 2 \frac{10^{-D}}{|h_n|} & \text{if } |y(x)| \leq 1 \end{cases}$$

where D is the number of significant digits in the floating-point representation of numbers. Suppose, also, that we are willing to tolerate a roundoff error

$$R'(T_{0,n}) = \begin{cases} 2T \cdot 10^{-D+v} & \text{if } |T| > 1 \\ 2 \cdot 10^{-D+v} & \text{if } |T| \leq 1 \end{cases}$$

Then we must have $R(T_{0,n}) \leq R'(T_{0,n})$, which is satisfied when

$$h_n = \frac{\max(1, |y(x)|)}{\max(1, |T|)} \cdot 10^{-v} \quad (4)$$

Finally, we set

$$h_1 = \text{sgn}(h) \cdot \min(n \cdot |h_n|, |h|) \quad (5)$$

guaranteeing that the evaluation of the function $y = y(t)$ is restricted to the closed interval $[x, x+h]$.

2. Programming considerations

Numerical experience shows that, because of increasing roundoff errors, it is generally fruitless to perform more than ten extrapolations. Thus, the

subroutines use $n = 10$, and consequently, it is only necessary that $y = y(t)$ be eleven-times differentiable, rather than analytic. It is easy to see that in the case $n = 10$, $y = y(t)$ must be evaluated at twelve points in the closed interval $[x, x+h]$.

The parameter lists of both subroutines contain the decision parameter IH . If the user wants the maximum step size to equal $|h|$, he must set $IH = 0$. In all other cases ($IH \neq 0$) the procedure determines the maximum step size by itself, using formulas (4) and (5) with $n = 10$. Step size h_1 and all the other step sizes h_k ($k = 2, \dots, 10$) are successively stored in the single storage location HH .

As previously explained, the computation of the T -values is performed along the upward diagonals of the triangular Romberg scheme. Therefore, only a one-dimensional internal storage vector, named AUX , with ten storage locations is necessary. Figure 31 shows the storage administration and the sequence of computations (numbers in parentheses).

AUX(1)	$T_{0,10}^{(46)}$			
AUX(2)	$T_{0,9}^{(37)}$	$T_{1,9}^{(47)}$		
AUX(3)	$T_{0,8}^{(29)}$	$T_{1,8}^{(38)}$	$T_{2,8}^{(48)}$	
AUX(4)	$T_{0,7}^{(22)}$	$T_{1,7}^{(30)}$	$T_{2,7}^{(39)}$...
AUX(5)	$T_{0,6}^{(16)}$	$T_{1,6}^{(23)}$	$T_{2,6}^{(31)}$...
AUX(6)	$T_{0,5}^{(11)}$	$T_{1,5}^{(17)}$	$T_{2,5}^{(24)}$...
AUX(7)	$T_{0,4}^{(7)}$	$T_{1,4}^{(12)}$	$T_{2,4}^{(18)}$...
AUX(8)	$T_{0,3}^{(4)}$	$T_{1,3}^{(8)}$	$T_{2,3}^{(13)}$...
AUX(9)	$T_{0,2}^{(2)}$	$T_{1,2}^{(5)}$	$T_{2,2}^{(9)}$...
AUX(10)	$T_{0,1}^{(1)}$	$T_{1,1}^{(3)}$	$T_{2,1}^{(6)}$...

$T_{7,3}^{(53)}$		
$T_{7,2}^{(44)}$	$T_{8,2}^{(54)}$	
$T_{7,1}^{(36)}$	$T_{8,1}^{(45)}$	$T_{9,1}^{(55)}$

Figure 31. Storage administration and sequence of calculations

Each extrapolation loop, the computation of the elements on an upward diagonal, is terminated as soon as the absolute values of the differences between adjacent diagonal elements stop decreasing, showing the influence of roundoff errors. The computed T -value that differs least in absolute value from its immediately preceding diagonal neighbor is the desired value Z .

3. Accuracy of results

Tests of the single-precision (double-precision) subroutine on the functions $y(t) = t^2$, $1/t$, e^t , $\tan t$, and $\sin t$ showed that the accuracy obtained using the step size determined by the subroutine was 2-4 (10-12) significant digits near poles, 4-6(13-14) decimal places near points with horizontal tangents, and 4-6(11-13) significant digits otherwise.

For reference see S. Fillipi and H. Engles, "Altes und Neues zur numerischen Differentiation," *Elektronische Datenverarbeitung*, iss. 2 (1966) pp. 57-65.

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SUBROUTINE DBAR
PURPOSE
  TO COMPUTE, AT A GIVEN POINT X, AN APPROXIMATION Z TO THE
  DERIVATIVE OF AN ANALYTICALLY GIVEN FUNCTION FCT THAT IS 11-
  TIMES DIFFERENTIABLE IN A DOMAIN CONTAINING A CLOSED INTERVAL
  THE SET OF T BETWEEN X AND X+H (H POSITIVE OR NEGATIVE) - USING
  FUNCTION VALUES ONLY ON THAT INTERVAL.
USAGE
  CALL DBAR(X,H,HH,FCT,Z)
  PARAMETER FCT REQUIRES AN EXTERNAL STATEMENT
DESCRIPTION OF PARAMETERS
  X - THE POINT AT WHICH THE DERIVATIVE IS TO BE COMPUTED
  H - THE NUMBER THAT DEFINES THE CLOSED INTERVAL WHOSE END-
  POINTS ARE X AND X+H (SEE PURPOSE)
  HH - INPUT PARAMETER (SEE REMARKS AND METHOD)
  HH NON-ZERO - THE SUBROUTINE GENERATES THE INTERNAL
  VALUE HH
  HH = 0 - THE INTERNAL VALUE HH IS SET TO H
  FCT - THE NAME OF THE EXTERNAL FUNCTION SUBPROGRAM THAT WILL
  GENERATE THE NECESSARY FUNCTION VALUES
  Z - RESULTING DERIVATIVE VALUE
REMARKS
  (1) IF H = 0, THEN THERE IS NO COMPUTATION.
  (2) THE (MAGNITUDE OF THE) INTERNAL VALUE HH, WHICH IS DETER-
  MINED ACCORDING TO HH, IS THE MAXIMUM STEP-SIZE USED IN
  THE COMPUTATION OF THE ONE-SIDED DIVIDED DIFFERENCES (SEE
  METHOD.) IF HH IS NON-ZERO, THEN THE SUBROUTINE GENERATES
  HH ACCORDING TO CRITERIA THAT BALANCE ROUND-OFF AND TRUN-
  CATION ERROR. HH ALWAYS HAS THE SAME SIGN AS H AND IT IS
  ALWAYS LESS THAN OR EQUAL TO THE MAGNITUDE OF H IN AB-
  SOLUTE VALUE, SO THAT ALL COMPUTATION OCCURS IN THE CLOSED
  INTERVAL DETERMINED BY H.
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  THE EXTERNAL FUNCTION SUBPROGRAM FCT(IT) MUST BE FURNISHED BY
  THE USER.
METHOD
  THE COMPUTATION OF Z IS BASED ON RICHARDSON'S AND ROMBERG'S
  EXTRAPOLATION METHOD AS APPLIED TO THE SEQUENCE OF ONE-SIDED
  DIVIDED DIFFERENCES ASSOCIATED WITH THE POINT PAIRS
  (X, X+(K*HH)/10) K=1, ..., 10. (SEE FILLIPT, S. AND ENGELS, H.,
  ALTES UND NEUES ZUR NUMERISCHEN DIFFERENTIATION, ELECTRONISCHE
  DATENVERARBEITUNG, ISS. 2 (1966), PP. 57-65.)
SUBROUTINE DBAR(X,H,HH,FCT,Z)
DIMENSION AUX(10)
  NO ACTION IN CASE OF ZERO INTERVAL LENGTH
  IF(H)1,17,1
  GENERATE STEPSIZE HH FOR DIVIDED DIFFERENCES
  1 C=ABS(H)
  B=H
  D=X
  D=FCT(D)
  IF(I)2,9,2
  2 HH=.5
  IF(C-HH)3,4,4
  3 HH=B
  4 HH=SIGN(HH,B)
  Z=ABS(FCT(X+HH)-D)/HH
  A=ABS(D)
  HH=1.
  IF(A-.1)6,6,5
  5 HH=HH*A
  6 IF(Z-.1)8,8,7
  7 HH=HH/Z
  8 IF(HH-C)10,10,9
  9 HH=B
  10 HH=SIGN(HH,B)
  INITIALIZE DIFFERENTIATION LOOP
  Z=(FCT(X+HH)-D)/HH
  J=10
  JJ=J-1
  AUX(J)=Z
  DH=HH/DFLOAT(J)
  DZ=1.E75
  START DIFFERENTIATION LOOP
  11 J=J-1
  C=J
  HH=C*DH
  AUX(J)=(FCT(X+HH)-D)/HH
  INITIALIZE EXTRAPOLATION LOOP
  DZ=1.E75
  R=0
  A=1./C
  START EXTRAPOLATION LOOP
  DO 12 I=J,1
  D1=D2
  B=B*A
  HH=(AUX(I)-AUX(I+1))/B
  AUX(I+1)=AUX(I)+HH
  TEST ON OSCILLATING INCREMENTS
  D2=ABS(HH)
  IF(D2-D1)12,13,13
  12 CONTINUE
  END OF EXTRAPOLATION LOOP
  UPDATE RESULT VALUE Z
  I=J+1
  GO TO 14
  13 D2=D1
  JJ=J
  14 IF(D2-D1)15,16,16
  15 D2=D2
  Z=AUX(I)
  16 IF(J-1)17,17,11
  END OF DIFFERENTIATION LOOP
  17 RETURN
  END

```

Ordinary Differential Equations

Subroutine RK1

This subroutine integrates a given function using the Runge-Kutta technique and produces the final computed value of the integral.

The ordinary differential equation:

$$\frac{dy}{dx} = f(x, y) \tag{1}$$

with initial condition $y(x_0) = y_0$ is solved numerically using a fourth-order Runge-Kutta integration process. This is a single-step method in which the value of y at $x = x_n$ is used to compute $y_{n+1} = y(x_{n+1})$ and earlier values y_{n-1}, y_{n-2} , etc. are not used.

The relevant formulas are:

$$y_{n+1} = y_n + 1/6 [k_0 + 2k_1 + 2k_2 + k_3] \tag{2}$$

where, for step size h :

$$\begin{cases} k_0 = hf(x_n, y_n) \\ k_1 = hf(x_n + h/2, y_n + k_0/2) \\ k_2 = hf(x_n + h/2, y_n + k_1/2) \\ k_3 = hf(x_n + h, y_n + k_2) \end{cases} \tag{3}$$

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C .....RK1 510
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C .....RK1 530
C .....RK1 540

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C .....C IN COLUANA 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION STATEMENT WHICH FOLLOWS.
C .....C .....RK1 550
C .....C .....RK1 560
C .....C .....RK1 570
C .....C .....RK1 580
C .....C .....RK1 590
C .....C .....RK1 600
C .....C .....RK1 610
C .....C .....RK1 620
C .....C .....RK1 630
C .....C .....RK1 640
C .....C .....RK1 650
C .....C .....RK1 660
C .....C .....RK1 670
C .....C .....RK1 680
C .....C .....RK1 690
C .....C .....RK1 700
C .....C .....RK1 705
C .....C .....RK1 710
C .....C .....RK1 720
C .....C .....RK1 730
C .....C .....RK1 740
C .....C .....RK1 750
C .....C .....RK1 760
C .....C .....RK1 770
C .....C .....RK1 780
C .....C .....RK1 790
C .....C .....RK1 800
C .....C .....RK1 810
C .....C .....RK1 820
C .....C .....RK1 830
C .....C .....RK1 840
C .....C .....RK1 850
C .....C .....RK1 860
C .....C .....RK1 870
C .....C .....RK1 880
C .....C .....RK1 890
C .....C .....RK1 900
C .....C .....RK1 910
C .....C .....RK1 920
C .....C .....RK1 930
C .....C .....RK1 940
C .....C .....RK1 950
C .....C .....RK1 960
C .....C .....RK1 970
C .....C .....RK1 980
C .....C .....RK1 990
C .....C .....RK1 1000
C .....C .....RK1 1010
C .....C .....RK1 1020
C .....C .....RK1 1030
C .....C .....RK1 1040
C .....C .....RK1 1050
C .....C .....RK1 1060
C .....C .....RK1 1070
C .....C .....RK1 1080
C .....C .....RK1 1090
C .....C .....RK1 1100
C .....C .....RK1 1110
C .....C .....RK1 1120
C .....C .....RK1 1130
C .....C .....RK1 1140
C .....C .....RK1 1150
C .....C .....RK1 1160
C .....C .....RK1 1170
C .....C .....RK1 1180
C .....C .....RK1 1190
C .....C .....RK1 1200
C .....C .....RK1 1210
C .....C .....RK1 1220
C .....C .....RK1 1230
C .....C .....RK1 1240
C .....C .....RK1 1250
C .....C .....RK1 1260
C .....C .....RK1 1270
C .....C .....RK1 1280
C .....C .....RK1 1290
C .....C .....RK1 1300
C .....C .....RK1 1310
C .....C .....RK1 1320
C .....C .....RK1 1330
C .....C .....RK1 1340
C .....C .....RK1 1350
C .....C .....RK1 1360
C .....C .....RK1 1370
C .....C .....RK1 1380
C .....C .....RK1 1390
C .....C .....RK1 1400
C .....C .....RK1 1410
C .....C .....RK1 1420
C .....C .....RK1 1430
C .....C .....RK1 1440
C .....C .....RK1 1450
C .....C .....RK1 1460
C .....C .....RK1 1470
C .....C .....RK1 1480
C .....C .....RK1 1490
C .....C .....RK1 1500
C .....C .....RK1 1510
C .....C .....RK1 1520
C .....C .....RK1 1530
C .....C .....RK1 1540
C .....C .....RK1 1550
C .....C .....RK1 1560
C .....C .....RK1 1570
C .....C .....RK1 1580
C .....C .....RK1 1590
C .....C .....RK1 1600
C .....C .....RK1 1610
C .....C .....RK1 1620
C .....C .....RK1 1630
C .....C .....RK1 1640
C .....C .....RK1 1650
C .....C .....RK1 1660
C .....C .....RK1 1670
C .....C .....RK1 1680
C .....C .....RK1 1690
C .....C .....RK1 1700
C .....C .....RK1 1710
C .....C .....RK1 1720
C .....C .....RK1 1730
C .....C .....RK1 1740
C .....C .....RK1 1750
C .....C .....RK1 1760
C .....C .....RK1 1770
C .....C .....RK1 1780
C .....C .....RK1 1790
C .....C .....RK1 1800
C .....C .....RK1 1810
C .....C .....RK1 1820
C .....C .....RK1 1830
C .....C .....RK1 1840

```

Subroutine RK2

This subroutine integrates a given function using the Runge-Kutta technique and produces tabulated values of the computed integral.

The ordinary differential equation:

$$\frac{dy}{dx} = f(x, y) \quad (1)$$

with initial condition $y(x_0) = y_0$ is solved numerically using a fourth-order Runge-Kutta integration process. This is a single-step method in which the value of y at $x = x_n$ is used to compute $y_{n+1} = y(x_{n+1})$ and earlier values $y_{n-1}, y_{n-2},$ etc. are not used

The relevant formulas are:

$$y_{n+1} = y_n + 1/6 [k_0 + 2k_1 + 2k_2 + k_3] \quad (2)$$

where, for step size h :

$$\begin{cases} k_0 = hf(x_n, y_n) \\ k_1 = hf(x_n + h/2, y_n + k_0/2) \\ k_2 = hf(x_n + h/2, y_n + k_1/2) \\ k_3 = hf(x_n + h, y_n + k_2) \end{cases} \quad (3)$$

```
C      ..... RK2 10
C      ..... RK2 20
C      ..... RK2 30
C      ..... RK2 40
C      ..... RK2 50
C      ..... RK2 60
C      ..... RK2 70
C      ..... RK2 80
C      ..... RK2 90
C      ..... RK2 100
C      ..... RK2 110
C      ..... RK2 120
C      ..... RK2 130
C      ..... RK2 140
C      ..... RK2 150
C      ..... RK2 160
C      ..... RK2 170
C      ..... RK2 180
C      ..... RK2 190
C      ..... RK2 200
C      ..... RK2 210
C      ..... RK2 220
C      ..... RK2 230
C      ..... RK2 240
C      ..... RK2 250
C      ..... RK2 260
C      ..... RK2 270
C      ..... RK2 280
C      ..... RK2 290
C      ..... RK2 300
C      ..... RK2 310
C      ..... RK2 320
C      ..... RK2 330
C      ..... ASRK2 340
C      ..... RK2 350
C      ..... RK2 360
C      ..... RK2 370
C      ..... RK2 380
C      ..... RK2 390
C      ..... RK2 400
C      ..... RK2 410
C      ..... RK2 420
C      ..... RK2 430
C      ..... RK2 440
C      ..... RK2 450
C      ..... RK2 460
C      ..... RK2 470
C      ..... RK2 480
C      ..... RK2 490
C      ..... RK2 500
C      ..... RK2 510
C      ..... RK2 520
C      ..... RK2 530
C      ..... RK2 540
C      ..... RK2 550
C      ..... RK2 560
C      ..... RK2 570
C      ..... RK2 580
C      ..... RK2 590
C      ..... RK2 600
C      ..... RK2 610
C      ..... RK2 620
C      ..... RK2 630
C      ..... RK2 640
C      ..... RK2 650
C      ..... RK2 660
C      ..... RK2 670
C      ..... RK2 680
C      ..... RK2 690
C      ..... RK2 700
C      ..... RK2 710
C      ..... RK2 720

C
C      SUBROUTINE RK2
C
C      PURPOSE
C      INTEGRATES A FIRST ORDER DIFFERENTIAL EQUATION
C      DY/DX=FUN(X,Y) AND PRODUCES A TABLE OF INTEGRATED VALUES
C
C      USAGE
C      CALL RK2(FUN,H,XI,YI,K,N,VEC)
C
C      DESCRIPTION OF PARAMETERS
C      FUN-USER-SUPPLIED FUNCTION SUBPROGRAM WITH ARGUMENTS X,Y
C      WHICH GIVES DY/DX
C      H -STEP SIZE
C      XI -INITIAL VALUE OF X
C      YI -INITIAL VALUE OF Y WHERE YI=Y(XI)
C      K -THE INTERVAL AT WHICH COMPUTED VALUES ARE TO BE STORED
C      N -THE NUMBER OF VALUES TO BE STORED
C      VEC-THE RESULTANT VECTOR OF LENGTH N IN WHICH COMPUTED
C      VALUES OF Y ARE TO BE STORED
C
C      REMARKS
C      NONE
C
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C      FUN - USER-SUPPLIED FUNCTION SUBPROGRAM FOR DY/DX
C      CALLING PROGRAM MUST HAVE FORTRAN EXTERNAL STATEMENT
C      CONTAINING NAMES OF FUNCTION SUBPROGRAMS LISTED IN CALL TO
C      RK2
C
C      METHOD
C      FOURTH ORDER RUNGE-KUTTA INTEGRATION ON A RECURSIVE BASIS
C      SHOWN IN F.B. HILDEBRAND, "INTRODUCTION TO NUMERICAL
C      ANALYSIS", MCGRAW-HILL, NEW YORK, 1956
C
C      .....
C
C      SUBROUTINE RK2(FUN,H,XI,YI,K,N,VEC)
C
C      .....
C
C      IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE
C      C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION
C      STATEMENT WHICH FOLLOWS.
C
C      DOUBLE PRECISION H,XI,YI,VEC,H2,Y,X,T1,T2,T3,T4,FUN
C
C      THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS
C      APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS
C      ROUTINE.
C
C      USER FUNCTION SUBPROGRAM, FUN, MUST BE IN DOUBLE PRECISION.
C
C      .....
C
C      DIMENSION VEC(1)
C      H2=H/2.
C      Y=YI
C      X=XI
C      DO 2 I=1,N
C      DO 1 J=1,K
C      T1=H*FUN(X,Y)
C      T2=H*FUN(X+H2,Y+T1/2.)
C      T3=H*FUN(X+H2,Y+T2/2.)
C      T4=H*FUN(X+H,Y+T3)
C      Y= Y+(T1+2.*T2+2.*T3+T4)/6.
C 1 X=X+H
C 2 VEC(I)=Y
C      RETURN
C      END
```


Subroutines RKGS and DRKGS

These subroutines use the Runge-Kutta method for the solution of initial-value problems.

The purpose of the Runge-Kutta method is to obtain an approximate solution of a system of first-order ordinary differential equations with given initial values. It is a fourth-order integration procedure which is stable and self-starting; that is, only the functional values at a single previous point are required to obtain the functional values ahead. For this reason it is easy to change the step size h at any step in the calculations. On the other hand, each Runge-Kutta step requires the evaluation of the right-hand side of the system four times, which is a great disadvantage compared with other methods of the same order of accuracy, especially predictor-corrector methods. Another disadvantage of the method is that neither the truncation errors nor estimates of them are obtained in the calculation procedure. Therefore, control of accuracy and adjustment of the step size h is done by comparison of the results due to double and single step size $2h$ and h .

Given the system of first-order ordinary differential equations:

$$\begin{aligned} y_1' &= \frac{dy_1}{dx} = f_1(x, y_1, y_2, \dots, y_n) \\ y_2' &= \frac{dy_2}{dx} = f_2(x, y_1, y_2, \dots, y_n) \\ &\dots\dots\dots \\ y_n' &= \frac{dy_n}{dx} = f_n(x, y_1, y_2, \dots, y_n) \end{aligned}$$

and the initial values:

$$y_1(x_0) = y_{1,0}, y_2(x_0) = y_{2,0}, \dots, y_n(x_0) = y_{n,0}$$

and using the following vector notations:

$$Y(x) = \begin{pmatrix} y_1(x) \\ y_2(x) \\ \vdots \\ y_n(x) \end{pmatrix}, F(x, Y) = \begin{pmatrix} f_1(x, Y) \\ f_2(x, Y) \\ \vdots \\ f_n(x, Y) \end{pmatrix}, Y_0 = \begin{pmatrix} y_{1,0} \\ y_{2,0} \\ \vdots \\ y_{n,0} \end{pmatrix}$$

where Y , F and Y_0 are column vectors, the given problem appears as follows:

$$Y' = \frac{dY}{dx} = F(x, Y) \text{ with } Y(x_0) = Y_0$$

With respect to storage requirements and compensation of accumulated roundoff errors, Gill's modification of the classical Runge-Kutta formulas is preferred. Thus, starting at x_0 with $Y(x_0) = Y_0$ and vector $Q_0 = 0$, the resulting vector $Y_4 = Y(x_0 + h)$ is computed by the following formulas:

$$\begin{aligned} K_1 &= h \cdot F(x_0, Y_0) \quad ; \quad Y_1 = Y_0 + \frac{1}{2}(K_1 - 2Q_0) \quad ; \\ Q_1 &= Q_0 + 3\left[\frac{1}{2}(K_1 - 2Q_0)\right] - \frac{1}{2}K_1 \\ K_2 &= h \cdot F\left(x_0 + \frac{h}{2}, Y_1\right) \quad ; \quad Y_2 = Y_1 + (1 - \sqrt{\frac{1}{2}})(K_2 - Q_1) \quad ; \\ Q_2 &= Q_1 + 3\left[(1 - \sqrt{\frac{1}{2}})(K_2 - Q_1)\right] - (1 - \sqrt{\frac{1}{2}})K_2 \quad (1) \\ K_3 &= h \cdot F\left(x_0 + \frac{h}{2}, Y_2\right) \quad ; \quad Y_3 = Y_2 + (1 + \sqrt{\frac{1}{2}})(K_3 - Q_2) \quad ; \\ Q_3 &= Q_2 + 3\left[(1 + \sqrt{\frac{1}{2}})(K_3 - Q_2)\right] - (1 + \sqrt{\frac{1}{2}})K_3 \\ K_4 &= h \cdot F(x_0 + h, Y_3) \quad ; \quad Y_4 = Y_3 + \frac{1}{6}(K_4 - 2Q_3) \quad ; \\ Q_4 &= Q_3 + 3\left[\frac{1}{6}(K_4 - 2Q_3)\right] - \frac{1}{2}K_4 \end{aligned}$$

where $K_1, K_2, K_3, K_4, Y_1, Y_2, Y_3, Y_4, Q_1, Q_2, Q_3, Q_4$ are all column vectors with n components. If the procedure were carried out with infinite precision (that is, no rounding errors), vector Q_4 defined above would be zero. In practice this is not true, and Q_4 represents approximately three times the roundoff error in Y_4 accumulated during one step. To compensate for this accumulated roundoff, Q_4 is used as Q_0 for the next step. Also $(x_0 + h)$ and Y_4 serve as x_0 and Y_0 respectively at the next step.

For initial control of accuracy, an approximation for $Y(x_0 + 2h)$ called $Y^{(2)}(x_0 + 2h)$ is computed using the step size $2h$, and then an approximation called $Y^{(1)}(x_0 + 2h)$, using two times the step size h . From these two approximations, a test value δ for accuracy is generated in the following way:

$$\delta = \frac{1}{15} \sum_{i=1}^n a_i \cdot |y_i^{(1)} - y_i^{(2)}| \quad (2)$$

where the coefficients a_i are error-weights specified in the input of the procedure.

Test value δ is an approximate measure for the local truncation error at point $x_0 + 2h$. If δ is greater than a given tolerance ϵ_2 , increment h is halved and the procedure starts again at the point x_0 . If δ is less than ϵ_2 , the results $Y^{(1)}(x_0 + h)$ and $Y^{(1)}(x_0 + 2h)$

are assumed to be correct. They are then handed, together with $x_0 + h$ and $x_0 + 2h$ and the derivatives at these points -- that is, the values of $F[x_0 + h, Y^{(1)}(x_0+h)]$ and $F[x_0+2h, Y^{(1)}(x_0+2h)]$ respectively -- to a user-supplied output subroutine.

If δ is less than $\epsilon_1 = \epsilon_2/50$, the next step is carried out with the doubled increment. However, care is taken in the procedure that the increment never becomes greater than the increment h specified as an input parameter, and further that all points $x_0 + j \cdot h$ (where $j = 1, 2, \dots$) which are situated between the lower and upper bound of the integration interval are included in the output. Finally, the increment of the last step of the procedure is chosen in such a way that the upper bound of the integration interval is reached exactly.

The entire input of the procedure is:

1. Lower and upper bound of the integration interval, initial increment of the independent variable, upper bound ϵ_2 of the local truncation error
2. Initial values of the dependent variables and weights for the local truncation errors in each component of the dependent variables
3. The number of differential equations in the system
4. As external subroutine subprograms, the computation of the right-hand side of the system of differential equations; for flexibility in output, an output subroutine
5. An auxiliary storage array named AUX with 8 rows and n columns

Output is done in the following way. If a set of approximations to the dependent variables $Y(x)$ is found to be of sufficient accuracy, it is handed -- together with x , the derivative $F[x, Y(x)]$, the number of bisections of the initial increment, the number of differential equations, the lower and upper bound of the interval, the initial step size, error bound ϵ_2 , and a parameter for terminating subroutine RKGS or DRKGS -- to the output subroutine. Because of this output subroutine, the user has the opportunity to choose his own output format, to handle the output values as he wants, to change the upper error bound, and to terminate subroutine RKGS or DRKGS at any output point. In particular, the user is able to drop the output of some intermediate points, printing only the result values at the special points $x_0 + n \cdot h$ ($n = 0, 1, 2, \dots$). The user may also perform intermediate computation using the integration results before continuing the process.

For better understanding of the flowchart and of the FORTRAN program, Figure 32 shows the allocation of special intermediate result vectors within the storage array AUX.

For reference see A. Ralston/H. S. Wilf, Mathematical Methods for Digital Computers, Wiley, New York/London, 1960, pp. 110-120.

AUX

function vector $Y(x)$	1. row (AUX (1) in flowchart)
derivative vector $F(x, Y(x))$	2. row (AUX (2) in flowchart)
vector of accumulated roundoff at point x	3. row (AUX (3) in flowchart)
function vector $Y(x+2h)$ for testing purposes	4. row (AUX (4) in flowchart)
function vector $Y(x+h)$	5. row (AUX (5) in flowchart)
vector of accumulated roundoff at point $x+h$	6. row (AUX (6) in flowchart)
derivative vector $F(x+h, Y(x+h))$	7. row (AUX (7) in flowchart)
vector of error weights multiplied by $1/15$	8. row (AUX (8) in flowchart)

Figure 32. Storage allocation in auxiliary storage array AUX (RKGS-DRKGS)

```

C .....
C                                     RKGS 10
C                                     RKGS 20
C                                     RKGS 30
C SUBROUTINE RKGS                       RKGS 40
C                                     RKGS 50
C PURPOSE                               RKGS 60
C TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY DIFFERENTIAL   RKGS 70
C EQUATIONS WITH GIVEN INITIAL VALUES.                   RKGS 80
C                                     RKGS 90
C USAGE                                  RKGS 100
C CALL RKGS (PRMT,Y,DERY,NDIM,IHLF,FCT,OUTP,AUX)          RKGS 110
C PARAMETERS FCT AND OUTP REQUIRE AN EXTERNAL STATEMENT.  RKGS 120
C                                     RKGS 130
C DESCRIPTION OF PARAMETERS              RKGS 140
C PRMT - AN INPUT AND OUTPUT VECTOR WITH DIMENSION GREATER  RKGS 150
C OR EQUAL TO 5, WHICH SPECIFIES THE PARAMETERS FOR       RKGS 160
C THE INTERVAL AND OF ACCURACY AND WHICH SERVES FOR       RKGS 170
C COMMUNICATION BETWEEN OUTPUT SUBROUTINE (FURNISHED     RKGS 180
C BY THE USER) AND SUBROUTINE RKGS, EXCEPT PRMT(5)     RKGS 190
C THE COMPONENTS ARE NOT DESTROYED BY SUBROUTINE         RKGS 200
C RKGS AND THEY ARE                                     RKGS 210
C PRMT(1) - LOWER BOUND OF THE INTERVAL (INPUT).          RKGS 220
C PRMT(2) - UPPER BOUND OF THE INTERVAL (INPUT).          RKGS 230
C PRMT(3) - INITIAL INCREMENT OF THE INDEPENDENT VARIABLE  RKGS 240
C (INPUT),                                               RKGS 250
C PRMT(4) - UPPER ERROR BOUND (INPUT). IF ABSOLUTE ERROR IS  RKGS 260
C GREATER THAN PRMT(4), INCREMENT GETS HALVED.           RKGS 270
C IF INCREMENT IS LESS THAN PRMT(3) AND ABSOLUTE         RKGS 280
C ERROR LESS THAN PRMT(4)/50, INCREMENT GETS DOUBLED.   RKGS 290
C THE USER MAY CHANGE PRMT(4) BY MEANS OF HIS           RKGS 300
C OUTPUT SUBROUTINE.                                    RKGS 310
C PRMT(5) - NO INPUT PARAMETER. SUBROUTINE RKGS INITIALIZES  RKGS 320
C PRMT(5)=0. IF THE USER WANTS TO TERMINATE              RKGS 330
C SUBROUTINE RKGS AT ANY OUTPUT POINT, HE HAS TO         RKGS 340
C CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE     RKGS 350
C OUTP. FURTHER COMPONENTS OF VECTOR PRMT ARE           RKGS 360
C FEASIBLE IF ITS DIMENSION IS DEFINED GREATER          RKGS 370
C THAN 5, HOWEVER SUBROUTINE RKGS DOES NOT REQUIRE      RKGS 380
C AND CHANGE THEM. NEVERTHELESS THEY MAY BE USEFUL     RKGS 390
C FOR HANDLING RESULT VALUES TO THE MAIN PROGRAM       RKGS 400
C (CALLING RKGS) WHICH ARE OBTAINED BY SPECIAL         RKGS 410
C MANIPULATIONS WITH OUTPUT DATA IN SUBROUTINE OUTP.  RKGS 420
C Y - INPUT VECTOR OF INITIAL VALUES. (DESTROYED)       RKGS 430
C LATERON Y IS THE RESULTING VECTOR OF DEPENDENT        RKGS 440
C VARIABLES COMPUTED AT INTERMEDIATE POINTS X.          RKGS 450
C DERY - INPUT VECTOR OF ERROR WEIGHTS. (DESTROYED)      RKGS 460
C THE SUM OF ITS COMPONENTS MUST BE EQUAL TO 1.          RKGS 470
C LATERON DERY IS THE VECTOR OF DERIVATIVES, WHICH      RKGS 480
C BELONG TO FUNCTION VALUES Y AT A POINT X.            RKGS 490
C NDIM - AN INPUT VALUE, WHICH SPECIFIES THE NUMBER OF   RKGS 500
C EQUATIONS IN THE SYSTEM.                               RKGS 510
C IHLF - AN OUTPUT VALUE, WHICH SPECIFIES THE NUMBER OF  RKGS 520
C BISECTIONS OF THE INITIAL INCREMENT. IF IHLF GETS     RKGS 530
C GREATER THAN 10, SUBROUTINE RKGS RETURNS WITH        RKGS 540
C ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM. ERROR       RKGS 550
C MESSAGE IHLF=12 OR IHLF=13 APPEARS IN CASE           RKGS 560
C PRMT(3)=0 OR IN CASE SIGN(PRMT(3)).NE.SIGN(PRMT(2))-RKGS 570
C PRMT(1) RESPECTIVELY.                                  RKGS 580
C FCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. THIS   RKGS 590
C SUBROUTINE COMPUTES THE RIGHT HAND SIDES DERY OF     RKGS 600
C THE SYSTEM TO GIVEN VALUES X AND Y. ITS PARAMETER   RKGS 610
C LIST MUST BE X,Y,DERY. SUBROUTINE FCT SHOULD        RKGS 620
C NOT DESTROY X AND Y.                                  RKGS 630
C OUTP - THE NAME OF AN EXTERNAL OUTPUT SUBROUTINE USED. RKGS 640
C ITS PARAMETER LIST MUST BE X,Y,DERY,IHLF,NDIM,PRMT.  RKGS 650
C NONE OF THESE PARAMETERS (EXCEPT, IF NECESSARY,    RKGS 660
C PRMT(4),PRMT(5),...) SHOULD BE CHANGED BY           RKGS 670
C SUBROUTINE OUTP. IF PRMT(5) IS CHANGED TO NON-ZERO,  RKGS 680
C SUBROUTINE RKGS IS TERMINATED.                       RKGS 690
C AUX - AN AUXILIARY STORAGE ARRAY WITH 8 ROWS AND NDIM  RKGS 700
C COLUMNS.                                             RKGS 710
C                                     RKGS 720
C REMARKS                                               RKGS 730
C THE PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF  RKGS 740
C (1) MORE THAN 10 BISECTIONS OF THE INITIAL INCREMENT ARE  RKGS 750

```

```

C          NECESSARY TO GET SATISFACTORY ACCURACY (ERROR MESSAGE   RKGS 760
C          IHLF=11),                                             RKGS 770
C          (2) INITIAL INCREMENT IS EQUAL TO 0 OR HAS WRONG SIGN   RKGS 780
C          (ERROR MESSAGES IHLF=12 OR IHLF=13),                 RKGS 790
C          (3) THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH,   RKGS 800
C          (4) SUBROUTINE OUTP HAS CHANGED PRMT(5) TO NON-ZERO.   RKGS 810
C
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED           RKGS 820
C          THE EXTERNAL SUBROUTINES FCT(X,Y,DERY) AND             RKGS 830
C          OUTP(X,Y,DERY,IHLF,NDIM,PRMT) MUST BE FURNISHED BY THE   RKGS 840
C          USER. RKGS 850
C
C          METHOD                                                 RKGS 860
C          EVALUATION IS DONE BY MEANS OF FOURTH ORDER RUNGE-KUTTA  RKGS 870
C          FORMULAE IN THE MODIFICATION DUE TO GILL. ACCURACY IS    RKGS 880
C          TESTED COMPARING THE RESULTS OF THE PROCEDURE WITH SINGLE  RKGS 890
C          AND DOUBLE INCREMENT.                                   RKGS 900
C          SUBROUTINE RKGS AUTOMATICALLY ADJUSTS THE INCREMENT DURING  RKGS 910
C          THE WHOLE COMPUTATION BY HALVING OR DOUBLING. IF MORE THAN  RKGS 920
C          10 BISECTIONS OF THE INCREMENT ARE NECESSARY TO GET       RKGS 930
C          SATISFACTORY ACCURACY, THE SUBROUTINE RETURNS WITH       RKGS 940
C          ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM.                 RKGS 950
C          TO GET FULL FLEXIBILITY IN OUTPUT, AN OUTPUT SUBROUTINE   RKGS 960
C          MUST BE FURNISHED BY THE USER.                           RKGS 970
C          FOR REFERENCE, SEE                                       RKGS 980
C          RALSTON/WILF, MATHEMATICAL METHODS FOR DIGITAL COMPUTERS,  RKGS 990
C          WILEY, NEW YORK/LONDON, 1960, PP.110-120.                RKGS1000
C
C          .....
C          SUBROUTINE RKGS(PRMT,Y,DERY,NDIM,IHLF,FCT,OUTP,AUX1)    RKGS1010
C
C          DIMENSION Y(1),DERY(1),AUX(8,1),A(4),B(4),C(4),PRMT(11)  RKGS1020
C          DO 1 I=1,NDIM                                           RKGS1030
C          1 AUX(8,I)=.06666667*DERY(I)                             RKGS1040
C          X=PRMT(1)                                               RKGS1050
C          XEND=PRMT(2)                                             RKGS1060
C          H=PRMT(3)                                               RKGS1070
C          PRMT(5)=0.                                              RKGS1080
C          CALL FCT(X,Y,DERY)                                       RKGS1090
C
C          ERROR TEST                                             RKGS1100
C          IF(H*(XEND-X))38,37,2                                    RKGS1110
C
C          PREPARATIONS FOR RUNGE-KUTTA METHOD                     RKGS1120
C          2 A(1)=.5                                               RKGS1130
C          A(2)=.2928932                                           RKGS1140
C          A(3)=1.707107                                           RKGS1150
C          A(4)=.1666667                                           RKGS1160
C          B(1)=2.                                                 RKGS1170
C          B(2)=1.                                                 RKGS1180
C          B(3)=1.                                                 RKGS1190
C          B(4)=2.                                                 RKGS1200
C          C(1)=.5                                                 RKGS1210
C          C(2)=.2928932                                           RKGS1220
C          C(3)=1.707107                                           RKGS1230
C          C(4)=.5                                                 RKGS1240
C
C          PREPARATIONS OF FIRST RUNGE-KUTTA STEP                 RKGS1250
C          DO 3 I=1,NDIM                                           RKGS1260
C          AUX(1,I)=Y(I)                                           RKGS1270
C          AUX(2,I)=DERY(I)                                         RKGS1280
C          AUX(3,I)=0.                                             RKGS1290
C          3 AUX(6,I)=0.                                           RKGS1300
C          IREC=0                                                  RKGS1310
C          H=H*H                                                    RKGS1320
C          IHLF=-1                                                 RKGS1330
C          ISTEP=0                                                 RKGS1340
C          IEND=0                                                  RKGS1350
C
C          START OF A RUNGE-KUTTA STEP                             RKGS1360
C          4 IF((X+H-XEND)/H)7,6,5                                  RKGS1370
C          5 H=XEND-X                                              RKGS1380
C          6 IEND=1                                               RKGS1390
C
C          RECORDING OF INITIAL VALUES OF THIS STEP              RKGS1400
C          7 CALL OUTP(X,Y,DERY,IREC,NDIM,PRMT)                   RKGS1410
C          IF(PRMT(5))40,8,40                                       RKGS1420
C          8 ITEST=0                                              RKGS1430
C          9 ISTEP=ISTEP+1                                         RKGS1440
C
C          START OF INNERMOST RUNGE-KUTTA LOOP                    RKGS1450
C          J=1                                                     RKGS1460
C          10 AJ=A(J)                                              RKGS1470
C          BJ=B(J)                                                 RKGS1480
C          CJ=C(J)                                                 RKGS1490
C          DO 11 I=1,NDIM                                          RKGS1500
C          R1=H*DERY(I)                                           RKGS1510
C          R2=AJ*(R1-BJ*AUX(6,I))                                  RKGS1520
C          Y(I)=Y(I)+R2                                           RKGS1530
C          R2=R2+R2+R2                                           RKGS1540
C          11 AUX(6,I)=AUX(6,I)+R2-CJ*R1                            RKGS1550
C          IF(J-1)12,15,15                                         RKGS1560
C          12 J=J+1                                               RKGS1570
C          IF(J-1)13,14,13                                         RKGS1580
C          13 X=X+.5*H                                             RKGS1590
C          14 CALL FCT(X,Y,DERY)                                   RKGS1600
C          GOTO 10                                                 RKGS1610
C          END OF INNERMOST RUNGE-KUTTA LOOP                       RKGS1620
C
C          TEST OF ACCURACY                                       RKGS1630
C          15 IF(ITEST)16,16,20                                    RKGS1640
C
C          IN CASE ITEST=0 THERE IS NO POSSIBILITY FOR TESTING OF  RKGS1650
C          ACCURACY                                               RKGS1660
C          16 DO 17 I=1,NDIM                                       RKGS1670
C          17 AUX(4,I)=Y(I)                                         RKGS1680
C          ITEST=1                                               RKGS1690
C          ISTEP=ISTEP+ISTEP-2                                     RKGS1700
C          18 IHLF=IHLF+1                                         RKGS1710
C          X=X-H                                                 RKGS1720
C          H=.5*H                                                 RKGS1730
C          DO 19 I=1,NDIM                                          RKGS1740
C          Y(I)=AUX(1,I)                                           RKGS1750
C          DERY(I)=AUX(2,I)                                         RKGS1760
C          19 AUX(6,I)=AUX(3,I)                                     RKGS1770
C          GOTO 9                                                 RKGS1780
C
C          IN CASE ITEST=1 TESTING OF ACCURACY IS POSSIBLE       RKGS1790
C          20 IMOD=ISTEP/2                                         RKGS1800
C          IF(ISTEP-IMOD-IMOD)21,23,21                             RKGS1810
C          21 CALL FCT(X,Y,DERY)                                   RKGS1820
C          DO 22 I=1,NDIM                                          RKGS1830
C          AUX(5,I)=Y(I)                                           RKGS1840
C          22 AUX(7,I)=DERY(I)                                       RKGS1850
C          GOTO 9                                                 RKGS1860

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C          COMPUTATION OF TEST VALUE DELT                       RKGS2050
C          DELT=0. I=1,NDIM                                       RKGS2060
C          DO 23 I=1,NDIM                                         RKGS2070
C          23 DELT=DELT+AUX(8,I)*ABS(AUX(4,I)-Y(I))                 RKGS2080
C          IF(DELT-PRMT(4))28,28,25                                RKGS2090
C
C          ERROR IS TOO GREAT                                     RKGS2100
C          25 IF(IHLF-10)26,36,36                                  RKGS2110
C          DO 27 I=1,NDIM                                         RKGS2120
C          27 AUX(4,I)=AUX(5,I)                                    RKGS2130
C          ISTEP=ISTEP+ISTEP-4                                    RKGS2140
C          X=X-H                                                  RKGS2150
C          IEND=0                                                 RKGS2160
C          GOTO 18                                                 RKGS2170
C
C          RESULT VALUES ARE GOOD                              RKGS2180
C          28 CALL FCT(X,Y,DERY)                                   RKGS2190
C          DO 29 I=1,NDIM                                         RKGS2200
C          AUX(1,I)=Y(I)                                           RKGS2210
C          AUX(2,I)=DERY(I)                                         RKGS2220
C          AUX(3,I)=AUX(6,I)                                       RKGS2230
C          Y(I)=AUX(5,I)                                           RKGS2240
C          29 DERY(I)=AUX(7,I)                                       RKGS2250
C          CALL OUTP(X-H,Y,DERY,IHLF,NDIM,PRMT)                 RKGS2260
C          IF(PRMT(5))40,30,40                                       RKGS2270
C          DO 31 I=1,NDIM                                         RKGS2280
C          31 Y(I)=AUX(1,I)                                         RKGS2290
C          31 DERY(I)=AUX(2,I)                                       RKGS2300
C          IREC=IHLF                                              RKGS2310
C          IF(IEND)32,32,39                                       RKGS2320
C
C          INCREMENT GETS DOUBLED                                RKGS2330
C          32 IHLF=IHLF-1                                         RKGS2340
C          ISTEP=ISTEP/2                                         RKGS2350
C          H=H*H                                                  RKGS2360
C          IF(IHLF)4,33,33                                       RKGS2370
C          33 IMOD=ISTEP/2                                         RKGS2380
C          IF(ISTEP-IMOD-IMOD)4,34,4                                RKGS2390
C          34 IF(DELT-.02*PRMT(4))35,35,4                          RKGS2400
C          35 IHLF=IHLF-1                                         RKGS2410
C          ISTEP=ISTEP/2                                         RKGS2420
C          H=H*H                                                  RKGS2430
C          GOTO 4                                                 RKGS2440
C
C          RETURNS TO CALLING PROGRAM                            RKGS2450
C          36 IHLF=11                                             RKGS2460
C          CALL FCT(X,Y,DERY)                                       RKGS2470
C          GOTO 39                                                 RKGS2480
C          37 IHLF=12                                             RKGS2490
C          GOTO 39                                                 RKGS2500
C          38 IHLF=13                                             RKGS2510
C          39 CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)                 RKGS2520
C          40 RETURN                                             RKGS2530
C          END                                                    RKGS2540

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C          ..... DRKG 10
C          ..... DRKG 20
C          ..... DRKG 30
C          SUBROUTINE DRKGS                                       DRKG 40
C          ..... DRKG 50
C          ..... DRKG 60
C          PURPOSE                                               DRKG 70
C          TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY DIFFERENTIAL  DRKG 80
C          EQUATIONS WITH GIVEN INITIAL VALUES.                 DRKG 90
C          USAGE                                                 DRKG 100
C          CALL DRKGS (PRMT,Y,DERY,NDIM,IHLF,FCT,OUTP,AUX)       DRKG 110
C          PARAMETERS FCT AND OUTP REQUIRE AN EXTERNAL STATEMENT. DRKG 120
C          ..... DRKG 130
C          DESCRIPTION OF PARAMETERS                             DRKG 140
C          PRMT - DOUBLE PRECISION INPUT AND OUTPUT VECTOR WITH  DRKG 150
C          DIMENSION GREATER THAN OR EQUAL TO 5, WHICH          DRKG 160
C          SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF       DRKG 170
C          ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN   DRKG 180
C          OUTPUT SUBROUTINE (FURNISHED BY THE USER) AND        DRKG 190
C          SUBROUTINE DRKGS. EXCEPT PRMT(5) THE COMPONENTS    DRKG 200
C          ARE NOT DESTROYED BY SUBROUTINE DRKGS AND THEY ARE    DRKG 210
C          PRMT(1)- LOWER BOUND OF THE INTERVAL (INPUT),         DRKG 220
C          PRMT(2)- UPPER BOUND OF THE INTERVAL (INPUT),         DRKG 230
C          PRMT(3)- INITIAL INCREMENT OF THE INDEPENDENT VARIABLE DRKG 240
C          (INPUT),                                               DRKG 250
C          PRMT(4)- UPPER ERROR BOUND (INPUT). IF ABSOLUTE ERROR IS DRKG 260
C          GREATER THAN PRMT(4), INCREMENT GETS HALVED.         DRKG 270
C          IF INCREMENT IS LESS THAN PRMT(3) AND ABSOLUTE        DRKG 280
C          ERROR LESS THAN PRMT(4)/50, INCREMENT GETS DOUBLED.   DRKG 290
C          THE USER MAY CHANGE PRMT(4) BY MEANS OF HIS           DRKG 300
C          OUTPUT SUBROUTINE.                                     DRKG 310
C          PRMT(5)- NO INPUT PARAMETER. SUBROUTINE DRKGS INITIALIZES DRKG 320
C          PRMT(5)=0. IF THE USER WANTS TO TERMINATE             DRKG 330
C          SUBROUTINE DRKGS AT ANY OUTPUT POINT, HE HAS TO      DRKG 340
C          CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE     DRKG 350
C          OUTP. FURTHER COMPONENTS OF VECTOR PRMT ARE           DRKG 360
C          FEASIBLE IF ITS DIMENSION IS DEFINED GREATER          DRKG 370
C          THAN 5. HOWEVER SUBROUTINE DRKGS DOES NOT REQUIRE     DRKG 380
C          AND CHANGE THEM. NEVERTHELESS THEY MAY BE USEFUL     DRKG 390
C          FOR HANDLING RESULT VALUES TO THE MAIN PROGRAM       DRKG 400
C          (CALLING DRKGS) WHICH ARE OBTAINED BY SPECIAL         DRKG 410
C          MANIPULATIONS WITH OUTPUT DATA IN SUBROUTINE OUTP.  DRKG 420
C          Y - DOUBLE PRECISION INPUT VECTOR OF INITIAL VALUES  DRKG 430
C          (DESTROYED). LATERON Y IS THE RESULTING VECTOR OF     DRKG 440
C          DEPENDENT VARIABLES COMPUTED AT INTERMEDIATE          DRKG 450
C          POINTS X.                                             DRKG 460
C          DERY - DOUBLE PRECISION INPUT VECTOR OF ERROR WEIGHTS DRKG 470
C          (DESTROYED). THE SUM OF ITS COMPONENTS MUST BE       DRKG 480
C          EQUAL TO 1. LATERON DERY IS THE VECTOR OF              DRKG 490
C          DERIVATIVES, WHICH BELONG TO FUNCTION VALUES Y AT    DRKG 500
C          INTERMEDIATE POINTS X.                                DRKG 510
C          NDIM - AN INPUT VALUE, WHICH SPECIFIES THE NUMBER OF  DRKG 520
C          EQUATIONS IN THE SYSTEM.                               DRKG 530
C          IHLF - AN OUTPUT VALUE, WHICH SPECIFIES THE NUMBER OF  DRKG 540
C          BISECTIONS OF THE INITIAL INCREMENT. IF IHLF GETS    DRKG 550
C          GREATER THAN 10, SUBROUTINE DRKGS RETURNS WITH        DRKG 560
C          ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM. ERROR       DRKG 570
C          MESSAGE IHLF=12 OR IHLF=13 APPEARS IN CASE            DRKG 580
C          PRMT(3)=0 OR IN CASE SIGN(PRMT(3)).NE.SIGN(PRMT(2))-DRKG 590
C          PRMT(1)) RESPECTIVELY.                                 DRKG 600
C          FCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. THIS  DRKG 610
C          SUBROUTINE COMPUTES THE RIGHT HAND SIDES DERY OF      DRKG 620
C          THE SYSTEM TO GIVEN VALUES X AND Y. ITS PARAMETER    DRKG 630
C          LIST MUST BE X,Y,DERY. SUBROUTINE FCT SHOULD          DRKG 640
C          NOT DESTROY X AND Y.                                   DRKG 650

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C      OUTP - THE NAME OF AN EXTERNAL OUTPUT SUBROUTINE USED. DRKG 660
C      ITS PARAMETER LIST MUST BE X,Y,DERY,IHLF,NDIM,PRMT, DRKG 670
C      NONE OF THESE PARAMETERS (EXCEPT, IF NECESSARY, DRKG 680
C      PRMT(4),PRMT(5),...) SHOULD BE CHANGED BY DRKG 690
C      SUBROUTINE OUTP. IF PRMT(5) IS CHANGED TO NON-ZERO, DRKG 700
C      SUBROUTINE DRKGS IS TERMINATED. DRKG 710
C      AUX - DOUBLE PRECISION AUXILIARY STORAGE ARRAY WITH 8 DRKG 720
C      ROWS AND NDIM COLUMNS. DRKG 730
C
C      REMARKS
C      THE PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF DRKG 760
C      (1) MORE THAN 10 BISECTIONS OF THE INITIAL INCREMENT ARE DRKG 77C
C      NECESSARY TO GET SATISFACTORY ACCURACY (ERROR MESSAGE DRKG 780
C      IHLF=11). DRKG 790
C      (2) INITIAL INCREMENT IS EQUAL TO 0 OR HAS WRONG SIGN DRKG 800
C      (ERROR MESSAGES IHLF=12 OR IHLF=13). DRKG 810
C      (3) THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH, DRKG 820
C      (4) SUBROUTINE OUTP HAS CHANGED PRMT(5) TO NON-ZERO. DRKG 830
C
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DRKG 840
C      THE EXTERNAL SUBROUTINES FCT(X,Y,DERY) AND DRKG 850
C      OUTP(X,Y,DERY,IHLF,NDIM,PRMT) MUST BE FURNISHED BY THE USER. DRKG 870
C
C      METHOD
C      EVALUATION IS DONE BY MEANS OF FOURTH ORDER RUNGE-KUTTA DRKG 890
C      FORMULAE IN THE MODIFICATION DUE TO GILL. ACCURACY IS DRKG 900
C      TESTED COMPARING THE RESULTS OF THE PROCEDURE WITH SINGLE DRKG 910
C      AND DOUBLE INCREMENT. DRKG 920
C      SUBROUTINE DRKGS AUTOMATICALLY ADJUSTS THE INCREMENT DURING DRKG 940
C      THE WHOLE COMPUTATION BY HALVING OR DOUBLING. IF MORE THAN DRKG 950
C      10 BISECTIONS OF THE INCREMENT ARE NECESSARY TO GET DRKG 960
C      SATISFACTORY ACCURACY, THE SUBROUTINE RETURNS WITH DRKG 970
C      ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM. DRKG 980
C      TO GET FULL FLEXIBILITY IN OUTPUT, AN OUTPUT SUBROUTINE DRKG 990
C      MUST BE FURNISHED BY THE USER. DRKG 1000
C      FOR REFERENCE, SEE DRKG1010
C      RALSTON/WILF, MATHEMATICAL METHODS FOR DIGITAL COMPUTERS, DRKG1020
C      WILEY, NEW YORK/LONDON, 1960, PP.110-120. DRKG1030
C
C      ..... DRKG1040
C      SUBROUTINE DRKGS(PRMT,Y,DERY,NDIM,IHLF,FCT,OUTP,AUX) DRKG1050
C
C      DIMENSION Y(1),DERY(1),AUX(8,1),A(4),B(4),C(4),PRMT(1) DRKG1060
C      DOUBLE PRECISION PRMT,Y,DERY,AUX,A,B,C,X,XEND,H,AJ,BJ,CJ,R1,R2, DRKG1070
C      IDELT DRKG1080
C      DD 1 I=1,NDIM DRKG1090
C      1 AUX(8,1)=-.06666666666666666709*DERY(1) DRKG1100
C      X=PRMT(1) DRKG1110
C      XEND=PRMT(2) DRKG1120
C      H=PRMT(3) DRKG1130
C      PRMT(5)=0.00 DRKG1140
C      CALL FCT(X,Y,DERY) DRKG1150
C
C      ERROR TEST DRKG1160
C      IF(H*(XEND-X))38,37,2 DRKG1170
C
C      PREPARATIONS FOR RUNGE-KUTTA METHOD DRKG1180
C      2 A(1)=-.500 DRKG1190
C      A(2)=-.2928932188134524800 DRKG1200
C      A(3)=1.707106781186547500 DRKG1210
C      A(4)=-.16666666666666666700 DRKG1220
C      B(1)=2.00 DRKG1230
C      B(2)=1.00 DRKG1240
C      B(3)=1.00 DRKG1250
C      B(4)=2.00 DRKG1260
C      C(1)=-.500 DRKG1270
C      C(2)=-.2928932188134524800 DRKG1280
C      C(3)=1.707106781186547500 DRKG1290
C      C(4)=-.500 DRKG1300
C
C      PREPARATIONS OF FIRST RUNGE-KUTTA STEP DRKG1310
C      DD 3 I=1,NDIM DRKG1320
C      AUX(1,1)=Y(1) DRKG1330
C      AUX(2,1)=DERY(1) DRKG1340
C      AUX(3,1)=0.00 DRKG1350
C      3 AUX(6,1)=0.00 DRKG1360
C      IREC=0 DRKG1370
C      H=H+H DRKG1380
C      IHLF=-1 DRKG1390
C      ISTEP=0 DRKG1400
C      IEND=0 DRKG1410
C
C      START OF A RUNGE-KUTTA STEP DRKG1420
C      4 IF(X=H*(XEND+H))7,6,5 DRKG1430
C      5 H=XEND-X DRKG1440
C      6 IEND=1 DRKG1450
C
C      RECORDING OF INITIAL VALUES OF THIS STEP DRKG1460
C      7 CALL OUTP(X,Y,DERY,IREC,NDIM,PRMT) DRKG1470
C      IF(PRMT(5))40,8,40 DRKG1480
C      8 ITEST=0 DRKG1490
C      9 ISTEP=ISTEP+1 DRKG1500
C
C      START OF INNERMOST RUNGE-KUTTA LOOP DRKG1510
C      J=1 DRKG1520
C      10 AJ=A(J) DRKG1530
C      BJ=B(J) DRKG1540
C      CJ=C(J) DRKG1550
C      DD 11 I=1,NDIM DRKG1560
C      R1=H*DERY(I) DRKG1570
C      R2=AJ*(R1-BJ*AUX(6,I)) DRKG1580
C      Y(I)=Y(I)+R2 DRKG1590
C      R2=R2+R2 DRKG1600
C      11 AUX(8,I)=AUX(6,I)+R2-CJ*R1 DRKG1610
C      IF(J=4)12,15,15 DRKG1620
C      12 J=J+1 DRKG1630
C      IF(J=3)13,14,13 DRKG1640
C      13 X=X+.500*H DRKG1650
C      14 CALL FCT(X,Y,DERY) DRKG1660
C      GOTO 10 DRKG1670
C      END OF INNERMOST RUNGE-KUTTA LOOP DRKG1680
C
C      TEST OF ACCURACY DRKG1690
C      15 IF(ISTEST)16,16,20 DRKG1700
C
C      IN CASE ITEST=0 THERE IS NO POSSIBILITY FOR TESTING OF ACCURACY DRKG1710
C      16 DD 17 I=1,NDIM DRKG1720
C      17 AUX(4,I)=Y(I) DRKG1730
C      ITEST=1 DRKG1740
C      ISTEP=ISTEP+ISTEP-2 DRKG1750
C      18 IHLF=IHLF+1 DRKG1760
C      X=X+H DRKG1770
C      H=.500*H DRKG1780
C      DD 19 I=1,NDIM DRKG1790
C      Y(I)=AJX(I,1) DRKG1800
C      DERY(I)=AUX(2,1) DRKG1810
C      19 AUX(6,I)=AUX(3,1) DRKG1820
C      GOTO 9 DRKG1830
C
C      IN CASE ITEST=1 TESTING OF ACCURACY IS POSSIBLE DRKG1840
C      20 IMOD=ISTEP/2 DRKG1850
C      IF(ISTEP=IMOD-IMOD)21,23,21 DRKG1860
C      21 CALL FCT(X,Y,DERY) DRKG1870
C      DD 22 I=1,NDIM DRKG1880
C      AUX(5,I)=Y(I) DRKG1890
C      22 AUX(7,I)=DERY(I) DRKG1900
C      GOTO 9 DRKG1910
C
C      COMPUTATION OF TEST VALUE DELT DRKG1920
C      23 DELT=0.00 DRKG1930
C      DD 24 I=1,NDIM DRKG1940
C      24 DELT=DELT+AUX(8,I)*DABS(AUX(4,I)-Y(I)) DRKG1950
C      IF(DELT-PRMT(4))28,28,25 DRKG1960
C
C      ERROR IS TOO GREAT DRKG1970
C      25 IF(IHLF-10)26,36,36 DRKG1980
C      DD 27 I=1,NDIM DRKG1990
C      27 AUX(4,I)=AUX(5,I) DRKG2000
C      ISTEP=ISTEP-ISTEP-4 DRKG2010
C      X=X-H DRKG2020
C      IEND=0 DRKG2030
C      GOTO 18 DRKG2040
C
C      RESULT VALUES ARE GOOD DRKG2050
C      28 CALL FCT(X,Y,DERY) DRKG2060
C      DD 29 I=1,NDIM DRKG2070
C      AUX(1,I)=Y(I) DRKG2080
C      AUX(2,I)=DERY(I) DRKG2090
C      AUX(3,I)=AUX(6,I) DRKG2100
C      Y(I)=AJX(5,I) DRKG2110
C      29 DERY(I)=AUX(7,I) DRKG2120
C      CALL OUTP(X,H,Y,DERY,IHLF,NDIM,PRMT) DRKG2130
C      IF(PRMT(5))40,30,40 DRKG2140
C      DD 31 I=1,NDIM DRKG2150
C      Y(I)=AUX(1,I) DRKG2160
C      31 DERY(I)=AUX(2,I) DRKG2170
C      IREC=IHLF DRKG2180
C      IF(IEND)32,32,39 DRKG2190
C
C      INCREMENT GETS DOUBLED DRKG2200
C      32 IHLF=IHLF-1 DRKG2210
C      ISTEP=ISTEP/2 DRKG2220
C      H=H+H DRKG2230
C      33 IMOD=ISTEP/2 DRKG2240
C      IF(IHLF=14,33,33 DRKG2250
C      34 IF(DELT-.0200*PRMT(4))35,35,4 DRKG2260
C      35 IHLF=IHLF-1 DRKG2270
C      ISTEP=ISTEP/2 DRKG2280
C      H=H+H DRKG2290
C      GOTO 4 DRKG2300
C
C      RETURNS TO CALLING PROGRAM DRKG2310
C      36 IHLF=11 DRKG2320
C      CALL FCT(X,Y,DERY) DRKG2330
C      GOTO 39 DRKG2340
C      37 IHLF=12 DRKG2350
C      GOTO 39 DRKG2360
C      38 IHLF=13 DRKG2370
C      39 CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT) DRKG2380
C      40 RETURN DRKG2390
C      END DRKG2400

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Subroutines HPCG and DHPCG

These subroutines use Hamming's modified predictor-corrector method for the solution of general initial-value problems.

The purpose of Hamming's modified predictor-corrector method is to obtain an approximate solution of a general system of first-order ordinary differential equations with given initial values. It is a stable fourth-order integration procedure that requires the evaluation of the right-hand side of the system only two times per step. This is a great advantage compared with other methods of the same order of accuracy, especially the Runge-Kutta method, which requires the evaluation of the right-hand side four times per step. Another advantage is that at each step the calculation procedure gives an estimate for the local truncation error; thus the procedure is able, without a significant amount of calculation time, to choose and change the step size h . On the other hand, Hamming's predictor-corrector method itself is not self-starting; that is, the functional values at a single previous point are not enough to get the functional values ahead. Therefore, to obtain the starting values, a special Runge-Kutta procedure followed by one iteration step is added to the predictor-corrector method.

Given the general system of first-order ordinary differential equations:

$$y_1' = \frac{dy_1}{dx} = f_1(x, y_1, y_2, \dots, y_n)$$

$$y_2' = \frac{dy_2}{dx} = f_2(x, y_1, y_2, \dots, y_n)$$

.....

$$y_n' = \frac{dy_n}{dx} = f_n(x, y_1, y_2, \dots, y_n)$$

and the initial values:

$$y_1(x_0) = y_{1,0}, y_2(x_0) = y_{2,0}, \dots, y_n(x_0) = y_{n,0}$$

and using the following vector notations:

$$Y(x) = \begin{pmatrix} y_1(x) \\ y_2(x) \\ \vdots \\ y_n(x) \end{pmatrix}, F(x, Y) = \begin{pmatrix} f_1(x, Y) \\ f_2(x, Y) \\ \vdots \\ f_n(x, Y) \end{pmatrix}, Y_0 = \begin{pmatrix} y_{1,0} \\ y_{2,0} \\ \vdots \\ y_{n,0} \end{pmatrix}$$

where Y , F , and Y_0 are column vectors, the given problem appears as follows:

$$Y' = \frac{dY}{dx} = F(x, Y) \text{ with } Y(x_0) = Y_0$$

For stability purposes, the modification by Hamming of Milne's classical modified predictor-corrector method is preferred. Thus, knowing the results at the equidistant points $x_{j-3}, x_{j-2}, x_{j-1}$ and x_j , the results at point $x_{j+1} = x_j + h$ are computed by the formulas below.

$$\begin{aligned} \text{Predictor: } P_{j+1} &= Y_{j-3} \\ &+ \frac{4h}{3} (2Y'_j - Y'_{j-1} + 2Y'_{j-2}) \end{aligned} \quad (1)$$

$$\begin{aligned} \text{Modifier: } M_{j+1} &= P_{j+1} - \frac{112}{121} (P_j - C_j); \\ M'_{j+1} &= F(x_{j+1}, M_{j+1}) \end{aligned} \quad (2), (3)$$

$$\begin{aligned} \text{Corrector: } C_{j+1} &= \frac{1}{8} [9Y_j - Y_{j-2} \\ &+ 3h(M'_{j+1} + 2Y'_j - Y'_{j-1})] \end{aligned} \quad (4)$$

$$\begin{aligned} \text{Final value: } Y_{j+1} &= C_{j+1} \\ &+ \frac{9}{121} (P_{j+1} - C_{j+1}) \end{aligned} \quad (5)$$

where Y , Y' , P , M , M' , F and C are column vectors with n components. Formulas (1) and (4) have local truncation errors:

$$T_1 = \frac{14}{45} h^5 Y^{(5)}(\xi_1) \text{ with } \xi_1 \in (x_{j-3}, x_{j+1})$$

and

$$T_2 = -\frac{1}{40} h^5 Y^{(5)}(\xi_2) \text{ with } \xi_2 \in (x_{j-2}, x_{j+1})$$

respectively, such that

$$C_{j+1} - P_{j+1} = \frac{121}{360} h^5 Y^{(5)}(\xi) \left[\xi \in (x_{j-3}, x_{j+1}) \right]$$

Assuming that $Y^{(5)}(x)$ does not vary to any great extent in the interval (x_{j-3}, x_{j+1}) , it follows that:

$$T_2 \approx \frac{9}{121} (P_{j+1} - C_{j+1})$$

This formula shows that the components of column vector $P_{j+1} - C_{j+1}$ are measures for the local truncation errors in the components of column vector Y_{j+1} , and therefore control of accuracy and adjustment of step size h can be done by generating the following test value:

$$\delta = \sum_{i=1}^n a_i \cdot |p_{j+1,i} - c_{j+1,i}| \quad (6)$$

where the coefficients a_i ($i = 1, 2, \dots, n$) are error-weights specified in the input of the procedure.

If δ is greater than a given tolerance $\epsilon \dagger$, increment h is halved and the procedure computes

$Y_{j+1/2}$ -- that is, $Y(x_j + \frac{h}{2})$ -- after having interpolated $Y_{j-1/2} = Y(x_j - \frac{h}{2})$ and $Y_{j-3/2} = Y(x_j - \frac{3}{2}h)$, with previous increment h , using the following sixth-order interpolation formulas):

$$Y_{j-1/2} = \frac{1}{256} (80Y_j + 135Y_{j-1} + 40Y_{j-2} + Y_{j-3}) + \frac{h}{2} \cdot \frac{15}{128} (-Y'_j + 6Y'_{j-1} + Y'_{j-2}) \quad (7)$$

$$Y_{j-3/2} = \frac{1}{256} (12Y_j + 135Y_{j-1} + 108Y_{j-2} + Y_{j-3}) + \frac{h}{2} \cdot \frac{3}{128} (-Y'_j - 18Y'_{j-1} + 9Y'_{j-2}) \quad (8)$$

If δ is less than ϵ , the result Y_{j+1} is assumed to be correct and is handed, together with x_{j+1} and the vector of derivatives $Y'_{j+1} = F(x_{j+1}, Y_{j+1})$, to a user-supplied output subroutine.

\dagger Numerical experience seems to show that the procedure does not exceed a global relative error approximately equal to ϵ .

If δ is less than $\epsilon/50$, the next step is carried out with the doubled increment; however, care is taken in the procedure that the increment never gets greater than the increment h specified as an input parameter, and further, that among the output are all points $x_0 + j \cdot h$ (where $j = 0, 1, 2, \dots$, and h is the input step size) which are situated between the lower and the upper bound of the integration interval.

Changing the step size by halving or doubling requires changing of $P_j - C_j$ or $P_{j+1} - C_{j+1}$, respectively. Using the following interpolation formula:

$$Y_j = Y_{j-3} + \frac{3}{8} h(Y'_{j-3} + 3Y'_{j-2} + 3Y'_{j-1} + Y'_j) - \frac{3}{80} h^5 Y^{(5)}(\xi_3) \left[\xi_3 \epsilon(x_{j-3}, x_j) \right]$$

and assuming that $Y^{(5)}(x)$ does not vary to any great extent in this interval, $P_j - C_j$ can be written as:

$$P_j - C_j \approx \frac{242}{27} (Y_j - Y_{j-3}) - \frac{121}{36} h(Y'_j + 3Y'_{j-1} + 3Y'_{j-2} + Y'_{j-3})$$

When halving increment h , this formula becomes:

$$P_j - C_j \approx \frac{242}{27} (Y_j - Y_{j-3/2}) - \frac{121}{36} \cdot \frac{h}{2} (Y'_j + 3Y'_{j-1/2} + 3Y'_{j-1} + Y'_{j-3/2}) \quad (9)$$

and when doubling:

$$P_{j+1} - C_{j+1} \approx \frac{242}{27} (Y_{j+1} - Y_{j-5}) - \frac{121}{36} \cdot 2h(Y'_{j+1} + 3Y'_{j-1} + 3Y'_{j-3} + Y'_{j-5}) \quad (10)$$

Starting Hamming's modified predictor-corrector method requires the functional and derivative values at four preceding equidistant points; that is, x_0, x_1, x_2 and x_3 . The values Y_0 and $Y'_0 = F(x_0, Y_0)$ are specified by input. For computation of $Y_1, Y'_1, Y_2, Y'_2, Y_3$ and Y'_3 and for adjustment of the step size h to accuracy requirements, a special Runge-Kutta procedure suggested by Ralston is used. Starting at x_j , result values at point $x_{j+1} = x_j + h$ are computed using the following formulas:

$$K_1 = h \cdot Y'_j \quad (11)$$

$$K_2 = h \cdot F(x_j + 0.4h, Y_j + 0.4K_1) \quad (12)$$

$$K_3 = h \cdot F(x_j + 0.45573725421878943h, Y_j + 0.29697760924775360 K_1 + 0.15875964497103583 K_2) \quad (13)$$

$$K_4 = h \cdot F(x_j + h, Y_j + 0.21810038822592047 K_1 - 3.0509651486929308 K_2 + 3.8328647604670103 K_3) \quad (14)$$

$$Y_{j+1} = Y_j + 0.17476028226269037 K_1 - 0.55148066287873294 K_2 + 1.2055355993965235 K_3 + 0.17118478121951903 K_4 \quad (15)$$

where $Y_j, Y_{j+1}, K_1, K_2, K_3$ and K_4 are all column vectors with n components.

These formulas are not very stable, but this does not matter because they are used only in three successive steps ($j = 0, 1, 2$). On the other hand, they have the smallest bound of truncation error of all fourth-order Runge-Kutta procedures. Therefore they are best suited to start other integration methods which are not self-starting.

For initial control of accuracy and adjustment of step size h , in starting the procedure an approximation for $Y_2 = Y(x_0 + h)$, named $Y_2^{(1)}$, is computed using the step size h , and then an approximation named $Y_2^{(2)}$, using the step size $h/2$ twice. From these two approximations a test value for accuracy is generated in the following way:

$$\delta = \frac{1}{15} \sum_{i=1}^n a_i \cdot |y_{2,i}^{(1)} - y_{2,i}^{(2)}| \quad (16)$$

If δ is greater than ϵ , increment h is halved, and the procedure starts again at point x_0 .

If δ is less than ϵ , the results $Y_1^{(2)} = Y(x_0 + \frac{h}{2})$ and $Y_2^{(2)} = Y(x_0 + h)$ are assumed to be correct, and a third step follows, which computes the results at point $x_0 + \frac{3}{2}h$ -- that is, $Y_3 = Y(x_0 + \frac{3}{2}h)$. The step size $h/2$ of these three steps is handed as initial step size h to the predictor-corrector method.

It is very important that the starting values be as accurate as possible, because errors in these starting values may increase during the following predictor-corrector procedure. Therefore the starting values computed by the Runge-Kutta method are refined by one iteration step using the following fourth-order interpolation formulas:

$$Y_1 = Y_0 + \frac{h}{24}(9 Y'_0 + 19 Y'_1 - 5 Y'_2 + Y'_3) \quad (17)$$

$$Y_2 = Y_0 + \frac{h}{3}(Y'_0 + 4 Y'_1 + Y'_2) \quad (18)$$

$$Y_3 = Y_0 + \frac{3h}{8}(Y'_0 + 3 Y'_1 + 3 Y'_2 + Y'_3) \quad (19)$$

Use of these must be considered an iteration procedure; that is, first the result values of the Runge-Kutta method are used in the right-hand side of formula (17) to compute a refined Y_1 . After computing the refined $Y'_1 = F(x_1, Y_1)$, the refined vector Y_2 is generated using formula (18). Finally, the refined $Y'_2 = F(x_2, Y_2)$ is used, together with the other values, in the right-hand side of formula (19) to compute the refined vector Y_3 . During this iteration, the refined data sets x_j, Y_j, Y'_j are handed, together with the number of bisections of the initial step size (specified by input), to the output subroutine.

It can be shown that, using this iterative procedure, the initial column vector $P_3 - C_3$ used in formula (2) for $j=3$ is equal to zero.

The entire input of the procedure is:

1. Lower and upper bound of the integration interval, initial step size h of the independent variable, and upper bound ϵ of the local truncation error
2. Initial values Y_0 of the dependent variables and weights a_i ($i = 1, 2, \dots, n$) for the local truncation errors in each component of the dependent variables
3. The number n of differential equations in the system
4. As external subroutine subprograms, the computation of the right-hand side of the system of differential equations; for flexibility in output, an output subroutine
5. An auxiliary storage array named AUX with 16 rows and n columns


```

C
C
DIMENSION PRMT(1),Y(1),DERY(1),AUX(16,1)
N=1
IHLF=0
X=PRMT(1)
H=PRMT(3)
PRMT(5)=0.
DO 1 I=1,NDIM
AUX(16,I)=0.
AUX(15,I)=DERY(I)
1 AUX(1,I)=Y(I)
IF(H*(PRMT(2)-X))3,2,4
C
C
ERROR RETURNS
2 IHLF=12
GOTO 4
3 IHLF=13
C
C
COMPUTATION OF DERY FOR STARTING VALUES
4 CALL FCT(X,Y,DERY)
C
C
RECORDING OF STARTING VALUES
CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)
IF(PRMT(5))6,5,6
5 IF(IHLF)7,7,6
6 RETURN
7 DO 8 I=1,NDIM
8 AUX(8,I)=DERY(I)
C
C
COMPUTATION OF AUX(2,1)
ISW=1
GOTO 100
C
C
9 X=X+H
DO 10 I=1,NDIM
10 AUX(2,I)=Y(I)
C
C
INCREMENT H IS TESTED BY MEANS OF BISECTION
11 IHLF=IHLF+1
X=X+H
DO 12 I=1,NDIM
12 AUX(4,I)=AUX(2,I)
H=.5*H
N=1
ISW=2
GOTO 100
C
C
13 X=X+H
CALL FCT(X,Y,DERY)
N=2
DO 14 I=1,NDIM
AUX(2,I)=Y(I)
14 AUX(9,I)=DERY(I)
ISW=3
GOTO 100
C
C
COMPUTATION OF TEST VALUE DELT
15 DELT=0.
DO 16 I=1,NDIM
16 DELT=DELT+AUX(15,I)*ABS(Y(I)-AUX(4,I))
DELT=.06666667*DELT
IF(DELT-PRMT(4))19,19,17
17 IF(IHLF-10)11,18,18
C
C
NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.
18 IHLF=11
X=X+H
GOTO 4
C
C
THERE IS SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS.
19 X=X+H
CALL FCT(X,Y,DERY)
DO 20 I=1,NDIM
AUX(3,I)=Y(I)
20 AUX(10,I)=DERY(I)
N=3
ISW=4
GOTO 100
C
C
21 N=1
X=X+H
CALL FCT(X,Y,DERY)
X=PRMT(1)
DO 22 I=1,NDIM
AUX(11,I)=DERY(I)
22CY(I)=AUX(1,I)+.375*AUX(8,I)+.7916667*AUX(9,I)
I=-.2083333*AUX(10,I)+.04166667*DERY(I)
23 X=X+H
N=N+1
CALL FCT(X,Y,DERY)
CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)
IF(PRMT(5))6,24,6
24 IF(N-4)25,200,200
25 DO 26 I=1,NDIM
AUX(N,I)=Y(I)
26 AUX(N+7,I)=DERY(I)
IF(N-3)27,29,200
C
C
27 DO 28 I=1,NDIM
DELT=AUX(9,I)+AUX(9,I)
DELT=DELT*DELT
28 Y(I)=AUX(11,I)+.3333333*H*(AUX(8,I)+DELT+AUX(10,I))
GOTO 23
C
C
29 DO 30 I=1,NDIM
DELT=AUX(9,I)+AUX(10,I)
DELT=DELT*DELT*DELT
30 Y(I)=AUX(11,I)+.375*H*(AUX(8,I)+DELT+AUX(11,I))
GOTO 23
C
C
THE FOLLOWING PART OF SUBROUTINE HPCG COMPUTES BY MEANS OF
RANGE-KUTTA METHOD STARTING VALUES FOR THE NOT SELF-STARTING
PREDICTOR-CORRECTOR METHOD.
100 DO 101 I=1,NDIM
Z=H*AUX(N+7,I)
AUX(5,I)=Z
101 Y(I)=AUX(N,I)+.4*Z
Z IS AN AUXILIARY STORAGE LOCATION
Z=X+.4*H
CALL FCT(Z,Y,DERY)
DO 102 I=1,NDIM
Z=H*DERY(I)
AUX(6,I)=Z
102 Y(I)=AUX(N,I)+.2969776*AUX(5,I)+.1587596*Z
Z=X+.4557372*H
CALL FCT(Z,Y,DERY)
HPCG1090
HPCG1100
HPCG1110
HPCG1120
HPCG1130
HPCG1140
HPCG1150
HPCG1160
HPCG1170
HPCG1180
HPCG1190
HPCG1200
HPCG1210
HPCG1220
HPCG1230
HPCG1240
HPCG1250
HPCG1260
HPCG1270
HPCG1280
HPCG1290
HPCG1300
HPCG1310
HPCG1320
HPCG1330
HPCG1340
HPCG1350
HPCG1360
HPCG1370
HPCG1380
HPCG1390
HPCG1400
HPCG1410
HPCG1420
HPCG1430
HPCG1440
HPCG1450
HPCG1460
HPCG1470
HPCG1480
HPCG1490
HPCG1500
HPCG1510
HPCG1520
HPCG1530
HPCG1540
HPCG1550
HPCG1560
HPCG1570
HPCG1580
HPCG1590
HPCG1600
HPCG1610
HPCG1620
HPCG1630
HPCG1640
HPCG1650
HPCG1660
HPCG1670
HPCG1680
HPCG1690
HPCG1700
HPCG1710
HPCG1720
HPCG1730
HPCG1740
HPCG1750
HPCG1760
HPCG1770
HPCG1780
HPCG1790
HPCG1800
HPCG1810
HPCG1820
HPCG1830
HPCG1840
HPCG1850
HPCG1860
HPCG1870
HPCG1880
HPCG1890
HPCG1900
HPCG1910
HPCG1920
HPCG1930
HPCG1940
HPCG1950
HPCG1960
HPCG1970
HPCG1980
HPCG1990
HPCG2000
HPCG2010
HPCG2020
HPCG2030
HPCG2040
HPCG2050
HPCG2060
HPCG2070
HPCG2080
HPCG2090
HPCG2100
HPCG2110
HPCG2120
HPCG2130
HPCG2140
HPCG2150
HPCG2160
HPCG2170
HPCG2180
HPCG2190
HPCG2200
HPCG2210
HPCG2220
HPCG2230
HPCG2240
HPCG2250
HPCG2260
HPCG2270
HPCG2280
HPCG2290
HPCG2300
HPCG2310
HPCG2320
HPCG2330
HPCG2340
HPCG2350
HPCG2360
HPCG2370
DO 103 I=1,NDIM
Z=H*DERY(I)
AUX(7,I)=Z
103 Y(I)=AUX(N,I)+.2181004*AUX(5,I)-.3.050965*AUX(6,I)+3.832865*Z
Z=X+H
CALL FCT(Z,Y,DERY)
DO 104 I=1,NDIM
104OY(I)=AUX(N,I)+.1747603*AUX(5,I)-.5514807*AUX(6,I)
I=1.20553AUX(7,I)-.1711848*H*DERY(I)
GOTO(9,13,15,21),ISW
C
C
POSSIBLE BREAK-POINT FOR LINKAGE
C
C
STARTING VALUES ARE COMPUTED.
NOW START HARRINGS MODIFIED PREDICTOR-CORRECTOR METHOD.
200 ISTEP=3
201 IF(N-8)204,202,204
C
C
N=8 CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS
202 DO 203 N=2,7
DO 203 I=1,NDIM
AUX(N-1,I)=AUX(N,I)
203 AUX(N+6,I)=AUX(N+7,I)
N=7
C
C
N LESS THAN 8 CAUSES N+1 TO GET N
204 N=N+1
C
C
COMPUTATION OF NEXT VECTOR Y
DO 205 I=1,NDIM
AUX(N-1,I)=Y(I)
205 AUX(N+6,I)=DERY(I)
X=X+H
206 ISTEP=ISTEP+1
DO 207 I=1,NDIM
ODELT=AUX(N-4,I)+.1.333333*H*(AUX(N+6,I)+AUX(N+6,I)-AUX(N+5,I)+
IAUX(N+6,I)+AUX(N+4,I))
Y(I)=DELT-.9256198*AUX(16,I)
207 AUX(16,I)=DELT
C
C
PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX; MODIFIED PREDICTOR
IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.
CALL FCT(X,Y,DERY)
DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY
DO 208 I=1,NDIM
ODELT=.125*H*.AUX(N-1,I)-AUX(N-3,I)+3.*H*(DERY(I)+AUX(N+6,I)+
IAUX(N+6,I)-AUX(N+5,I))
AUX(16,I)=AUX(16,I)-DELT
208 Y(I)=DELT+.07438017*AUX(16,I)
C
C
TEST WHETHER H MUST BE HALVED OR DOUBLED
DELT=C.
DO 209 I=1,NDIM
209 DELT=DELT+AUX(15,I)*ABS(AUX(15,I))
IF(DELT-PRMT(4))210,222,222
C
C
H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.
210 CALL FCT(X,Y,DERY)
CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)
IF(PRMT(5))212,211,212
211 IF(IHLF-11)213,212,212
212 RETURN
213 IF(H*(X-PRMT(2)))214,212,212
214 IF(ABS(X-PRMT(2)))-.1*ABS(H))212,215,215
215 IF(DELT-.02*PRMT(4))216,216,201
C
C
H COULD BE DOUBLED IF ALL NECESSARY PRECEEDING VALUES ARE
AVAILABLE
216 IF(IHLF)201,201,217
217 IF(N-7)201,218,218
218 IF(ISTEP-4)201,219,219
219 IMOD=ISTEP/2
IF(ISTEP-IMOD-IMOD)201,220,201
220 H=H*H
IHLF=IHLF-1
ISTEP=0
DO 221 I=1,NDIM
AUX(N-1,I)=AUX(N-2,I)
AUX(N-2,I)=AUX(N-4,I)
AUX(N-3,I)=AUX(N-6,I)
AUX(N+6,I)=AUX(N+5,I)
AUX(N+5,I)=AUX(N+3,I)
AUX(N+4,I)=AUX(N+1,I)
DELT=AUX(N+6,I)+AUX(N+5,I)
DELT=DELT*DELT*DELT
221OAU(16,I)=.962963*(Y(I)-AUX(N-3,I))-3.361111*H*(DERY(I)+DELT
I+AUX(N+4,I))
GOTO 201
C
C
H MUST BE HALVED
222 IHLF=IHLF+1
IF(IHLF-10)223,223,210
223 H=.5*H
ISTEP=0
DO 224 I=1,NDIM
OY(I)=.00390625*(80.*AUX(N-1,I)+135.*AUX(N-2,I)+40.*AUX(N-3,I)+
IAUX(N-4,I))-1.171875*(AUX(N+6,I)-6.*AUX(N+5,I)-AUX(N+4,I))*H
OAU(N-4,I)=.00390625*(12.*AUX(N-1,I)+135.*AUX(N-2,I)+
11*8.*AUX(N-3,I)+AUX(N-4,I))-0.234375*(AUX(N+6,I)+18.*AUX(N+5,I)-
29.*AUX(N+4,I))*H
AUX(N-3,I)=AUX(N-2,I)
224 AUX(N+4,I)=AUX(N+5,I)
X=X+H
DELT=X-(H*H)
CALL FCT(DELT,Y,DERY)
DO 225 I=1,NDIM
AUX(N-2,I)=Y(I)
AUX(N-5,I)=DERY(I)
225 Y(I)=AUX(N-4,I)
DELT=DELT-(H*H)
CALL FCT(DELT,Y,DERY)
DO 226 I=1,NDIM
DELT=AUX(N+5,I)+AUX(N+4,I)
DELT=DELT*DELT*DELT
OAU(16,I)=.962963*(AUX(N-1,I)-Y(I))-3.361111*H*(AUX(N+6,I)+DELT
I+DERY(I))
226 AUX(N-3,I)=DERY(I)
GOTO 206
END
HPCG2380
HPCG2390
HPCG2400
HPCG2410
HPCG2420
HPCG2430
HPCG2440
HPCG2450
HPCG2460
HPCG2470
HPCG2480
HPCG2490
HPCG2500
HPCG2510
HPCG2520
HPCG2530
HPCG2540
HPCG2550
HPCG2560
HPCG2570
HPCG2580
HPCG2590
HPCG2600
HPCG2610
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HPCG2770
HPCG2780
HPCG2790
HPCG2800
HPCG2810
HPCG2820
HPCG2830
HPCG2840
HPCG2850
HPCG2860
HPCG2870
HPCG2880
HPCG2890
HPCG2900
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HPCG2950
HPCG2960
HPCG2970
HPCG2980
HPCG2990
HPCG3000
HPCG3010
HPCG3020
HPCG3030
HPCG3040
HPCG3050
HPCG3060
HPCG3070
HPCG3080
HPCG3090
HPCG3100
HPCG3110
HPCG3120
HPCG3130
HPCG3140
HPCG3150
HPCG3160
HPCG3170
HPCG3180
HPCG3190
HPCG3200
HPCG3210
HPCG3220
HPCG3230
HPCG3240
HPCG3250
HPCG3260
HPCG3270
HPCG3280
HPCG3290
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HPCG3550
HPCG3560
HPCG3570
HPCG3580
HPCG3590
HPCG3600

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C		DHCG 10	C	COMPUTATION OF DERY FOR STARTING VALUES	
C		DHCG 20	C	4 CALL FCT(X,Y,DERY)	DHCG1300
C		DHCG 30	C		DHCG1310
C		DHCG 40	C		DHCG1320
C	SUBROUTINE DHPCG	DHCG 50	C	RECORDING OF STARTING VALUES	DHCG1330
C	PURPOSE	DHCG 60	C	CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)	DHCG1340
C	TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY GENERAL	DHCG 70	C	IF(PRMT(5))16,5,6	DHCG1350
C	DIFFERENTIAL EQUATIONS WITH GIVEN INITIAL VALUES.	DHCG 80	C	5 IF(IHLF)7,6	DHCG1360
C		DHCG 90	C	6 RETURN	DHCG1370
C	USAGE	DHCG 100	C	7 DO 8 I=1,NDIM	DHCG1380
C	CALL DHPCG (PRMT,Y,DERY,NDIM,IHLF,FCT,OUTP,AUX)	DHCG 110	C	8 AUX(8,I)=DERY(I)	DHCG1390
C	PARAMETERS FCT AND OUTP REQUIRE AN EXTERNAL STATEMENT.	DHCG 120	C		DHCG1400
C	DESCRIPTION OF PARAMETERS	DHCG 130	C	COMPUTATION OF AUX(2,I)	DHCG1410
C	PRMT - DOUBLE PRECISION INPUT AND OUTPUT VECTOR WITH	DHCG 140	C	ISW=1	DHCG1420
C	DIMENSION GREATER THAN OR EQUAL TO 5, WHICH	DHCG 150	C	GOTO 100	DHCG1430
C	SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF	DHCG 160	C		DHCG1440
C	ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN	DHCG 170	C	9 X=X+H	DHCG1450
C	OUTPUT SUBROUTINE (FURNISHED BY THE USER) AND	DHCG 180	C	DO 10 I=1,NDIM	DHCG1460
C	SUBROUTINE DHPCG, EXCEPT PRMT(5) THE COMPONENTS	DHCG 190	C	10 AUX(2,I)=Y(I)	DHCG1470
C	ARE NOT DESTROYED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 200	C		DHCG1480
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 210	C	INCREMENT H IS TESTED BY MEANS OF BISECTION	DHCG1490
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 220	C	11 IHLF=IHLF*1	DHCG1500
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 230	C	DO 12 I=1,NDIM	DHCG1510
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 240	C	12 AUX(4,I)=AUX(2,I)	DHCG1520
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 250	C	H=.500*H	DHCG1530
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 260	C	N=1	DHCG1540
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 270	C	ISW=2	DHCG1550
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 280	C	GOTO 100	DHCG1560
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 290	C		DHCG1570
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 300	C	13 X=X+H	DHCG1580
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 310	C	CALL FCT(X,Y,DERY)	DHCG1590
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 320	C	N=2	DHCG1600
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 330	C	DO 14 I=1,NDIM	DHCG1610
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 340	C	AUX(2,I)=DERY(I)	DHCG1620
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 350	C	ISW=3	DHCG1630
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 360	C	GOTO 100	DHCG1640
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 370	C		DHCG1650
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 380	C	COMPUTATION OF TEST VALUE DELT	DHCG1660
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 390	C	15 DELT=0.00	DHCG1670
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 400	C	DO 16 I=1,NDIM	DHCG1680
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 410	C	16 DELT=DELT+AUX(5,I)*DABS(Y(I)-AUX(4,I))	DHCG1690
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 420	C	DELT=.00666666666666666666700*DELT	DHCG1700
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 430	C	IF(DELT-PRMT(4))19,19,17	DHCG1710
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 440	C	17 IF(IHLF=10)11,18,18	DHCG1720
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 450	C		DHCG1730
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 460	C	NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.	DHCG1740
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 470	C	18 IHLF=11	DHCG1750
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 480	C	X=X+H	DHCG1760
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 490	C	GOTO 4	DHCG1770
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 500	C		DHCG1780
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 510	C	THERE IS SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS.	DHCG1790
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 520	C	19 X=X+H	DHCG1800
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 530	C	CALL FCT(X,Y,DERY)	DHCG1810
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 540	C	DO 20 I=1,NDIM	DHCG1820
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 550	C	AUX(3,I)=Y(I)	DHCG1830
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 560	C	AUX(3,I)=Y(I)	DHCG1840
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 570	C	20 AUX(10,I)=DERY(I)	DHCG1850
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 580	C	N=3	DHCG1860
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 590	C	ISW=4	DHCG1870
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 600	C	GOTO 100	DHCG1880
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 610	C		DHCG1890
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 620	C	21 N=1	DHCG1900
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 630	C	X=X+H	DHCG1910
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 640	C	CALL FCT(X,Y,DERY)	DHCG1920
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 650	C	X=PRMT(1)	DHCG1930
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 660	C	DO 22 I=1,NDIM	DHCG1940
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 670	C	AUX(11,I)=DERY(I)	DHCG1950
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 680	C	220Y(I)=AUX(11,I)+.37500*AUX(8,I)+.7916666666666666700*AUX(9,I)	DHCG1960
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 690	C	I=-208333333333333333300*AUX(10,I)+.0416666666666666666700*DERY(I)	DHCG1970
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 700	C		DHCG1980
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 710	C	23 X=X+H	DHCG1990
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 720	C	N=N+1	DHCG2000
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 730	C	CALL FCT(X,Y,DERY)	DHCG2010
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 740	C	CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)	DHCG2020
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 750	C	IF(PRMT(5))16,25,6	DHCG2030
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 760	C	24 IF(N-4)25,200,200	DHCG2040
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 770	C	DO 26 I=1,NDIM	DHCG2050
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 780	C	AUX(N,I)=Y(I)	DHCG2060
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 790	C	26 AUX(N+7,I)=DERY(I)	DHCG2070
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 800	C	IF(N-3)27,29,200	DHCG2080
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 810	C		DHCG2090
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 820	C	27 DO 28 I=1,NDIM	DHCG2100
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 830	C	DELTA=AUX(9,I)+AUX(9,I)	DHCG2110
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 840	C	DELTA=DELT+DELT	DHCG2120
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 850	C	28 Y(I)=AUX(11,I)+.333333333333333333300*H*(AUX(8,I)+DELT+AUX(10,I))	DHCG2130
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 860	C	GOTO 23	DHCG2140
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 870	C		DHCG2150
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 880	C	29 DO 30 I=1,NDIM	DHCG2160
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 890	C	DELT=AUX(9,I)+AUX(10,I)	DHCG2170
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 900	C	DELT=DELT+DELT+DELT	DHCG2180
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 910	C	30 Y(I)=AUX(11,I)+.37500*H*(AUX(8,I)+DELT+AUX(10,I))	DHCG2190
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 920	C	GOTO 23	DHCG2200
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 930	C		DHCG2210
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 940	C	THE FOLLOWING PART OF SUBROUTINE DHPCG COMPUTES BY MEANS OF	DHCG2220
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 950	C	RUNGE-KUTTA METHOD STARTING VALUES FOR THE NOT SELF-STARTING	DHCG2230
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 960	C	PREDICTOR-CORRECTOR METHOD.	DHCG2240
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 970	C	100 DO 101 I=1,NDIM	DHCG2250
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 980	C	Z=H*AUX(N+7,I)	DHCG2260
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 990	C	AUX(5,I)=Z	DHCG2270
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1000	C	101 Y(I)=AUX(N,I)+.400*Z	DHCG2280
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1010	C	Z IS AN AUXILIARY STORAGE LOCATION	DHCG2290
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1020	C		DHCG2300
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1030	C	Z=X+.400*H	DHCG2310
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1040	C	CALL FCT(Z,Y,DERY)	DHCG2320
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1050	C	DO 102 I=1,NDIM	DHCG2330
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1060	C	Z=H*DERY(I)	DHCG2340
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1070	C	AUX(6,I)=Z	DHCG2350
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1080	C	102 Y(I)=AUX(N,I)+.2969776092477536000*AUX(5,I)+.1587596449710358300*Z	DHCG2360
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1090	C		DHCG2370
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1100	C	Z=X+.4557372524187894300*H	DHCG2380
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1110	C	CALL FCT(Z,Y,DERY)	DHCG2390
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1120	C	DO 103 I=1,NDIM	DHCG2400
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1130	C	Z=H*DERY(I)	DHCG2410
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1140	C	AUX(7,I)=Z	DHCG2420
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1150	C	103 Y(I)=AUX(N,I)+.2181003882259204700*AUX(5,I)+.3.050965148692930800*Z	DHCG2430
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1160	C	AUX(6,I)+.3.832864760467010300*Z	DHCG2440
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1170	C		DHCG2450
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1180	C	Z=X+H	DHCG2460
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1190	C	CALL FCT(Z,Y,DERY)	DHCG2470
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1200	C	DO 104 I=1,NDIM	DHCG2480
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1210	C	1040Y(I)=AUX(N,I)+.1747602822626903700*AUX(5,I)+.5514806629787329400*Z	DHCG2490
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1220	C	AUX(6,I)+.1.205535599396523500*AUX(7,I)+.171184781219510300*Z	DHCG2500
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1230	C	Z=H*DERY(I)	DHCG2510
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1240	C	GOTO(9,13,15,21),ISW	DHCG2520
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1250	C		DHCG2530
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1260	C	POSSIBLE BREAK-POINT FOR LINKAGE	DHCG2540
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1270	C		DHCG2550
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1280	C	STARTING VALUES ARE COMPUTED.	DHCG2560
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1290	C	NOW START HAMMING'S MODIFIED PREDICTOR-CORRECTOR METHOD.	DHCG2570
C	CHANGED BY SUBROUTINE DHPCG AND THEY ARE	DHCG 1300	C	100 ISTEP=3	DHCG2580

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201 IF(N-8)204,202,204
C
C N=8 CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS
202 DO 203 N=2,7
DO 203 I=1,NDIM
AUX(N-1,I)=AUX(N,I)
203 AUX(N+6,I)=AUX(N+7,I)
N=7
C
C N LESS THAN 8 CAUSES N+1 TO GET N
204 N=N+1
C
C COMPUTATION OF NEXT VECTOR Y
DO 205 I=1,NDIM
AUX(N-1,I)=Y(I)
205 AUX(N+6,I)=DERY(I)
X=X+H
206 ISTEP=ISTEP+1
DO 207 I=1,NDIM
COELT=AUX(N-4,I)+1.333333333333333300*H*(AUX(N+6,I)+AUX(N+6,I)-
1AUX(N+5,I)+AUX(N+4,I)+AUX(N+4,I))
Y(I)=DELT-.925619834710743900*AUX(16,I)
207 AUX(16,I)=DELT
PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX, MODIFIED PREDICTOR
IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.
C
C CALL FCT(X,Y,DERY)
C DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY
C
DO 208 I=1,NDIM
ODELT=.12500*(9.00*AUX(N-1,I)-AUX(N-3,I)+3.00*H*(DERY(I)+AUX(N+6,I)
1+AUX(N+6,I)-AUX(N+5,I)))
AUX(16,I)=AUX(16,I)-DELT
208 Y(I)=DELT+.074390165289256200*AUX(16,I)
C
C TEST WHETHER H MUST BE HALVED OR DOUBLED
DELT=0.00
DO 209 I=1,NDIM
209 DELT=DELT+AUX(15,I)*DABS(AUX(16,I))
IF(DELT-PRMT(4))210,222,222
C
C H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.
210 CALL FCT(X,Y,DERY)
CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)
IF(PRMT(5))212,211,212
211 IF(IHLF-1)213,212,212
212 RETURN
213 IF(H*(X-PRMT(2))214,212,212
214 IF(DABS(X-PRMT(2))-100*DABS(H))212,215,215
215 IF(DELT-.0200*PRMT(4))216,216,201
C
C H COULD BE DOUBLED IF ALL NECESSARY PRECEEDING VALUES ARE
AVAILABLE
216 IF(IHLF)201,201,217
217 IF(N-7)201,218,218
218 IF(ISTEP-4)201,219,219
219 IMOD=ISTEP/2
IF(ISTEP-IMOD-IMOD)201,220,201
220 H=H*H
IHLF=IHLF-1
ISTEP=0
DO 221 I=1,NDIM
AUX(N-1,I)=AUX(N-2,I)
AUX(N-2,I)=AUX(N-4,I)
AUX(N-3,I)=AUX(N-6,I)
AUX(N+6,I)=AUX(N+5,I)
AUX(N+5,I)=AUX(N+3,I)
AUX(N+4,I)=AUX(N+1,I)
DELT=AUX(N+6,I)+AUX(N+5,I)
DELT=DELT+DELT+DELT
221O AUX(16,I)=8.96296296296296300*(Y(I)-AUX(N-3,I))
1-3.361111111111111100*H*(DERY(I)+DELT+AUX(N+4,I))
GOTO 201
C
C H MUST BE HALVED
222 IHLF=IHLF+1
IF(IHLF-10)223,223,210
223 H=.500*H
ISTEP=0
DO 224 I=1,NDIM
OY(I)=.3906250-2*(8.01*AUX(N-1,I)+135.00*AUX(N-2,I)+4.01*AUX(N-3,I)
1+AUX(N-4,I))-117187500*(AUX(N+6,I)-6.00*AUX(N+5,I)-AUX(N+4,I))H
O AUX(N-4,I)=.3906250-2*(12.00*AUX(N-1,I)+135.00*AUX(N-2,I)+
1108.00*AUX(N-3,I)+AUX(N-4,I))-023437500*(AUX(N+6,I)+
218.00*AUX(N+5,I)+9.00*AUX(N+4,I))H
AUX(N-3,I)=AUX(N-2,I)
224 AUX(N+4,I)=AUX(N+5,I)
X=X-H
DELT=X-(H+H)
CALL FCT(DELT,Y,DERY)
DO 225 I=1,NDIM
AUX(N-2,I)=Y(I)
AUX(N+5,I)=DERY(I)
225 Y(I)=AUX(N-4,I)
DELT=DELT-(H+H)
CALL FCT(DELT,Y,DERY)
DO 226 I=1,NDIM
DELT=AUX(N+5,I)+AUX(N+4,I)
DELT=DELT+DELT+DELT
O AUX(16,I)=8.96296296296296300*(AUX(N-1,I)-Y(I))
1-3.361111111111111100*H*(AUX(N+6,I)+DELT+DERY(I))
226 AUX(N+3,I)=DERY(I)
GOTO 206
END

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DHCG2590
DHCG2600
DHCG2610
DHCG2620
DHCG2630
DHCG2640
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DHCG2670
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DHCG3010
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DHCG3070
DHCG3080
DHCG3090
DHCG3100
DHCG3110
DHCG3120
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DHCG3150
DHCG3160
DHCG3170
DHCG3180
DHCG3190
DHCG3200
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DHCG3560
DHCG3570
DHCG3580
DHCG3590
DHCG3600
DHCG3610
DHCG3620
DHCG3630
DHCG3640

Subroutines HPCL and DHPCL

These subroutines use Hamming's modified predictor-corrector method for the solution of linear initial - value problems. The purpose of this version of Hamming's modified predictor-corrector method is to obtain an approximate solution of a linear system of first-order ordinary differential equations with given initial values.† It is a stable fourth-order integration procedure, requiring the evaluation of the right-hand side of the system only two times per step. This is a great advantage compared with other methods of the same order of accuracy, especially the Runge-Kutta method, which requires the evaluation of the right-hand side four times per step. Another advantage is that at each step the calculation procedure gives an estimate for the local truncation error; thus the procedure is able -- without a significant amount of calculation time -- to choose and change the step size h. On the other hand, Hamming's predictor-corrector method is not self-starting; that is, the functional values at a single previous point are not enough to obtain the functional values ahead. Therefore, to get the starting values, a special Runge-Kutta procedure followed by one iteration step is added to the predictor-corrector method.

Given the linear system of first-order ordinary differential equations:

$$y'_1 = \frac{dy_1}{dx} = a_{11}(x)y_1 + a_{12}(x)y_2 + \dots + a_{1n}(x)y_n + f_1(x)$$

$$y'_2 = \frac{dy_2}{dx} = a_{21}(x)y_1 + a_{22}(x)y_2 + \dots + a_{2n}(x)y_n + f_2(x)$$

.....

$$y'_n = \frac{dy_n}{dx} = a_{n1}(x)y_1 + a_{n2}(x)y_2 + \dots + a_{nn}(x)y_n + f_n(x)$$

† Solution can be done with subroutines HPCG and DHPCG too. The main reason for this special version, suitable to systems of linear differential equations, is that external subroutines furnished by the user for the solution of linear boundary-value problems can be used without changes by subroutine HPCL or DHPCL for the solution of corresponding linear initial-value problems.

and the initial values:

$$y_1(x_0) = y_{1,0}, y_2(x_0) = y_{2,0}, \dots, y_n(x_0) = y_{n,0}$$

and using the following vector and matrix notations:

$$Y(x) = \begin{pmatrix} y_1(x) \\ y_2(x) \\ \vdots \\ y_n(x) \end{pmatrix}, \quad f(x) = \begin{pmatrix} f_1(x) \\ f_2(x) \\ \vdots \\ f_n(x) \end{pmatrix},$$

$$A(x) = \begin{pmatrix} a_{11}(x) & a_{12}(x) & \dots & a_{1n}(x) \\ a_{21}(x) & a_{22}(x) & \dots & a_{2n}(x) \\ \dots & \dots & \dots & \dots \\ a_{n1}(x) & a_{n2}(x) & \dots & a_{nn}(x) \end{pmatrix}$$

$$\text{and } Y_0 = \begin{pmatrix} y_{1,0} \\ y_{2,0} \\ \vdots \\ y_{n,0} \end{pmatrix}$$

where Y , F and Y_0 are column vectors and A is an n by n square matrix, the given problem appears as follows:

$$Y' = \frac{dY}{dx} = A(x) * Y + F(x) \text{ with } Y(x_0) = Y_0$$

For stability purposes, the modification by Hamming of Milne's classical modified predictor-corrector method is preferred. Thus, knowing the results at the equidistant points x_{j-3} , x_{j-2} , x_{j-1} and x_j , the results at point $x_{j+1} = x_j + h$ are computed by the formulas given below.

$$\begin{aligned} \text{Predictor: } P_{j+1} &= Y_{j-3} + \frac{4h}{3} (2Y'_j - Y'_{j-1} \\ &\quad + 2Y'_{j-2}) \end{aligned} \quad (1)$$

$$\text{Modifier: } M_{j+1} = P_{j+1} - \frac{112}{121} (P_j - C_j) \quad (2)$$

$$M'_{j+1} = A(x_{j+1}) * M_{j+1} + F(x_{j+1}) \quad (3)$$

$$\begin{aligned} \text{Corrector: } C_{j+1} &= \frac{1}{8} \left[9Y_j - Y_{j-2} + 3h \right. \\ &\quad \left. (M'_{j+1} + 2Y'_j - Y'_{j-1}) \right] \end{aligned} \quad (4)$$

$$\text{Final Value: } Y_{j+1} = C_{j+1} + \frac{9}{121} (P_{j+1} - C_{j+1}) \quad (5)$$

where Y , Y' , P , M , M' and C are all column vectors with n components, and A is an n by n square matrix. Formulas (1) and (4) have local truncation errors:

$$T_1 = \frac{14}{45} h^5 Y^{(5)}(\xi_1) \text{ with } \xi_1 \in (x_{j-3}, x_{j+1})$$

and

$$T_2 = -\frac{1}{40} h^5 Y^{(5)}(\xi_2) \text{ with } \xi_2 \in (x_{j-2}, x_{j+1})$$

respectively such that

$$C_{j+1} - P_{j+1} = \frac{121}{360} h^5 Y^{(5)}(\xi) \text{ with } \xi \in (x_{j-3}, x_{j+1})$$

Assuming that $Y^{(5)}(x)$ does not vary to any great extent in the interval (x_{j-3}, x_{j+1}) , it follows that:

$$T_2 \approx \frac{9}{121} (P_{j+1} - C_{j+1})$$

This formula shows that the components of column vector $P_{j+1} - C_{j+1}$ are measures for the local truncation errors in the components of column vector Y_{j+1} . Therefore, control of accuracy and adjustment of step size h can be done by generating the following test value:

$$\delta = \sum_{i=1}^n a_i \cdot |P_{j+1,i} - C_{j+1,i}| \quad (6)$$

where the coefficients a_i ($i = 1, 2, \dots, n$) are error-weights specified in the input of the procedure.

If δ is greater than a given tolerance ϵ^\dagger , increment h is halved and the procedure computes $Y_{j-\frac{1}{2}}$ -- that is, $Y(x_j + \frac{h}{2})$ -- after having interpolated $Y_{j-\frac{1}{2}} = Y(x_j - \frac{h}{2})$ and $Y_{j-\frac{3}{2}} = Y(x_j - \frac{3h}{2})$, with previous increment h , using the following sixth-order interpolation formulas:

$$\begin{aligned} Y_{j-\frac{1}{2}} &= \frac{1}{256} (80Y_j + 135Y_{j-1} + 40Y_{j-2} + Y_{j-3}) \\ &\quad + \frac{h}{2} \cdot \frac{15}{128} (-Y'_j + 6Y'_{j-1} + Y'_{j-2}) \end{aligned} \quad (7)$$

[†] Numerical experience seems to show that the procedure does not exceed a global relative error approximately equal to ϵ .

$$Y_{j-3} = \frac{1}{256} (12 Y_j + 135 Y_{j-1} + 108 Y_{j-2} + Y_{j-3}) + \frac{h}{2} \cdot \frac{3}{128} (-Y'_j - 18 Y'_{j-1} + 9 Y'_{j-2}) \quad (8)$$

If δ is less than ϵ , the result Y_{j+1} is assumed to be correct and is handed, together with x_{j+1} and the vector of derivatives Y'_{j+1} , to a user-supplied output subroutine.

If δ is less than $\epsilon/50$, the next step is carried out with the doubled increment. However, care is taken in the procedure, so that the increment never becomes greater than the increment h specified as an input parameter, and further that among the output are all points $x_0 + j \cdot h$ (where $j = 0, 1, 2, \dots$, and h is the input step size) which are situated between the lower and the upper bound of the integration interval.

Changing the step size by halving or doubling requires changing of $P_j - C_j$ or $P_{j+1} - C_{j+1}$ respectively. Using the following interpolation formula:

$$Y_j = Y_{j-3} + \frac{3}{8} h (Y'_{j-3} + 3 Y'_{j-2} + 3 Y'_{j-1} + Y'_j) - \frac{3}{80} h^5 Y^{(5)}(\xi_3)$$

with

$$\xi_3 \in (x_{j-3}, x_j)$$

and assuming that $Y^{(5)}(x)$ does not vary to any great extent in this interval, $P_j - C_j$ can be written in the following form:

$$P_j - C_j \approx \frac{242}{27} (Y_j - Y_{j-3}) - \frac{121}{36} h (Y'_j + 3 Y'_{j-1} + 3 Y'_{j-2} + Y'_{j-3})$$

When halving increment h , this formula becomes:

$$P_j - C_j \approx \frac{242}{27} (Y_j - Y_{j-\frac{3}{2}}) - \frac{121}{36} \cdot \frac{h}{2} (Y'_j + 3 Y'_{j-\frac{3}{2}} + 3 Y'_{j-1} + Y'_{j-\frac{3}{2}}) \quad (9)$$

and when doubling:

$$P_{j+1} - C_{j+1} \approx \frac{242}{27} (Y_{j+1} - Y_{j-5}) - \frac{121}{36} \cdot 2 h (Y'_{j+1} + 3 Y'_{j-1} + 3 Y'_{j-3} + Y'_{j-5}) \quad (10)$$

Starting Hamming's modified predictor-corrector method requires the functional and derivative values at four preceding equidistant points: x_0, x_1, x_2 and x_3 . The values Y_0 and $Y'_0 = A(x_0) * Y_0 + F(x_0)$ are specified by input. For computation of $Y_1, Y'_1, Y_2, Y'_2, Y_3$ and Y'_3 and for adjustment of step size h to accuracy requirements, a special Runge-Kutta procedure suggested by Ralston is used. Starting at x_j , result values at point $x_{j+1} = x_j + h$ are computed using the following formulas:

$$K_1 = h \cdot Y'_j \quad (11)$$

$$K_2 = h \cdot \left[A(x_j + 0.4 h) * (Y_j + 0.4 K_1) + F(x_j + 0.4 h) \right] \quad (12)$$

$$K_3 = h \cdot \left[A(x_j + 0.45573725421878943 h) * (Y_j + 0.29697760924775360 K_1 + 0.15875964497103583 K_2) + F(x_j + 0.45573725421878943 h) \right] \quad (13)$$

$$K_4 = h \cdot \left[A(x_j + h) * (Y_j + 0.21810038822592047 K_1 - 3.0509651486929308 K_2 + 3.8328647604670103 K_3) + F(x_j + h) \right] \quad (14)$$

$$Y_{j+1} = Y_j + 0.17476028226269037 K_1 - 0.55148066287873294 K_2 + 1.2055355993965235 K_3 + 0.17118478121951903 K_4 \quad (15)$$

where $Y_j, Y_{j+1}, Y'_j, K_1, K_2, K_3$ and K_4 are all column vectors with n components, and A is an n by n square matrix. These formulas are not very stable, but this does not matter because they are used only in three successive steps ($j = 0, 1, 2$). On the other hand, they have the smallest bound of truncation errors of all fourth-order Runge-Kutta procedures. Therefore they are best suited to start other integration methods which are not self-starting.

For initial control of accuracy and adjustment of step size h , in starting the procedure an approximation for $Y_2 = Y(x_0 + h)$ called $Y_2^{(1)}$ is computed using the step size h , and then an approximation called $Y_2^{(2)}$, using the step size $h/2$ twice. From these two approximations, a test value δ for accuracy is generated in the following way:

$$\delta = \frac{1}{15} \sum_{i=1}^n a_i \cdot |y_{2,i}^{(1)} - y_{2,i}^{(2)}| \quad (16)$$

If δ is greater than ϵ , increment h is halved and the procedure starts anew at point x_0 .

If δ is less than ϵ , the results $Y_1^{(2)} = Y(x_0 + \frac{h}{2})$ and $Y_2^{(2)} = Y(x_0 + h)$ are assumed to be correct and a third step follows which computes the results at point $x_0 + \frac{3h}{2}$ -- that is, $Y_3 = Y(x_0 + \frac{3}{2}h)$.

The step size $h/2$ of these three steps is used as initial step size h in the predictor-corrector method.

It is very important that the starting values be as accurate as possible, because errors in these starting values may increase during the following predictor-corrector procedure. Therefore the starting values computed by the Runge-Kutta method are refined by one iteration step using the following fourth-order interpolation formulas:

$$Y_1 = Y_0 + \frac{h}{24} (9 Y'_0 + 19 Y'_1 - 5 Y'_2 + Y'_3) \quad (17)$$

$$Y_2 = Y_0 + \frac{h}{3} (Y'_0 + 4 Y'_1 + Y'_2) \quad (18)$$

$$Y_3 = Y_0 + \frac{3h}{8} (Y'_0 + 3 Y'_1 + 3 Y'_2 + Y'_3) \quad (19)$$

which must be considered as an iteration procedure. That is, first the result values of the Runge-Kutta method are handed to the right-hand side of formula (17) to compute a refined Y_1 . After having computed the refined Y_1 , the refined vector Y_2 is generated using formula (18). Finally, refined Y'_2 is used, together with the other values, in the right-hand side of formula (19) to compute the refined vector Y_3 . During this iteration, the refined data sets x_j , Y_j , Y'_j are handed, together with the number of bisections of the initial step size (specified by input), to the output subroutine.

It can be shown that, using this iterative procedure, the initial column vector $P_3 - C_3$ used in formula (2) for $j = 3$ is equal to zero.

The entire input of the procedure is:

1. Lower and upper bound of the integration interval, initial step size h of the independent variable, and upper bound ϵ of the local truncation error
2. Initial values Y_0 of the dependent variables and weights a_i ($i = 1, 2, \dots, n$) for the local truncation errors in each component of the dependent variables
3. The number n of differential equations in the system

4. As external subroutine subprograms, the computation of the right-hand side matrix A of the system of linear differential equations and of the inhomogeneous vector F ; for flexibility in output, an output subroutine

5. An auxiliary storage array with 16 rows and n columns

6. An n by n matrix as auxiliary storage array

Output is done in the following way. If a set of approximations to the dependent variables $Y(x)$ is found to be of sufficient accuracy, it is handed -- together with x , the derivative $Y'(x)$, the number of bisections of the initial increment, the number of differential equations, the lower and upper bound of the interval, the initial step size, error bound ϵ , and a parameter for terminating subroutine HPCL or DHPCL -- to the output subroutine. By means of this output subroutine, the user has the opportunity to choose his own output format, to handle the output values as he wants, to change the upper error bound and to terminate subroutine HPCL or DHPCL at any output point. In particular, the user is able to drop the output of some intermediate points, printing only the result values at the special points $x_0 + j \cdot h$, where $j = 0, 1, 2, \dots$, and h is the initial step size specified by input. The user may also perform intermediate computation using the integration results before continuing the process. For better understanding of the flowchart and of the FORTRAN program, see the allocation of special intermediate result vectors within the storage array AUX, shown previously in Figure 12.

For reference see:

- (1) A. Ralston/H.S. Wilf, Mathematical Methods for Digital Computers, Wiley, New York/London, 1960, pp. 95 - 109.
- (2) A. Ralston, "Runge-Kutta Methods with Minimum Error Bounds", MTAC, vol. 16, no. 80 (1962), pp. 431 - 437.

HPCL 10	MS=0.	HPCL 1300
HPCL 20	DO 2 L=1,NDIM	HPCL 1310
HPCL 30	LL=LL+NDIM	HPCL 1320
HPCL 40	2 HS=HS+ALL *Y(L)	HPCL 1330
HPCL 50	3 DERY(1)=DERY(M)	HPCL 1340
HPCL 60	GOTO(105,202,204,206,115,122,125,308,312,327,329,128),15W2	HPCL 1350
HPCL 70	C POSSIBLE BREAK-POINT FOR LINKAGE	HPCL 1360
HPCL 80	C	HPCL 1370
HPCL 90	C	HPCL 1380
HPCL 100	100 N=1	HPCL 1390
HPCL 110	IHLF=0	HPCL 1400
HPCL 120	X=PRMT(1)	HPCL 1410
HPCL 130	H=PRMT(3)	HPCL 1420
HPCL 140	PRMT(5)=0.	HPCL 1430
HPCL 150	DO 101 I=1,NDIM	HPCL 1440
HPCL 160	AUX(16,I)=0.	HPCL 1450
HPCL 170	AUX(15,I)=DERY(I)	HPCL 1460
HPCL 180	101 AUX(1,I)=Y(I)	HPCL 1470
HPCL 190	IF(H*(PRMT(2)-X) I03,102,104	HPCL 1480
HPCL 200	C	HPCL 1490
HPCL 210	C ERROR RETURNS	HPCL 1500
HPCL 220	102 IHLF=12	HPCL 1510
HPCL 230	GOTO 104	HPCL 1520
HPCL 240	103 IHLF=13	HPCL 1530
HPCL 250	C	HPCL 1540
HPCL 260	C COMPUTATION OF DERY FOR STARTING VALUES	HPCL 1550
HPCL 270	104 ISW2=1	HPCL 1560
HPCL 280	GOTO 1	HPCL 1570
HPCL 290	C	HPCL 1580
HPCL 300	C RECORDING OF STARTING VALUES	HPCL 1590
HPCL 310	105 CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)	HPCL 1600
HPCL 320	IF(PRMT(5) I07,106,107	HPCL 1610
HPCL 330	106 IF(IHLF I08,108,107	HPCL 1620
HPCL 340	107 RETURN	HPCL 1630
HPCL 350	108 DO 109 I=1,NDIM	HPCL 1640
HPCL 360	109 AUX(8,I)=DERY(I)	HPCL 1650
HPCL 370	C	HPCL 1660
HPCL 380	C COMPUTATION OF AUX(2,I)	HPCL 1670
HPCL 390	ISW1=1	HPCL 1680
HPCL 400	GOTO 200	HPCL 1690
HPCL 410	C	HPCL 1700
HPCL 420	110 X=X+H	HPCL 1710
HPCL 430	DO 111 I=1,NDIM	HPCL 1720
HPCL 440	111 AUX(2,I)=Y(I)	HPCL 1730
HPCL 450	C	HPCL 1740
HPCL 460	C INCREMENT H IS TESTED BY MEANS OF BISECTION	HPCL 1750
HPCL 470	112 IHLF=IHLF+1	HPCL 1760
HPCL 480	X=X-H	HPCL 1770
HPCL 490	DO 113 I=1,NDIM	HPCL 1780
HPCL 500	113 AUX(4,I)=AUX(2,I)	HPCL 1790
HPCL 510	H=.5*H	HPCL 1800
HPCL 520	N=1	HPCL 1810
HPCL 530	ISW1=2	HPCL 1820
HPCL 540	GOTO 200	HPCL 1830
HPCL 550	C	HPCL 1840
HPCL 560	114 X=X+H	HPCL 1850
HPCL 570	ISW2=5	HPCL 1860
HPCL 580	GOTO 1	HPCL 1870
HPCL 590	115 N=2	HPCL 1880
HPCL 600	DO 116 I=1,NDIM	HPCL 1890
HPCL 610	AUX(2,I)=Y(I)	HPCL 1900
HPCL 620	116 AUX(9,I)=DERY(I)	HPCL 1910
HPCL 630	ISW1=3	HPCL 1920
HPCL 640	GOTO 200	HPCL 1930
HPCL 650	C	HPCL 1940
HPCL 660	C COMPUTATION OF TEST VALUE DELT	HPCL 1950
HPCL 670	117 DELT=0.	HPCL 1960
HPCL 680	DO 118 I=1,NDIM	HPCL 1970
HPCL 690	118 DELT=DELT+AUX(15,I)*ABS(Y(I)-AUX(4,I))	HPCL 1980
HPCL 700	DELT=.0666667*DELT	HPCL 1990
HPCL 710	IF(DELT=PRMT(4) I21,I21,119	HPCL 2000
HPCL 720	119 IF(IHLF=10 I12,120,120	HPCL 2010
HPCL 730	C	HPCL 2020
HPCL 740	C NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.	HPCL 2030
HPCL 750	120 IHLF=11	HPCL 2040
HPCL 760	X=X+H	HPCL 2050
HPCL 770	GOTO 104	HPCL 2060
HPCL 780	C	HPCL 2070
HPCL 790	C SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS	HPCL 2080
HPCL 800	121 X=X+H	HPCL 2090
HPCL 810	ISW2=6	HPCL 2100
HPCL 820	GOTO 1	HPCL 2110
HPCL 830	122 DO 123 I=1,NDIM	HPCL 2120
HPCL 840	AUX(3,I)=Y(I)	HPCL 2130
HPCL 850	123 AUX(10,I)=DERY(I)	HPCL 2140
HPCL 860	N=3	HPCL 2150
HPCL 870	ISW1=4	HPCL 2160
HPCL 880	GOTO 200	HPCL 2170
HPCL 890	C	HPCL 2180
HPCL 900	C	HPCL 2190
HPCL 910	124 N=1	HPCL 2200
HPCL 920	X=X+H	HPCL 2210
HPCL 930	ISW2=7	HPCL 2220
HPCL 940	GOTO 1	HPCL 2230
HPCL 950	125 X=PRMT(1)	HPCL 2240
HPCL 960	DO 126 I=1,NDIM	HPCL 2250
HPCL 970	AUX(11,I)=DERY(I)	HPCL 2260
HPCL 980	126 Y(I)=AUX(1,I)+H*(.375*AUX(8,I)+.7916667*AUX(9,I)	HPCL 2270
HPCL 990	I-.2083333*AUX(10,I)+.04166667*DERY(I))	HPCL 2280
HPCL 1000	127 X=X+H	HPCL 2290
HPCL 1010	N=N+1	HPCL 2300
HPCL 1020	ISW2=12	HPCL 2310
HPCL 1030	GOTO 1	HPCL 2320
HPCL 1040	128 CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)	HPCL 2330
HPCL 1050	IF(PRMT(5) I07,129,107	HPCL 2340
HPCL 1060	129 IF(N=4)130,300,300	HPCL 2350
HPCL 1070	130 DO 131 I=1,NDIM	HPCL 2360
HPCL 1080	AUX(N,I)=Y(I)	HPCL 2370
HPCL 1090	131 AUX(N+7,I)=DERY(I)	HPCL 2380
HPCL 1100	IF(N=3)132,134,300	HPCL 2390
HPCL 1110	C	HPCL 2400
HPCL 1120	132 DO 133 I=1,NDIM	HPCL 2410
HPCL 1130	DELT=AUX(9,I)+AUX(9,I)	HPCL 2420
HPCL 1140	DELT=DELT*DELT	HPCL 2430
HPCL 1150	133 Y(I)=AUX(1,I)+.3333333*H*(AUX(8,I)+DELT+AUX(10,I))	HPCL 2440
HPCL 1160	GOTO 127	HPCL 2450
HPCL 1170	C	HPCL 2460
HPCL 1180	134 DO 135 I=1,NDIM	HPCL 2470
HPCL 1190	DELT=AUX(9,I)+AUX(10,I)	HPCL 2480
HPCL 1200	DELT=DELT*DELT*DELT	HPCL 2490
HPCL 1210	135 Y(I)=AUX(1,I)+.375*H*(AUX(8,I)+DELT+AUX(11,I))	HPCL 2500
HPCL 1220	GOTO 127	HPCL 2510
HPCL 1230	C	HPCL 2520
HPCL 1240	C THE FOLLOWING PART OF SUBROUTINE HPCL COMPUTES BY MEANS OF	HPCL 2530
HPCL 1250	C RUNGE-KUTTA METHOD STARTING VALUES FOR THE NOT SELF-STARTING	HPCL 2540
HPCL 1260	C PREDICTOR-CORRECTOR METHOD.	HPCL 2550
HPCL 1270	200 Z=X	HPCL 2560
HPCL 1280	DO 201 I=1,NDIM	HPCL 2570
HPCL 1290	X=H*AUX(N+7,I)	HPCL 2580
	AUX(5,I)=X	HPCL 2590

SUBROUTINE HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A)
THE FOLLOWING FIRST PART OF SUBROUTINE HPCL (UNTIL FIRST BREAK-
POINT FOR LINKAGE) HAS TO STAY IN CORE DURING THE WHOLE
COMPUTATION
DIMENSION PRMT(1),Y(1),DERY(1),AUX(16,1),A(1)
GOTO 100
THIS PART OF SUBROUTINE HPCL COMPUTES THE RIGHT HAND SIDE DERY OF
THE GIVEN SYSTEM OF LINEAR DIFFERENTIAL EQUATIONS.
1 CALL AFCT(X,A)
CALL FCT(X,DERY)
DO 3 M=1,NDIM
LL=M-NDIM

```

201 Y(I)=AUX(N,I)+.4*X
C X IS AN AUXILIARY STORAGE LOCATION
C X=Z+.4*H
ISW2=2
GOTO 1
202 DO 203 I=1,NDIM
X=H*DERY(I)
AUX(16,I)=X
203 Y(I)=AUX(N,I)+.2969776*AUX(5,I)+.1587596*X
C X=Z+.4557372*H
ISW2=3
GOTO 1
204 DO 205 I=1,NDIM
X=H*DERY(I)
AUX(7,I)=X
205 Y(I)=AUX(N,I)+.2181004*AUX(5,I)-.3.050965*AUX(6,I)+3.832865*X
C X=Z+H
ISW2=4
GOTO 1
206 DO 207 I=1,NDIM
207CV(I)=AUX(N,I)+.1747603*AUX(5,I)-.5514807*AUX(6,I)
I=1.205536*AUX(7,I)+.1711848*H*DERY(I)
X=Z
GOTO(110,114,117,124),ISW1
C POSSIBLE BREAK-POINT FOR LINKAGE
C STARTING VALUES ARE COMPUTED.
NOW START HAMMING'S MODIFIED PREDICTOR-CORRECTOR METHOD.
300 ISTEP=3
301 IF(N-8)304,302,304
C N=8 CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS
302 DO 303 N=2,7
DO 303 I=1,NDIM
AUX(N-1,I)=AUX(N,I)
303 AUX(N+6,I)=AUX(N+7,I)
N=7
C N LESS THAN 8 CAUSES N+1 TO GET N
304 N=N+1
C COMPUTATION OF NEXT VECTOR Y
DO 305 I=1,NDIM
AUX(N-1,I)=Y(I)
305 AUX(N+6,I)=DERY(I)
X=X+H
306 ISTEP=ISTEP+1
DO 307 I=1,NDIM
ODELT=AUX(N-4,I)+1.333333*H*(AUX(N+6,I)+AUX(N+6,I))-AUX(N+5,I)+
1AUX(N+4,I)+1AUX(N+4,I)
Y(I)=DELT-.9256198*AUX(16,I)
307 AUX(16,I)=DELT
PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX, MODIFIED PREDICTOR
IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.
ISW2=8
GOTO 1
C DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY
308 DO 309 I=1,NDIM
ODELT=.125*(9.*AUX(N-1,I)-AUX(N-3,I))+3.*H*(DERY(I)+AUX(N+6,I)+
1AUX(N+6,I)-AUX(N+5,I))
AUX(16,I)=AUX(16,I)-DELT
309 Y(I)=DELT+.07438017*AUX(16,I)
C TEST WHETHER H MUST BE HALVED OR DOUBLED
DELT=0.
DO 310 I=1,NDIM
310 DELT=DELT+AUX(15,I)*ABS(AUX(16,I))
IF(DELT-PRMT(4))311,324,324
C H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.
311 ISW2=9
GOTO 1
312 CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)
IF(PRMT(5))314,313,314
313 IF(IHLF=1)315,314,314
314 RETURN
315 IF(N-K-PRMT(2))316,314,314
316 IF(ABS(X-PRMT(2))-1)*ABS(H)314,317,317
317 IF(DELT-.02*PRMT(4))318,318,301
C H COULD BE DOUBLED IF ALL NECESSARY PRECEEDING VALUES ARE
AVAILABLE
318 IF(IHLF=301,301,319)
319 IF(N-7)301,320,320
320 IF(ISTEP=4)301,321,321
321 IMOD=ISTEP/2
IF(ISTEP=IMOD-IMOD)301,322,301
322 H=H*H
IHLF=IHLF-1
ISTEP=0
DO 323 I=1,NDIM
AUX(N-1,I)=AUX(N-2,I)
AUX(N-2,I)=AUX(N-4,I)
AUX(N-3,I)=AUX(N-6,I)
AUX(N+6,I)=AUX(N+5,I)
AUX(N+5,I)=AUX(N+3,I)
AUX(N+4,I)=AUX(N+1,I)
DELT=AUX(N+6,I)+AUX(N+5,I)
DELT=DELT+DELT+DELT
323OAU(16,I)=8.962963*(Y(I)-AUX(N-3,I))-3.361111*H*(DERY(I)+DELT
1+AUX(N+4,I))
GOTO 301
C H MUST BE HALVED
324 IHLF=IHLF+1
IF(IHLF=10)325,325,311
325 H=.5*H
ISTEP=0
DO 326 I=1,NDIM
OY(I)=.00390625*(80.*AUX(N-1,I)+135.*AUX(N-2,I)+40.*AUX(N-3,I)+
1AUX(N-4,I))-1171875*(AUX(N+6,I)-6.*AUX(N+5,I)-AUX(N+4,I))*H
OAU(N-4,I)=.00390625*(12.*AUX(N-1,I)+135.*AUX(N-2,I)+
1108.*AUX(N-3,I)+AUX(N-4,I))-0234375*(AUX(N+6,I)+18.*AUX(N+5,I)-
29.*AUX(N+4,I))+H
AUX(N-3,I)=AUX(N-2,I)
326 AUX(N+4,I)=AUX(N+5,I)
DELT=X+H
X=DELT-(H+H)
ISW2=10
GOTO 1
327 DO 328 I=1,NDIM
AUX(N-2,I)=Y(I)

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AUX(N+5,I)=DERY(I)
328 Y(I)=AUX(N-4,I)
X=X-(H+H)
ISW2=11
GOTO 1
329 X=DELT
DO 330 I=1,NDIM
DELT=AUX(N+5,I)+AUX(N+4,I)
DELT=DELT+DELT+DELT
OAU(16,I)=8.962963*(AUX(N-1,I)-Y(I))-3.361111*H*(AUX(N+6,I)+DELT
1+DERY(I))
330 AUX(N+3,I)=DERY(I)
GOTO 306
END
C
C .....
C DHCL 20
C DHCL 20
SUBROUTINE DHPCCL
C DHCL 30
C DHCL 40
PURPOSE
C DHCL 50
TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY LINEAR
C DHCL 60
DIFFERENTIAL EQUATIONS WITH GIVEN INITIAL VALUES.
C DHCL 70
C DHCL 80
USAGE
C DHCL 90
CALL DHPCCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AJX,A)
C DHCL 100
PARAMETERS AFCT,FCT AND OUTP REQUIRE AN EXTERNAL STATEMENT.
C DHCL 110
C DHCL 120
DESCRIPTION OF PARAMETERS
C DHCL 130
PRMT - DOUBLE PRECISION INPUT AND OUTPUT VECTOR WITH
C DHCL 140
DIMENSION GREATER THAN OR EQUAL TO 5, WHICH
C DHCL 150
SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF
C DHCL 160
ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN
C DHCL 170
OUTPUT SUBROUTINE (FURNISHED BY THE USER) AND
C DHCL 180
SUBROUTINE DHPCCL. EXCEPT PRMT(5) THE COMPONENTS
C DHCL 190
ARE NOT DESTROYED BY SUBROUTINE DHPCCL AND THEY ARE
C DHCL 200
PRMT(1)- LOWER BOUND OF THE INTERVAL (INPUT),
C DHCL 210
PRMT(2)- UPPER BOUND OF THE INTERVAL (INPUT),
C DHCL 220
PRMT(3)- INITIAL INCREMENT OF THE INDEPENDENT VARIABLE
C DHCL 230
(INPUT),
C DHCL 240
PRMT(4)- UPPER ERROR BOUND (INPUT). IF ABSOLUTE ERROR IS
C DHCL 250
GREATER THAN PRMT(4), INCREMENT GETS HALVED.
C DHCL 260
IF INCREMENT IS LESS THAN PRMT(3) AND ABSOLUTE
C DHCL 270
ERRR LESS THAN PRMT(4)/50, INCREMENT GETS DOUBLED.
C DHCL 280
THE USER MAY CHANGE PRMT(4) BY MEANS OF HIS
C DHCL 290
OUTPUT SUBROUTINE.
C DHCL 300
PRMT(5)- NO INPUT PARAMETER. SUBROUTINE DHPCCL INITIALIZES
C DHCL 310
PRMT(5)=0. IF THE USER WANTS TO TERMINATE
C DHCL 320
SUBROUTINE DHPCCL AT ANY OUTPUT POINT, HE HAS TO
C DHCL 330
CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE
C DHCL 340
OUTP. FURTHER COMPONENTS OF VECTOR PRMT ARE
C DHCL 350
FEASIBLE IF ITS DIMENSION IS DEFINED GREATER
C DHCL 360
THAN 5. HOWEVER SUBROUTINE DHPCCL DOES NOT REQUIRE
C DHCL 370
AND CHANGE THEM. NEVERTHELESS THEY MAY BE USEFUL
C DHCL 380
FOR HANDLING RESULT VALUES TO THE MAIN PROGRAM
C DHCL 390
(CALLING DHPCCL) WHICH ARE OBTAINED BY SPECIAL
C DHCL 400
MANIPULATIONS WITH OUTPUT DATA IN SUBROUTINE OUTP.
C DHCL 410
Y - DOUBLE PRECISION INPUT VECTOR OF INITIAL VALUES
C DHCL 420
(DESTROYED). LATERON Y IS THE RESULTING VECTOR OF
C DHCL 430
DEPENDENT VARIABLES COMPUTED AT INTERMEDIATE
C DHCL 440
POINTS X.
C DHCL 450
DERY - DOUBLE PRECISION INPUT VECTOR OF ERROR WEIGHTS
C DHCL 460
(DESTROYED). THE SUM OF ITS COMPONENTS MUST BE
C DHCL 470
EQUAL TO 1. LATERON DERY IS THE VECTOR OF
C DHCL 480
DERIVATIVES, WHICH BELONG TO FUNCTION VALUES Y AT
C DHCL 490
INTERMEDIATE POINTS X.
C DHCL 500
NDIM - AN INPUT VALUE, WHICH SPECIFIES THE NUMBER OF
C DHCL 510
EQUATIONS IN THE SYSTEM.
C DHCL 520
IHLF - AN OUTPUT VALUE, WHICH SPECIFIES THE NUMBER OF
C DHCL 530
BISECTIONS OF THE INITIAL INCREMENT. IF IHLF GETS
C DHCL 540
GREATER THAN 10, SUBROUTINE DHPCCL RETURNS WITH
C DHCL 550
ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM.
C DHCL 560
PRMT(3)=0 OR IN CASE SIGN(PRMT(3)).NE.SIGN(PRMT(2))-DHCL
C DHCL 570
PRMT(1)) RESPECTIVELY.
C DHCL 580
AFCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. IT
C DHCL 590
COMPUTES MATRIX A (FACTOR OF VECTOR Y ON THE
C DHCL 600
RIGHT HAND SIDE OF THE SYSTEM) FOR A GIVEN X-VALUE.
C DHCL 610
IT'S PARAMETER LIST MUST BE X,A. THE SUBROUTINE
C DHCL 620
SHOULD NOT DESTROY X.
C DHCL 630
FCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. IT
C DHCL 640
COMPUTES VECTOR F (INHOMOGENEOUS PART OF THE
C DHCL 650
RIGHT HAND SIDE OF THE SYSTEM) FOR A GIVEN X-VALUE.
C DHCL 660
IT'S PARAMETER LIST MUST BE X,F. THE SUBROUTINE
C DHCL 670
SHOULD NOT DESTROY X.
C DHCL 680
OUTP - THE NAME OF AN EXTERNAL OUTPUT SUBROUTINE USED.
C DHCL 690
IT'S PARAMETER LIST MUST BE X,Y,DERY,IHLF,NDIM,PRMT.
C DHCL 700
NONE OF THESE PARAMETERS (EXCEPT, IF NECESSARY,
C DHCL 710
PRMT(4), PRMT(5),...) SHOULD BE CHANGED BY
C DHCL 720
SUBROUTINE OUTP. IF PRMT(5) IS CHANGED TO NON-ZERO,
C DHCL 730
SUBROUTINE DHPCCL IS TERMINATED.
C DHCL 740
AUX - DOUBLE PRECISION AUXILIARY STORAGE ARRAY WITH 16
C DHCL 750
ROWS AND NDIM COLUMNS.
C DHCL 760
A - DOUBLE PRECISION NDIM BY NDIM MATRIX, WHICH IS USED
C DHCL 770
AS AUXILIARY STORAGE ARRAY.
C DHCL 780
REMARKS
C DHCL 790
THE PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF
C DHCL 800
(1) MORE THAN 10 BISECTIONS OF THE INITIAL INCREMENT ARE
C DHCL 810
NECESSARY TO GET SATISFACTORY ACCURACY (ERROR MESSAGE
C DHCL 820
IHLF=11),
C DHCL 830
(2) INITIAL INCREMENT IS EQUAL TO 0 OR HAS WRONG SIGN
C DHCL 840
(ERROR MESSAGE IHLF=12 OR IHLF=13),
C DHCL 850
(3) THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH,
C DHCL 860
(4) SUBROUTINE OUTP HAS CHANGED PRMT(5) TO NON-ZERO.
C DHCL 870
C DHCL 880
C DHCL 890
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C DHCL 900
THE EXTERNAL SUBROUTINES AFCT(X,A), FCT(X,F) AND
C DHCL 910
OUTP(X,Y,DERY,IHLF,NDIM,PRMT) MUST BE FURNISHED BY THE USER.
C DHCL 920
C DHCL 930
C DHCL 940
METHOD
C DHCL 950
EVALUATION IS DONE BY MEANS OF HAMMING'S MODIFIED PREDICTOR-
C DHCL 960
CORRECTOR METHOD. IT IS A FOURTH ORDER METHOD USING 4
C DHCL 970
PRECEEDING POINTS FOR COMPUTATION OF A NEW VECTOR Y OF THE
C DHCL 980
DEPENDENT VARIABLES.
C DHCL 990
FOURTH ORDER RUNGE-KUTTA METHOD SUGGESTED BY RALSTON IS
C DHCL 1000
USED FOR ADJUSTMENT OF THE INITIAL INCREMENT AND FOR
C DHCL 1010
COMPUTATION OF STARTING VALUES.
C DHCL 1020
SUBROUTINE DHPCCL AUTOMATICALLY ADJUSTS THE INCREMENT DURING
C DHCL 1030
THE WHOLE COMPUTATION BY HALVING OR DOUBLING.
C DHCL 1040
C DHCL 1050

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C      TO GET FULL FLEXIBILITY IN OUTPUT, AN OUTPUT SUBROUTINE      DHCL1060      IF(PRMT(5))107,129,107      DHCL2350
C      MUST BE CODED BY THE USER.      DHCL1070      129 IF(N-4)130,300,300      DHCL2360
C      FOR REFERENCE, SEE      DHCL1080      130 DO 131 I=1,NDIM      DHCL2370
C      (1) RALSTON/HLF, MATHEMATICAL METHODS FOR DIGITAL      DHCL1090      AUX(I,1)=Y(I)      DHCL2380
C      COMPUTERS, WILEY, NEW YORK/LONDON, 1960, PP.95-109.      DHCL1100      131 AUX(N+7,1)=DERY(I)      DHCL2390
C      (2) RALSTON, RUNGE-KUTTA METHODS WITH MINIMUM ERROR BOUNDS,      DHCL1110      IF(N-3)132,134,300      DHCL2400
C      MTAC, VOL.16, ISS-80 (1962), PP.431-437.      DHCL1120      C      DHCL2410
C      .....      DHCL1130      132 DO 133 I=1,NDIM      DHCL2420
C      .....      DHCL1140      DELT=AUX(9,1)+AUX(9,1)      DHCL2430
C      .....      DHCL1150      DELT=DELT+DELT      DHCL2440
C      SUBROUTINE DHPCL(PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A)      DHCL1160      133 Y(I)=AUX(1,1)+.333333333333333300*(AUX(8,1)+DELT+AUX(10,1))      DHCL2450
C      .....      DHCL1170      GOTO 127      DHCL2460
C      .....      DHCL1180      C      DHCL2470
C      THE FOLLOWING FIRST PART OF SUBROUTINE DHPCL (UNTIL FIRST BREAK-      DHCL1190      134 DO 135 I=1,NDIM      DHCL2480
C      POINT FOR LINKAGE) HAS TO STAY IN CORE DURING THE WHOLE      DHCL1200      DELT=AUX(9,1)+AUX(10,1)      DHCL2490
C      COMPUTATION      DHCL1210      DELT=DELT+DELT+DELT      DHCL2500
C      .....      DHCL1220      135 Y(I)=AUX(1,1)+.37500*(AUX(8,1)+DELT+AUX(11,1))      DHCL2510
C      .....      DHCL1230      GOTO 127      DHCL2520
C      .....      DHCL1240      C      DHCL2530
C      DIMENSION PRMT(1),Y(1),DERY(1),AUX(16,1),A(1)      DHCL1250      C      DHCL2540
C      DOUBLE PRECISION PRMT,Y,DERY,AUX,X,H,Z,DELT,A,H5      DHCL1260      C      DHCL2550
C      GOTO 100      DHCL1270      C      DHCL2560
C      THIS PART OF SUBROUTINE DHPCL COMPUTES THE RIGHT HAND SIDE DERY OF      DHCL1280      200 Z=X      DHCL2570
C      THE GIVEN SYSTEM OF LINEAR DIFFERENTIAL EQUATIONS.      DHCL1290      DO 201 I=1,NDIM      DHCL2580
C      1 CALL FCT(X,A)      DHCL1300      X=X+AUX(N+7,1)      DHCL2590
C      CALL FCT(X,DERY)      DHCL1310      AUX(5,1)=X      DHCL2600
C      DO 3 M=1,NDIM      DHCL1320      201 Y(I)=AUX(N,1)+.400*X      DHCL2610
C      LL=M-NDIM      DHCL1330      X IS AN AUXILIARY STORAGE LOCATION      DHCL2620
C      HS=0.00      DHCL1340      C      DHCL2630
C      DO 2 L=1,NDIM      DHCL1350      X=Z+.400*H      DHCL2640
C      LL=L+NDIM      DHCL1360      ISW2=2      DHCL2650
C      2 HS=HS+ALL*(Y(L)      DHCL1370      GOTO 1      DHCL2660
C      3 DERY(M)=HS+DERY(M)      DHCL1380      202 DO 203 I=1,NDIM      DHCL2670
C      GOTO(105,202,204,206,115,122,125,308,312,327,329,128),ISW2      DHCL1390      X=H*DERY(I)      DHCL2680
C      .....      DHCL1400      AUX(6,1)=X      DHCL2690
C      .....      DHCL1410      203 Y(I)=AUX(N,1)+.2969776092477536000*AUX(5,1)+.1587596449710358300*X      DHCL2700
C      .....      DHCL1420      C      DHCL2710
C      .....      DHCL1430      X=Z+.4557372542187894300*H      DHCL2720
C      .....      DHCL1440      ISW2=3      DHCL2730
C      .....      DHCL1450      GOTO 1      DHCL2740
C      .....      DHCL1460      204 DO 205 I=1,NDIM      DHCL2750
C      .....      DHCL1470      X=H*DERY(I)      DHCL2760
C      .....      DHCL1480      AUX(7,1)=X      DHCL2770
C      .....      DHCL1490      205 Y(I)=AUX(N,1)+.2181003882259204700*AUX(5,1)+.3050965148692930800*      DHCL2780
C      .....      DHCL1500      1AUX(6,1)+3.832864760467010300*X      DHCL2790
C      .....      DHCL1510      C      DHCL2800
C      .....      DHCL1520      X=Z+H      DHCL2810
C      .....      DHCL1530      ISW2=4      DHCL2820
C      .....      DHCL1540      GOTO 1      DHCL2830
C      .....      DHCL1550      206 DO 207 I=1,NDIM      DHCL2840
C      .....      DHCL1560      207 Y(I)=AUX(N,1)+.1747602822626903700*AUX(5,1)+.5514806623787329400*      DHCL2850
C      .....      DHCL1570      1AUX(6,1)+1.205535599396523500*AUX(7,1)+.1711847812195190300*      DHCL2860
C      .....      DHCL1580      2H*DERY(I)      DHCL2870
C      .....      DHCL1590      X=Z      DHCL2880
C      .....      DHCL1600      GOTO(110,114,117,124),ISW1      DHCL2890
C      .....      DHCL1610      C      DHCL2900
C      .....      DHCL1620      POSSIBLE BREAK-POINT FOR LINKAGE      DHCL2910
C      .....      DHCL1630      C      DHCL2920
C      .....      DHCL1640      STARTING VALUES ARE COMPUTED.      DHCL2930
C      .....      DHCL1650      NOW START HAMMING'S MODIFIED PREDICTOR-CORRECTOR METHOD.      DHCL2940
C      .....      DHCL1660      300 ISTEP=3      DHCL2950
C      .....      DHCL1670      301 IF(N-8)304,302,304      DHCL2960
C      .....      DHCL1680      C      DHCL2970
C      .....      DHCL1690      N=8 CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS      DHCL2980
C      .....      DHCL1700      302 DO 303 I=2,7      DHCL2990
C      .....      DHCL1710      DO 303 I=1,NDIM      DHCL3000
C      .....      DHCL1720      AUX(N-1,1)=AUX(N,1)      DHCL3010
C      .....      DHCL1730      303 AUX(N+6,1)=AUX(N+7,1)      DHCL3020
C      .....      DHCL1740      N=7      DHCL3030
C      .....      DHCL1750      C      DHCL3040
C      .....      DHCL1760      N LESS THAN 8 CAUSES N+1 TO GET N      DHCL3050
C      .....      DHCL1770      304 N=N+1      DHCL3060
C      .....      DHCL1780      C      DHCL3070
C      .....      DHCL1790      COMPUTATION OF NEXT VECTOR Y      DHCL3080
C      .....      DHCL1800      DO 305 I=1,NDIM      DHCL3090
C      .....      DHCL1810      AUX(N-1,1)=Y(I)      DHCL3100
C      .....      DHCL1820      305 AUX(N+6,1)=DERY(I)      DHCL3110
C      .....      DHCL1830      X=X+H      DHCL3120
C      .....      DHCL1840      306 ISTEP=ISTEP+1      DHCL3130
C      .....      DHCL1850      DO 307 I=1,NDIM      DHCL3140
C      .....      DHCL1860      ODELT=AUX(N-4,1)+1.33333333333333300*(AUX(N+6,1)+AUX(N+6,1)-      DHCL3150
C      .....      DHCL1870      1AUX(N+5,1)+AUX(N+4,1)+AUX(N+4,1))      DHCL3160
C      .....      DHCL1880      Y(I)=DELT-.925619834710743800*AUX(16,1)      DHCL3170
C      .....      DHCL1890      307 AUX(16,1)=DELT      DHCL3180
C      .....      DHCL1900      C      DHCL3190
C      .....      DHCL1910      PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX, MODIFIED PREDICTOR      DHCL3200
C      .....      DHCL1920      IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.      DHCL3210
C      .....      DHCL1930      GOTO 1      DHCL3220
C      .....      DHCL1940      C      DHCL3230
C      .....      DHCL1950      DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY      DHCL3240
C      .....      DHCL1960      308 DO 309 I=1,NDIM      DHCL3250
C      .....      DHCL1970      ODELT=.12500*Y.00*AUX(N-1,1)-AUX(N-3,1)+3.00*(DERY(I)+AUX(N+6,1)      DHCL3260
C      .....      DHCL1980      1+AUX(N+6,1)-AUX(N+5,1))      DHCL3270
C      .....      DHCL1990      AUX(16,1)=AUX(16,1)-DELT      DHCL3280
C      .....      DHCL2000      309 Y(I)=DELT+.0743801652892562000*AUX(16,1)      DHCL3290
C      .....      DHCL2010      C      DHCL3300
C      .....      DHCL2020      TEST WHETHER H MUST BE HALVED OR DOUBLED      DHCL3310
C      .....      DHCL2030      DELT=.00      DHCL3320
C      .....      DHCL2040      DO 310 I=1,NDIM      DHCL3330
C      .....      DHCL2050      310 DELT=DELT+AUX(15,1)*0.085(AUX(16,1))      DHCL3340
C      .....      DHCL2060      IF(DELT-PRMT(4))311,324,324      DHCL3350
C      .....      DHCL2070      C      DHCL3360
C      .....      DHCL2080      H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.      DHCL3370
C      .....      DHCL2090      311 ISW2=9      DHCL3380
C      .....      DHCL2100      C      DHCL3390
C      .....      DHCL2110      312 CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)      DHCL3400
C      .....      DHCL2120      IF(PRMT(5))314,313,314      DHCL3410
C      .....      DHCL2130      313 IF(IHLF-1)315,314,314      DHCL3420
C      .....      DHCL2140      314 RETURN      DHCL3430
C      .....      DHCL2150      315 IF(H*(X-PRMT(2)))316,314,314      DHCL3440
C      .....      DHCL2160      316 IF(0.085(X-PRMT(2))-.100*0.085(H))314,317,317      DHCL3450
C      .....      DHCL2170      317 IF(DELT-.0200*PRMT(4))318,318,301      DHCL3460
C      .....      DHCL2180      C      DHCL3470
C      .....      DHCL2190      H COULD BE DOUBLED IF ALL NECESSARY PRECEEDING VALUES ARE      DHCL3480
C      .....      DHCL2200      AVAILABLE      DHCL3490
C      .....      DHCL2210      318 IF(IHLF)301,301,319      DHCL3500
C      .....      DHCL2220      319 IF(N-7)301,320,320      DHCL3510
C      .....      DHCL2230      320 IF(ISTEP-4)301,321,321      DHCL3520
C      .....      DHCL2240      321 IMOD=ISTEP/2      DHCL3530
C      .....      DHCL2250      IF(ISTEP-IMOD-1)301,322,301      DHCL3540
C      .....      DHCL2260      322 H=H*H      DHCL3550
C      .....      DHCL2270      IHLF=IHLF-1      DHCL3560
C      .....      DHCL2280      ISTEP=0      DHCL3570
C      .....      DHCL2290      DO 323 I=1,NDIM      DHCL3580
C      .....      DHCL2300      AUX(N-1,1)=AUX(N-2,1)      DHCL3590
C      .....      DHCL2310      AUX(N-2,1)=AUX(N-4,1)      DHCL3600
C      .....      DHCL2320      AUX(N-3,1)=AUX(N-6,1)      DHCL3610
C      .....      DHCL2330      AUX(N+6,1)=AUX(N+5,1)      DHCL3620
C      .....      DHCL2340      AUX(N+5,1)=AUX(N+3,1)      DHCL3630

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AUX(N+4, I)=AUX(N+1, I)
DELT=AUX(N+6, I)+AUX(N+5, I)
DELT=DELT+DELT+DELT
3230AUX(16, I)=8.96296296296296300*(Y(I)-AUX(N-3, I))
1-3.361111111111111100*H*(DERY(I)+DELT+AUX(N+4, I))
GOTO 301
C
H MUST BE HALVED
324 IMLF=IMLF+1
IF (IMLF-10) 325, 325, 311
325 H=.500*H
ISTEP=0
DO 326 I=1, NDIM
OY(I)=.3906250-2*(6.01*AUX(N-1, I)+135.00*AUX(N-2, I)+4.01*AUX(N-3, I)
1+AUX(N-4, I))-117187500*(AUX(N+6, I)-6.00*AUX(N+5, I)-AUX(N+4, I))*H
0AUX(N-4, I)=.3906250-2*(12.00*AUX(N-1, I)+135.00*AUX(N-2, I)+
1108.00*AUX(N-3, I)+AUX(N-4, I))-0.23437500*(AUX(N+6, I)+
218.00*AUX(N+5, I)-9.00*AUX(N+4, I))*H
AUX(N-3, I)=AUX(N-2, I)
326 AUX(N+4, I)=AUX(N+5, I)
DELT=K-H
K=DELT-(H+H)
ISW2=10
GOTO 1
327 DO 328 I=1, NDIM
AUX(N-2, I)=Y(I)
AUX(N+5, I)=DERY(I)
328 Y(I)=AUX(N-4, I)
X=X-(H+H)
ISW2=11
GOTO 1
329 X=DELT
DO 330 I=1, NDIM
DELT=AUX(N+5, I)+AUX(N+4, I)
DELT=DELT+DELT+DELT
0AUX(16, I)=8.96296296296296300*(AUX(N-1, I)-Y(I))
1-3.361111111111111100*H*(AUX(N+6, I)+DELT+DERY(I))
330 AUX(N+3, I)=DERY(I)
GOTO 306
END
DHCL3640
DHCL3650
DHCL3660
DHCL3670
DHCL3680
DHCL3690
DHCL3700
DHCL3710
DHCL3720
DHCL3730
DHCL3740
DHCL3750
DHCL3760
DHCL3770
DHCL3780
DHCL3790
DHCL3800
DHCL3810
DHCL3820
DHCL3830
DHCL3840
DHCL3850
DHCL3860
DHCL3870
DHCL3880
DHCL3890
DHCL3900
DHCL3910
DHCL3920
DHCL3930
DHCL3940
DHCL3950
DHCL3960
DHCL3970
DHCL3980
DHCL3990
DHCL4000
DHCL4010
DHCL4020
DHCL4030

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Subroutines LBVP and DLBVP

These subroutines generate an approximate solution of a given linear boundary-value problem consisting of a system of linear first-order ordinary differential equations with linear boundary conditions. Solution is done by the method of adjoint equations, which generates successively adjoint initial-value problems. By means of the solutions of these adjoint initial-value problems (done by Hamming's modified predictor-corrector method) it is possible to generate missing boundary conditions, which are necessary to compute initial values suitable to the given boundary-value problem (done by subroutine GELG or DGELG: solution of simultaneous linear equations by means of Gauss elimination). Thus the boundary-value problem is reduced to a linear initial-value problem, which is finally solved by Hamming's modified predictor-corrector method also.

Given the system of n linear first-order ordinary differential equations:

$$\begin{aligned}
 y'_1 &\equiv \frac{dy_1}{dx} = a_{11}(x)y_1 + a_{12}(x)y_2 + \dots \\
 &\quad + a_{1n}(x)y_n + f_1(x) \\
 y'_2 &\equiv \frac{dy_2}{dx} = a_{21}(x)y_1 + a_{22}(x)y_2 + \dots \\
 &\quad + a_{2n}(x)y_n + f_2(x) \\
 &\dots \\
 y'_n &\equiv \frac{dy_n}{dx} = a_{n1}(x)y_1 + a_{n2}(x)y_2 + \dots \\
 &\quad + a_{nn}(x)y_n + f_n(x)
 \end{aligned}$$

together with n boundary conditions:

$$\begin{aligned}
 &b_{11}y_1(x_1) + b_{12}y_2(x_1) + \dots + b_{1n}y_n(x_1) + c_{11}y_1(x_u) \\
 &\quad + c_{12}y_2(x_u) + \dots + c_{1n}y_n(x_u) = r_1 \\
 &b_{21}y_1(x_1) + b_{22}y_2(x_1) + \dots + b_{2n}y_n(x_1) + c_{21}y_1(x_u) \\
 &\quad + c_{22}y_2(x_u) + \dots + c_{2n}y_n(x_u) = r_2 \\
 &\dots \\
 &b_{n1}y_1(x_1) + b_{n2}y_2(x_1) + \dots + b_{nn}y_n(x_1) + c_{n1}y_1(x_u) \\
 &\quad + c_{n2}y_2(x_u) + \dots + c_{nn}y_n(x_u) = r_n
 \end{aligned}$$

where x_1 and x_u are the lower and upper bound respectively of the integration interval, and using the following vector and matrix notations:

$$Y(x) = \begin{pmatrix} y_1(x) \\ y_2(x) \\ \vdots \\ y_n(x) \end{pmatrix}, \quad F(x) = \begin{pmatrix} f_1(x) \\ f_2(x) \\ \vdots \\ f_n(x) \end{pmatrix},$$

$$Y_1 = \begin{pmatrix} y_1(x_1) \\ y_2(x_1) \\ \vdots \\ y_n(x_1) \end{pmatrix}, \quad Y_u = \begin{pmatrix} y_1(x_u) \\ y_2(x_u) \\ \vdots \\ y_n(x_u) \end{pmatrix},$$

$$R = \begin{pmatrix} r_1 \\ r_2 \\ \vdots \\ r_n \end{pmatrix},$$

$$A(x) = \begin{pmatrix} a_{11}(x)a_{12}(x)\dots a_{1n}(x) \\ a_{21}(x)a_{22}(x)\dots a_{2n}(x) \\ \dots \\ a_{n1}(x)a_{n2}(x)\dots a_{nn}(x) \end{pmatrix}$$

$$B = \begin{pmatrix} b_{11} & b_{12} & \dots & b_{1n} \\ b_{21} & b_{22} & \dots & b_{2n} \\ \dots & \dots & \dots & \dots \\ b_{n1} & b_{n2} & \dots & b_{nn} \end{pmatrix} \quad \text{and}$$

$$C = \begin{pmatrix} c_{11} & c_{12} & \dots & c_{1n} \\ c_{21} & c_{22} & \dots & c_{2n} \\ \dots & \dots & \dots & \dots \\ c_{n1} & c_{n2} & \dots & c_{nn} \end{pmatrix}$$

where $Y(x)$, $F(x)$, Y_1 , Y_u and R are column vectors with n components, and $A(x)$, and B and C are n by n square matrices, the given problem appears as follows:

$$Y' \equiv \frac{dY}{dx} = A(x) * Y + F(x) \quad (1)$$

with

$$B * Y_1 + C * Y_u = R \quad (2)$$

The first problem is to generate new boundary conditions. Assuming that B has fewer zero-columns than C^\dagger , the procedure eliminates Y_u from the boundary conditions and generates a system of simultaneous linear equations for the unknown initial values $y_1(x_1)$, $y_2(x_1)$, \dots , $y_n(x_1)$. This is done in the following way.

Assuming that the k^{th} column of matrix C ($k = 1, 2, \dots, n$) contains at least one nonzero element (that is, $y_k(x_u)$ appears in the boundary conditions), the following adjoint linear initial-value problem is generated and solved by Hamming's modified predictor-corrector method:

$$z'_1(x) \equiv \frac{dz_1}{dx} = -a_{11}(x)z_1 - a_{21}(x)z_2 - \dots - a_{n1}(x)z_n$$

$$z'_2(x) \equiv \frac{dz_2}{dx} = -a_{12}(x)z_1 - a_{22}(x)z_2 - \dots - a_{n2}(x)z_n$$

...

$$z'_n(x) \equiv \frac{dz_n}{dx} = -a_{1n}(x)z_1 - a_{2n}(x)z_2 - \dots - a_{nn}(x)z_n$$

with initial values:

$$z_1(x_u) = 0, z_2(x_u) = 0, \dots, z_{k-1}(x_u) = 0, z_k(x_u) = 1, z_{k+1}(x_u) = 0, \dots, z_n(x_u)$$

or in vector and matrix notations $\dagger\dagger$:

$$Z' \equiv \frac{dZ}{dx} = -A^T(x) * Z \quad (3)$$

$$\text{with initial values } Z(x_u) = E_k \quad (4)$$

\dagger If this is not the case, the procedure interchanges x_1 with x_u and B with C , in order to get a minimum number of adjoint initial-value problems.

$\dagger\dagger$ As vectors Z and Z' are actually stored in the same storage arrays as Y and Y' , in the flowchart and the FORTRAN program they are also named Y and $DERY$.

where $A^T(x)$ is the transpose of $A(x)$, and E_k is the column vector with only one nonzero element; that is, 1 as k^{th} element.

Assuming that $Z_k(x)$ is the solution of this k^{th} adjoint initial-value problem, and using equations (1) and (3), then:

$$\begin{aligned} \frac{d}{dx} \left[\sum_{i=1}^n z_i^{(k)}(x) \cdot y_i(x) \right] &= \frac{d}{dx} \left[Z_k^T(x) * Y(x) \right] \\ &= Z_k^T(x) * Y'(x) + Z_k'^T(x) * Y(x) \\ &= Z_k^T * (A * Y + F) + (-A^T * Z_k)^T * Y \\ &= Z_k^T * A * Y + Z_k^T * F - Z_k^T * A * Y \\ &= Z_k^T * F \end{aligned}$$

from which it follows that:

$$\frac{d}{dx} \left[\sum_{i=1}^n z_i^{(k)}(x) \cdot y_i(x) \right] = \left[\sum_{i=1}^n z_i^{(k)}(x) \cdot f_i(x) \right]$$

Integrating this equation from x_1 up to x_u the result is:

$$\begin{aligned} \sum_{i=1}^n z_i^{(k)}(x_u) \cdot y_i(x_u) - \sum_{i=1}^n z_i^{(k)}(x_1) \cdot y_i(x_1) \\ = \int_{x_1}^{x_u} \left[\sum_{i=1}^n z_i^{(k)}(x) \cdot f_i(x) \right] dx \end{aligned}$$

or:

$$y_k(x_u) = \sum_{i=1}^n z_i^{(k)}(x_1) \cdot y_i(x_1) - \text{sum}_k(x_1) \quad (5)$$

with:

$$\text{sum}_k(x_1) = \int_{x_u}^{x_1} \left[\sum_{i=1}^n z_i^{(k)}(x) \cdot f_i(x) \right] dx \quad (6)$$

Elimination of $y_k(x_u)$ in the boundary conditions can be done by the following transformation formulas, which transform matrix B_{k-1} and column vector R_{k-1} into matrix B_k and column vector R_k (with $B_0 = B$ and $R_0 = R$) on the storage locations of B and R :

$$\left. \begin{aligned} b_{ij}^{(k)} &= b_{ij}^{(k-1)} + c_{ik} \cdot z_j^{(k)}(x_1) \quad (j = 1, 2, \dots, n) \\ r_i^{(k)} &= r_i^{(k-1)} + c_{ik} \cdot \text{sum}_k(x_1) \end{aligned} \right\} \begin{array}{l} (i-1, 2, \\ \dots, n) \end{array} \quad (7)$$

If the k^{th} column of matrix C contains only zero-elements (that is, $y_k(x_u)$ does not appear in the boundary conditions), elimination of $y_k(x_u)$ is not necessary, and k can at once be increased by one.

If at least all $y_k(x_u)$ ($k = 1, 2, \dots, n$) in the boundary conditions are eliminated, the remaining system of simultaneous linear equations

$$B_n * Y_1 = R_n \quad (9)$$

is solved by Gauss elimination (subroutine GELG or DGELG). However, this is only possible if matrix B_n is not singular. In case of a singular matrix B_n (that is, the pivot element at any elimination step is exactly equal to zero), the procedure is bypassed, giving an error message which shows that the given boundary-value problem has no or more than one solution, or that the method of adjoint equations was not able to find a solution because one or more of the generated new boundary conditions were linear combinations of the given boundary conditions.

There is another critical case in the solution of equation (9), indicated by a warning given by subroutine GELG or DGELG which means possible loss of significance in the Gauss elimination of at least as many significant digits as specified by the upper bound ϵ of the local truncation error in the integration procedures. If this warning appears, it is highly probable that matrix B_n is singular too. But as this may not necessarily be the case, the procedure goes on after having given a warning to the user's output subroutine in the form of a negative number of bisections of the initial step size together with the resulting initial values of the finally generated initial-value problem (first set of output values). The absolute value of this "warning parameter" indicates the step of the Gauss algorithm immediately preceding the detection of the loss of significance.

After the vector of initial values Y_1 is computed (that is after the boundary-value problem is reduced to an initial-value problem), the final step to solve the generated initial-value problem is done by

Hamming's modified predictor-corrector method, incorporated in subroutines LBVP and DLBVP.

Both the solution of adjoint linear initial-value problems described above and the solution of the finally generated linear initial-value problem equivalent to the given boundary-value problem are done by means of Hamming's modified predictor-corrector method for systems of linear differential equations. An extensive description of this method can be found in the mathematical description of subroutines HPCL and DHPCL (except that control of accuracy and adjustment of step size is done differently). Therefore it will be sufficient to give a short description of this method in the form of a notation of the formulas used.

1. Problem to be solved --

System of linear differential equations $Y' = L(x, Y)$ with initial values $Y(x_0) = Y_0$, $Y'(x_0) = L(x_0, Y_0) = Y'_0$

For adjoint initial-value problems, this is:

$$Y' \equiv L(x, Y) = -A^T(x) * Y$$

$$x_0 = x_u, Y(x_0) = E_k, Y'(x_0) = -A^T(x_0) * E_k, h$$

$$= \frac{1}{16} (x_1 - x_u)$$

and for the finally generated initial-value problem:

$$Y' = L(x, Y) = A(x) * Y + F(x)$$

$$x_0 = x_1, Y_0 = Y_1, Y'_0 = A(x_1) * Y_1 + F(x_1)$$

2. Hamming's modified predictor-corrector formulas -- (h represents the step size adjusted to accuracy requirements) for $j = 3, 4, 5, \dots$ (that means at points $x_j = x_3, x_4, x_5, \dots$)

$$\begin{aligned} \text{Predictor: } P_{j+1} &= Y_{j-3} + \frac{4}{3} h (2 Y'_j - Y'_{j-1} \\ &\quad + 2 Y'_{j-2}) \end{aligned} \quad (10)$$

$$\text{Modifier: } M_{j+1} = P_{j+1} - \frac{112}{121} (P_j - C_j) \quad (11)$$

$$M'_{j+1} = L(x_{j+1}, M_{j+1}) \quad (12)$$

$$\begin{aligned} \text{Corrector: } C_{j+1} &= \frac{1}{8} \left[9 Y_j - Y_{j-2} + 3 h \cdot \right. \\ &\quad \left. (M'_{j+1} + 2 Y'_j - Y'_{j-1}) \right] \end{aligned} \quad (13)$$

$$\text{Final value: } Y_{j+1} = C_{j+1} + \frac{9}{121} (P_{j+1}$$

$$- C_{j+1}) \quad (14)$$

3. Test value for control of accuracy and adjustment of step size h in predictor-corrector part ("local truncation error") †:

$$\delta = \max_i \frac{a_i \cdot |p_{j+1, i} - c_{j+1, i}|}{\max(1, |y_{j+1, i}|)} \quad (15)$$

with error weights $a_i = 1$ ($i=1, 2, \dots, n$) for the adjoint initial-value problems, and given by input for the finally generated initial-value problem.

Adjustment of step size h: halving, if $\delta > \epsilon$

doubling, if $\delta \leq \epsilon / 50$

with the upper bound ϵ for the local truncation error given by input.

4. Formulas for interpolating intermediate points in case of halving the step size h:

$$\begin{aligned} Y_{j-1/2} &\equiv Y(x_j - \frac{h}{2}) = \frac{1}{256} (80 Y_j + 135 Y_{j-1} \\ &\quad + 40 Y_{j-2} + Y_{j-3}) - \frac{h}{2} \cdot \frac{15}{128} \cdot \\ &\quad (Y'_j - 6 Y'_{j-1} - Y'_{j-2}) \end{aligned} \quad (16)$$

$$\begin{aligned} Y_{j-3/2} &\equiv Y(x_j - \frac{3h}{2}) = \frac{1}{256} (12 Y_j + 135 Y_{j-1} \\ &\quad + 108 Y_{j-2} + Y_{j-3}) - \frac{h}{2} \cdot \frac{3}{128} \cdot \\ &\quad (Y'_j + 18 Y'_{j-1} - 9 Y'_{j-2}) \end{aligned} \quad (17)$$

5. Changing vectors $P_j - C_j$ in case of halving, or $P_{j+1} - C_{j+1}$ in case of doubling the step size h:

$$\begin{aligned} P_j - C_j &= \frac{242}{27} (Y_j - Y_{j-3/2}) - \frac{121}{36} \cdot \frac{h}{2} (Y'_j + 3 Y'_{j-1/2} \\ &\quad + 3 Y'_{j-1} + Y'_{j-3/2}) \end{aligned} \quad (18)$$

$$\begin{aligned} P_{j+1} - C_{j+1} &= \frac{242}{27} (Y_{j+1} - Y_{j-5}) - \frac{121}{36} \cdot 2h (Y'_{j+1} \\ &\quad + 3 Y'_{j-1} + 3 Y'_{j-3} + Y'_{j-5}) \end{aligned} \quad (19)$$

† The terms from which δ is generated by searching for the maximum are weighted relative errors if the absolute values of $y_{j+1, i}(x)$ are greater than 1, and weighted absolute errors if the absolute values are not greater than 1.

6. Starting Hamming's modified predictor-corrector method by means of three Runge-Kutta steps:

For $j = 0, 1, 2$

$$K_1 = h \cdot Y'_j \quad (20)$$

$$K_2 = h \cdot L(x_j + 0.4h, Y_j + 0.4K_1) \quad (21)$$

$$K_3 = h \cdot L(x_j + 0.45573725421878943h, Y_j + 0.29697760924775360K_1 + 0.15875964497103583K_2) \quad (22)$$

$$K_4 = h \cdot L(x_j + h, Y_j + 0.21810038822592047K_1 - 3.0509651486929308K_2 + 3.8328647604670103K_3) \quad (23)$$

$$Y_{j+1} = Y_j + 0.17476028226269037K_1 - 0.55148066287873294K_2 + 1.2055355993965235K_3 + 0.17118478121951903K_4 \quad (24)$$

7. Test value for control of accuracy and adjustment of step size h in the Runge-Kutta part ("local truncation error")†:

$$\delta = \frac{1}{15} \cdot \max_i a_i \frac{|y_{2,i}^{(1)} - y_{2,i}^{(2)}|}{\max(1, |y_{2,i}^{(2)}|)} \quad (25)$$

with error weights $a_i = 1$ ($i = 1, 2, \dots, n$) for adjoint initial-value problems and given by input for the finally generated initial-value problem. Step size h is adjusted by halving if $\delta > \epsilon$, with the upper bound ϵ of the local truncation error given by input.

† The terms from which δ is generated by searching for the maximum are weighted relative errors if the absolute values of $y_{2,i}^{(2)}$ are greater than 1, and weighted absolute errors if the absolute values are not greater than 1.

8. Iteration formulas for refinement of Runge-Kutta results:

$$Y_1 = Y_0 + \frac{h}{24} (9Y'_0 + 19Y'_1 - 5Y'_2 + Y'_3) \quad (26)$$

$$Y_2 = Y_0 + \frac{h}{3} (Y'_0 + 4Y'_1 + Y'_2) \quad (27)$$

$$Y_3 = Y_0 + \frac{3h}{8} (Y'_0 + 3Y'_1 + 3Y'_2 + Y'_3) \quad (28)$$

As transformation formulas (7) and (8) show, the output of Hamming's modified predictor-corrector method for the solution of any adjoint initial-value problem must contain only the vector $Z_k(x_1)$ of function values at the lower bound x_1 (actually stored in vector Y) and the integral value $\text{sum}_k(x_1)$. With respect to the predictor-corrector method, which is a fourth-order integration procedure generating function vectors $Z_k(x)$ (in storage array Y) and derivative vectors $Z'_k(x)$ (in storage array $DERY$) at intermediate (not necessarily equidistant) points x , the following fourth-order Hermitian integration formula -- using the function and the first derivative values of the function to be integrated -- is suitable to accumulate integral values $\text{sum}_k(x)$ and finally $\text{sum}_k(x_1)$:

$$\text{sum}_k(x+h) = \text{sum}_k(x) + \frac{h}{2} \left\{ g'_k(x) + g'_k(x+h) + \frac{h}{6} \left[g''_k(x) - g''_k(x+h) \right] \right\} \quad (29)$$

using the instantaneous step size h of the predictor-corrector method, and with:

$$g_k(x) = \sum_{i=1}^n z_i^{(k)}(x) f_i(x) = Z_k^T(x) + F(x) \quad (30)$$

and:

$$g'_k(x) = \sum_{i=1}^n \left[\frac{dz_i^{(k)}}{dx} \cdot f_i(x) + z_i^{(k)} \cdot \frac{df_i}{dx} \right] = \frac{dZ_k^T}{dx} * F(x) + Z_k^T(x) * \frac{dF}{dx} \quad (31)$$

Therefore, generation of $\text{sum}_k(x+h)$ is done by means of the following formulas:

$$\begin{aligned} g_u^{(k)} &= g_k(x+h) = \sum_{i=1}^n z_i^{(k)}(x+h) f_i(x+h) \\ &= Z_k^T(x+h) * F(x+h) \end{aligned} \quad (32)$$

$$\begin{aligned} dg_u^{(k)} &= g'_k(x+h) = \sum_{i=1}^n \left[z_i^{(k)}(x+h) f_i(x+h) \right. \\ &\quad \left. + z_i^{(k)}(x+h) f'_i(x+h) \right] = Z_k^T(x+h) * F(x+h) \\ &\quad + Z_k^T(x+h) * F'(x+h) \end{aligned} \quad (33)$$

$$\begin{aligned} \text{sum}_k(x+h) &= \text{sum}_k(x) + \frac{h}{2} \left[g_1^{(k)} + g_u^{(k)} \right. \\ &\quad \left. + \frac{h}{6} (dg_1^{(k)} - dg_u^{(k)}) \right] \end{aligned} \quad (34)$$

After these three formulas have been evaluated, $g_u^{(k)}$ becomes $g_1^{(k)}$, and $dg_u^{(k)}$ becomes $dg_1^{(k)}$. Initial values of $g_1^{(k)}$ and $dg_1^{(k)}$ are generated, using formulas (30) and (31) at point $x = x_u$, leading to:

$$g_1^{(k)} = g_k(x_u) = f_k(x_u) \quad (35)$$

and:

$$dg_1^{(k)} = g'_k(x_u) = f'_k(x_u) - \sum_{i=1}^n a_{ki}(x_u) * f_i(x_u) \quad (36)$$

The entire input of subroutines LBVP and DLBVP is:

1. Lower and upper bound x_1 and x_u of the integration interval, initial step size h of the independent variable and upper bound ϵ (≤ 1) of the local "relative" truncation error in integration procedures
2. Coefficient matrices B and C of vectors Y_1 and Y_u in boundary conditions and right-hand side vector R
3. Vector of error weights a_i ($i = 1, 2, \dots, n$) for the local "relative" truncation error in each component of the dependent variables ($a_i \leq 1$ for all i)

4. The number n of differential equations and boundary conditions

5. As external subroutine subprograms, the computation of the right-hand side matrix $A(x)$ of the system of linear differential equations, and the computation of the inhomogeneous vector $F(x)$ and of its derivative $F'(x)$; for flexibility in output, an output subroutine

6. A one-dimensional auxiliary storage array with n storage locations, an n by n auxiliary storage array, and a two-dimensional auxiliary storage array (named AUX in flowchart, FORTRAN subroutine, and mathematical description) with 20 rows and n columns

Output is done in the following way. If a set of approximations to the dependent variables $Y(x)$ is found to be of sufficient accuracy (that is $\delta \leq \epsilon$), it is handed -- together with x , the vector of derivatives $Y'(x)$, the number of bisections of the initial increment, the number of differential equations, the lower and upper bound of the integration interval, the initial step size, error bound ϵ , and a parameter for terminating subroutine LBVP or DLBVP -- to the output subroutine. By means of this output subroutine, the user has the opportunity to choose his own output format, to handle the output values as he wants, to change the upper error bound and to terminate subroutine LBVP or DLBVP at any output point (for example, in case of possible loss of accuracy in Gauss elimination). In particular, the user is able to drop the output of some intermediate points, printing only the result values at the special points $x_0 + j \cdot h$, where $j = 0, 1, 2, \dots$, and h is the initial step size specified by input. The user may also perform intermediate computations using the integration results before continuing the process.

For better understanding of the flowchart and of the FORTRAN program, Figure 34 shows the allocation of special intermediate result vectors within the storage array AUX.

For reference see:

- (1) G.N. Lance, Numerical Methods for High Speed Computers, Pitman, London, 1960, pp. 64 - 67.
- (2) A. Ralston/H.S. Wilf, Mathematical Methods for Digital Computers, Wiley, New York/London, 1960, pp. 95 - 109.
- (3) A. Ralston, "Runge-Kutta Methods with Minimum Error Bounds", MTAC, vol. 16, no. 80 (1962), pp. 431 - 437.
- (4) R. Zurmühl, Praktische Mathematik für Ingenieure und Physiker, Springer, Berlin/Göttingen/Heidelberg, 1963, pp. 227 - 232.

function vector	$Y_{j-6} = Y(x_{j-6})$	1. row (AUX (1) in flowchart)
function vector	$Y_{j-5} = Y(x_{j-5})$	2. row (AUX (2) in flowchart)
function vector	$Y_{j-4} = Y(x_{j-4})$	3. row (AUX (3) in flowchart)
function vector	$Y_{j-3} = Y(x_{j-3})$	4. row (AUX (4) in flowchart)
function vector	$Y_{j-2} = Y(x_{j-2})$	5. row (AUX (5) in flowchart)
function vector	$Y_{j-1} = Y(x_{j-1})$	6. row (AUX (6) in flowchart)
function vector	$Y_j = Y(x_j)$	7. row (AUX (7) in flowchart)
derivative vector	$Y'_{j-6} = Y'(x_{j-6})$	8. row (AUX (8) in flowchart)
derivative vector	$Y'_{j-5} = Y'(x_{j-5})$	9. row (AUX (9) in flowchart)
derivative vector	$Y'_{j-4} = Y'(x_{j-4})$	10. row (AUX (10) in flowchart)
derivative vector	$Y'_{j-3} = Y'(x_{j-3})$	11. row (AUX (11) in flowchart)
derivative vector	$Y'_{j-2} = Y'(x_{j-2})$	12. row (AUX (12) in flowchart)
derivative vector	$Y'_{j-1} = Y'(x_{j-1})$	13. row (AUX (13) in flowchart)
derivative vector	$Y'_j = Y'(x_j)$	14. row (AUX (14) in flowchart)
vector of error weights		15. row (AUX (15) in flowchart)
vector $P_j - C_j$		16. row (AUX (16) in flowchart)
decision vector for zero-columns in Matrix C		17. row (AUX (17) in flowchart)
vector $F(x_j)$		18. row (AUX (18) in flowchart)
vector $F'(x_j)$		19. row (AUX (19) in flowchart)
right-hand side vector R		20. row (AUX (20) in flowchart)

Figure 34. Storage allocation in auxiliary storage array AUX (LBVP-DLBVP)

```

C
C ..... LBVP 10
C ..... LBVP 20
C ..... LBVP 30
C ..... LBVP 40
C ..... LBVP 50
C ..... LBVP 60
C ..... LBVP 70
C ..... LBVP 80
C ..... LBVP 90
C ..... LBVP 100
C ..... LBVP 110
C ..... LBVP 120
C ..... LBVP 130
C ..... LBVP 140
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C ..... LBVP 440
C ..... LBVP 450
C ..... LBVP 460
C ..... LBVP 470
C ..... LBVP 480
C ..... LBVP 490
C ..... LBVP 500
C ..... LBVP 510

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C
C R - AN INPUT VECTOR WITH DIMENSION NDIM. (DESTROYED) LBVP 520
C IT SPECIFIES THE RIGHT HAND SIDE OF THE LBVP 530
C BOUNDARY CONDITIONS. LBVP 540
C
C Y - AN AUXILIARY VECTOR WITH DIMENSION NDIM. LBVP 550
C IT IS USED AS STORAGE LOCATION FOR THE RESULTING LBVP 560
C VALUES OF DEPENDENT VARIABLES COMPUTED AT LBVP 570
C INTERMEDIATE POINTS. LBVP 580
C
C DERY - INPUT VECTOR OF ERROR WEIGHTS. (DESTROYED) LBVP 590
C ITS MAXIMAL COMPONENT SHOULD BE EQUAL TO 1. LBVP 600
C LATERON DERY IS THE VECTOR OF DERIVATIVES, WHICH LBVP 610
C BELONG TO FUNCTION VALUES Y AT INTERMEDIATE POINTS. LBVP 620
C
C NDIM - AN INPUT VALUE, WHICH SPECIFIES THE NUMBER OF LBVP 630
C DIFFERENTIAL EQUATIONS IN THE SYSTEM. LBVP 640
C
C IHLF - AN OUTPUT VALUE, WHICH SPECIFIES THE NUMBER OF LBVP 650
C BISECTIONS OF THE INITIAL INCREMENT. IF IHLF GETS LBVP 660
C GREATER THAN 10, SUBROUTINE LBVP RETURNS WITH LBVP 670
C ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM. LBVP 680
C ERROR MESSAGE IHLF=12 OR IHLF=13 APPEARS IN CASE LBVP 690
C PRMT(3)=0 OR IN CASE SIGN(PRMT(3)).NE.SIGN(PRMT(2))-LBVP 700
C PRMT(1) RESPECTIVELY, FINALLY ERROR MESSAGE LBVP 710
C IHLF=14 INDICATES, THAT THERE IS NO SOLUTION OR LBVP 720
C THAT THERE ARE MORE THAN ONE SOLUTION OF THE LBVP 730
C PROBLEM. LBVP 740
C
C A NEGATIVE VALUE OF IHLF HANDED TO SUBROUTINE OUTP LBVP 750
C TOGETHER WITH INITIAL VALUES OF FINALLY GENERATED LBVP 760
C INITIAL VALUE PROBLEM INDICATES, THAT THERE WAS LBVP 770
C POSSIBLE LOSS OF SIGNIFICANCE IN THE SOLUTION OF LBVP 780
C THE SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS FOR LBVP 790
C THESE INITIAL VALUES. THE ABSOLUTE VALUE OF IHLF LBVP 800
C SHOWS, AFTER WHICH ELIMINATION STEP OF GAUSS LBVP 810
C ALGORITHM POSSIBLE LOSS OF SIGNIFICANCE WAS LBVP 820
C DETECTED. LBVP 830
C
C AFCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. IT LBVP 840
C COMPUTES THE COEFFICIENT MATRIX A OF VECTOR Y ON LBVP 850
C EQUATIONS FOR A GIVEN X-VALUE. ITS PARAMETER LIST LBVP 860
C MUST BE X,A. SUBROUTINE AFCT SHOULD NOT DESTROY X. LBVP 880
C
C FCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. IT LBVP 890
C COMPUTES VECTOR F (INHOMOGENEOUS PART OF THE LBVP 900
C RIGHT HAND SIDE OF THE SYSTEM OF DIFFERENTIAL LBVP 910
C EQUATIONS) FOR A GIVEN X-VALUE. ITS PARAMETER LIST LBVP 920
C MUST BE X,F. SUBROUTINE FCT SHOULD NOT DESTROY X. LBVP 930
C
C DFCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. IT LBVP 940
C COMPUTES VECTOR DF (DERIVATIVE OF THE INHOMOGENEOUS LBVP 950
C PART ON THE RIGHT HAND SIDE OF THE SYSTEM OF LBVP 960
C DIFFERENTIAL EQUATIONS) FOR A GIVEN X-VALUE. ITS LBVP 970
C PARAMETER LIST MUST BE X,DF. SUBROUTINE DFCT LBVP 980
C SHOULD NOT DESTROY X. LBVP 990
C
C OUTP - THE NAME OF AN EXTERNAL OUTPUT SUBROUTINE USED. LBVP 1000
C ITS PARAMETER LIST MUST BE X,Y,DERY,IHLF,NDIM,PRMT-LBVP 1010
C NONE OF THESE PARAMETERS (EXCEPT, IF NECESSARY, LBVP 1020
C PRMT(4),PRMT(5),...) SHOULD BE CHANGED BY LBVP 1030
C SUBROUTINE OUTP. IF PRMT(5) IS CHANGED TO NON-ZERO, LBVP 1040
C SUBROUTINE LBVP IS TERMINATED. LBVP 1050
C
C AUX - AN AUXILIARY STORAGE ARRAY WITH 20 ROWS AND LBVP 1060
C NDIM COLUMNS. LBVP 1070
C
C A - AN NDIM BY NDIM MATRIX, WHICH IS USED AS AUXILIARY LBVP 1080
C STORAGE ARRAY. LBVP 1090
C
C REMARKS LBVP 1100
C
C THE PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF LBVP 1120
C (1) MORE THAN 10 BISECTIONS OF THE INITIAL INCREMENT ARE LBVP 1130
C NECESSARY TO GET SATISFACTORY ACCURACY (ERROR MESSAGE LBVP 1140
C IHLF=11), LBVP 1150
C (2) INITIAL INCREMENT IS EQUAL TO 0 OR IF IT HAS WRONG SIGN LBVP 1160
C (ERROR MESSAGES IHLF=12 OR IHLF=13), LBVP 1170
C (3) THERE IS NO OR MORE THAN ONE SOLUTION OF THE PROBLEM LBVP 1180
C (ERROR MESSAGE IHLF=14), LBVP 1190
C (4) THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH, LBVP 1200
C (5) SUBROUTINE OUTP HAS CHANGED PRMT(5) TO NON-ZERO. LBVP 1210
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED LBVP 1220
C
C SUBROUTINE GELG SYSTEM OF LINEAR EQUATIONS. LBVP 1240
C THE EXTERNAL SUBROUTINES AFCT(X,A), FCT(X,F), DFCT(X,DF), LBVP 1250
C AND OUTP(X,Y,DERY,IHLF,NDIM,PRMT) MUST BE FURNISHED LBVP 1260
C BY THE USER. LBVP 1270
C
C METHOD LBVP 1280
C
C EVALUATION IS DONE USING THE METHOD OF ADJOINT EQUATIONS. LBVP 1290
C HAMMINGS FOURTH ORDER MODIFIED PREDICTOR-CORRECTOR METHOD LBVP 1300
C IS USED TO SOLVE THE ADJOINT INITIAL VALUE PROBLEMS AND FI- LBVP 1310
C NALLY TO SOLVE THE GENERATED INITIAL VALUE PROBLEM FOR Y(X). LBVP 1320
C THE INITIAL INCREMENT PRMT(3) IS AUTOMATICALLY ADJUSTED. LBVP 1330
C FOR COMPUTATION OF INTEGRAL SUM, A FOURTH ORDER HERMITEAN LBVP 1340
C INTEGRATION FORMULA IS USED. LBVP 1350
C FOR REFERENCE, SEE LBVP 1360
C (1) LANGE, NUMERICAL METHODS FOR HIGH SPEED COMPUTERS, LBVP 1380
C ILIFFE, LONDON, 1960, PP.64-67. LBVP 1390
C (2) RALSTON/WILF, MATHEMATICAL METHODS FOR DIGITAL LBVP 1400
C COMPUTERS, WILEY, NEW YORK/LONDON, 1960, PP.95-109. LBVP 1410
C (3) RALSTON, RUNGE-KUTTA METHODS WITH MINIMUM ERROR BOUNDS, LBVP 1420
C MTAC, VOL.16, ISS.00 (1962), PP.431-437. LBVP 1430
C (4) ZURMUEHL, PRAKTIISCHE MATHEMATIK FUER INGENIEURE UND LBVP 1440
C PHYSIKER, SPRINGER, BERLIN/GOETTINGEN/WEIDELBERG, 1963, LBVP 1450
C PP.227-232. LBVP 1460
C
C ..... LBVP 1470
C ..... LBVP 1480
C ..... LBVP 1490
C ..... LBVP 1500
C ..... LBVP 1510
C ..... LBVP 1520
C ..... LBVP 1530
C ..... LBVP 1540
C ..... LBVP 1550
C ..... LBVP 1560
C ..... LBVP 1570
C ..... LBVP 1580
C ..... LBVP 1590
C ..... LBVP 1600
C ..... LBVP 1610
C ..... LBVP 1620
C ..... LBVP 1630
C ..... LBVP 1640
C ..... LBVP 1650
C ..... LBVP 1660
C ..... LBVP 1670
C ..... LBVP 1680
C ..... LBVP 1690
C ..... LBVP 1700
C ..... LBVP 1710
C ..... LBVP 1720
C ..... LBVP 1730
C ..... LBVP 1740
C ..... LBVP 1750
C ..... LBVP 1760
C ..... LBVP 1770
C ..... LBVP 1780
C ..... LBVP 1790
C ..... LBVP 1800

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IC=IC+1
AUX(17,K)=0.
7 CONTINUE
C
C DETERMINATION OF LOWER AND UPPER BOUND
IF(IC-18)B,11,11
8 H=PRMT(2)
PRMT(2)=PRMT(1)
PRMT(1)=H
PRMT(3)=PRMT(3)
DO 9 I=1,NDIM
9 AUX(17,I)=AUX(1,I)
I=NDIM*NDIM
DO 10 I=1,11
H=B(I)
B(1)=C(1)
10 C(1)=H
C
C PREPARATIONS FOR CONSTRUCTION OF ADJOINT INITIAL VALUE PROBLEMS
11 X=PRMT(2)
CALL FCT(X,Y)
CALL DFCT(X,DERY)
DO 12 I=1,NDIM
AUX(18,I)=Y(I)
12 AUX(19,I)=DERY(I)
C
C POSSIBLE BREAK-POINT FOR LINKAGE
C
C THE FOLLOWING PART OF SUBROUTINE LBVP UNTIL NEXT BREAK-POINT FOR
C LINKAGE HAS TO REMAIN IN CORE DURING THE WHOLE REST OF THE
C COMPUTATIONS
C
C START LOOP FOR GENERATING ADJOINT INITIAL VALUE PROBLEMS
K=0
KK=0
100 K=K+1
IF(AUX(17,K))108,108,101
C
C INITIALIZATION OF ADJOINT INITIAL VALUE PROBLEM
101 X=PRMT(2)
CALL AFCT(X,A)
SUM=0.
GL=AUX(18,K)
DGL=AUX(19,K)
I=K
DO 104 I=1,NDIM
H=-A(I)
DERY(I)=H
AUX(20,I)=R(I)
Y(I)=0.
IF(I-K)103,102,103
102 Y(I)=L.
103 DGL=DGL+H*AUX(18,I)
104 I=I+NDIM
XEND=PRMT(1)
H=-.0625*(XEND-X)
ISW=0
GOTO 400
C
C THIS IS BRANCH TO ADJOINT LINEAR INITIAL VALUE PROBLEM
C
C THIS IS RETURN FROM ADJOINT LINEAR INITIAL VALUE PROBLEM
105 IF(IHLF-10)106,106,117
C
C UPDATING OF COEFFICIENT MATRIX B AND VECTOR R
106 DO 107 I=1,NDIM
KK=KK+1
H=C(KK)
R(I)=AUX(20,I)+H*SUM
I=I+1
DO 107 J=1,NDIM
B(I)=B(I)+H*Y(J)
107 I=I+NDIM
GOTO 109
108 KK=KK+NDIM
109 IF(K-NDIM)100,110,110
C
C GENERATION OF LAST INITIAL VALUE PROBLEM
110 X=PRMT(4)
CALL GELGIR(B,NDIM,I,X,I)
IF(I)111,112,112
111 IHLF=14
RETURN
C
112 PRMT(5)=0.
IHLF=-I
X=PRMT(1)
XEND=PRMT(2)
H=PRMT(3)
DO 113 I=1,NDIM
Y(I)=R(I)
113 Y(I)=R(I)
ISW=1
114 ISW=12
GOTO 200
115 ISW=1
GOTO 300
116 IF(IHLF/400,400,117
C
C THIS WAS BRANCH INTO INITIAL VALUE PROBLEM
C
C THIS IS RETURN FROM INITIAL VALUE PROBLEM
117 RETURN
C
C THIS PART OF LINEAR BOUNDARY VALUE PROBLEM COMPUTES THE RIGHT
C HAND SIDE DERY OF THE SYSTEM OF ADJOINT LINEAR DIFFERENTIAL
C EQUATIONS (IN CASE ISW=0) OR OF THE GIVEN SYSTEM (IN CASE ISW=1).
200 CALL AFCT(X,A)
IF(ISW)201,201,205
C
C ADJOINT SYSTEM
201 LL=0
DO 203 M=1,NDIM
HS=0.
DO 202 L=1,NDIM
LL=LL+1
202 HS=HS+A(LL)*Y(L)
203 DERY(M)=HS
204 GOTO(502,504,506,407,415,418,608,617,632,634,421,1151,ISW2)
C
C GIVEN SYSTEM
205 CALL FCT(X,DERY)
DO 207 M=1,NDIM
LL=M-NDIM
HS=0.
DO 206 L=1,NDIM
LL=LL+NDIM
206 HS=HS+A(LL)*Y(L)
207 DERY(M)=HS+DERY(M)
GOTO 204
C
C THIS PART OF LINEAR BOUNDARY VALUE PROBLEM COMPUTES THE VALUE OF
LBVP1810
LBVP1820
LBVP1830
LBVP1840
LBVP1850
LBVP1860
LBVP1870
LBVP1880
LBVP1890
LBVP1900
LBVP1910
LBVP1920
LBVP1930
LBVP1940
LBVP1950
LBVP1960
LBVP1970
LBVP1980
LBVP1990
LBVP2000
LBVP2010
LBVP2020
LBVP2030
LBVP2040
LBVP2050
LBVP2060
LBVP2070
LBVP2080
LBVP2090
LBVP2100
LBVP2110
LBVP2120
LBVP2130
LBVP2140
LBVP2150
LBVP2160
LBVP2170
LBVP2180
LBVP2190
LBVP2200
LBVP2210
LBVP2220
LBVP2230
LBVP2240
LBVP2250
LBVP2260
LBVP2270
LBVP2280
LBVP2290
LBVP2300
LBVP2310
LBVP2320
LBVP2330
LBVP2340
LBVP2350
LBVP2360
LBVP2370
LBVP2380
LBVP2390
LBVP2400
LBVP2410
LBVP2420
LBVP2430
LBVP2440
LBVP2450
LBVP2460
LBVP2470
LBVP2480
LBVP2490
LBVP2500
LBVP2510
LBVP2520
LBVP2530
LBVP2540
LBVP2550
LBVP2560
LBVP2570
LBVP2580
LBVP2590
LBVP2600
LBVP2610
LBVP2620
LBVP2630
LBVP2640
LBVP2650
LBVP2660
LBVP2670
LBVP2680
LBVP2690
LBVP2700
LBVP2710
LBVP2720
LBVP2730
LBVP2740
LBVP2750
LBVP2760
LBVP2770
LBVP2780
LBVP2790
LBVP2800
LBVP2810
LBVP2820
LBVP2830
LBVP2840
LBVP2850
LBVP2860
LBVP2870
LBVP2880
LBVP2890
LBVP2900
LBVP2910
LBVP2920
LBVP2930
LBVP2940
LBVP2950
LBVP2960
LBVP2970
LBVP2980
LBVP2990
LBVP3000
LBVP3010
LBVP3020
LBVP3030
LBVP3040
LBVP3050
LBVP3060
LBVP3070
LBVP3080
LBVP3090
C
C INTEGRAL SUM, WHICH IS A PART OF THE OUTPUT OF ADJOINT INITIAL
C VALUE PROBLEM (IN CASE ISW=0) OR RECORDS RESULT VALUES OF THE
C FINAL INITIAL VALUE PROBLEM (IN CASE ISW=1).
300 IF(ISW)301,301,305
C
C ADJOINT PROBLEM
301 CALL FCT(X,R)
GU=0.
DGU=0.
DO 302 L=1,NDIM
GU=GU+Y(L)*R(L)
302 DGU=DGU+DERY(L)*R(L)
CALL DFCT(X,R)
DO 303 L=1,NDIM
303 DGU=DGU+Y(L)*R(L)
SUM=SUM+.5*H*(DGL+GU)+.1666667*H*(DGL-DGU)
GL=GU
DGL=DGU
304 IF(ISW)3116,422,618
C
C GIVEN PROBLEM
305 CALL OUTPIX,Y,DERY,IHLF,NDIM,PRMT)
IF(PRMT(5))117,304,117
C
C POSSIBLE BREAK-POINT FOR LINKAGE
C
C THE FOLLOWING PART OF SUBROUTINE LBVP SOLVES IN CASE ISW=0 THE
C ADJOINT INITIAL VALUE PROBLEM. IT COMPUTES INTEGRAL SUM AND
C THE VECTOR Y OF DEPENDENT VARIABLES AT THE LOWER BOUND PRMT(1).
C IN CASE ISW=1 IT SOLVES FINALLY GENERATED INITIAL VALUE PROBLEM.
400 N=1
XST=X
IHLF=0
DO 401 I=1,NDIM
AUX(16,I)=0.
AUX(1,I)=Y(I)
401 AUX(18,I)=DERY(I)
ISW=1
GOTO 500
C
402 X=X+H
DO 403 I=1,NDIM
403 AUX(2,I)=Y(I)
C
C INCREMENT H IS TESTED BY MEANS OF BISECTION
404 IHLF=IHLF+1
X=X-H
DO 405 I=1,NDIM
405 AUX(4,I)=AUX(2,I)
H=.5*H
N=N+1
ISW=2
GOTO 500
C
406 X=X+H
ISW=6
GOTO 200
407 N=2
DO 408 I=1,NDIM
AUX(2,I)=Y(I)
408 AUX(19,I)=DERY(I)
ISW=3
GOTO 500
C
C TEST ON SATISFACTORY ACCURACY
409 DO 414 I=1,NDIM
Z=ABS(Y(I))
IF(Z-.1,410,411,411
410 Z=.1
411 DELT=.0666667*ABS(Y(I)-AUX(4,I))
IF(ISW)413,413,412
412 DELT=AUX(15,I)*DELT
413 IF(DELT-Z*PRMT(4))1414,414,429
414 CONTINUE
C
C SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS
X=X+H
ISW=5
GOTO 200
415 DO 416 I=1,NDIM
AUX(3,I)=Y(I)
416 AUX(10,I)=DERY(I)
N=3
ISW=4
GOTO 500
C
417 N=1
X=X+H
ISW=6
GOTO 200
418 X=XST
DO 419 I=1,NDIM
AUX(11,I)=DERY(I)
419 C(Y)=AUX(1,I)+H*(.375*AUX(8,I)+.7916667*AUX(9,I)
1-.2083333*AUX(10,I)+.04166667*DERY(I))
420 X=X+H
N=N+1
ISW=11
GOTO 200
421 ISW=0
GOTO 300
422 IF(N-4)423,600,600
423 DO 424 I=1,NDIM
AUX(1,I)=Y(I)
424 AUX(17,I)=DERY(I)
IF(N-3)425,427,600
C
425 DO 426 I=1,NDIM
DELT=AUX(9,I)+AUX(9,I)
DELT=DELT+DELT
426 Y(I)=AUX(1,I)+.3333333*H*(AUX(8,I)+DELT+AUX(10,I))
GOTO 420
C
427 DO 428 I=1,NDIM
DELT=AUX(9,I)+AUX(10,I)
DELT=DELT+DELT+DELT
428 Y(I)=AUX(1,I)+.375*H*(AUX(8,I)+DELT+AUX(11,I))
GOTO 420
C
C NO SATISFACTORY ACCURACY. H MUST BE HALVED.
429 IF(IHLF-10)404,430,430
C
C NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.
430 IHLF=11
X=X+H
IF(ISW)105,105,114
C
C THIS PART OF LINEAR INITIAL VALUE PROBLEM COMPUTES
C STARTING VALUES BY MEANS OF RUNGE-KUTTA METHOD.
LBVP3100
LBVP3110
LBVP3120
LBVP3130
LBVP3140
LBVP3150
LBVP3160
LBVP3170
LBVP3180
LBVP3190
LBVP3200
LBVP3210
LBVP3220
LBVP3230
LBVP3240
LBVP3250
LBVP3260
LBVP3270
LBVP3280
LBVP3290
LBVP3300
LBVP3310
LBVP3320
LBVP3330
LBVP3340
LBVP3350
LBVP3360
LBVP3370
LBVP3380
LBVP3390
LBVP3400
LBVP3410
LBVP3420
LBVP3430
LBVP3440
LBVP3450
LBVP3460
LBVP3470
LBVP3480
LBVP3490
LBVP3500
LBVP3510
LBVP3520
LBVP3530
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LBVP3550
LBVP3560
LBVP3570
LBVP3580
LBVP3590
LBVP3600
LBVP3610
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LBVP3650
LBVP3660
LBVP3670
LBVP3680
LBVP3690
LBVP3700
LBVP3710
LBVP3720
LBVP3730
LBVP3740
LBVP3750
LBVP3760
LBVP3770
LBVP3780
LBVP3790
LBVP3800
LBVP3810
LBVP3820
LBVP3830
LBVP3840
LBVP3850
LBVP3860
LBVP3870
LBVP3880
LBVP3890
LBVP3900
LBVP3910
LBVP3920
LBVP3930
LBVP3940
LBVP3950
LBVP3960
LBVP3970
LBVP3980
LBVP3990
LBVP4000
LBVP4010
LBVP4020
LBVP4030
LBVP4040
LBVP4050
LBVP4060
LBVP4070
LBVP4080
LBVP4090
LBVP4100
LBVP4110
LBVP4120
LBVP4130
LBVP4140
LBVP4150
LBVP4160
LBVP4170
LBVP4180
LBVP4190
LBVP4200
LBVP4210
LBVP4220
LBVP4230
LBVP4240
LBVP4250
LBVP4260
LBVP4270
LBVP4280
LBVP4290
LBVP4300
LBVP4310
LBVP4320
LBVP4330
LBVP4340
LBVP4350
LBVP4360
LBVP4370
LBVP4380

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500 Z=X
DO 501 I=1,NDIM
  XH=AUX(N+7,I)
  AUX(5,I)=X
C
501 Y(I)=AUX(N,I)+.4*X
  X=Z+.4*H
  ISW2=1
  GOTO 200
502 DO 503 I=1,NDIM
  X=H*DERY(I)
  AUX(6,I)=X
C
503 Y(I)=AUX(N,I)+.2969776*AUX(5,I)+.1587596*X
  X=Z+.4557372*H
  ISW2=2
  GOTO 200
504 DO 505 I=1,NDIM
  X=H*DERY(I)
  AUX(7,I)=X
C
505 Y(I)=AUX(N,I)+.2181004*AUX(5,I)+.050965*AUX(6,I)+.3.832865*X
  X=Z+H
  ISW2=3
  GOTO 200
506 DO 507 I=1,NDIM
  5070Y(I)=AUX(N,I)+.1747603*AUX(5,I)+.5514807*AUX(6,I)
  1+.205536*AUX(7,I)+.1711840*H*DERY(I)
  X=Z
  GOTO(402,406,409,417),ISW1
C
C POSSIBLE BREAK-POINT FOR LINKAGE
C
C STARTING VALUES ARE COMPUTED.
C NOW START HAMMING'S MODIFIED PREDICTOR-CORRECTOR METHOD.
600 ISTEP=3
601 IF(N-8)604,602,604
C
C N=8 CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS
602 DO 603 I=1,NDIM
  DO 603 J=1,NDIM
    AUX(N-1,I)=AUX(N,I)
  603 AUX(N+6,I)=AUX(N+7,I)
  N=7
C
C N LESS THAN 8 CAUSES N+1 TO GET N
604 N=N+1
C
C COMPUTATION OF NEXT VECTOR Y
DO 605 I=1,NDIM
  AUX(N-1,I)=Y(I)
  605 AUX(N+6,I)=DERY(I)
  X=X+H
  606 ISTEP=ISTEP+1
  DO 607 I=1,NDIM
    ODELTA=AUX(N-4,I)+.333333*H*(AUX(N+6,I)+AUX(N+6,I)-AUX(N+5,I))+
    1AUX(N+6,I)+AUX(N+6,I)
    Y(I)=DELTA-.9256198*AUX(16,I)
  607 AUX(16,I)=DELTA
C
C PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX; MODIFIED PREDICTOR
C IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.
  ISW2=7
  GOTO 200
C
C DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY.
608 DO 609 I=1,NDIM
  ODELTA=.125*(9*AUX(N-1,I)-AUX(N-3,I)+3*H*(DERY(I)+AUX(N+6,I)+
  1AUX(N+6,I)-AUX(N+5,I)))
  AUX(16,I)=AUX(16,I)-DELT
  609 Y(I)=DELTA+.07438017*AUX(16,I)
C
C TEST WHETHER H MUST BE HALVED OR DOUBLED
DELT=DELT/2
DO 616 I=1,NDIM
  Z=ABS(Y(I))
  IF(Z-1.1610,611,611)
  610 Z=1.
  611 Z=ABS(AUX(16,I))/Z
  IF(ISW)613,613,612
  612 Z=AUX(15,I)/Z
  613 IF(Z-PRMT(4))614,614,628
  614 IF(DELT-.21615,616,616)
  615 DELT=Z
  616 CONTINUE
C
C H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.
ISW2=8
GOTO 200
617 ISW3=1
GOTO 300
618 IF(H*(X-XEND))619,621,621
619 IF(ABS(X-XEND)-1*ABS(H))621,620,620
620 IF(DELT-.02*PRMT(4))622,622,601
621 IF(ISW)105,105,117
C
C H COULD BE DOUBLED IF ALL NECESSARY PRECEEDING VALUES ARE
C AVAILABLE.
622 IF(IHMF)601,601,623
623 IF(N-7)601,624,624
624 IF(ISTEP-4)601,625,625
625 IMOD=ISTEP/2
  IF(ISTEP-IMOD-IMOD)601,626,601
626 H=H*H
  IHMF=IHMF-1
  ISTEP=0
  DO 627 I=1,NDIM
    AUX(N-1,I)=AUX(N-2,I)
    AUX(N-2,I)=AUX(N-4,I)
    AUX(N-3,I)=AUX(N-6,I)
    AUX(N+6,I)=AUX(N+5,I)
    AUX(N+5,I)=AUX(N+3,I)
    AUX(N+4,I)=AUX(N+1,I)
    DELT=AUX(N+6,I)+AUX(N+5,I)
    DELTA=DELT+DELTA
  6270AUX(16,I)=.962963*(Y(I)-AUX(N-3,I))+.3.361111*H*(DERY(I)+DELT
  1+AUX(N+4,I))
  GOTO 601
C
C
C H MUST BE HALVED
628 IHMF=IHMF+1
  IF(IHMF-10)630,630,629
  629 IF(ISW)105,105,114
  630 H=.5*H
  ISTEP=0
  DO 631 I=1,NDIM
    OY(I)=.00390625*(80.*AUX(N-1,I)+135.*AUX(N-2,I)+40.*AUX(N-3,I)+

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LBPV4390
LBPV4400
LBPV4410
LBPV4420
LBPV4430
LBPV4440
LBPV4450
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LBPV4470
LBPV4480
LBPV4490
LBPV4500
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LBPV4990
LBPV5000
LBPV5010
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LBPV5110
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LBPV5160
LBPV5170
LBPV5180
LBPV5190
LBPV5200
LBPV5210
LBPV5220
LBPV5230
LBPV5240
LBPV5250
LBPV5260
LBPV5270
LBPV5280
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LBPV5300
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LBPV5640
LBPV5650
LBPV5660
LBPV5670

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  1AUX(N-4,I))+.1171875*(AUX(N+6,I)-6.*AUX(N+5,I)-AUX(N+4,I))+H
  OAU(X(N-4,I))-.00390625*(12.*AUX(N-1,I)+135.*AUX(N-2,I)+
  1108.*AUX(N-3,I)+AUX(N-4,I))+.0234375*(AUX(N+6,I)+18.*AUX(N+5,I)-
  29.*AUX(N+4,I))+H
  AUX(N-3,I)=AUX(N-2,I)
  631 AUX(N+4,I)=AUX(N+5,I)
  DELT=X-H
  X=DELTA*(H+H)
  ISW2=9
  GOTO 200
632 DO 633 I=1,NDIM
  AUX(N-2,I)=Y(I)
  AUX(N+5,I)=DERY(I)
  633 Y(I)=AUX(N-4,I)
  X=X-(H+H)
  ISW2=10
  GOTO 200
634 X=DELT
  DO 635 I=1,NDIM
    DELTA=AUX(N+5,I)+AUX(N+4,I)
    DELT=DELT+DELTA+DELT
    OAU(X(I))+.962963*(AUX(N-1,I)-Y(I))-3.361111*H*(AUX(N+6,I)+DELT
    1+DERY(I))
  635 AUX(N+3,I)=DERY(I)
  GOTO 606
C
C END OF INITIAL VALUE PROBLEM
END
C
C -----
C
C SUBROUTINE DLBVP
C
C PURPOSE
C TO SOLVE A LINEAR BOUNDARY VALUE PROBLEM, WHICH CONSISTS OF
C A SYSTEM OF NDM LINEAR FIRST ORDER DIFFERENTIAL EQUATIONS
C DY/DX=A(X)Y(X)+F(X)
C AND NDM LINEAR BOUNDARY CONDITIONS
C B=Y(XL)+C*Y(XU)=R.
C
C USAGE
C CALL DLBVP (PRMT,B,C,R,Y,DERY,NDIM,IHMF,AFCT,FCT,DFCT,OUTP,
C AUX,A)
C PARAMETERS AFCT,FCT,DFCT,OUTP REQUIRE AN EXTERNAL STATEMENT.
C
C DESCRIPTION OF PARAMETERS
C PRMT - DOUBLE PRECISION INPUT AND OUTPUT VECTOR WITH
C DIMENSION GREATER THAN OR EQUAL TO 5, WHICH
C SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF
C ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN
C OUTPUT SUBROUTINE (FURNISHED BY THE USER) AND
C SUBROUTINE DLBVP. EXCEPT PRMT(5) THE COMPONENTS
C ARE NOT DESTROYED BY SUBROUTINE DLBVP AND THEY ARE
C PRMT(1)- LOWER BOUND XU OF THE INTERVAL (INPUT),
C PRMT(2)- UPPER BOUND XU OF THE INTERVAL (INPUT),
C PRMT(3)- INITIAL INCREMENT OF THE INDEPENDENT VARIABLE
C (INPUT),
C PRMT(4)- UPPER ERROR BOUND (INPUT). IF RELATIVE ERROR IS
C GREATER THAN PRMT(4), INCREMENT GETS HALVED.
C IF INCREMENT IS LESS THAN PRMT(3) AND RELATIVE
C ERROR LESS THAN PRMT(4)/50, INCREMENT GETS DOUBLED.
C THE USER MAY CHANGE PRMT(4) BY MEANS OF HIS
C OUTPUT SUBROUTINE.
C PRMT(5)- NO INPUT PARAMETER. SUBROUTINE DLBVP INITIALIZES
C PRMT(5)=0. IF THE USER WANTS TO TERMINATE
C SUBROUTINE DLBVP AT ANY OUTPUT POINT, HE HAS TO
C CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE
C OUTP. FURTHER COMPONENTS OF VECTOR PRMT ARE
C FEASIBLE IF ITS DIMENSION IS DEFINED GREATER
C THAN 5. HOWEVER, SUBROUTINE DLBVP DOES NOT REQUIRE
C AND CHANGE THEM. NEVERTHELESS THEY MAY BE USEFUL
C FOR HANDING RESULT VALUES TO THE MAIN PROGRAM
C (CALLING DLBVP) WHICH ARE OBTAINED BY SPECIAL
C MANIPULATIONS WITH OUTPUT DATA IN SUBROUTINE OUTP.
C
C B - DOUBLE PRECISION NDM BY NDM INPUT MATRIX
C (DESTROYED). IT IS THE COEFFICIENT MATRIX OF Y(XL)
C IN THE BOUNDARY CONDITIONS.
C
C C - DOUBLE PRECISION NDM BY NDM INPUT MATRIX
C (POSSIBLY DESTROYED). IT IS THE COEFFICIENT MATRIX
C OF Y(XU) IN THE BOUNDARY CONDITIONS.
C
C R - DOUBLE PRECISION INPUT VECTOR WITH DIMENSION NDM
C (DESTROYED). IT SPECIFIES THE RIGHT HAND SIDE OF
C THE BOUNDARY CONDITIONS.
C
C Y - DOUBLE PRECISION AUXILIARY VECTOR WITH
C DIMENSION NDM. IT IS USED AS STORAGE LOCATION
C FOR THE RESULTING VALUES OF DEPENDENT VARIABLES
C COMPUTED AT INTERMEDIATE POINTS X.
C
C DERY - DOUBLE PRECISION INPUT VECTOR OF ERROR WEIGHTS
C (DESTROYED). ITS MAXIMAL COMPONENT SHOULD BE
C EQUAL TO 1. LATERON DERY IS THE VECTOR OF
C DERIVATIVES, WHICH BELONG TO FUNCTION VALUES Y AT
C INTERMEDIATE POINTS X.
C
C NDM - AN INPUT VALUE, WHICH SPECIFIES THE NUMBER OF
C DIFFERENTIAL EQUATIONS IN THE SYSTEM.
C
C IHMF - AN OUTPUT VALUE, WHICH SPECIFIES THE NUMBER OF
C BISECTIONS OF THE INITIAL INCREMENT. IF IHMF GETS
C GREATER THAN 10, SUBROUTINE DLBVP RETURNS WITH
C ERROR MESSAGE IHMF=11 INTO MAIN PROGRAM.
C
C ERROR MESSAGE IHMF=12 OR IHMF=13 APPEARS IN CASE
C PRMT(3)=0 OR IN CASE SIGN(PRMT(3)).NE.SIGN(PRMT(2))-DLBVP
C PRMT(1)) RESPECTIVELY. FINALLY ERROR MESSAGE
C IHMF=14 INDICATES, THAT THERE IS NO SOLUTION OR
C THAT THERE ARE MORE THAN ONE SOLUTION OF THE
C PROBLEM.
C
C A NEGATIVE VALUE OF IHMF HANDED TO SUBROUTINE OUTP
C TOGETHER WITH INITIAL VALUES OF FINALLY GENERATED
C INITIAL VALUE PROBLEM INDICATES, THAT THERE WAS
C POSSIBLE LOSS OF SIGNIFICANCE IN THE SOLUTION OF
C THE SYSTEM OF SIMULTANEOUS LINEAR EQUATIONS FOR
C THESE INITIAL VALUES. THE ABSOLUTE VALUE OF IHMF
C SHOWS, AFTER WHICH ELIMINATION STEP OF GAUSS
C ALGORITHM POSSIBLE LOSS OF SIGNIFICANCE WAS
C DETECTED.
C
C AFCT - THE NAME OF AN EXTERNAL SUBROUTINE USED, IT
C COMPUTES THE COEFFICIENT MATRIX A OF VECTOR Y ON
C THE RIGHT HAND SIDE OF THE SYSTEM OF DIFFERENTIAL
C EQUATIONS FOR A GIVEN X-VALUE. ITS PARAMETER LIST
C MUST BE X,A. SUBROUTINE AFCT SHOULD NOT DESTROY X.
C
C FCT - THE NAME OF AN EXTERNAL SUBROUTINE USED, IT
C COMPUTES VECTOR F (INHOMOGENEOUS PART OF THE
C RIGHT HAND SIDE OF THE SYSTEM OF DIFFERENTIAL

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C      EQUATIONS) FOR A GIVEN X-VALUE. ITS PARAMETER LIST DLBV 940
C      MUST BE X,F. SUBROUTINE FCT SHOULD NOT DESTROY X. DLBV 950
C      DLBV 960
C      DLBV 970
C      DLBV 980
C      DLBV 990
C      DLBV1000
C      DLBV1010
C      DLBV1020
C      DLBV1030
C      DLBV1040
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C      DLBV1080
C      DLBV1090
C      DLBV1100
C      DLBV1110
C      DLBV1120
C      DLBV1130
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C      DLBV1200
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C      EQUATIONS) FOR A GIVEN X-VALUE. ITS PARAMETER LIST
C      MUST BE X,F. SUBROUTINE FCT SHOULD NOT DESTROY X.
C      THE NAME OF AN EXTERNAL SUBROUTINE USED. IT
C      COMPUTES VECTOR DF (DERIVATIVE OF THE INHOMOGENEOUS
C      PART ON THE RIGHT HAND SIDE OF THE SYSTEM OF
C      DIFFERENTIAL EQUATIONS) FOR A GIVEN X-VALUE. ITS
C      PARAMETER LIST MUST BE X,DF. SUBROUTINE DFCT
C      SHOULD NOT DESTROY X.
C      THE NAME OF AN EXTERNAL OUTPUT SUBROUTINE USED.
C      ITS PARAMETER LIST MUST BE X,Y,DERY,IHLF,NDIM,PRMT.
C      NONE OF THESE PARAMETERS (EXCEPT, IF NECESSARY,
C      PRMT(4),PRMT(5),...) SHOULD BE CHANGED BY
C      SUBROUTINE OUTP. IF PRMT(5) IS CHANGED TO NON-ZERO,
C      SUBROUTINE DLBVP IS TERMINATED.
C      DOUBLE PRECISION AUXILIARY STORAGE ARRAY WITH 20
C      ROWS AND NDIM COLUMNS.
C      DOUBLE PRECISION NOIM BY NDIM MATRIX, WHICH IS USED
C      AS AUXILIARY STORAGE ARRAY.
C      REMARKS
C      THE PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF
C      (1) MORE THAN 10 BISECTIONS OF THE INITIAL INCREMENT ARE
C      NECESSARY TO GET SATISFACTORY ACCURACY (ERROR MESSAGE
C      IHLF=11),
C      (2) INITIAL INCREMENT IS EQUAL TO 0 OR IF IT HAS WRONG SIGN
C      (ERROR MESSAGE IHLF=12),
C      (3) THERE IS NO OR MORE THAN ONE SOLUTION OF THE PROBLEM
C      (ERROR MESSAGE IHLF=14),
C      (4) THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH,
C      (5) SUBROUTINE OUTP HAS CHANGED PRMT(5) TO NON-ZERO.
C      SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C      SUBROUTINE DGLG SYSTEM OF LINEAR EQUATIONS.
C      THE EXTERNAL SUBROUTINES AFCT(X,A), FCT(X,F), DFCT(X,DF),
C      AND OUTP(X,Y,DERY,IHLF,NDIM,PRMT) MUST BE FURNISHED
C      BY THE USER.
C      METHOD
C      EVALUATION IS DONE USING THE METHOD OF ADJOINT EQUATIONS.
C      HAWKINGS FOURTH ORDER MODIFIED PREDICTOR-CORRECTOR METHOD
C      IS USED TO SOLVE THE ADJOINT INITIAL VALUE PROBLEMS AND FI-
C      NALLY TO SOLVE THE GENERATED INITIAL VALUE PROBLEM FOR Y(X).
C      THE INITIAL INCREMENT PRMT(3) IS AUTOMATICALLY ADJUSTED.
C      FOR COMPUTATION OF INTEGRAL SUM, A FOURTH ORDER HERMITEAN
C      INTEGRATION FORMULA IS USED.
C      FOR REFERENCE, SEE
C      (1) LANGE, NUMERICAL METHODS FOR HIGH SPEED COMPUTERS,
C      ILLIFE, LONDON, 1960, PP.64-67.
C      (2) RALSTON/WILEY, MATHEMATICAL METHODS FOR DIGITAL
C      COMPUTERS, WILEY, NEW YORK/LONDON, 1960, PP.95-109.
C      (3) RALSTON, RUNGE-KUTTA METHODS WITH MINIMUM ERROR BOUNDS,
C      MTAC, VOL.16, ISS.80 (1962), PP.431-437.
C      (4) ZURMUEHL, PRAKTIISCHE MATHEMATIK FUER INGENIEURE UND
C      PHYSIKER, SPRINGER, BERLIN/GOETTINGEN/HEIDELBERG, 1963,
C      PP.227-232.
C      CSUBROUTINE DLBVP(PRMT,B,C,R,Y,DERY,NDIM,IHLF,AFCT,FCT,DFCT,OUTP,
C      I,AUX,A)
C      DIMENSION PRMT(1),B(1),C(1),R(1),Y(1),DERY(1),AUX(20,1),A(1)
C      DOUBLE PRECISION PRMT,B,C,R,Y,DERY,AUX,A,H,X,Z,G,I,HS,GU,SUM,
C      IDGL,DGU,XST,XEND,DELTA
C      ERROR TEST
C      IF(PRMT(3)+(PRMT(2)-PRMT(1))/2,1,3
C      1 IHLF=12
C      RETURN
C      2 IHLF=13
C      RETURN
C      SEARCH FOR ZERO-COLUMNS IN MATRICES B AND C
C      3 KK=NDIM
C      IB=C
C      IC=0
C      DO 7 K=1,NDIM
C      AUX(15,K)=DERY(K)
C      AUX(1,K)=1.00
C      AUX(17,K)=1.00
C      KK=KK+NDIM
C      DO 6 I=1,NDIM
C      II=KK+I
C      IF(B(II))5,4,5
C      4 CONTINUE
C      IB=IB+1
C      AUX(1,K)=0.00
C      5 DO 6 I=1,NDIM
C      II=KK+I
C      IF(C(II))7,6,7
C      6 CONTINUE
C      IC=IC+1
C      AUX(17,K)=0.00
C      7 CONTINUE
C      DETERMINATION OF LOWER AND UPPER BOUND
C      IF(IC-IB)8,11,11
C      8 H=PRMT(2)
C      PRMT(2)=PRMT(1)
C      PRMT(1)=H
C      DO 9 I=1,NDIM
C      9 AUX(17,I)=AUX(1,I)
C      II=NDIM+NDIM
C      DO 10 I=1,II
C      H=B(II)
C      B(II)=C(II)
C      C(II)=H
C      10 C(II)=H
C      PREPARATIONS FOR CONSTRUCTION OF ADJOINT INITIAL VALUE PROBLEMS
C      11 X=PRMT(2)
C      CALL FCT(X,Y)
C      CALL DFCT(X,DERY)
C      DO 12 I=1,NDIM
C      AUX(18,I)=Y(II)
C      12 AUX(19,I)=DERY(II)
C      POSSIBLE BREAK-POINT FOR LINKAGE
C      DLBV2120
C      DLBV2130
C      DLBV2140
C      DLBV2150
C      DLBV2160
C      DLBV2170
C      DLBV2180
C      DLBV2190
C      DLBV2200
C      DLBV2210
C      DLBV2220
C      THE FOLLOWING PART OF SUBROUTINE DLBVP UNTIL NEXT BREAK-POINT FOR
C      LINKAGE HAS TO REMAIN IN CORE DURING THE WHOLE REST OF THE
C      COMPUTATIONS
C      START LOOP FOR GENERATING ADJOINT INITIAL VALUE PROBLEMS
C      K=0
C      KK=0
C      100 K=K+1
C      IF(AUX(17,K))108,108,101
C      INITIALIZATION OF ADJOINT INITIAL VALUE PROBLEM
C      101 X=PRMT(2)
C      CALL AFCT(X,A)
C      SUM=0.00
C      GL=AUX(18,K)
C      DGL=AUX(19,K)
C      II=K
C      DO 104 I=1,NDIM
C      H=A(II)
C      DERY(II)=H
C      AUX(20,II)=R(II)
C      Y(II)=0.00
C      IF(I-K)103,102,103
C      102 Y(II)=1.00
C      103 DGL=DGL+H*AUX(18,I)
C      104 II=II+NDIM
C      XEND=PRMT(1)
C      H=.062500*(XEND-X)
C      ISW=0
C      GOTO 400
C      THIS IS BRANCH TO ADJOINT LINEAR INITIAL VALUE PROBLEM
C      C
C      THIS IS RETURN FROM ADJOINT LINEAR INITIAL VALUE PROBLEM
C      105 IF(IHLF=10)106,106,117
C      UPDATING OF COEFFICIENT MATRIX B AND VECTOR R
C      106 DO 107 J=1,NDIM
C      KK=KK+1
C      H=C(KK)
C      R(II)=AUX(20,I)+H*SUM
C      II=I
C      DO 107 J=1,NDIM
C      B(II)=B(II)+H*Y(J)
C      107 II=II+NDIM
C      GOTO 109
C      108 KK=KK+NDIM
C      109 IF(K-NDIM)100,110,110
C      GENERATION OF LAST INITIAL VALUE PROBLEM
C      110 EPS=PRMT(4)
C      CALL DGLG(R,B,NDIM,I,EPS,I)
C      IF(II)111,112,112
C      111 IHLF=14
C      RETURN
C      112 PRMT(5)=0.00
C      IHLF=1
C      X=PRMT(1)
C      XEND=PRMT(2)
C      H=PRMT(3)
C      DO 113 I=1,NDIM
C      113 Y(II)=R(II)
C      ISW=1
C      114 ISW2=12
C      GOTO 200
C      115 ISW3=1
C      GOTO 300
C      116 IF(IHLF=1400,400,117
C      THIS WAS BRANCH INTO INITIAL VALUE PROBLEM
C      C
C      THIS IS RETURN FROM INITIAL VALUE PROBLEM
C      117 RETURN
C      THIS PART OF LINEAR BOUNDARY VALUE PROBLEM COMPUTES THE RIGHT
C      HAND SIDE DERY OF THE SYSTEM OF ADJOINT LINEAR DIFFERENTIAL
C      EQUATIONS (IN CASE ISW=0) OR OF THE GIVEN SYSTEM (IN CASE ISW=1).
C      200 CALL AFCT(X,A)
C      IF(ISW)201,201,205
C      ADJOINT SYSTEM
C      201 LL=0
C      DO 203 M=1,NDIM
C      HS=0.00
C      DO 202 L=1,NDIM
C      LL=LL+1
C      202 HS=HS+A(LL)*Y(L)
C      203 DERY(M)=HS
C      204 GOTO(502,504,506,407,415,418,608,617,632,634,421,115),ISW2
C      GIVEN SYSTEM
C      205 CALL FCT(X,DERY)
C      DO 207 M=1,NDIM
C      LL=M-NDIM
C      HS=0.00
C      DO 206 L=1,NDIM
C      LL=LL+NDIM
C      206 HS=HS+A(LL)*Y(L)
C      207 DERY(M)=HS+DERY(M)
C      GOTO 204
C      THIS PART OF LINEAR BOUNDARY VALUE PROBLEM COMPUTES THE VALUE OF
C      INTEGRAL SUM, WHICH IS A PART OF THE OUTPUT OF ADJOINT INITIAL
C      VALUE PROBLEM (IN CASE ISW=0) OR RECORDS RESULT VALUES OF THE
C      FINAL INITIAL VALUE PROBLEM (IN CASE ISW=1).
C      300 IF(ISW)301,301,305
C      ADJOINT PROBLEM
C      301 CALL FCT(X,R)
C      GU=0.00
C      DGU=0.00
C      DO 302 L=1,NDIM
C      GU=GU+Y(L)*R(L)
C      302 DGU=DGU+DERY(L)*R(L)
C      CALL DFCT(X,R)
C      DO 303 L=1,NDIM
C      303 DGU=DGU+Y(L)*R(L)
C      SUM=SUM+.500*H*(GL+GU)+.16666666666666700*H*(DGL-DGU)
C      GL=GU
C      DGL=DGU
C      304 IF(ISW)116,422,618
C      GIVEN PROBLEM
C      305 CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)
C      IF(PRMT(5))117,304,117
C      POSSIBLE BREAK-POINT FOR LINKAGE
C      C
C      THE FOLLOWING PART OF SUBROUTINE DLBVP SOLVES IN CASE ISW=0 THE
C      ADJOINT INITIAL VALUE PROBLEM, IT COMPUTES INTEGRAL SUM AND
C      THE VECTOR Y OF DEPENDENT VARIABLES AT THE LOWER BOUND PRMT(1).
C      IN CASE ISW=1 IT SOLVES FINALLY GENERATED INITIAL VALUE PROBLEM.
C      400 N=1
C      XST=X
C      IHLF=0
C      DO 401 I=1,NDIM
C      AUX(16,I)=0.00
C      AUX(1,I)=Y(II)

```

```

401 AUX(8, I)=DERY(I)
ISW1=1
GOTO 500
C
402 X=X+H
DO 403 I=1,NDIM
403 AUX(2, I)=Y(I)
C
C INCREMENT H IS TESTED BY MEANS OF BISECTION
404 IHLF=IHLF+1
X=X-H
DO 405 I=1,NDIM
405 AUX(4, I)=AUX(2, I)
H=.500*H
N=1
ISW1=2
GOTO 500
C
406 X=X+H
ISW2=4
GOTO 200
407 N=2
DO 408 I=1,NDIM
AUX(2, I)=Y(I)
408 AUX(9, I)=DERY(I)
ISW1=3
GOTO 500
C
C TEST ON SATISFACTORY ACCURACY
409 DO 414 I=1,NDIM
Z=DABS(Y(I))
IF(Z-L.D0)410,411,411
410 Z=1.00
411 DELT=.0666666666666666700*DABS(Y(I)-AUX(4, I))
IF(ISW)413,413,412
412 DELT=AUX(15, I)*DELT
413 IF(DELT-Z*PRMT(4))414,414,429
414 CONTINUE
C
C SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS
X=X+H
ISW2=5
GOTO 200
415 DO 416 I=1,NDIM
AUX(3, I)=Y(I)
416 AUX(10, I)=DERY(I)
N=3
ISW1=4
GOTO 500
C
417 N=1
X=X+H
ISW2=6
GOTO 200
418 X=X+H
DO 419 I=1,NDIM
AUX(11, I)=DERY(I)
419 OY(I)=AUX(1, I)+H*(-.37500*AUX(8, I)+.7916666666666666700*AUX(9, I)
I-.2083333333333333300*AUX(10, I)+.0416666666666666700*DERY(I))
420 X=X+H
N=N+1
ISW2=11
GOTO 200
421 ISW3=0
GOTO 300
422 IF(N-4)423,600,600
423 DO 424 I=1,NDIM
AUX(N, I)=Y(I)
424 AUX(N+7, I)=DERY(I)
IF(N-3)425,427,600
C
425 DO 426 I=1,NDIM
DELT=AUX(9, I)+AUX(9, I)
DELT=DELT+DELT
426 Y(I)=AUX(1, I)+.3333333333333333300*H*(AUX(8, I)+DELT+AUX(10, I))
GOTO 420
C
427 DO 428 I=1,NDIM
DELT=AUX(9, I)+AUX(10, I)
DELT=DELT+DELT+DELT
428 Y(I)=AUX(1, I)+.37500*H*(AUX(8, I)+DELT+AUX(11, I))
GOTO 420
C
C NO SATISFACTORY ACCURACY. H MUST BE HALVED.
429 IF(IHLF-10)404,430,430
C
C NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.
430 IHLF=11
X=X+H
IF(ISW)105,105,114
C
C THIS PART OF LINEAR INITIAL VALUE PROBLEM COMPUTES
STARTING VALUES BY MEANS OF RUNGE-KUTTA METHOD.
500 Z=X
DO 501 I=1,NDIM
X=H*AUX(N+7, I)
AUX(5, I)=X
501 Y(I)=AUX(N, I)+.400*X
X=Z+.400*H
ISW2=1
GOTO 200
502 DO 503 I=1,NDIM
X=H*DERY(I)
AUX(6, I)=X
503 Y(I)=AUX(N, I)+.2969776092477536000*AUX(5, I)+.1587596449710358300*DLB
V4570
C
X=Z+.4557372542187894300*H
ISW2=2
GOTO 200
504 DO 505 I=1,NDIM
X=H*DERY(I)
AUX(7, I)=X
505 Y(I)=AUX(N, I)+.2181003882259204700*AUX(5, I)-3.050965148692930800*
LAUX(6, I)+3.8328647604670103000*X
X=Z+H
ISW2=3
GOTO 200
506 DO 507 I=1,NDIM
507 OY(I)=AUX(N, I)+.17476028226269037000*AUX(5, I)-.5514806628787329400*
LAUX(6, I)+1.2055355993965233000*AUX(7, I)+.1711847812195190300*
2H*DERY(I)
X=Z
GOTO(402,406,409,417),ISW1
C
C POSSIBLE BREAK-POINT FOR LINKAGE
C
C STARTING VALUES ARE COMPUTED.
DLB3520
DLB3530
DLB3540
DLB3550
DLB3560
DLB3570
DLB3580
DLB3590
DLB3600
DLB3610
DLB3620
DLB3630
DLB3640
DLB3650
DLB3660
DLB3670
DLB3680
DLB3690
DLB3700
DLB3710
DLB3720
DLB3730
DLB3740
DLB3750
DLB3760
DLB3770
DLB3780
DLB3790
DLB3800
DLB3810
DLB3820
DLB3830
DLB3840
DLB3850
DLB3860
DLB3870
DLB3880
DLB3890
DLB3900
DLB3910
DLB3920
DLB3930
DLB3940
DLB3950
DLB3960
DLB3970
DLB3980
DLB3990
DLB4000
DLB4010
DLB4020
DLB4030
DLB4040
DLB4050
DLB4060
DLB4070
DLB4080
DLB4090
DLB4100
DLB4110
DLB4120
DLB4130
DLB4140
DLB4150
DLB4160
DLB4170
DLB4180
DLB4190
DLB4200
DLB4210
DLB4220
DLB4230
DLB4240
DLB4250
DLB4260
DLB4270
DLB4280
DLB4290
DLB4300
DLB4310
DLB4320
DLB4330
DLB4340
DLB4350
DLB4360
DLB4370
DLB4380
DLB4390
DLB4400
DLB4410
DLB4420
DLB4430
DLB4440
DLB4450
DLB4460
DLB4470
DLB4480
DLB4490
DLB4500
DLB4510
DLB4520
DLB4530
DLB4540
DLB4550
DLB4560
DLB4570
DLB4580
DLB4590
DLB4600
DLB4610
DLB4620
DLB4630
DLB4640
DLB4650
DLB4660
DLB4670
DLB4680
DLB4690
DLB4700
DLB4710
DLB4720
DLB4730
DLB4740
DLB4750
DLB4760
DLB4770
DLB4780
DLB4790
DLB4800
C
C NOW START HAMMING'S MODIFIED PREDICTOR-CORRECTOR METHOD.
600 ISTEP=3
601 IF(N-8)604,602,604
C
C N=8 CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS
602 DO 603 N=2,7
DO 603 I=1,NDIM
AUX(N-1, I)=AUX(N, I)
603 AUX(N+6, I)=AUX(N+7, I)
N=7
C
C N LESS THAN 8 CAUSES N+1 TO GET N
604 N=N+1
C
C COMPUTATION OF NEXT VECTOR Y
DO 605 I=1,NDIM
AUX(N-1, I)=Y(I)
605 AUX(N+6, I)=DERY(I)
X=X+H
606 ISTEP=ISTEP+1
DO 607 I=1,NDIM
ODELT=AUX(N-4, I)+1.33333333333333300*H*(AUX(N+6, I)+AUX(N+6, I)-
LAUX(N+5, I)+AUX(N+4, I)+AUX(N+4, I))
Y(I)=DELT-.925619834710743000*AUX(16, I)
607 AUX(16, I)=DELT
C
C PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX, MODIFIED PREDICTOR
IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.
C
ISW2=7
GOTO 200
C
C DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY.
608 DO 609 I=1,NDIM
ODELT=.12500*(9.000*AUX(N-1, I)-AUX(N-3, I)+3.000*(DERY(I)+AUX(N+6, I)
I+AUX(N+6, I)-AUX(N+5, I)))
AUX(16, I)=AUX(16, I)-DELT
609 Y(I)=DELT+.0743801652892562000*AUX(16, I)
C
C TEST WHETHER H MUST BE HALVED OR DOUBLED
DELT=.00
DO 616 I=1,NDIM
Z=DABS(Y(I))
IF(Z-L.D0)610,611,611
610 Z=1.00
611 Z=DABS(AUX(16, I))/Z
IF(ISW)613,613,612
612 Z=AUX(15, I)*Z
613 IF(Z-PRMT(4))614,614,628
614 IF(DELT-Z)615,616,616
615 DELT=Z
616 CONTINUE
C
C H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.
ISW2=8
GOTO 200
617 ISW3=1
GOTO 300
618 IF(H*X-XEND)619,621,621
619 IF(DABS(X-XEND)-.100*DABS(H))621,620,620
620 IF(DELT-.0200*PRMT(4))622,622,601
621 IF(ISW)105,105,117
C
C H COULD BE DOUBLED IF ALL NECESSARY PRECEEDING VALUES ARE
AVAILABLE.
622 IF(IHLF)601,601,623
623 IF(N-7)601,624,624
624 IF(ISTEP-4)601,625,625
625 IMOD=ISTEP/2
IF(ISTEP-IMOD-IMOD)601,626,601
626 H=H*H
IHLF=IHLF-1
ISTEP=0
DO 627 I=1,NDIM
AUX(N-1, I)=AUX(N-2, I)
AUX(N-2, I)=AUX(N-4, I)
AUX(N-3, I)=AUX(N-6, I)
AUX(N+6, I)=AUX(N+5, I)
AUX(N+5, I)=AUX(N+3, I)
AUX(N+4, I)=AUX(N+1, I)
DELT=AUX(N+6, I)+AUX(N+5, I)
DELT=DELT+DELT+DELT
627 OUX(16, I)=8.962962962963000*(Y(I)-AUX(N-3, I))
I-3.361111111111111000*H*(DERY(I)+DELT+AUX(N+4, I))
GOTO 601
C
C H MUST BE HALVED
628 IHLF=IHLF+1
IF(IHLF-10)630,630,629
629 IF(ISW)105,105,114
630 H=.500*H
ISTEP=0
DO 631 I=1,NDIM
OY(I)=.3906250-2*(8.01*AUX(N-1, I)+135.00*AUX(N-2, I)+4.01*AUX(N-3, I)
I+AUX(N-4, I))-117187500*(AUX(N+6, I)-4.00*AUX(N+5, I)-AUX(N+4, I))*H
OAX(N-4, I)=.3906250-2*(12.00*AUX(N-1, I)+135.00*AUX(N-2, I)+
1108.00*AUX(N-3, I)+AUX(N-4, I))-0.23437500*(AUX(N+6, I)+
218.00*AUX(N+5, I)-9.00*AUX(N+4, I))*H
AUX(N-3, I)=AUX(N-2, I)
AUX(N+4, I)=AUX(N+5, I)
631 AUX(N+4, I)=AUX(N+5, I)
DELT=X-H
X=DELT-(H*H)
ISW2=9
GOTO 200
632 DO 633 I=1,NDIM
AUX(N-2, I)=Y(I)
AUX(N+5, I)=DERY(I)
633 Y(I)=AUX(N-4, I)
X=X-(H*H)
ISW2=10
GOTO 200
634 X=DELT
DO 635 I=1,NDIM
DEL=AUX(N+5, I)+AUX(N+4, I)
DELT=DELT+DELT+DELT
OAX(16, I)=8.962962962963000*(AUX(N-1, I)-Y(I))
I-3.361111111111111000*H*(AUX(N+6, I)+DELT+DERY(I))
635 AUX(N+3, I)=DERY(I)
GOTO 606
C
C END OF INITIAL VALUE PROBLEM
END
DLB4810
DLB4820
DLB4830
DLB4840
DLB4850
DLB4860
DLB4870
DLB4880
DLB4890
DLB4900
DLB4910
DLB4920
DLB4930
DLB4940
DLB4950
DLB4960
DLB4970
DLB4980
DLB4990
DLB5000
DLB5010
DLB5020
DLB5030
DLB5040
DLB5050
DLB5060
DLB5070
DLB5080
DLB5090
DLB5100
DLB5110
DLB5120
DLB5130
DLB5140
DLB5150
DLB5160
DLB5170
DLB5180
DLB5190
DLB5200
DLB5210
DLB5220
DLB5230
DLB5240
DLB5250
DLB5260
DLB5270
DLB5280
DLB5290
DLB5300
DLB5310
DLB5320
DLB5330
DLB5340
DLB5350
DLB5360
DLB5370
DLB5380
DLB5390
DLB5400
DLB5410
DLB5420
DLB5430
DLB5440
DLB5450
DLB5460
DLB5470
DLB5480
DLB5490
DLB5500
DLB5510
DLB5520
DLB5530
DLB5540
DLB5550
DLB5560
DLB5570
DLB5580
DLB5590
DLB5600
DLB5610
DLB5620
DLB5630
DLB5640
DLB5650
DLB5660
DLB5670
DLB5680
DLB5690
DLB5700
DLB5710
DLB5720
DLB5730
DLB5740
DLB5750
DLB5760
DLB5770
DLB5780
DLB5790
DLB5800
DLB5810
DLB5820
DLB5830
DLB5840
DLB5850
DLB5860
DLB5870
DLB5880
DLB5890
DLB5900
DLB5910
DLB5920
DLB5930
DLB5940
DLB5950
DLB5960
DLB5970
DLB5980
DLB5990
DLB6000

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Special Functions.

Subroutine GMMMA

This subroutine computes the value of the gamma function for a given argument x . The calculation of the gamma function, $\Gamma(x)$ is defined for $x > 0$ by:

$$\Gamma(x) = \int_0^{\infty} t^{x-1} \cdot e^{-t} dt \quad (1)$$

This function satisfies the recurrence relation:

$$\Gamma(x) = (x-1) \cdot \Gamma(x-1) \quad (2)$$

which defines $\Gamma(x)$ for any x not a negative integer.

Note that when x is a positive integer, $\Gamma(x) = (x-1)!$

To compute $\Gamma(x)$ for $x > 1$, apply the recurrence (2), r times until $1 < x-r = y \leq 2$. Thus, for $x > 1$:

$$\Gamma(x) = (x-1)(x-2) \dots (x-r) \Gamma(y) \quad (3)$$

$\Gamma(y)$ is computed from the following formula:

$$\begin{aligned} \Gamma(y) \approx & 1 - 0.57710166(y-1) + 0.98585399(y-1)^2 \\ & - 0.87642182(y-1)^3 + 0.83282120(y-1)^4 \\ & - 0.56847290(y-1)^5 + 0.25482049(y-1)^6 \\ & - 0.05149930(y-1)^7 \end{aligned} \quad (4)$$

For $x < 1$, the recurrence (2) is taken in the direction of decreasing n , giving:

$$\Gamma(x) = \frac{\Gamma(y)}{x(x+1)(x+2) \dots (x+r-1)} \quad (5)$$

where $1 < x+r = y \leq 2$.

As before, $\Gamma(y)$ is computed using equation (4).

```

C .....
C SUBROUTINE GMMMA
C PURPOSE
C COMPUTES THE GAMMA FUNCTION FOR A GIVEN ARGUMENT
C USAGE
C CALL GMMMA(XX,GX,IER)
C DESCRIPTION OF PARAMETERS
C XX -THE ARGUMENT FOR THE GAMMA FUNCTION
C GX -THE RESULTANT GAMMA FUNCTION VALUE
C IER-RESULTANT ERROR CODE WHERE
C IER=0 NO ERROR
C IER=1 XX IS WITHIN .000001 OF BEING A NEGATIVE INTEGER
C IER=2 XX GT 57, OVERFLOW, GX SET TO 1.0E75
C REMARKS
C NONE
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NONE
C METHOD
C THE RECURSION RELATION AND POLYNOMIAL APPROXIMATION
C BY C.HASTINGS,JR., 'APPROXIMATIONS FOR DIGITAL COMPUTERS',
C PRINCETON UNIVERSITY PRESS, 1955
C .....
C SUBROUTINE GMMMA(XX,GX,IER)
C IF(XX-57.16,6,4
C 4 IER=2
C GX=1.E75
C RETURN
C 6 X=XX
C ERR=1.0E-6
C IER=0
C GX=1.0
C IF(X-2.0)50,50,15
C 10 IF(X-2.0)110,110,15
C 15 X=X-1.0
C GX=GX*X
C GO TO 10
C 50 IF(X-1.0)60,120,110
C
C SEE IF X IS NEAR NEGATIVE INTEGER OR ZERO
C
C 60 IF(X-ERR)62,62,80
C 62 Y=FLD(1/(INT(X))-X
C IF(ABS(Y)-ERR)130,130,64
C 64 IF(1.0-Y-ERR)130,130,70
C
C X NOT NEAR A NEGATIVE INTEGER OR ZERO
C
C 70 IF(X-1.0)80,80,110
C 80 GX=GX/X
C X=X+1.0
C GO TO 70
C 110 Y=X-1.0
C CY=1.0+Y*(1-0.5771017+Y*(1+0.9858540+Y*(-0.8764218+Y*(1+0.8328212+
C 1Y*(-0.5684729+Y*(1+0.2548205+Y*(-0.0514993))))))
C GX=GX*CY
C 120 RETURN
C 130 IER=1
C RETURN
C END
C .....
C GMMH 10
C GMMH 20
C GMMH 30
C GMMH 40
C GMMH 50
C GMMH 60
C GMMH 70
C GMMH 80
C GMMH 90
C GMMH 100
C GMMH 110
C GMMH 120
C GMMH 130
C GMMH 140
C GMMH 150
C GMMH 160
C GMMH 170
C GMMH 180
C GMMH 190
C GMMH 200
C GMMH 210
C GMMH 220
C GMMH 230
C GMMH 240
C GMMH 250
C GMMH 260
C GMMH 270
C GMMH 280
C GMMH 290
C GMMH 300
C GMMH 310
C GMMH 320
C GMMH 330
C GMMH 340
C GMMH 350
C GMMH 360
C GMMH 370
C GMMH 380
C GMMH 390
C GMMH 400
C GMMH 410
C GMMH 420
C GMMH 430
C GMMH 440
C GMMH 450
C GMMH 460
C GMMH 470
C GMMH 480
C GMMH 490
C GMMH 500
C GMMH 510
C GMMH 520
C GMMH 530
C GMMH 540
C GMMH 550
C GMMH 560
C GMMH 570
C GMMH 580
C GMMH 590
C GMMH 600
C GMMH 610
C GMMH 620
C GMMH 630
C GMMH 640
C GMMH 650
C GMMH 660
C GMMH 670
C GMMH 680
C GMMH 690

```

Subroutine DLGAM

This subroutine computes the double-precision natural logarithm of the gamma function of a given double-precision argument, x, where $10^{-9} < x < 10^{70}$. The Euler-McLaurin expansion, to the seventh derivative term, is used. For $x > 0$:

$$\begin{aligned} \log \Gamma(x) &\approx (x - 1/2) \log x \\ &+ 1/2 \log 2\pi - x + 1/12x - 1/360x^3 \\ &+ 1/1260x^5 - 1/1680x^7 \end{aligned} \tag{1}$$

This expression is very accurate for $x > 18$. If $x \leq 18$, x is replaced by $z = k + x$, where k is an integer such that $z > 18$. $\log \Gamma(z)$ is then evaluated by (1), and $\log x + \log(x+1) + \dots + \log(x+k-1)$ is subtracted to obtain the desired result.

If x is between 10^{10} and 10^{70} , terms of lowest order in (1) are neglected, and $\log \Gamma(x)$ is computed as:

$$\log \Gamma(x) = x (\log(x) - 1) \tag{2}$$

Subroutine DLGAM is available in a double-precision format only. If the single-precision value of the log gamma function of a given single-precision argument is desired, subroutine GMMMA should be used along with the FORTRAN-supplied natural logarithm function.

For reference see M. Abramowitz and I. A. Stegun, Handbook of Mathematical Functions. U. S. Department of Commerce, National Bureau of Standards Applied Mathematics Series, 1966, equation 6.1.41.

```
C      DLGA 10
C      DLGA 20
C      DLGA 30
C      DLGA 40
C      DLGA 50
C      DLGA 60
C      DLGA 70
C      DLGA 80
C      DLGA 90
C      DLGA 100
C      DLGA 110
C      DLGA 120
C      DLGA 130
C      DLGA 140
C      DLGA 150
C      DLGA 160
C      DLGA 170
C      DLGA 180
C      DLGA 190
C      DLGA 200
C      DLGA 210
C      DLGA 220
C      DLGA 230
C      DLGA 240
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C      DLGA 260
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C      DLGA 280
C      DLGA 290
C      DLGA 300
C      DLGA 310
C      DLGA 320
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C      DLGA 340
C      DLGA 350
C      DLGA 360
C      DLGA 370
C      DLGA 380
C      DLGA 390
C      DLGA 400
C      DLGA 410
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C      DLGA 430
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C      DLGA 470
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C      DLGA 510
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C      DLGA 600
C      DLGA 610
C      DLGA 620
C      DLGA 630
C      DLGA 640
C      DLGA 650
C      DLGA 660
C      DLGA 670
C      DLGA 680
C      DLGA 690
C      DLGA 700
C      DLGA 710
C      DLGA 720
C      DLGA 730
C      DLGA 740
C      DLGA 750
C      DLGA 760
C      DLGA 770
```

```
-----
SUBROUTINE DLGAM
PURPOSE
  COMPUTES THE DOUBLE PRECISION NATURAL LOGARITHM OF THE
  GAMMA FUNCTION OF A GIVEN DOUBLE PRECISION ARGUMENT.
USAGE
  CALL DLGAM(XY,DLNG,IER)
DESCRIPTION OF PARAMETERS
  XX  - THE DOUBLE PRECISION ARGUMENT FOR THE LOG GAMMA
        FUNCTION.
  DLNG - THE RESULTANT DOUBLE PRECISION LOG GAMMA FUNCTION
        VALUE.
  IER  - RESULTANT ERROR CODE WHERE
        IER= 0----NO ERROR.
        IER=-1----XX IS WITHIN 10**(-9) OF BEING ZERO OR XX
        IS NEGATIVE. DLNG IS SET TO -1.0D75.
        IER=+1----XX IS GREATER THAN 10**70. DLNG IS SET TO
        +1.0D75.
REMARKS
  NONE
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
METHOD
  THE EULER-MCLAURIN EXPANSION TO THE SEVENTH DERIVATIVE TERM
  IS USED, AS GIVEN BY M. ABRAMOWITZ AND I.A. STEGUN,
  'HANDBOOK OF MATHEMATICAL FUNCTIONS', U. S. DEPARTMENT OF
  COMMERCE, NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS
  SERIES, 1966, EQUATION 6.1.41.
-----
SUBROUTINE DLGAM(XY,DLNG,IER)
DOUBLE PRECISION XY,XZ,TERM,ZZ,DLNG
IER=0
ZZ=XY
1 IF (XX-1.D70) 3,9,0
SEE IF XX IS NEAR ZERO OR NEGATIVE
2 IF (XX-1.D-9) 3,3,4
3 IER=-1
DLNG=-1.D75
GO TO 10
XX GREATER THAN ZERO AND LESS THAN OR EQUAL TO 1.D+10
4 TERM=1.00
5 IF (ZZ-18.D0) 6,6,7
6 TERM=TERM*77
ZZ=ZZ+1.00
GO TO 5
7 R2Z=1.00/ZZ**7
DLNG = (Z**(-0.500)*DLNG(ZZ)-ZZ *C.9169385332046727 -DLNG(TERM)+
1(1.00/ZZ)*(.833333333333330-1 -(R2Z*(.277777777777777-2 *(R2Z*
2(.7936507936507936D-3 -(R2Z*(.5952380952380952D-3))))))
GO TO 10
XX GREATER THAN 1.D+10 AND LESS THAN 1.D+70
8 DLNG=ZZ*(DLNG(ZZ)-1.00)
GO TO 10
XX GREATER THAN OR EQUAL TO 1.D+70
9 IER=+1
DLNG=1.975
10 RETURN
END
```

Subroutine BESJ

This subroutine computes the J Bessel function for a given argument and integer order by using the recurrence relationship:

$$F_{n+1}(x) + F_{n-1}(x) = \left(\frac{2n}{x}\right) F_n(x) \quad (1)$$

The desired Bessel function is:

$$J_n(x) = \frac{F_n(x)}{\alpha} \quad (2)$$

where:

$$\alpha = F_0(x) + 2 \sum_{m=1}^{M-2} F_{2m}(x) \quad (3)$$

M is initialized at M_0 .

M_0 is the greater of M_A and M_B where;

$$M_A = \begin{cases} [x+6] & \text{if } x < 5 \\ [1.4x+60/x] & \text{if } x \geq 5 \end{cases}$$

$$M_B = [n+x/4+2]$$

$F_{M-2}, F_{M-3}, \dots, F_2, F_1, F_0$ is evaluated using equation (1) with $F_M = 0$ and $F_{M-1} = 10^{-30}$. Values of α and $J_n(x)$ are then computed using equations (3) and (2) respectively.

The computation is repeated for $M+3$.

The values of $J_n(x)$ for M and $M+3$ are compared:

$$\text{If } \left| J_n(x)_M - J_n(x)_{M+3} \right| \leq \delta \left| J_n(x)_{M+3} \right|$$

this value is accepted as $J_n(x)$; if not, the computation is repeated by adding 3 to M and using this as a new value for M. If M reaches M_{MAX} before the desired accuracy is obtained, execution is terminated. M_{MAX} is defined as:

$$M_{MAX} = \begin{cases} \left[20 + 10x - \frac{x^2}{3} \right] & \text{for } x \leq 15 \\ [90 + x/2] & \text{for } x > 15 \end{cases} \quad (4)$$

```

C ..... BESJ 10
C ..... BESJ 20
C ..... BESJ 30
C ..... BESJ 40
C ..... BESJ 50
C ..... BESJ 60
C ..... BESJ 70
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C ..... BESJ 140
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C ..... BESJ 670
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C ..... BESJ 790
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C ..... BESJ 820
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C ..... BESJ 850
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C ..... BESJ 880
C ..... BESJ 890
C ..... BESJ 900
C ..... BESJ 910
C ..... BESJ 920
C ..... BESJ 930
C ..... BESJ 940
C ..... BESJ 950
C ..... BESJ 960
C ..... BESJ 970
C ..... BESJ 980
C ..... BESJ 990
C ..... BESJ1000
C ..... BESJ1010
C ..... BESJ1020
C ..... BESJ1030
C ..... BESJ1040
C ..... BESJ1050
SUBROUTINE BESJ
PURPOSE
  COMPUTE THE J BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER
USAGE
  CALL BESJ(X,N,BJ,D,IER)
DESCRIPTION OF PARAMETERS
  X -THE ARGUMENT OF THE J BESSEL FUNCTION DESIRED
  N -THE ORDER OF THE J BESSEL FUNCTION DESIRED
  BJ -THE RESULTANT J BESSEL FUNCTION
  D -REQUIRED ACCURACY
  IER-RESULTANT ERROR CODE WHERE
      IER=0 NO ERROR
      IER=1 N IS NEGATIVE
      IER=2 X IS NEGATIVE OR ZERO
      IER=3 REQUIRED ACCURACY NOT OBTAINED
      IER=4 RANGE OF N COMPARED TO X NOT CORRECT (SEE REMARKS)
REMARKS
  N MUST BE GREATER THAN OR EQUAL TO ZERO, BUT IT MUST BE
  LESS THAN
  20*10**X-X** 2/3 FOR X LESS THAN OR EQUAL TO 15
  90+X/2 FOR X GREATER THAN 15
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
  NONE
METHOD
  RECURRENCE RELATION TECHNIQUE DESCRIBED BY H. GOLDSTEIN AND
  R.M. THALER, 'RECURRENCE TECHNIQUES FOR THE CALCULATION OF
  BESSEL FUNCTIONS', M.T.A.C., V.13, PP.102-108 AND I.A. STEGUN
  AND M. ABRAMOWITZ, 'GENERATION OF BESSEL FUNCTIONS ON HIGH
  SPEED COMPUTERS', M.T.A.C., V.11, 1957, PP.255-257
SUBROUTINE BESJ(X,N,BJ,D,IER)
  BJ=.0
  IF(N)10,20,20
10 IER=1
  RETURN
20 IF(X)130,30,31
30 IER=2
  RETURN
31 IF(X-15.)32,32,34
32 NTEST=20.*10.**X-X** 2/3
  GO TO 36
34 NTEST=90.+X/2.
36 IF(N-NTEST)40,38,38
38 IER=4
  RETURN
40 IER=0
  N1=N-1
  BPREV=.0
  COMPUTE STARTING VALUE OF M
  IF(X-5.)150,60,60
50 MA=X+6.
  GO TO 70
60 MA=L.4*X+60./X
70 MB=N+IF(X)4+2
  NZERO=MAX0(MA,MB)
  SET UPPER LIMIT OF M
  MMAX=NTEST
100 DO 190 M=NZERO,MMAX,3
  SET F(M),F(M-1)
  FM1=1.0E-28
  FM=.0
  ALPHA=.0
  IF(M-(M/2)*2)120,110,120
110 JT=-1
  GO TO 130
120 JT=1
130 M2=M-2
  DO 160 K=1,M2
  MK=M-K
  BMK=2.*FLOAT(MK)*FM1/X-FM
  FM=FM1
  FM1=BMK
  IF(MK-N)1150,140,150
140 BJ=BMK
150 JT=-JT
  S=1+JT
160 ALPHA=ALPHA+BMK*S
  BMK=2.*FM1/X-FM
  IF(N)180,170,180
170 BJ=BMK
180 ALPHA=ALPHA+BMK
  BJ=BJ/ALPHA
  IF(ABS(BJ-BPREV))-ABS(D*BJ)1200,200,190
190 BPREV=BJ
  IER=3
200 RETURN
  END

```

Subroutine BESY

This subroutine computes the Y Bessel function for a given argument x and order n. The recurrence relation:

$$Y_{n+1}(x) = \left(\frac{2n}{x}\right) \cdot Y_n(x) - Y_{n-1}(x) \quad (1)$$

is used for this evaluation.

For $x > 4$

$$Y_0(x) = \sqrt{\frac{2}{\pi x}} \left(P_0(x) \sin\left(x - \frac{\pi}{4}\right) + Q_0(x) \cos\left(x - \frac{\pi}{4}\right) \right) \quad (2)$$

$$Y_1(x) = \sqrt{\frac{2}{\pi x}} \left(-P_1(x) \cos\left(x - \frac{\pi}{4}\right) + Q_1(x) \sin\left(x - \frac{\pi}{4}\right) \right) \quad (3)$$

$P_0(x)$, $Q_0(x)$, $P_1(x)$, and $Q_1(x)$ are:

$$\frac{1}{\sqrt{2\pi}} P_0\left(\frac{4}{t}\right) = 0.3989422793 - 0.0017530620t^2 + 0.0001734300t^4 - 0.0000487613t^6 + 0.0000173565t^8 - 0.0000037043t^{10} \quad (4)$$

$$t \frac{1}{\sqrt{2\pi}} Q_0\left(\frac{4}{t}\right) = -0.0124669441 + 0.0004564324t^2 - 0.0000869791t^4 + 0.0000342468t^6 - 0.0000142078t^8 + 0.0000032312t^{10} \quad (5)$$

$$\sqrt{2\pi} P_1\left(\frac{4}{t}\right) = 0.3989422819 + 0.0029218256t^2 - 0.0002232030t^4 + 0.0000580759t^6 - 0.0000200920t^8 + 0.0000042414t^{10} \quad (6)$$

$$t \frac{1}{\sqrt{2\pi}} Q_1\left(\frac{4}{t}\right) = 0.0374008364 - 0.0006390400t^2 - 0.0001064741t^4 - 0.0000398708t^6 - 0.0000162200t^8 - 0.0000042414t^{10} \quad (7)$$

where $t = \frac{4}{x}$

For $x \leq 4$

$$Y_0(x) = \frac{2}{\pi} \sum_{m=0}^{15} (-1)^m \left(\frac{x}{2}\right)^{2m} \frac{1}{(m!)^2} \left[\log \frac{x}{2} + \gamma - H_m \right] \quad (8)$$

where:

$$H_m = \begin{cases} \sum_{r=1}^m \frac{1}{r} & \text{if } m \geq 1 \\ 0 & \text{if } m = 0 \end{cases} \quad (9)$$

and $\gamma = \text{Euler's constant} = 0.5772156649$

$$Y_1(x) = -\frac{2}{\pi x} + \frac{2}{\pi} \sum_{m=1}^{16} (-1)^{m+1} \left(\frac{x}{2}\right)^{2m-1} \frac{1}{m!(m-1)!} \cdot \left[\log \frac{x}{2} + \gamma - H_m + \frac{1}{2m} \right] \quad (10)$$

```

C ..... BESY 10
C ..... BESY 20
C ..... BESY 30
C ..... BESY 40
C ..... BESY 50
C ..... BESY 60
C ..... BESY 70
C ..... BESY 80
C ..... BESY 90
C ..... BESY 100
C ..... BESY 110
C ..... BESY 120
C ..... BESY 130
C ..... BESY 140
C ..... BESY 150
C ..... BESY 160
C ..... BESY 170
C ..... BESY 180
C ..... BESY 190
C ..... BESY 200
C ..... BESY 210
C ..... BESY 220
C ..... BESY 230
C ..... BESY 240
C ..... BESY 250
C ..... BESY 260
C ..... BESY 270
C ..... BESY 280
C ..... BESY 290
C ..... BESY 300
C ..... BESY 310
C ..... BESY 320
C ..... BESY 330
C ..... BESY 340
C ..... BESY 350
C ..... BESY 360
C ..... BESY 370
C ..... BESY 380
C ..... BESY 390
C .....

```

SUBROUTINE BESY
 PURPOSE
 COMPUTE THE Y-BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER
 USAGE
 CALL BESY(X,N,BY,IER)
 DESCRIPTION OF PARAMETERS
 X - THE ARGUMENT OF THE Y BESSEL FUNCTION DESIRED
 N - THE ORDER OF THE Y BESSEL FUNCTION DESIRED
 BY - THE RESULTANT Y BESSEL FUNCTION
 IER - RESULTANT ERROR CODE WHERE
 IER=0 NO ERROR
 IER=1 N IS NEGATIVE
 IER=2 X IS NEGATIVE OR ZERO
 IER=3 BY HAS EXCEEDED MAGNITUDE OF 10**70
 REMARKS
 VERY SMALL VALUES OF X MAY CAUSE THE RANGE OF THE LIBRARY
 FUNCTION ALLOC TO BE EXCEEDED
 X MUST BE GREATER THAN ZERO
 N MUST BE GREATER THAN OR EQUAL TO ZERO
 SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
 NONE
 METHOD
 RECURRENCE RELATION AND POLYNOMIAL APPROXIMATION TECHNIQUE
 AS DESCRIBED BY A.J.M.HITCHCOCK, "POLYNOMIAL APPROXIMATIONS
 TO BESSEL FUNCTIONS OF ORDER ZERO AND ONE AND TO RELATED
 FUNCTIONS", M.T.A.C., V.11,1957,PP.86-88, AND G.N. WATSON,
 "A TREATISE ON THE THEORY OF BESSEL FUNCTIONS", CAMBRIDGE
 UNIVERSITY PRESS, 1958, P. 62


```

C
C SUBROUTINE BESY(X,N,BY,IER)
C CHECK FOR ERRORS IN N AND X
C IF(N)180,10,10
C IF(X)190,190,20
C BRANCH IF X LESS THAN OR EQUAL 4
C 20 IF(X-4.0)40,40,30
C COMPUTE Y0 AND Y1 FOR X GREATER THAN 4
C
C 30 T1=4.0/X
C T2=T1*1
C P0=(((1-.000037043)*T2+.000173565)*T2-.0000487613)*T2
C P1=(((1+.00017343)*T2-.001753062)*T2+.3989423
C Q0=(((1.0000032312*T2-.0000142078)*T2+.0000342468)*T2
C Q1=((-0.0000869791)*T2+.0004564324)*T2-.01246694
C P1=(((1.0000042414)*T2-.0000200920)*T2+.0000580759)*T2
C Q1=((-0.000223203)*T2+.002921826)*T2+.3989423
C Q1=(((1-.0000036594)*T2+.0001622)*T2-.0000398708)*T2
C P1=(((1+.0001064741)*T2-.0006390400)*T2+.03740084
C A=2.0/SQRT(X)
C B=A*T1
C C=X-.7853982
C Y0=A*P0+Q0*(C)+B*Q0*COS(C)
C Y1=-A*P1*Q0*(C)+B*Q1*P1*(C)
C GO TO 90
C
C COMPUTE Y0 AND Y1 FOR X LESS THAN OR EQUAL TO 4
C
C 40 XX=X/2.
C X2=XX*XX
C T=ALOG(XX)+.5772157
C SUM=0.
C TERM=T
C Y0=T
C DO 70 L=1,15
C IF(L-1)50,60,50
C SUM=SUM+1./FLOAT(L-1)
C 60 FL=L
C TS=T-SUM
C TERM=(TERM*(-X2)/FL**2)*(1.-L./((FL*TS)))
C 70 Y0=Y0+TERM
C TERM = XX*(T-.5)
C SUM=0.
C Y1=TERM
C DO 80 L=2,16
C SUM=SUM+1./FLOAT(L-1)
C FL=L
C FL1=FL-1.
C TS=T-SUM
C TERM=(TERM*(-X2)/(FL1*FL1))*((TS-.5/FL1)/(TS+.5/FL1))
C 80 Y1=Y1+TERM
C P12=-.6366198
C Y0=P12*Y0
C Y1=-P12/X*Y1+Y1
C
C CHECK IF ONLY Y0 OR Y1 IS DESIRED
C
C 90 IF(N-1)100,100,130
C
C RETURN EITHER Y0 OR Y1 AS REQUIRED
C
C 100 IF(N)110,120,110
C 110 BY=Y1
C GO TO 170
C 120 BY=Y0
C GO TO 170
C
C PERFORM RECURRENCE OPERATIONS TO FIND YN(X)
C
C 130 YA=Y0
C YB=Y1
C K=1
C 140 T=FLOAT(2*K)/X
C YC=T*YB-YA
C IF(ABS(YC)-1.0E70)145,145,141
C 141 IER=3
C RETURN
C 145 K=K+1
C IF(K-N)150,160,150
C 150 YA=YB
C YB=YC
C GO TO 140
C 160 BY=YC
C 170 RETURN
C 180 IER=1
C RETURN
C 190 IER=2
C RETURN
C END

```

```

0ESY 400
0ESY 410
0ESY 420
0ESY 430
0ESY 440
0ESY 450
0ESY 460
0ESY 470
0ESY 480
0ESY 490
0ESY 500
0ESY 510
0ESY 520
0ESY 530
0ESY 540
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0ESY 560
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0ESY 600
0ESY 610
0ESY 620
0ESY 630
0ESY 640
0ESY 650
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0ESY 780
0ESY 790
0ESY 800
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0ESY 820
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0ESY 840
0ESY 850
0ESY 860
0ESY 870
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0ESY 960
0ESY 970
0ESY 980
0ESY 990
0ESY1000
0ESY1010
0ESY1020
0ESY1030
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0ESY1270
0ESY1280
0ESY1290
0ESY1300
0ESY1310
0ESY1320
0ESY1330
0ESY1340

```

Subroutine I0

This subroutine computes the modified Bessel function $I_0(x)$ for a given argument (x).

For $-3.75 \leq x \leq 3.75$; $t = x/3.75$

$$I_0(x) = 1 + 3.515623t^2 + 3.089942t^4 + 1.206749t^6 + 0.2659732t^8 + 0.0360768t^{10} + 0.0045813t^{12} + \epsilon$$

with $|\epsilon| < 1.6 \cdot 10^{-7}$

For $3.75 \leq |x| < \infty$; $t = 3.75/|x|$

$$\sqrt{|x|} e^{-|x|} I_0(x) = 0.3989423 + 0.01328592t + 0.00225319t^2 - 0.00157565t^3 + 0.00916281t^4 - 0.02057706t^5 + 0.02635537t^6 - 0.01647633t^7 + 0.00392377t^8 + \epsilon$$

with $|\epsilon| < 1.9 \cdot 10^{-7}$

```

C
C .....
C
C SUBROUTINE IC
C
C FLRFESE
C COMPUTE THE MODIFIED BESSEL FUNCTION I OF ORDER ZERO
C
C LSACE
C CALL IC(X,MIC)
C
C DESCRIPTION OF PARAMETERS
C X - GIVEN ARGUMENT OF THE BESSEL FUNCTION I OF ORDER 0
C MIC - RESULTANT VALUE OF THE BESSEL FUNCTION I OF ORDER 0
C
C REMARKS
C LARGE VALUES OF THE ARGUMENT MAY CAUSE OVERFLOW IN THE
C BUILT-IN EXP-FUNCTION
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C ACNE
C
C METHOD
C POLYNOMIAL APPROXIMATIONS GIVEN BY E.E. ALLEN ARE USED FOR
C CALCULATION.
C FOR REFERENCE SEE
C P. ABRAMOWITZ AND I.A. STEGUN, HANDBOOK OF MATHEMATICAL
C FUNCTIONS*, U.S. DEPARTMENT OF COMMERCE, NATIONAL BUREAU OF
C STANDARDS APPLIED MATHEMATICS SERIES, 1968, F.378.
C
C .....
C
C SUBROUTINE IC(X,MIC)
C MIC=RES(X)
C IF(MIC-3.75)1,1,2
C 1 Z=0.000111111E-2
C MIC=(((1+.5813E-3)*Z+.6076E-2)*Z+2.659732E-1)*Z+1.206749E0)*Z
C 1+.3089942E0)*Z+.515623E0)*Z+.1.
C PETHA
C Z=2.75/RIC
C RIC=EXP(RIC)/SQRT(MIC)*(((1+(3.92377E-3)*Z-1.647633E-2)*Z
C 1+.2659732E-2)*Z-2.057706E-2)*Z+.16281E-3)*Z-1.57565E-3)*Z
C 2+.25319E-3)*Z+1.328592E-2)*Z+.43985423E-1)
C PETHA
C
C

```

Subroutine INUE

This subroutine computes the modified Bessel functions $I_1(x)$, $I_2(x)$, ..., $I_n(x)$ for a given argument x , where n is the given maximum order.

The recurrence relation

$$I_{k+1}(x) + \frac{2k}{x} I_k(x) - I_{k-1}(x) = 0 \quad (1)$$

is used for this evaluation.

From (1) the values $G_k = I_k/I_{k-1}$ (2)

satisfy
$$G_k = \frac{1}{\frac{2k}{x} + G_{k+1}} \quad (3)$$

Therefore, G_{n+1} may be calculated from the continued fraction

$$G_{n+1} = \frac{1}{\frac{2(n+1)}{x} + \frac{1}{\frac{2(n+2)}{x} + \frac{1}{\frac{2(n+3)}{x} + \dots}} \quad (4)$$

This continued fraction is evaluated using the following forward A-B process:

Let $A_{-1} = 1, A_0 = 0, A_k = \frac{2(n+k)}{x} A_{k-1} + A_{k-2}$ (5)

$B_{-1} = 0, B_0 = 1, B_k = \frac{2(n+k)}{x} B_{k-1} + B_{k-2}$
for $k = 1, 2, \dots$

Then $G_{n+1} = \lim_{k \rightarrow \infty} \frac{A_k}{B_k}$ (6)

From G_{n+1} the values G_n, G_{n-1}, \dots, G_1 are obtained

applying (3) successively, with $k = n, n-1, \dots, 1$.

Finally the values I_1, I_2, \dots, I_n are computed using $I_k = G_k \cdot I_{k-1}$, where I_0 is the value of (7)

Bessel function I of order zero, for example, as obtained using subroutine I0.

```

C
C .....
C SUBROUTINE INUE
C
C PURPOSE
C COMPUTE THE MODIFIED BESSEL FUNCTIONS I FOR ORDERS 1 TO N
C
C USAGE
C CALL INUE(X,N,ZI,RI)
C
C DESCRIPTION OF PARAMETERS
C X - GIVEN ARGUMENT OF THE BESSEL FUNCTIONS I
C N - GIVEN MAXIMUM ORDER OF BESSEL FUNCTIONS I
C ZI - GIVEN VALUE OF BESSEL FUNCTION I OF ORDER ZERO
C FOR ARGUMENT X
C RI - RESULTANT VECTOR OF DIMENSION N, CONTAINING THE
C VALUES OF THE FUNCTIONS I FOR ORDERS 1 TO N
C
C REMARKS
C THE VALUE OF ZI MAY BE CALCULATED USING SUBROUTINE I0.
C USING A DIFFERENT VALUE HAS THE EFFECT THAT ALL VALUES OF
C BESSEL FUNCTIONS I ARE MULTIPLIED BY THE FACTOR ZI/I(0,X)
C WHERE I(0,X) IS THE VALUE OF I FOR ORDER 0 AND ARGUMENT X.
C THIS MAY BE USED DISADVANTAGEOUSLY IF ONLY THE RATIOS OF I
C FOR DIFFERENT ORDERS ARE REQUIRED.
C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C NCNE
C
C METHOD
C THE VALUES ARE OBTAINED USING BACKWARD RECURRENCE RELATION
C TECHNIQUE. THE RATIO I(N+1,X)/I(N,X) IS OBTAINED FROM A
C CONTINUED FRACTION.
C FOR REFERENCE SEE
C G. BLANCHI, 'NUMERICAL EVALUATION OF CONTINUED FRACTIONS',
C SIAM REVIEW, VOL.6,NO.4,1964,PP.383-421.
C .....
C SUBROUTINE INUE(X,N,ZI,RI)
C DIMENSION RI(1)
C IF(N<10,10,1)
C 1 FN=N*N
C Q1=X/FN
C IF(ABS(X)-5.E-416,6,7)
C 2 A0=1.
C A1=0.
C B0=0.
C B1=L.
C FI=FN
C 3 FI=FI+2.
C AN=FI/ABS(X)
C A=AN*A1+A0
C B=AN*B1+B0
C A0=A1
C B0=B1
C A1=A
C B1=B
C Q0=Q1
C Q1=A/B
C 4 IF(X<5,6,6)
C 5 C1=-Q1
C K=N
C 7 Q1=X/(FN+X*Q1)
C RI(K)=Q1
C FN=FN-2.
C K=K-1
C IF(K<10,8,7)
C 8 FI=ZI
C DO 9 I=1,N
C FI=FI*RI(I)
C 9 RI(I)=FI
C 10 RETURN
C END
INUF 10
INUE 20
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INUE 730
INUE 740
INUE 750
INUE 760

```

Subroutine BESK

This subroutine computes the K Bessel function for a given argument x and order n. The recurrence relation:

$$K_{n+1}(x) = \frac{2n}{x} K_n(x) + K_{n-1}(x) \quad (1)$$

is used for this evaluation.

The initial values K_0 and K_1 are found as follows:

For $x > 1$:

$$K_0(x) = e^{-x} \sqrt{\frac{\pi}{2x}} G_0(x) \quad (2)$$

$$K_1(x) = e^{-x} \sqrt{\frac{\pi}{2x}} G_1(x) \quad (3)$$

where $x = 1/t$ for $t < 1$:

$$G_0\left(\frac{1}{t}\right) \cdot \sqrt{\frac{\pi}{2}} = 1.2533141 - 0.1566642t - 0.08811128t^2 - 0.09139095t^3 + 0.1344596t^4 - 0.2299850t^5 + 0.3792410t^6 - 0.5247277t^7 + 0.5575368t^8 - 0.4262633t^9 + 0.2184518t^{10} - 0.06680977t^{11} + 0.009189383t^{12} \quad (4)$$

$$G_1\left(\frac{1}{t}\right) \cdot \sqrt{\frac{\pi}{2}} = 1.2533141 + 0.4699927t - 0.1468583t^2 + 0.1280427t^3 - 0.1736432t^4 + 0.2847618t^5 - 0.4594342t^6 + 0.6283381t^7 - 0.6632295t^8 + 0.5050239t^9 - 0.2581304t^{10} + 0.07880001t^{11} - 0.0108242t^{12} \quad (5)$$

For $x \leq 1$:

$$\gamma = \text{Euler's constant} = 0.5772156649 \quad (6)$$

$$K_0(x) = -\left(\gamma + \log \frac{x}{2}\right) + \sum_{s=1}^6 \left(\frac{x}{2}\right)^{2s} \frac{1}{(s!)^2} \left[H_s - \left(\gamma + \log \frac{x}{2}\right) \right] \quad (7)$$

where:

$$H_s = \sum_{r=1}^s \frac{1}{r} \quad (8)$$

$$K_1(x) = \frac{1}{x} + \sum_{s=1}^8 \left(\frac{x}{2}\right)^{2s-1} \frac{1}{(s!)^2} \left[\frac{1}{2} + s \cdot \left(\gamma + \log \frac{x}{2} - H_s\right) \right] \quad (9)$$

```

C ..... BESK 10
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C ..... BESK 670
C ..... BESK 680
C ..... BESK 690
C ..... BESK 700
C ..... BESK 710
C ..... BESK 720
C ..... BESK 730

```

```

C      25 G1=0*(1.2522141+.4655527*(1)-.1468563*(2)+.1280427*(3)
      2-.1726432*(4)+.2647618*(5)-.4554342*(6)+.6283321*(7)
      3-.8622254*(8)+.5650225*(9)-.2561304*(10)+.0788000*(11)
      4-.0106418*(12)+0
      IF(A-112C,30,31)
30  BK=G1
   RETURN
C
C      FRCR KC,K1 CCFPLTE KN USING RECURRENCE RELATION
C
C      31 CC 35 J=2,A
      GJ=2.0*(FLCAT(J)-1.)*C1/X+GC
      IF(6J-1.CE7C133,23,32)
32  IER=4
      CC 1C 24
33  CC=G1
34  C1=GJ
35  BK=GJ
   RETURN
36  B=J/2.
      A=.5772157+ALCG(B)
      C=0
      IF(A-1137.43,37)
C
C      CCFPLTE KC USING SERIES EXPANSION
C
C      37 CC=0
      X2J=1.
      FACT=1.
      FJ=C
      CC 4C J=1,6
      RJ=1./FLCAT(J)
      X2J=X2J*JC
      FACT=FACT*RJ*RJ
      FJ=FJ+FJ
40  GC=GC+X2J*FACT*(FJ-A)
      IF(A-143.42,43)
42  BK=GC
   RETURN
C
C      CCFPLTE K1 USING SERIES EXPANSION
C
C      43 X2J=0
      FACT=1.
      FJ=1.
      C1=1./X+X2J*(1.5+A-FJ)
      CC 5C J=2,8
      X2J=X2J*JC
      RJ=1./FLCAT(J)
      FACT=FACT*RJ*RJ
      FJ=FJ+FJ
50  G1=G1+X2J*FACT*(1.5+(A-FJ)*FLCAT(J))
      IF(A-1131.52,31)
52  BK=G1
   RETURN
   END

```

```

BESK 740
BESK 750
BESK 760
BESK 770
BESK 780
BESK 790
BESK 800
BESK 810
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BESK 830
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BESK1290
BESK1300

```

Subroutine EXPI

This subroutine computes the exponential integral for a given value of the argument x.

The exponential integral is defined as:

$$E_1(x) = -\text{Ei}(-x) = \int_x^\infty \frac{e^{-t}}{t} dt = \int_0^x \frac{1-e^{-t}}{t} dt - C - \ln(x)$$

where $C = 0.57 \dots$ is Euler's constant.

The integral

$$\int_x^\infty \frac{e^{-t}}{t} dt \text{ has a logarithmic singularity at } x = 0.$$

Therefore, it must be evaluated in the Cauchy Principal Value sense for negative values of x.

For $x = 0$ the routine returns $-1.E75$ as value of $E_1(x)$.

For $x \geq 1$:

$$\begin{aligned} \text{AUX} &= x e^x E_1(x) \\ &= (x^4 + 8.5733287401x^3 + 18.0590169730x^2 \\ &\quad + 8.6347608925x + 0.2677737343)/ \\ &\quad (x^4 + 9.5733223454x^3 + 25.6329561486x^2 \\ &\quad + 21.0996530827x + 3.9584969228) + \epsilon \end{aligned}$$

with $|\epsilon| < 2.E-8$.

For $-3 \leq x \leq 1$:

$$\begin{aligned} \text{AUX} &= (E_1(x) + \ln|x| + C)/x \\ &= 9.999999E-1 - 2.500001E-1 \cdot x \\ &\quad + 5.555682E-2 \cdot x^2 - 1.041576E-2 \cdot x^3 \\ &\quad + 1.664156E-3 \cdot x^4 - 2.335379E-4 \cdot x^5 \\ &\quad + 2.928433E-5 \cdot x^6 - 1.766345E-6 \cdot x^7 \\ &\quad + 7.122452E-7 \cdot x^7 + \epsilon \end{aligned}$$

with $|\epsilon| < 7.3E-8$.

Subroutine CS

This subroutine computes the Fresnel integrals for a given value of the argument x.

The Fresnel integrals are defined as:

$$C(x) = \frac{1}{\sqrt{2\pi}} \int_0^x \frac{\cos(t)}{\sqrt{t}} dt = \int_0^{\sqrt{\frac{2}{\pi}x}} \cos\left(\frac{\pi}{2}u^2\right) du$$

and

$$S(x) = \frac{1}{\sqrt{2\pi}} \int_0^x \frac{\sin(t)}{\sqrt{t}} dt = \int_0^{\sqrt{\frac{2}{\pi}x}} \sin\left(\frac{\pi}{2}u^2\right) du$$

The subroutine CS calculates both C(x) and S(x) simultaneously.

If x is negative, |x| is used in CS.

For $0 \leq x \leq 4$ and $t = 16 - x^2$:

$$C(x)/\sqrt{x} = 1.840962E-1 + 1.102544E-2 \cdot t + 1.020418E-3 \cdot t^2 + 3.273308E-5 \cdot t^3 + 5.451182E-7 \cdot t^4 + 5.244297E-9 \cdot t^5 + 5.100785E-11 \cdot t^6 +$$

with $|\epsilon| < 8.5E-9$

$$S(x)/\sqrt{x^3} = 8.026490E-2 + 6.121300E-3 \cdot t + 2.441816E-4 \cdot t^2 + 5.051141E-6 \cdot t^3 + 5.883158E-8 \cdot t^4 + 6.677681E-10 \cdot t^5 + \epsilon$$

with $|\epsilon| < 3.5E-8$.

For $x > 4$ and $t = 4/x$:

$$C(x) = \frac{1}{2} + \sqrt{\frac{4}{x}} (\sin(x) \cdot P(x) + \cos(x) \cdot Q(x)) + \epsilon$$

$$S(x) = \frac{1}{2} + \sqrt{\frac{4}{x}} (-\cos(x) \cdot P(x) + \sin(x) \cdot Q(x)) + \epsilon$$

where $|\epsilon| < 1.3E-8$ and

$$P(x) = 1.994712E-1 - 1.207998E-6 \cdot t - 9.314911E-3 \cdot t^2 - 4.027145E-4 \cdot t^3 + 7.428246E-3 \cdot t^4 - 7.271690E-3 \cdot t^5 + 3.401409E-3 \cdot t^6 - 6.633926E-4 \cdot t^7$$

and

$$Q(x) = 4.444091E-9 - 2.493322E-2 \cdot t - 1.606428E-5 \cdot t^2 + 5.972151E-3 \cdot t^3 - 3.095341E-4 \cdot t^4 - 6.792801E-3 \cdot t^5 + 7.970943E-3 \cdot t^6 - 4.169289E-3 \cdot t^7 + 8.768258E-4 \cdot t^8$$

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```

Subroutines CEL1 and DCEL1

These subroutines compute the complete elliptic integral of the first kind. This is defined as:

$$K(k) = \int_0^{\pi/2} \frac{dt}{\sqrt{1-k^2 \sin^2 t}}, \quad 0 \leq k < 1$$

An equivalent definition is:

$$K(k) = \int_0^{\infty} \frac{dx}{\sqrt{(1+x^2)(1+k_c^2 x^2)}}$$

where k_c is the complementary modulus:

$$k_c^2 + k^2 = 1, \quad 0 < k_c^2 \leq 1$$

The subroutines CEL1, DCEL1 calculate $K(k)$ for given modulus k . The calculation of $RES = K(k)$ is based on the process of the arithmetic-geometric mean.

Starting with the pair of numbers:

$$a_0 = 2, \quad g_0 = 2 \cdot k_c$$

the sequences of numbers (a_n) , (g_n) are generated using the definition:

$$a_n = (a_{n-1} + g_{n-1}), \quad g_n = 2\sqrt{a_{n-1} \cdot g_{n-1}}$$

This iterative process is stopped at the N^{th} step, when $a_N = g_N$.

If D is the number of decimal digits in the mantissa of floating-point numbers, then the equality $a_N = g_N$ must be interpreted as $|a_N - g_N|$ is less than $a_N \cdot 10^{-D}$.

Since the sequences $(2^{-(n+1)} a_n)$, $(2^{-(n+1)} g_n)$ converge quadratically to the same limit (arithmetic-geometric mean) the test for the end of iteration may be replaced by comparing $|a_{N-1} - g_{N-1}|$ against $a_{N-1} \cdot 10^{-D/2}$, thus saving one calculation of the geometric mean.

$$\text{The value of } K(k) = \frac{2N\pi}{a_N}$$

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C .....DCEL 1000

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Subroutines CEL2 and DCEL2

These subroutines compute the generalized complete elliptic integral of the second kind. This is defined as:

$$\text{cel 2 } (k; A, B) = \int_0^{\pi/2} \frac{A + (B - A)\sin^2 t}{\sqrt{1 - k^2 \sin^2 t}} dt$$

Equivalent is the definition:

$$\text{cel 2 } (k; A, B) = \int_0^{\infty} \frac{A + Bx^2}{(1 + x^2)\sqrt{(1 + x^2)(1 + k_c^2 x^2)}} dx$$

where k_c is the complementary modulus:

$$k_c^2 + k^2 = 1, \quad 0 < k_c^2 \leq 1$$

The subroutines CEL2, DCEL2 calculate cel 2 (k; A, B) for given modulus k and constants A, B. The calculation of RES = cel 2 (k; A, B) is based on the process of the arithmetic-geometric mean.

Starting with the pair of numbers:

$$a_0 = 2, \quad g_0 = 2 \cdot k_c$$

the sequences of numbers (a_n) , (g_n) are generated using for definition:

$$a_n = (a_{n-1} + g_{n-1}), \quad g_n = 2\sqrt{a_{n-1}g_{n-1}}$$

This iteration process is stopped at the N^{th} step when $a_N = g_N$.

Further needed are the sequences (A_i) , (B_i) , defined by means of:

$$A_0 = A, \quad B_0 = B$$

$$A_n = B_{n-1}/a_{n-1} + A_{n-1}$$

$$B_n = 2(B_{n-1} + g_{n-1} \cdot A_{n-1})$$

If D is the number of decimal digits in the mantissa of floating-point numbers, the iteration process is stopped as soon as $(a_{N-1} - g_{N-1})$ is less than

$$a_{N-1} \cdot 10^{-D/2}$$

Since $(2^{-(n+1)}a_n)$, $(2^{-(n+1)}g_n)$ converge quadratically to the same limit (arithmetic-geometric mean), this implies that $(a_N - g_N)$ is less than $a_N \cdot 10^{-D}$.

The value of cel 2 (k, A, B) = $\frac{\pi}{4} \cdot \frac{A_{N+1}}{a_N}$

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C ..... CEL2 800

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Subroutines ELI1 and DELI1

These subroutines compute the elliptic integral of the first kind, where:

$$\text{eli } 1(x, ck) = \int_0^x \frac{dt}{\sqrt{(1+t^2)(1+ck^2 t^2)}}$$

Equivalent definitions are:

$$\text{eli } 1(x, ck) = \int_0^{\arctan x} \frac{dt}{\cos t \sqrt{1+ck^2 \tan^2 t}}$$

$$= \int_0^{\arctan x} \frac{dt}{\sqrt{1-k^2 \sin^2 t}}$$

where k is the modulus and ck the complementary modulus.

For reason of numerical stability, ck is chosen as input parameter instead of modulus k :

$$0 \leq ck^2 < \infty \text{ and } k^2 + ck^2 = 1.$$

This allows k to be any pure imaginary or real number such that $k^2 \leq 1$. In standard notation:

$$F(\varphi, k) = \text{eli } 1(\tan \varphi, ck)$$

Computation is based on the process of the arithmetic-geometric mean together with Landen's transformation:

$$\text{eli } 1(x, ck) = \frac{1}{1+ck} \text{eli } 1(x_1, ck_1)$$

where:

$$ck_1 = \frac{2\sqrt{ck}}{1+ck}$$

$$x_1 = \frac{(1+ck)x}{1-ck \cdot x^2}$$

$$\phi_1 = \arctan x_1$$

$$\sin \phi_1 = \frac{x_1}{\sqrt{1+x_1^2}}$$

The iteration process begins with $\text{ari}_0 = 1$, $\text{geo}_0 = |ck|$, and the sequences (ari_n) , (geo_n) are generated using for definition:

$$\text{ari}_{n+1} = \text{ari}_n + \text{geo}_n$$

$$\text{geo}_{n+1} = 2\sqrt{\text{ari}_n \cdot \text{geo}_n}$$

The iteration process is stopped at the N^{th} step when $\text{ari}_N = \text{geo}_N$.

Further needed is an iteration scheme for transformation of the argument x .

$$\text{Setting } \text{ang}_i = \frac{\text{ari}_i}{x_i}$$

$$\text{then } \text{ang}_0 = 1/|x|$$

$$\text{ang}_{n+1} = \text{ang}_n - \frac{\text{ari}_n \cdot \text{geo}_n}{\text{ang}_n}$$

Doing the iteration up to the N^{th} step (characterized by $\text{ari}_N = \text{geo}_N$):

$$\text{eli } 1(x, ck) = \frac{\text{ari}_0}{\text{ari}_N} \text{eli } 1(x_N, ck_N)$$

$$\text{with } \sin \phi_N = \frac{\text{ari}_N}{\pm \sqrt{\text{ang}_N^2 + \text{ari}_N^2}}$$

The sign determination of $\sin \phi_N$ must be done so that $\phi = \arctan x_i$ is continuously increasing with index i . With $\text{ari}_N = \text{geo}_N$, then $ck_N = 1$, $k_N = 0$ and therefore:

$$\text{eli } 1(x_N, ck_N) = \int_0^{\phi_N} dt = \phi_N$$

and the final result is:

$$\text{eli } 1(x, ck) = \frac{\phi_N}{\text{ari}_N}$$

Degenerate cases of argument and modulus:

$x = 0$ gives result $\text{eli } 1 = 0$

$ck = 0$ gives result $\text{eli } 1 = \text{sgn } x \ln(|x| + \sqrt{1+x^2})$

```

C ..... ELI1 10 IF(X)2,1,2 DEL1 470
C ..... ELI1 20 1 RES=0.00 DEL1 480
C ..... ELI1 30 RETURN DEL1 490
C ..... ELI1 40 C DEL1 500
C SUBROUTINE ELI1 ELI1 50 2 IF(CK)4,3,4 DEL1 510
C PURPOSE ELI1 60 3 RES=DLOG(DABS(X)+DSQRT(1.00+X*X)) DEL1 520
C COMPUTES THE ELLIPTIC INTEGRAL OF FIRST KIND ELI1 70 GOTO 13 DEL1 530
C ELI1 80 DEL1 540
C USAGE ELI1 90 4 ANGLE=DARS(1.00/X) DEL1 550
C CALL ELI1(RES,X,CK) ELI1 100 GEO=DABS(CK) DEL1 560
C ELI1 110 ARI=1.00 DEL1 570
C ELI1 120 PIM=0.00 DEL1 580
C DESCRIPTION OF PARAMETERS ELI1 130 5 SQGEO=ARI+GEO DEL1 590
C RES - RESULT VALUE ELI1 140 AARI=ARI DEL1 600
C X - UPPER INTEGRATION BOUND (ARGUMENT OF ELLIPTIC ELI1 150 ARI=GEO+ARI DEL1 610
C INTEGRAL OF FIRST KIND) ELI1 160 ANGLE=-SQGEO/ANGLE+ANGLE DEL1 620
C CK - COMPLEMENTARY MODULUS ELI1 170 SQGEO=DSQRT(SQGEO) DEL1 630
C ELI1 180 IF(ANGLE)7,6,7 DEL1 640
C REMARKS ELI1 190 C DEL1 650
C MODULUS K = SQRT(1.-CK*CK). ELI1 200 C DEL1 660
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED ELI1 210 C DEL1 670
C NONE ELI1 220 C DEL1 680
C ELI1 230 DEL1 690
C METHOD ELI1 240 IF(DABS(AARI-GEO)-TEST)10,10,8 DEL1 700
C DEFINITION ELI1 250 8 GEO=SQGEO+SQGEO DEL1 710
C RES=INTEGRAL(1/SQRT((1+T*T)*(1+(CK*T)**2))), SUMMED ELI1 260 PIM=PIM+PIM DEL1 720
C OVER T FROM 0 TO X). ELI1 270 PIM=SQGEO+SQGEO DEL1 730
C EQUIVALENT ARE THE DEFINITIONS ELI1 280 9 PIM=PIM+3.1415926535897932 DEL1 740
C RES=INTEGRAL(1/(COS(T)+SQRT(1+(CK*TAN(T))**2))), SUMMED ELI1 290 GOTO 5 DEL1 750
C OVER T FROM 0 TO ATAN(X)). ELI1 300 10 IF(ANGLE)11,12,12 DEL1 760
C RES=INTEGRAL(1/SQRT(1-(K*SIN(T))**2))), SUMMED OVER ELI1 310 11 PIM=PIM+3.1415926535897932 DEL1 770
C T FROM 0 TO ATAN(X)). ELI1 320 12 RES=(ATAN(ARI/ANGLE)+PIM)/ARI DEL1 780
C EVALUATION ELI1 330 13 IF(X)14,15,15 DEL1 790
C LANDENS TRANSFORMATION IS USED FOR CALCULATION. ELI1 340 14 RES=-RES DEL1 800
C REFERENCE ELI1 350 15 RETURN DEL1 810
C R. BULIRSCH, NUMERICAL CALCULATION OF ELLIPTIC INTEGRALS AND DELI1 360 END DEL1 820
C ELLIPTIC FUNCTIONS. ELI1 370
C HANDBOOK SERIES OF SPECIAL FUNCTIONS ELI1 380
C NUMERISCHE MATHEMATIK VOL. 7, 1965, PP. 78-90. ELI1 390
C ..... ELI1 400
C SUBROUTINE ELI1(RES,X,CK) ELI1 410
C IF(X)2,1,2 ELI1 420
C 1 RES=0. ELI1 430
C RETURN ELI1 440
C 2 IF(CK)4,3,4 ELI1 450
C 3 RES=DLOG(DABS(X)+SQRT(1.+X*X)) ELI1 460
C GOTO 13 ELI1 470
C 4 ANGLE=DARS(1./X) ELI1 480
C GEO=DABS(CK) ELI1 490
C ARI=1. ELI1 500
C PIM=0. ELI1 510
C 5 SQGEO=ARI+GEO ELI1 520
C AARI=ARI ELI1 530
C ARI=GEO+ARI ELI1 540
C ANGLE=-SQGEO/ANGLE+ANGLE ELI1 550
C SQGEO=SQRT(SQGEO) ELI1 560
C IF(ANGLE)7,6,7 ELI1 570
C REPLACE 0 BY SMALL VALUE ELI1 580
C 6 ANGLE=SQGEO*1.E-8 ELI1 600
C 7 TEST=AARI*1.E-4 ELI1 610
C IF(DABS(AARI-GEO)-TEST)10,10,8 ELI1 620
C 8 GEO=SQGEO+SQGEO ELI1 630
C PIM=PIM+PIM ELI1 640
C IF(ANGLE)9,5,5 ELI1 650
C 9 PIM=PIM+3.1415927 ELI1 660
C GOTO 5 ELI1 670
C 10 IF(ANGLE)11,12,12 ELI1 680
C 11 PIM=PIM+3.1415927 ELI1 690
C 12 RES=(ATAN(ARI/ANGLE)+PIM)/ARI ELI1 700
C 13 IF(X)14,15,15 ELI1 710
C 14 RES=-RES ELI1 720
C 15 RETURN ELI1 730
C END ELI1 740

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C ..... DELI 770
C ..... DELI 780
C ..... DELI 790
C ..... DELI 800
C ..... DELI 810
C ..... DELI 820

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Subroutines ELI2 and DELI2

These subroutines compute the generalized elliptic integral of the second kind, where:

$$\text{eli 2}(x, ck, a, b) = \int_0^x \frac{(a + bt^2) dt}{(1+t^2)\sqrt{(1+t^2)(1+ck^2t^2)}}$$

Equivalent are the definitions:

$$\begin{aligned} \text{eli 2}(x, ck, a, b) &= \int_0^{\arctan x} \frac{(a + b \tan^2 t) dt}{\sqrt{(1+\tan^2 t)(1+ck^2 \tan^2 t)}} \\ &= \int_0^{\arctan x} \frac{(a + (b-a)\sin^2 t) dt}{\sqrt{1 - k^2 \sin^2 t}} \end{aligned}$$

where k is the modulus and ck the complementary modulus.

For reasons of numerical stability, ck is chosen as input parameter instead of modulus k :

$$0 \leq ck^2 < \infty \text{ and } k^2 + ck^2 = 1$$

This allows k to be any pure imaginary or real number such that $k^2 \leq 1$.

In standard notation:

$$\begin{aligned} E(\varphi, k) &= \text{eli 2}(\tan \varphi, ck, 1, ck^2) \\ F(\varphi, k) &= \text{eli 2}(\tan \varphi, ck, 1, 1) \end{aligned}$$

Computation is based on the process of the arithmetic-geometric mean together with Landen's transformation:

$$\begin{aligned} \text{eli 2}(x, ck, a, b) &= \frac{1}{1+ck} \left(\text{eli 2}(x_1, ck_1, a_1, b_1) + \right. \\ &\quad \left. \frac{1}{2}(a-b) \frac{x_1}{\sqrt{1+x_1^2}} \right) \end{aligned}$$

where:

$$a_1 = \frac{1}{2}(a+b)$$

$$b_1 = \frac{1}{1+ck}(b+a \cdot ck)$$

$$ck_1 = \frac{2\sqrt{ck}}{1+ck}$$

$$a_1 - b_1 = \frac{1}{2}(a-b) \frac{1-ck}{1+ck}$$

$$x_1 = \frac{(1+ck)x}{1-ck \cdot x^2}$$

$$k_1 = \frac{1-ck}{1+ck}$$

$$\phi_1 = \arctan x_1$$

$$\sin \phi_1 = \frac{x_1}{\sqrt{1+x_1^2}}$$

The iteration process begins with $\text{ari}_0 = 1$, $\text{geo}_0 = |ck|$, and the sequences (ari_n) , (geo_n) are generated, using for definition:

$$\text{ari}_{n+1} = \text{ari}_n + \text{geo}_n$$

$$\text{geo}_{n+1} = 2\sqrt{\text{ari}_n \cdot \text{geo}_n}$$

The iteration process is stopped at the N^{th} step when $\text{ari}_N = \text{geo}_N$.

Further needed are the sequences (A_i) , (B_i) , defined by means of:

$A_i = a_i$, $B_i = b_i \cdot \text{ari}_i$; that is, by the iteration scheme

$$A_0 = a, B_0 = b$$

$$A_{n+1} = \frac{1}{2} \left(A_n + \frac{B_n}{\text{ari}_n} \right)$$

$$B_{n+1} = B_n + \text{geo}_n \cdot A_n$$

Finally an iteration scheme is needed for transformation of the argument x .

$$\text{Setting } \text{ang}_i = \frac{\text{ari}_i}{x_i}$$

$$\text{gives } \text{ang}_0 = 1/|x|$$

$$\text{ang}_{n+1} = \text{ang}_n - \frac{\text{ari}_n \cdot \text{geo}_n}{\text{ang}_n}$$

Doing the iteration scheme up to the N^{th} step (characterized by $\text{ari}_N = \text{geo}_N$):

$$\text{eli}_2(x, ck, a, b) = \frac{\text{ari}_0}{\text{ari}_N} \text{eli}_2(x_N, ck_N, a_N, b_N) + \text{SUM}$$

$$\text{where SUM} = \frac{a-b}{2} \left(\frac{1}{\text{ari}_1} \sin \phi_1 + \frac{1}{\text{ari}_2} \frac{\text{ari}_0 - \text{geo}_0}{\text{ari}_1} \frac{\sin \phi_2}{2} + \dots + \frac{1}{\text{ari}_N} \frac{\text{ari}_0 - \text{geo}_0}{\text{ari}_1} \dots \frac{\text{ari}_{N-2} - \text{geo}_{N-2}}{\text{ari}_{N-1}} \right)$$

$$\frac{\sin \phi_N}{2^{N-1}}$$

$$\text{with } \sin \phi_n = \frac{\text{ari}_n}{\sqrt{\text{ang}_n^2 + \text{ari}_n^2}}$$

The sign determination of $\sin \phi_n$ must be done so that $\phi_n = \arctan x_n$ is continuously increasing with index n .

With $\text{ari}_N = \text{geo}_N$, then $ck_N = 1$, $k_N = 0$, and therefore

$$\text{eli}_2(x_N, ck_N, a_N, b_N) = \int_0^{\phi_N} [a_N + (b_N - a_N) \sin^2 t] dt$$

$$= \frac{a_N + b_N}{2} \phi_N - \frac{1}{2} (b_N - a_N) \sin \phi_N \cos \phi_N$$

The final result is:

$$\text{eli}_2(x, ck, a, b) = \frac{A_{N+1}}{\text{ari}_N} \cdot \arctan \frac{\text{ari}_N}{\text{ang}_N} + \text{SUM} +$$

$$\frac{1}{\text{ari}_N} \left(\frac{a_N - b_N}{2} \right) \sin \phi_N \cos \phi_N$$

Degenerate cases of argument and modulus:

$x = 0$ gives result $\text{eli}_2 = 0$

$ck = 0$ gives result $\text{eli}_2 = \left[b \cdot \ln(|x| + \sqrt{1+x^2}) \right] +$

$$(a-b) \frac{|x|}{\sqrt{1+x^2}} \text{sgn } x$$

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C ..... ELI2 870
C ..... ELI2 880
C ..... ELI2 890
C ..... ELI2 900
C ..... ELI2 910
C ..... ELI2 920
C ..... ELI2 930
C ..... ELI2 940
C ..... ELI2 950
C ..... ELI2 960
C ..... ELI2 970
C ..... ELI2 980
C ..... ELI2 990
C ..... ELI21000
C ..... ELI21010
C ..... ELI21020
C ..... ELI21030
C ..... ELI21040
C ..... ELI21050
C ..... ELI21060
C ..... ELI21070
C ..... ELI21080
C ..... ELI21090

```

the final result is the iteration scheme:

$$c_{N+1} = a_{N+1} \cot(\gamma \cdot a_{N+1})$$

$$d_{N+1} = 1$$

$$c_n = d_{n+1} \cdot c_{n+1}$$

$$d_n = \frac{c_{n+1}^2 / a_{n+2} + \text{geo}_{n+1}}{c_{n+1}^2 / a_{n+2} + a_{n+1}}$$

for $n = N, N-1, \dots, 1$.

Then $c_1 = \cot \varphi$, and:

$$\text{sn}(x, k) = \frac{1}{\sqrt{1+c_1^2}} = \frac{1}{\sqrt{1+\cot^2 \varphi}} = \sin \varphi$$

$$\text{cn}(x, k) = \text{sn} \cdot c_1 = \sin \varphi \cdot \cot \varphi = \cos \varphi$$

$$\text{dn}(x, k) = d_1 = \sqrt{1-k^2} \sin \varphi$$

```

C ..... JELF 10
C ..... JELF 20
C ..... JELF 30
C ..... JELF 40
C ..... JELF 50
C ..... JELF 60
C ..... JELF 70
C ..... JELF 80
C ..... JELF 90
C ..... JELF 100
C ..... JELF 110
C ..... JELF 120
C ..... JELF 130
C ..... JELF 140
C ..... JELF 150
C ..... JELF 160
C ..... JELF 170
C ..... JELF 180
C ..... JELF 190
C ..... JELF 200
C ..... JELF 210
C ..... JELF 220
C ..... JELF 230
C ..... JELF 240
C ..... JELF 250
C ..... JELF 260
C ..... JELF 270
C ..... JELF 280
C ..... JELF 290
C ..... JELF 300
C ..... JELF 310
C ..... JELF 320
C ..... JELF 330
C ..... JELF 340
C ..... JELF 350
C ..... JELF 360
C ..... JELF 370
C ..... JELF 380
C ..... JELF 390
C ..... JELF 400
C ..... JELF 410
C ..... JELF 420
C ..... JELF 430
C ..... JELF 440
C ..... JELF 450
C ..... JELF 460
C ..... JELF 470
C ..... JELF 480
C ..... JELF 490
C ..... JELF 500

```

```

1 D=EXP(X) JELF 510
A=1./D JELF 520
B=A*D JELF 530
CN=2./B JELF 540
DN=CN JELF 550
SN=TANH(X) JELF 560
C DEGENERATE CASE SCK=0 GIVES RESULTS JELF 570
C CN X = DN X = 1/COSH X JELF 580
C SN X = TANH X JELF 590
2 RETURN JELF 600
C JACOBI'S MODULUS TRANSFORMATION JELF 610
3 D=1.-SCK JELF 620
CM=-SCK/D JELF 630
D=SQRT(D) JELF 640
Y=D*X JELF 650
4 A=1. JELF 660
DN=1. JELF 670
DO 6 I=1,12 JELF 680
L=1 JELF 690
ARI(I)=A JELF 700
CM=SQRT(CM) JELF 710
GEO(I)=CM JELF 720
C=(A+CM)*.5 JELF 730
IF(ABS(A-CM)-1.E-4*4)7,7,5 JELF 740
5 CM=A*CM JELF 750
6 A=C JELF 760
C JELF 770
C START BACKWARD RECURSION JELF 780
7 Y=C*Y JELF 790
SN=SIN(Y) JELF 800
CN=COS(Y) JELF 810
IF(SN)9,13,8 JELF 820
8 A=CM/SN JELF 830
C=A*C JELF 840
DO 9 I=1,L JELF 850
K=L-I+1 JELF 860
B=ARI(K) JELF 870
A=C*A JELF 880
C=DN*C JELF 890
DN=(GEO(K)+A)/(B+A) JELF 900
9 A=C/B JELF 910
A=1./SQRT(C*C+1.) JELF 920
IF(SN)10,11,11 JELF 930
10 SN=-A JELF 940
GOTO 12 JELF 950
11 SN=A JELF 960
12 CM=C*SN JELF 970
13 IF(SCK)14,2,2 JELF 980
14 A=DN JELF 990
DN=CN JELF 1000
CN=A JELF 1010
SN=SN/D JELF 1020
RETURN JELF 1030
END JELF 1040

```

```

C ..... DJEL 10
C ..... DJEL 20
C ..... DJEL 30
C ..... DJEL 40
C ..... DJEL 50
C ..... DJEL 60
C ..... DJEL 70
C ..... DJEL 80
C ..... DJEL 90
C ..... DJEL 100
C ..... DJEL 110
C ..... DJEL 120
C ..... DJEL 130
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C ..... DJEL 390
C ..... DJEL 400
C ..... DJEL 410
C ..... DJEL 420
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C ..... DJEL 500
C ..... DJEL 510
C ..... DJEL 520
C ..... DJEL 530
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C ..... DJEL 560
C ..... DJEL 570
C ..... DJEL 580
C ..... DJEL 590
C ..... DJEL 600
C ..... DJEL 610
C ..... DJEL 620
C ..... DJEL 630
C ..... DJEL 640
C ..... DJEL 650
C ..... DJEL 660
C ..... DJEL 670
C ..... DJEL 680
C ..... DJEL 690
C ..... DJEL 700
C ..... DJEL 710

```

```

4 A=1.00
DN=1.00
DO 6 I=1,12
L=I
AR(I)=A
CM=DSQRT(CM)
GEO(I)=CM
C=(A+CM)*.500
IF(DABS(A-CM)-1.0-9*A)7,7,5
5 CM=A*CM
6 A=C
C
C
START BACKWARD RECURSION
C
7 Y=C*Y
SN=DSIN(Y)
CN=DCOS(Y)
IF(SN18.13,8
8 A=CN/SN
C=A*C

```

```

DJEL 720
DJEL 730
DJEL 740
DJEL 750
DJEL 760
DJEL 770
DJEL 780
DJEL 790
DJEL 800
DJEL 810
DJEL 820
DJEL 830
DJEL 840
DJEL 850
DJEL 860
DJEL 870
DJEL 880
DJEL 890
DJEL 900
DJEL 910

```

```

DO 9 I=1,L
K=L-I+1
B=ARI(K)
A=C*A
C=DN*C
DN=(GEO(K)+A)/(8+A)
9 A=C/B
A=1.00/DSQRT(C*C+1.00)
IF(SN)10,11,11
10 SN=-A
GOTO 12
11 SN=A
12 CN=C*SN
13 IF(SCK)14,2,2
14 A=DN
DN=CN
CN=A
SN=SN/D
RETURN
END

```

```

DJEL 920
DJEL 930
DJEL 940
DJEL 950
DJEL 960
DJEL 970
DJEL 980
DJEL 990
DJEL1000
DJEL1010
DJEL1020
DJEL1030
DJEL1040
DJEL1050
DJEL1060
DJEL1070
DJEL1080
DJEL1090
DJEL1100
DJEL1110

```

APPENDIX A: ACCURACY OF SUBROUTINES

The subroutines in SSP can be broken down into three major categories from the standpoint of accuracy. They are (1) subroutines having little or no effect on accuracy, (2) subroutines whose accuracy is dependent on the characteristics of the input data, and (3) subroutines in which definite statements on accuracy can be made.

SUBROUTINES HAVING LITTLE OR NO EFFECT ON ACCURACY

The following subroutines do not materially affect the accuracy of the results, either because of the simple nature of the computation or because they do not modify the data:

ABSNT	-- detection of missing data	GAUSS	-- normal random numbers
ARRAY	-- vector storage/double-dimensioned conversion	GMADD	-- add two general matrices
ATSE, DATSE	-- table selection out of an equidistant table	GMSUB	-- subtract two general matrices
ATSG, DATSG	-- table selection out of a general table	GMTRA	-- transpose of a general matrix
ATSM, DATSM	-- table selection out of a monotonic table	KOLM2	-- Kolmogorov - Smirnov two-sample test
AVDAT	-- data storage allocation	KRANK	-- Kendall rank correlation
BISER	-- biserial correlation coefficient	LOC	-- location in compressed-stored matrix
BOUND	-- selection of observations within bounds	MADD	-- add two matrices
CADD	-- add column of one matrix to column of another matrix	MCPY	-- matrix copy
CCPY	-- copy column of matrix into vector	MFUN	-- matrix transformation by a function
CCUT	-- partition by column	MOMEN	-- first four moments
CHISQ	-- χ^2 test for a contingency table	MPAIR	-- Wilcoxin's signed rank test
CINT	-- interchange two columns	MPRC, DMPCRC	-- permutations of rows or columns of a matrix
CONVT	-- single-precision/double-precision conversion	MSTR	-- storage conversion
CSRT	-- sort matrix columns	MSUB	-- subtract two matrices
CSUM	-- sum the columns of a matrix	MTRA	-- transpose a matrix
CTAB	-- tabulate the columns of a matrix	ORDER	-- rearrangement of intercorrelations
CTIE	-- adjoin two matrices by column	PADD	-- add two polynomials
DCLA	-- replace diagonal with scalar	PADDM	-- multiply polynomial by constant and add to another polynomial
DCPY	-- copy diagonal of matrix into vector	PCLA	-- replace one polynomial by another
FRAT, DFRAT	-- used with ARAT used with DARAT	PERM	-- inverse of permutation - transposition
		PHI	-- phi coefficient
		PMPY	-- multiply two polynomials
		PNORM	-- normalize coefficient vector of polynomial
		PPRCN	-- operations with permutations
		PSUB	-- subtract one polynomial from another
		PVSUB	-- substitute variable of polynomial by another polynomial
		QTEST	-- Cochran Q-test
		RADD	-- add row of one matrix to row of another matrix
		RANDU	-- uniform random numbers
		RANK	-- rank observations
		RCPY	-- copy row of matrix into vector
		RCUT	-- partition by row

RECP -- reciprocal function for MFUN
 RINT -- interchange two rows
 RSRT -- sort matrix rows
 RSUM -- sum the rows of a matrix
 RTAB -- tabulate the rows of a matrix
 RTIE -- adjoin two matrices by row
 SADD -- add scalar to matrix
 SCLA -- matrix clear and add scalar
 SCMA -- scalar-multiply column and add to another column
 SDIV -- matrix divided by a scalar
 SIGNT -- sign test
 SMPY -- matrix multiplied by a scalar
 SRANK -- Spearman rank correlation
 SRATE -- survival rate
 SRMA -- scalar-multiply row and add to another row
 SSUB -- subtract scalar from a matrix
 SUBMX -- build subset matrix
 SUBST -- subset selection from observation matrix
 TAB1 -- tabulation of data (one variable)
 TAB2 -- tabulation of data (two variables)
 TIE -- calculation of ties in ranked observations
 TRACE -- cumulative percentage of eigenvalues
 TTEST -- tests on population means
 TWOAV -- Friedman two-way analysis of variance
 UTEST -- Mann-Whitney U-test
 WTEST -- Kendall coefficient of concordance
 XCPY -- copy submatrix from given matrix

SUBROUTINES WHOSE ACCURACY IS DATA-DEPENDENT

The accuracy of the following subroutines cannot be predicted because it is dependent on the characteristics of the input data and on the size of the problem. The programmer using these subroutines must be aware of the limitations dictated by numerical analyses considerations. It cannot be assumed that the results are accurate simply because subroutine execution is completed. Subroutines in this category are:

ACFI, -- continued fraction interpolation
 DACFI
 AHI, -- Aitken-Hermite interpolation
 DAHI
 ALI, -- Aitken-Lagrange interpolation
 DALI
 APCH, -- construction of normal equations for a polynomial least-squares fit to a tabulated function
 DAPCH
 APFS, -- solution of normal equations for least-squares fit
 DAPFS
 APLL, -- construction of normal equations for least-squares fit to tabulated function
 DAPLL
 APMM, -- Chebyshev approximation of tabulated functions
 DAPMM
 ARAT, -- least-squares rational approximation of tabulated functions
 DARAT
 ATEIG -- eigenvalues of a real Hessenberg matrix
 AUTO -- autocovariances
 AVCAL -- Σ and Δ operation
 CANOR -- canonical correlation
 CNPS, -- value of series expansion in Chebyshev polynomials
 DCNPS
 CORRE -- means, standard deviations, and correlations
 CROSS -- cross covariances
 CSPS, -- value of series expansion in shifted Chebyshev polynomials
 DCSPS
 DBAR, -- first derivative of a function at the border of the definition interval
 DDBAR
 DCAR, -- first derivative of a function at the center of the definition interval
 DDCAR
 DET3, -- differentiation of equidistantly tabulated functions using three points interpolation
 DDET3

DET5, -- differentiation of equidistantly tabulated	LBVP, -- solution of system of linear first-order
DDET5 functions using five points interpolation	DLBVP ordinary differential equations with
DGT3, -- differentiation of tabulated functions	linear boundary conditions by method
DDGT3 using three points interpolation	of adjoint equations
DISCR -- discriminant functions	LEPS, -- value of series expansion in Legendre
DMATX -- means and dispersion matrix	DLEPS polynomials
EIGEN -- eigenvalues and eigenvectors of a real,	LLSQ, -- solution of linear least-squares
symmetric matrix	DLLSQ problems
EXSMO -- triple exponential smoothing	LOAD -- factor loading
FACTR -- factorization of a matrix into a product	MCHB, -- factorization of a symmetric positive
of triangular matrices	DMCHB definite band matrix
FMCG, -- unconstrained minimum of a function of	MATA -- transpose product of a matrix
DFMCG several variables--conjugate gradient	MEANQ -- mean square operation
method	MFGR, -- matrix factorization and rank determina-
FMFP, -- unconstrained minimum of a function of	DMFGR tion
DFMFP several variables--Davidon method	MFSD, -- factorizes a symmetric positive definite
FORIF -- Fourier analysis of a given function	DMFSD matrix (square root method)
FORIT -- Fourier analysis of a tabulated function	MFSS, -- rank determination and factorization of
GDATA -- data generation	DMFSS symmetric positive semidefinite matrix
GELB, -- system of general simultaneous linear	MINV -- matrix inversion
DGELB equations with band-structured	MISR -- missing value correlations
coefficients	MLSS, -- solve a system of linear equations with
GELG, -- system of general simultaneous linear	DMLSS symmetric positive semidefinite matrix
DGELG equations by Gauss elimination	MPRD -- matrix product
GELS, -- system of general simultaneous linear	MTDS, -- division of a matrix by a triangular matrix
DGELS equations with symmetric coefficients	DMTDS
GMPRD -- product of two general matrices	MULTR -- multiple regression and correlation
GTPRD -- transpose product, general matrices	NROOT -- eigenvalues and eigenvectors of a special
HARM, -- complex three-dimensional analysis	nonsymmetric matrix
DHARM	PCLD -- complete linear division
HEPS, -- value of series expansion in Hermite	PDER -- derivative of a polynomial
DHEPS polynomials	PDIV -- divide polynomials
HPCG, -- solution of general system of first-order	PECN, -- economization of a polynomial for
DHPCG ordinary differential equations with	DPECN symmetric range
given initial values by Hamming's	PECS, -- economization of a polynomial for
modified predictor-corrector method	DPECS unsymmetric range
HPCL, -- solution of linear system of first-	PFQB, -- determination of a quadratic factor of a
DHPCL order ordinary differential equations	DPFQB polynomial
with given initial values by Hamming's	PGCD -- greatest common divisor of two poly-
modified predictor-corrector method	nomials
HSBG -- reduction of a real matrix to	PILD -- evaluate polynomial and its first deriva-
Hessenberg form	tive
KOLMO -- Kolmogorov-Smirnov one-sample test	PINT -- integral of a polynomial
LAPS, -- value of series expansion in Laguerre	POINT -- point biserial correlation
DLAPS	

POLRT	-- real and complex roots of a real polynomial	RKI	-- solution of first-order differential equation by Runge-Kutta method
PQSD	-- quadratic synthetic division of a polynomial	RK2	-- tabulated solution of first-order differential equation by Runge-Kutta method
PRBM, DPRBM	-- roots of a polynomial with real coefficients--Bairstow's method	RKGS, DRKGS	-- solution of system of first-order ordinary differential equations with given initial values by the Runge-Kutta method
PROBT	-- probit analysis	RSLMC	-- solution of a system of linear equations
PRQD, DPRQD	-- roots of a real polynomial by QD algorithm with displacement	RTMI, DRTMI	-- determine root within a range by Mueller's iteration
PVAL	-- evaluate polynomial	RTNI, DRTNI	-- refine estimate of root by Newton's iteration
QA2- QA10, DQA4- DQA32	-- integration of a given function by associated Gaussian-Laguerre quadrature formulas	RTWI, DRTWI	-- refine estimate of root by Wegstein's iteration
QATR, DQATR	-- integration of a given function by trapezoidal rule together with Romberg's extrapolation method	SE13, DSE13	-- local least-squares smoothing of equidistantly tabulated functions
QG2- QG10, DQG4- DQG32	-- integration of a given function by Gaussian quadrature formulas	SE15, DSE15	local least-squares smoothing of equidistantly tabulated functions
QH2 QH10, DQH8- DQH64	-- integration of a given function by Gaussian - Hermite quadrature formulas	SE35, DSE35	-- local least-squares smoothing of equidistantly tabulated functions
QHFE, DQHFE	-- integration of equidistantly tabulated function with first derivative by Hermitian formula of first order	SG13, DSG13	-- local least-squares smoothing of tabulated functions
QHFG, DQHFG	-- integration of monotonically tabulated function with first derivative by Hermitian formula of first order	SIMQ	-- solution of simultaneous linear, algebraic equations
QHSG, DQHSG	-- integration of monotonically tabulated function with first and second derivatives by Hermitian formula of first order	SINV, DSINV	-- inversion of a symmetric positive definite matrix
QHSE, DQHSE	-- integration of equidistantly tabulated function with first and second derivatives by Hermitian formula of second order	SMO	-- application of filter coefficients (weights)
QL2- QL10, DQL4- DQL32	-- integration of a given function by Gaussian-Laguerre quadrature formulas	STPRG	-- stepwise regression
QSF, DQSF	-- integration of equidistantly tabulated function by Simpson's rule	TALLY	-- totals, means, standard deviations, minimums, and maximums
QTFE, DQTFE	integration of equidistantly tabulated function by trapezoidal rule	TCNP, DTCNP	-- transform series expansion in Chebyshev polynomials to a polynomial
QTFG, DQTFG	-- integration of monotonically tabulated function by trapezoidal rule	TCSP, DTCSP	-- transform series expansion in shifted Chebyshev polynomials to a polynomial
RHARM, DRHARM	-- real one-dimensional analysis	TETRA	-- tetrachoric correlation
		THEP, DTHEP	-- transform series expansion in Hermite polynomials to a polynomial
		TLAP, DTLAP	-- transform series expansion in Laguerre polynomials to a polynomial
		TLEP, DTLEP	-- transform a series expansion in Legendre polynomials to a polynomial
		TPRD	-- transpose product
		VARMX	-- varimax rotation

SUBROUTINES WITH DEFINITE ACCURACY CHARACTERISTICS

The subroutines in this section have accuracy characteristics that can be specified on an individual basis. The mathematical descriptions for many of these subroutines contain information on truncation error of a strictly theoretical nature. The actual implementation of these subroutines on System/360 results in the accuracy noted in Table 1. The standard reference for comparing the accuracy of these subroutines is M. Abramowitz, I. A. Stegun, Handbook of Mathematical Functions, National Bureau of Standards, Washington, D. C., March 1965. However, in certain cases, other tables were used, as noted below. It should be remembered that in System

/360 single-precision floating point, there are just over six significant figures.

Maximum differences below are given in terms of number of decimal places (D. P.) and/or number of significant digits (S. D.) which agree. The number of digits tabled should be considered when accuracy statements are viewed; that is, certain tables are given to only five places, whereas the algorithms used may be more accurate. In compiling maximum differences, the maximum was taken over the set of points indicated in the table. The average difference was normally much smaller.

The notation $x = a (b) c$ implies that $a, a + b, a + 2b, \dots, c$ were the arguments (x) used.

TABLE 1

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
BDTR	$p = I_x^{-1}(a, b)$	$I_x^{-1}(a, b)$ Tables by Leon H. Harter: New Tables of the Incomplete Gamma Function Ratio and of Percentage Points of the χ^2 and Beta Distribution, 1964	$p = .0001, .0005$ $a = 1 (1) 40$ $b = 5(5) 40$ $p = .0100, .0500$ $a = 2 (2) 10$ $b = 5 (5) 30$	correct to 5 D. P.
		"t" distribution: $t(x, n) = [1 + I_z(c, d)] / 2$ where $z = x^2 / (x^2 + n)$ $c = 1/2$ $d = n/2$ Tables: Biometrika vol. 1	$x = .01, \text{ and}$ $x = .5 (.5) 4$ for $n = 1 (1) 24, \text{ and}$ $n = 30, 40, 60, 120$.5 in 5th D. P.

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
BESJ J Bessel function Parameter D=1 · E - 6	$J_n(x)$	$J_n(x)$	n=0(1)2 x=0(0.2)17.4 n=3(1)9 x=0(0.2)20 n=10(1)11 x=10(0.2)20 n=0(1)20 20(10)50 100 x=1,2,5,10,50, 100	2 in 5th S. D. 1 in 5th S. D. for $J_n(x) > 1.0$ exact to 5 D. P. for $J_n(x) < 1.0$ (limit of table) 3 in 5th S. D. 2 in 5th S. D.
BESK K Bessel function	$K_n(x)$	$e^x K_n(x)$ $e^x K_n(x)$ $K_n(x)$	n=0(1)2 x=0.2(0.2)20 n=3(1)9 x=0.2(0.2)10 =10(1.0)20 n=0(1)20 x=1,2,5,10 20(10)50 50,100 100	1 in 6th S. D. 1 in 5th S. D. 2 in 5th S. D.
BESY Y Bessel function	$Y_n(x)$	$Y_n(x)$	n=0(1)2 x=0.2(0.2)17.4 n=3(1)9 x=0.2(0.2)20 n=10 x=10(0.2)20 n=0(1)20 20(10)50 100 x=1,2,5,10,50,100	3 in 5th S. D. 1 in 5th S. D. for $Y_n(x) > 1.0$ exact to 5 D. P. for $Y_n(x) < 1.0$ (limit of table) 3 in 5th S. D. 1 in 5th S. D.
CDTR	y = P _g (x) where P is the χ^2 distribution function with para- meter g.	y = P _g (x)	x=.001(.001).01; .01(.01)1.0; 1.0(.1)2.0; 2.0(.2)10.0; 10.0(.5)20.0; 20(1)40 40(2)76 for g=1(1)30	1 in the 5th D. P.

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
CEL1 Complete elliptic 1st integral	K(k)	K(m); $k = \sqrt{m}$ K(α); $k = \sin \alpha$ (α in degrees)	m = .01 (.01).99 $\alpha = 1(1)73$ $\alpha = 74(1)86$	2 in 7th S. D. 2 in 7th S. D. 3 in 7th S. D.
DCEL1 Complete elliptic 1st integral	K(k)	K(m); $k = \sqrt{m}$ K(α); $k = \sin \alpha$ (α in degrees)	m = .01(.01).86 m = .87(.01).96 m = .97(.01).99 $\alpha = 1(1)75$ $\alpha = 76(1)80$ $\alpha = 81(1)86$	1 in 16th S. D. 4 in 16th S. D. 11 in 16th S. D. 1 in 16th S. D. 2 in 16th S. D. 11 in 16th S. D.
CEL2 Generalized complete elliptic 2nd integral	K(k) with A = B = 1 E(k) with A = 1 B = 1 - k ²	K(m); $k = \sqrt{m}$ K(α); $k = \sin \alpha$ (α in degrees) E(m); $k = \sqrt{m}$ E(α); $k = \sin \alpha$ K'E + E'K - KK' (Legendre's relation)	m = .01(.01).99 $\alpha = 1(1)73$ $\alpha = 74(1)86$ m = .01(01) $\alpha = 1(1)86$ m = .01(.01).99 $\alpha = 1(1)89$	2 in 7th S. D. 2 in 7th S. D. 3 in 7th S. D. 2 in 7th S. D. 2 in 7th S. D. 7 in 7th S. D. 1 in 6th S. D.
DCEL2 Generalized complete elliptic 2nd integral	K(k) with A = B = 1 E(k) with A = 1 B = 1 - k ²	K(m); $k = \sqrt{m}$ K(α); $k = \sin \alpha$ (α in degrees) E(α); $k = \sin \alpha$ K'E + E'K - KK' (Legendre's relation)	m = .01(.01).99 $\alpha = 1(1)80$ $\alpha = 81(1)86$ $\alpha = 1(1)89$ m = .01(.01).99 $\alpha = 1(1)89$	2 in 16th S. D. 2 in 16th S. D. 11 in 16th S. D. 2 in 16th S. D. 9 in 16th S. D. 9 in 16th S. D.
CNP Chebyshev polynomials	T _n (x)	T _n (x) n = 0(1)12 T _n (x) n = 0(1)50	x = .0(.2)1.0 x = .00(.05)1.00	1 in 5th D. P. 6 in 5th D. P. +

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
DCNP Chebyshev polynomials	$T_n(x)$	$T_n(x)$ $n = 0(1)12$	$x = .0(.2)1.0$	No error in 10th D. P.
CS Fresnel integrals	$C_2(u)$ $S_2(u)$ with $u = \frac{\pi}{2} x^2$	$C_2(u)$ $S_2(u)$	$x = .02(.02).78$ $0 < u < 1$ $x = .80(.02)1.58$ $1 < u < 4$ $x = 1.60(.02)5.00$ $4 < u < 40$ $x = .02(.02).78$ $0 < u < 1$ $x = .80(.02)1.58$ $1 < u < 4$ $x = 1.60(.02)5.00$ $4 < u < 40$	1 in 7th D. P. 6 in 7th S. D. 2 in 7th S. D. 1 in 7th D. P. 8 in 7th S. D. 2 in 7th S. D.
CSP Shifted Chebyshev polynomials	$T_n^*(x)$	$T_n^*(x) = T_n(2x - 1)$ $n = 0(1)12$ $T_n^*(x)$ $n = 0(1)50$	$x = .5(.1)1.0$ $x = .00(.05)1.00$	2 in 5th D. P. 7 in 5th D. P. +
DCSP Shifted Chebyshev polynomials	$T_n^*(x)$	$T_n^*(x) = T_n(2x - 1)$ $n = 0(1)12$	$x = .5(.1)1.0$	No error in 10th D. P.
DLGAM (log of the gamma function)	$\ln \Gamma(x)$	$\ln \Gamma(x)$ $\log_{10} \Gamma(x)$	$x=1$ $x=1.005(.005)$ 1.025 $x=1.980(.005)$ 1.995 $x=1.03(.01)1.31$ $x=1.32(.01)1.67$ $x=1.68(.01)1.97$ $x=2$ $x=3.0(1.0)100.0$	6 in 9th D. P. 9 in 8th D. P. 9 in 8th S. D. 8 in 9th S. D. 8 in 10th S. D. 7 in 9th S. D. 6 in 9th S. D. No error in 8 place tables

+ Differences between results of single- and double-precision routines

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
ELI1 Incomplete elliptic 1st integral	$F(\zeta/\alpha)$ with $x = \tan \zeta$ $k = \frac{\sin \alpha}{\sqrt{1-k^2}}$ $ck = \sqrt{1-k^2}$	$F(\zeta/\alpha)$ $(\zeta, \alpha \text{ in degrees})$	$\zeta = 0(5)10$ $\alpha = 0(2)90$ $\zeta = 15(5)35$ $\alpha = 0(2)90$ $\zeta = 40(5)50$ $\alpha = 0(2)90$ $\zeta = 55(5)85$ $\alpha = 0(2)90$	2 in 7th D. P. 7 in 7th S. D. 11 in 7th D. P. 3 in 7th S. D.
DELI1 Incomplete elliptic 1st integral	$F(\varphi/\alpha)$ with $x = \tan \varphi$ $k = \frac{\sin \alpha}{\sqrt{1-k^2}}$ $ck = \sqrt{1-k^2}$	$F(\varphi/\alpha)$ $(\varphi, \alpha \text{ in degrees})$ $F(\varphi/\alpha) + F(\psi/\alpha)$ $= F\left(\frac{\pi}{2}/\alpha\right)$ $(\varphi, \alpha, \psi \text{ in degrees})$	$\varphi = 0(5)85$ $\alpha = 0(2)90$ $\varphi = 0(5)85$ $\alpha = 0(2)80$ $\psi = \text{Arctan } f$ $f = 1/(\cos \alpha \cdot \tan \varphi)$	1 in 9th D. P. (probably due to rounding errors in table) 2 in 15th D. P.
ELI2 Generalized incomplete 2nd integral	$F(\zeta/\alpha)$ with $A = B = 1$ $E(\zeta/\alpha)$ with $A = 1$ and $B = 1 - k^2$ $x = \tan \zeta$ $k = \frac{\sin \alpha}{\sqrt{1-k^2}}$ $ck = \sqrt{1-k^2}$	$F(\zeta/\alpha)$ $(\zeta, \alpha \text{ in degrees})$ $E(\zeta/\alpha)$ $(\zeta, \alpha \text{ in degrees})$	$\zeta = 0(5)10$ $\alpha = 0(2)90$ $\zeta = 15(5)35$ $\alpha = 0(2)90$ $\zeta = 40(5)50$ $\alpha = 0(2)90$ $\zeta = 55(5)85$ $\alpha = 0(2)90$ $\zeta = 0, 5$ $\alpha = 0(2)90$ $\zeta = 10(5)35$ $\alpha = 0(2)90$ $\zeta = 40(5)55$ $\alpha = 0(2)90$ $\zeta = 60(5)85$ $\alpha = 0(2)90$	2 in 7th D. P. 7 in 7th S. D. 11 in 7th D. P. 3 in 7th S. D. 2 in 7th D. P. 7 in 7th S. D. 12 in 7th D. P. 36 in 7th D. P.

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
DELI2 Generalized incomplete elliptic 2nd integral	$F(\varphi/\alpha)$ with $A = B = 1$ $E(\varphi/\alpha)$ with $A = 1$ $B = 1 - k^2$ and $x = \tan \varphi$ $k = \sin \alpha$ $ck = \sqrt{1 - k^2}$	$F(\varphi/\alpha)$ ($\varphi, / \alpha$ in degrees) $E(\varphi/\alpha)$ (φ, α in degrees) $E(\varphi/\alpha) + E(\psi/\alpha)$ $= E\left(\frac{\pi}{2}/\alpha\right) + \sin^2 \alpha \sin \phi$ $\sin \psi$ (φ, α in degrees) $F(\varphi/\alpha) + F(\psi/\alpha)$ $= F\left(\frac{\pi}{2}/\alpha\right)$ (φ, α in degrees)	$\varphi = 0(5)85$ $\alpha = 0(2)90$ $\varphi = 0(5)85$ $\alpha = 0(2)90$ $\varphi = 0(5)85$ $\alpha = 0(2)90$ $\psi = \text{Arctan } f$ $f = 1/(\cos \alpha \cdot \tan \varphi)$ $\varphi = 0(5)85$ $\alpha = 0(2)82$ $\psi = \text{Arctan } f$ $f = 1/(\cos \alpha \cdot \tan \varphi)$	1 in 9th D. P. (probably due to rounding errors in table) 1 in 9th D. P. (probably due to rounding errors in table) 2 in 15th D. P. 3 in 15th D. P.
EXPI Exponential integral	$-E_1(-x)$ when $x < 0$ $E_1(x)$ when $x > 0$	$(E_1(x) + \ln x + \gamma)/x$ $E_1(x)$ $xe^xE_1(x)$ $(-E_1(-x) + \ln x + \gamma)/x$ $-E_1(-x)$ $-xe^xE_1(-x)$	$x = .01(.01).50$ $x = .50(.01)1.00$ $x = 1.00(.01)2.00$ $x = 2.0(.1)4.0$ $x = 4.0(.1)10.0$ $x = -.01(-.01)-.50$ $x = -.50(.01)-1.00$ $x = -1.00(-.01)-2.00$ $x = -2.0(-.1)-4.0$	1 in 7th S. D. 4 in 7th S. D. 7 in 7th S. D. 2 in 4th S. D. 2 in 7th S. D. 1 in 7th S. D. 3 in 7th S. D. 4 in 7th S. D. 4 in 6th S. D.
GMMMA Gamma function	$\tau(x)$	$\tau(x)$	$x = 1.0(0.005)2.0$ $x = 1.0(1.0)57.0$	3 in 6th S. D. 6 in 6th S. D.
HEP Hermite polynomials	$H_n(x)$	$H_n(x)$ $n = 0(1)12$ $H_n(x)$ $n = 0(1)50$	$x = 0.5, 1, 3, 5, 10$ $x = 0.0(.1)1.0$ $x = 1(1)10$	Maximum relative error $2 \cdot 10^{-7}$ Maximum relative error $3 \cdot 10^{-5+}$

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
DHEP Hermite polynomials	$H_n(x)$	$H_n(x)$ $n = 0(1)12$	$x = 0.5, 1, 3, 5, 10$	No error in 11th S. D.
I0	$I_0(x)$		$x = [1 (1) 20]$ (500 random numbers applied per unit interval)	1.2 in 6th D. P.
INUE	$I_n(x)$ $n = 1, 2, \dots, 10$		$x = [1 (1) 20]$ (500 random argu- ments per unit interval)	5.5 in 6th D. P.
JELF Jacobian elliptic functions	$\operatorname{sn} u = \sin \varphi$ $\operatorname{cn} u = \cos \varphi$ $\operatorname{dn} u = \sqrt{1-k^2 \sin^2 \varphi}$ with $\varphi = \operatorname{am} u$ or $u = F(\varphi/\alpha)$, $k = \sin \alpha$ $\operatorname{sck} = 1 - k^2$	$\operatorname{sn} u = \sin \varphi$ (φ, α in degrees) $\operatorname{cn} u = \cos \varphi$ (φ, α in degrees) $\operatorname{dn} u = \sqrt{1-k^2 \sin^2 \varphi}$ (φ, α in degrees) $\operatorname{sn} u$ $\operatorname{cn} u$ $\operatorname{dn} u$ $\operatorname{sn} u - \operatorname{sn}(2K-u)$ $\operatorname{sn} u + \operatorname{sn}(2K + u)$ $\operatorname{sn} u + \operatorname{sn}(4K - u)$ $\operatorname{cn} u + \operatorname{cn}(2K - u)$ $\operatorname{cn} u + \operatorname{cn}(2K + u)$ $\operatorname{cn} u - \operatorname{cn}(4K - u)$ $\operatorname{dn} u - \operatorname{dn}(2K - u)$ $\operatorname{dn} u - \operatorname{dn}(2K + u)$ $\operatorname{dn} u - \operatorname{dn}(4K - u)$	$\varphi = 0(1)89$ $\alpha = 0(5)85$ $\varphi = 0(1)89$ $\alpha = 0(5)85$ $\varphi = 0(1)89$ $\alpha = 0(5)85$ $k^2 = .00(.05).95$ $t = 0(1)25$ $u = t. K(k)/25$ $k^2 = .00(.05).95$ $t = 0(1)25$ $u = t. K(k)/25$ $k^2 = .00(.05).95$ $t = 0(1)25$ $u = t. K(k)/25$ $k^2 = .00(.05).90$ $t = 0(1)25$ $u = t. K(k)/25$ $k^2 = .00(.05).90$ $t = 0(1)25$ $u = t. K(k)/25$ $k^2 = .00(.05).90$ $t = 0(1)25$ $u = t. K(k)/25$	1 in 6th D. P. + 2 in 6th D. P. + 1 in 6th D. P. + 1 in 6th D. P. ++ 2 in 6th D. P. ++ 1 in 6th D. P. ++ 6 in 6th D. P. 6 in 6th D. P. 10 in 6th D. P. 4 in 6th D. P. 4 in 6th D. P. 6 in 6th D. P. 3 in 6th D. P. 3 in 6th D. P. 5 in 6th D. P.

+ Calculation of $\mu = f(\varphi/\alpha)$ with double-precision subroutine

++ Difference between result of single- and double-precision routines

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
DJELF	sn u = sin φ	sn u = sin φ (φ, α in degrees)	$\varphi = 5(5)85$ $\alpha = 0(2)90$	2 in 15th D. P. +
Jacobian elliptic functions	cn u = cos φ	cn u = cos φ (φ, α in degrees)	$\varphi = 5(5)85$ $\alpha = 0(2)90$	3 in 15th D. P. +
	dn u = $\sqrt{1 - k^2 \alpha}$ ($\alpha = \sin^2 \varphi$ with $\varphi = \text{am } u$ $u = F(\varphi/\alpha)$ $k = \sin \alpha$ $sck = 1 - k^2$)	dn u = $\sqrt{1 - k^2 \sin^2 \varphi}$ (φ, α in degrees)	$\varphi = 5(5)85$ $\alpha = 0(2)90$	2 in 15th D. P. +
		sn u - sn(2K - u)	$k^2 = .00(.05).90$ $t = 0(1)25$	5 in 15th D. P.
		sn u + sn(2K + u)	$u = t.K(k)/25$	5 in 15th D. P.
		sn u + sn(4K - u)		12 in 15th D. P.
		cn u + cn(2K - u)	$k^2 = .00(.05).90$ $t = 0(1)25$	3 in 15th D. P.
		cn u + cn(2K + u)	$u = t.K(k)/25$	3 in 15th D. P.
		cn u - cn(4K - u)		7 in 15th D. P.
		dn u - dn(2K - u)	$k^2 = .00(.05).90$ $t = 0(1)25$	3 in 15th D. P.
		dn u - dn(2K + u)	$u = t.K(k)/25$	2 in 15th D. P.
	dn u - dn(4K - u)		6 in 15th D. P.	
LAP Laguerre polynomials	$L_n(x)$	$L_n(x)$ $n = 0(1)12$ $L_n(x)$ $n = 0(1)50$	$x = 0.5, 1, 3$ $x = 5, 10$ $x = 0.0(.1)1.0$ except arguments with $L_n(x) < 0.1$ $x = 1(1)10$ except arguments with $L_n(x) < 0.1$	2 in 6th D. P. 1 in 5th S. D. Maximum relative error $4 \cdot 10^{-6} + +$ Maximum relative error $1 \cdot 10^{-5} + +$
DLAP Laguerre polynomials	$L_n(x)$	$L_n(x)$ $n = 0(1)12$	$x = 0.5, 1, 3, 5, 10$	No error in 10th D. P.

+ Calculation of $\mu = F(\varphi/\alpha)$ with double-precision routine

++ Difference between results of single- and double-precision routines

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
LEP Legendre polynomials	$P_n(x)$	$P_n(x)$ $n = 0, 1, 2, 3, 9, 10$ $P_n(x)$ $n = 0(1)50$	$x = .00(.05)1.00$ $x = .00(.05)1.00$	1 in 6th D. P. 5 in 6th D. P. +
DLEP Legendre Polynomials	$P_n(x)$	$P_n(x)$ $n = 0, 1, 2, 3, 9, 10$	$x = .00(.05)1.00$	No error in 8th D. P.
NDTR	$y = P(x)$ $P = \text{normal}$ pdf.	$y = P(x)$	$x = -6(.01)6$	7 in 7th D. P.
NDTRI	$x = P^{-1}(y)$ $p = \text{normal}$ pdf.	$x = P^{-1}(y)$	$y = .01(.01).99$	5 in 4th D. P.
SICI SINE integral and cosine integral	$s_i(x)$ $c_i(x)$	$s_i(x)/x$ $s_i(x)$ $-(c_i(x) - \ln x - \gamma)/x^2$ $c_i(x)$	$x = .01(.01).50$ $x = .50(.01)2.00$ $x = 2.0(.1)10.0$ $x = .01(.01).50$ $x = .50(.01)1.50$ $x = 1.50(.01)2.00$ $x = 2.0(.1)4.0$ $x = 4.0(.1)10.0$	1 in 7th S. D. 1 in 7th S. D. 1 in 7th S. D. 1 in 7th S. D. 2 in 7th S. D. 1 in 6th S. D. 2 in 6th D. P. 1 in 7th D. P.

+Difference between results of single- and double-precision routines.

Name	Functions calculated	Functions checked with reference	Range checked with reference	Maximum difference
SMIRN Kolmogorov-Smirnov limiting distribution	L(x)	L (x); Tables by N. Smirnov, reprinted in Annals of Math. Stat. 19, pp. 280-281 (6- and 7- place tables). Double-precision version differences are given in parentheses in the right-hand column.	x = 0(.01) .61 x = .62 x = .63 (.01) 1.04 x = 1.05(.01)1.15 x = 1.16(.01) 1.20 x = 1.21 (.01) 1.45 x = 1.46(.01) 1.65 x = 1.66(.01) 1.86 x = 1.87 x = 1.88 (.01) 2.04 x = 2.05 (.01) 2.50 x = 2.51 (.01) 3.5	1 in 6 th D. P. (1 in 6 th D. P.) 3 in 5 th D. P. (see program comments) (3 in 5 th D. P.) 3 in 6 th D. P. (2 in 6 th D. P.) 6 in 6 th D. P. (2 in 6 th D. P.) 9 in 6 th D. P. (2 in 6 th D. P.) 8 in 6 th D. P. (3 in 6 th D. P.) 6 in 6 th D. P. (1 in 6 th D. P.) 2 in 6 th D. P. (0 in 6 th D. P.) 2 in 5 th D. P. (2 in 5 th D. P.) 2 in 6 th D. P. (1 in 6 th D. P.) 1 in 6 th D. P. (1 in 6 th D. P.) 2 in 7 th D. P. (1 in 7 th D. P.)

APPENDIX B: SAMPLE PROGRAM DESCRIPTIONS

DATA SCREENING

Problem Description

A set of observations is read along with information on propositions to be satisfied and limits on a selected variable. From this input a subset is obtained and a histogram of frequency over given class intervals is plotted for the selected variable. Total, average, standard deviation, minimum, and maximum are calculated for the selected variable. This procedure is repeated until all sets of input data have been processed.

Program

Description

The data screening sample program consists of a main routine, DASC, and six subroutines; namely, SUBST, TAB1, LOC, BOOL, HIST, and MATIN. Three of these (SUBST, TAB1, LOC) are from the Scientific Subroutine Package. MATIN is a sample input routine. HIST is a program for plotting a histogram. For a description of subroutine BOOL see subroutine SUBST.

Capacity

The maximum size of matrix of observations has been set at 1000 elements, the number of observations at 200, and the number of conditions at 21. All of these can be increased as described under "Program Modification" below.

Input

Control Cards

A parameter card with the following format must precede each matrix of observations:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem</u>
1 - 2	Blank	
3 - 6	Up to four-digit identification code (numeric only)	0001
7 - 10	Number of observations	0100
11 - 14	Number of variables	0004

Each matrix of observations must be followed by a card with a 9 punch in column 1. The condition matrix and bounds data are preceded by a card

containing the number of conditions and the variable to be selected for analysis:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem</u>
1 - 2	Number of conditions	02
3 - 4	Variable to be selected	03

A blank card after the last set of input data terminates the run.

Data Cards

1. For the observation matrix--data cards have seven fields of ten columns each. The decimal point may appear anywhere in a field. If no decimal point is included, it is assumed that the decimal point is to the right of the last digit. The number in each field may be preceded by blanks. All values for an observation are punched consecutively and may continue from card to card. However, a new observation must start in the first field of the next card.

2. For the condition matrix (see description in the subroutine SUBST)--each ten-column field contains a condition to be satisfied. The first two columns contain the variable number (right-justified), the third column the relational code, and the last seven columns of each field a floating-point number. This number may be punched anywhere in the seven-column field but must contain a decimal point. There may be as many as seven conditions per card and a total of three cards or 21 conditions.

3. For the UBO vector (see description in the subroutine TAB1)--the UBO vector is punched in three fields of ten columns each as a floating-point number with decimal point.

Deck Setup

The deck setup is shown in Figure 35.

Sample

A listing of input cards for the sample problem is presented in Figure 36. Card 002 is the parameter card for the matrix of observations. It shows that there are 100 observations and four variables in matrix number 1. Card 003 is the first observation, card 102 the last. Each observation represents an individual with four characteristics (variables). The variables are, in the order shown, (1) age in years, (2) height in inches, (3) weight in pounds, and (4) education in years.

Card 103 signals the end of the matrix of observations.

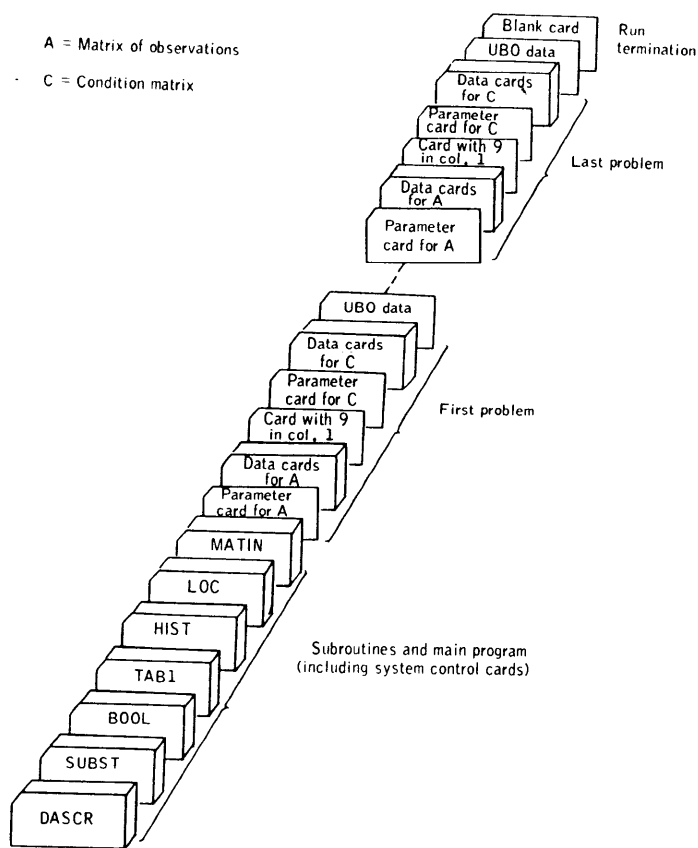


Figure 35. Deck setup (data screening)

Card 104 indicates that there are two conditions to be satisfied and that variable 3 (weight) is selected for analysis. Card 105 shows the condition matrix. The first condition states that variable 1 (age) must be less than or equal to 65, and therefore observations for individuals over 65 will be rejected. The second condition states that variable 4 (education) must be greater than eight years, and consequently observations for individuals with less than eight years of education will be rejected.

Card 106 contains the information on bounds and number of intervals for the selected variable. It shows that the lower bound is 120, the upper bound is 210, and that there are 20 intervals (including one for under lower bound and another for equal to or greater than upper bound).

Card 107 is a blank card for terminating the run.

Output

Description

The output consists of the subset vector showing which observations are rejected (zero) and accepted

(nonzero), summary statistics for the selected variable, and a histogram of frequencies versus intervals for that variable.

Sample

The output listing for the sample problem is shown in Figure 37.

Program Modification

The size of the maximum problem to be solved can be increased or decreased by changing the DIMENSION statement in DASC.

Subroutine BOOL can be replaced if the user wishes to use a different boolean expression (see description in subroutine SUBST). The boolean expression provided in the sample program is for both conditions to be satisfied:

$$T = R(1) * R(2)$$

Operating Instructions

The sample program for data screening is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and logical unit 6 is used for output. Data set 13 is used for intermediate storage.

Error Messages

The following error conditions will result in messages:

1. Reserved storage area is too small for matrix--DIMENSIONED AREA TOO SMALL FOR INPUT MATRIX. GO ON TO NEXT CASE.
2. Number of data cards does not correspond to that required by parameter card--INCORRECT NUMBER OF DATA CARDS FOR MATRIX. EXECUTION TERMINATED.

Error condition 1 allows the computer run to continue. Error condition 2, however, terminates execution and requires another run to process succeeding cases.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 42 seconds.

```

/ DATA
00101000004
46. 64. 173. 12.
24. 72. 179. 8.
32. 71. 154. 16.
41. 68. 129. 10.
50. 65. 192. 9.
63. 75. 203. 12.
29. 79. 122. 14.
28. 64. 136. 13.
52. 77. 147. 11.
36. 67. 153. 18.
31. 68. 165. 9.
72. 70. 178. 10.
53. 71. 205. 14.
21. 65. 213. 12.
49. 63. 150. 6.
28. 62. 160. 16.
53. 72. 161. 13.
47. 73. 142. 15.
37. 67. 193. 18.
64. 58. 156. 14.
65. 60. 114. 10.
62. 64. 153. 12.
19. 68. 225. 9.
46. 67. 158. 11.
33. 72. 121. 4.
37. 55. 132. 13.
41. 76. 148. 16.
52. 71. 123. 16.
29. 68. 128. 14.
32. 65. 155. 17.
24. 72. 172. 16.
56. 73. 163. 10.
63. 65. 158. 11.
67. 69. 146. 2.
58. 66. 171. 9.
41. 65. 153. 12.
49. 66. 165. 14.
52. 72. 172. 16.
23. 78. 183. 15.
56. 71. 195. 16.
52. 68. 118. 7.
40. 66. 165. 14.
39. 68. 215. 16.
23. 71. 154. 12.
56. 65. 149. 10.
25. 65. 152. 16.
37. 68. 152. 16.
46. 70. 159. 15.
41. 69. 137. 14.
62. 71. 163. 12.
29. 72. 191. 4.
19. 68. 168. 10.
46. 63. 158. 16.
37. 64. 139. 18.
34. 68. 156. 10.
64. 67. 153. 12.
57. 67. 141. 13.
32. 68. 157. 17.
29. 70. 183. 15.
53. 72. 164. 18.
47. 72. 156. 18.
56. 73. 160. 16.
61. 74. 159. 12.
21. 68. 161. 10.
25. 76. 178. 11.
23. 72. 157. 16.
29. 68. 185. 16.
39. 70. 159. 14.
42. 70. 154. 10.
56. 62. 159. 12.
63. 70. 177. 12.
51. 71. 161. 9.
41. 66. 158. 10.
33. 69. 158. 16.
37. 68. 157. 16.
25. 70. 163. 15.
63. 68. 159. 12.
53. 71. 202. 6.
51. 72. 167. 14.
47. 73. 164. 14.
39. 75. 151. 12.
28. 68. 166. 10.
64. 59. 156. 16.
55. 67. 144. 16.
51. 66. 177. 10.
46. 55. 157. 12.
72. 66. 125. 10.
66. 65. 131. 12.
28. 74. 149. 18.
27. 71. 168. 11.
23. 72. 158. 12.
23. 72. 163. 12.
60. 66. 157. 9.
30. 66. 142. 10.
39. 67. 162. 16.
46. 74. 154. 16.
50. 68. 158. 10.
61. 66. 161. 14.
36. 64. 157. 15.
32. 71. 156. 16.
9
0203
12 65. 46 8.
120. 20. 210.

```

```

10
20
30
40
50
60
70
80
90
100
110
120
130
140
150
160
170
180
190
200
210
220
230
240
250
260
270
280
290
300
310
320
330
340
350
360
370
380
390
400
410
420
430
440
450
460
470
480
490
500
510
520
530
540
550
560
570
580
590
600
610
620
630
640
650
660
670
680
690
700
710
720
730
740
750
760
770
780
790
800
810
820
830
840
850
860
870
880
890
900
910
920
930
940
950
960
970
980
990
1000
1010
1020
1030
1040
1050
1060
1070

```

```

DATA SCREENING PROBLEM 1
SUBSET VECTOR
1 1.
2 0.0
3 1.
4 1.
5 1.
6 1.
7 1.
8 1.
9 1.
10 1.
11 1.
12 0.0
13 1.
14 1.
15 0.0
16 1.
17 1.
18 1.
19 1.
20 1.
21 1.
22 1.
23 1.
24 1.
25 0.0
26 1.
27 1.
28 1.
29 1.
30 1.
31 1.
32 1.
33 1.
34 0.0
35 1.
36 1.
37 1.
38 1.
39 1.
40 1.
41 0.0
42 1.
43 1.
44 1.
45 1.
46 1.
47 1.
48 1.
49 1.
50 1.
51 0.0
52 1.
53 1.
54 1.
55 1.
56 1.
57 1.
58 1.
59 1.
60 1.
61 1.
62 1.
63 1.
64 1.
65 1.
66 1.
67 1.
68 1.
69 1.
70 1.
71 1.
72 1.
73 1.
74 1.
75 1.
76 1.
77 1.
78 0.0
79 1.
80 1.
81 1.
82 1.
83 1.
84 1.
85 1.
86 1.
87 0.0
88 0.0
89 1.
90 1.
91 1.
92 1.
93 1.
94 1.
95 1.
96 1.
97 1.
98 1.
99 1.
100 1.

```

Figure 36. Input cards sample problem (data screening)

Figure 37. Output listing (data screening)

SUMMARY STATISTICS FOR VARIABLE 3

TOTAL = 14492.000 AVERAGE = 161.022 STANDARD DEVIATION = 19.329 MINIMUM = 114.000 MAXIMUM = 225.000

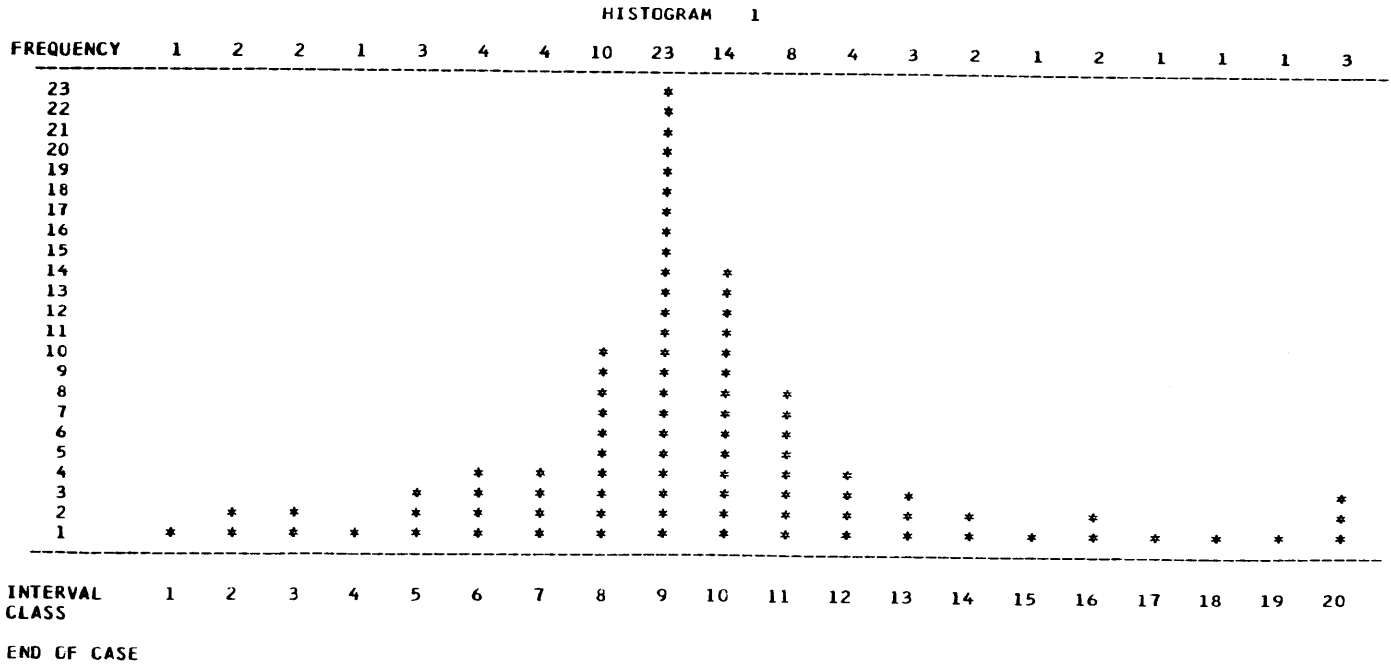


Figure 37. Output listing (data screening) (Continued)

```

C                                     DASC 10                               WRITE(6,10)KC                               DASC 610
C ..... DASC 20                               WRITE(6,11)                               DASC 620
C SAMPLE MAIN PROGRAM FOR DATA SCREENING - DASC R DASC 30                               WRITE(6,13) (I,S(I),I=1,NO)                UASC 630
C                                     DASC 40                               CALL TAB1(A,S,NOVAR,UBO,FREQ,PCT,STATS,NO,NV) DASC 640
C                                     DASC 50                               WRITE(6,20) NOVAR                          DASC 650
C PURPOSE DASC 60                               WRITE(6,21)(STATS(I),I=1,5)                DASC 660
C PERFORM DATA SCREENING CALCULATIONS ON A SET OF OBSERVATIONS DASC 70                               JZ=UBO(2)                                  DASC 67C
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DASC 80                               CALL HIST(KC,FREQ,JZ)                       DASC 680
C SUBST DASC 90                               WRITE(6,15)                                DASC 69C
C TAB1 DASC 100                              GO TO 24                                    DASC 700
C LOC DASC 110                              5C RETURN                                  DASC 710
C BOOL DASC 120                              END                                          DASC 720
C HIST DASC 130
C MATIN DASC 140
C METHOD DASC 150
C DERIVE A SUBSET OF OBSERVATIONS SATISFYING CERTAIN DASC 160
C CONDITIONS ON THE VARIABLES. FOR THIS SUBSET, THE FREQUENCY DASC 17C
C OF A SELECTED VARIABLE OVER GIVEN CLASS INTERVALS IS DASC 180
C OBTAINED. THIS IS PLOTTED IN THE FORM OF A HISTOGRAM. DASC 190
C TOTAL, AVERAGE, STANDARD DEVIATION, MINIMUM, AND MAXIMUM DASC 200
C ARE ALSO CALCULATED. DASC 210
C ..... DASC 220
C DIMENSION A(1000),C(63),UBO(3),S(200),R(21),FREQ(20), DASC 22C
C IPCT(2),STATS(5) DASC 230
C EXTENSAL BOOL DASC 240
C 10 FORMAT(1H1,22HDATA SCREENING PROGRAM,13) DASC 250
C 11 FORMAT(1H0,44HDIENSIONED AREA TOO SMALL FOR INPUT MATRIX ,14) DASC 260
C 12 FORMAT(1H0,20HEXECUTION TERMINATED) DASC 270
C 13 FORMAT(1H0,42HINCORRECT NUMBER OF DATA CARDS FOR MATRIX ,14) DASC 280
C 14 FORMAT(1H0,18HGO ON TO NEXT CASE) DASC 290
C 15 FORMAT(1H0,11HEND OF CASE) DASC 300
C 16 FORMAT(7F2.0,F1.0,F7.3) DASC 310
C 17 FORMAT(3F10.0) DASC 320
C 18 FORMAT(1H0,13HSUBSET VECTOR,///) DASC 330
C 19 FORMAT(1H ,13,F5.0) DASC 340
C 20 FORMAT(1H1,32HSUMMARY STATISTICS FOR VARIABLE ,13) DASC 350
C 21 FORMAT(1H0,7HTOTAL =,F10.3,2X,9HAVERAGE =,F10.3,2X,2CHSTANDARD DEVDASC 360
C [ATTN] =,F10.3,2X,9HMINIMUM =,F10.3,2X,9HMAXIMUM =,F10.3) DASC 370
C 22 FORMAT(2I) DASC 380
C KC=C DASC 390
C 24 KC=KC+1 DASC 400
C CALL MATIN(ICDD,A,1000,NO,NV,MS,IER) DASC 410
C IF(ND) 25,50,25 DASC 420
C 25 IF(IER-1) 40,30,35 DASC 430
C 30 WRITE(6,11) ICDD DASC 440
C WRITE(6,14) DASC 450
C GO TO 24 DASC 460
C 35 WRITE(6,13) DASC 470
C WRITE(6,12) DASC 480
C GO TO 50 DASC 490
C 40 READ(5,22)NC,NOVAR DASC 500
C JC=NC*3 DASC 510
C READ(5,16)(C(I),I=1,JC) DASC 520
C READ(5,17)(UBO(I),I=1,3) DASC 530
C CALL SUBST(A,C,R,BOOL,S,NO,NV,NC) DASC 540
DASC 550
DASC 560
DASC 570
DASC 580
DASC 590
DASC 600

```

MULTIPLE LINEAR REGRESSION

Problem Description

Multiple linear regression analysis is performed for a set of independent variables and a dependent variable. Selection of different sets of independent variables and designation of a dependent variable can be made as many times as desired.

The sample problem for multiple linear regression consists of 30 observations with six variables as presented in Table 4. The first five variables are independent variables (predictors), and the last variable is the dependent variable (criteria). All five independent variables are used to predict the dependent variable in the first analysis, and only the second, third, and fifth variables are used to predict the dependent variable in the second analysis.

Table 4. Sample Data for Multiple Linear Regression

Observation	Variables					
	X ₁	X ₂	X ₃	X ₄	X ₅	X ₆
1	29	289	216	85	14	1
2	30	391	244	92	16	2
3	30	424	246	90	18	2
4	30	313	239	91	10	0
5	35	243	275	95	30	2
6	35	365	219	95	21	2
7	43	396	267	100	39	3
8	43	356	274	79	19	2
9	44	346	255	126	56	3
10	44	156	258	95	28	0
11	44	278	249	110	42	4
12	44	349	252	88	21	1
13	44	141	236	129	56	1
14	44	245	236	97	24	1
15	45	297	256	111	45	3
16	45	310	262	94	20	2
17	45	151	339	96	35	3
18	45	370	357	88	15	4
19	45	379	198	147	64	4
20	45	463	206	105	31	3
21	45	316	245	132	60	4
22	45	280	225	108	36	4
23	44	395	215	101	27	1
24	49	139	220	136	59	0
25	49	245	205	113	37	4
26	49	373	215	88	25	1
27	51	224	215	118	54	3
28	51	677	210	116	33	4
29	51	424	210	140	59	4
30	51	150	210	105	30	0

Program

Description

The multiple linear regression program consists of the main routine named REGRE, a special input subroutine named DATA, and four subroutines from the Scientific Subroutine Package:

CORRE, ORDER, MINV, and MULTR.

Capacity

The capacity of the sample program and the format required for data input have been set up as follows:

1. Up to 40 variables, including both independent and dependent variables

2. Up to 99,999 observations, if observations are read into the computer one at a time by the special input subroutine named DATA. If all data are to be stored in core prior to the calculation of correlation coefficients, the limitation on the number of observations depends on the size of core storage available for input data

3. (12F6.0) format for input data cards.

Therefore, if a problem satisfies the above conditions, the sample program need not be modified. However, if there are more than 40 variables, dimension statements in the sample main program must be modified to handle this particular problem. Similarly, if input data cards are prepared using a different format, the input format in the input subroutine, DATA, must be modified. The general rules for program modification are described later.

Input

Control Card

One control card is required for each problem and is read by the main program, REGRE. This card is prepared as follows:

Columns	Contents	For Sample Problem
1 - 6	Problem number (may be alphameric)	SAMPLE
7 - 11	Number of observations	00030
12 - 13	Number of variables	06
14 - 15	Number of selection cards (see below)	02

Leading zeros are not required to be keypunched.

Data Cards

Since input data are read into the computer one observation at a time, each row of data in Table 4 is keypunched on a separate card using the format (12F6.0). This format assumes twelve 6-column fields per card.

If there are more than twelve variables in a problem, each row of data is continued on the second and third cards until the last data point is keypunched. However, each row of data must begin on a new card.

Selection Card

The selection card is used to specify a dependent variable and a set of independent variables in a multiple linear regression analysis. Any variable in the set of original variables can be designated as a dependent variable, and any number of variables can be specified as independent variables. Selection of a dependent variable and a set of independent variables can be performed over and over again using the same set of original variables.

The selection card is prepared as follows:

Columns	Contents	For Sample Problem	
		Selec- tion 1	Selec- tion 2
1 - 2	Option code for table of residuals: 00 if it is not desired 01 if it is desired	01	01
3 - 4	Dependent variable designated for the forthcoming regression	06	06
5 - 6	Number of independent variables included in the forthcoming regression (the subscript numbers of individual variables are specified below)	05	03
7 - 8	1st independent variable included	01	02
9 - 10	2nd independent variable included	02	03
11 - 12	3rd independent variable included	03	05
13 - 14	4th independent variable included	04	
15 - 16	5th independent variable included	05	
etc.			

The input format of (36I2) is used for the selection card.

Deck Setup

The deck setup is shown in Figure 38.

Sample

The listing of input cards for the sample problem is presented in Figure 39.

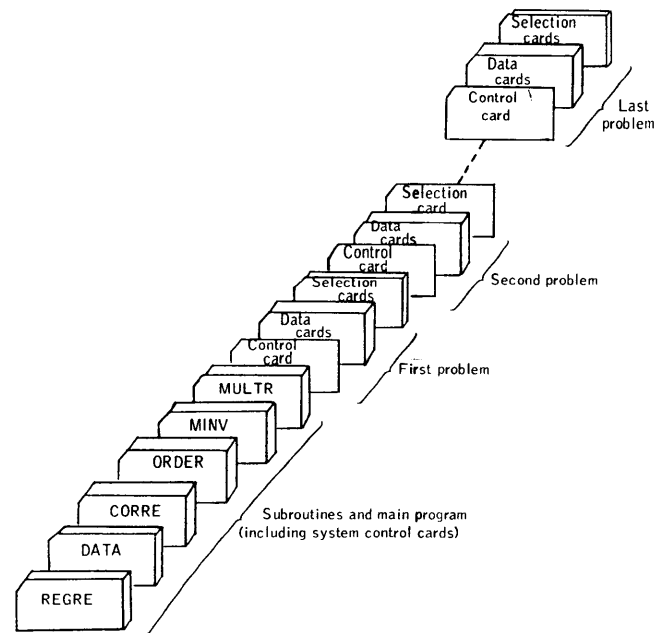


Figure 38. Deck setup (multiple linear regression)

Output

Description

The output of the sample program for multiple linear regression includes:

1. Means
2. Standard deviations
3. Correlation coefficients between the independent variables and the dependent variable
4. Regression coefficients
5. Standard errors of regression coefficients
6. Computed t-values
7. Intercept
8. Multiple correlation coefficients
9. Standard error of estimate
10. Analysis of variance for the multiple regression
11. Table of residuals (optional)

Sample

The output listing for the sample problem is shown in Figure 40.

Program Modification

Program capacity can be increased or decreased by making changes in dimension statements. Input data in a different format can also be handled by providing a specific format statement. In order to familiarize

```

/ DATA
SAMPLE000300402
29 289 216 95 14 1
30 391 244 92 16 2
30 424 246 90 18 2
30 313 239 91 10 0
35 243 275 95 30 2
35 365 219 95 21 2
43 396 267 100 39 3
43 356 274 79 19 2
44 346 255 126 56 3
44 156 258 95 28 0
44 278 249 110 42 4
44 369 252 88 21 1
44 141 236 129 56 1
44 245 236 97 24 1
45 297 256 111 45 3
45 310 262 94 20 2
45 151 339 96 35 3
45 370 357 88 15 4
45 379 198 147 64 4
45 463 206 105 31 3
45 316 245 132 60 4
45 280 225 108 36 4
44 395 215 121 27 1
49 139 220 136 59 0
49 245 205 113 37 4
49 373 215 88 25 1
51 224 215 118 54 3
51 677 210 116 33 6
51 424 210 140 59 4
51 150 210 105 30 0
010609C102030405
010609C20305

```

Figure 39. Input listing (multiple regression)

the user with the program modification, the following general rules are supplied in terms of the sample problem:

1. Changes in the dimension statements of the main program, REGRE
 - a. The dimension of arrays XBAR, STD, D, RY, ISAVE, B, SB, T, and W must be greater than or equal to the number of variables, m. Since there are six variables in the sample problem, the value of m is 6.
 - b. The dimension of array RX must be greater than or equal to the product of m x m. For the sample problem this product is 36 = 6 x 6.
 - c. The dimension of array R must be greater than or equal to (m + 1)m/2. For the sample problem this number is 21 = (6 + 1)6/2.

2. Changes in the input format statement of the special input subroutine, DATA:

Only the format statement for input data may be changed. Since sample data are either one-, two-, or three-digit numbers, rather than using six-column fields as in the sample problem, each row of data may be keypunched in six 3-column fields, and, if so, the format is changed to (6F3.0).

The special input subroutine, DATA, is normally written by the user to handle different formats for different problems. The user may modify this subroutine to perform testing of input data, transformation of data, and so on.

```

MULTIPLE REGRESSION.....SAMPLE
SELECTION..... 1

```

VARIABLE NO.	MEAN	STANDARD DEVIATION	CORRELATION X VS Y	REGRESSION COEFFICIENT	STD. ERROR OF REG. COEF.	COMPUTED T VALUE
1	43.15333	6.52176	0.28422	0.01242	0.03635	0.34171
2	316.1665C	114.4259C	0.42189	0.00735	0.00186	3.96545
3	241.7999C	36.43074	0.11500	0.01504	0.00635	2.36881
4	165.8666C	17.85640	0.37822	0.00151	0.03679	0.04100
5	34.13333	15.97571	0.39412	0.04919	0.04141	1.18782
DEPENDENT						
6	2.26667	1.41259				

```

INTERCEPT -6.07528
MULTIPLE CORRELATION 0.73575
STD. ERROR OF ESTIMATE 1.05162

```

```

ANALYSIS OF VARIANCE FOR THE REGRESSION

```

SOURCE OF VARIATION	DEGREES OF FREEDOM	SUM OF SQUARES	MEAN SQUARES	F VALUE
ATTRIBUTABLE TO REGRESSION	5	31.32506	6.26501	5.66508
DEVIATION FROM REGRESSION	24	26.29461	1.1059C	
TOTAL	29	57.86667		

```

MULTIPLE REGRESSION.....SAMPLE
SELECTION..... 1

```

```

TABLE OF RESIDUALS

```

CASE NO.	Y VALUE	Y ESTIMATE	RESIDUAL
1	1.00000	0.48091	0.51909
2	2.00000	1.17670	0.82330
3	2.00000	2.14586	-0.14586
4	0.0	0.02880	-0.02880
5	2.00000	1.50522	0.49478
6	2.00000	1.52125	0.47875
7	3.00000	3.46447	-0.46447
8	2.00000	2.25887	-0.25887
9	3.00000	3.00255	-0.00255
10	0.0	1.02042	-1.02042
11	4.00000	2.49735	1.50265
12	1.00000	2.00066	-1.00066
13	1.00000	2.00735	-1.00735
14	1.00000	1.15308	-0.15308
15	3.00000	2.90046	0.09954
16	2.00000	1.83532	0.16468
17	3.00000	2.56604	0.43396
18	4.00000	3.45225	0.54775
19	4.00000	3.62661	0.37339
20	3.00000	2.68080	0.31920
21	4.00000	3.64889	0.35111
22	4.00000	1.86542	2.13458
23	1.00000	2.09863	-1.09863
24	0.0	1.97217	-1.97217
25	4.00000	1.41253	2.58747
26	1.00000	1.88027	-0.88027
27	3.00000	2.27646	0.72354
28	4.00000	4.31080	-0.31080
29	4.00000	3.95745	0.04255
30	0.0	0.45456	-0.45456

Figure 40. Output listing (multiple regression)

Operating Instructions

The sample program for multiple linear regression is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and data set 6 is used for output. A scratch tape (data set 13) is used as intermediate storage.

Error Messages

The following error conditions will result in messages:

1. The number of selection cards is not specified on the control card--NUMBER OF SELECTIONS NOT SPECIFIED. JOB TERMINATED.

2. The matrix of correlation coefficients is singular--THE MATRIX IS SINGULAR. THIS SELECTION IS SKIPPED.

Error condition 2 allows the computer run to continue; however, error condition 1 terminates execution of the job.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 42 seconds.

```

C ..... REGR 10
C ..... REGR 20
C ..... REGR 30
C ..... REGR 40
C ..... REGR 50
C ..... REGR 60
C ..... REGR 70
C ..... REGR 80
C ..... REGR 90
C ..... REGR 100
C ..... REGR 110
C ..... REGR 120
C ..... REGR 130
C ..... REGR 140
C ..... REGR 150
C ..... REGR 160
C ..... REGR 170
C ..... REGR 180
C ..... REGR 190
C ..... REGR 200
C ..... REGR 210
C ..... REGR 220
C ..... REGR 230
C ..... REGR 240
C ..... REGR 250
C ..... REGR 260
C ..... REGR 270
C ..... REGR 280
C ..... REGR 290
C ..... REGR 300
C ..... REGR 310
C ..... REGR 320
C ..... REGR 330
C ..... REGR 340
C ..... REGR 350
C ..... REGR 360
C ..... REGR 370
C ..... REGR 380
C ..... REGR 390
C ..... REGR 400
C ..... REGR 410
C ..... REGR 420
C ..... REGR 430
C ..... REGR 440
C ..... REGR 450
C ..... REGR 460
C ..... REGR 470
C ..... REGR 480
C ..... REGR 490
C ..... REGR 500
C ..... REGR 510
C ..... REGR 520
C ..... REGR 530
C ..... REGR 540
C ..... REGR 550
C ..... REGR 560
C ..... REGR 570
C ..... REGR 580
C ..... REGR 590
C ..... REGR 600
C ..... REGR 610
C ..... REGR 620
C ..... REGR 630
C ..... REGR 640
C ..... REGR 650
C ..... REGR 660
C ..... REGR 670
C ..... REGR 680
C ..... REGR 690
C ..... REGR 700
C ..... REGR 710
C ..... REGR 720
C ..... REGR 730
C ..... REGR 740
C ..... REGR 750
C ..... REGR 760
C ..... REGR 770
C ..... REGR 780
C ..... REGR 790
C ..... REGR 800
C ..... REGR 810
C ..... REGR 820
C ..... REGR 830
C ..... REGR 840
C ..... REGR 850
C ..... REGR 860
C ..... REGR 870
C ..... REGR 880
C ..... REGR 890
C ..... REGR 900
C ..... REGR 910
C ..... REGR 920
C ..... REGR 930
C ..... REGR 940
C ..... REGR 950
C ..... REGR 960
C ..... REGR 970
C ..... REGR 980
C ..... REGR 990
C ..... REGR 1000
C ..... REGR 1010
C ..... REGR 1020
C ..... REGR 1030
C ..... REGR 1040
C ..... REGR 1050
C ..... REGR 1060
C ..... REGR 1070
C ..... REGR 1080
C ..... REGR 1090
C ..... REGR 1100
C ..... REGR 1110
C ..... REGR 1120

```

```

X=0.0 REGR1130
C CALL CORRE (M,M,I0,X,XBAR,STD,RX,R,D,B,T) REGR1140
C ..... REGR1150
C ..... REGR1160
C ..... REGR1170
C ..... REGR1180
C ..... REGR1190
C ..... REGR1200
C ..... REGR1210
C ..... REGR1220
C ..... REGR1230
C ..... REGR1240
C ..... REGR1250
C ..... REGR1260
C ..... REGR1270
C ..... REGR1280
C ..... REGR1290
C ..... REGR1300
C ..... REGR1310
C ..... REGR1320
C ..... REGR1330
C ..... REGR1340
C ..... REGR1350
C ..... REGR1360
C ..... REGR1370
C ..... REGR1380
C ..... REGR1390
C ..... REGR1400
C ..... REGR1410
C ..... REGR1420
C ..... REGR1430
C ..... REGR1440
C ..... REGR1450
C ..... REGR1460
C ..... REGR1470
C ..... REGR1480
C ..... REGR1490
C ..... REGR1500
C ..... REGR1510
C ..... REGR1520
C ..... REGR1530
C ..... REGR1540
C ..... REGR1550
C ..... REGR1560
C ..... REGR1570
C ..... REGR1580
C ..... REGR1590
C ..... REGR1600
C ..... REGR1610
C ..... REGR1620
C ..... REGR1630
C ..... REGR1640
C ..... REGR1650
C ..... REGR1660
C ..... REGR1670
C ..... REGR1680
C ..... REGR1690
C ..... REGR1700
C ..... REGR1710
C ..... REGR1720
C ..... REGR1730
C ..... REGR1740
C ..... REGR1750
C ..... REGR1760
C ..... REGR1770
C ..... REGR1780
C ..... REGR1790
C ..... REGR1800
C ..... REGR1810
C ..... REGR1820
C ..... REGR1830
C ..... REGR1840
C ..... REGR1850
C ..... REGR1860
C ..... REGR1870
C ..... REGR1880
C ..... REGR1890
C ..... REGR1900
C ..... REGR1910
C ..... REGR1920
C ..... REGR1930
C ..... REGR1940
C ..... REGR1950
C ..... REGR1960

```

POLYNOMIAL REGRESSION

Problem Description

Powers of an independent variable are generated to calculate polynomials of successively increasing degrees. If there is no reduction in the residual sum of squares between two successive degrees of polynomials, the program terminates the problem before completing the analysis for the highest degree polynomial specified.

The sample problem for polynomial regression consists of 15 observations, as presented in Table 5. The highest degree polynomial specified for this problem is 4.

Program

Description

The polynomial regression program consists of the main routine named POLRG, a special plot subroutine named PLOT, and four subroutines from the Scientific Subroutine Package: GDATA, ORDER, MINV, and MULTR.

Capacity

The capacity of the sample program and the format required for data input have been set up as follows:

1. Up to 100 observations
2. Up to 10th degree polynomial
3. (2F6.0) format for input data cards

Therefore, if a problem satisfies the above conditions it is not necessary to modify the sample program. However, if there are more than 100 observations or if greater than 10th degree polynomial is desired, dimension statements in the sample main program must be modified to handle this particular problem. Similarly, if input data cards are prepared using a different format, the input format in the sample main program must be modified. The general rules for program modification are described later.

Input

Control Card

One control card is required for each problem and is read by the main program, POLRG. This card is prepared as follows:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem</u>
1 - 6	Problem number (may be alphameric)	SAMPLE
7 - 11	Number of observations	00015
12 - 13	Highest degree polynomial to be fitted	04
14	Option code for plotting Y values and Y estimates:	1
	0 if it is not desired	
	1 if it is desired	

Leading zeros are not required to be keypunched.

Data Cards

Since input data are read into the computer one observation at a time, each pair of X and Y data in Table 5 is keypunched in that order on a separate card using the format (2F6.0).

Table 5. Sample Data for Polynomial Regression

<u>X</u>	<u>Y</u>
1	10
2	16
3	20
4	23
5	25
6	26
7	30
8	36
9	48
10	62
11	78
12	94
13	107
14	118
15	127

Deck Setup

The deck setup is shown in Figure 41.

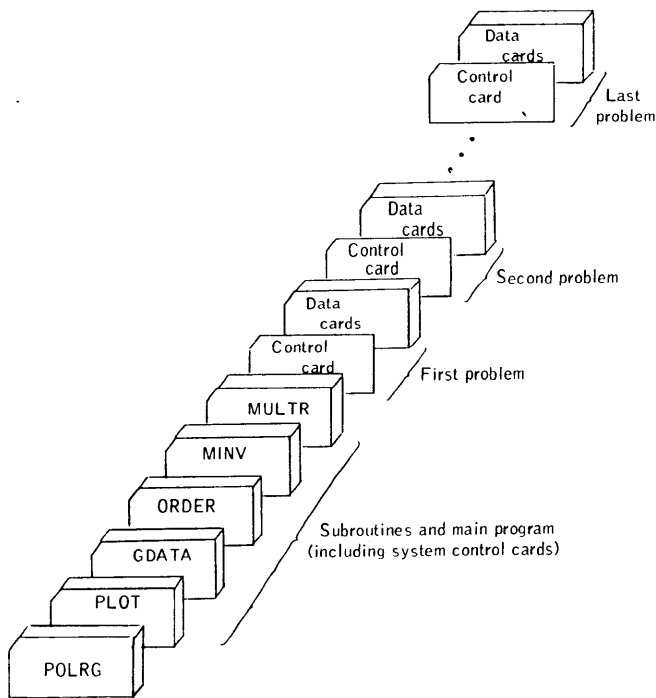


Figure 41. Deck setup (polynomial regression)

Sample

The listing of input cards for the sample problem is presented in Figure 42.

Output

Description

The output of the sample program for polynomial regression includes:

1. Regression coefficients for successive degree polynomials
2. Analysis-of-variance table for successive degree polynomials
3. Table of residuals for the final degree polynomial (optional)
4. Plot of Y values and Y estimates (optional)

/DATA		10
SAMPLE00015041		20
1	10	30
2	16	40
3	20	50
4	23	60
5	25	70
6	26	80
7	30	90
8	36	100
9	48	110
10	62	120
11	78	130
12	94	140
13	107	150
14	118	160
15	127	170

Figure 42. Input card listing (polynomial regression)

Sample

The output listing for the sample problem is shown in Figure 43.

Program Modification

Program capacity can be increased or decreased by making changes in dimension statements. Input data in a different format can also be handled by providing a specific format statement. In order to familiarize the user with the program modification, the following general rules are supplied in terms of the sample problem.

1. Changes in the dimension statements of the main program, POLRG:
 - a. The dimension of array X must be greater than or equal to the product of $n(m + 1)$, where n is the number of observations and m is the highest degree polynomial to be fitted. Since there are 15 observations and the highest degree polynomial specified is 4, the product is $75 = 15(4 + 1)$.
 - b. The dimension of array DI must be greater than or equal to the product of $m \times m$. For the sample problem this product is $16 = 4 \times 4$.
 - c. The dimension of array D must be greater than or equal to $(m + 2)(m + 1)/2$. For the sample problem this number is $15 = (4 + 2)(4 + 1)/2$.
 - d. The dimension of arrays B, E, SB, and T must be greater than or equal to the highest degree polynomial to be fitted, m . For the sample problem the value of m is 4.
 - e. The dimension of arrays XBAR, STD, COE, SUMSQ, and ISAVE must be greater than or equal to $(m + 1)$. For the sample problem this value is $5 = (4 + 1)$.
 - f. The dimension of array P must be greater than or equal to $3(n)$. For the sample problem this value is $45 = 3(15)$. The array P is used when a plot of Y values and Y estimates is desired.

2. Changes in the input format statement of the main program, POLRG:

Only the format statement for input data may be changed. Since sample data are either one-, two-, or three-digit numbers, rather than using six-column fields as in the sample problem, each row of data may be keypunched in two 3-column fields, and if so the format is changed to (2F3.0).

POLYNOMIAL REGRESSION.....SAMPLE

NUMBER OF OBSERVATIONS 15

POLYNOMIAL REGRESSION OF DEGREE 1

INTERCEPT -13.87613

REGRESSION COEFFICIENTS
R.56785

ANALYSIS OF VARIANCE FOR 1 DEGREE POLYNOMIAL

SOURCE OF VARIATION	DEGREE OF FREEDOM	SUM OF SQUARES	MEAN SQUARE	F VALUE	IMPROVEMENT IN TERMS OF SUM OF SQUARES
DUE TO REGRESSION	1	20554.26172	20554.26172	135.56577	20554.26172
DEVIATION ABOUT REGRESSION	13	1971.03906	151.61838		
TOTAL	14	22525.30078			

POLYNOMIAL REGRESSION OF DEGREE 2

INTERCEPT 15.07547

REGRESSION COEFFICIENTS
-1.64957 C.67856

ANALYSIS OF VARIANCE FOR 2 DEGREE POLYNOMIAL

SOURCE OF VARIATION	DEGREE OF FREEDOM	SUM OF SQUARES	MEAN SQUARE	F VALUE	IMPROVEMENT IN TERMS OF SUM OF SQUARES
DUE TO REGRESSION	2	22235.39062	11117.69531	460.18506	1681.12801
DEVIATION ABOUT REGRESSION	12	289.91016	24.15918		
TOTAL	14	22525.30078			

POLYNOMIAL REGRESSION OF DEGREE 3

INTERCEPT 18.49472

REGRESSION COEFFICIENTS
-3.88107 0.97684 -0.01409

ANALYSIS OF VARIANCE FOR 3 DEGREE POLYNOMIAL

SOURCE OF VARIATION	DEGREE OF FREEDOM	SUM OF SQUARES	MEAN SQUARE	F VALUE	IMPROVEMENT IN TERMS OF SUM OF SQUARES
DUE TO REGRESSION	3	22256.32812	7418.77344	303.40063	20.93750
DEVIATION ABOUT REGRESSION	11	268.97266	24.45206		
TOTAL	14	22525.30078			

POLYNOMIAL REGRESSION OF DEGREE 4

NO IMPROVEMENT

POLYNOMIAL REGRESSION.....SAMPLE

POLYNOMIAL REGRESSION OF DEGREE 3

TABLE OF RESIDUALS

OBSERVATION NO.	X VALUE	Y VALUE	Y ESTIMATE	RESIDUAL
1	1.00000	10.00000	15.57588	-5.57588
2	2.00000	16.00000	14.52666	1.47334
3	3.00000	20.00000	15.26157	4.73803
4	4.00000	23.00000	17.69725	5.30275
5	5.00000	25.00000	21.74792	3.25208
6	6.00000	26.00000	27.32945	-1.32945
7	7.00000	30.00000	34.35724	-4.35724
8	8.00000	36.00000	42.74675	-6.74675
9	9.00000	40.00000	52.41338	-4.41338
10	10.00000	62.00000	63.27257	-1.27257
11	11.00000	78.00000	75.23578	2.76022
12	12.00000	94.00000	88.23039	5.76961
13	13.00000	107.00000	102.15950	4.84010
14	14.00000	118.00000	116.94366	1.05634
15	15.00000	127.00000	132.49715	-5.49715

Figure 43. Output listing (polynomial regression)

CHART 3

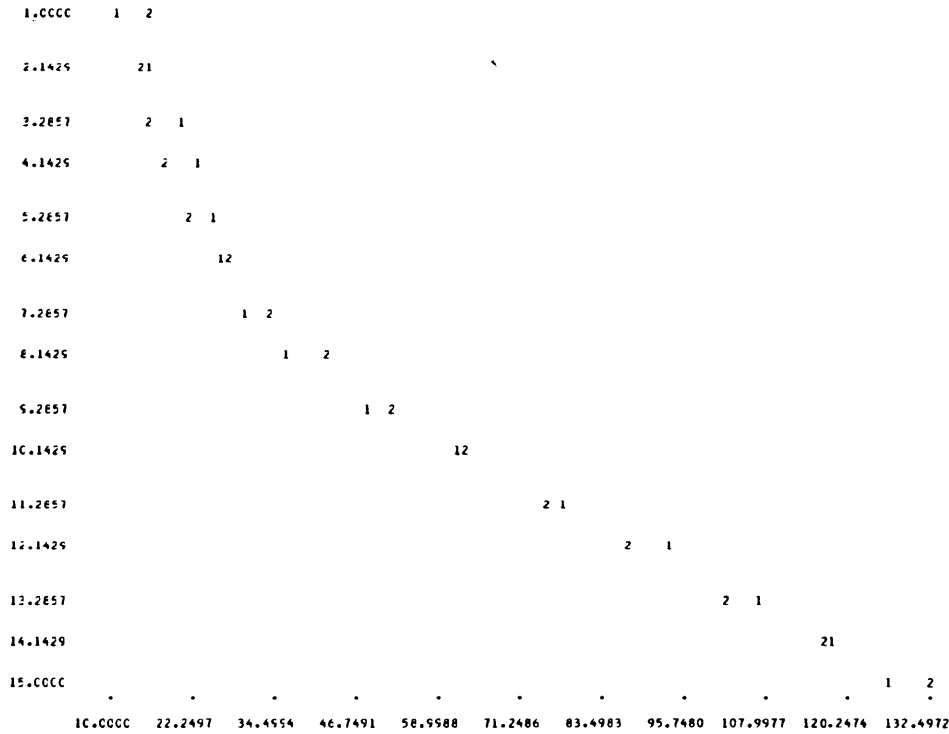


Figure 43. Output listing (polynomial regression) (Continued)

Operating Instructions

The sample program for polynomial regression is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and data set 6 is used for output. A scratch tape (data set 13) is used as intermediate storage when Y values and Y estimates are plotted.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 35 seconds.

```

C ..... PLRG 10
C ..... PLRG 20
C ..... PLRG 30
C ..... PLRG 40
C ..... PLRG 50
C ..... PLRG 60
C ..... PLRG 70
C ..... PLRG 80
C ..... PLRG 90
C ..... PLRG 100
C ..... PLRG 110
C ..... PLRG 120
C ..... PLRG 130
C ..... PLRG 140
C ..... PLRG 150
C ..... PLRG 160
C ..... PLRG 170
C ..... PLRG 180
C ..... PLRG 190
C ..... PLRG 200
C ..... PLRG 210
C ..... PLRG 220
C ..... PLRG 230
C ..... PLRG 240
C ..... PLRG 250
C ..... PLRG 260
C ..... PLRG 270
C ..... PLRG 280
C ..... PLRG 290
C ..... PLRG 300
C ..... PLRG 310
C ..... PLRG 320
C ..... PLRG 330
C ..... PLRG 340

```

SAMPLE MAIN PROGRAM FOR POLYNOMIAL REGRESSION - POLRG

PURPOSE

(1) READ THE PROBLEM PARAMETER CARD FOR A POLYNOMIAL REGRES-
 SION, (2) CALL SUBROUTINES TO PERFORM THE ANALYSIS, (3)
 PRINT THE REGRESSION COEFFICIENTS AND ANALYSIS OF VARIANCE
 TABLE FOR POLYNOMIALS OF SUCCESSIVELY INCREASING DEGREES,
 AND (4) OPTIONALLY PRINT THE TABLE OF RESIDUALS AND A PLOT
 OF Y VALUES AND Y ESTIMATES.

REMARKS

THE NUMBER OF OBSERVATIONS, N, MUST BE GREATER THAN M+1,
 WHERE M IS THE HIGHEST DEGREE POLYNOMIAL SPECIFIED.
 IF THERE IS NO REDUCTION IN THE RESIDUAL SUM OF SQUARES
 BETWEEN TWO SUCCESSIVE DEGREES OF THE POLYNOMIALS, THE
 PROGRAM TERMINATES THE PROBLEM BEFORE COMPLETING THE ANALY-
 SIS FOR THE HIGHEST DEGREE POLYNOMIAL SPECIFIED.

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

GOATA PLRG 230
 ORDER PLRG 240
 XINV PLRG 250
 MULTR PLRG 260
 PLOT (A SPECIAL PLOT SUBROUTINE PROVIDED FOR THE SAMPLE
 PROGRAM.) PLRG 270
 PLRG 280
 PLRG 290

METHOD

REFER TO B. JSTLE, "STATISTICS IN RESEARCH", THE IOWA STATE
 COLLEGE PRESS, 1954, CHAPTER 6.
 PLRG 310
 PLRG 320
 PLRG 330
 PLRG 340

```

C
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE
C PRODUCT OF N*(M+1), WHERE N IS THE NUMBER OF OBSERVATIONS AND M
C IS THE HIGHEST DEGREE POLYNOMIAL SPECIFIED..
C DIMENSION X(1100)
C
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE
C PRODUCT OF M*M..
C DIMENSION D(100)
C
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO
C (M+2)*(M+1)/2..
C DIMENSION D(66)
C
C THE FOLLOWING DIMENSIONS MUST BE GREATER THAN OR EQUAL TO M..
C DIMENSION B(10),E(10),SB(10),T(10)
C
C THE FOLLOWING DIMENSIONS MUST BE GREATER THAN OR EQUAL TO (M+1)..
C DIMENSION XBAR(11),STD(11),COE(11),SUMSQ(11),ISAVE(11)
C
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO 10..
C DIMENSION ANS(10)
C
C THE FOLLOWING DIMENSION WILL BE USED IF THE PLOT OF OBSERVED DATA
C AND ESTIMATES IS DESIRED. THE SIZE OF THE DIMENSION, IN THIS
C CASE, MUST BE GREATER THAN OR EQUAL TO N*3. OTHERWISE, THE SIZE
C OF DIMENSION MAY BE SET TO 1.
C DIMENSION P(300)
C
C .....
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE
C C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION
C STATEMENT WHICH FOLLOWS.
C
C DOUBLE PRECISION X,XBAR,STD,D,SUMSQ,DI,E,B,SB,T,ANS,DET,COE
C
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS
C ROUTINE.
C
C .....
C 1 FORMAT(A4,A2,15,I2,11)
C 2 FORMAT(2F6.0)
C 3 FORMAT(27H1POLYNOMIAL REGRESSION.....A4,A2//)
C 4 FORMAT(23H0NUMBER OF OBSERVATIONS,I6//)
C 5 FORMAT(32H0POLYNOMIAL REGRESSION OF DEGREE,I3)
C 6 FORMAT(12H0 INTERCEPT,E29.7)
C 7 FORMAT(26H0 REGRESSION COEFFICIENTS/(6E20.7))
C 8 FORMAT(1H0/24X,24HANALYSIS OF VARIANCE FOR,I4,I9H DEGREE POLYNOMIAL
C 1AL//)
C 9 FORMAT(1H0,5X,19HSOURCE OF VARIATION,7X,9HDEGREE OF,7X,6HSUM OF,9XPLRG 940
C 1,4HMEAN,10X,1HF,9X,20HIMPROVEMENT IN TERMS/33X,7HFREEDOM,8X,7HSQUARPLRG 950
C 2RES,7X,6HSQUARE,7X,9HVALUE,8X,17HOF SUM OF SQUARES)
C 10 FORMAT(23H0 DUE TO REGRESSION,I2X,I6,F17.5,F14.5,F13.5,F20.5)
C 11 FORMAT(32H0 DEVIATION ABOUT REGRESSION ,I6,F17.5,F14.5)
C 12 FORMAT(8X,5HTOTAL,I9X,I6,F17.5//)
C 13 FORMAT(17H0 NO IMPROVEMENT)
C 14 FORMAT(1H0//27X,18HTABLE OF RESIDUALS//16H OBSERVATION NO.,5X,7MH
C 1VALUE,7X,7HY VALUE,7X,10HY ESTIMATE,7X,8HRESIDUAL/)
C 15 FORMAT(1H0,3X,I6,F18.5,F14.5,F17.5,F15.5)
C
C .....
C READ PROBLEM PARAMETER CARD
C
C 100 READ (5,1) PR,PRI,N,M,NPLOT
C
C PR....PROBLEM NUMBER (MAY BE ALPHAMERIC)
C PRI....PROBLEM NUMBER (CONTINUED)
C N.....NUMBER OF OBSERVATIONS
C M.....HIGHEST DEGREE POLYNOMIAL SPECIFIED
C NPLOT,OPTION CODE FOR PLOTTING
C 0 IF PLOT IS NOT DESIRED.
C 1 IF PLOT IS DESIRED.
C
C PRINT PROBLEM NUMBER AND N.
C
C WRITE (6,3) PR,PRI
C WRITE (6,4) N
C
C READ INPUT DATA
C
C L=N*M
C DO 110 I=1,N
C J=L+I
C
C PLRG 350
C PLRG 360
C PLRG 370
C PLRG 380
C PLRG 390
C PLRG 400
C PLRG 410
C PLRG 420
C PLRG 430
C PLRG 440
C PLRG 450
C PLRG 460
C PLRG 470
C PLRG 480
C PLRG 490
C PLRG 500
C PLRG 510
C PLRG 520
C PLRG 530
C PLRG 540
C PLRG 550
C PLRG 560
C PLRG 570
C PLRG 580
C PLRG 590
C PLRG 600
C PLRG 610
C PLRG 620
C PLRG 630
C PLRG 640
C PLRG 650
C PLRG 660
C PLRG 670
C PLRG 680
C PLRG 690
C PLRG 700
C PLRG 710
C PLRG 720
C PLRG 730
C PLRG 740
C PLRG 750
C PLRG 760
C PLRG 770
C PLRG 780
C PLRG 790
C PLRG 800
C PLRG 810
C PLRG 820
C PLRG 830
C PLRG 840
C PLRG 850
C PLRG 860
C PLRG 870
C PLRG 880
C PLRG 890
C PLRG 900
C PLRG 910
C PLRG 920
C PLRG 930
C PLRG 940
C PLRG 950
C PLRG 960
C PLRG 970
C PLRG 980
C PLRG 990
C PLRG1000
C PLRG1010
C PLRG1020
C PLRG1030
C PLRG1040
C PLRG1050
C PLRG1060
C PLRG1070
C PLRG1080
C PLRG1090
C PLRG1100
C PLRG1110
C PLRG1120
C PLRG1130
C PLRG1140
C PLRG1150
C PLRG1160
C PLRG1170
C PLRG1180
C PLRG1190
C PLRG1200
C PLRG1210
C PLRG1220
C PLRG1230
C PLRG1240
C PLRG1250
C PLRG1260
C PLRG1270
C PLRG1280
C
C X(I) IS THE INDEPENDENT VARIABLE, AND X(J) IS THE DEPENDENT
C VARIABLE.
C
C 110 READ (5,2) X(I),X(J)
C
C CALL GDATA (N,M,X,XBAR,STD,D,SUMSQ)
C
C MM=N+1
C SUM=0.0
C NT=N-1
C
C DO 200 I=1,M
C ISAVE(I)=1
C
C FORM SUBSET OF CORRELATION COEFFICIENT MATRIX
C
C CALL ORDER (MM,D,MM,I,(SAVE,DI,E))
C
C INVERT THE SUBMATRIX OF CORRELATION COEFFICIENTS
C
C CALL MINV (DI,I,DET,B,T)
C
C CALL MJLTR (N,I,XBAR,STD,SUMSQ,DI,E,ISAVE,D,SB,T,ANS)
C
C PRINT THE RESULT OF CALCULATION
C
C WRITE (6,5) I
C IF(ANS(7)) 140,130,130
C 130 SUMIP=ANS(4)-SUM.
C IF(SUMIP) 140, 140, 150
C 140 WRITE (6,13)
C GJ TO 210
C 150 WRITE (6,6) ANS(I)
C WRITE (6,7) (B(J),J=1,I)
C WRITE (6,8) I
C WRITE (6,9)
C SUM=ANS(4)
C WRITE (6,10) I,ANS(4),ANS(6),ANS(10),SUMIP
C NI=ANS(8)
C WRITE (6,11) NI,ANS(7),ANS(9)
C WRITE (6,12) NT,SUMSQ(MM)
C
C SAVE COEFFICIENTS FOR CALCULATION OF Y ESTIMATES
C
C COE(I)=ANS(I)
C DO 160 J=1,I
C 160 COE(J+1)=B(J)
C LA=I
C 200 CONTINUE
C
C TEST WHETHER PLOT IS DESIRED
C
C 210 IF(NPLOT) 190, 100, 220
C
C CALCULATE ESTIMATES
C
C 220 NP3=N*N
C DO 230 I=1,N
C NP3=NP3+1
C P(NP3)=COE(I)
C L=I
C DO 230 J=L,LA
C P(NP3)=P(NP3)+X(L)*COE(J+1)
C 230 L=L+N
C
C COPY OBSERVED DATA
C
C N2=N
C L=N*M
C DO 240 I=1,N
C P(I)=X(I)
C N2=N2+1
C L=L+1
C 240 P(N2)=X(L)
C
C PRINT TABLE OF RESIDUALS
C
C WRITE (6,3) PR,PRI
C WRITE (6,5) LA
C WRITE (6,14)
C NP2=N
C NP3=N*N
C DO 250 I=1,N
C NP2=NP2+1
C NP3=NP3+1
C RESID=P(NP2)-P(NP3)
C 250 WRITE (6,15) I,P(I),P(NP2),P(NP3),RESID
C
C CALL PLOT (LA,P,N,3,C,1)
C
C GO TO 100
C END
C
C PLRG1290
C PLRG1300
C PLRG1310
C PLRG1320
C PLRG1330
C PLRG1340
C PLRG1350
C PLRG1360
C PLRG1370
C PLRG1380
C PLRG1390
C PLRG1400
C PLRG1410
C PLRG1420
C PLRG1430
C PLRG1440
C PLRG1450
C PLRG1460
C PLRG1470
C PLRG1480
C PLRG1490
C PLRG1500
C PLRG1510
C PLRG1520
C PLRG1530
C PLRG1540
C PLRG1550
C PLRG1560
C PLRG1570
C PLRG1580
C PLRG1590
C PLRG1600
C PLRG1610
C PLRG1620
C PLRG1630
C PLRG1640
C PLRG1650
C PLRG1660
C PLRG1670
C PLRG1680
C PLRG1690
C PLRG1700
C PLRG1710
C PLRG1720
C PLRG1730
C PLRG1740
C PLRG1750
C PLRG1760
C PLRG1770
C PLRG1780
C PLRG1790
C PLRG1800
C PLRG1810
C PLRG1820
C PLRG1830
C PLRG1840
C PLRG1850
C PLRG1860
C PLRG1870
C PLRG1880
C PLRG1890
C PLRG1900
C PLRG1910
C PLRG1920
C PLRG1930
C PLRG1940
C PLRG1950
C PLRG1960
C PLRG1970
C PLRG1980
C PLRG1990
C PLRG2000
C PLRG2010
C PLRG2020
C PLRG2030
C PLRG2040
C PLRG2050
C PLRG2060
C PLRG2070
C PLRG2080
C PLRG2090
C PLRG2100
C PLRG2110
C PLRG2120
C PLRG2130
C PLRG2140
C PLRG2150
C PLRG2160
C PLRG2170
C PLRG2180
C PLRG2190
C PLRG2200
C PLRG2210

```

STEPWISE MULTIPLE REGRESSION

Problem Description

Stepwise multiple regression is a statistical technique for analyzing a relationship between a dependent variable (y) and a set of independent variables (x_1, x_2, \dots, x_m) and for selecting the independent variables in the order of their importance. The criterion of importance is based on the reduction of sums of squares, and the independent variable most important in this reduction in a given step is entered in the regression. Any variable in the original set can be named as the dependent variable. A set of variables can be forced to enter in the regression, and another set of variables can be deleted.

The sample problem for stepwise multiple regression consists of 30 observations on six variables as presented in Table 4. The first five variables are independent variables (predictors), and the last variable is the dependent variable (criterion). All five independent variables are available for selection in the first analysis. In the second analysis, the third variable is forced to enter in the regression, the fourth variable is deleted, and the remaining three independent variables are available for selection. Note that the same sample problem has been used for multiple linear regression and that the results of these two programs may be compared.

Program

Description

The stepwise multiple regression program consists of the main routine named STEPR, a special input subroutine named DATA, a special output subroutine named STOUT, and four subroutines from the Scientific Subroutine Package: CORRE, MSTR, LOC, and STPRG.

Capacity

The capacity of the sample program and the format required for data input have been set up as follows:

1. Up to 35 variables, including both dependent and independent variables
2. Up to 99,999 observations, if observations are read into the computer one at a time by the special input subroutine named DATA. If all data are to be stored in core prior to the calculation of correlation coefficients, the limitation on the number of observations depends on the size of core storage available for input data.
3. (12F6.0) format for input data cards

Therefore, if a problem satisfies the above conditions, it is not necessary to modify the sample program. However, if there are more than 35 variables, dimension statements in the sample main program must be modified to handle this particular problem. Similarly, if input data cards are prepared using a different format, the format in the input subroutine, DATA, must be modified. The general rules for program modification are described later.

Input

Control Card

One control card is required for each problem and is read by the main program, STEPR. This card is prepared as follows:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem</u>
1-6	Problem code (may be alphameric)	SAMPLE
7-11	Number of observations	00030
12-13	Number of variables	06
14-15	Number of selection cards (see below)	02
16-21	This constant is the proportion of the sum of squares which will be used to limit the entering of variables into the regression. Unless the proportion of the sum of squares attributable to an entering variable is greater than this value, the variable will not be entered. The keypunched value should have a decimal point.*	0.0
22	Option code for table of residuals 0--if it is not desired 1--if it is desired	1

*The choice of value depends upon the purpose of analysis. A suggested trial value is 0.01 (one percent). If all variables are to be included in the regression, use 0.0.

Leading zeros are not required to be keypunched.

Data Cards

Since input data can be read into the computer one observation at a time, each row of data in Table 4 is keypunched on a separate card using the format (12F6.0). This format assumes twelve 6-column fields per card.

If there are more than twelve variables in a problem, each row of data is continued on the second and third cards until the last data point is keypunched. However, each row of data must begin on a new card.

Selection Card

The selection card is used to specify a dependent variable, independent variables to be forced to enter in the regression, variables to be deleted, and independent variables to be chosen by the program to enter in the regression. Any one variable in the set of original variables can be designated as a dependent variable, and any number of variables can be specified as forcing variables, deleting variables, and unrestricted variables to be chosen by the program. The specification of the variables can be performed over and over again using the same set of original variables.

In a selection card, each variable is specified using one of the following codes:

<u>Code</u>	<u>Specification</u>
0 or blank	Independent variable to be chosen by the program to enter in the regression
1	Independent variable forced by the user to enter in the regression
2	Variable to be deleted
3	Dependent variable

The selection card itself is prepared as follows:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem Selections</u>	
		<u>1</u>	<u>2</u>
1	Code for 1st variable	0	0
2	Code for 2nd variable	0	0
3	Code for 3rd variable	0	1
4	Code for 4th variable	0	2
5	Code for 5th variable	0	0
6	Code for 6th variable	3	3
etc.			

The input format of (72II) is used for the selection card.

Deck Setup

The deck setup is shown in Figure 44.

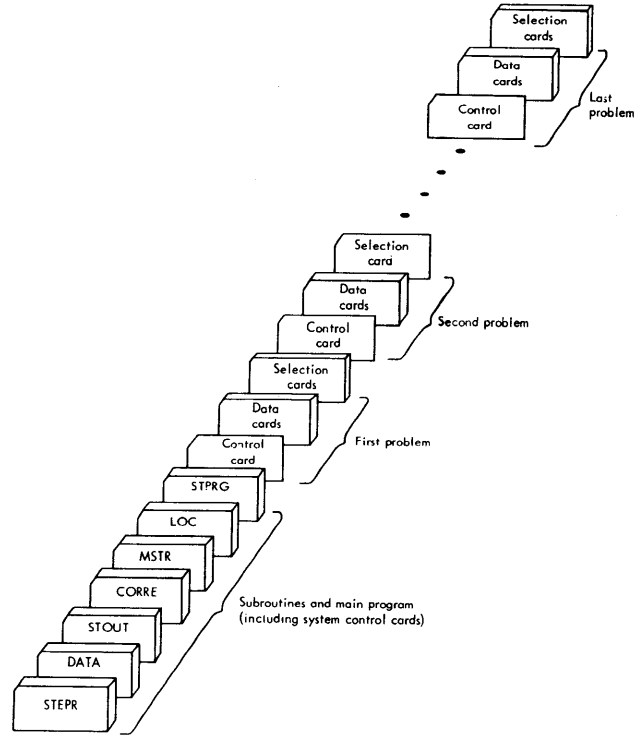


Figure 44. Deck setup (stepwise multiple regression)

Sample

The listing of input cards for the sample problem is presented in Figure 45.

```

/ DATA
SAMPLE 30 6 2 C.001
29 289 216 85 14 1
30 391 244 92 16 2
30 424 246 90 18 2
30 313 239 91 10 0
35 243 275 95 30 2
35 365 219 95 21 2
43 396 267 100 30 3
43 356 274 79 19 2
44 346 255 126 56 3
44 156 258 95 28 0
44 278 249 110 42 4
44 349 252 88 21 1
44 141 236 129 56 1
44 245 236 97 24 1
45 297 256 111 45 3
45 310 262 94 20 2
45 151 339 96 35 3
45 370 357 88 15 4
45 379 198 147 64 4
45 463 206 105 31 3
45 316 245 132 60 4
45 280 225 108 36 4
44 395 215 101 27 1
49 139 220 136 59 0
49 245 205 113 37 4
49 373 215 88 25 1
51 224 215 118 54 3
51 677 210 116 33 4
51 424 210 140 59 4
51 150 210 105 30 0
ooccc3
001203
10
20
30
40
50
60
70
80
90
100
110
120
130
140
150
160
170
180
190
200
210
220
230
240
250
260
270
280
290
300
310
320
330
340
    
```

Figure 45.

Output

Description

The output of the sample program for stepwise multiple regression includes:

1. For all variables --
 - a. Means
 - b. Standard deviations
 - c. Correlation coefficient matrix
2. For each step of multiple regression --
 - a. Sum of squares reduced
 - b. Proportion reduced
 - c. Cumulative sum of squares reduced
 - d. Cumulative proportion reduced
 - e. Multiple correlation coefficient (adjusted and unadj.)
 - f. F-value for analysis of variance
 - g. Standard error of estimate (adjusted and unadj.)
 - h. Regression coefficients
 - i. Standard errors of regression coefficients
 - j. Computed t-values
3. Tables of residuals (optional)

Sample

The output listing for the sample problem is shown in Figure 46.

```
STEP-WISE MULTIPLE REGRESSION.....SAMPLE
NUMBER OF OBSERVATIONS 30
NUMBER OF VARIABLES 6
NUMBER OF SELECTIONS 2
CONSTANT TO LIMIT VARIABLES C.C
VARIABLE MEAN STANDARD DEVIATION
NO.
1 43.13333 6.52176
2 316.16650 114.42990
3 241.79999 36.43074
4 105.66666 17.85640
5 34.13333 15.97571
6 2.26667 1.41259
CORRELATION MATRIX
ROW 1
1.00000 -0.06721 -0.13689 0.49755 0.55849 0.28422
ROW 2
-0.06721 1.00000 -0.17857 -0.05227 -0.18381 0.42189
ROW 3
-0.13689 -0.17857 1.00000 -0.40874 -0.26319 0.11900
ROW 4
0.49755 -0.05227 -0.40874 1.00000 0.93552 0.37822
ROW 5
0.55849 -0.18381 -0.26319 0.93552 1.00000 0.39412
ROW 6
0.28422 0.42189 0.11900 0.37822 0.39412 1.00000
SELECTION..... 1
DEPENDENT VARIABLE..... 6
NUMBER OF VARIABLES FORCED.... 0
NUMBER OF VARIABLES DELETED... 0
STEP 1
VARIABLE ENTERED..... 2
SUM OF SQUARES REDUCED IN THIS STEP.... 10.300
PROPORTION REDUCED IN THIS STEP..... 0.178
CUMULATIVE SUM OF SQUARES REDUCED..... 10.300
CUMULATIVE PROPORTION REDUCED..... 0.178 OF 57.867
```

Figure 46.

```
FOR 1 VARIABLES ENTERED
MULTIPLE CORRELATION COEFFICIENT... 0.422
(ADJUSTED FOR D.F.)..... 0.422
F-VALUE FOR ANALYSIS OF VARIANCE... 6.063
STANDARD ERROR OF ESTIMATE..... 1.303
(ADJUSTED FOR D.F.)..... 1.303
VARIABLE REGRESSION STD. ERROR OF COMPUTED
NUMBER COEFFICIENT REG. COEFF. T-VALUE
2 C.C0521 C.C0212 2.462
INTERCEPT C.62005
STEP 2
VARIABLE ENTERED..... 5
SUM OF SQUARES REDUCED IN THIS STEP.... 13.324
PROPORTION REDUCED IN THIS STEP..... 0.230
CUMULATIVE SUM OF SQUARES REDUCED..... 23.624
CUMULATIVE PROPORTION REDUCED..... 0.408 OF 57.867
FOR 2 VARIABLES ENTERED
MULTIPLE CORRELATION COEFFICIENT... 0.639
(ADJUSTED FOR D.F.)..... 0.622
F-VALUE FOR ANALYSIS OF VARIANCE... 9.314
STANDARD ERROR OF ESTIMATE..... 1.126
(ADJUSTED FOR D.F.)..... 1.146
VARIABLE REGRESSION STD. ERROR OF COMPUTED
NUMBER COEFFICIENT REG. COEFF. T-VALUE
2 0.C0632 C.C0186 3.397
5 C.C4316 C.C0132 3.241
INTERCEPT -1.20349
STEP 3
VARIABLE ENTERED..... 3
SUM OF SQUARES REDUCED IN THIS STEP.... 7.572
PROPORTION REDUCED IN THIS STEP..... 0.131
CUMULATIVE SUM OF SQUARES REDUCED..... 31.196
CUMULATIVE PROPORTION REDUCED..... 0.539 OF 57.867
FOR 3 VARIABLES ENTERED
MULTIPLE CORRELATION COEFFICIENT... 0.734
(ADJUSTED FOR D.F.)..... 0.711
F-VALUE FOR ANALYSIS OF VARIANCE... 10.137
STANDARD ERROR OF ESTIMATE..... 1.013
(ADJUSTED FOR D.F.)..... 1.050
VARIABLE REGRESSION STD. ERROR OF COMPUTED
NUMBER COEFFICIENT REG. COEFF. T-VALUE
2 C.C0744 C.C0172 4.318
5 C.C5363 C.C01258 4.265
3 C.C01497 C.C0551 2.717
INTERCEPT -5.53529
STEP 4
VARIABLE ENTERED..... 1
SUM OF SQUARES REDUCED IN THIS STEP.... 0.127
PROPORTION REDUCED IN THIS STEP..... 0.002
CUMULATIVE SUM OF SQUARES REDUCED..... 31.323
CUMULATIVE PROPORTION REDUCED..... 0.541 OF 57.867
FOR 4 VARIABLES ENTERED
MULTIPLE CORRELATION COEFFICIENT... 0.736
(ADJUSTED FOR D.F.)..... 0.699
F-VALUE FOR ANALYSIS OF VARIANCE... 7.375
STANDARD ERROR OF ESTIMATE..... 1.030
(ADJUSTED FOR D.F.)..... 1.088
VARIABLE REGRESSION STD. ERROR OF COMPUTED
NUMBER COEFFICIENT REG. COEFF. T-VALUE
2 C.C0741 C.C0175 4.222
5 C.C5076 C.C01524 3.332
3 C.C01493 C.C0561 2.662
1 C.C01226 C.C03541 0.346
INTERCEPT -5.94617
STEP 5
VARIABLE ENTERED..... 4
SUM OF SQUARES REDUCED IN THIS STEP.... 0.002
PROPORTION REDUCED IN THIS STEP..... 0.000
CUMULATIVE SUM OF SQUARES REDUCED..... 31.325
CUMULATIVE PROPORTION REDUCED..... 0.541 OF 57.867
FOR 5 VARIABLES ENTERED
MULTIPLE CORRELATION COEFFICIENT... 0.736
(ADJUSTED FOR D.F.)..... 0.684
F-VALUE FOR ANALYSIS OF VARIANCE... 5.665
STANDARD ERROR OF ESTIMATE..... 1.052
(ADJUSTED FOR D.F.)..... 1.133
VARIABLE REGRESSION STD. ERROR OF COMPUTED
NUMBER COEFFICIENT REG. COEFF. T-VALUE
2 C.C0739 C.C0186 3.965
5 C.C4919 C.C4141 1.188
3 C.C01504 C.C0635 2.369
1 C.C01242 C.C03635 0.342
4 C.C0151 C.C03679 0.041
INTERCEPT -6.07929
```

Figure 46. (Continued)

SELECTION..... 1

TABLE OF RESIDUALS

CASE NO.	Y VALUE	Y ESTIMATE	RESIDUAL
1	1.00000	0.48090	C.51910
2	2.00000	1.77670	C.22330
3	2.00000	2.14586	-C.14586
4	C.0	0.82880	-0.82880
5	2.00000	1.90522	C.09478
6	2.00000	1.52125	0.47875
7	3.00000	3.46447	-0.46447
8	2.00000	2.25887	-0.25887
9	3.00000	3.80259	-0.80259
10	0.0	1.02042	-1.02042
11	4.00000	2.49735	1.50265
12	1.00000	2.00065	-1.00065
13	1.00000	2.00736	-1.00736
14	1.00000	1.15308	-C.15308
15	3.00000	2.90446	C.09554
16	2.00000	1.83531	0.16469
17	3.00000	2.56004	C.43996
18	4.00000	3.45228	0.54772
19	4.00000	3.62661	C.37339
20	3.00000	2.60068	C.31932
21	4.00000	3.64886	C.35114
22	4.00000	1.86541	2.13459
23	1.00000	2.09863	-1.09863
24	C.0	1.97217	-1.97217
25	4.00000	1.41254	2.58746
26	1.00000	1.88027	-C.88027
27	3.00000	2.27646	C.72354
28	4.00000	4.51080	-C.51080
29	4.00000	3.95746	-C.04254
30	0.0	0.45458	-C.45458

SELECTION..... 2

DEPENDENT VARIABLE..... 6
 NUMBER OF VARIABLES FORCED..... 1
 NUMBER OF VARIABLES DELETED..... 1

STEP 1

VARIABLE ENTERED..... 3
 (FORCED VARIABLE)

SUM OF SQUARES REDUCED IN THIS STEP.... C.819
 PROPORTION REDUCED IN THIS STEP..... C.014
 CUMULATIVE SUM OF SQUARES REDUCED..... 0.819
 CUMULATIVE PROPORTION REDUCED..... C.014 DF 57.867

FOR 1 VARIABLES ENTERED

MULTIPLE CORRELATION COEFFICIENT... C.119
 (ADJUSTED FOR D.F.)..... C.119
 F-VALUE FOR ANALYSIS OF VARIANCE... C.402
 STANDARD ERROR OF ESTIMATE..... 1.427
 (ADJUSTED FOR D.F.)..... 1.427

VARIABLE NUMBER	REGRESSION COEFFICIENT	STD. ERROR OF REG. COEFF.	COMPUTED T-VALUE
3	0.00461	0.00728	C.634
INTERCEPT	1.15093		

STEP 2

VARIABLE ENTERED..... 2

SUM OF SQUARES REDUCED IN THIS STEP.... 11.738
 PROPORTION REDUCED IN THIS STEP..... 0.203
 CUMULATIVE SUM OF SQUARES REDUCED..... 12.557
 CUMULATIVE PROPORTION REDUCED..... C.217 DF 57.867

FOR 2 VARIABLES ENTERED

MULTIPLE CORRELATION COEFFICIENT... 0.466
 (ADJUSTED FOR D.F.)..... 0.435
 F-VALUE FOR ANALYSIS OF VARIANCE... 3.741
 STANDARD ERROR OF ESTIMATE..... 1.295
 (ADJUSTED FOR D.F.)..... 1.318

VARIABLE NUMBER	REGRESSION COEFFICIENT	STD. ERROR OF REG. COEFF.	COMPUTED T-VALUE
3	C.00778	C.00671	1.160
2	C.00565	C.00214	2.645
INTERCEPT	-1.42194		

STEP 3

VARIABLE ENTERED..... 5

SUM OF SQUARES REDUCED IN THIS STEP.... 18.639
 PROPORTION REDUCED IN THIS STEP..... 0.322
 CUMULATIVE SUM OF SQUARES REDUCED..... 31.196
 CUMULATIVE PROPORTION REDUCED..... C.539 DF 57.867

FOR 3 VARIABLES ENTERED

MULTIPLE CORRELATION COEFFICIENT... C.734
 (ADJUSTED FOR D.F.)..... 0.711
 F-VALUE FOR ANALYSIS OF VARIANCE... 10.137
 STANDARD ERROR OF ESTIMATE..... 1.013
 (ADJUSTED FOR D.F.)..... 1.050

VARIABLE NUMBER	REGRESSION COEFFICIENT	STD. ERROR OF REG. COEFF.	COMPUTED T-VALUE
3	C.01497	C.00551	2.717
2	C.00744	C.00172	4.318
5	C.05363	C.01258	4.263
INTERCEPT	-5.53528		

Figure 46. (Continued)

STEP 4

VARIABLE ENTERED..... 1

SUM OF SQUARES REDUCED IN THIS STEP.... 0.127
 PROPORTION REDUCED IN THIS STEP..... 0.002
 CUMULATIVE SUM OF SQUARES REDUCED..... 31.323
 CUMULATIVE PROPORTION REDUCED..... 0.541 DF 57.867

FOR 4 VARIABLES ENTERED

MULTIPLE CORRELATION COEFFICIENT... 0.736
 (ADJUSTED FOR D.F.)..... C.699
 F-VALUE FOR ANALYSIS OF VARIANCE... 7.375
 STANDARD ERROR OF ESTIMATE..... 1.030
 (ADJUSTED FOR D.F.)..... 1.098

VARIABLE NUMBER	REGRESSION COEFFICIENT	STD. ERROR OF REG. COEFF.	COMPUTED T-VALUE
3	C.01493	0.00561	2.662
2	C.00741	0.00175	4.222
5	C.05076	C.01524	3.332
1	C.71226	C.03541	C.346
INTERCEPT	-5.94617		

SELECTION..... 2

TABLE OF RESIDUALS

CASE NO.	Y VALUE	Y ESTIMATE	RESIDUAL
1	1.00000	0.48498	C.51502
2	2.00000	1.77220	C.22780
3	2.00000	2.14799	-C.14799
4	C.0	0.81528	-0.81528
5	2.00000	1.91082	0.08918
6	2.00000	1.52156	0.47844
7	3.00000	3.47954	-0.47954
8	2.00000	2.27251	-C.27251
9	3.00000	3.80533	-C.80533
10	0.0	1.02152	-1.02152
11	4.00000	2.50144	1.49856
12	1.00000	2.00604	-1.00604
13	1.00000	2.00340	-1.00340
14	1.00000	1.14922	-0.14922
15	3.00000	2.91121	0.08879
16	2.00000	1.82797	0.17203
17	3.00000	2.56125	0.43875
18	4.00000	3.43668	0.56332
19	4.00000	3.61723	0.38277
20	3.00000	2.68358	C.31642
21	4.00000	3.64918	0.35082
22	4.00000	1.85056	2.13434
23	1.00000	2.09898	-1.09898
24	C.0	1.96334	-1.96334
25	4.00000	1.40769	2.59231
26	1.00000	1.89582	-0.89582
27	3.00000	2.28895	0.71105
28	4.00000	4.50336	-C.50336
29	4.00000	3.94940	C.05060
30	C.0	0.44790	-0.44790

Figure 46. (Continued)

Program Modification

Program capacity can be increased or decreased by making changes in dimension statements. Input data in a different format can also be handled by providing a different format statement. If the user encounters problems with large or small numbers in his output, he may wish to change output format statements from F to E notation. In order to familiarize the user with the program modification, the following general rules are supplied in terms of the sample problem.

1. Changes in the dimension statements of the main program, STEPR:

- a. The dimension of arrays XBAR, STD, D, B, T, IDX, and L must each be greater than or equal to the number of variables, m. Since there are six variables in the sample problem, the value of m is 6.
- b. The dimension of array RX must be greater than or equal to the product of m x m. For the sample problem this product is 36 = 6 x 6.
- c. The dimension of array R must be greater than or equal to (m+1)m/2. For the sample problem this number is 21 = (6+1)6/2.

2. Changes in the input format statement of the special input subroutine, DATA:

Only the format statement for input data may be changed. If sample data are either one-, two-, or three-digit numbers, each row of data may be keypunched in six 3-column fields rather than using six-column fields as in the sample problem; in such case the format is changed to (6F3.0).

The special input subroutine, DATA, is normally written by the user to handle different formats for different problems. The user may modify this subroutine to perform testing of input data, transformation of data, and so on.

Operating Instructions

The sample program for stepwise multiple regression is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and data set 6 is used for output. A scratch tape (data set 13) written in binary mode is used as intermediate storage.

Error Messages

The following error conditions will result in messages:

1. The number of selection cards is not specified on the control card--NUMBER OF SELECTIONS NOT SPECIFIED. JOB TERMINATED. This error terminates execution of the job.
2. More than one dependent variable is specified on a selection card--SELECTION CARD (N) DOES NOT NAME ONE AND ONLY ONE DEPENDENT VARIABLE. SELECTION IGNORED.
3. A control digit is not 0, 1, 2, or 3 on a selection card--COLUMN (K) OF SELECTION CARD (N) IS IN ERROR. IT IS POSSIBLE THAT COLUMNS SUCCEEDING THAT COLUMN ARE ALSO INCORRECT. THE SELECTION IS IGNORED.
4. There are too few observations for estimation to take place--(N) OBSERVATIONS ARE TOO FEW TO ALLOW PARAMETER ESTIMATION FOR (M) VARIABLES. JOB TERMINATED.
5. The correlation matrix is singular or badly conditioned--EITHER THE MATRIX IS SINGULAR, OR THE RESIDUAL SUM OF SQUARES IS NEGATIVE IMPLYING EXTREME ILL-CONDITION. SELECTION IGNORED.

Two other error types are not detected:

1. If the number of observations is incorrect, the job deck will be such that results on that selection and on succeeding jobs will be incorrect. The user should take care in preparing his job deck according to instructions given above.
2. If some variable is constant over all observations, a zero standard deviation will occur, and

results for that selection will be incorrect or not forthcoming.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 45 seconds.

C	STEP 10
C		STEP 20
C	SAMPLE MAIN PROGRAM FOR STEP-WISE MULTIPLE REGRESSION - STEPR	STEP 30
C		STEP 40
C	PURPOSE	STEP 50
C	(1) READ THE PROBLEM PARAMETER CARD FOR A STEP-WISE MULTIPLE	STEP 60
C	REGRESSION. (2) READ SUBSET SELECTION CARDS. (3) CALL THE	STEP 70
C	SUBROUTINE TO CALCULATE MEANS, STANDARD DEVIATIONS, SIMPLE	STEP 80
C	CORRELATION COEFFICIENTS, AND (4) CALL THE SUBROUTINE TO	STEP 100
C	PERFORM EACH STEP OF REGRESSION ANALYSIS.	STEP 110
C		STEP 120
C	REMARKS	STEP 130
C	THE NUMBER OF OBSERVATIONS, N, MUST BE GREATER THAN M+2,	STEP 140
C	WHERE M IS THE NUMBER OF VARIABLES. IF SELECTION CARDS ARE	STEP 150
C	NOT PRESENT, THIS PROGRAM CAN NOT PERFORM STEP-WISE MULTIPLE	STEP 160
C	REGRESSION.	STEP 170
C		STEP 180
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	STEP 190
C	CORRE (WHICH, IN TURN, CALLS THE SUBROUTINE DATA)	STEP 200
C	MSTR (WHICH, IN TURN, CALLS THE SUBROUTINE LOC)	STEP 210
C	STPGG (WHICH, IN TURN, CALLS THE SUBROUTINE STOUT)	STEP 220
C		STEP 230
C	METHOD	STEP 240
C	REFER TO C. A. BENNETT AND N. L. FRANKLIN, 'STATISTICAL	STEP 250
C	ANALYSIS IN CHEMISTRY AND THE CHEMICAL INDUSTRY', JOHN WILEY	STEP 260
C	AND SONS, 1954, APPENDIX 6A.	STEP 270
C		STEP 280
C	STEP 290
C		STEP 300
C	THE FOLLOWING DIMENSIONS MUST BE GREATER THAN OR EQUAL TO THE	STEP 310
C	NUMBER OF VARIABLES, M..	STEP 320
C		STEP 330
C	DIMENSION XBAR(35),STD(35),D(35),B(35),T(35),DX(35),L(35)	STEP 340
C		STEP 350
C	THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE	STEP 360
C	PRODUCT OF M*M..	STEP 370
C		STEP 380
C	DIMENSION RX(1225)	STEP 390
C		STEP 400
C	THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE	STEP 410
C	(M+1)*M/2..	STEP 420
C		STEP 430
C	DIMENSION R(630)	STEP 440
C		STEP 450
C	THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO 5..	STEP 460
C		STEP 470
C	DIMENSION NSTEP(5)	STEP 480
C		STEP 490
C	THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO 11..	STEP 500
C		STEP 510
C	DIMENSION ANS(11)	STEP 520
C		STEP 530
C	STEP 540
C		STEP 550
C	IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE	STEP 560
C	C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION	STEP 570
C	STATEMENT WHICH FOLLOWS.	STEP 580
C		STEP 590
C	DOUBLE PRECISION XBAR,STD,RX,R,B,T,ANS,YES	STEP 600
C		STEP 610
C	THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS	STEP 620
C	APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS	STEP 630
C	ROUTINE.	STEP 640
C		STEP 650
C	STEP 660
C		STEP 670
C	1 FORMAT(A4,A2,I5,2I2,F6.0,I1)	STEP 680
C	2 FORMAT(5HNUMBER OF SELECTIONS NOT SPECIFIED. JOB TERMINATED.)	STEP 690
C	3 FORMAT(35HSTEP-WISE MULTIPLE REGRESSION.....A4,A2)	STEP 700
C	4 FORMAT(31H0VARIABLE MEAN STANDARD/4X,3HNO.16X,9HDEVIATION)STEP	STEP 710
C	5 FORMAT(4X,I2,F14.5,F12.5)	STEP 720
C	6 FORMAT(19H1CORRELATION MATRIX)	STEP 730
C	7 FORMAT(4H0R0M13/110F12.5)	STEP 740
C	8 FORMAT(12I1)	STEP 750
C	9 FORMAT(23H0NUMBER OF OBSERVATIONS)I5)	STEP 760
C	10 FORMAT(20H NUMBER OF VARIABLES)3X,I5)	STEP 770
C	11 FORMAT(21H NUMBER OF SELECTIONS)2X,I5)	STEP 780
C	12 FORMAT(28H0CONSTANT TO LIMIT VARIABLES)F9.5)	STEP 790
C	13 FORMAT(15H1SELECTION.....I2)	STEP 800
C	14 FORMAT(16X,10HITABLE OF RESIDUALS//9H CASE NO.5X,7HY VALUE5X,10HY ESTE	STEP 810
C	15 FORMAT(17,F15.5,2F14.5)	STEP 820
C	16 FORMAT(1H)	STEP 830
C	17 FORMAT(1H)	STEP 840
C	18 FORMAT(1H)	STEP 850
C	19 FORMAT(1H0,'****COLUMN',I4,' OF SELECTION CARD',I5,' IS IN ERROR.	STEP 860
C	1 T IT IS POSSIBLE THAT COLUMNS SUCCEEDING THAT COLUMN ARE ALSO	STEP 870
C	2/ INCORRECT. THE SELECTION IS IGNORED.****)	STEP 880
C	19 FORMAT(1H0,'****SELECTION CARD',I5,' DOES NOT NAME ONE AND ONLY ONSTEP	STEP 890
C	1E DEPENDENT VARIABLE. SELECTION IGNORED.****)	STEP 900
C	20 FORMAT(1H0,'****EITHER THE MATRIX IS SINGULAR, OR THE RESIDUAL SUMSTEP	STEP 910
C	1 OF SQUARES IS NEGATIVE IMPLYING EXTREME ILL CONDITION.*/', SELECSTEP	STEP 920
C	2TION IGNORED.****)	STEP 930
C	21 FORMAT(1H0,'****,I6,' OBSERVATIONS ARE TOO FEW TO ALLOW PARAMETERSTEP	STEP 940
C	1 ESTIMATION FOR',I5,' VARIABLES. JOB TERMINATED.****)	STEP 950
C		STEP 960
C	READ PROBLEM PARAMETER CARD	STEP 970
C		STEP 980
C	100 READ (5,1) PR1,PR2,N,M,NS,PCT,NR	STEP 990
C	PR1.....PROBLEM CODE (MAY BE ALPHAMERIC)	STEP1000
C	PR2.....PROBLEM CODE (CONTINUED)	STEP1010
C	NNUMBER OF OBSERVATIONS	STEP1020
C	MNUMBER OF VARIABLES	STEP1030
C	NS.....NUMBER OF SELECTIONS	STEP1040
C	PCT.....A CONSTANT VALUE OF PROPORTION OF SUM OF SQUARES THAT	STEP1050
C	WILL BE USED TO LIMIT VARIABLES ENTERING IN THE REGRES-	STEP1060
C	SION	STEP1070
C	NR.....OPTION CODE FOR TABLE OF RESIDUALS	STEP1080

```

C          0 - IF IT IS NOT DESIRED
C          1 - IF IT IS DESIRED
C
C      WRITE (6,3) PR1,PR2
C      WRITE (6,9) N
C      WRITE (6,10) M
C      IF(N-M=2) 101,101,102
101 WRITE(6,21) N,M
C      STOP
102 WRITE (6,11) NS
C      WRITE (6,12) PCT
C
C      LOGICAL TAPE 13 IS USED AS INTERMEDIATE STORAGE TO HOLD INPUT
C      DATA. THE INPUT DATA ARE WRITTEN ON LOGICAL TAPE 13 BY THE
C      SPECIAL INPUT SUBROUTINE NAMED DATA. THE STORED DATA MAY BE USED
C      FOR RESIDUAL ANALYSIS.
C
C      REWIND 13
C
C      IO=0
C      X=0.0
C
C      CALL COPRF (N,M,IO,X,XBAR,STD,RR,R,B,D,T)
C
C      REWIND 13
C
C      PRINT MEANS AND STANDARD DEVIATION
C
C      WRITE (6,4)
C      DO 105 I=1,M
105 WRITE (6,5) I,XBAR(I),STD(I)
C
C      PRINT CORRELATION MATRIX
C
C      WRITE (6,6)
C      DO 130 I=1,M
C      DO 125 J=1,M
C      IF(I=J) 110, 120, 120
110 K=I+(J-M)-J/2
C      GO TO 125
120 K=J+(I-M)-I/2
125 Y(J)=R(K)
130 WRITE (6,7) I,(T(J),J=1,M)
C
C      TEST NUMBER OF SELECTIONS
C
C      IF(NS) 135, 135, 140
135 WRITE (6,2)
C      GO TO 200
C
C      SAVE THE MATRIX OF SUMS OF CROSS-PRODUCTS OF DEVIATIONS
C
140 CALL MSTP (RX,R,M,0,1)
C
C      NSEL=1
C      GO TO 150
C
C      COPY THE MATRIX OF SUMS OF CROSS-PRODUCTS OF DEVIATIONS
C
145 CALL MSTR (K,RX,M,1,0)
C
C      READ A SELECTION CARD
C
150 WRITE (6,13) NSEL
C      READ (5,8) (IDX(J),J=1,M)
C
C      IN EACH POSITION OF IDX, ONE OF THE FOLLOWING CODES MUST BE
C      SPECIFIED..
C      0 OR BLANK - INDEPENDENT VARIABLE AVAILABLE FOR SELECTION
C      1 - INDEPENDENT VARIABLE TO BE FORCED IN REGRESSION
C      2 - VARIABLE TO BE DELETED
C      3 - DEPENDENT VARIABLE
C
C      N35=0
C      DO 155 K=1,M
C      IF (IDX(K)) 152,153,153
152 WRITE (6,18) K,NSEL
C      GO TO 185
153 IF (IDX(K)=3) 155,154,152
154 N35=N35+1
155 CONTINUE
C      IF (N35=1) 156,157,156
156 WRITE (6,19) NSEL
C      GO TO 185
C      CALL THE SUBROUTINE TO PERFORM A STEP-WISE REGRESSION ANALYSIS
157 CALL STPRG (M,N,RX,XBAR,IDX,PCT,NSTEP,ANS,L,B,STD,1,D,IER)
C      IF (IER) 158,159,158
158 WRITE (6,20)
C      GO TO 185
C
C      FIND WHETHER TO PRINT THE TABLE OF RESIDUALS
159 IF(NP) 185, 185, 160
C
C      PRINT THE TABLE OF RESIDUALS
C
160 WRITE (6,13) NSEL
C      WRITE (6,16)
C      WRITE (6,14)
C      MM=NSTEP(1)
C      DO 180 I=1,L
C      READ (13) (D(J),J=1,M)
C      YEST=ANS(9)
C      K=NSTEP(4)
C      DO 170 J=1,K
C      KK=L+J
170 YEST=YEST+B(J)*D(KK)
C      RESI=DMMI-YEST
180 WRITE (6,15) I,DMMI,YEST,RESI
C      REWIND 13
C
C      TEST TO SEE WHETHER ALL SELECTIONS ARE COMPLETED
185 IF(NSEL=NS) 190, 100, 100
190 NSEL=NSEL+1
C      WRITE (6,17)
C      GO TO 145
C
200 CONTINUE
C      END

```

```

STEP1090
STEP1100
STEP1110
STEP1120
STEP1130
STEP1140
STEP1150
STEP1160
STEP1170
STEP1180
STEP1190
STEP1200
STEP1210
STEP1220
STEP1230
STEP1240
STEP1250
STEP1260
STEP1270
STEP1280
STEP1290
STEP1300
STEP1310
STEP1320
STEP1330
STEP1340
STEP1350
STEP1360
STEP1370
STEP1380
STEP1390
STEP1400
STEP1410
STEP1420
STEP1430
STEP1440
STEP1450
STEP1460
STEP1470
STEP1480
STEP1490
STEP1500
STEP1510
STEP1520
STEP1530
STEP1540
STEP1550
STEP1560
STEP1570
STEP1580
STEP1590
STEP1600
STEP1610
STEP1620
STEP1630
STEP1640
STEP1650
STEP1660
STEP1670
STEP1680
STEP1690
STEP1700
STEP1710
STEP1720
STEP1730
STEP1740
STEP1750
STEP1760
STEP1770
STEP1780
STEP1790
STEP1800
STEP1810
STEP1820
STEP1830
STEP1840
STEP1850
STEP1860
STEP1870
STEP1880
STEP1890
STEP1900
STEP1910
STEP1920
STEP1930
STEP1940
STEP1950
STEP1960
STEP1970
STEP1980
STEP1990
STEP2000
STEP2010
STEP2020
STEP2030
STEP2040
STEP2050
STEP2060
STEP2070
STEP2080
STEP2090
STEP2100
STEP2110
STEP2120
STEP2130
STEP2140
STEP2150
STEP2160
STEP2170
STEP2180
STEP2190
STEP2200
STEP2210
STEP2220
STEP2230
STEP2240
STEP2250
STEP2260
STEP2270
STEP2280
STEP2290
STEP2300

```

CANONICAL CORRELATION

Problem Description

An analysis of the interrelations between two sets of variables measured on the same subjects is performed by this program. These variables are predictors in one set and criteria in the other set, but it is irrelevant whether the variables in the first set or in the second set are considered as the prediction variables. The canonical correlation, which gives the maximum correlation between linear functions of the two sets of variables, is calculated. χ^2 is also computed to test the significance of canonical correlation.

The sample problem for canonical correlation consists of four variables in the first set (left-hand side) and three variables in the second set (right-hand side) as presented in Table 6. These two sets of measurements have been made on 23 subjects.

Table 6. Sample Data for Canonical Correlation

Observation	First set				Second set		
	X ₁	X ₂	X ₃	X ₄	Y ₁	Y ₂	Y ₃
1	191	155	65	19	179	145	70
2	195	149	70	20	201	152	69
3	181	148	71	19	185	149	75
4	183	153	82	18	188	149	86
5	176	144	67	18	171	142	71
6	208	157	81	22	192	152	77
7	189	150	75	21	190	149	72
8	197	159	90	20	189	152	82
9	188	152	76	19	197	159	84
10	192	150	78	20	187	151	72
11	179	158	99	18	186	148	89
12	183	147	65	18	174	147	70
13	174	150	71	19	185	152	65
14	190	159	91	19	195	157	99
15	188	151	98	20	187	158	87
16	163	137	59	18	161	130	63
17	195	155	85	20	183	158	81
18	196	153	80	21	173	148	74
19	181	145	77	20	182	146	70
20	175	140	70	19	165	137	81
21	192	154	69	20	185	152	63
22	174	143	79	20	178	147	73
23	176	139	70	20	176	143	69

Program

Description

The canonical correlation program consists of the main routine named MCANO, a special input subroutine named DATA, and five subroutines from the Scientific Subroutine Package: CORRE, CANOR, MINV, NROOT, and EIGEN.

Capacity

The capacity of the sample program and the format required for data input have been set up as follows:

1. Up to 20 variables, including both the first set of variables (that is, left-hand variables) and the second set of variables (that is, right-hand variables) The number of variables in the first set must be greater than or equal to the number of variables in the second set.

2. Up to 99,999 observations

3. (12F6.0) format for input data cards

Therefore, if a problem satisfies the above conditions it is not necessary to modify the sample program. However, if there are more than 20 variables, dimension statements in the sample main program must be modified to handle the particular problem. Similarly, if input data cards are prepared using a different format, the input format in the input subroutine, DATA, must be modified. The general rules for program modification are described later.

Input

Control Card

One control card is required for each problem and is read by the main program, MCANO. This card is prepared as follows:

Columns	Contents	For Sample Problem
1 - 6	Problem number (may be alphanumeric)	SAMPLE
7 - 11	Number of observations	00023
12 - 13	Number of variables in the first set (that is, left-hand variables)*	04
14 - 15	Number of variables in the second set (that is, right-hand variables)	03

*The number of variables in the first set must be greater than or equal to the number of variables in the second set.

Leading zeros are not required to be keypunched.

Data Cards

Since input data are read into the computer one observation at a time, each row of data in Table 6 is keypunched on a separate card using the format (12F6.0). This format assumes twelve 6-column fields per card.

If there are more than twelve variables in a problem, each row of data is continued on the second

card until the last data point is keypunched. However, each row of data must begin on a new card.

Deck Setup

The deck setup is shown in Figure 47.

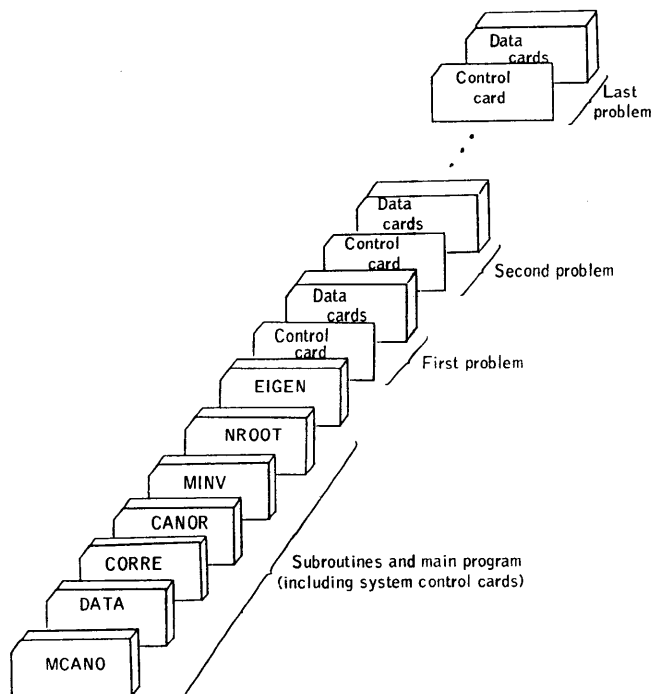


Figure 47. Deck setup (canonical correlation)

Sample

The listing of input cards for the sample problem is presented in Figure 48.

Output

Description

The output of the sample program for canonical correlation includes:

1. Means
2. Standard deviations
3. Correlation coefficients
4. Eigenvalues and corresponding canonical correlation
5. Lambda
6. Chi-square and degrees of freedom
7. Coefficients for left- and right-hand variables

Sample

Program Modification

The output listing for the sample problem is shown in Figure 49 of this sample problem.

Program capacity can be increased or decreased by making changes in dimension statements. Input data in a different format can also be handled by providing a specific format statement. In order to familiarize the user with the program modification, the following general rules are supplied in terms of the sample problem.

/DATA								10
SAMPLE00230403								20
191	155	65	19	179	145	70	30	
195	149	70	20	201	152	69	40	
181	148	71	19	185	149	75	50	
183	153	82	18	188	149	86	60	
176	144	67	18	171	142	71	70	
208	157	81	22	192	152	77	80	
189	150	75	21	190	149	72	90	
197	159	90	20	189	152	82	100	
188	152	76	19	197	159	84	110	
192	150	78	20	187	151	72	120	
179	158	99	18	196	148	89	130	
183	147	65	18	174	147	70	140	
174	150	71	19	185	152	65	150	
190	159	91	19	195	157	99	160	
188	151	98	20	187	158	87	170	
163	137	59	18	161	130	63	180	
195	155	85	20	183	158	81	190	
196	153	80	21	173	148	74	200	
181	145	77	20	182	146	70	210	
175	140	70	19	165	137	81	220	
192	154	69	20	185	152	63	230	
174	143	79	20	178	147	73	240	
176	139	70	20	176	143	69	250	

Figure 48. Input card listing (canonical correlation)

1. Changes in the dimension statements of the main program, MCANO:
 - a. The dimension of arrays XBAR, STD, CANR, CHISQ, and NDF must be greater than or equal to the total number of variables m ($m = p + q$, where p is the number of left-hand variables and q is the number of right-hand variables). Since there are seven variables, four on left and three on right, the value of m is 7.

```

CANONICAL CORRELATION.....SAMPLE
NO. OF OBSERVATIONS      23
NO. OF LEFT HAND VARIABLES  4
NO. OF RIGHT HAND VARIABLES 3

MEANS
185.47826   149.91304   76.86955   19.47826   183.00000   148.82608   75.73912

STANDARD DEVIATIONS
10.10342   6.31673   10.46338   1.08165   9.84424   6.73965   9.05647

CORRELATION COEFFICIENTS
ROW 1
1.00000   0.74852   0.37082   0.66441   0.62291   0.66080   0.24683
ROW 2
0.74852   1.00000   0.63252   0.22590   0.66811   0.72780   0.53194
ROW 3
0.37082   0.63252   1.00000   0.20657   0.47394   0.60169   0.79684
ROW 4
0.66441   0.22590   0.20657   1.00000   0.32870   0.34863   -0.10733
ROW 5
0.62291   0.66811   0.47394   0.32870   1.00000   0.82555   0.39258
ROW 6
0.66080   0.72780   0.60169   0.34863   0.82555   1.00000   0.47657
ROW 7
0.24683   0.53194   0.79684   -0.10733   0.39258   0.47657   1.00000

NUMBER OF LARGEST CORRESPONDING DEGREES
EIGENVALUES EIGENVALUE CANONICAL LAMBDA CHI-SQUARE OF
REMOVED REMAINING CORRELATION          FREEDOM
0           0.79880         0.89376   0.11598   40.93277   12
1           0.41910         0.64738   0.57644   10.46676   6
2           0.00767         0.08760   0.99233   9.14636    2

CANONICAL CORRELATION   0.89376
COEFFICIENTS FOR LEFT HAND VARIABLES
0.66310   -0.16059   1.05822   -0.56651
COEFFICIENTS FOR RIGHT HAND VARIABLES
-0.02133   0.44090   0.89710

CANONICAL CORRELATION   0.64738
COEFFICIENTS FOR LEFT HAND VARIABLES
0.09454   -0.83915   0.66305   -0.64892
COEFFICIENTS FOR RIGHT HAND VARIABLES
-0.43841   -0.55503   0.70692

CANONICAL CORRELATION   0.08760
COEFFICIENTS FOR LEFT HAND VARIABLES
0.02681   0.36955   -0.28827   -0.32496
COEFFICIENTS FOR RIGHT HAND VARIABLES
0.70325   -0.70384   0.10028

1F0031217
    
```

Figure 49. Output listing (canonical correlation)

- b. The dimension of array RX must be greater than or equal to the product of $m \times m$. For the sample problem this product is $49 = 7 \times 7$.
- c. The dimension of array R must be greater than or equal to $(m + 1) m/2$. For the sample problem this number is $28 = (7 + 1)7/2$.
- d. The dimension of array COEFL must be greater than or equal to the product of $p \times q$. For the sample problem this product is $12 = 4 \times 3$.
- e. The dimension of array COEFR must be greater than or equal to the product of $q \times q$. For the sample problem this product is $9 = 3 \times 3$.

2. Changes in the input format statement of the special input subroutine, DATA:

Only the format statement for input data may be changed. Since sample data are either two- or three-digit numbers, rather than using six-column fields as in the sample problem, each row of data may be keypunched in seven 3-column fields, and, if so, the format is changed to (7F3.0).

The special input subroutine, DATA, is normally written by the user to handle different formats for different problems. The user may modify this subroutine to perform testing of input data, transformation of data, and so on.

Operating Instructions

The sample program for canonical correlation is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and data set 6 is used for output.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 19 seconds.

C	MCAN 10
C	MCAN 20
C	MCAN 30
C	SAMPLE MAIN PROGRAM FOR CANONICAL CORRELATION - MCAN0	MCAN 40
C	PURPOSE	MCAN 50
C	(1) READ THE PROBLEM PARAMETER CARD FOR A CANONICAL	MCAN 60
C	CORRELATION, (2) CALL TWO SUBROUTINES TO CALCULATE SIMPLE	MCAN 70
C	CORRELATIONS, CANONICAL CORRELATIONS, CHI-SQUARES, DEGREES	MCAN 80
C	OF FREEDOM FOR CHI-SQUARES, AND COEFFICIENTS FOR LEFT AND	MCAN 90
C	RIGHT HAND VARIABLES, NAMELY CANONICAL VARIATES, AND (3)	MCAN 100
C	PRINT THE RESULTS.	MCAN 110
C	REMARKS	MCAN 120
C	(1) THE NUMBER OF LEFT HAND VARIABLES MUST BE GREATER THAN	MCAN 130
C	OR EQUAL TO THE NUMBER OF RIGHT HAND VARIABLES.	MCAN 140
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	MCAN 150
C	CORR (WHICH, IN TURN, CALLS THE INPUT SUBROUTINE NAMED	MCAN 160
C	DATA.)	MCAN 170
C	CANOR (WHICH, IN TURN, CALLS THE SUBROUTINES MINV AND	MCAN 180
C	NROOT. NROOT, IN TURN, CALLS THE SUBROUTINE EIGEN.)	MCAN 190
C	METHOD	MCAN 200
C		MCAN 210
C		MCAN 220
C		MCAN 230
C		MCAN 240

C	REFER TO W. W. COOLEY AND P. R. LOMNES, 'MULTIVARIATE PRO-	MCAN 250
C	CEDURES FOR THE BEHAVIORAL SCIENCES', JOHN WILEY AND SONS,	MCAN 260
C	1962, CHAPTER 3.	MCAN 270
C	MCAN 280
C	MCAN 290
C	MCAN 300
C	THE FOLLOWING DIMENSIONS MUST BE GREATER THAN OR EQUAL TO THE	MCAN 310
C	TOTAL NUMBER OF VARIABLES M (M=MP+MQ, WHERE MP IS THE NUMBER OF	MCAN 320
C	LEFT HAND VARIABLES, AND MQ IS THE NUMBER OF RIGHT HAND VARI-	MCAN 330
C	ABLES)..	MCAN 340
C	DIMENSION XBAR(20),STD(2),CANR(20),CHISQ(20),NDF(20)	MCAN 350
C	MCAN 360
C	THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE	MCAN 370
C	PRODUCT OF M*M..	MCAN 380
C	DIMENSION RX(400)	MCAN 390
C	MCAN 400
C	THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO	MCAN 410
C	(M+1)*M/2..	MCAN 420
C	DIMENSION R(210)	MCAN 430
C	MCAN 440
C	THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE	MCAN 450
C	PRODUCT OF MP*MQ..	MCAN 460
C	DIMENSION COEFL(400)	MCAN 470
C	MCAN 480
C	THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE	MCAN 490
C	PRODUCT OF MQ*MQ..	MCAN 500
C	DIMENSION COEFR(400)	MCAN 510
C	MCAN 520
C	MCAN 530
C	MCAN 540
C	MCAN 550
C	MCAN 560
C	MCAN 570
C	MCAN 580
C	MCAN 590
C	IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE	MCAN 600
C	C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION	MCAN 610
C	STATEMENT WHICH FOLLOWS.	MCAN 620
C	DOUBLE PRECISION XBAR,STD,RX,R,CANR,CHISQ,COEFL,COEFR	MCAN 630
C	MCAN 640
C	THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS	MCAN 650
C	APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS	MCAN 660
C	ROUTINE.	MCAN 670
C	MCAN 680
C	MCAN 690
C	MCAN 700
C	MCAN 710
C	MCAN 720
C	1 FORMAT(A4,A2,I5,Z12)	MCAN 730
C	2 FORMAT(27HCANONICAL CORRELATION:.....,A4,A2//22H NO. OF OBSERVAT	MCAN 740
C	IONS,8X,14Z9H NO. OF LEFT HAND VARIABLES,15/30H NO. OF RIGHT	MCAN 750
C	3 HAND VARIABLES,I4F1)	MCAN 760
C	3 FORMAT(6HMEANS/(8F15.5))	MCAN 770
C	4 FJRMAT(20HCSTANDARD DEVIATIONS/(8F15.5))	MCAN 780
C	5 FORMAT(25HOCORRELATION COEFFICIENTS)	MCAN 790
C	6 FORMAT(4HOROW,13/(10F12.5))	MCAN 800
C	7 FJRMAT(1HC//12H NUMBER OF,7X,7HLARGEST,7X,13HCORRESPONDING,31X,7MCAN	MCAN 810
C	1HDEGREES/13H EIGENVALUES,5X,10HEIGENVALUE,7X,9HCANONICAL,7X,6HLMCAN	MCAN 820
C	28DA,5X,10HCHI-SQUARE,7X,2HOF/4X,7HREMOVED,7X,9HREMAINING,7X,11HCORCAN	MCAN 830
C	3RELATION,32X,7HFREEDOM/)	MCAN 840
C	8 FORMAT(1H ,17,F19.5,F16.5,2F14.5,5X,(5)	MCAN 850
C	9 FORMAT(1H//22H CANONICAL CORRELATION,F12.5)	MCAN 860
C	10 FORMAT(39H COEFFICIENTS FOR LEFT HAND VARIABLES/(8F15.5))	MCAN 870
C	11 FORMAT(40H COEFFICIENTS FOR RIGHT HAND VARIABLES/(8F15.5))	MCAN 880
C	MCAN 890
C	MCAN 900
C	MCAN 910
C	MCAN 920
C	100 READ (5,1) PR,PR1,N,MP,MQ	MCAN 930
C	PR,.....PROBLEM NUMBER (MAY BE ALPHAMERIC)	MCAN 940
C	PR1,.....PROBLEM NUMBER (CONTINUED)	MCAN 950
C	N,.....NUMBER OF OBSERVATIONS	MCAN 960
C	MP,.....NUMBER OF LEFT HAND VARIABLES	MCAN 970
C	MQ,.....NUMBER OF RIGHT HAND VARIABLES	MCAN 980
C	MCAN 990
C	WRITE (6,2) PR,PR1,N,MP,MQ	MCAN1000
C	MCAN1010
C	M=MP+MQ	MCAN1020
C	IO=0	MCAN1030
C	X=0.0	MCAN1040
C	MCAN1050
C	CALL CORRE (N,M,IO,X,XBAR,STD,RX,R,CANR,CHISQ,COEFL)	MCAN1060
C	MCAN1070
C	PRINT MEANS, STANDARD DEVIATIONS, AND CORRELATION	MCAN1080
C	COEFFICIENTS OF ALL VARIABLES	MCAN1090
C	MCAN1100
C	MCAN1110
C	WRITE (6,3) (XBAR(I),I=1,M)	MCAN1120
C	WRITE (6,4) (STD(I),I=1,M)	MCAN1130
C	WRITE (6,5)	MCAN1140
C	DD 160 I=1,M	MCAN1150
C	DD 150 J=1,M	MCAN1160
C	IF(I-J) 120, 130, 130	MCAN1170
C	120 L=I+(J+J-1)/2	MCAN1180
C	GO TO 140	MCAN1190
C	130 L=J+(I+I-1)/2	MCAN1200
C	140 CANR(J)=R(L)	MCAN1210
C	150 CONTINUE	MCAN1220
C	160 WRITE (6,6) I,(CANR(J),J=1,M)	MCAN1230
C	MCAN1240
C	CALL CANOR (N,MP,MQ,R,XBAR,STD,CANR,CHISQ,NDF,COEFR,COEFL,RX)	MCAN1250
C	MCAN1260
C	PRINT EIGENVALUES, CANONICAL CORRELATIONS, LAMBDA, CHI-SQUARES,	MCAN1270
C	DEGREES OF FREEDOMS	MCAN1280
C	MCAN1290
C	WRITE (6,7)	MCAN1300
C	DO 170 I=1,MQ	MCAN1310
C	N1=I-1	MCAN1320
C	MCAN1330
C	TEST WHETHER EIGENVALUE IS GREATER THAN ZERO	MCAN1340
C	MCAN1350
C	IF(XBAR(I)) 165, 165, 170	MCAN1360
C	165 MM=N1	MCAN1370
C	GJ TO 175	MCAN1380
C	170 WRITE (6,8) N1,XBAR(I),CANR(I),STD(I),CHISQ(I),NDF(I)	MCAN1390
C	MM=MQ	MCAN1400
C	MCAN1410
C	PRINT CANONICAL COEFFICIENTS	MCAN1420
C	MCAN1430
C	175 N1=0	MCAN1440
C	N2=0	MCAN1450
C	DO 200 I=1,MH	MCAN1460
C	WRITE (6,9) CANR(I)	MCAN1470
C	DO 180 J=1,MP	MCAN1480
C	N1=N1+1	MCAN1490
C	180 XBAR(J)=COEFL(N1)	MCAN1500
C	WRITE (6,10) (XBAR(J),J=1,MP)	MCAN1510
C	DO 190 J=1,MQ	MCAN1520
C	N2=N2+1	MCAN1530
C	190 XBAR(J)=COEFR(N2)	MCAN1540
C	WRITE (6,11) (XBAR(J),J=1,MQ)	MCAN1550
C	200 CONTINUE	MCAN1560
C	GO TO 100	MCAN1570
C	END	

ANALYSIS OF VARIANCE

Problem Description

An analysis of variance is performed for a factorial design by use of three special operators suggested by H. O. Hartley.* The analysis of many other designs can be derived by reducing them first to factorial designs, and then pooling certain components of the analysis-of-variance table.

Consider a three-factor factorial experiment in a randomized complete block design as presented in Table 7. In this experiment, factor A has four levels, factors B and C have three levels, and the entire experiment is replicated twice. The replicates are completely unrelated and do not constitute a factor. Nevertheless, for the purpose of this program a four-factor experiment (with factors A, B, C, and R) is assumed. Thus, each element of the data in Table 5 may be represented in the form:

$$x_{\text{abcr}} \quad \text{where} \quad \begin{aligned} a &= 1, 2, 3, 4 \\ b &= 1, 2, 3 \\ c &= 1, 2, 3 \\ r &= 1, 2 \end{aligned}$$

The general principle of the analysis-of-variance procedure used in the program is first to perform a formal factorial analysis and then to pool certain components in accordance with summary instructions that specifically apply to the particular design. The summary instructions for four different designs are presented in the output section.

Program

Description

The analysis-of-variance program consists of the main routine named ANOVA, and three subroutines from the Scientific Subroutine Package: AVDAT, AVCAL, and MEANQ.

*H. O. Hartley, "Analysis of Variance", Mathematical Methods for Digital Computers, edited by A. Ralston and H. Wilf, John Wiley and Sons, 1962, Chapter 20.

Table 7. Sample Data for Analysis of Variance

Replicate (Block)		b ₁				b ₂				b ₃			
		a ₁	a ₂	a ₃	a ₄	a ₁	a ₂	a ₃	a ₄	a ₁	a ₂	a ₃	a ₄
r ₁	c ₁	3	10	9	8	24	8	9	3	2	8	9	8
	c ₂	4	12	3	9	22	7	16	2	2	2	7	2
	c ₃	5	10	5	8	23	9	17	3	2	8	6	3
r ₂	c ₁	2	14	9	13	29	16	11	3	2	7	5	3
	c ₂	7	11	5	8	28	18	10	6	6	6	5	9
	c ₃	9	10	27	8	28	16	11	7	8	9	8	15

Capacity

The capacity of the sample program and the format required for data input have been set up as follows:

1. Up to six-factor factorial experiment
2. Up to a total of 3000 data points. The total number of data points in a problem is calculated by the formula:

$$T = \prod_{i=1}^k (\text{LEVEL}_i + 1)$$

where LEVEL_i = number of levels of ith factor
 k = number of factors
 Π = notation for cumulative multiplication

3. (12F6.0) format for input data cards

Therefore, if a problem satisfies the above conditions it is not necessary to modify the sample program. However, if there are more than six factors or if the total number of data points is more than 3000, dimension statements in the sample main program must be modified. Similarly, if input data cards are prepared using a different format, the input format statement in the sample main program must be modified. The general rules for program modifications are described later.

Input

Control Card

One control card is required for each problem and is read by the main program, ANOVA. This card is prepared as follows:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem</u>
1- 6	Problem number (may be alphameric)	SAMPLE
7- 8	Number of factors	04
9-15	Blank	
{ 16	Label for the first factor	A
{ 17-20	Number of levels of the first factor	0004
{ 21	Label for the second factor	B
{ 22-25	Number of levels of the second factor	0003
{ 26	Label for the third factor	C
{ 27-30	Number of levels of the third factor	0003
{ 31	Label for the fourth factor	R
{ 32-35	Number of levels of the fourth factor	0002
.		
.		
.		
{ 66	Label for the eleventh factor (if present)	
{ 67-70	Number of levels of the eleventh factor	

If there are more than eleven factors, continue to the second card in the same manner.

<u>Columns</u>	<u>Contents</u>
{ 1	Label for the twelfth factor
{ 2 - 5	Number of levels of the twelfth factor
⋮	
etc.	

Leading zeros are not required to be keypunched.

Data Cards

Data are keypunched in the following order: X₁₁₁₁, X₂₁₁₁, X₃₁₁₁, X₄₁₁₁, X₁₂₁₁, X₂₂₁₁, X₃₂₁₁, ..., X₄₃₃₂. In other words, the innermost subscript is changed first -- namely, the first factor -- and then the second, third, and fourth subscripts. In the sample problem, the first subscript corresponds to factor A, and the second, third, and fourth subscripts to factors B, C, and R. Since the number of data fields per card is twelve, implied by the format (12F6.0), each row in Table 7 is keypunched on a separate card.

Deck Setup

The deck setup is shown in Figure 50.

Sample

The listing of input cards for the sample problem is presented in Figure 51.

Output

Description

The output of the sample analysis-of-variance program includes the numbers of levels of factors as input, the mean of all data, and the table of analysis of variance. In order to complete the analysis of variance properly, however, certain components in the table may need to be pooled. This is accomplished by means of summary instructions that specifically apply to the particular experiment. These are presented in Table 8.

As mentioned earlier, the sample problem is a randomized complete block design with three factors replicated twice. Therefore, it is necessary to pool certain components in the table of analysis of variance shown in Figure 52. Specifically, the components AR, BR, ABR, CR, ACR, BCR, and ABCR are combined into one value called the error term. The result is indicated in Figure 52. Since these data are purely hypothetical, interpretations of the various effects are not made.

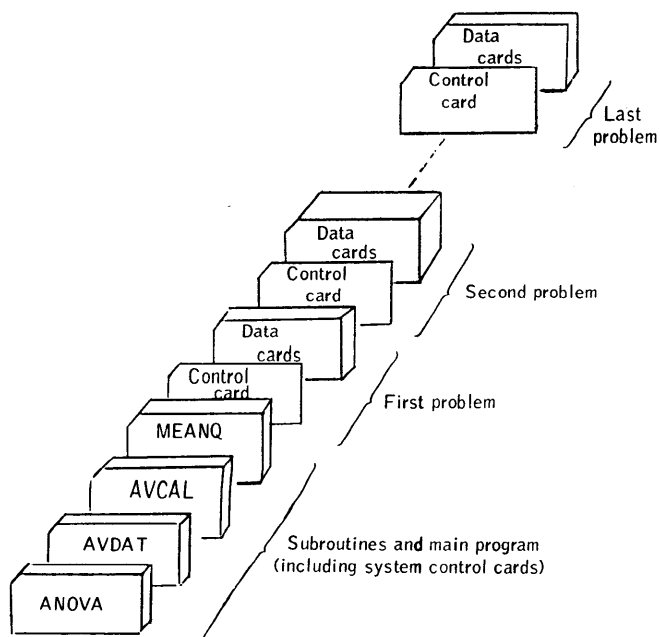


Figure 50. Deck setup (analysis of variance)

Table 8. Instructions to Summarize Components of Analysis of Variance

	Single Classification with Replicates	Two-way Classification with Cell Replicates	Randomized Complete Block with Two Factors	Split Plot
(Input)				
Factor No. 1	Groups = A	Rows = A	Factor 1 = A	Main treatment = A
2	Replicates = R	Columns = B	Factor 2 = B	Subtreatment = B
3		Replicates = R	Blocks = R	Blocks = R
(Output)				
Sums of squares	A R AR	A B AB R AR BR ABR	A B AB R AR BR ABR	A B AB R AR BR ABR
Summary instruction	Error = R + (AR)	Error = R + (AR) + (BR) + (ABR)	Error = (AR) + (BR) + (ABR)	Error = (BR) + (ABR) (b)
Analysis of variance	Groups A Error	Rows A Columns B Interaction AB Error	Factor 1 A Factor 2 B Interaction AB Blocks R Error	Main treatment A Blocks R Error (a) AR Subtreatment B Interaction AB Error (b)

ANALYSIS OF VARIANCE-----SAMPLE

LEVELS OF FACTORS

A	4
B	3
C	3
R	2

GRAND MEAN 9.40278

SOURCE OF VARIATION	SUMS OF SQUARES	DEGREES OF FREEDOM	MEAN SQUARES
A	229.04166	3	76.34721
B	722.69434	2	361.34717
AB	1382.08325	6	230.34720
C	55.11110	2	27.55554
AC	42.00000	6	7.00000
BC	13.13889	4	3.28472
ABC	140.75000	12	11.72917
R	141.68054	1	141.68054
AR	18.81944	3	6.27315
BR	0.02778	2	0.01389
ABR	176.97221	6	29.49536
CR	40.77777	2	20.38889
ACR	50.55554	6	8.42592
BCR	62.63889	4	15.65972
ABCR	151.02777	12	12.58565
TOTAL	3233.31763	71	

(Block) Error = (506.81940)* (35)* (14.48054)*

*summarized after the computer output is obtained.

Figure 52. Output listing (analysis of variance)

Sample

The output listing for the sample problem is shown in Figure 52.

Program Modification

Program capacity can be increased or decreased by making changes in dimension statements. Input data in a different format can also be handled by providing a specific format statement. In order to familiarize the user with the program modification, the following general rules are supplied in terms of the sample problem.

1. Changes in the dimension statements of the main program, ANOVA:
 - a. The dimension of array X must be greater than or equal to the total number of data points as calculated by the formula in the program capacity section above. For the sample problem, the total number of data points is $240 = (4+1)(3+1)(3+1)(2+1)$.

- b. The dimension of arrays HEAD, LEVEL, ISTEP, KOUNT, and LASTS must be greater than or equal to the number of factors, k. Since there are four factors in the sample problem (4 = 3 original factors + 1 pseudo factor), the value of k is 4.
 - c. The dimension of arrays SUMSQ, NDF, and SMEAN must be greater than or equal to $n = 2^k - 1$, where k is the number of factors. For the sample problem, the value of n is $15 = 2^4 - 1$.
2. Change in the input format statement of the main program, ANOVA:

Only the format statement for input data may be changed. Since sample data are either one- or two-digit numbers, rather than using six-column fields as in the sample problem, each data may be keypunched in a two-column field, and, if so, the format is changed to (12F2.0). This format assumes twelve 2-column fields per card, beginning in column 1.

```

/ DATA
SAMPLE04 10
          4000480003C0003R00C2 20
3 10 9 8 24 8 9 3 2 8 9 8 10
4 12 3 9 22 7 16 2 2 2 7 2 40
5 10 5 8 23 9 17 3 2 8 6 3 50
2 14 9 13 29 16 11 3 2 7 5 3 60
7 11 5 8 28 19 10 6 6 6 5 9 70
9 10 27 8 28 16 11 7 8 9 8 15 80
    
```

Figure 51. Input listing (analysis of variance)

Operating Instructions

The sample analysis-of-variance program is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and data set 6 is used for output.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 11 seconds.

```
C ..... ANOV 19
C ..... ANOV 20
C ..... ANOV 30
C ..... ANOV 40
C ..... ANOV 50
C ..... ANOV 60
C ..... ANOV 70
C ..... ANOV 80
C ..... ANOV 90
C ..... ANOV 100
C ..... ANOV 110
C ..... ANOV 120
C ..... ANOV 130
C ..... ANOV 140
C ..... ANOV 150
C ..... ANOV 160
C ..... ANOV 170
C ..... ANOV 180
C ..... ANOV 190
C ..... ANOV 200
C ..... ANOV 210
C ..... ANOV 220
C ..... ANOV 230
C ..... ANOV 240
C ..... ANOV 250
C ..... ANOV 260
C ..... ANOV 270
C ..... ANOV 280
C ..... ANOV 290
C ..... ANOV 300
C ..... ANOV 310
C ..... ANOV 320
C ..... ANOV 330
C ..... ANOV 340
C ..... ANOV 350
C ..... ANOV 360
C ..... ANOV 370
C ..... ANOV 380
C ..... ANOV 390
C ..... ANOV 400
C ..... ANOV 410
C ..... ANOV 420
C ..... ANOV 430
C ..... ANOV 440
C ..... ANOV 450
C ..... ANOV 460
C ..... ANOV 470
C ..... ANOV 480
C ..... ANOV 490
C ..... ANOV 500
C ..... ANOV 510
C ..... ANOV 520
C ..... ANOV 530
C ..... ANOV 540
C ..... ANOV 550
C ..... ANOV 560
C ..... ANOV 570
C ..... ANOV 580
C ..... ANOV 590
C ..... ANOV 600
C ..... ANOV 610
C ..... ANOV 620
C ..... ANOV 630
C ..... ANOV 640
C ..... ANOV 650
C ..... ANOV 660
C ..... ANOV 670
C ..... ANOV 680
C ..... ANOV 690
C ..... ANOV 700
C ..... ANOV 710
C ..... ANOV 720
C ..... ANOV 730
C ..... ANOV 740
C ..... ANOV 750
C ..... ANOV 760
C ..... ANOV 770
C ..... ANOV 780
C ..... ANOV 790
C ..... ANOV 800
C ..... ANOV 810
C ..... ANOV 820
C ..... ANOV 830
C ..... ANOV 840
C ..... ANOV 850
C ..... ANOV 860
C ..... ANOV 870
C ..... ANOV 880
C ..... ANOV 890
C ..... ANOV 900
C ..... ANOV 910
C ..... ANOV 920
C ..... ANOV 930
C ..... ANOV 940
C ..... ANOV 950
C ..... ANOV 960
C ..... ANOV 970
C ..... ANOV 980
C ..... ANOV 990
C ..... ANOV 1000
C ..... ANOV 1010
C ..... ANOV 1020
C ..... ANOV 1030
C ..... ANOV 1040
C ..... ANOV 1050
C ..... ANOV 1060
C ..... ANOV 1070
C ..... ANOV 1080
C ..... ANOV 1090
C ..... ANOV 1100
C ..... ANOV 1110
C ..... ANOV 1120
C ..... ANOV 1130
C ..... ANOV 1140
C ..... ANOV 1150
C ..... ANOV 1160
C ..... ANOV 1170
C ..... ANOV 1180
C ..... ANOV 1190
C ..... ANOV 1200
C ..... ANOV 1210
C ..... ANOV 1220
C ..... ANOV 1230
C ..... ANOV 1240
C ..... ANOV 1250
C ..... ANOV 1260
C ..... ANOV 1270
C ..... ANOV 1280
C ..... ANOV 1290
C ..... ANOV 1300
C ..... ANOV 1310
C ..... ANOV 1320
C ..... ANOV 1330
C ..... ANOV 1340
C ..... ANOV 1350
C ..... ANOV 1360
C ..... ANOV 1370
C ..... ANOV 1380
C ..... ANOV 1390
C ..... ANOV 1400
C ..... ANOV 1410
C ..... ANOV 1420
```

```
110 FMT(1)=BLANK ANOV1180
NN=0 ANOV1190
SUM=7.0 ANOV1200
120 NN=NN+1 ANOV1210
L=0 ANOV1220
DO 140 I=1,K ANOV1230
FMT(I)=BLANK ANOV1240
IF(ISTEP(I)) 130, 140, 130 ANOV1250
130 L=L+1 ANOV1260
FMT(L)=HEAD(I) ANOV1270
140 CONTINUE ANOV1280
WRITE (6,6) (FMT(I),I=1,L5),SUMSQ(NN),NDF(NN),SMEAN(NN) ANOV1290
SUM=SUM+SUMSQ(NN) ANOV1300
IF(NN-LL) 145, 170, 170 ANOV1310
145 DO 160 I=1,K ANOV1320
IF(ISTEP(I)) 147, 150, 147 ANOV1330
147 ISTEP(I)=0 ANOV1340
GO TO 160 ANOV1350
150 ISTEP(I)=1 ANOV1360
GO TO 120 ANOV1370
160 CONTINUE ANOV1380
170 NN=N ANOV1390
WRITE (6,7) SUM,N ANOV1400
GO TO 100 ANOV1410
END ANOV1420
```

DISCRIMINANT ANALYSIS

Problem Description

A set of linear functions is calculated from data on many groups for the purpose of classifying new individuals into one of several groups. The classification of an individual into a group is performed by evaluating each of the calculated linear functions, then finding the group for which the value is the largest.

The sample problem for discriminant analysis consists of four groups of observations as presented in Table 9. The number of observations in the first group is eight; the second group, seven; the third group, seven; and the fourth group, eight. The number of variables is six in all groups.

Program

Description

The discriminant analysis program consists of the main routine named MDISC, and three subroutines from the Scientific Subroutine Package: DMATX, MINV, and DISCR.

Capacity

The capacity of the sample program and the format required for data input have been set up as follows:

1. Up to five groups
2. Up to ten variables
3. Up to a total number of 250 observations in all groups combined
4. (12F6.0) format for input data cards

Therefore, if a problem satisfies the above conditions it is not necessary to modify the sample program. However, if there are more than five groups, more than ten variables, or more than 250 observations, dimension statements in the sample

Table 9. Sample Data for Discriminant Analysis

	Observation	X ₁	X ₂	X ₃	X ₄	X ₅	X ₆
Group 1	1	3	10	9	8	24	8
	2	4	12	3	8	22	7
	3	9	3	2	8	9	8
	4	16	2	2	2	7	2
	5	5	10	5	8	23	9
	6	17	3	2	8	6	3
	7	2	10	9	8	29	16
	8	7	10	5	8	28	18
Group 2	1	9	10	27	8	28	16
	2	11	7	8	9	8	15
	3	8	10	2	8	27	16
	4	1	6	8	14	14	13
	5	7	8	9	6	18	2
	6	7	9	8	2	19	9
	7	7	10	5	8	27	17
Group 3	1	3	11	9	15	20	10
	2	9	4	10	7	9	9
	3	4	13	10	7	21	15
	4	8	5	16	16	16	7
	5	6	9	10	5	23	11
	6	8	10	5	8	27	16
	7	17	3	2	7	6	3
Group 4	1	3	10	8	8	23	8
	2	4	12	3	8	23	7
	3	9	3	2	8	21	7
	4	15	2	2	2	7	2
	5	9	10	26	8	27	16
	6	8	9	2	8	26	16
	7	7	8	6	9	18	2
	8	7	10	5	8	26	16

main program must be modified to handle this particular problem. Similarly, if input data cards are prepared using a different format, the input format statement in the sample main program must be modified. The general rules for program modification are described later.

Input

Control Card

One control card is required for each problem and is read by the main program, MDISC. This card is prepared as follows:

Columns	Contents	For Sample Problem
1- 6	Problem number (may be alphameric)	SAMPLE
7- 8	Number of groups	04
9-10	Number of variables	06
11-15	Number of observations in first group	00008
16-20	Number of observations in second group	00007
21-25	Number of observations in third group	00007
26-30	Number of observations in fourth group	00008
:		
65-70	Number of observations in twelfth group (if present)	

If there are more than twelve groups in the problem, continue to the second card in the same manner.

Columns	Contents
1- 5	Number of observations in thirteenth group
6-10	Number of observations in fourteenth group

Leading zeros are not required to be keypunched.

Data Cards

Since input data are read into the computer one observation at a time, each row of data in Table 9 is keypunched on a separate card using the format (12F6.0). This format assumes twelve 6-column fields per card.

If there are more than twelve variables in a problem, each row of data is continued on the second and third cards until the last data point is keypunched. However, each row of data must begin on a new card.

Deck Setup

The deck setup is shown in Figure 53.

Sample

The listing of input cards for the sample problem is presented in Figure 54.

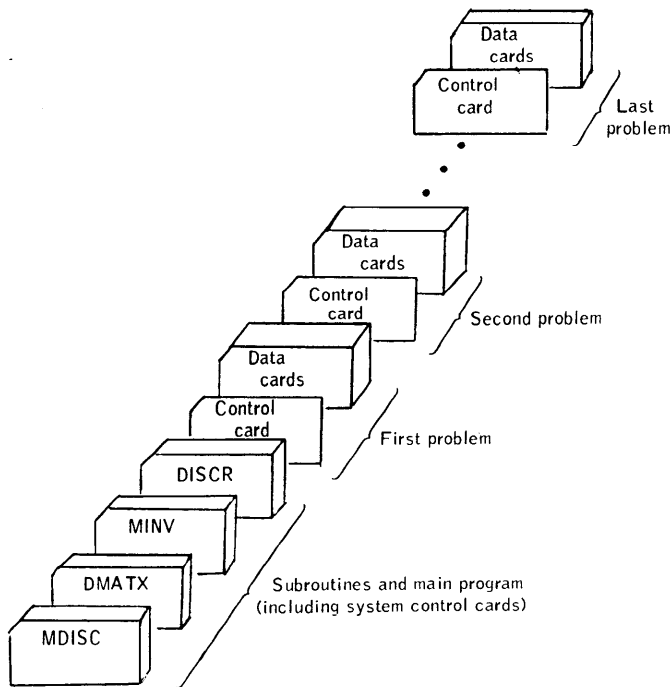


Figure 53. Deck setup (discriminant analysis)

Output

Description

The output of the sample program for discriminant analysis includes:

1. Means of variables in each group
2. Pooled dispersion matrix
3. Common means
4. Generalized Mahalanobis D-square
5. Constant and coefficients of each discriminant function
6. Probability associated with the largest discriminant function evaluated for each observation.

```

/ DATA
SAMPLEC4060C00B000C70C90T00008
3 10 9 8 24 7 8
4 12 3 8 22 7
9 3 2 8 9 5
16 2 2 2 7 2
5 10 5 8 23 9
17 3 2 8 6 3
2 10 9 8 29 16
7 10 5 8 28 18
9 10 27 8 28 16
11 7 8 9 8 15
8 10 2 8 27 16
1 6 8 14 14 13
7 8 9 6 18 2
7 9 8 2 19 9
3 10 5 8 27 17
3 11 9 15 20 10
9 4 10 7 9 9
4 13 10 7 21 15
8 5 16 16 16 7
6 9 10 5 23 11
8 10 5 8 27 16
17 3 2 7 6 3
3 10 8 8 23 8
4 12 3 8 23 7
9 3 2 8 21 7
15 2 2 2 7 2
9 10 26 8 27 16
8 9 2 8 26 16
7 8 6 9 18 2
7 10 5 8 26 16

```

Figure 54. Input listing (discriminant analysis)

Sample

The output listing for the sample problem is shown in Figure 55.

Program Modification

Program capacity can be increased or decreased by making changes in dimension statements. Input data in a different format can also be handled by providing a specific format statement. In order to familiarize the user with the program modification, the following general rules are supplied in terms of the sample problem.

1. Changes in the dimension statements of the main program, MDISC:
 - a. The dimension of array N must be greater than or equal to the number of groups, k. Since there are four groups in the sample problem, the value of k is 4.
 - b. The dimension of array CMEAN must be greater than or equal to the number of variables, m. Since there are six variables in the sample problem, the value of m is 6.
 - c. The dimension of array XBAR must be greater than or equal to the product of m times k. For the sample problem this product is $24 = 6 \times 4$.
 - d. The dimension of array C must be greater than or equal to the product of $(m+1)k$. For the sample problem this product is $28 = (6+1)4$.
 - e. The dimension of array D must be greater than or equal to the product of m times m. For the sample problem this product is $36 = 6 \times 6$.
 - f. The dimension of arrays P and LG must be greater than or equal to the total number of observations in all groups combined, t. For the sample problem this total is $30 = 8 + 7 + 7 + 8$.

```

DISCRIMINANT ANALYSIS.....SAMPLE
NUMBER OF GROUPS          4
NUMBER OF VARIABLES       6
SAMPLE SIZES...
GROUP
  1          8
  2          7
  3          7
  4          8
GROUP 1 MEANS
7.87500      7.50000      4.62500      7.25000      18.90000      8.87500
GROUP 2 MEANS
7.14286      8.57143      5.57143      7.85714      20.14285      12.57143
GROUP 3 MEANS
7.85714      7.85714      8.85714      5.28571      17.42856      10.14286
GROUP 4 MEANS
7.75000      8.00000      6.75000      7.37500      21.37500      9.25000

```

Figure 55. Output listing (discriminant analysis)

```

POOLED DISPERSION MATRIX
ROW 1 19.61876 -11.16208 -5.21497 -6.09890 -22.74855 -9.54052
ROW 2 -11.16208 11.54505 5.61813 1.91758 22.60982 10.66757
ROW 3 -5.21497 5.61813 35.45938 3.93681 16.23486 9.34546
ROW 4 -6.09890 1.91758 3.93681 9.83310 4.62156 3.83791
ROW 5 -22.74855 22.60982 16.23486 4.62156 82.78633 30.18262
ROW 6 -9.54052 10.66757 9.34546 3.83791 30.18262 29.57480

COMMON MEANS
7.66667 7.96667 7.33333 7.90000 19.39998 10.13332

GENERALIZED MAHALANOBIS D-SQUARE
12.76063

DISCRIMINANT FUNCTION 1
CONSTANT * COEFFICIENTS
-28.49431 * 2.63870 2.12205 -0.17167 1.91198 0.59476 -0.40477

DISCRIMINANT FUNCTION 2
CONSTANT * COEFFICIENTS
-29.21017 * 2.61930 2.25230 -0.04816 1.88319 0.43732 -0.21784

DISCRIMINANT FUNCTION 3
CONSTANT * COEFFICIENTS
-31.86435 * 2.74452 2.39588 -0.06457 2.13260 0.42619 -0.32718

DISCRIMINANT FUNCTION 4
CONSTANT * COEFFICIENTS
-30.82028 * 2.71860 2.63937 -0.13352 1.94539 0.71677 -0.48760

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION
GROUP 1 PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION
OBSERVATION 1 0.39065 4
2 0.37045 1
3 0.36261 1
4 0.44190 1
5 0.34456 1
6 0.44215 3
7 0.31787 2
8 0.29274 2

GROUP 2 PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION
OBSERVATION 1 0.51029 2
2 0.50582 3
3 0.34760 4
4 0.43130 3
5 0.44882 4
6 0.36467 2
7 0.28515 2

GROUP 3 PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION
OBSERVATION 1 0.67811 3
2 0.46829 2
3 0.54636 2
4 0.66888 2
5 0.30602 2
6 0.33043 4
7 0.39005 3

GROUP 4 PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION
OBSERVATION 1 0.33727 4
2 0.37475 1
3 0.42340 4
4 0.45697 1
5 0.52175 2
6 0.34061 4
7 0.43135 4
8 0.27849 1

```

Figure 55. Output listing (discriminant analysis) (Continued)

g. The dimension of array X must be greater than or equal to the total number of data points that is equal to the product of t times m. For the sample this product is $180 = 30 \times 6$.

2. Changes in the input format statement of the main program, MDISC:

Only the format statement for input data may be changed. Since sample data are either one- or two-digit numbers, rather than using six-column fields as in the sample problem, each row of data may be keypunched in two-column fields, and, if so, the format is changed to (6F2.0). This format assumes six 2-column fields per card, beginning in column 1.

Operating Instructions

The sample program for discriminant analysis is a standard FORTRAN program. Special operating

instructions are not required. Data set 5 is used for input, and data set 6 is used for output.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 30 seconds.

```

C MDIS 10
C MDIS 20
C MDIS 30
C SAMPLE MAIN PROGRAM FOR DISCRIMINANT ANALYSIS - MDISC MDIS 40
C MDIS 50
C PURPOSE MDIS 60
C (1) READ THE PROBLEM PARAMETER CARD AND DATA FOR DISCRIMINANT ANALYSIS, (2) CALL THREE SUBROUTINES TO CALCULATE VARI- MDIS 70
C ABLE MEANS IN EACH GROUP, POOLED DISPERSION MATRIX, COMMON MEANS OF MDIS 80
C VARIABLES, GENERALIZED MAHALANOBIS D SQUARE, COEFFICIENTS OF DISCRIMINANT FUNCTIONS, AND PROBABILITY MDIS 100
C ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION OF EACH CASE IN EACH GROUP, AND (3) PRINT THE RESULTS. MDIS 110
C MDIS 120
C MDIS 130
C MDIS 140
C REMARKS MDIS 150
C THE NUMBER OF VARIABLES MUST BE GREATER THAN OR EQUAL TO MDIS 160
C THE NUMBER OF GROUPS. MDIS 170
C MDIS 180
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED MDIS 190
C DMATX MDIS 200
C MINV MDIS 210
C DISCR MDIS 220
C MDIS 230
C METHOD MDIS 240
C REFER TO '360 COMPUTER PROGRAMS MANUAL', EDITED BY W. J. MDIS 250
C DIXON, UCL, 1964, AND T. W. ANDERSON, 'INTRODUCTION TO MDIS 260
C MULTIVARIATE STATISTICAL ANALYSIS', JOHN WILEY AND SONS, MDIS 270
C 1958, SECTION 6.6-6.8. MDIS 280
C MDIS 290
C MDIS 300
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE MDIS 310
C NUMBER OF GROUPS, K.. MDIS 320
C MDIS 330
C DIMENSION N(5) MDIS 340
C MDIS 350
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE MDIS 360
C TOTAL OF SAMPLE SIZES OF K GROUPS COMBINED, T (T = N(1)+N(2)+... MDIS 370
C +N(K)).. MDIS 380
C MDIS 390
C DIMENSION C(4*(10)) MDIS 400
C MDIS 410
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE MDIS 420
C PRODUCT OF M*K.. MDIS 430
C MDIS 440
C DIMENSION XBAR(50) MDIS 450
C MDIS 460
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE MDIS 470
C PRODUCT OF (M+1)*K.. MDIS 480
C MDIS 490
C DIMENSION C(55) MDIS 500
C MDIS 510
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE MDIS 520
C PRODUCT OF M*K.. MDIS 530
C MDIS 540
C DIMENSION D(100) MDIS 550
C MDIS 560
C THE FOLLOWING DIMENSIONS MUST BE GREATER THAN OR EQUAL TO THE MDIS 570
C TOTAL OF SAMPLE SIZES OF K GROUPS COMBINED, T (T = N(1)+N(2)+... MDIS 580
C +N(K)).. MDIS 590
C MDIS 600
C DIMENSION P(250),LG(250) MDIS 610
C MDIS 620
C THE FOLLOWING DIMENSION MUST BE GREATER THAN OR EQUAL TO THE MDIS 630
C TOTAL DATA POINTS WHICH IS EQUAL TO THE PRODUCT OF T*M.. MDIS 640
C MDIS 650
C DIMENSION X(2500) MDIS 660
C MDIS 670
C MDIS 680
C MDIS 690
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE MDIS 700
C C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION MDIS 710
C STATEMENT WHICH FOLLOWS. MDIS 720
C MDIS 730
C DOUBLE PRECISION CMEAN,XBAR,D,DET,C,V,P MDIS 740
C MDIS 750
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS MDIS 760
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS MDIS 770
C ROUTINE. MDIS 780
C MDIS 790
C MDIS 800
C MDIS 810
C 1 FORMAT(A4,A2,2I2,12I5/(14I5)) MDIS 820
C 2 FORMAT(27H1)DISCRIMINANT ANALYSIS.....A4,A2/19H) NUMBER OF GROUPS MDIS 830
C 1,7,13/22H) NUMBER OF VARIABLES,17/17H) SAMPLE SIZES.,12X,5HGR MDIS 840
C ZUP) MDIS 850
C 3 FORMAT(12X,13,9X,14) MDIS 860
C 4 FORMAT(14H) MDIS 870
C 5 FORMAT(12F6.0) MDIS 880
C 6 FORMAT(6H)GROUP,13,7H) MEANS/(8F15.5) MDIS 890
C 7 FORMAT(14H)25H) POOLED DISPERSION MATRIX) MDIS 900
C 8 FORMAT(4H)ORDR,13/(8F15.5) MDIS 910
C 7 FORMAT(14H)13H) COMMON MEANS/(8F15.5) MDIS 920
C 1) FORMAT(14H)133H) GENERALIZED MAHALANOBIS D-SQUARE,F15.5/1) MDIS 930
C 1) FORMAT(22H)DISCRIMINANT FUNCTION,13/1H,4X,27H)CONSTANT * COEFF MDIS 940
C LICIENTS/1H)F14.5,74 * ,7F14.5/(12X,7F14.5) MDIS 950
C 12) FORMAT(14H)160H) EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH MDIS 960
C OBSERVATION) MDIS 970
C 13) FORMAT(6H)GROUP,13/19X,27H)PROBABILITY ASSOCIATED WITH,11X,7H)LARGEST MDIS 980
C OBSERVATION,5X,29H)LARGEST DISCRIMINANT FUNCTION,8X,12H)FUNCT MDIS 990
C ZION NO.) MDIS 1000
C 14) FORMAT(1H +17,20X,F8.5,2CX,(6) MDIS 1010
C MDIS 1020
C MDIS 1030
C MDIS 1040
C READ PROBLEM PARAMETER CARD MDIS 1050
C MDIS 1060
C 100 READ (5:1) PR,PRI,K,M,(N(1),I=1,K) MDIS 1070
C PR.....PROBLEM NUMBER (MAY BE ALPHAMERIC) MDIS 1080
C PRI.....PROBLEM NUMBER (CONTINUED) MDIS 1090
C K.....NUMBER OF GROUPS MDIS 1100

```

```

C      M.....NUMBER OF VARIABLES
C      N.....VECTOR OF LENGTH K CONTAINING SAMPLE SIZES
C
C      WRITE (6,2) PR,PR1,K,M
C      DD 110 I=1,K
110  WRITE (6,3) I,N(I)
C      WRITE (6,4)
C
C      READ DATA
C
C      L=C
C      DD 130 I=1,K
C      N1=N(I)
C      DD 120 J=1,M1
C      READ (5,5) (CMEAN(IJ),IJ=1,M)
C      L=L+1
C      N2=L-N1
C      DD 12C IJ=1,M
C      N2=N2+N1
120  X(N2)=CMEAN(IJ)
130  L=N2
C
C      CALL OMATX (K,M,N,X,XBAR,D,CMEAN)
C
C      PRINT MEANS AND POOLED DISPERSION MATRIX
C
C      L=C
C      DD 150 I=1,K
C      DD 140 J=1,M
C      L=L+1
140  CMEAN(IJ)=XBAR(L)
150  WRITE (6,6) I,(CMEAN(IJ),J=1,M)
C      WRITE (6,7)
C      DD 170 I=1,M
C      L=L+1
C      DD 160 J=1,M
C      L=L+M
160  CMEAN(IJ)=D(L)
170  WRITE (6,8) I,(CMEAN(IJ),J=1,M)
C
C      CALL MINV (D,M,DET,CMEAN,C)
C
C      CALL DISCR (K,M,N,X,XBAR,D,CMEAN,V,C,P,LG)
C
C      PRINT COMMON MEANS
C
C      WRITE (6,9) (CMEAN(I),I=1,M)
C
C      PRINT GENERALIZED MAHALANOBIS D-SQUARE
C
C      WRITE (6,10) V
C
C      PRINT CONSTANTS AND COEFFICIENTS OF DISCRIMINANT FUNCTIONS
C
C      N1=1
C      N2=M+1
C      DD 180 I=1,K
C      WRITE (6,11) I,(C(J),J=N1,N2)
C      N1=N1+(M+1)
C      N2=N2+(M+1)
180  N2=N2+(M+1)
C
C      PRINT EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION
C
C      WRITE (6,12)
C      N1=1
C      N2=N(I)
C      DD 210 I=1,K
C      WRITE (6,13) I
C      L=0
C      DD 190 J=N1,N2
C      L=L+1
190  WRITE (6,14) L,P(I),L5(IJ)
C      IF (L-K) 200, 100, 100
200  N1=N1+N(I)
C      N2=N2+N(I+1)
210  CONTINUE
C      END

```

FACTOR ANALYSIS

Problem Description

A principal component solution and the varimax rotation of the factor matrix are performed. Principal component analysis is used to determine the minimum number of independent dimensions needed to account for most of the variance in the original set of variables. The varimax rotation is used to simplify columns (factors) rather than rows (variables) of the factor matrix.

The sample problem for factor analysis consists of 23 observations with nine variables as presented in Table 10. In order to keep the number of independent dimensions as small as possible, only those eigenvalues (of correlation coefficients) greater than or equal to 1.0 are retained in the analysis.

Table 10. Sample Data for Factor Analysis

Observation	X ₁	X ₂	X ₃	X ₄	X ₅	X ₆	X ₇	X ₈	X ₉
1	7	7	9	7	15	36	60	15	24
2	13	18	25	15	13	35	61	18	30
3	9	18	24	23	12	43	62	14	31
4	7	13	25	36	11	12	63	26	32
5	6	8	20	7	15	46	18	28	15
6	10	12	30	11	10	42	27	12	17
7	7	6	11	7	15	35	60	20	25
8	16	19	25	16	13	30	64	20	30
9	9	22	26	24	13	40	66	15	32
10	8	15	26	30	13	10	66	25	34
11	8	10	20	8	17	40	20	30	18
12	9	12	28	11	8	45	30	15	19
13	11	17	21	30	10	45	60	17	30
14	9	16	26	27	14	31	59	19	17
15	10	15	24	18	12	29	48	18	26
16	11	11	30	19	19	26	57	20	30
17	16	9	16	20	18	31	60	21	17
18	9	8	19	14	16	33	67	9	19
19	7	18	22	9	15	37	62	11	20
20	8	11	23	18	9	36	61	22	24
21	6	6	27	23	7	40	55	24	31
22	10	9	26	26	10	37	57	27	29
23	8	10	26	15	11	42	59	20	28

Program

Description

The factor analysis program consists of the main routine named FACTO, a special input subroutine named DATA, and five subroutines from the Scientific Subroutine Package: CORRE, EIGEN, TRACE, LOAD, and VARMX.

Capacity

The capacity of the sample program and the format required for data input have been set up as follows:

1. Up to 35 variables
2. Up to 99,999 observations
3. (12F6.0) format for input data cards

Therefore, if a problem satisfies the above conditions it is not necessary to modify the sample program. However, if there are more than 35 variables, dimension statements in the sample main program must be modified to handle this particular problem. Similarly, if input data cards are prepared using a different format, the input format statement in the input subroutine, DATA, must be modified. The general rules for program modification are described later.

Input

Control Card

One control card is required for each problem and is read by the main program, FACTO. This card is prepared as follows:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem</u>
1- 6	Problem number (may be alphameric)	SAMPLE
7-11	Number of observations	00023
12-13	Number of variables	09
14-19	Value used to limit the number of eigenvalues of correlation coefficients. Only those eigenvalues greater than or equal to this value are retained in the analysis. (A decimal point must be specified.)	0001.0

Leading zeros are not required to be keypunched.

Data Cards

Since input data are read into the computer one observation at a time, each row of data in Table 10 is keypunched on a separate card using the format (12F6.0). This format assumes twelve 6-column fields per card.

If there are more than twelve variables in a problem, each row of data is continued on the second and third cards until the last data point is keypunched. However, each row of data must begin on a new card.

Deck Setup

The deck setup is shown in Figure 56.

Sample

The listing of input cards for the sample problem is presented in Figure 57.

Output

Description

The output of the sample program for factor analysis includes:

1. Means
2. Standard deviations
3. Correlation coefficients
4. Eigenvalues
5. Cumulative percentage of eigenvalues
6. Eigenvectors
7. Factor matrix
8. Variance of the factor matrix for each iteration cycle

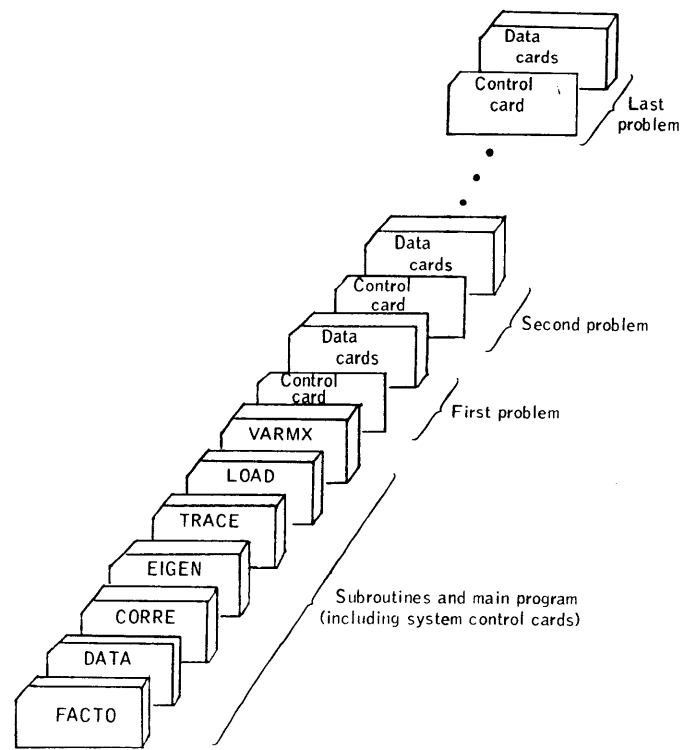


Figure 56. Deck setup (factor analysis)

9. Rotated factor matrix
10. Check on communalities

Sample

The output listing for the sample problem is shown in Figure 58.

Program Modification

Program capacity can be increased or decreased by making changes in dimension statements. Input data in a different format can also be handled by providing a specific format statement. In order to familiarize the user with the program modification, the

```

/ DATA
SAMPLEC0G2309001.0
  7 7 9 7 15 36 60 15 24
 13 18 25 15 13 35 61 18 30
 9 18 24 23 12 43 62 14 31
 7 13 25 36 11 12 63 26 32
 6 8 20 7 15 46 18 28 15
10 12 30 11 10 42 27 12 17
 7 6 11 7 15 35 60 20 25
16 19 25 16 13 30 64 20 30
 9 22 26 24 13 40 66 15 32
 8 15 26 30 13 10 66 25 34
 9 10 20 8 17 40 20 30 18
 9 12 23 11 8 45 30 15 19
11 17 21 30 10 45 60 17 30
 9 16 26 27 14 31 59 19 17
10 15 24 18 12 29 48 18 26
11 11 30 19 19 26 57 20 30
16 9 16 20 18 31 60 21 17
 9 8 19 14 16 33 67 9 19
 7 18 22 9 15 37 62 11 20
 8 11 23 18 9 36 61 22 24
 6 6 27 23 7 40 55 24 31
10 9 26 26 10 37 57 27 29
 8 10 26 15 11 42 59 20 28
  
```

Figure 57. Input listing (factor analysis)

FACTOR ANALYSIS.....SAMPLE

NO. OF CASES 73
 NO. OF VARIABLES 9

MEANS
 9.30435 12.60470 23.00000 14.00000 12.86957 14.82608 16.27776 15.37111
 25.11043

STANDARD DEVIATIONS
 7.70412 4.59978 5.33427 8.33393 3.13781 5.27149 16.87621 1.00000
 6.09249

CORRELATION COEFFICIENTS

ROW 1	1.00000	0.34987	0.11975	0.12102	0.21917	-0.09549	0.20901	-0.12908	0.00000
ROW 2	0.34987	1.00000	0.41311	0.35572	-0.08243	-0.09100	-0.20922	-0.32664	0.00000
ROW 3	0.11975	0.41311	1.00000	0.41512	-0.43179	-0.08346	-0.10252	0.03215	0.00000
ROW 4	0.12102	0.35572	0.41512	1.00000	-0.41288	-0.50365	0.49856	0.22539	0.00000
ROW 5	0.21917	-0.08243	-0.43179	-0.41288	1.00000	-0.23000	0.03310	-0.00475	-0.00000
ROW 6	-0.09549	-0.09100	-0.08346	-0.50365	-0.23000	1.00000	-0.44520	-0.25441	-0.37666
ROW 7	0.20901	0.20922	-0.10252	0.49856	0.03310	-0.44520	1.00000	-0.28050	0.00124
ROW 8	-0.12908	-0.32044	0.03215	0.22539	-0.00475	-0.25441	-0.28050	1.00000	0.12516
ROW 9	0.05818	0.35387	0.27833	0.59890	-0.30341	-0.37456	0.40124	0.13516	1.00000

EIGENVALUES
 2.94988 1.64368 1.55514 1.06579
 0.32776 0.51040 0.68319 0.80181

CUMULATIVE PERCENTAGE OF EIGENVALUES
 0.32776 0.51040 0.68319 0.80181

EIGENVECTORS

VECTOR 1	0.16437	0.34836	0.24797	0.49661	-0.16806	-0.32927	0.39935	0.01287	0.47518
VECTOR 2	0.34837	0.06552	-0.44647	-0.11893	0.61210	-0.26428	0.38860	-0.24845	-0.66014
VECTOR 3	-0.29899	-0.46825	-0.23534	0.17377	0.14468	-0.43545	0.01881	0.61587	0.13470
VECTOR 4	0.54441	0.16909	0.38288	0.04163	0.30537	-0.16163	-0.43410	0.40283	-0.23789

FACTOR MATRIX (4 FACTORS)

VARIABLE 1	0.28732	0.44663	-0.37286	0.56203
VARIABLE 2	0.59831	0.09400	-0.58394	0.17457
VARIABLE 3	0.49460	-0.57240	-0.29348	0.39528
VARIABLE 4	0.85293	-0.15248	0.21671	0.04297
VARIABLE 5	-0.28865	0.78475	0.18043	0.31525
VARIABLE 6	-0.56544	-0.33887	-0.54303	-0.16686
VARIABLE 7	0.68590	0.49821	0.02345	-0.44816
VARIABLE 8	0.02711	-0.31851	0.76802	0.41587
VARIABLE 9	0.81614	-0.07710	0.15551	-0.24559

ITERATION CYCLE

0	0.211288
1	0.336137
2	0.397022
3	0.403005
4	0.405177
5	0.405528
6	0.405581
7	0.405587
8	0.405588
9	0.405587
10	0.405587
11	0.405587
12	0.405587

ROTATED FACTOR MATRIX (4 FACTORS)

VARIABLE 1	0.05498	0.07183	-0.05578	0.85017
VARIABLE 2	0.29329	-0.39653	-0.35581	0.60549
VARIABLE 3	0.05114	-0.87493	0.15068	0.32984
VARIABLE 4	0.74040	-0.41401	0.24579	0.13972
VARIABLE 5	-0.04091	0.83662	0.13425	0.39229

Figure 58. Output listing (factor analysis)


```

      10=C
      N=0.0
C
      CALL CORRE (N,M,I0,X,XBAR,S,V,R,D,B,T)
C
C
      PRINT MEANS
C
      WRITE (6,2) (XBAR(J),J=1,M)
C
      PRINT STANDARD DEVIATIONS
C
      WRITE (6,3) (S(J),J=1,M)
C
      PRINT CORRELATION COEFFICIENTS
C
      WRITE (6,4)
      DO 120 I=1,M
      DO 110 J=1,M
      IF (I=J) C2= 104, 104
102 L=I*(J+J-1)/2
      GO TO 110
104 L=J*(I+I-1)/2
110 D(J)=R(L)
120 WRITE (6,5) I,(D(J),J=1,M)
C
      MV=0
      CALL EIGEN (R,V,M,MV)
C
      CALL TRACE (M,R,COV,K,D)
C
      PRINT EIGENVALUES
C
      DO 130 I=1,K
      L=I*(I+I-1)/2
130 S(I)=R(L)
      WRITE (6,6) (S(J),J=1,K)
C
      PRINT CUMULATIVE PERCENTAGE OF EIGENVALUES
C
      WRITE (6,7) (D(J),J=1,K)
C
      PRINT EIGENVECTORS
C
      WRITE (6,8)
      L=0
      DO 150 J=1,K
      DO 140 I=1,M
      L=L+1
140 D(I)=V(L)
150 WRITE (6,9) J,(D(I),I=1,M)
C
      CALL LOAD (M,K,R,V)
C
      PRINT FACTOR MATRIX
C
      WRITE (6,10) K
      DO 180 I=1,M
      DO 170 J=1,K
      L=M*(J-1)+I
170 D(J)=V(L)
180 WRITE (6,11) I,(D(J),J=1,K)
C
      IF (K=1) 185, 185, 188
185 WRITE (6,19) K
      GO TO 100
C
188 CALL VARMX (M,K,V,NC,TV,B,T,D)
C
      PRINT VARIANCES
C
      NV=NC+1
      WRITE (6,12)
      DO 190 I=1,NV
      NC=I-1
190 WRITE (6,13) NC,TV(I)
C
      PRINT ROTATED FACTOR MATRIX
C
      WRITE (6,14) K
      DO 220 I=1,M
      DO 210 J=1,K
      L=M*(J-1)+I
210 S(I)=V(L)
220 WRITE (6,15) I,(S(J),J=1,K)
C
      PRINT COMMUNALITIES
C
      WRITE (6,16)
      DO 230 I=1,M
230 WRITE (6,17) I,(F(I),T(I),D(I))
      GO TO 100
      END
      FCT0 970
      FCT0 980
      FCT0 49C
      FCT0100C
      FCT0110
      FCT01320
      FCT0103C
      FCT0104G
      FCT0105F
      FCT01060
      FCT0107U
      FCT01080
      FCT0109C
      FCT01100
      FCT0111C
      FCT0112C
      FCT01130
      FCT0114A
      FCT01150
      FCT01160
      FCT01170
      FCT01180
      FCT0119C
      FCT0120A
      FCT01210
      FCT01220
      FCT0123C
      FCT01240
      FCT01250
      FCT01260
      FCT0127C
      FCT0128A
      FCT0129C
      FCT01300
      FCT01310
      FCT0132C
      FCT0133C
      FCT0134C
      FCT0135C
      FCT0136C
      FCT01370
      FCT01380
      FCT01390
      FCT0140C
      FCT0141C
      FCT01420
      FCT0143C
      FCT01440
      FCT01450
      FCT01460
      FCT01470
      FCT0148C
      FCT01490
      FCT0150C
      FCT01510
      FCT01520
      FCT01530
      FCT01540
      FCT0155C
      FCT01560
      FCT01570
      FCT01580
      FCT01590
      FCT0160C
      FCT01610
      FCT01620
      FCT0163C
      FCT01640
      FCT01650
      FCT01660
      FCT01670
      FCT01680
      FCT01690
      FCT0170C
      FCT01710
      FCT0172C
      FCT01730
      FCT01740
      FCT01750
      FCT01760
      FCT01770
      FCT01780
      FCT01790
      FCT01800
      FCT01810
      FCT01820
      FCT01830
      FCT01840
      FCT01850
      FCT01860
      FCT01870
      FCT01880

```

KOLMOGOROV - SMIRNOV TEST

Problem Description

This program is concerned with the problem of determining (a) from what probability density function a particular sample is drawn, or (b) whether two different samples were drawn from the same population. In other words, in the one sample case, the actual distribution function of the sample is compared with one or more theoretical distribution functions, which may be normal, and/or exponential, and/or Cauchy, and/or uniform, and/or a user-specified distribution. In the two-sample case, the pair of sample (actual) distribution functions are compared with one another.

From the above comparisons, a statistic is derived. In the one sample case, this statistic evaluates the probability that the statistic will be as great as or greater than its current value, if the hypothesis that the actual (sample) and the theoretical distribution functions are equal is correct. In other words, if the probability is determined to be 0.40, for example, rejecting the hypothesis of equality of the distribution functions will be an incorrect action 40 times out of 100. Similarly, in the two-sample case, the hypothesis being tested is the equality of the two actual (sample) distribution functions.

This probability is calculated using asymptotic formulas. This means that the sample sizes involved should be large. Sizes greater than 100 are suggested by the literature. In this connection, the remarks given under the topic "Subroutine SMIRN" should be considered.

Note also that added problems arise when, in the one sample case, the parameters of the continuous distribution in question are estimated from the sample. Lilliefors discusses these problems (see reference given in KOLMO description).

Program

Description

This program consists of the main routine KOLM, and four subroutines from the Scientific Subroutine Package: KOLMO, KOLM2, SMIRN, and NDTR.

Capacity

This program allows up to two samples each with 500 or fewer observations to be examined. If the user desires to modify this program to handle more observations, the instructions given below under "Program Modification" should be followed.

Input

After two initializing cards (1, 2 below) each job consists of two control cards and the data cards (3-5 below).

1. Initializing card (minus signs in cc 1-4)
2. Names of distribution functions (as supplied, these are the normal, exponential, Cauchy, uniform, and user's pdf). These names are punched in the order given, centrally located in 16 digit fields on one card; that is, "normal" is punched in cc 1-16, "exponential" in cc 17-32, and so on.
3. Job control card (minus signs in cc 1-4)
4. Program control card

Each job requires one program control card, defined below:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problems</u>	<u>Columns</u>	<u>Contents</u>	<u>For Sample Problems</u>
1 - 20	Title (alphameric)	Uniform test (Job 1)	63 - 67	s -- right endpoint of uniform pdf	1.0 (job 1)
		Uniform-Gauss Test (job 2)	68	0 -- Do not compare with user's pdf.	0 (job 1)
21	1 -- one-sample test	1 (job 1)		1 -- Compare with user-specified pdf.	
	2 -- two-sample test	2 (job 2)	69 - 73	u } Parameters for	0 (job 1)
22	Leave blank for one-sample test.	0 (job 1)	74 - 78	s } user-specified pdf	0 (job 1)
	0 -- Read both samples (two-sample tests).	1 (job 2)			
	1 -- Read only one sample and compare it with the first sample read on preceding job.			u and s are described fully in "Description of Parameters" under subroutine KOLMO, and are read using Format F 5.0; decimal points will override the format specification.	
23	0 -- Do not print the sample(s).	0 (job 1)			
	1 -- Print the sorted sample(s). (F10.3, ten per line)	1 (job 2)			
(The rest of this control card pertains to a one-sample test.)					
24	0 -- Do not compare with normal pdf.	1 (job 1)			
	1 -- Compare with normal pdf.				
25 - 29	u -- mean of the normal pdf	0.5 (job 1)			
30 - 34	s -- standard deviation of the normal pdf	0.5 (job 1)			
35	0 -- Do not compare with exponential pdf.				
	1 -- Compare with exponential pdf.	1 (job 1)			
36 - 40	u -- mean of the exponential pdf	0.5 (job 1)			
41 - 45	s -- standard deviation of the exponential pdf	1.0 (job 1)			
46	0 -- Do not compare with Cauchy pdf.				
	1 -- Compare with Cauchy pdf.	1 (job 1)			
47 - 51	u -- median of the Cauchy pdf	0.5 (job 1)			
52 - 56	s -- u-s is the first quartile of the Cauchy pdf	1.0 (job 1)			
57	0 -- Do not compare with uniform pdf.				
	1 -- Compare with uniform pdf.	1 (job 1)			
58 - 62	u -- left endpoint of the uniform pdf	0 (job 1)			

5. Data is read into the computer one sample at a time. The reading of a sample is terminated by a data element of 999999. New samples must begin on a new card. Data elements are punched on cards using format F6.0, which assumes twelve 6-column fields per card; decimal points on the card override the format specification. Since the routines KOLMO and KOLM2 sort the samples, no particular order within a sample is necessary.

Deck Setup

See figure 59.

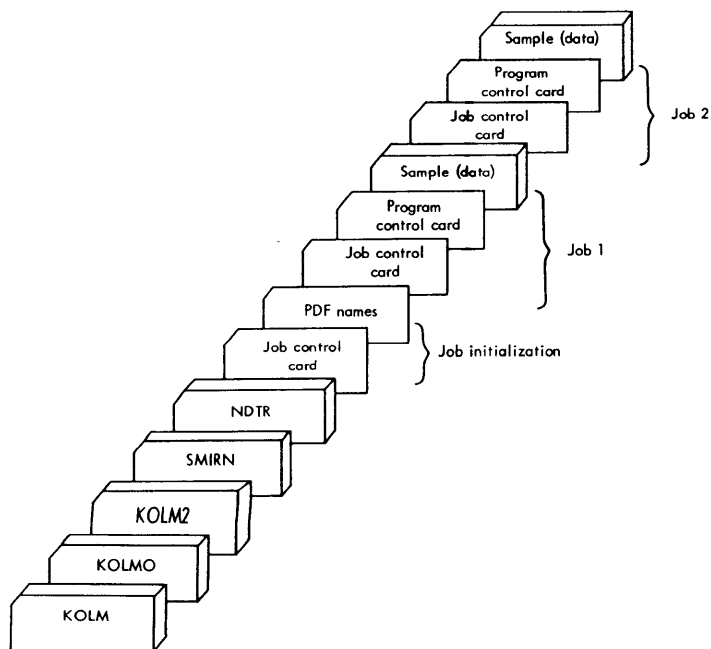


Figure 59. Deck setup (Kolmogorov - Smirnov test)

Sample Data

See Figure 60.

/DATA	NORMAL	EXPONENTIAL	CAUCHY	UNIFORM	USER*	10
UNIFORM TEST	ICCC100.500C.5100C.5000C1100C.5000C1100000000C1					20
0.377	0.260	0.172	0.688	0.581	0.290	0.514
0.795	0.837	0.870	0.686	0.288	0.555	0.737
0.231	0.806	0.753	0.263	0.804	0.458	0.508
0.005	0.951	0.664	0.425	0.570	0.596	0.444
0.282	0.201	0.662	0.167	0.043	0.750	0.117
0.692	0.663	0.867	0.054	0.518	0.624	0.083
0.458	0.694	0.041	0.995	0.604	0.666	0.561
0.139	0.536	0.963	0.956	0.068	0.801	0.199
0.670	0.640	0.805	0.073	0.196	0.516	0.336
0.242	0.200	0.025	0.349	0.870	0.080	0.652
0.636	0.190	0.416	0.786	0.973	0.767	0.845
0.652	0.632	0.923	0.844	0.761	0.969	0.965
0.243	0.008	0.860	0.093	0.816	0.058	0.006
0.982	0.666	0.154	0.933	0.215	0.890	0.409
0.501	0.123	0.228	0.264	0.531	0.810	0.083
0.503	0.117	0.170	0.972	0.298	0.042	0.574
0.996	0.292	0.790	0.111	0.556	0.337	0.012
0.353	0.397	0.206	0.662	0.119	0.754	0.450
0.842	0.859	0.577	0.725	0.163	0.450	0.232
0.236	0.622	0.607	0.042	0.787	0.348	0.006
0.136	0.113	0.455	0.708	0.158	0.572	0.012
0.629	0.220	0.657	0.962	0.860	0.501	0.268
0.909	0.148	0.708	0.909	0.088	0.345	0.277
0.542	0.294	0.041	0.630	0.303	0.478	0.835
0.581	0.224	0.112	0.659	0.945	0.741	0.940
0.422	0.967	0.005	0.328	0.924	0.595	0.253
0.913	0.422	0.516	0.502	0.364	0.667	0.724
0.457	0.021	0.019	0.923	0.365	0.882	0.010
0.459	0.009	0.919	0.434	0.331	0.079	0.500
0.178	0.978	0.272	0.827	0.512	0.634	0.195
0.524	0.294	0.041	0.630	0.303	0.478	0.835
0.463	0.471	0.664	0.742	0.476	0.178	0.785
0.611	0.988	0.401	0.699	0.312	0.580	0.672
0.679	0.603	0.504	0.595	0.033	0.846	0.783
0.376	0.062	0.990	0.381	0.371	0.801	0.467
0.388	0.055	0.836	0.518	0.585	0.842	0.793
0.085	0.311	0.102	0.816	0.973	0.494	0.208
0.546	0.698	0.205	0.339	0.607	0.594	0.102
0.202	0.207	0.188	0.264	0.895	0.991	0.893
0.208	0.696	0.304	0.557	0.605	0.617	0.756
0.141	0.153	0.654	0.544	0.376	0.363	0.793
0.644	0.263	0.785	0.341	0.982	0.829999999	
UNIFORM-GAUSS TEST	211					
-0.283	0.916	0.776	0.690	0.910	0.506	0.816
0.515	0.227	1.253	0.421	0.499	0.288	1.189
0.273	0.154	0.861	0.937	0.446	0.702	1.451
-1.157	0.902	0.533	1.270	0.766	1.110	1.190
0.547	1.145	0.667	-0.077	0.422	-0.159	-0.307
-0.324	0.025	0.632	0.365	0.375	0.694	-0.236
-0.011	0.653	0.266	1.035	0.536	0.936	1.177
0.714	0.607	0.374	0.341	0.190	0.302	1.075
0.048	0.938	0.733	-0.340	-0.012	0.497	0.418
0.656	0.660	0.584	0.837	0.454	0.695	0.606
1.173	0.762	0.642	0.185	-0.023	0.037	0.008
-0.299	0.196	1.086	0.487	0.317	0.635	0.462
0.313	0.387	1.067	0.996	0.702	0.068	-0.777
1.049	0.226	-0.297	0.930	0.828	0.884	1.217
0.418	1.075	0.083	-0.020	0.362	0.601	0.637
-0.602	0.763	1.261	0.302	-0.063	0.704	0.446
-0.064	1.087	-0.737	-0.476	1.156	0.648	0.624
-0.552	-0.183	0.583	0.740	0.592	-0.144	0.222
0.818	0.686	0.683	0.514	0.284	-0.280	0.358
0.899	0.400	0.994	0.880	0.743	0.102	1.120
0.512	1.132	0.916	0.838	0.445	1.330	0.563
0.448	-0.475	0.317	0.858	0.839	-0.297	0.214
0.467	1.188	0.536	0.381	1.339	-0.011	0.064
0.297	0.203	0.378	1.313	0.829	0.422	0.678
0.633	1.116	0.118	-0.469	0.663	0.708	0.685
0.643	-0.055	-0.000	0.881	1.163	0.520	0.787
-0.541	1.176	0.236	0.675	1.119	1.000	0.250
0.686	0.764	0.007	0.697	0.789	0.259	0.414
1.394	0.131	0.963	0.699	0.404	-0.124	0.583
0.125	1.670	0.224	0.400	0.658	0.900	1.034
0.387	1.243	0.875	0.989	0.718	-0.152	0.009
0.160	0.177	-0.025	1.125	0.217	1.206	1.221
0.388	0.772	1.046	0.067	0.760	0.428	0.852
-0.011	-0.205	1.084	0.609	1.119	0.438	1.050
0.346	-1.018	1.049	0.417	1.230	1.127	1.435
0.812	0.537	0.875	0.190	0.707	0.857	0.094
1.709	0.133	0.460	0.828	-0.174	0.457	0.584
-0.177	0.913	0.673	0.303	0.035	1.226	-0.072
0.951	0.307	0.798	1.479	0.196	1.558	0.873
-0.072	0.988	0.351	0.053	0.248	0.430	-0.379
-0.263	-0.084	0.301	1.486	0.351	0.806	-0.374
999999						

Figure 60.

Output

Description

The output from the program KOLM gives the statistics and probability statements described below, and in addition identifies the distribution functions being considered. Sorted samples are printed on option.

The following items are produced as output:
 1. Z score, where $z = \sqrt{n} D_n$ for the one-sample

test; n is the sample size, and D_n is the maximum difference between the empirical distribution function and the theoretical distribution function.

$$z = \sqrt{\frac{mn}{m+n}} D_{m,n}$$

for the two-sample test, m is the size of the second sample; n is the size of the first sample; $D_{m,n}$ is the maximum difference between the two empirical distribution functions.

2. The probability of incorrectly rejecting the hypothesis of equality of distribution functions.

Sample

See Figure 61.

Program Modification

1. Program capacity may be increased or decreased by making changes in the dimension statements. If this is done, the statements DO 111 I = 1, 50 and DO 117 I = 1, 50 may require modification (under READ SAMPLE comments card in listing of program). This will also be true if data formats require changing. The "read sample" sections of the program use FORMAT statement 3, and the user may wish to change these sections.

2. Any modifications to the subroutine KOLMO in terms of added continuous pdf's should be reflected in the program KOLM. It may be necessary to:

- a. Modify the dimensions of DIST (5, 3), which contains the switches calling on pdf's and also contains the parameters u and s used by KOLMO
- b. Modify the pdf titling card, statement 6 (FORMAT), the READ (5, 6)TIT1 card which reads titles, and the dimension of TIT1 (now 20, to hold five 16-digit titles)
- c. Modify the section of the program from statement 121 through 132 to reflect changes a and b above. These statements call KOLMO to perform tests and output results.

3. List of names in KOLM, and their usage:

- D -- Temporary vector used in reading samples
- DAS2 -- Initializing card name (----)
- DASH -- Job control card name (----)
- DIST -- 5 by 3 matrix. The five elements in column 1 are switches that allow the (5) pdf's to be used in one-sample tests. Columns 2 and 3 contain the parameters u and s for the associated test.
- IFL -- Error indicator (job deck error)
- IER -- Error (in KOLMO, used for skipping the test concerned)
- IES -- Error (in KOLMO, used for error message)

UNIFORM TEST

A 1 SAMPLE TEST WAS REQUESTED

THE SIZE OF SAMPLE 1 IS 498.

THE HYPOTHESIS THAT THE SAMPLE IS FROM A(N) NORMAL DISTRIBUTION WITH MEAN 0.5000 AND VARIANCE 0.2500 CAN BE REJECTED WITH PROBABILITY 0.0 OF BEING INCORRECT. THE STATISTIC Z IS 0.3584E 01 FOR THIS SAMPLE.

THE HYPOTHESIS THAT THE SAMPLE IS FROM A(N) EXPONENTIAL DISTRIBUTION WITH MEAN 0.5000 AND VARIANCE 1.0000 CAN BE REJECTED WITH PROBABILITY 0.0 OF BEING INCORRECT. THE STATISTIC Z IS 0.8803E 01 FOR THIS SAMPLE.

THE HYPOTHESIS THAT THE SAMPLE IS FROM A(N) CAUCHY DISTRIBUTION WITH MEDIAN 0.5000 AND FIRST QUARTILE -0.5000 CAN BE REJECTED WITH PROBABILITY 0.0 OF BEING INCORRECT. THE STATISTIC Z IS 0.7887E 01 FOR THIS SAMPLE.

THE HYPOTHESIS THAT THE SAMPLE IS FROM A(N) UNIFORM DISTRIBUTION IN THE INTERVAL 0.0 TO 1.0000 INCLUSIVE CAN BE REJECTED WITH PROBABILITY 0.989 OF BEING INCORRECT. THE STATISTIC Z IS 0.4444E 00 FOR THIS SAMPLE.

THE JOB WITH TITLE UNIFORM TEST WAS COMPLETED.

UNIFORM-GAUSS TEST

A 2 SAMPLE TEST WAS REQUESTED

THE SIZE OF SAMPLE 2 IS 492.

SORTED SAMPLE ONE FOLLOWS

0.0	0.005	0.005	0.004	0.006	0.006	0.008	0.009	0.010	0.012
0.012	0.018	0.019	0.019	0.021	0.021	0.022	0.022	0.025	0.033
0.033	0.033	0.037	0.041	0.041	0.042	0.042	0.042	0.043	0.047
0.053	0.054	0.055	0.058	0.062	0.065	0.068	0.073	0.073	0.077
0.079	0.079	0.080	0.083	0.083	0.085	0.088	0.092	0.093	0.093
0.097	0.098	0.102	0.102	0.103	0.111	0.112	0.113	0.113	0.113
0.117	0.117	0.119	0.121	0.123	0.136	0.139	0.139	0.141	0.143
0.148	0.151	0.153	0.154	0.156	0.157	0.158	0.161	0.163	0.164
0.164	0.167	0.168	0.170	0.172	0.177	0.178	0.178	0.178	0.178
0.181	0.181	0.183	0.188	0.190	0.190	0.193	0.195	0.195	0.196
0.197	0.199	0.200	0.201	0.202	0.203	0.204	0.206	0.207	0.208
0.208	0.209	0.215	0.220	0.224	0.225	0.228	0.231	0.231	0.232
0.236	0.242	0.242	0.243	0.244	0.253	0.256	0.256	0.260	0.263
0.263	0.264	0.264	0.266	0.268	0.269	0.272	0.275	0.277	0.282
0.283	0.284	0.285	0.287	0.288	0.288	0.290	0.292	0.294	0.298
0.299	0.301	0.302	0.302	0.302	0.303	0.304	0.311	0.311	0.312
0.326	0.328	0.331	0.336	0.337	0.339	0.340	0.341	0.343	0.344
0.345	0.348	0.348	0.349	0.349	0.353	0.360	0.363	0.364	0.365
0.365	0.365	0.365	0.367	0.367	0.371	0.371	0.376	0.376	0.376
0.377	0.377	0.381	0.381	0.382	0.383	0.388	0.390	0.397	0.400
0.409	0.411	0.416	0.416	0.422	0.422	0.425	0.427	0.430	0.431
0.434	0.434	0.441	0.442	0.444	0.447	0.450	0.450	0.450	0.453
0.454	0.455	0.455	0.457	0.458	0.458	0.459	0.462	0.462	0.462
0.463	0.463	0.467	0.469	0.470	0.471	0.472	0.476	0.477	0.478
0.482	0.482	0.492	0.494	0.500	0.501	0.502	0.503	0.503	0.504
0.508	0.512	0.514	0.514	0.515	0.516	0.516	0.518	0.518	0.520
0.520	0.524	0.531	0.536	0.539	0.540	0.544	0.545	0.546	0.546
0.554	0.555	0.556	0.556	0.557	0.560	0.561	0.562	0.565	0.570
0.570	0.572	0.574	0.577	0.580	0.581	0.581	0.585	0.588	0.589
0.591	0.592	0.594	0.594	0.595	0.595	0.595	0.596	0.597	0.603
0.604	0.605	0.607	0.607	0.607	0.607	0.608	0.610	0.611	0.615
0.617	0.622	0.622	0.624	0.629	0.630	0.632	0.634	0.634	0.636
0.637	0.638	0.639	0.640	0.644	0.644	0.652	0.652	0.654	0.657
0.659	0.662	0.662	0.664	0.664	0.665	0.666	0.666	0.667	0.668
0.668	0.670	0.671	0.672	0.677	0.679	0.683	0.686	0.688	0.692
0.694	0.694	0.696	0.697	0.698	0.699	0.699	0.701	0.702	0.707
0.708	0.708	0.709	0.715	0.722	0.724	0.725	0.726	0.728	0.733
0.734	0.737	0.741	0.742	0.743	0.745	0.745	0.746	0.750	0.751
0.752	0.753	0.754	0.759	0.761	0.761	0.766	0.767	0.783	0.785
0.785	0.786	0.787	0.790	0.793	0.793	0.795	0.801	0.801	0.803
0.804	0.805	0.806	0.810	0.810	0.810	0.812	0.814	0.816	0.816
0.816	0.817	0.827	0.829	0.833	0.835	0.836	0.837	0.840	0.842
0.842	0.843	0.843	0.844	0.845	0.846	0.851	0.859	0.860	0.860
0.864	0.867	0.868	0.870	0.870	0.876	0.880	0.882	0.882	0.888
0.889	0.890	0.892	0.893	0.895	0.896	0.907	0.909	0.909	0.913
0.913	0.918	0.919	0.923	0.923	0.924	0.926	0.928	0.928	0.931
0.931	0.933	0.936	0.939	0.940	0.945	0.946	0.950	0.951	0.953
0.953	0.956	0.956	0.962	0.963	0.963	0.964	0.965	0.967	0.969
0.969	0.972	0.973	0.973	0.976	0.978	0.982	0.982	0.984	0.984
0.985	0.988	0.990	0.991	0.994	0.995	0.996	0.996		

Figure 61.

SORTED SAMPLE TWO FOLLOWS

-1.157	-1.018	-0.737	-0.718	-0.643*	-0.602	-0.552	-0.541	-0.476	-0.475
-0.469	-0.467	-0.410	-0.397	-0.391	-0.381	-0.379	-0.374	-0.373	-0.340
-0.340	-0.324	-0.313	-0.302	-0.301	-0.299	-0.297	-0.297	-0.283	-0.280
-0.276	-0.275	-0.264	-0.263	-0.262	-0.249	-0.232	-0.227	-0.206	-0.205
-0.188	-0.183	-0.179	-0.174	-0.172	-0.159	-0.152	-0.145	-0.144	-0.131
-0.124	-0.096	-0.088	-0.077	-0.072	-0.072	-0.069	-0.067	-0.064	-0.064
-0.063	-0.055	-0.038	-0.037	-0.026	-0.025	-0.023	-0.023	-0.021	-0.020
-0.012	-0.011	-0.011	-0.011	-0.010	-0.004	-0.003	0.0	0.004	0.005
0.007	0.007	0.009	0.009	0.012	0.025	0.035	0.035	0.037	0.037
0.048	0.051	0.053	0.053	0.057	0.060	0.064	0.068	0.071	0.078
0.083	0.088	0.091	0.094	0.098	0.099	0.102	0.109	0.113	0.113
0.118	0.124	0.125	0.126	0.131	0.133	0.143	0.147	0.149	0.154
0.160	0.174	0.176	0.177	0.181	0.185	0.190	0.191	0.191	0.196
0.196	0.196	0.198	0.198	0.203	0.203	0.204	0.204	0.214	0.217
0.222	0.222	0.224	0.226	0.227	0.231	0.234	0.236	0.248	0.250
0.257	0.259	0.266	0.272	0.273	0.284	0.287	0.288	0.288	0.297
0.301	0.301	0.302	0.302	0.303	0.305	0.307	0.310	0.313	0.313
0.315	0.317	0.317	0.322	0.341	0.346	0.348	0.351	0.351	0.358
0.359	0.362	0.365	0.372	0.373	0.374	0.374	0.375	0.376	0.378
0.381	0.387	0.387	0.388	0.388	0.391	0.394	0.399	0.400	0.400
0.401	0.404	0.406	0.406	0.411	0.414	0.417	0.418	0.418	0.421
0.422	0.422	0.428	0.430	0.433	0.436	0.438	0.445	0.445	0.446
0.446	0.447	0.448	0.454	0.457	0.457	0.460	0.462	0.464	0.467
0.484	0.487	0.490	0.494	0.494	0.497	0.499	0.501	0.506	0.508
0.512	0.514	0.515	0.515	0.520	0.524	0.524	0.524	0.533	0.533
0.536	0.536	0.537	0.547	0.559	0.559	0.562	0.563	0.563	0.566
0.571	0.573	0.578	0.583	0.583	0.583	0.584	0.584	0.586	0.592
0.601	0.604	0.606	0.606	0.607	0.610	0.610	0.616	0.619	0.622
0.624	0.629	0.630	0.632	0.632	0.633	0.634	0.635	0.642	0.643
0.643	0.648	0.653	0.656	0.657	0.658	0.659	0.660	0.663	0.667
0.673	0.675	0.675	0.680	0.683	0.685	0.686	0.686	0.687	0.687
0.688	0.690	0.693	0.694	0.695	0.697	0.699	0.699	0.702	0.702
0.704	0.704	0.707	0.708	0.714	0.718	0.719	0.733	0.735	0.740
0.743	0.760	0.761	0.762	0.763	0.764	0.770	0.772	0.776	0.782
0.786	0.787	0.789	0.790	0.798	0.801	0.801	0.806	0.812	0.816
0.818	0.823	0.828	0.828	0.829	0.832	0.837	0.838	0.839	0.840
0.849	0.849	0.850	0.852	0.852	0.857	0.858	0.861	0.867	0.868
0.873	0.874	0.875	0.875	0.880	0.881	0.884	0.884	0.887	0.898
0.899	0.900	0.902	0.910	0.913	0.916	0.916	0.916	0.917	0.920
0.920	0.930	0.933	0.936	0.937	0.938	0.951	0.951	0.954	0.954
0.958	0.963	0.963	0.968	0.975	0.983	0.985	0.988	0.989	0.994
1.006	1.000	1.004	1.022	1.024	1.034	1.035	1.046	1.049	1.049
1.050	1.053	1.058	1.063	1.067	1.070	1.075	1.075	1.084	1.086
1.087	1.108	1.110	1.116	1.119	1.120	1.125	1.127	1.132	1.145
1.149	1.156	1.163	1.173	1.176	1.176	1.177	1.184	1.188	1.189
1.190	1.203	1.206	1.207	1.217	1.217	1.221	1.226	1.230	1.238
1.243	1.253	1.255	1.261	1.261	1.265	1.270	1.295	1.313	1.317
1.329	1.330	1.339	1.352	1.356	1.366	1.376	1.384	1.394	1.394
1.435	1.451	1.479	1.486	1.493	1.598	1.600	1.644	1.670	1.709
1.799	1.838								

THE HYPOTHESIS THAT THE TWO SAMPLES ARE FROM THE SAME POPULATION CAN BE REJECTED WITH (ASYMPTOTIC) PROBABILITY OF BEING INCORRECT OF 0.000. THE STATISTIC Z IS 0.2590E 01 FOR THESE SAMPLES.

THE JOB WITH TITLE UNIFORM-GAUSS TEST WAS COMPLETED.

Figure 61. (Continued)

- IO -- Switch (used for printing samples)
- IR -- Number of samples to be read in current job
- IS -- Number of samples to be used in current job (1 or 2)
- K -- Counter used to print correct pdf name for pdf used in the test
- M -- Size of second sample
- N -- Size of first sample
- N1 -- 1 or 2, for number of samples tested
- P -- Probability of being incorrect if hypothesis is rejected
- S2 -- Temporary storage for u and s output
- TIT1 -- Current pdf names
- TITLE -- Job title
- X -- Sample 1
- Y -- Sample 2
- Z -- Z statistic, from KOLMO or KOLM2

Operating Instructions

This sample program is a standard FORTRAN program and needs no special operating instructions. Data set 5 is used for input, and 6 for output.

Error Messages

The following error conditions will result in messages, followed by the action specified:

1. Neither a one- nor two-sample test is requested, or the size of either sample is larger than 500 -- CC.21, CONTROL CARD, INCORRECT, OR SAMPLE SIZE TOO LARGE. JOB IGNORED. Action: Cards are read until a new job control card is found, or until the hopper is empty.

2. Sample size is less than 100 (not an error) -- NOTE THE REMARKS CONCERNING ASYMPTOTIC RESULTS AND SAMPLE SIZE IN SUBROUTINE SMIRN. Action: None - job continues.

3. The requirement of subroutine KOLMO that certain parameters be nonzero or positive is violated -- AT LEAST ONE (S) ENTRY PARAMETER FOR THE SUBROUTINE KOLMO WAS INCORRECT. THE TEST FOR THE ASSOCIATED CONTINUOUS PDF WAS IGNORED. Action: All tests are made for cases where the parameter s was correct.

4. A case in which an error requires aborting the job, and the succeeding job in the job stack requests a two-sample test where the second sample is to be

compared with a (first) sample which was read on the previous job -- THIS JOB CALLS FOR THE USE OF A PREVIOUSLY READ SAMPLE, AND THE PREVIOUS JOB WAS IGNORED BECAUSE OF ERRORS. JOB IGNORED. Action: Cards are read until a new job control card is found, or until the hopper is empty.

5. The job control card preceding a job is not there or is incorrect -- FIRST CARD IN JOB DECK (JOB CONTROL CARD) IS INCORRECT. Action: Cards are read until a new job control card is found, or until the hopper is empty.

Timing

The execution time of this program on a System/360, Model 40, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 Printer as output, is:

- 33 seconds for job 1
- 50 seconds for job 2

```

C          SELECT PROGRAM CONTROLS
C
100 READ(5,15)DAS2
    IF(DASH-DAS2)101,102,101
101 WRITE(6,17)
    GO TO 107
102 READ(5,1)TITLE,IS,IP,IO,((DIST(I,J),J=1,3),I=1,5)
    IES=0
    WRITE(6,4)TITLE
    WRITE(6,5)IS
C
C          NUMBER OF SAMPLES DECISION
C
    IF(I1)103,105,103
103 IF(I1L)104,115,104
104 WRITE(6,16)
    GO TO 107
105 IF(I1S-1)106,109,109
C
C          NOT ONE OR TWO SAMPLES
C
106 WRITE(6,2)
107 READ(5,15)DAS2
    IF(DASH-DAS2)107,108,107
108 IFL=1
    GO TO 107
C
C          READ FIRST SAMPLE
C
109 N=0
    DO 111 I=1,50
      READ(5,3)D
      DO 111 J=1,12
        IF(D(J)-999999.0)110,112,110
110 N=N+1
    IF(N=50)111,106,106
111 X(N)=D(J)
112 N1=1
    WRITE(6,12)N1,N
C
C          CHECK THE SIZE OF N
C
    IF(N-100)113,113,114
113 WRITE(6,13)
114 IF(I1S-2)121,115,106
C
C          READ SECOND SAMPLE
C
115 M=0
    DO 117 I=1,50
      READ(5,3)D
      DO 117 J=1,12
        IF(D(J)-999999.0)116,118,116
116 M=M+1
    IF(M=50)117,106,106
117 Y(M)=D(J)
118 M1=2
    WRITE(6,12)M1,M
C
C          CHECK THE SIZE OF M
C
    IF(M-100)119,119,120
119 WRITE(6,13)
120 IF(I1S-1)121,121,133
C
C          ONE SAMPLE TEST USING ALL DISTRIBUTIONS REQUESTED
C
121 DO 130 I=1,5
    IF(DIST(I,1))130,130,122
122 CALL KOLM2(X,N,Z,P,I,DIST(I,2),DIST(I,3),IER)
    IES=IER+IES
    IF(IER)130,124,130
123 WRITE(6,14)
    GO TO 136
C
C          OUTPUT RESULTS
C
124 K=4*I-3
    WRITE(6,9)TIT1(K),TIT1(K+1),TIT1(K+2),TIT1(K+3)
    IF(I-3)125,126,127
125 S2=DIST(I,3)**2
    WRITE(6,18)DIST(I,2),S2
    GO TO 129
126 S2=DIST(I,2)-DIST(I,3)
    WRITE(6,19)DIST(I,2),S2
    GO TO 129
127 IF(I-4)128,128,130
128 WRITE(6,20)DIST(I,2),DIST(I,3)
129 WRITE(6,21)P,Z
130 CONTINUE
C
C          OUTPUT SAMPLE ONE DECISION
C
    IF(I)131,132,131
131 WRITE(6,8)
    WRITE(6,7)(X(J),J=1,N)
132 IF(IES)123,136,123
C
C          TWO SAMPLE TEST
C
133 CALL KOLM2(X,Y,N,M,Z,P)
C
C          OUTPUT SAMPLES DECISION
C
    IF(I)134,135,134
134 WRITE(6,8)
    WRITE(6,7)(X(J),J=1,N)
    WRITE(6,10)
    WRITE(6,7)(Y(J),J=1,M)
135 WRITE(6,11)P,Z
136 WRITE(6,22)TITLE
    GO TO 100
END

```

```

C          KOLM 10
C          .....KOLM 20
C          SAMPLE MAIN PROGRAM FOR THE KOLMGOROV-SMIRNOV TEST-KOLM KOLM 30
C          KOLM 40
C          PURPOSE KOLM 50
C          (1) READ THE CONTROL CARD FOR A ONE OR TWO SAMPLE TEST KOLM 70
C          (2) READ THE SAMPLE DATA AND DETERMINE THE SAMPLE SIZES KOLM 80
C          (3) PRINT RESULTS KOLM 90
C          REMARKS KOLM 100
C          THE USER SHOULD NOTE THE REMARKS GIVEN IN SUBROUTINES KOLM 110
C          KOLM2, AND SMIRN, AND THE MATHEMATICAL DESCRIPTIONS KOLM 120
C          FOR THESE SUBROUTINES. KOLM 130
C          KOLM 140
C          SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED KOLM 150
C          KOLM 160
C          KOLM2 KOLM 170
C          SMIRN KOLM 180
C          NOTR KOLM 190
C          KOLM 200
C          KOLM 210
C          METHOD KOLM 220
C          REFER TO SUBROUTINES KOLM2, AND SMIRN KOLM 230
C          KOLM 240
C          .....KOLM 250
C          THE FOLLOWING DIMENSIONS MUST BE GREATER THAN THE NUMBER OF DATA KOLM 260
C          ELEMENTS IN THE TWO SAMPLES, M AND N KOLM 270
C          KOLM 280
C          DIMENSION X(501),Y(501) KOLM 290
C          KOLM 300
C          .....KOLM 310
C          DIMENSION TITLE(5),D(12),TIT(120),DIST(5,3) KOLM 320
C          KOLM 330
C          .....KOLM 340
C          .....KOLM 350
C          .....KOLM 360
C          .....KOLM 370
C          1 FORMAT(5A4,3I1,5F10.2F5.0) KOLM 380
C          2 FORMAT('CC.21, CONTROL CARD, INCORRECT, OR SAMPLE SIZE IS TOO LAKOLM 390
C          1FGE. JOB IGNORED. ') KOLM 400
C          3 FORMAT(12F6.0) KOLM 410
C          4 FORMAT(1H1,5A4) KOLM 420
C          5 FORMAT('2H A,12, SAMPLE TEST WAS REQUESTED') KOLM 430
C          6 FORMAT(20A4) KOLM 440
C          7 FORMAT('10F10.3) KOLM 450
C          8 FORMAT(' SORTED SAMPLE ONE FOLLOWS') KOLM 460
C          9 FORMAT(' THE HYPOTHESIS THAT THE SAMPLE IS FROM A(N) ',4A4, ' DKOLM 470
C          11STRIUTION') KOLM 480
C          10 FORMAT(' SORTED SAMPLE TWO FOLLOWS') KOLM 490
C          11 FORMAT(' THE HYPOTHESIS THAT THE TWO SAMPLES ARE FROM THE SAME PKOLM 500
C          10PULATION CAN BE REJECTED WITH (ASYMPTOTIC) ',/, ' PROBABILITY OF BEKOLM 510
C          2ING INCORRECT OF ',F6.3,%. ' THE STATISTIC Z IS ',E12.4, ' FOR THESEKOLM 520
C          3 SAMPLES. ') KOLM 530
C          12 FORMAT(' THE SIZE OF SAMPLE',I3, ' IS',I4, ' ') KOLM 540
C          13 FORMAT(' NOTE THE REMARKS CONCERNING ASYMPTOTIC RESULTS AND SAMKOLM 550
C          1PLE SIZE IN SUBROUTINE SMIPN') KOLM 560
C          14 FORMAT(' AT LEAST ONE (S) ENTRY PARAMETER FOR THE SUBROUTINE KOKOLM 570
C          1LMO WAS INCORRECT. ' THE TEST FOR THE ASSOCIATED CONTINUOUS POF WKOLM 580
C          2AS (IGNORED. ') KOLM 590
C          15 FORMAT(A4) KOLM 600
C          16 FORMAT(' THIS JOB CALLS FOR THE USE OF A PREVIOUSLY READ SAMPLEKOLM 610
C          1, AND THE PREVIOUS JOB WAS IGNORED BECAUSE OF ERRORS. ' / ' JOB IGNOKOLM 620
C          2FED. ') KOLM 630
C          17 FORMAT(' FIRST CARD IN JOB DECK (JOB CONTROL CARD) IS INCORRECTKOLM 640
C          1 ') KOLM 650
C          18 FORMAT('H ', WITH MEAN',F13.4, ' AND VARIANCE',F13.4) KOLM 660
C          19 FORMAT('H ', WITH MEDIAN',F13.4, ' AND FIRST QUARTILE',F13.4) KOLM 670
C          20 FORMAT('H ', IN THE INTERVAL',F13.4, ' TO',F13.4, ' INCLUSIVE') KOLM 680
C          21 FORMAT('H ', CAN BE REJECTED WITH PROBABILITY',F6.3, ' OF BEING INKOLM 690
C          1ORRECT. THE STATISTIC Z',/, ' IS',E12.4, ' FOR THIS SAMPLE. ') KOLM 700
C          22 FORMAT(' THE JOB WITH TITLE ',5A4, ' WAS COMPLETED. ') KOLM 710
C          KOLM 720
C          READ DISTRIBUTION NAMES AND JOB CONTROL CARD KOLM 730
C          KOLM 740
C          IFL=0 KOLM 750
C          READ(5,15)DASH KOLM 760
C          READ(5,6)ITITL KOLM 770
C          KOLM 780

```


TRIPLE EXPONENTIAL SMOOTHING

Problem Description

Given a time series X , a smoothing constant, and three coefficients of the prediction equation, this sample program finds the triple exponentially smoothed series S of the time series X .

Program

Description

The sample program for triple exponential smoothing consists of the main program named EXPON, and one subroutine, EXSMO, from the Scientific Subroutine Package.

Capacity

The capacity of the sample program and the format required for data input have been set up as follows:

1. Up to 1000 data points in a given time series
2. (12F6.0) format for input data cards

Therefore, if a problem satisfies the above conditions, the sample program need not be modified. However, if there are more than 1000 data points, the dimension statement in the sample main program must be modified to handle this particular problem. Similarly, if input data cards are prepared using a different format, the input format in the sample main program must be modified. The general rules for program modification are described later.

Input

Control Card

One control card is required for each problem and is read by the main program, EXPON. This card is prepared as follows:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem</u>
1- 6	Problem number (may be alphameric)	SAMPLE
7-10	Number of data points in a given time series	0038
11-15	Smoothing constant, α ($0.0 < \alpha < 1.0$)	0.1
16-25	First coefficient (A) of the prediction equation	0.0
26-35	Second coefficient (B) of the prediction equation	0.0
36-45	Third coefficient (C) of the prediction equation	0.0

Smoothing constant and three coefficients must be keypunched with decimal points.

Leading zeros are not required to be keypunched.

Data Card

Time series data are keypunched using the format (12F6.0). This format assumes that each data point is keypunched in a six-column field and twelve fields per card.

Deck Setup

The deck setup is shown in Figure 62.

Sample

The listing of input cards for the sample problem is presented in Figure 63.

Output

Description

The output of the sample program for triple exponential smoothing includes:

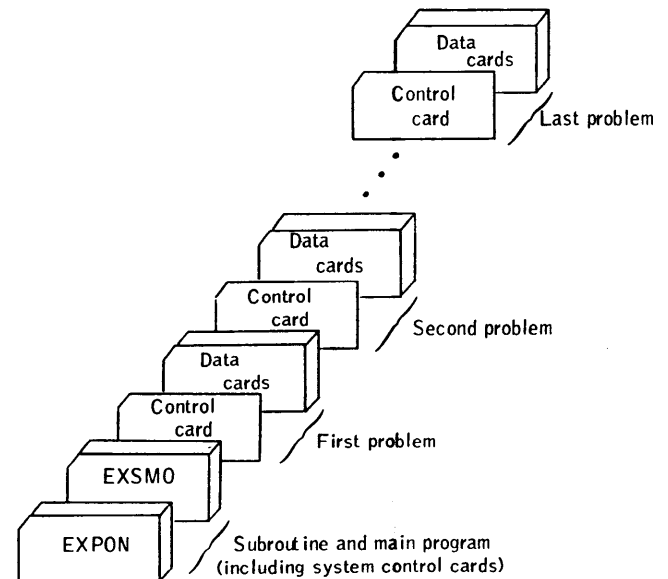


Figure 62. Deck setup (triple exponential smoothing)

```

/ DATA
SAMPLE 38 0.1 0.0 0.0 0.0 10
      430 426 422 419 414 413 412 409 411 417 422 430 20
      438 441 447 455 461 453 448 449 454 463 470 472 40
      476 481 483 487 491 492 485 486 482 479 479 476 50
      472 470 60
    
```

Figure 63. Input listing (triple exponential smoothing)


```

C      READ TIME SERIES DATA
C      READ (5,2) (X(I),I=1,NX)
C      CALL EXSMD (X,NX,AL,A,B,C,S)
C      PRINT UPDATED COEFFICIENTS
C      WRITE (6,6) A,B,C
C      PRINT INPUT AND SMOOTHED DATA
C      WRITE (6,7)
C      DO 200 I=1,NX
200  WRITE (6,8) X(I),S(I)
C      GO TO 100
C      END

```

```

EXPO 610
EXPO 620
EXPO 630
EXPO 640
EXPO 650
EXPO 660
EXPO 670
EXPO 680
EXPO 690
EXPO 700
EXPO 710
EXPO 720
EXPO 730
EXPO 740
EXPO 750
EXPO 760
EXPO 770
EXPO 780

```

MATRIX ADDITION

Problem Description

An input matrix is added to another input matrix to form a resultant matrix. Each set of input matrices and the corresponding output matrix is printed. This procedure is repeated until all sets of input matrices have been processed.

Program

Description

The matrix addition program consists of a main routine, ADSAM, and four subroutines, MATIN, MADD, MXOUT, and LOC. MADD and LOC are from the Scientific Subroutine Package. MATIN and MXOUT are sample subroutines for matrix input and output (see program listings).

Capacity

Matrix size has arbitrarily been set at 1000 data elements.

Input

Control Cards

Each input matrix must be preceded by a parameter card with the following format:

Columns	Contents	For Sample Problem
1-2	Blank	
3-6	Up to four-digit identification code	0001
7-10	Number of rows in matrix	0008
11-14	Number of columns in matrix	0011
15-16	Storage mode of matrix 0 for general matrix 1 for symmetric matrix 2 for diagonal matrix	0

Each input matrix must be followed by a card with a 9-punch in column 1.

A blank card after the last pair of input matrices terminates the run.

Data Cards

Data cards are assumed to have seven fields of ten columns each. The decimal point may appear anywhere in a field. If no decimal point is included, it is assumed that the decimal point is to the right of the last digit. The number in each field may be preceded by blanks. Data elements must be punched by row. A row may continue from card to card. However, each new row must start in the first field of the next card. Only the upper triangular portion of a symmetric matrix or the diagonal elements of a diagonal matrix are contained on data cards. The first element of each new row will be the diagonal element for a matrix with symmetric or diagonal storage mode. Columns 71-80 of data cards may be used for identification, sequence numbering, and so on.

Deck Setup

The deck setup is shown in Figure 65.

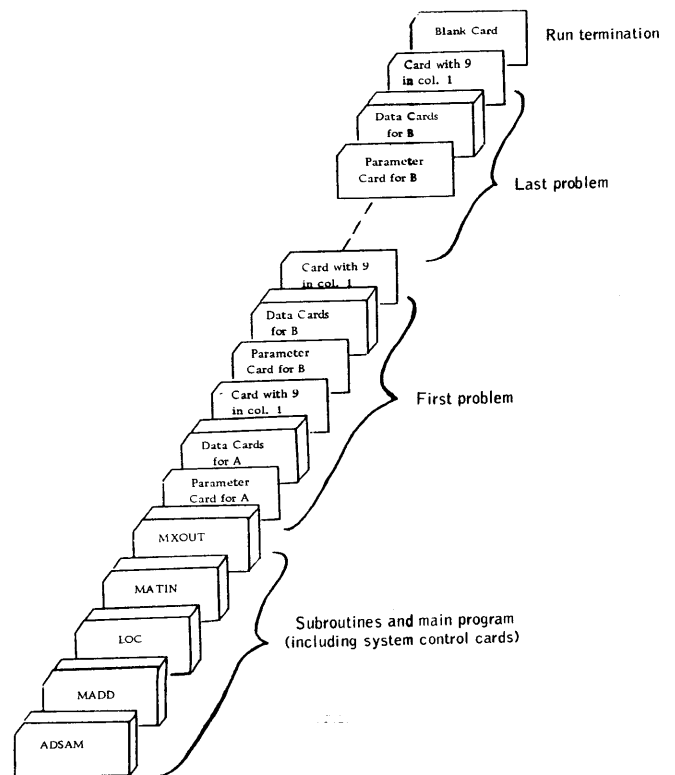


Figure 65. Deck setup (matrix addition)

Sample

A listing of input cards for the sample problem is presented in Figure 66.

```

/ DATA
00010008001100
0.7601008 0.6271892 1.0000000 0.7086843 0.4058519 0.0031426 0.6876602
0.6751766 0.8635910 0.7446845 0.6496329
0.6544085 1.0000000 0.6271892 0.6194650 0.3547574 0.0027470 0.6010878
0.5571068 0.7125728 0.6144597 0.5745585
1.0000000 0.6644085 0.7601008 0.7507505 0.4299425 0.0033291 0.7284786
0.6373449 0.8152021 0.7029582 0.6573101
0.6963269 0.5745585 0.6573101 0.6492243 0.3718001 0.0028789 0.6299642
0.6295047 0.8051740 0.6943108 0.6492243
0.7446845 0.6144597 0.7029582 0.6943108 0.3976204 0.0030789 0.6737132
0.3605070 0.4611099 0.3976204 0.3718001
0.6751766 0.5571068 0.6373449 0.6295047 0.3605070 0.0027915 0.6108296
0.0033291 0.0027470 0.0030789 0.0028789
0.6108296 0.7812874 0.6737132 0.6299642
0.4299425 0.3547574 0.4058519 0.4038593 1.0000000 0.0017776 0.3889673
1.0000000 0.7241215 0.6244183 0.5838704
00020008001100
0.7547505 0.6194650 0.7986843 1.0000000 0.4008593 0.0031039 0.6792011
0.7241215 1.0000000 0.7986843 0.7468050
0.7446845 0.6144597 0.7029582 0.6943108 0.3976204 0.0030789 0.6737132
0.6244183 0.7986843 1.0000000 0.6439786
0.8635910 0.7125728 0.8152021 0.8051740 0.4611099 0.0035705 0.7812874
0.5838704 0.7468050 0.6439786 1.0000000
0.6963269 0.5745585 0.6573101 0.6492243 0.3718001 0.0028789 0.6299642
1.0000000 0.6644085 0.7601008 0.7507505 0.4299425 0.0033291 0.7284786
0.6751766 0.5571068 0.6373449 0.6295047 0.3605070 0.0027915 0.6108296
0.7284786 0.6108296 0.6876602 0.6899673 0.0030119 1.0000000
0.7446845 0.6144597 0.7029582 0.6943108 0.3976204 0.0030789 0.6737132
0.4299425 0.3547574 0.4058519 0.4038593 1.0000000 0.0017776 0.3889673
0.8635910 0.7125728 0.8152021 0.8051740 0.4611099 0.0035705 0.7812874
0.7601008 0.6271892 1.0000000 0.7086843 0.4058519 0.0031426 0.6876602
0.7601008 0.6271892 1.0000000 0.7086843 0.4058519 0.0031426 0.6876602
0.6963269 0.5745585 0.6573101 0.6492243 0.3718001 0.0028789 0.6299642

```

```

MATRIX 1 8 ROWS 11 COLUMNS STORAGE MODE 0 PAGE 1
COLUMN 1 2 3 4 5 6
ROW 1 0.760100E 00 0.627180E 00 0.100000E 01 0.708684E 00 0.405852E 00 0.314260E-02
ROW 2 0.664408E 00 0.100000E 01 0.627180E 00 0.619465E 00 0.354757E 00 0.274700E-02
ROW 3 0.100000E 01 0.664408E 00 0.760101E 00 0.750750E 00 0.429942E 00 0.332910E-02
ROW 4 0.649632E 00 0.574558E 00 0.657310E 00 0.649224E 00 0.371800E 00 0.287890E-02
ROW 5 0.744684E 00 0.614460E 00 0.702958E 00 0.694311E 00 0.397620E 00 0.307890E-02
ROW 6 0.675177E 00 0.557107E 00 0.637345E 00 0.629505E 00 0.360507E 00 0.279150E-02
ROW 7 0.332910E-02 0.274700E-02 0.314260E-02 0.310390E-02 0.177760E-02 0.100000E 01
ROW 8 0.429942E 00 0.354757E 00 0.405852E 00 0.400859E 00 0.100000E 01 0.177760E-02

MATRIX 1 8 ROWS 11 COLUMNS STORAGE MODE 0 PAGE 2
COLUMN 7 8 9 10 11
ROW 1 0.687660E 00 0.675177E 00 0.863591E 00 0.744684E 00 0.696327E 00
ROW 2 0.610829E 00 0.557107E 00 0.712573E 00 0.614460E 00 0.574558E 00
ROW 3 0.728478E 00 0.637345E 00 0.815202E 00 0.702958E 00 0.657310E 00
ROW 4 0.629942E 00 0.629505E 00 0.805174E 00 0.694311E 00 0.649224E 00
ROW 5 0.673713E 00 0.360507E 00 0.461110E 00 0.397620E 00 0.371800E 00
ROW 6 0.610829E 00 0.675177E-02 0.357050E-02 0.307890E-02 0.287890E-02
ROW 7 0.354757E-02 0.610829E 00 0.781287E 00 0.673713E 00 0.629964E 00
ROW 8 0.388967E 00 0.100000E 01 0.724121E 00 0.624418E 00 0.583870E 00

MATRIX 2 8 ROWS 11 COLUMNS STORAGE MODE 0 PAGE 1
COLUMN 1 2 3 4 5 6
ROW 1 0.750750E 00 0.619465E 00 0.708684E 00 0.100000E 01 0.400859E 00 0.310390E-02
ROW 2 0.744684E 00 0.614460E 00 0.702958E 00 0.694311E 00 0.397620E 00 0.307890E-02
ROW 3 0.863591E 00 0.712573E 00 0.815202E 00 0.805174E 00 0.461110E 00 0.357050E-02
ROW 4 0.696327E 00 0.574558E 00 0.657310E 00 0.649224E 00 0.371800E 00 0.287890E-02
ROW 5 0.675177E 00 0.557107E 00 0.637345E 00 0.629505E 00 0.360507E 00 0.279150E-02
ROW 6 0.744684E 00 0.614460E 00 0.702958E 00 0.694311E 00 0.397620E 00 0.307890E-02
ROW 7 0.675177E 00 0.557107E 00 0.637345E 00 0.629505E 00 0.360507E 00 0.279150E-02
ROW 8 0.760101E 00 0.627180E 00 0.100000E 01 0.708684E 00 0.405852E 00 0.314260E-02

MATRIX 2 8 ROWS 11 COLUMNS STORAGE MODE 0 PAGE 2
COLUMN 7 8 9 10 11
ROW 1 0.679201E 00 0.724121E 00 0.100000E 01 0.798684E 00 0.746805E 00
ROW 2 0.673713E 00 0.624418E 00 0.798684E 00 0.100000E 01 0.643979E 00
ROW 3 0.781287E 00 0.583870E 00 0.746805E 00 0.643979E 00 0.100000E 01
ROW 4 0.629964E 00 0.100000E 01 0.664408E 00 0.760101E 00 0.750750E 00
ROW 5 0.610830E 00 0.728478E 00 0.610829E 00 0.687660E 00 0.679201E 00
ROW 6 0.673713E 00 0.429942E 00 0.354757E 00 0.405852E 00 0.400859E 00
ROW 7 0.781287E 00 0.760101E 00 0.627180E 00 0.100000E 01 0.708684E 00
ROW 8 0.687660E 00 0.696327E 00 0.574558E 00 0.657310E 00 0.649224E 00

MATRIX 3 8 ROWS 11 COLUMNS STORAGE MODE 0 PAGE 1
COLUMN 1 2 3 4 5 6
ROW 1 0.151085E 01 0.124644E 01 0.170868E 01 0.170868E 01 0.804711E 00 0.624490E-02
ROW 2 0.140909E 01 0.161446E 01 0.133014E 01 0.131378E 01 0.752378E 00 0.582590E-02
ROW 3 0.186359E 01 0.137698E 01 0.157530E 01 0.155592E 01 0.891052E 00 0.689940E-02
ROW 4 0.139245E 01 0.114912E 01 0.131462E 01 0.129845E 01 0.743600E 00 0.575780E-02
ROW 5 0.141966E 01 0.117157E 01 0.134030E 01 0.132382E 01 0.758127E 00 0.587040E-02
ROW 6 0.141966E 01 0.117157E 01 0.134030E 01 0.132382E 01 0.758127E 00 0.587040E-02
ROW 7 0.864920E 00 0.715320E 00 0.818345E 00 0.808278E 00 0.462876E 00 0.100357E 01
ROW 8 0.119040E 01 0.981938E 00 0.140565E 01 0.110954E 01 0.140585E 01 0.492020E-02

MATRIX 3 8 ROWS 11 COLUMNS STORAGE MODE 0 PAGE 2
COLUMN 7 8 9 10 11
ROW 1 0.136686E 01 0.139930E 01 0.186359E 01 0.154935E 01 0.144313E 01
ROW 2 0.127480E 01 0.118152E 01 0.151124E 01 0.161446E 01 0.121854E 01
ROW 3 0.150977E 01 0.122122E 01 0.156201E 01 0.134684E 01 0.165731E 01
ROW 4 0.125993E 01 0.162950E 01 0.146958E 01 0.145441E 01 0.139977E 01
ROW 5 0.128454E 01 0.108899E 01 0.106220E 01 0.105828E 01 0.105100E 01
ROW 6 0.128454E 01 0.432734E 00 0.358328E 00 0.408931E 00 0.403738E 00
ROW 7 0.784299E 00 0.137093E 01 0.140847E 01 0.167371E 01 0.133865E 01
ROW 8 0.107663E 01 0.169633E 01 0.129868E 01 0.128173E 01 0.123309E 01
END OF CASE

```

Figure 66. Input listing (matrix addition)

Output

Description

The resultant matrix is printed for any size array as a general matrix regardless of the storage mode. Each page is headed with the matrix code number, dimensions, and storage mode. Columns and rows are headed with their respective number. The code number for the output matrix is derived by adding the code numbers for the input matrices.

Sample

The output listing for the sample problem is shown in Figure 67.

Program Modification

Matrix size can be increased or reduced by making the following changes in ADSAM:

1. Modify the DIMENSION statement to reflect the number of elements for A, B, and R.
2. Insert the same number in the third parameter of the two CALL MATIN statements (20 and 45).

Figure 67. Output listing (matrix addition)

The output listing is set for 60 print lines per page, 132 print positions across the page, and double spacing. This can be changed by means of the last three parameters in the three-call MXOUT statements in ADSAM (statements 40, 80, 90).

Operating Instructions

The matrix addition sample program is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and data set 6 is used for output.

Error Messages

The following error conditions will result in messages:

1. Reserved storage area is too small for matrix -- DIMENSIONED AREA TOO SMALL FOR INPUT MATRIX (matrix code no.). GO ON TO NEXT CASE.

2. Input matrices do not have the same dimensions -- MATRIX DIMENSIONS NOT CONSISTENT. GO ON TO NEXT CASE.

3. Number of data cards does not correspond to that required by parameter card -- INCORRECT NUMBER OF DATA CARDS FOR MATRIX (matrix code no.). EXECUTION TERMINATED.

Error conditions 1 and 2 allow the computer run to continue. Error condition 3, however, terminates execution and requires another run to process succeeding cases.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 36 seconds.

```

C ..... AD SA 10
C ..... AD SA 20
C ..... AD SA 30
C ..... AD SA 40
C ..... AD SA 50
C ..... AD SA 60
C ..... AD SA 70
C ..... AD SA 80
C ..... AD SA 90
C ..... AD SA 100
C ..... AD SA 110
C ..... AD SA 120
C ..... AD SA 130
C ..... AD SA 140
C ..... AD SA 150
C ..... AD SA 160
C ..... AD SA 170
C ..... AD SA 180
C ..... AD SA 190
C ..... AD SA 200
C ..... AD SA 210
C ..... AD SA 220
C ..... AD SA 230
C ..... AD SA 240
C ..... AD SA 250
C ..... AD SA 260
C ..... AD SA 270
C ..... AD SA 280
C ..... AD SA 290
C ..... AD SA 300
C ..... AD SA 310
C ..... AD SA 320
C ..... AD SA 330
C ..... AD SA 340
C ..... AD SA 350
C ..... AD SA 360
C ..... AD SA 370
C ..... AD SA 380
C ..... AD SA 390
C ..... AD SA 400
C ..... AD SA 410
C ..... AD SA 420
C ..... AD SA 430
C ..... AD SA 440
C ..... AD SA 450
C ..... AD SA 460
C ..... AD SA 470
C ..... AD SA 480
C ..... AD SA 490
C ..... AD SA 500
C ..... AD SA 510
C ..... AD SA 520
C ..... AD SA 530
C ..... AD SA 540
C ..... AD SA 550
C ..... AD SA 560
C ..... AD SA 570
C ..... AD SA 580
C ..... AD SA 590
C ..... AD SA 600
C ..... AD SA 610
C ..... AD SA 620
C ..... AD SA 630
C ..... AD SA 640
C ..... AD SA 650
C ..... AD SA 660
C ..... AD SA 670
C ..... AD SA 680
C ..... AD SA 690
C ..... AD SA 700
C ..... AD SA 710

```

```

WRITE(6,15)
GO TO 20
55 WRITE(6,14) ICODB
GO TO 37
60 IF(NA-NB) 75,70,75
70 IF(MA-MB) 75,80,75
75 WRITE(6,13)
WRITE(6,15)
GO TO 20
80 CALL MXOUT(ICODB,B,NB,MB,MSB,50,120,2)
ICODR=ICODB+ICODB
CALL MADD(A,B,R,NA,MA,MSA,MSB)
MSR=MSA
IF(MSA=MSB) 90,90,85
85 MSR=MSB
90 CALL MXOUT(ICODR,R,NA,MA,MSR,60,120,2)
WRITE(6,16)
GO TO 20
95 RETURN
END

```

NUMERICAL QUADRATURE INTEGRATION

Problem Description

The tabulated values of a function for a given spacing are integrated. Multiple sets of tabulated values may be processed.

Program

Description

The numerical quadrature integration program consists of a main routine, QDINT, and one subroutine, QSF, from the Scientific Subroutine Package.

Capacity

Up to 500 tabulated values of a function may be integrated.

Input

Control Cards

Each integration requires a parameter card with the following format:

Columns	Contents	For Sample Problem
1- 5	Up to 5-digit numeric identification code	12345
6-10	Number of tabulated values for this function	0020
11-20	Interval between tabulated values	1.0

The first two parameters consist of up to five digits with no decimal point (FORMAT (2I5)). Note that the second parameter may not exceed 500. The third parameter consists of up to ten digits with decimal point. If no decimal point is included, it is assumed that the decimal point is to the right of the field (FORMAT (F10.0)). A blank card following the last set of data terminates the run.

Data Cards

Data cards are assumed to be seven fields of ten columns each. The decimal point may appear anywhere in the field. The number in each field may be preceded by blanks. Columns 71 through 80 of the data cards may be used for identification, sequence numbering, and so on. If there are more than seven tabulated values, the values should continue from card to card with seven values per card until the number of values specified in the parameter card has been reached.

Deck Setup

The deck setup is shown in Figure 68.

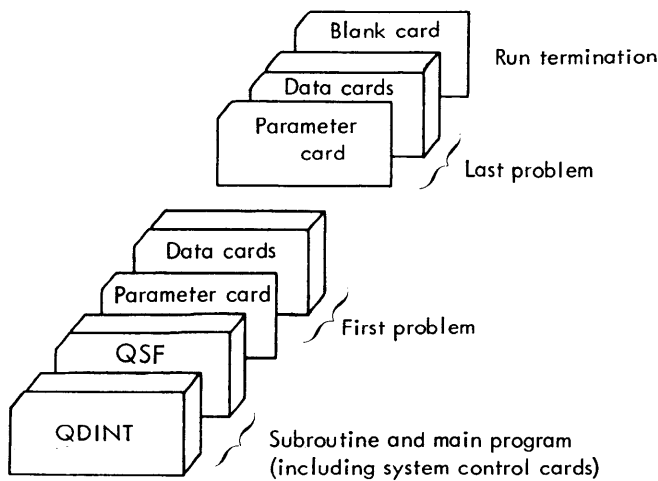


Figure 68 Deck setup (numerical quadrature integration)

Sample

A listing of input cards for the sample program is presented in Figure 69.

/DATA										
12345	20	1.0								10
	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	20
	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	30
	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	40
	10	1.0								50
543	1.0	2.0	3.0	4.0	5.0	6.0	7.0			60
	8.0	9.0	10.0							70
										80
										90

Figure 69. Input listing (numerical quadrature integration)

Output

Description

The identification code number, number of tabulated input values, the interval for the tabulated values, and the resultant integral values at each step are printed.

Sample

The output listing for the sample program is shown in Figure 70.

```

INTEGRATION OF TABULATED VALUES FOR DY/DX USING SUBROUTINE QSF
FUNCTION 12345      20 TABULATED VALUES      INTERVAL = 0.1000000E 01

      RESULTANT VALUE OF INTEGRAL AT EACH STEP IS
0.0      0.1000000E 01 0.3999999E 01 0.5999999E 01 0.7999999E 01 0.9999997E 01
0.1199999E 02 0.1399999E 02 0.1599999E 02 0.1799998E 02 0.1999998E 02 0.2199998E 02
0.2399998E 02 0.2599998E 02 0.2799998E 02 0.2999998E 02 0.3199998E 02 0.3399998E 02
0.3599998E 02 0.3799998E 02

INTEGRATION OF TABULATED VALUES FOR DY/DX USING SUBROUTINE QSF
FUNCTION 543      10 TABULATED VALUES      INTERVAL = 0.1000000E 01

      RESULTANT VALUE OF INTEGRAL AT EACH STEP IS
0.0      0.1499998E 01 0.3399997E 01 0.7499997E 01 0.1199997E 02 0.1749998E 02
0.2399998E 02 0.3149998E 02 0.3999998E 02 0.4949998E 02
    
```

Figure 70. Output listing (numerical quadrature integration)

Program Modification

The maximum number of tabulated values acceptable to the sample program may be changed by modifying the dimension statement in QDINT. The format of the parameter cards and data cards may be changed by modifying statements 10 and 40, respectively, in QDINT.

Operating Instructions

The numerical quadrature integration sample program is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and data set 6 is used for output.

Error Messages

The following conditions will result in error messages:

1. The number of tabulated values specified in the parameter card is less than or equal to one -- ILLEGAL CONDITION. NUMBER OF TABULATED VALUES IS LESS THAN THREE. The program will go on to the next set of data.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is six seconds.

```

C ..... QDIN 10
C ..... QDIN 20
C ..... QDIN 30
C ..... QDIN 40
C ..... QDIN 50
C ..... QDIN 60
C ..... QDIN 70
C ..... QDIN 80
C ..... QDIN 90
C ..... QDIN 100
C ..... QDIN 110
C ..... QDIN 120
C ..... QDIN 130
C ..... QDIN 140
C ..... QDIN 150
C ..... QDIN 160
C ..... QDIN 170
C ..... QDIN 180
C ..... QDIN 190
C ..... QDIN 200
C ..... QDIN 210
C ..... QDIN 220
C ..... QDIN 230
C ..... QDIN 240
C ..... QDIN 250
C ..... QDIN 260
C ..... QDIN 270
C ..... QDIN 280
C ..... QDIN 290
C ..... QDIN 300
C ..... QDIN 310
C ..... QDIN 320
C ..... QDIN 330
C ..... QDIN 340
C ..... QDIN 350
C ..... QDIN 360
C ..... QDIN 370
C ..... QDIN 380
C ..... QDIN 390
C ..... QDIN 400
C ..... QDIN 410
C ..... QDIN 420
C ..... QDIN 430
C ..... QDIN 440
C ..... QDIN 450
C ..... QDIN 460
C ..... QDIN 470
C ..... QDIN 480
C ..... QDIN 490
C ..... QDIN 500
C ..... QDIN 510
C ..... QDIN 520
C ..... QDIN 530
C ..... QDIN 540
C ..... QDIN 550
C ..... QDIN 560
C ..... QDIN 570
C ..... QDIN 580
C ..... QDIN 590
C ..... QDIN 600
C ..... QDIN 610
C ..... QDIN 620
C ..... QDIN 630
C ..... QDIN 640
C ..... QDIN 650
C ..... QDIN 660
C ..... QDIN 670

SAMPLE PROGRAM FOR INTEGRATION OF A TABULATED FUNCTION BY
NUMERICAL QUADRATURE - QDINT

PURPOSE
INTEGRATES A SET OF TABULATED VALUES FOR F(X) GIVEN THE
NUMBER OF VALUES AND THEIR SPACING

REMARKS
THE NUMBER OF VALUES MUST BE MORE THAN TWO AND THE SPACING
GREATER THAN ZERO

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
QSF

METHOD
READS CONTROL CARD CONTAINING THE CODE NUMBER, NUMBER OF
VALUES, AND THE SPACING OF THE FUNCTION VALUES CONTAINED
ON THE FOLLOWING DATA CARDS. DATA CARDS ARE THEN READ AND
INTEGRATION IS PERFORMED. MORE THAN ONE CONTROL CARD AND
CORRESPONDING DATA CAN BE INTEGRATED IN ONE RUN. EXECUTION
IS TERMINATED BY A BLANK CONTROL CARD.

.....
THE FOLLOWING DIMENSION MUST BE AS LARGE AS THE MAXIMUM NUMBER
OF TABULATED VALUES TO BE INTEGRATED

DIMENSION Z(500)

.....
IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE
C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION
STATEMENT WHICH FOLLOWS.

DOUBLE PRECISION Z,SPACE

.....
1C FORMAT (2I5,F10.0)
20 FORMAT(1H1,GZHIINTEGRATION OF TABULATED VALUES FOR DY/DX USING SUBR
1QUTINE QSF//1H ,10HFUNCTION ,15.3X,15,17H TABULATED VALUES,
25X,10HINTERVAL =,E15.8//)
22 FORMAT(1H ,17HILLEGAL CCNDITION/)
23 FORMAT(1H ,45HNUMBER OF TABULATED VALUES IS LESS THAN THREE)
30 FORMAT(1H ,7X,*RESULTANT VALUE OF INTEGRAL AT EACH STEP IS *,
11H ,6E15.8)
32 FORMAT(7F10.0)

35 READ(5,10)ICOD,NUMBR,SPACE
1F(1COD=NUMBR)70,70,38
38 WRITE(6,20)ICOD,NUMBR,SPACE
50 READ(5,32)(Z(I),I=1,NUMBR)
1F(NUMBR=3)1C0,55,55
55 CALL QSF(SPACE,I,NUMBR)
60 WRITE(6,30)(Z(I),I=1,NUMBR)
GO TO 35
70 RETURN
1CC WRITE(6,22)
WRITE (6,23)
GO TO 35
20C WRITE(6,22)
GO TO 35
END

```

RUNGE-KUTTA INTEGRATION

Problem Description

A differential equation of the form:

$$\frac{dy}{dx} = f(x, y)$$

is integrated with initial conditions as specified in a parameter card. The differential equation is defined in the form of a function subprogram that is provided by the user.

Program

Description

The Runge-Kutta integration program consists of a main routine RKINT, one subroutine RK2 from the Scientific Subroutine Package, and one user-supplied function subprogram FUN, which defines the differential equation to be integrated.

Capacity

Up to 500 values of the integral may be tabulated.

Input

Control Cards

Each integration requires a parameter card with the following format:

Columns	Contents	For Sample Problem
1-10	Initial value of $X = X_0$	1.0
11-20	Initial value of $Y = Y(X_0)$	0.0
21-30	Step size	0.01
31-35	Number of steps required between tabulated values	10
36-40	Total number of tabulated values required	30

The first three parameters consist of up to ten digits with decimal point. If no decimal point is included, it is assumed that the decimal point is to the right of the field.

(FORMAT (F10.0))

The last two parameters consist of up to four digits plus a blank with no decimal point.

(FORMAT (I5))

Multiple parameter cards may be used. A blank card terminates the run.

Data Cards

None.

Deck Setup

The deck setup is shown in Figure 71.

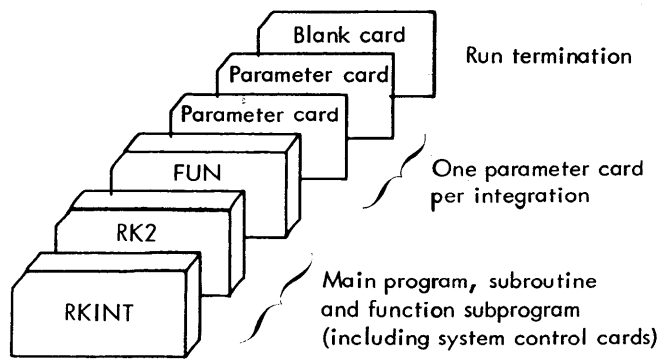


Figure 71. Deck setup (Runge-Kutta integration)

Sample

A listing of the input cards for the sample problem is presented in Figure 72.

Figure 72. Input listing (Runge-Kutta integration)

Output

Description

The values for the initial conditions and the tabulated values of the integral are printed.

Sample

The output listing for the sample problem is shown in Figure 73.

SOLUTION OF DY/DX=FUN(X,Y) BY RK2 SUBROUTINE

H= 0.010 X0= 1.000 Y0= 0.0

X	Y(X)
1.10	0.95310390E-01
1.20	0.18232232E 00
1.30	0.26236582E 00
1.40	0.33647484E 00
1.50	0.40546888E 00
1.60	0.47000873E 00
1.70	0.53063482E 00
1.80	0.58779466E 00
1.90	0.64186341E 00
2.00	0.69315827E 00
2.10	0.74194998E 00
2.20	0.78847140E 00
2.30	0.83292466E 00
2.40	0.87548572E 00
2.50	0.91630906E 00
2.60	0.95553130E 00
2.70	0.99327296E 00
2.80	0.10296392E 01
2.90	0.10647268E 01
3.00	0.10986242E 01
3.10	0.11314125E 01
3.20	0.11631584E 01
3.30	0.11939259E 01
3.40	0.12237749E 01
3.50	0.12527580E 01
3.60	0.12809258E 01
3.70	0.13083200E 01
3.80	0.13349857E 01
3.90	0.13609591E 01
4.00	0.13862734E 01

Figure 73. Output listing (Runge-Kutta integration)

Program Modification

The function subprogram FUN may be replaced by any function subprogram having the same name and parameter list. In this way, the user may define any desired first-order differential equation. The maxi-

imum number of tabulated values may be changed by altering the dimension statement in the sample program RKINT.

Operating Instructions

The sample program for Runge-Kutta integration is a standard FORTRAN program. Special operating instructions are not required. Data set reference 5 is used for input, and data set reference 6 is used for output.

Error Messages

None.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is twelve seconds.

```

C
C
C ..... RKIN 10
C ..... RKIN 20
C ..... RKIN 30
C SAMPLE PROGRAM FOR RUNGE-KUTTA INTEGRATION OF A GIVEN FUNCTION RKIN 40
C WITH TABULATED OUTPUT - RKINT RKIN 50
C ..... RKIN 60
C PURPOSE RKIN 70
C INTEGRATES THE FUNCTION SUBPROGRAM FUN USING THE INITIAL RKIN 80
C CONDITIONS CONTAINED IN CONTROL CARDS. PRODUCES TABULATED RKIN 90
C OUTPUT. RKIN 100
C ..... RKIN 110
C REMARKS RKIN 120
C NONE RKIN 130
C ..... RKIN 140
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED RKIN 150
C RK2 RKIN 160
C FUN - USER-SUPPLIED FUNCTION SUBPROGRAM GIVING RKIN 170
C DY/DX=FUN(X,Y) RKIN 180
C ..... RKIN 190
C METHOD RKIN 200
C READS CONTROL CARD CONTAINING INITIAL VALUES OF X AND Y, RKIN 210
C STEP SIZE, NUMBER OF STEPS DESIRED BETWEEN TABULATED VALUES, RKIN 220
C AND NUMBER OF TABULATED VALUES REQUIRED. PROGRAM THEN ENTERS RKIN 230
C RK2 TO PERFORM INTEGRATION. MULTIPLE CONTROL CARDS CAN BE RKIN 240
C USED ON THE SAME FUNCTION. RKIN 250
C ..... RKIN 260
C ..... RKIN 270
C THE FOLLOWING DIMENSION MUST BE AS LARGE AS THE MAXIMUM RKIN 280
C NUMBER OF TABULATED VALUES DESIRED RKIN 290
C ..... RKIN 300
C DIMENSION A(500) RKIN 310
C ..... RKIN 320
C EXTERNAL FUN RKIN 330
C ..... RKIN 340
C ..... RKIN 350
C ..... RKIN 360
C ..... RKIN 370
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE RKIN 380
C C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION RKIN 390
C STATEMENT WHICH FOLLOWS. RKIN 400
C ..... RKIN 410
C DOUBLE PRECISION H,X0,Y0,A,FUN RKIN 420
C ..... RKIN 430
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS RKIN 440
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS RKIN 450
C ROUTINE. RKIN 460
C ..... RKIN 470
C USER FUNCTION SUBPROGRAM, FUN, MUST BE IN DOUBLE PRECISION. RKIN 480
C ..... RKIN 490
C ..... RKIN 500
C ..... RKIN 510
C ..... RKIN 520
C 1 FORMAT (3F10.0,2I5) RKIN 530
C 2 FORMAT(1H1,7X,44HSOLUTION OF DY/DX=FUN(X,Y) BY RK2 SUBROUTINE// RKIN 540
C 11H ,1CX,2HH=,F7.3,2X,3HXD=,F7.3, 2X,3HYD=,F7.3//1H ,12X,1HX,18X, RKIN 550
C 24HY(X) //) RKIN 560
C 3 FORMAT(1H ,1CX,F5.2,10X,E15.8) RKIN 570
C ..... RKIN 580
C READ CONTROL CARD CONTAINING ITEMS LISTED UNDER METHOD. RKIN 590
C ..... RKIN 600
C 10 READ(5,1)X0,Y0,H,JNT,IENT RKIN 610
C ..... RKIN 620
C CHECK IF CARD IS BLANK. IF SO, RETURN. RKIN 630
C ..... RKIN 640
C IF(IENT)2C,4C,2C RKIN 650
C ..... RKIN 660
C WRITE HEADING INFORMATION. RKIN 670
C ..... RKIN 680
C 20 WRITE(6,2)H,X0,Y0 RKIN 690
C ..... RKIN 700
C PERFORM INTEGRATION RKIN 710
C ..... RKIN 720
C CALL RK2(FUN,H,X0,Y0,JNT,IENT,A) RKIN 730
C ..... RKIN 740
C WRITE OUTPUT RKIN 750
C ..... RKIN 760
C STEP=FLOAT(JNT)*H RKIN 770
C X=X0

```



```

DO 3C I=1,IENT
X=X+STEP
3C WRITE(6,3)X,A(1)
C
C      GC BACK AND CHECK FOR ADDITIONAL CONTROL CARD.
C
GO TO 10
4C RETURN
END

```

```

RKIN 780
RKIN 790
RKIN 800
RKIN 810
RKIN 820
RKIN 830
RKIN 840
RKIN 850
RKIN 860

```

POLYNOMIAL ROOTS

Problem Description

The real and complex roots are computed for a real polynomial with given coefficients. Multiple sets of coefficients may be processed.

Program

Description

The polynomial roots sample program consists of a main routine, SMPRT, and one subroutine POLRT from the Scientific Subroutine Package.

Capacity

Roots for polynomials of order 36 or less may be computed.

Input

Control Cards

Each set of data requires a control card with the following format:

<u>Columns</u>	<u>Contents</u>	<u>For Sample Problem</u>
1	Blank	
2-5	Up to four-digit identification code	360
6-8	Blank	
9-10	Order of polynomial	9

The first parameter consists of up to four digits without decimal point. The second parameter consists of up to two digits with no decimal point. The order of the polynomial must be less than or equal to 36.

Data Cards

Data cards are assumed to have seven fields of ten columns each. The decimal point may appear anywhere in the field. If no decimal point is included, it is assumed to be to the right of the field. The number in each field may be preceded by blanks. Columns 71 to 80 of the data cards may be used for identification, sequence numbering, and so on. If there are more than seven coefficients, the values should continue from card to card with seven values per card until the number of values has been reached that is one greater than the order of the polynomial.

The first coefficient is for the constant term of the polynomial and the last coefficient for the highest order term. Fields with zero coefficients may be left blank.

Deck Setup

The deck setup is shown in Figure 74.

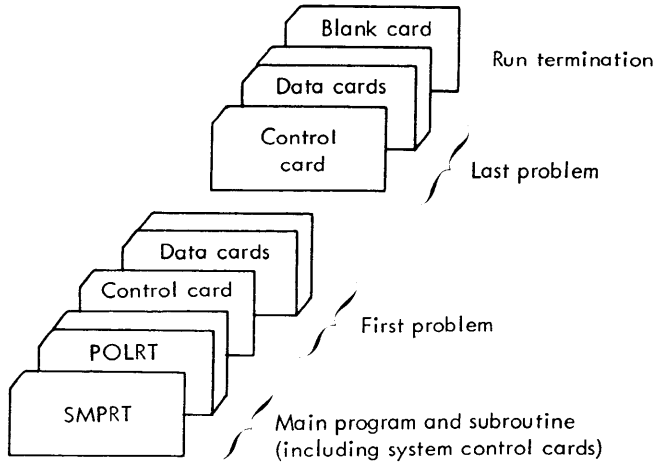


Figure 74. Deck setup (polynomial roots)

Sample

A listing of the input cards for the sample program is shown in Figure 75.

```

/ DATA          10
 36C            20
  -1.0         30
                40
                50
                1.0
                1.0
    
```

Figure 75. Input listing (polynomial roots)

Output

Description

The identification code, the polynomial order, the input coefficients, and the real and complex roots are printed.

Sample

The output listing of the sample program is shown in Figure 76.

```

REAL AND COMPLEX ROOTS OF A POLYNOMIAL USING SUBROUTINE POLRT
FOR POLYNOMIAL 360 OF ORDER 9
THE INPUT COEFFICIENTS ARE
-0.1000000E 01  0.0      0.0      0.0      0.0
 0.1000000E 01  0.0      0.0      0.0      0.0
                                0.1000000E 01  0.0      0.0

REAL ROOT      COMPLEX ROOT
0.7206228E 00  C.7609009E 00
0.7206228E 00  -0.7609009E 00
-0.1019271E 01  -0.2436276E 00
-0.1019271E 01  0.2436276E 00
C.9105257E 00  C.C
-0.4552628E 00  -C.7885384E 00
-0.4552628E 00  C.7885384E 00
C.2986479E 00  -0.1004528E 01
0.2986479E 00  C.1004528E 01
    
```

Figure 76. Output listing (polynomial roots)

Program Modification

The maximum order of the polynomial is fixed by the subroutine POLRT. The sample program can accept polynomials up to the maximum of 36th order, which is allowed by the subroutine. The format of the control card and data cards may be changed by modifying statements 10 and 40, respectively, in SMPRT.

Operating Instructions

The polynomial roots sample program is a standard FORTRAN program. Special operating instructions are not required. Data set 5 is used for input, and data set 6 is used for output.

Error Messages

The following conditions will result in error messages:

1. The order of the polynomial specified in the control card is less than one -- ORDER OF POLYNOMIAL LESS THAN ONE.
The program will go on to the next set of data.
2. The order of the polynomial specified in the control card is greater than 36 -- ORDER OF POLYNOMIAL GREATER THAN 36.
The program will go on to the next set of data.
3. The subroutine POLRT is unable to determine a root after 500 iterations on eight different starting values -- UNABLE TO DETERMINE ROOT. THOSE ALREADY FOUND ARE...

The program will print all the roots that were computed and then go on to the next set of data.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is eleven seconds.

```

C ..... SMPR 10
C ..... SMPR 20
C ..... SMPR 30
C ..... SMPR 40
C ..... SMPR 50
C ..... SMPR 60
C ..... SMPR 70
C ..... SMPR 80
C ..... SMPR 90
C ..... SMPR 100
C ..... SMPR 110
C ..... SMPR 120
C ..... SMPR 130
C ..... SMPR 140
C ..... SMPR 150
C ..... SMPR 160
C ..... SMPR 170
C ..... SMPR 180
C ..... SMPR 190
C ..... SMPR 200
C ..... SMPR 210
C ..... SMPR 220
C ..... SMPR 230
C ..... SMPR 240
C ..... SMPR 250
C ..... SMPR 260
C ..... SMPR 270
C ..... SMPR 280
C ..... SMPR 290
C ..... SMPR 300
C ..... SMPR 310
C ..... SMPR 320
C ..... SMPR 330
C ..... SMPR 340
C ..... SMPR 350
C ..... SMPR 360
C ..... SMPR 370
C ..... SMPR 380
C ..... SMPR 390
C ..... SMPR 400
C ..... SMPR 410
C ..... SMPR 420
C ..... SMPR 430
C ..... SMPR 440
C ..... SMPR 450
C ..... SMPR 460
C ..... SMPR 470
C ..... SMPR 480
C ..... SMPR 490
C ..... SMPR 500
C ..... SMPR 510
C ..... SMPR 520
C ..... SMPR 530
C ..... SMPR 540
C ..... SMPR 550
C ..... SMPR 560
C ..... SMPR 570
C ..... SMPR 580
C ..... SMPR 590
C ..... SMPR 600
C ..... SMPR 610
C ..... SMPR 620
C ..... SMPR 630
C ..... SMPR 640
C ..... SMPR 650
C ..... SMPR 660
C ..... SMPR 670
C ..... SMPR 680
C ..... SMPR 690
C ..... SMPR 700
C ..... SMPR 710
C ..... SMPR 720
C ..... SMPR 730
C ..... SMPR 740
C ..... SMPR 750
C ..... SMPR 760
C ..... SMPR 770

```

SOLUTION OF SIMULTANEOUS EQUATIONS

Problem Description

A solution is obtained for a set of simultaneous equations by the method of elimination using largest pivotal divisor. Both the input data and the solution values are printed. This procedure is repeated until all sets of input data have been processed.

Program

Description

The solution of the simultaneous equations program consists of a main routine, SOLN, and four subroutines, MATIN, SIMQ, MXOUT, and LOC. SIMQ and LOC are from the Scientific Subroutine Package. MATIN and MXOUT are sample subroutines for matrix input and output (see program listings).

Capacity

The program will solve up to 50 equations. This can easily be changed as described under "Program Modification" below.

Input

Control Cards

A parameter card with the following format must precede each matrix of coefficients:

Columns	Contents	For Sample Problem
1-2	Blank	
3-6	Up to four-digit identification code (numeric only)	1
7-10	Number of rows in matrix	10
11-14	Number of columns in matrix (same as number of rows)	10

Each matrix must be followed by a card with a 9-punch in column 1. This, in turn, is followed by the constant vector.

A blank card after the last set of input data terminates the run.

Data Cards

Data Cards are assumed to have seven fields of ten columns each. The decimal point may appear anywhere in a field. If no decimal point is included, it is assumed that the decimal point is to the right of the last digit. The number in each field may be preceded by blanks. Equation coefficients must be punched by row. A row may continue from card to card. However, each new row must start in the first field of the next card. The vector of constants is punched in continuous data fields following the 9 card. Columns 71-80 of data cards may be used for identification, sequence numbering, and so on.

Deck Setup

The deck setup is shown in Figure 77.

Sample

A listing of input cards for the sample problem is presented in Figure 78.

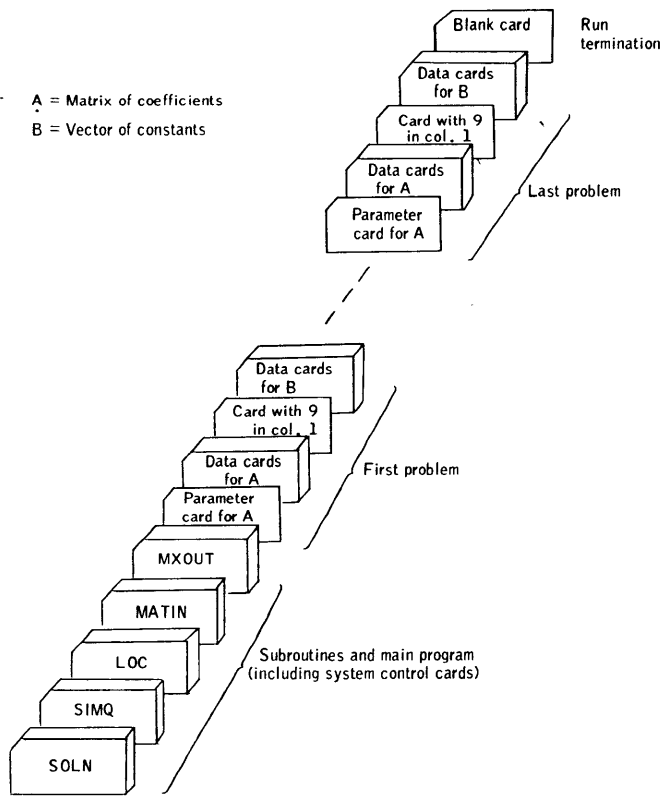


Figure 77. Deck setup (solution of simultaneous equations)

```

/DA
000100100010
1.000000 0.6644085 0.7501008 0.7507505 0.4299425 0.0033291 0.7284786
0.6751766 0.8635910 0.7446845
0.6644085 1.0000000 0.6271802 0.6194650 0.3547574 0.3027470 0.6010878
0.5571068 0.7125728 0.6144597
0.7601008 0.6271802 1.0000000 0.7086843 0.4058519 0.0031426 0.6876602
0.6373449 0.8152021 0.7029582
0.7507505 0.6194650 0.7086843 1.0000000 0.4008593 0.0031039 0.6792011
0.6295047 0.8051740 0.6943108
0.4299425 0.3547574 0.4058519 0.4008593 1.0000000 0.0017776 0.3889673
0.3605070 0.4611099 0.3976204
0.0033291 0.0027470 0.0031426 0.0031039 0.0017776 1.0000000 0.0030119
0.0027915 0.0035705 0.0030789
0.7284786 0.6010878 0.6876602 0.6792011 0.3889673 0.0030119 1.0000000
0.6108295 0.7812874 0.6737132
0.6751766 0.5571068 0.6373449 0.6295047 0.3605070 0.0027915 0.6108296
1.0000000 0.7241215 0.6244183
0.8635910 0.7125728 0.8152021 0.8051740 0.4611099 0.0035705 0.7812874
0.7241215 1.0000000 0.7986682
0.7446845 0.6144597 0.7029582 0.6943108 0.3976204 0.0030789 0.6737132
0.6244183 0.7986682 1.0000000
9
110. -120. 10. 145. -50. 44.2 -14.
38.5 22. 1650.

```

Figure 78. Input listing (solution of simultaneous equations)

Output

Description

The original matrix is printed for any size array. Each page is headed with the matrix code number, dimensions, and storage mode (always 0 in this sample program). Columns and rows are headed with their respective number. The original vector of constants is also printed. The solution values are then listed. This output is given for each case to be processed.

Sample

The output listing for the sample problem is shown in Figure 79.

MATRIX	1	10 ROWS	10 COLUMNS	STORAGE MODE 0	PAGE 1	5	6
COLUMN	1	2	3	4	5	6	
ROW 1	0.100000E 01	0.664408E 00	0.760101E 00	0.750750E 00	0.429942E 00	0.332910E-02	
ROW 2	0.664408E 00	0.100000E 01	0.627180E 00	0.619465E 00	0.354757E 00	0.274700E-02	
ROW 3	0.760101E 00	0.627180E 00	0.100000E 01	0.708684E 00	0.405852E 00	0.314260E-02	
ROW 4	0.750750E 00	0.619465E 00	0.708684E 00	0.100000E 01	0.400859E 00	0.310390E-02	
ROW 5	0.429942E 00	0.354757E 00	0.405852E 00	0.400859E 00	0.100000E 01	0.177740E-02	
ROW 6	0.332910E-02	0.274700E-02	0.314260E-02	0.310390E-02	0.177740E-02	0.100000E 01	
ROW 7	0.728479E 00	0.601088E 00	0.687660E 00	0.679201E 00	0.388967E 00	0.301190E-02	
ROW 8	0.675177E 00	0.557107E 00	0.637345E 00	0.629505E 00	0.360507E 00	0.279150E-02	
ROW 9	0.863591E 00	0.712573E 00	0.815202E 00	0.805174E 00	0.461110E 00	0.357050E-02	
ROW 10	0.744684E 00	0.614460E 00	0.702958E 00	0.694311E 00	0.397620E 00	0.307890E-02	

MATRIX	1	10 ROWS	10 COLUMNS	STORAGE MODE 0	PAGE 2	7	8	9	10
ROW 1	0.728479E 00	0.675177E 00	0.637345E 00	0.629505E 00	0.360507E 00	0.744684E 00			
ROW 2	0.601088E 00	0.557107E 00	0.637345E 00	0.629505E 00	0.360507E 00	0.614460E 00			
ROW 3	0.687660E 00	0.637345E 00	0.637345E 00	0.629505E 00	0.360507E 00	0.702958E 00			
ROW 4	0.679201E 00	0.629505E 00	0.637345E 00	0.629505E 00	0.360507E 00	0.694311E 00			
ROW 5	0.388967E 00	0.360507E 00	0.637345E 00	0.629505E 00	0.360507E 00	0.397620E 00			
ROW 6	0.301190E-02	0.279150E-02	0.357050E-02	0.357050E-02	0.357050E-02	0.307890E-02			
ROW 7	0.100000E 01	0.610830E 00	0.610830E 00	0.781287E 00	0.781287E 00	0.673713E 00			
ROW 8	0.610830E 00	0.100000E 01	0.724121E 00	0.724121E 00	0.724121E 00	0.624418E 00			
ROW 9	0.781287E 00	0.724121E 00	0.100000E 01	0.100000E 01	0.100000E 01	0.798668E 00			
ROW 10	0.673713E 00	0.624418E 00	0.624418E 00	0.798668E 00	0.798668E 00	0.100000E 01			

ORIGINAL B VECTOR

1	0.110000E 03
2	-0.120000E 03
3	0.100000E 02
4	0.145000E 03
5	-0.500000E 02
6	0.442000E 02
7	-0.140000E 02
8	0.385000E 02
9	0.220000E 02
10	0.165000E 04

SOLUTION VALUES

1	-0.283124E 03
2	-0.567240E 03
3	-0.516456E 03
4	-0.259155E 02
5	-0.179352E 03
6	0.435176E 02
7	-0.479274E 03
8	-0.230430E 03
9	-0.210172E 04
10	0.480574E 04

END OF CASE

Figure 79. Output listing (solution of simultaneous equations)

Program Modification

The size of the maximum problem to be solved can be increased or decreased by making the following changes in SOLN:

1. Modify the DIMENSION statement to reflect the maximum number of elements for matrix A (= N x N) and the maximum number of equations (N) for B.

2. Insert the dimension size for A in the third argument of the CALL MATIN statement (statement 25).

The matrix listing is set for 60 print lines per page, 120 print positions across the page, and double spacing. This can be changed by means of the last three arguments in the CALL MXOUT statement in SOLN (statement 65). The format of solution values can be altered by changing statement 21 in SOLN.

Operating Instructions

The sample program for the solution of simultaneous equations is a standard FORTRAN program. Special operating instructions are not required. Data set reference 5 is used for input, and data set reference 6 is used for output.

Error Messages

The following error conditions will result in messages:

1. Reserved storage area is too small for matrix -- DIMENSIONED AREA TOO SMALL FOR INPUT MATRIX (matrix code no.). GO ON TO NEXT CASE.
2. Matrix of coefficients is not square -- ROW AND COLUMN DIMENSIONS NOT EQUAL FOR MATRIX (matrix code no.). GO ON TO NEXT CASE.
3. Number of data cards does not correspond to that required by parameter card -- INCORRECT NUMBER OF DATA CARDS FOR MATRIX (matrix code no.). EXECUTION TERMINATED.
4. Singular input matrix -- MATRIX IS SINGULAR. GO ON TO NEXT CASE.

Error conditions 1, 2, and 4 allow the computer run to continue. Error condition 3, however, terminates execution and requires another run to process succeeding cases.

Timing

The execution time of this sample program on a System/360, Model 30, using an IBM 2540 Card Reader as input and an IBM 1403, Model 3 as output, is 21 seconds.

```

C .....SOLN 220
C MATRIX IS DIMENSIONED FOR 2500 ELEMENTS. THEREFORE, NUMBER OF SOLN 230
C EQUATIONS TO BE SOLVED CANNOT EXCEED 50 UNLESS DIMENSION SOLN 240
C STATEMENT IS CHANGED SOLN 250
C DIMENSION A(2500),B(50) SOLN 260
C SOLN 270
C SOLN 280
C SOLN 290
C 10 FORMAT(1H1,34HSOLUTION OF SIMULTANEOUS EQUATIONS) SOLN 300
C 11 FORMAT(1H0,44NDIMENSIONED AREA TOO SMALL FOR INPUT MATRIX ,I4) SOLN 310
C 12 FORMAT(1H0,20HEXECUTION TERMINATED) SOLN 320
C 13 FORMAT(1H0,4THROW AND COLUMN DIMENSIONS NOT EQUAL FOR MATRIX ,I4) SOLN 330
C 14 FORMAT(1H0,42HINCORRECT NUMBER OF DATA CARDS FOR MATRIX ,I4) SOLN 340
C 15 FORMAT(1H0,18HGO ON TO NEXT CASE) SOLN 350
C 16 FORMAT(1H0,30HSTRUCTURE CODE IS NOT ZERO FOR MATRIX ,I4) SOLN 360
C 17 FORMAT(1H1,17HORIGINAL B VECTOR,////) SOLN 370
C 18 FORMAT(1H1,15HSOLUTION VALUES,////) SOLN 380
C 19 FORMAT(1H0,18HMATRIX IS SINGULAR) SOLN 390
C 20 FORMAT(7F10.0) SOLN 400
C 21 FORMAT(13,10X,E16.6) SOLN 410
C 22 FORMAT(1H0,11HEND OF CASE) SOLN 420
C .....SOLN 430
C SOLN 440
C SOLN 450
C SOLN 460
C WRITE(6,10) SOLN 470
C 25 CALL MATIN(ICOO,A,2500,N,N,MS,IER) SOLN 480
C IF(N) 3C,95,30 SOLN 490
C 3C IF(IER-1) 45,35,40 SOLN 500
C 35 WRITE(6,11) IC00 SOLN 510
C GO TO 90 SOLN 520
C 40 WRITE(6,14) IC00 SOLN 530
C GO TO 95 SOLN 540
C 45 IF(N-N) 50,55,90 SOLN 550
C 50 WRITE(6,13) IC00 SOLN 560
C GO TO 90 SOLN 570
C 55 IF(N) 60,65,60 SOLN 580
C 60 WRITE(6,16) IC00 SOLN 590
C GO TO 90 SOLN 600
C 65 CALL MXOUT(ICOO,A,N,M,MS,60,120,2) SOLN 610
C READ(5,20) (B(I),I=1,M) SOLN 620
C WRITE(6,17) SOLN 630
C DO TO I=1,M SOLN 640
C 70 WRITE(6,21) I,B(I) SOLN 650
C CALL SING(A,B,N,KS) SOLN 660
C IF(KS-1) 80,75,80 SOLN 670
C 75 WRITE(6,19) SOLN 680
C WRITE(6,15) SOLN 690
C GO TO 25 SOLN 700
C 80 WRITE(6,18) SOLN 710
C DO 85 I=1,M SOLN 720
C 85 WRITE(6,21) I,B(I) SOLN 730
C WRITE(6,22) SOLN 740
C GO TO 25 SOLN 750
C 90 READ(5,20) (B(I),I=1,M) SOLN 760
C WRITE(6,15) SOLN 770
C GO TO 25 SOLN 780
C 95 WRITE(6,12) SOLN 790
C RETURN SOLN 800
C END

```

```

C .....SOLN 10
C .....SOLN 20
C .....SOLN 30
C .....SOLN 40
C .....SOLN 50
C .....SOLN 60
C .....SOLN 70
C .....SOLN 80
C .....SOLN 90
C .....SOLN 100
C .....SOLN 110
C .....SOLN 120
C .....SOLN 130
C .....SOLN 140
C .....SOLN 150
C .....SOLN 160
C .....SOLN 170
C .....SOLN 180
C .....SOLN 190
C .....SOLN 200
C .....SOLN 210

```



```

C
C   NLL=NL
C   IF(NS) 16, 16, 10
C   SORT BASE VARIABLE DATA IN ASCENDING ORDER
C
10 DO 15 I=1,N
   DO 14 J=1,N
     IF(A(I)-A(J)) 14, 14, 11
11 L=I-N
   LL=J-N
   DO 12 K=L,M
     L=L+N
     LL=LL+N
     F=A(L)
     A(LL)=A(LL)
12 A(LL)=F
14 CONTINUE
15 CONTINUE
C
C   TEST NLL
C
16 IF(NLL) 20, 18, 20
18 NLL=50
C
C   PRINT TITLE
C
20 WRITE(6,11)NO
C
C   DEVELOP BLANK AND DIGITS FOR PRINTING
C
REWIND 13
WRITE (13,4)
REWIND 13
READ (13,5) BLANK,(ANG(I),I=1,9)
REWIND 13
C
C   FIND SCALE FOR BASE VARIABLE
C
XSCAL=(A(N)-A(1))/(FLOAT(NLL-1))
C
C   FIND SCALE FOR CROSS-VARIABLES
C
M1=N+1
YMIN=A(M1)
YMAX=YMIN
M2=M*N
DO 40 J=M1,M2
  IF(A(J)-YMIN) 28,26,26
26 IF(A(J)-YMAX) 40,40,30
28 YMIN=A(J)
  GO TO 40
30 YMAX=A(J)
40 CONTINUE
  YSCAL=(YMAX-YMIN)/100.0
C
C   FIND BASE VARIABLE PRINT POSITION
C
XB=A(1)
L=1
MY=M-1
I=1
45 F=I-1
  XPR=XB+F*XSCAL
  IF(A(I)-XPR) 50,50,70
C
C   FIND CROSS-VARIABLES
C
50 DO 55 IX=1,101
  55 OUT(IX)=BLANK
  DO 60 J=1,MY
    LL=L+J*M
    JP=(A(LL)-YMIN)/YSCAL+1.0
    OUT(JP)=ANG(J)
60 CONTINUE
C
C   PRINT LINE AND CLEAR, OR SKIP
C
WRITE(6,2)XPR,(OUT(IZ),IZ=1,101)
L=L+1
GO TO 90
70 WRITE(6,3)
80 I=I+1
  IF(I-NLL) 45, 84, 86
84 XPR=AIN)
  GO TO 50
C
C   PRINT CROSS-VARIABLES NUMBERS
C
86 WRITE(6,7)
  YPR(1)=YMIN
  DO 90 KN=1,9
    YPR(KN+1)=YPR(KN)+YSCAL*10.0
  YPR(11)=YMAX
  WRITE(6,8)(YPR(IP),IP=1,11)
  RETURN
  END

```

PLOT 490
PLOT 500
PLOT 510
PLOT 520
PLOT 530
PLOT 540
PLOT 550
PLOT 560
PLOT 570
PLOT 580
PLOT 590
PLOT 600
PLOT 610
PLOT 620
PLOT 630
PLOT 640
PLOT 650
PLOT 660
PLOT 670
PLOT 680
PLOT 690
PLOT 700
PLOT 710
PLOT 720
PLOT 730
PLOT 740
PLOT 750
PLOT 760
PLOT 770
PLOT 780
PLOT 790
PLOT 800
PLOT 810
PLOT 820
PLOT 830
PLOT 840
PLOT 850
PLOT 860
PLOT 870
PLOT 880
PLOT 890
PLOT 900
PLOT 910
PLOT 920
PLOT 930
PLOT 940
PLOT 950
PLOT 960
PLOT 970
PLOT 980
PLOT 990
PLOT1000
PLOT1010
PLOT1020
PLOT1030
PLOT1040
PLOT1050
PLOT1060
PLOT1070
PLOT1080
PLOT1090
PLOT1100
PLOT1110
PLOT1120
PLOT1130
PLOT1140
PLOT1150
PLOT1160
PLOT1170
PLOT1180
PLOT1190
PLOT1200
PLOT1210
PLOT1220
PLOT1230
PLOT1240
PLOT1250
PLOT1260
PLOT1270
PLOT1280
PLOT1290
PLOT1300
PLOT1310
PLOT1320
PLOT1330
PLOT1340
PLOT1350
PLOT1360
PLOT1370
PLOT1380
PLOT1390
PLOT1400
PLOT1410
PLOT1420
PLOT1430
PLOT1440
PLOT1450
PLOT1460

```

C
C   SUBROUTINE MATIN
C   PURPOSE
C   READS CONTROL CARD AND MATRIX DATA ELEMENTS FROM LOGICAL
C   UNIT 5
C   USAGE
C   CALL MATIN(ICODE,A,ISIZE,IROW,ICOL,IS,IER)
C   DESCRIPTION OF PARAMETERS
C   ICODE-UPON RETURN, ICODE WILL CONTAIN FOUR DIGIT
C   IDENTIFICATION CODE FROM MATRIX PARAMETER CARD
C   A -DATA AREA FOR INPUT MATRIX
C   ISIZE-NUMBER OF ELEMENTS DIMENSIONED BY USER FOR AREA A
C   IROW-UPON RETURN, IROW WILL CONTAIN ROW DIMENSION FROM
C   MATRIX PARAMETER CARD
C   ICOL-UPON RETURN, ICOL WILL CONTAIN COLUMN DIMENSION FROM
C   MATRIX PARAMETER CARD
C   IS -UPON RETURN, IS WILL CONTAIN STORAGE MODE CODE FROM
C   MATRIX PARAMETER CARD WHERE
C   IS=0 GENERAL MATRIX
C   IS=1 SYMMETRIC MATRIX
C   IS=2 DIAGONAL MATRIX
C   IER -UPON RETURN, IER WILL CONTAIN AN ERROR CODE WHERE
C   IER=0 NO ERROR
C   IER=1 ISIZE IS LESS THAN NUMBER OF ELEMENTS IN
C   INPUT MATRIX
C   IER=2 INCORRECT NUMBER OF DATA CARDS
C   REMARKS
C   NONE
C   SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C   LOC
C   METHOD
C   SUBROUTINE ASSUMES THAT INPUT MATRIX CONSISTS OF PARAMETER
C   CARD FOLLOWED BY DATA CARDS
C   PARAMETER CARD HAS THE FOLLOWING FORMAT
C   COL. 1- 2 BLANK
C   COL. 3- 6 UP TO FOUR DIGIT IDENTIFICATION CODE
C   COL. 7-10 NUMBER OF ROWS IN MATRIX
C   COL.11-14 NUMBER OF COLUMNS IN MATRIX
C   COL.15-16 STORAGE MODE OF MATRIX WHERE
C   0 - GENERAL MATRIX
C   1 - SYMMETRIC MATRIX
C   2 - DIAGONAL MATRIX
C   DATA CARDS ARE ASSUMED TO HAVE SEVEN FIELDS OF TEN COLUMNS
C   EACH. DECIMAL POINT MAY APPEAR ANYWHERE IN A FIELD. IF NO
C   DECIMAL POINT IS INCLUDED, IT IS ASSUMED THAT THE DECIMAL
C   POINT IS AT THE END OF THE 10 COLUMN FIELD. NUMBER IN EACH
C   FIELD MAY BE PRECEDED BY BLANKS. DATA ELEMENTS MUST BE
C   PUNCHED BY ROW. A ROW MAY CONTINUE FROM CARD TO CARD.
C   HOWEVER EACH NEW ROW MUST START IN THE FIRST FIELD OF THE
C   NEXT CARD. ONLY THE UPPER TRIANGULAR PORTION OF A SYMMETRIC
C   OR THE DIAGONAL ELEMENTS OF A DIAGONAL MATRIX ARE CONTAINED
C   ON DATA CARDS. THE FIRST ELEMENT OF EACH NEW ROW WILL BE
C   THE DIAGONAL ELEMENT FOR A MATRIX WITH SYMMETRIC OR
C   DIAGONAL STORAGE MODE. COLUMNS 71-80 OF DATA CARDS MAY BE
C   USED FOR IDENTIFICATION, SEQUENCE NUMBERING, ETC..
C   THE LAST DATA CARD FOR ANY MATRIX MUST BE FOLLOWED BY A CARD
C   WITH A 9 PUNCH IN COLUMN 1.
C
C   SUBROUTINE MATIN(ICODE, A,ISIZE,IROW,ICOL,IS,IER)
C   DIMENSION CARD(8)
C   1 FORMAT(7F10.0)
C   2 FORMAT(16,2I4,I2)
C
C   IDC=7
C   IER=0
C   READ(5,2)ICODE,IROW,ICOL,IS
C   CALL LOC(IROW,ICOL,ICNT,IROW,ICOL,IS)
C   IF(ISIZE-ICNT)6,7,7
C   6 IER=1
C   7 IF (ICNT)38,38,8
C   8 ICOLT=ICOL
C   IROCR=1
C
C   COMPUTE NUMBER OF CARDS FOR THIS ROW
C
11 IRCDS=(ICOLT-1)/IDC+1
  IF(IS-11)5,15,12
12 IRCDS=1
C
C   SET UP LOOP FOR NUMBER OF CARDS IN ROW
C
15 DO 31 K=1,IRCDS
  READ(5,1)(CARD(I),I=1,IDC)
C
C   SKIP THROUGH DATA CARDS IF INPUT AREA TOO SMALL
C
  IF(IER)16,16,31
16 L=0
C
C   COMPUTE COLUMN NUMBER FOR FIRST FIELD IN CURRENT CARD
C
  JS=(K-1)*IDC+ICOL-ICOLT+1
  JE=JS+IDC-1
  IF(IS-11)9,19,17
17 JE=JS
C
C   SET UP LOOP FOR DATA ELEMENTS WITHIN CARD
C
19 DO 30 J=JS,JE
  IF(J-ICOL)20,20,31
20 CALL LOC(IROCR,J,I,J,IROW,ICOL,IS)
  L=L+1
30 A(I,J)=CARD(I)
31 CONTINUE
  IROCR=IROCR+1
  IF(IROW-IROCR) 38,35,35
35 IF(IS-1)37,36,36
36 ICOLT=ICOLT-1
37 GO TO 11
38 READ(5,1) CARD(1)
  IF(CARD(1)-9.E)39,40,39
39 IER=2
40 RETURN
  END

```

MATI 10
MATI 20
MATI 30
MATI 40
MATI 50
MATI 60
MATI 70
MATI 80
MATI 90
MATI 100
MATI 110
MATI 120
MATI 130
MATI 140
MATI 150
MATI 160
MATI 170
MATI 180
MATI 190
MATI 200
MATI 210
MATI 220
MATI 230
MATI 240
MATI 250
MATI 260
MATI 270
MATI 280
MATI 290
MATI 300
MATI 310
MATI 320
MATI 330
MATI 340
MATI 350
MATI 360
MATI 370
MATI 380
MATI 390
MATI 400
MATI 410
MATI 420
MATI 430
MATI 440
MATI 450
MATI 460
MATI 470
MATI 480
MATI 490
MATI 500
MATI 510
MATI 520
MATI 530
MATI 540
MATI 550
MATI 560
MATI 570
MATI 580
MATI 590
MATI 600
MATI 610
MATI 620
MATI 630
MATI 640
MATI 650
MATI 660
MATI 670
MATI 680
MATI 690
MATI 700
MATI 710
MATI 720
MATI 730
MATI 740
MATI 750
MATI 760
MATI 770
MATI 780
MATI 790
MATI 800
MATI 810
MATI 820
MATI 830
MATI 840
MATI 850
MATI 860
MATI 870
MATI 880
MATI 890
MATI 900
MATI 910
MATI 920
MATI 930
MATI 940
MATI 950
MATI 960
MATI 970
MATI 980
MATI 990
MATI1000
MATI1010
MATI1020
MATI1030
MATI1040
MATI1050
MATI1060
MATI1070
MATI1080
MATI1090
MATI1100
MATI1110
MATI1120
MATI1130
MATI1140
MATI1150
MATI1160
MATI1170
MATI1180
MATI1190
MATI1200
MATI1210
MATI1220
MATI1230
MATI1240
MATI1250



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